Methods in Irradiation Experiment Modelling Luka Snoj

Joint ICTP/IAEA Workshop "Research Reactors for Development of Materials and Fuels for Innovative Nuclear Energy Systems" 6-10 November 2017, ICTP, - Trieste, Italy





Outline

- Why modelling
- Building a computational model
- Verification and validation of a computational model
- Monte Carlo calculations
- Nuclear data
- Summary

About myself

- 2009 Ph D in Nuclear engineering, Faculty of mathematics and physicis, University of Ljubljana
- 2010, 2012, postdoc at Culham Centre for fusion energy, JET
- 2014+ Head of the Reactor physics division at the Jozef Stefan Institute, Ljubljana, Slovenija
- Theoretical and experimental reactor physics related to practical applications in power and research reactors, in particular:
 - integral reactor experiments, criticality experiments and calculations
 - evaluation of critical and other reactor physics experiments
 - Monte Carlo transport of neutrons and photons in fission and fusion nuclear reactors

Why modelling

• Experiments

- expensive (t & €) !
- Difficult to perform with low uncertainty
- Sometimes impossible to perform
- Calculations
 - Relatively cheap (t & €)
 - Relatively easy to perform
 - Practically everything can be calculated
 - Reliability, validity !!!

Neutron transport calculations

- deterministic codes
 - based on numerical or rarely analytical solving of neutron transport or diffusion equation
 - the computing errors are systematic
 - uncertainties in the cross section data
 - discretization of time-space-energy phase space
 - geometrical simplifications
 - computationally cheap → PC
- Monte Carlo codes
 - capable of treating very complex three-dimensional configurations
 - continuous treatment of energy, as well as space and angle → eliminates discretization errors
 - the computing errors are systematic and random
 - uncertainties in the cross section data (systematic)
 - other uncertainties (random)
 - computationally expensive → need for large computer clusters

Building a reactor model

- first step is to collect
 - material
 - geometry
 - operational data of the reactor
- the task is not trivial if we try to collect *"as built"* and not just typical or generic data of particular reactor
- the set of data required for the calculation depends also on
 - the computer code
 - the problems which is solved
 - Diffusion codes require only general reactor geometry and dimensions
 - Monte Carlo codes require detailed geometry and materials

Building a model: an example

• JSI TRIGA

TRIGA Mark II: side view



TRIGA Mark II: top view



TRIGA Mark II: reflector



Dimensions in cm

C98 0953

TRIGA Mark II: core



TRIGA Mark II: fuel element



All dimensions are in cm

Dimension in cm

Triga: Fuel rod types

Physical characteristics				
	fuel		cladding	
material	U-ZrH _x		stainless steel	
inner diameter	0.635 cm		3.703 cm	
outer diameter	3.645 cm		3.754 cm	
length	38.10 cm		-	
Fuel material composition				
fuel rod (FR) name	8.5 FR	12 FR	20 FR	30 FR
U concentration [w/o]	8.5	12	20	30
U-ZrH _x mass [g]	2235	2318	2462	2500
U enrichment	20	20	20	20
H:Zr	1.6	1.6	1.6	1.6
²³⁵ U mass [g]	38	55.6	99	150
Er concentration [w/o]	0	0	0.44	0.6

Computational model

- room temperature (T = 20 °C)
- fresh fuel (BU = 0 MWd)
- continuous energy scale



Computational model- top view



Computational model- side view



- Rotary groove
- Graphite
 Reflector
- Fuel element
- Irradiation channels
- water



Verification and validation of the model

- the calculated result is valuable only if we know:
 - reliability
 - uncertainty
- user of any computer code should not only know how the code works but has to be familiar also with the validity and the limitations of the code
- VERIFICATION check that the code does what is expected to do
- VALIDATION one has to compare the calculated results with experiments to verify the results
- verification and validation (V&V) the most important part of reactor calculations

Approach

- Make a detailed computational model of the TRIGA reactor in MCNP (later TRIPOLI, SERPENT, OPENMC)
- Validate calculation by measurements
- Use the validated model for safety analyses and to support experimental campaigns
 - Absolute neutron flux
 - Neutron flux spectra
 - Dose rates
 - Gamma flux and dose

