



# Cathode Catalyst Layers in PEFC: The Major Competitive Ground

Kourosh Malek, Jianfeng Liu, Michael Eikerling

Conference on Physics of Fuel Cells  
ICTP Trieste, May 21-25, 2007

Funding:



NISSAN  
Motor  
Corp.

## Outline

### I. Introduction

- Why focus on CCL?
- The major competitive ground...

### II. Self-Organization in Catalyst Layers

### III. Structural Picture and Model of Water Balance

- Three State Model: **watershed**
- Full Coupling: **mass transport vs. partial saturation**
- Steady State Diagram: **bistability**
- Parameter Study: **optimization**

### IV. Conclusions

## I. Why focus on catalyst layer?

“Go for the messes – that’s where the action is!”

S. Weinberg, *Scientist: Four golden lessons*, Nature 426, 389, 2003.

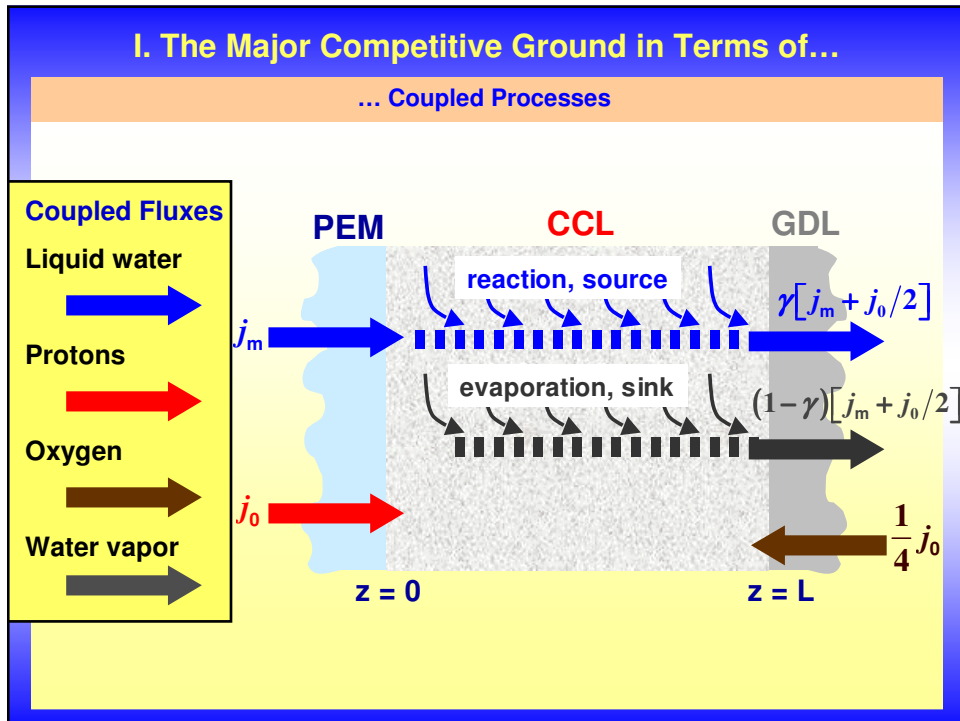
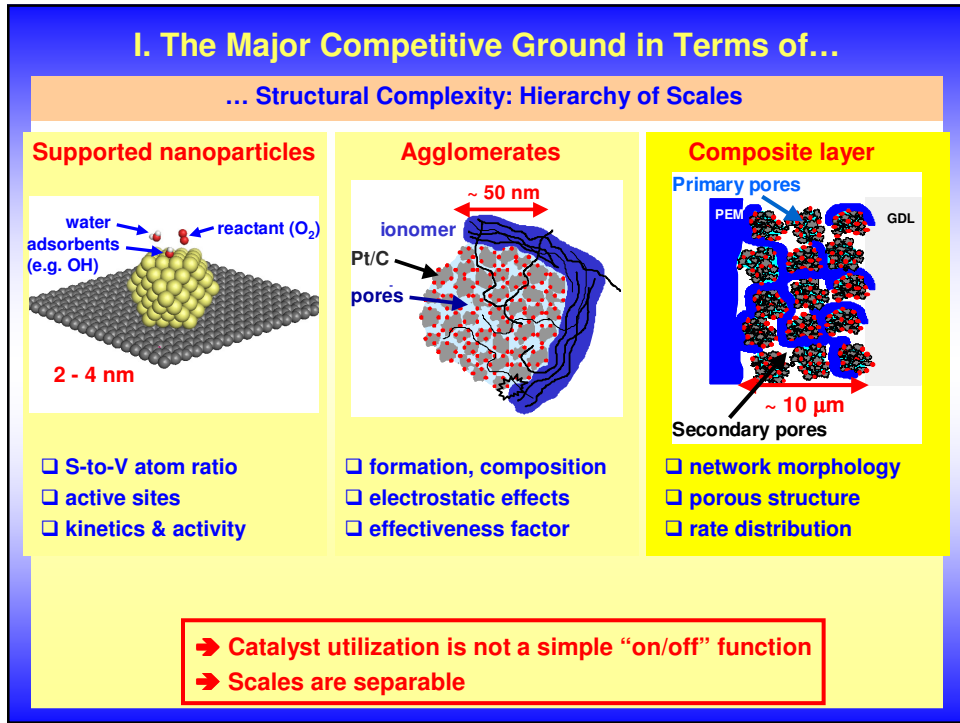
- Price and abundance of Pt: feasibility of PEFC
- Key importance for operation, performance, and design
- Randomness at multiple scales**
- Lack in systematic understanding & controversial issues
- Modeling: percolation, agglomerates, macrohom. approach

- From optimizing randomness towards rational design!
- High electrocatalytic activity with minimal amount of Pt

## I. Controversial Issues

- Assessment of catalyst utilization (diagnostics)
  - no “straightforward” technique
- Nature of electrocatalytically active interfaces
  - Pt|ionomer, Pt|liquid water or Pt|vapor?
- Distribution, structure and function of ionomer
  - needed or abundant?
- Distribution, structure and function of water
  - reaction product, proton solvent and asphyxiant
- Role of porous structure and liquid water accumulation
  - formation – steady state operation – degradation

How good are the currently used CCL?



