



**The Abdus Salam
International Centre for Theoretical Physics**



2031-1

**Joint ICTP/IAEA School on Novel Synchrotron Radiation
Applications**

16 - 20 March 2009

Powder Diffraction - Overview and Applications

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Joint ICTP/IAEA School on Novel Synchrotron Radiation Applications
Trieste, March 16-20, 2009

Powder Diffraction

overview and applications

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University of Trento





PRESENTATION OUTLINE

PART 1

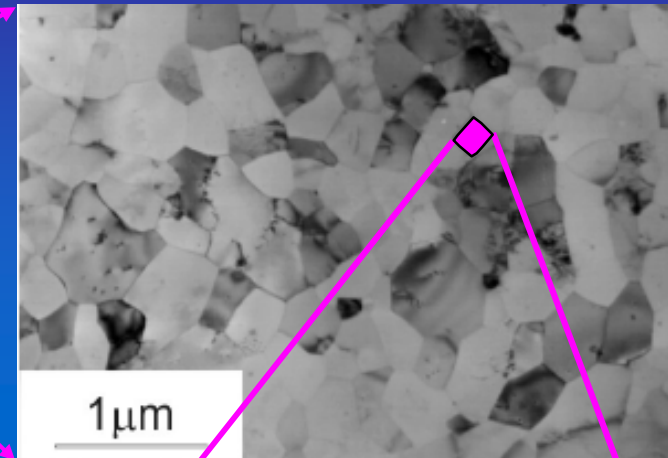
- Basic elements of crystallography and X-ray diffraction (XRD) theory
 - Some advantages and peculiarities of synchrotron radiation XRD (SRXRD)
-

PART 2

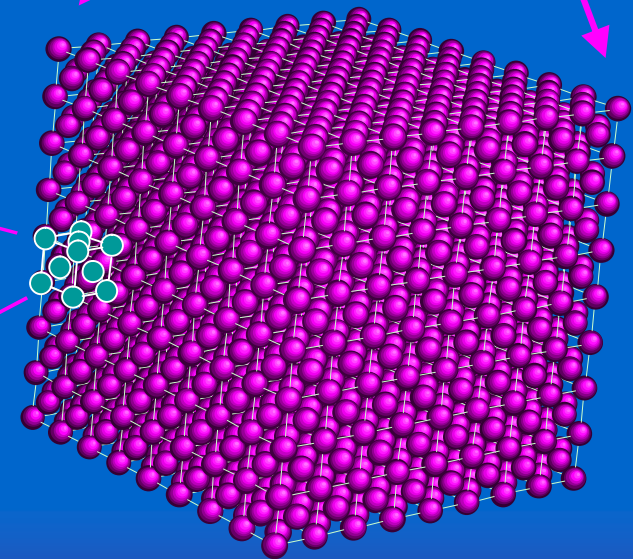
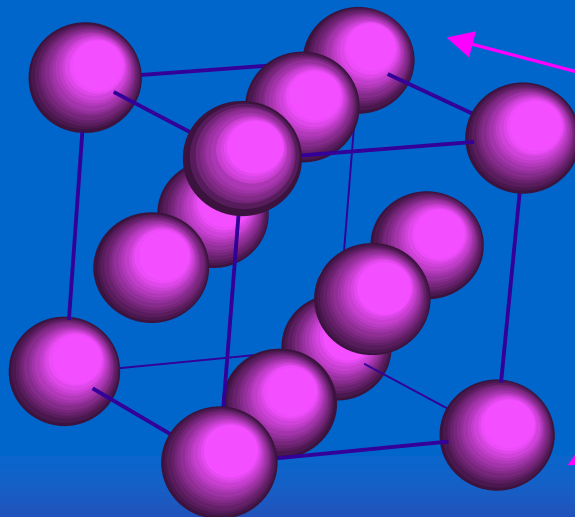
- SRXRD from nanocrystalline and highly deformed materials