Criticality benchmark core



Core 132

- fuel element
- regulating rod
- C shim rod
- src source element
- S safety rod
- transient rod Т
- vacant fuel-rod position (water)

SIC

Core 133

S

R

C98 0956

benchmark core k_{eff} comparison



Neutron flux distribution measurements Foils: Al (99.9 w/o)-Au (0.1 w/o) T_{irr} = 73 min at 250 kW



Results - core



Results – carrousel facility



Neutron spectrum measurements

- 4 irradiation channels (1 core centre, 2 core periphery, 1 carrousel facility in the reflector)
- The neutron spectrum adjustments performed by the JSIdeveloped code GRUPINT based on the dosimetry library IRDFF
- monitors
 - Al (99.9 w/o)-Au (0.1 w/o)
 - Ni (80.93 w/o)- Mo (15.16 w/o)-W (2.76 w/o)- Mn (0.41 w/o)- Au(0.29 w/o)
 - Zr (99.8 w/o)
 - Zn (99.99 w/o)
- reactions
 - ²⁷Al(n,α), ²⁷Al(n, γ), ¹⁹⁷Au(n,γ)
 - ⁵⁸Ni(n,p), ⁹²Mo(n,p), ⁶⁴Ni(n,γ), ⁹⁸Mo(n,γ), ¹⁰⁰Mo(n,γ), ⁵⁵Mn(n,γ), ¹⁸⁶W(n,γ), ¹⁹⁸Au(n,γ)
 - ⁹⁰Zr(n,p), ⁹⁰Zr(n,2n), ⁹⁴Zr(n, γ), ⁹⁶Zr(n, γ)
 - ⁶⁶Zn(n,p), ⁶⁴Zn(n,γ), ⁶⁸Zn(n,γ), ⁷⁰Zn(n,γ)





Reaction rate profile measuremenmts

- Absolutely calibrated fission chamber (CEA)
 - 98.49 % enriched ²³⁵U
 - Sensitive height ~4 mm
 - Diameter ~3 mm
- Au wires (JSI)
 - Al (99.9 w/o)-Au (0.1 w/o)
 - Activity measurements performed at JSI

Experimental setup 1







FISSION RATE AXIAL SCANS

Fission chamber

²³⁵U (98.5 %)

Reactor power:

100 W



FISSION RATE AXIAL SCANS

Fission chamber ²³⁸U (99.964 %)

Reactor power:

1000 W



Au wires EXPERIMENT

- Validational experiment using probes with Au wires
- Axial profiles of ${}^{197}Au(n,\gamma) {}^{198}Au$ reaction rates







 Experimental and calculational Au reaction rates with relative discrepancies



Monte Carlo neutron transport

- Monte Carlo codes
 - MCNP, KENO, SERPENT, TRIPOLI, MCBEND, MONK, PHITS, OPENMC, SUPERMC, TART, COG, MCU,....
- Solving particle transport problems with the Monte Carlo method is simple – just simulate the particle behavior
- the problem lies in details: how to calculate reactor parameters, which are usually defined by deterministic (transport or difussion) methods

Monte Carlo simulation

- faithfully simulate the history of a single neutron from birth to death
- random walk for a single particle
 - model collisions using physics equation & cross section data
 - model free-flight between collisions using computational geometry
 - tally the occurrences of events (absorption, scattering, fission, track length,..) in each region
 - save any secondary particles, analyze them later


Neutron random walk



Monte Carlo histories

- Monte Carlo method for particle transport consists of simulating a finite number, say N, of particle histories through the use of a random number.
- In each particle history random numbers are generated and used to sample appropriate probability distributions for scattering angles, track length distances between collisions etc.
- N ~ 10⁶ 10¹²



Jozef Stefan Institute, Reactor Physics Division

Particle tracks – water



Particle tracks – graphite









Mesh tally

- very useful for calculation of
 - neutron flux distribution
 - power distribution
 - reaction rate distribution
- a mesh of cells is superimposed over the problem geometry
- useful also for
 - checking results
 - plotting problem geometry (advanced option)