## I. The Major Competitive Ground in Terms of...

... Performance Optimization

$$j^0 = [m_{Pt}] 2 \cdot 10^3 j^{0*} \epsilon^{S/V} \Gamma_a g(S_r) \frac{f(X_{PtC}, X_{el})}{X_{PtC}}$$

Exchange  
current  
density

## I. Optimization Problem

large

$$j^0 = [m_{Pt}] 2 \cdot 10^3 j^{0*} \epsilon^{S/V} \Gamma_a g(S_r) \frac{f(X_{PtC}, X_{el})}{X_{PtC}}$$

Exchange  
current  
density

small

Losses in voltage efficiency – three causes:

- activation losses of kinetic processes
- statistical inhomogeneity
- non-uniformity of reaction rate distribution

## I. Optimization Problem

$$j^0 = [m_{\text{Pt}}] 2 \cdot 10^3 j^{0*} \epsilon^{S/V} \Gamma_a g(S_r) \frac{f(X_{\text{PtC}}, X_{\text{el}})}{X_{\text{PtC}}}$$

Exchange  
current  
density

### Electrocatalysis

- experiments on model catalysts
- electronic structure calculations

#### Systematic trends due to

- particle size (active sites)?
- shape, composition?
- surface structure?
- substrate effects?

→ activation losses

## I. Optimization Problem

$$j^0 = [m_{\text{Pt}}] 2 \cdot 10^3 j^{0*} \epsilon^{S/V} \Gamma_a g(S_r) \frac{f(X_{\text{PtC}}, X_{\text{el}})}{X_{\text{PtC}}}$$

Exchange  
current  
density

### Electrocatalysis

- experiments on model catalysts
- electronic structure calculations

#### Systematic trends due to

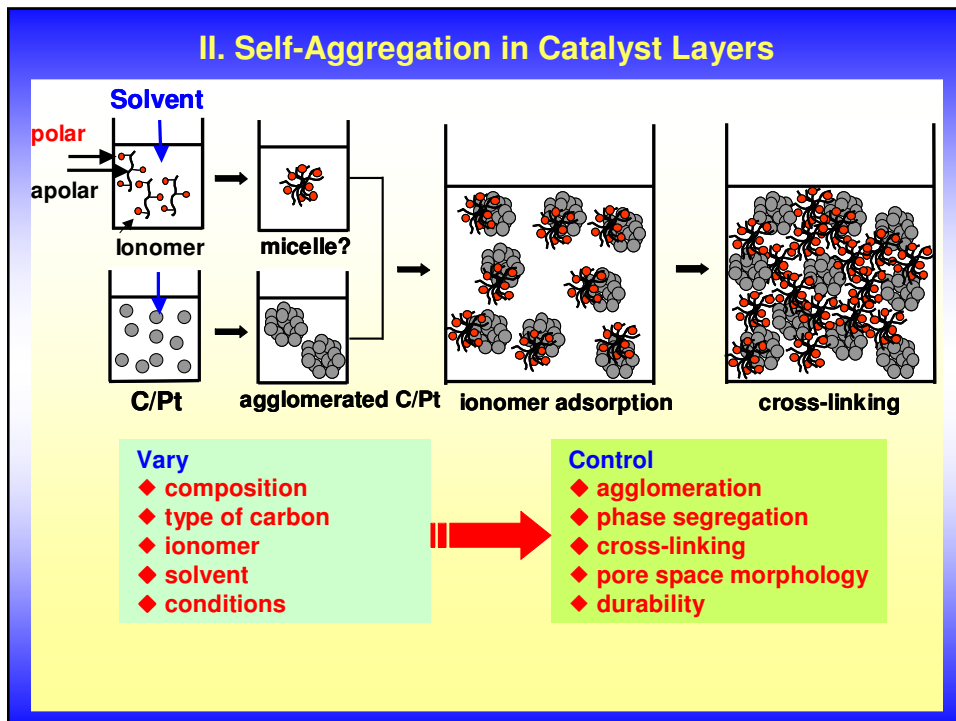
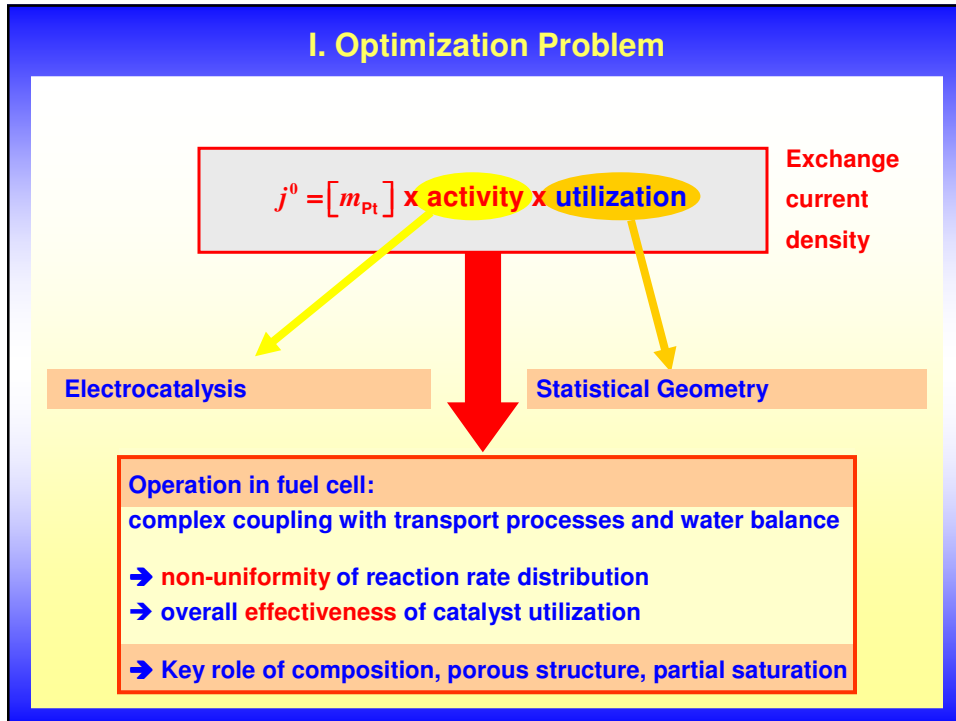
- particle size (active sites)?
- shape, composition?
- surface structure?
- substrate effects?