STRUCTURE & MICROSTRUCTURE



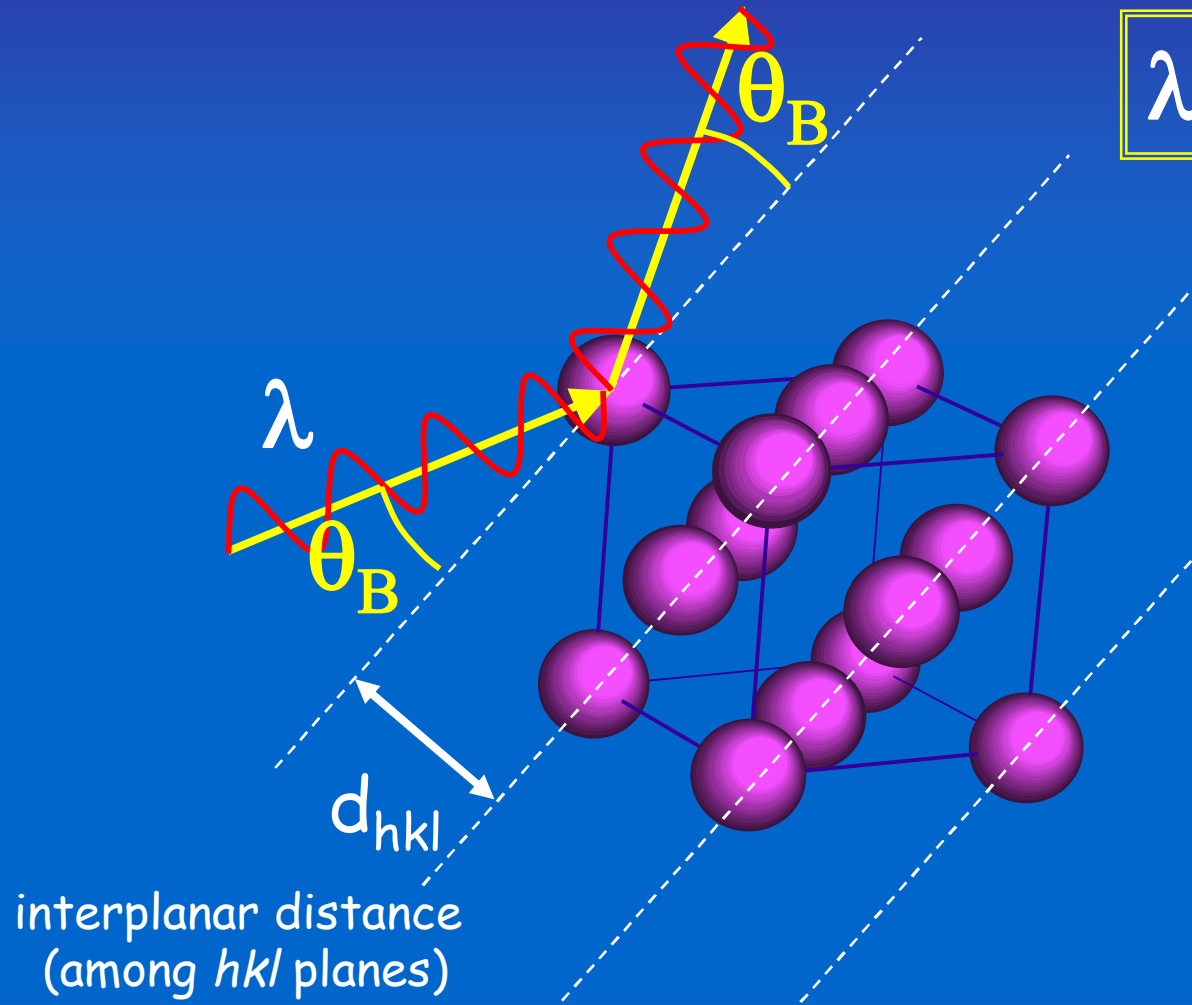
Al





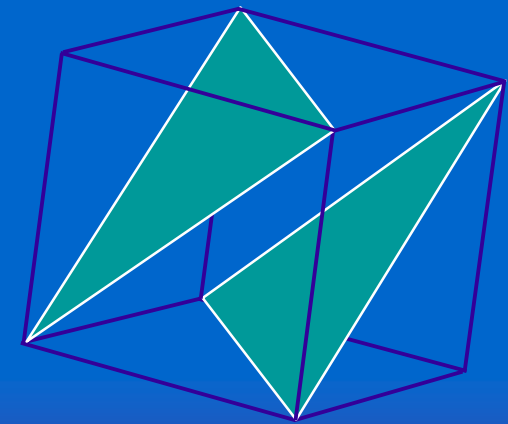
ATOMIC PLANES AND DIFFRACTION CONDITION

$$\lambda = 2 d_{hkl} \sin\theta_B$$



Miller indices (hkl)

(111)