Mesh tally – sample results



Jozef Stefan Institute, Reactor Physics Division











Neutron flux spectrum



Gamma spectrum (0 – 3.3) MeV



Gamma spectrum (3.3-6.6) MeV



Nuclear data

reaction rate = $\sigma \varphi = \int \sigma(E) \varphi(E) dE$

Source: <u>https://www-nds.iaea.org</u>



Flux to dose conversion factors



DPA –displacement per atom



https://www-nds.iaea.org/dpa/

Conclusion

- RR calculations
 - Reduce time required to optimise experiments
 - Provide insight into reactor physical parameter not possible by experiments
 - Provide large amounts of data in relatively short time
- RR codes and models should be verified and validated by experiments

RR simulator



- WWW: <u>http://reactorsimulator.ijs.si</u>
- @: reactor-simulator@ijs.si

Additional slides

Jožef Stefan Institute TRIGA reactor

- 1st criticality: 31st May, 1966
- P_{max}
 - 250 kW (steady state)
 - 1 GW (pulse)
- Fuel rod
 - UZrH (m~2300 g)
 - 12 wt. % U
 - 20 % enriched U
 - (m (²³⁵U) ~ 56 g)
 - SS cladding (h = 55cm, r = 1.8 cm)





TRIGA Mark II Reactor Ljubljana



- 1st criticality: 31st May, 1966
- P_{max}
 - 250 kW (steady state)
 - 1 GW (pulse)
- Fuel
 - UZrH (12 wt. % U)
 - E= 20 %



Present utilisation

- research
 - verification and validation of computer codes and nuclear data – experimental benchmarks
 - testing and development of experimental equipment used for core physics tests at the Krško Nuclear Power Plant
 - testing of nuclear instrumentation (SPND, SPGD, miniature FC)
 - radiation hardness studies
- neutron activation analysis
- training (domestic + international courses)

Radiation hardness studies

• since 2001

- ~2000 samples/y, CERN, DESY, KEK and various universities and institutes.
- Neutron and gamma testing







Advanced European Infrastructures for Detectors at Accelerators



a standard or point of reference against which things may be compared

verb

evaluate (something) by comparison with a standard.

Jozef Stefan Institute, Reactor Physics Division

Experiment can serve as benchmark experiment, if performed with relatively low uncertainty

 Monte Carlo results can serve as benchmark for diffusion and/or transport codes



Jozef Stefan Institute, Reactor Physics Division



Jozef Stefan Institute, Reactor Physics Division

Uncertaities

- Experiment
 - Measurement (measured physical quantity)
 - Material
 - Geometry
 - Temperature
 - other
- Calculation
 - Statistical
 - Nuclear data (cross section, emission spectra, Q values,...
 - other

Sensitivity studies

$$\sigma_i = \frac{dk}{dP_i} \sigma_{P_i}, \quad \frac{dk}{dP_i} \equiv \text{sensitivity coefficient}$$

Jozef Stefan Institute, Reactor Physics Division

biases

- Mostly due to simplifications
 - Geometry
 - Materials
 - Computational methods
 - Other...
- Bias also has features uncertainty

Benchmark model

- Model of the experiment suitable for computatonal modelling – can be simplified
- Benchmark model uncertainty
 - Experimental uncertainty + bias uncertainty
- Computational uncertainty
 - Statistical uncertainty + nuclear data uncertainty


Uncertainties explained









Data sources

- All relevant geometry and material data should be in principle contained in the Final Safety Analysis Report (FSAR) of the reactor. In practice, only part of these information is found there.
- It is also not very reliable and accurate since the, reactor description in SAR is often based on generic and not on "as built" data.
- The most reliable source of practical data is the design documentation of the reactor (plans, blueprints, drawings, fabrication specifications). It contains normally detailed data on geometry but only general data on material specifications.

Material data

- The material data are normally found in internal reports of the reactor manufacturer or in general literature
- Such data are, however, also mainly generic and normally approximately correspond to the particular case.
- The exception are the data about the enrichment and mass of uranium which are part of the safeguard documentation and are for this reason in details provided together with the fuel elements.
- The rest of the material data (e.g, material density, metallurgical composition in case of alloys, impurities important for neutrons, concentration of burnable poisons, ...) are normally not available for the particular reactor, especially if the reactor is old.