→ activation losses

### Statistical Geometry

- particle size effects  
(surface-to-volume atom ratio)
- phase segregation, agglomeration  
(electrostatic effects)
- triple phase boundary  
(percolation effects)
- porous structure, partial saturation

→ statistical spatial inhomogeneity

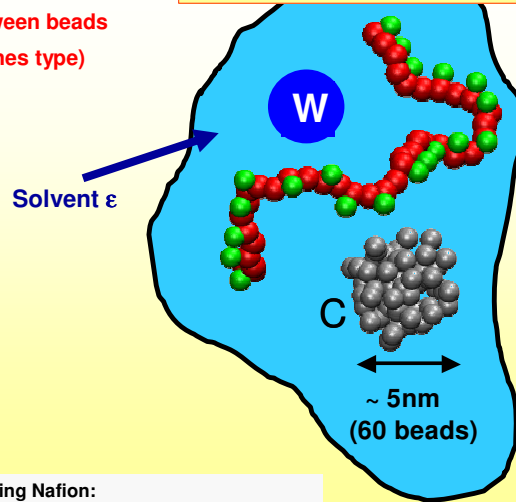


## II. Computational Modeling with Coarse-grained MD

### Systems at micro-to-meso level

- replace components by spherical beads
- renormalized interactions between beads (pair potentials of Lennard-Jones type)

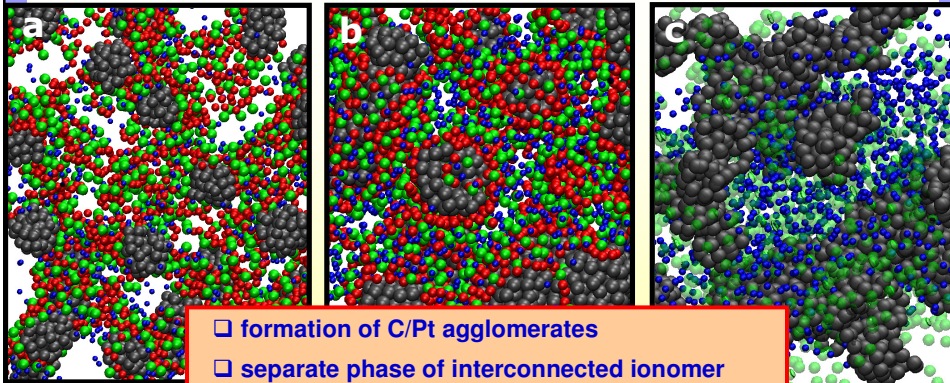
Coarse-grained model of Nafion, 20-unit oligomer, length ~ 30 nm



Coarse-grained approaches for simulating Nafion:  
 J. T. Wescott et al. 2006, J. Chem. Phys., 124, 134702.  
 D. Y. Galperin, A. R. Khokhlov 2006, Macromol. Theory and Simul. 15, 137.

## II. Formation of Phase-Segregated CCL Morphology

Annealed structure ..... → Equilibrated structure



- formation of C/Pt agglomerates
- separate phase of interconnected ionomer
- ionomer backbones attached to C
- no penetration of ionomer into agglomerates!

K. Malek, M. Eikerling, Q. Wang,  
 T. Navessin, and S. Liu, JPC B, accepted.

### III. Effects of Composition and Liquid Saturation

$$j^0 = [m_{Pt}] 2 \cdot 10^3 j^{0*} \varepsilon^{S/V} \Gamma_a g(S_r) \frac{f(X_{PtC}, X_{el})}{X_{PtC}}$$

Interpenetrating networks – volume portions:

$$X_{PtC}, X_{el}, X_p = 1 - X_{PtC} - X_{el}$$

Liquid saturation:  $S_r = \frac{1}{X_p} \int_0^r dr' \frac{dX_p(r')}{dr'}$

Mesoscopic scale:

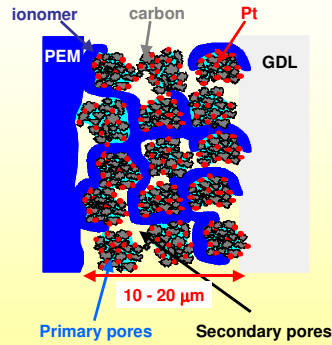
fraction of wetted Pt  $g(S_r) \leq 1$

Macroscopic scale:

triple-phase boundary  $\frac{f(X_{PtC}, X_{el})}{X_{PtC}} \leq 0.3$

Statistical limit of catalyst utilization in random composites

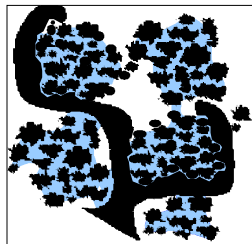
20-25%



M. Eikerling, A.S. Ioselevich, A. A. Kornyshev, *Fuel Cells* 4, 131 (2004).  
 M. Eikerling, *J. Electrochem. Soc.* 153, E58 (2006).