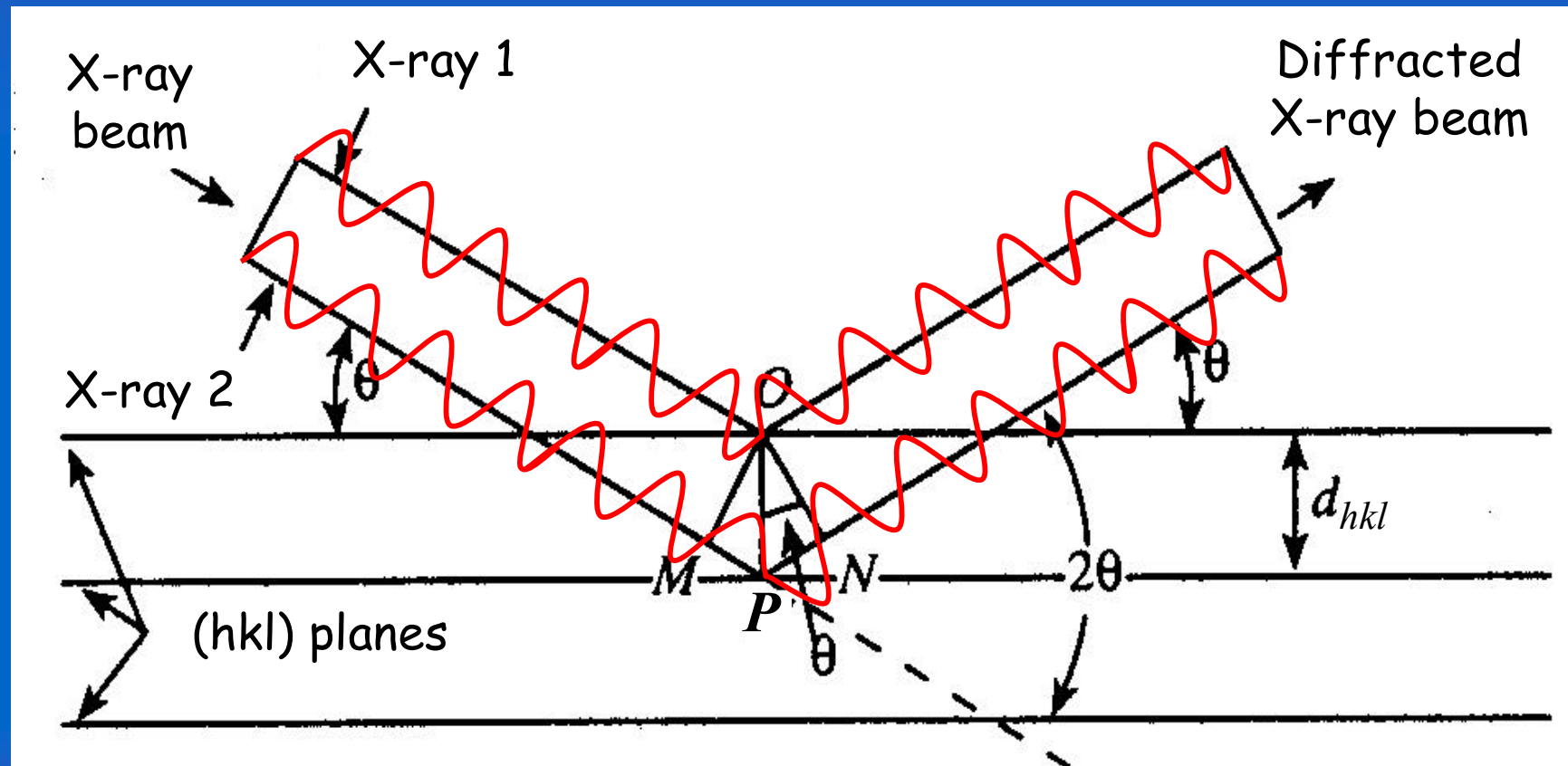


interplanar distance
(among hkl planes)



ATOMIC PLANES AND DIFFRACTION CONDITION

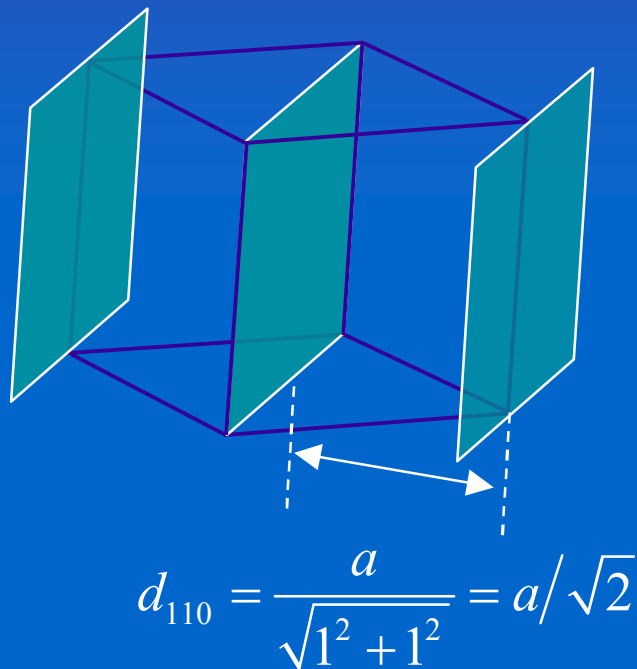
$$MP + PN = 2d_{hkl} \sin \theta = n\lambda \quad \text{Bragg Law}$$