### III. Effects of Porous Structure and Water Balance

Partially saturated porous medium



activity vs. transport

Two-level approach

composition & structure

effective properties (in REV)

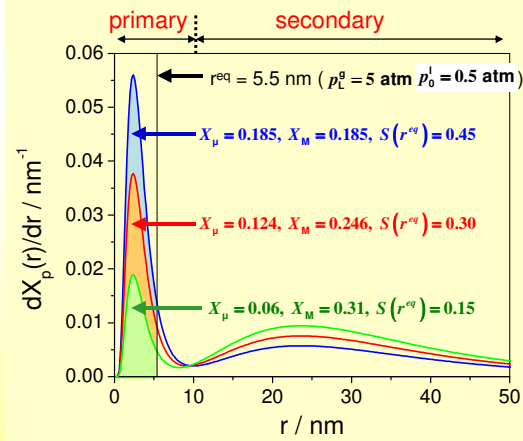
performance

M. Eikerling, *J. Electrochem. Soc.* 153, E58 (2006).



### III. From Structural Picture to Model of Water Balance

Bimodal log-normal pore size distribution



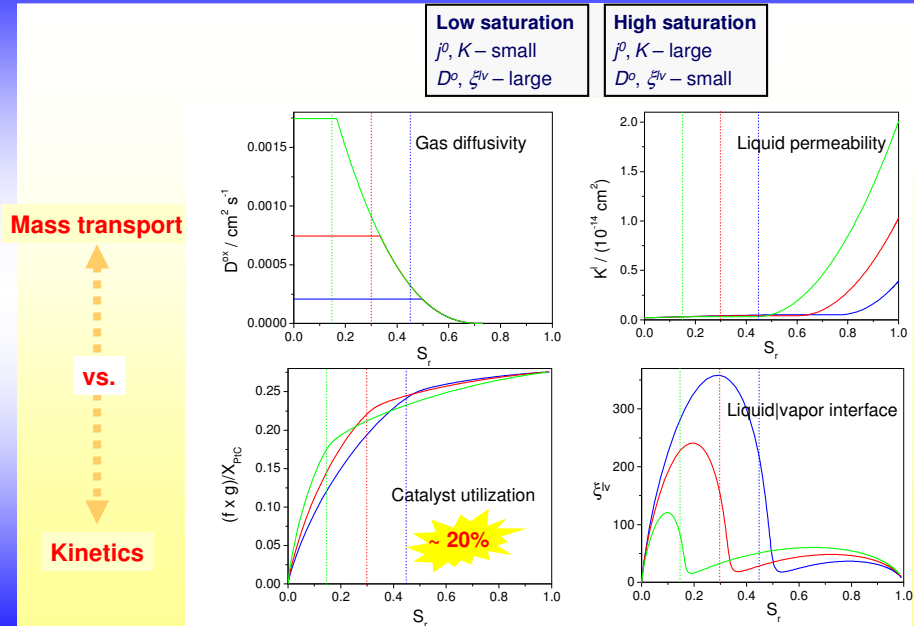
Capillary equilibrium controls pore filling – significance of wetting angle



$$p^c = \frac{2\sigma \cos(\theta)}{r_c} = p^g - p^l$$

Laplace eq.

### III. Effective Properties



### III. Transport and Reaction in CCL – Conservation Laws

General form of the continuity equation:  ~~$\frac{\partial \rho(\vec{r}, t)}{\partial t} + \nabla \cdot \vec{j}(\vec{r}, t) = Q(\vec{r}, t)$~~

Consider steady state operation, neglect gas convection:

$\phi$  – el. potential  $\frac{d^2 \phi(z)}{dz^2} = \frac{1}{\sigma_{el}} Q^{ec}(z)$

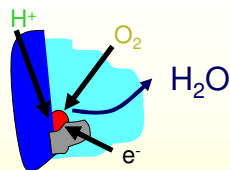
$p$  – ox. pressure  $4fD^o(S_r) \frac{dp(z)}{dz} = j_o - j^p(z)$

$q$  – vapor press.  $-f \frac{d}{dz} \left[ D^v(S_r) \frac{dq(z)}{dz} \right] = Q^{lv}(z)$

$p^l$  – liquid press.  $\frac{F}{V_m \mu^l} K^l(S_r) \frac{dp^l(z)}{dz} = \left( n + \frac{1}{2} \right) j^p(z) + j^v(z) - j_m - \frac{j_o}{2}$

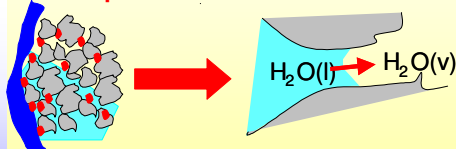
### III. Source Terms

Electrochemical source term



$$Q^{ec}(z) = \frac{j^0(S_r)}{L} \frac{p(z)}{p_L} \exp(\alpha f \phi(z))$$

Vaporization source term

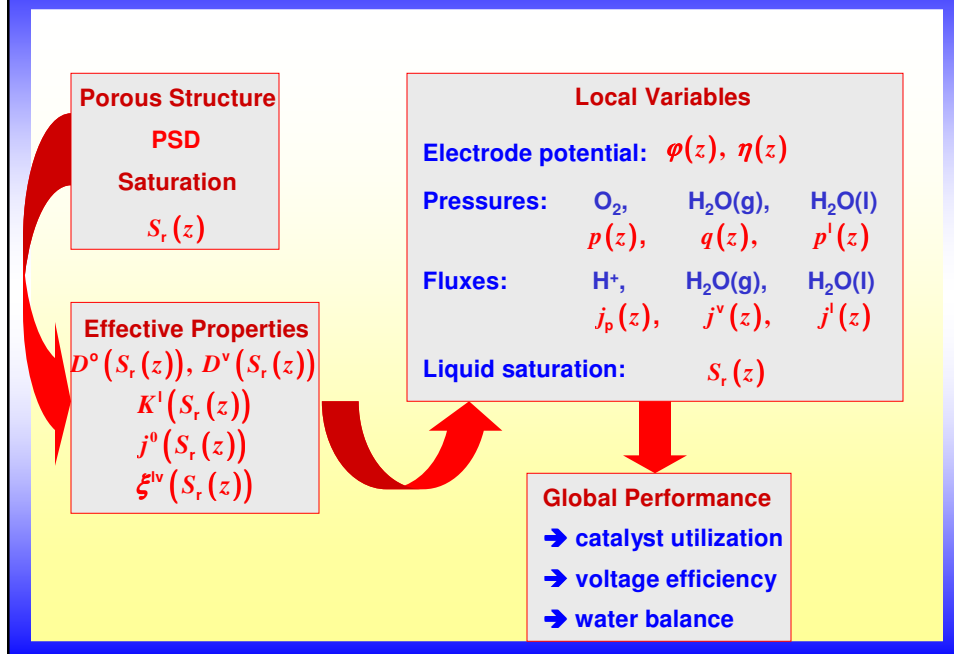


$$Q^{lv}(z) = \frac{\epsilon_0 K^e}{L} \xi^{lv}(S_r) \{q_r^s(T) - q(z)\}$$

with saturated vapor pressure (Kelvin equation)

$$q_r^s(T) = q^{s,\infty}(T) \exp\left(-\frac{2\sigma \cos(\theta) V_m}{RT r_c}\right), \quad q^{s,\infty}(T) = q^0 \exp\left(-\frac{E_a}{k_B T}\right)$$

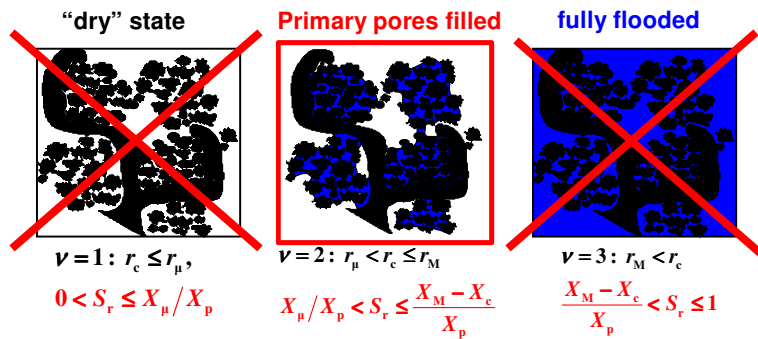
### III. Modeling Strategy: Two Main Steps



### III. Previous Results: Three State Model

Simplistic psd ( $\delta$ -distribution):

$$\frac{dX_p(r)}{dr} = X_\mu \delta(r - r_\mu) + X_M \delta(r - r_M)$$



Constant coefficients in each state! – Analytical solutions can be obtained.

Focus on operation in intermediate state.

### III. Three State Model: Main Insights

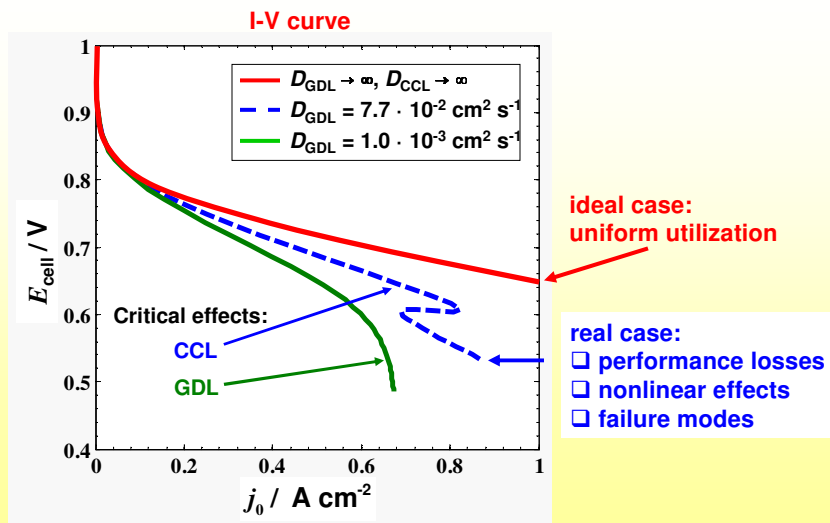
CCL acts like a watershed in the cell

- controls water fluxes and vaporization in PEFC
- prone to flooding at relevant current densities
- porous structure and liquid saturation are key

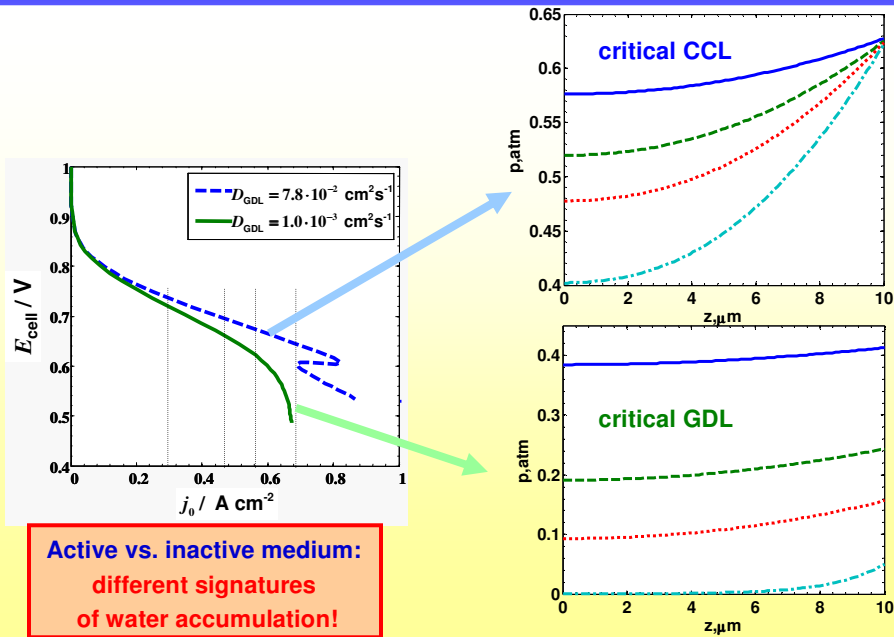
Sensitive dependences of performance on parameters

- **structure:** thickness, psd, wetting angle
- **operation:** water flux from PEM, gas/liquid pressures

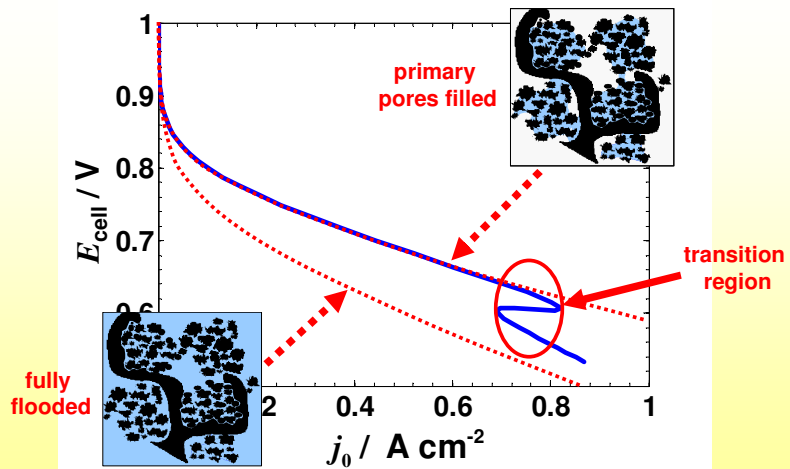
### III. Full Coupling: Water Formation – Where?



### III. Oxygen Distribution in CCL

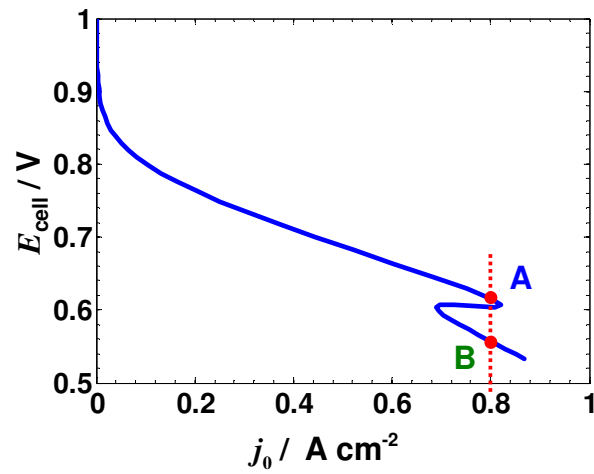


### III. Current-Voltage Curve

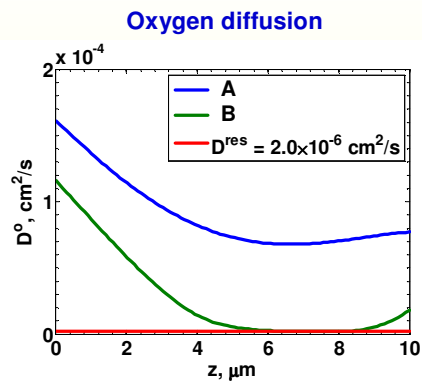
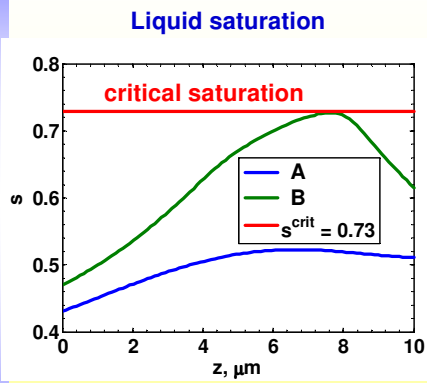


... interplay between liquid saturation and oxygen starvation!  
Effect of nonuniform, critical liquid water formation!

### III. Transition Region: Steady State Multiplicity

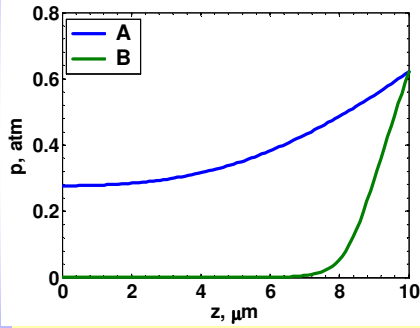


### III. Transition Region: Coexisting States

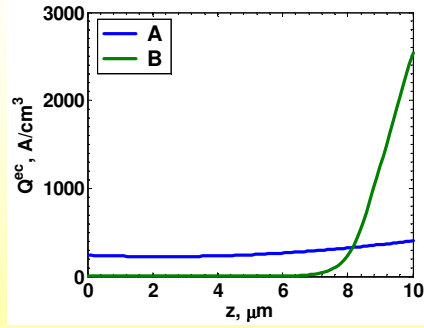


### III. Transition Region: Coexisting States

Oxygen partial pressure

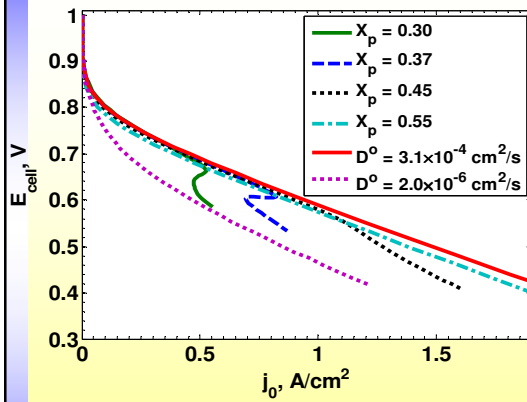


Reaction rate distribution



Transition from uniform to non-uniform reaction rate distribution due to coupling between liquid water saturation and oxygen transport

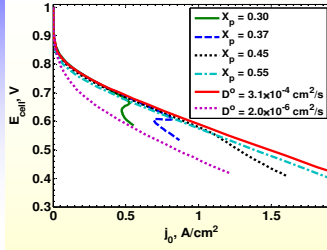
### III. Parameter Study: Total Porosity



Total porosity > 45% sufficient

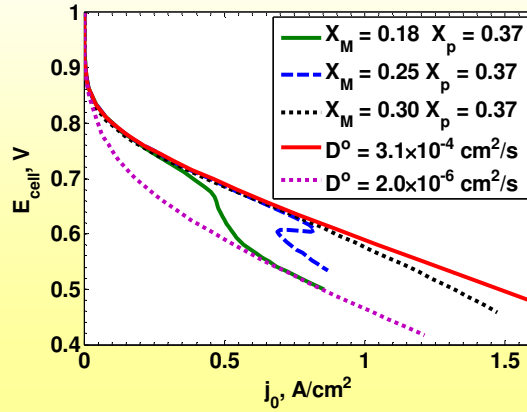
### III. Parameter Study: Pore Space Morphology

#### Total porosity

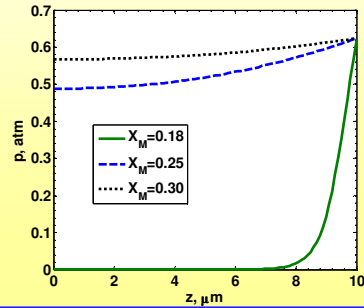
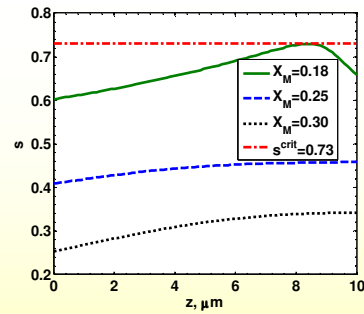
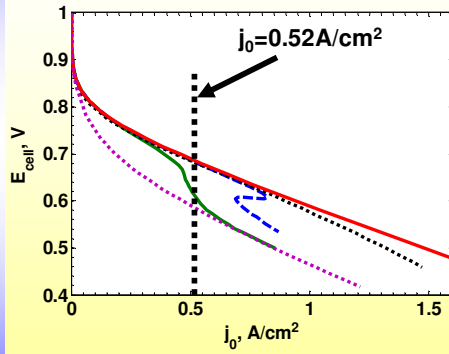


Secondary pores  
(between agglom.)  
are vital

#### Volume fraction of secondary pores

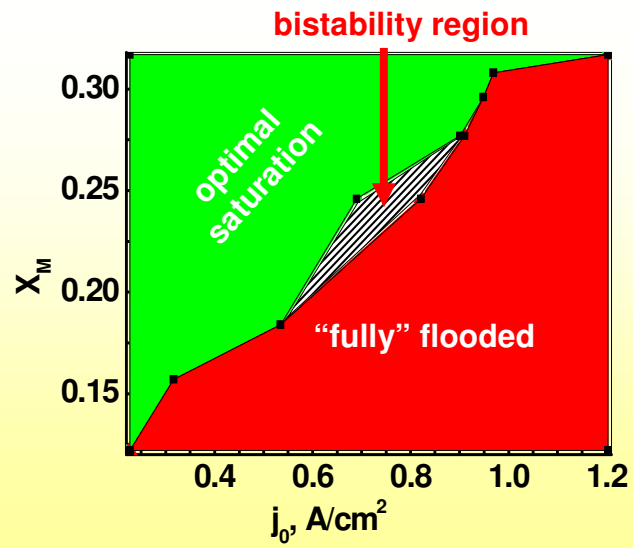


### III. Parameter Study: Pore Space Morphology



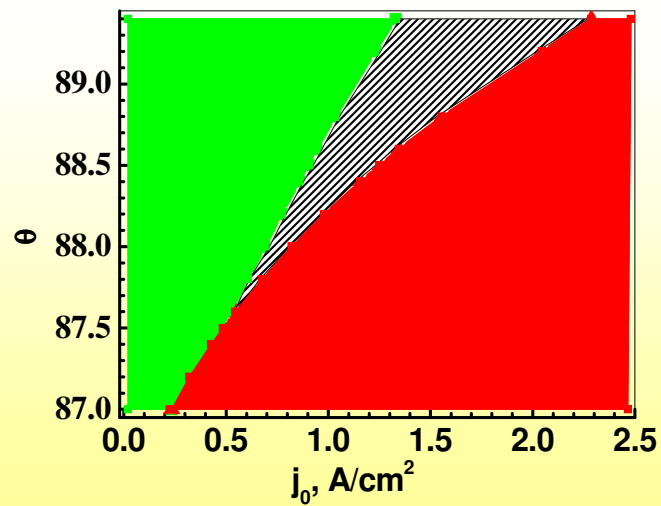


### III. Steady State Diagram – Fraction of Second. Pores



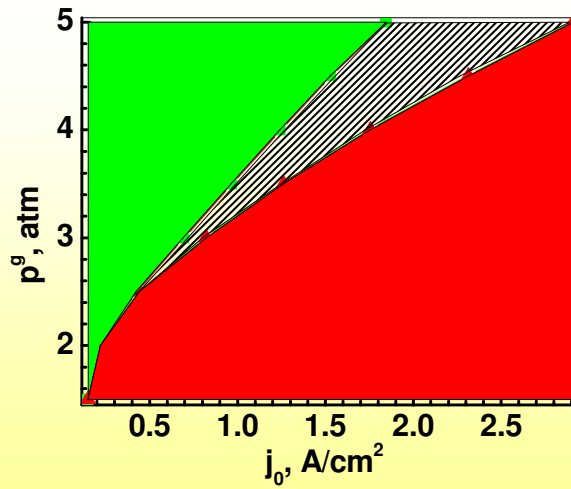
→ tool for evaluating CCL design

### III. Steady State Diagram: Wetting Angle

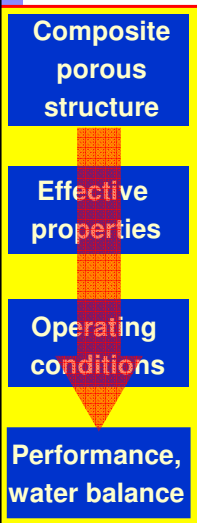


Important parameter – difficult to control!

### III. Steady State Diagram: Total Gas Pressure



### III. Main Results



#### Role of bimodal psd: controls distinct functions

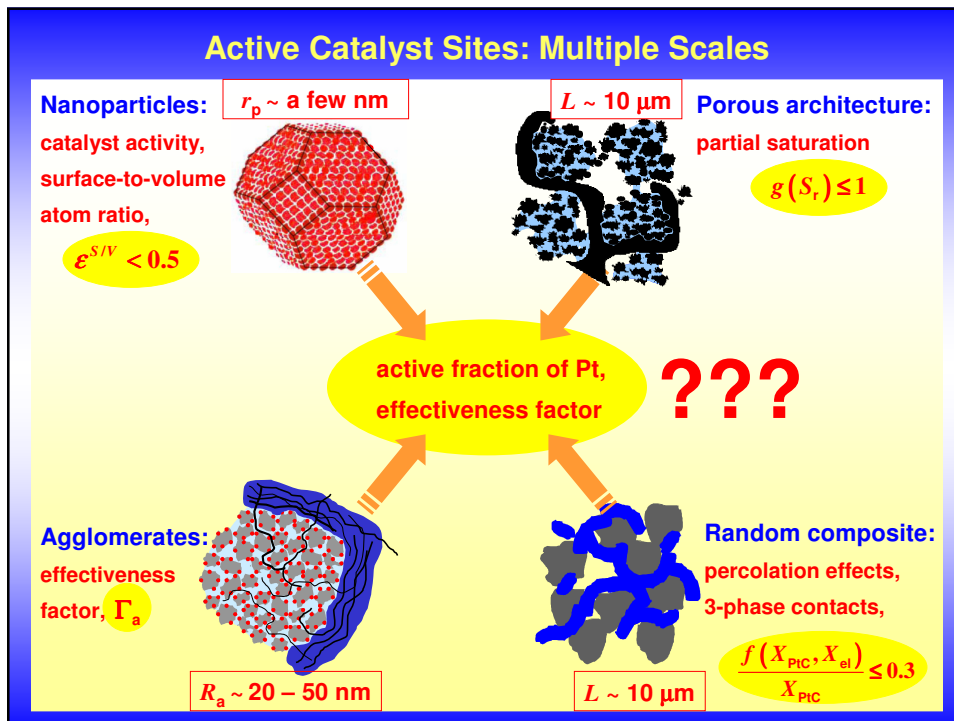
- small pores: active area → hydrophilic
- large pores: mass transport & water balance → hydrophobic
- affects uniformity of reaction rate distribution

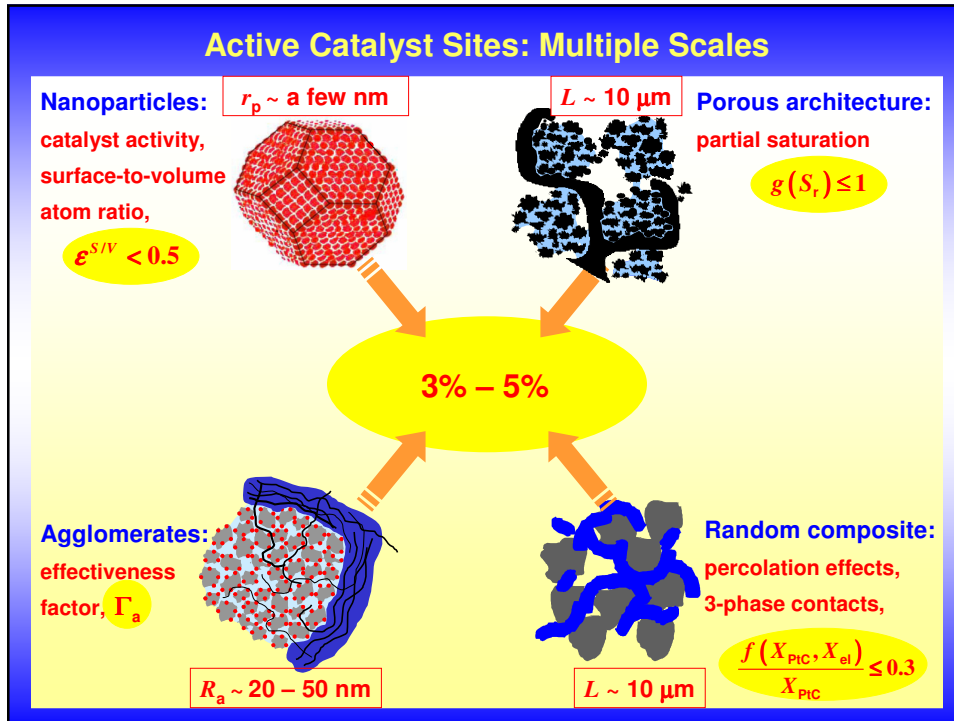
#### Interplay between oxygen transport and water accumulation

- distinct signatures of CCL and GDL
- critical conditions in CCL: bistability in I-V curves
- main parameters:  $X_M$ ,  $X_p$ ,  $\theta$ ,  $p^g$

## IV. Outlook

- ❑ Theoretical understanding: water accumulation vs. mass transport
- ❑ More detailed characterization of wetting properties
- ❑ Water distribution and structure (surface – bulk, ionomer - pores)
- ❑ Validate and refine parameterization of effective properties
- ❑ Coupling to water balance in other components
- ❑ Evaluate CCL design options
  - ➔ improvement of current design?
  - ➔ radically new design?
  - ➔ **don't forget about porous structure and water balance**
- ❑ Linking the scales: from structure formation to performance





### Reference Parameters Used in Calculations

$L, \mu\text{m}$	10	Thickness of CCL	
$L_{PTL}, \mu\text{m}$	125	Thickness of PTL	
$X_{pic}$	0.3	Volume fraction of Solid phase	
$X_{el}$	0.33	Volume fraction of electrolyte	
$X_p = 1 - X_{pic} - X_{el}$	0.37	Volume fraction of void space	
Psd#2	$X_\mu$	0.124	Volume fraction of primary pores
	$X_M$	0.246	Volume fraction of secondary pores
$T, ^\circ\text{C}$	60	Temperature	
$p^g, \text{atm}$	3.0	Total gas pressure	
$p_{GDL}, \text{atm}$	0.63	Oxygen pressure	
$\theta, \text{deg}$	88	Contact angle of pore and water system	
$D^{res}, \text{cm}^2 / \text{s}$	$2.0 \times 10^{-6}$	Residual gas diffusivity	