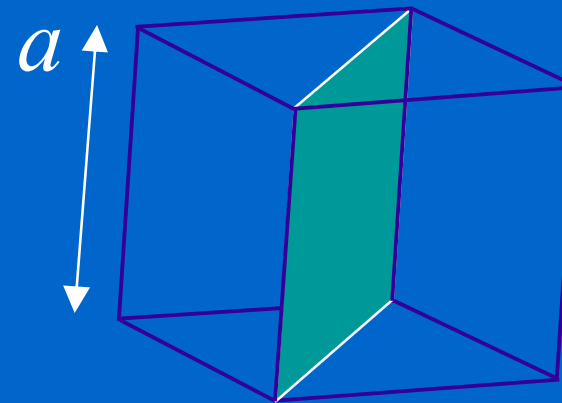


ATOMIC PLANES AND DIFFRACTION CONDITION

Interplanar distance, d_{hkl}



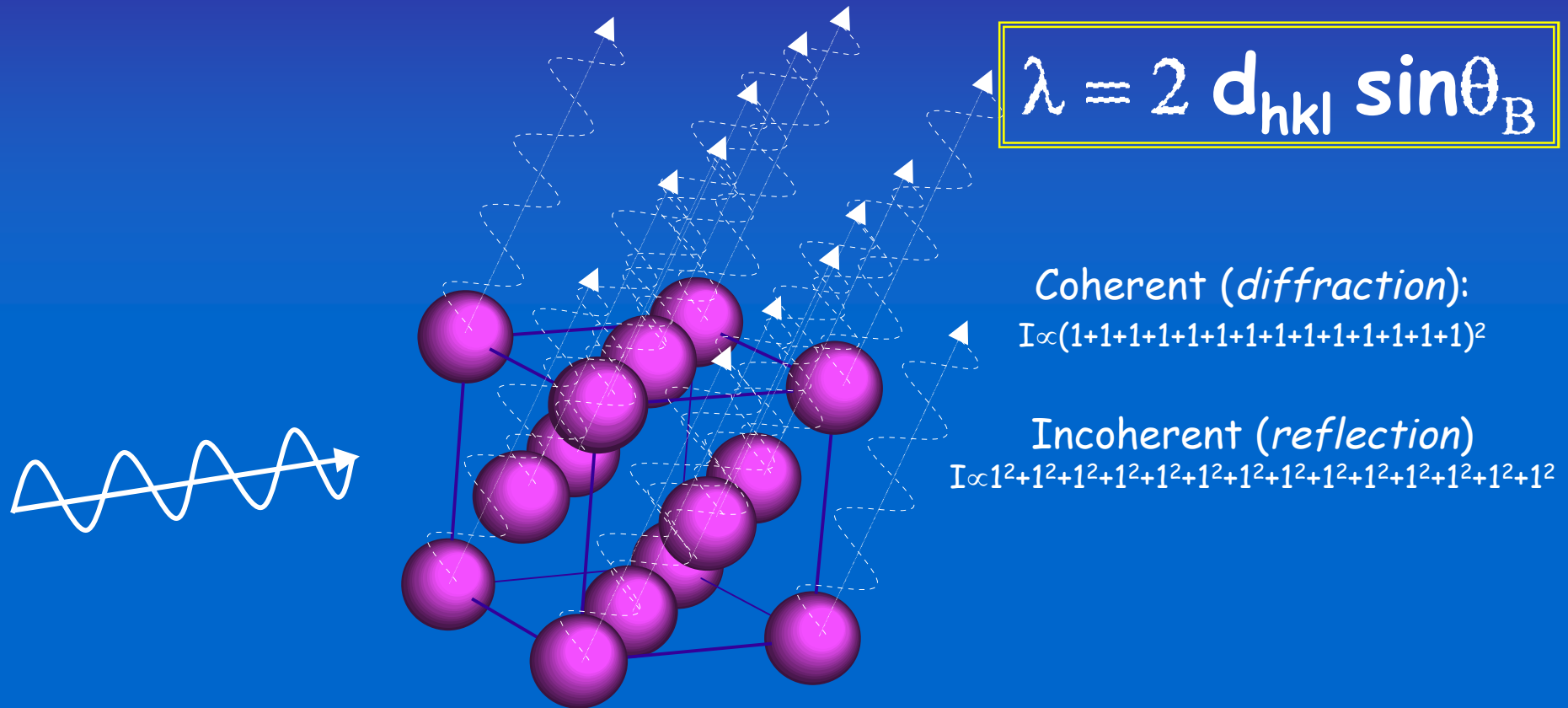
(110)



For cubic materials:
$$d_{hkl} = \frac{a}{\sqrt{h^2 + k^2 + l^2}}$$



COHERENT vs INCOHERENT SCATTERING



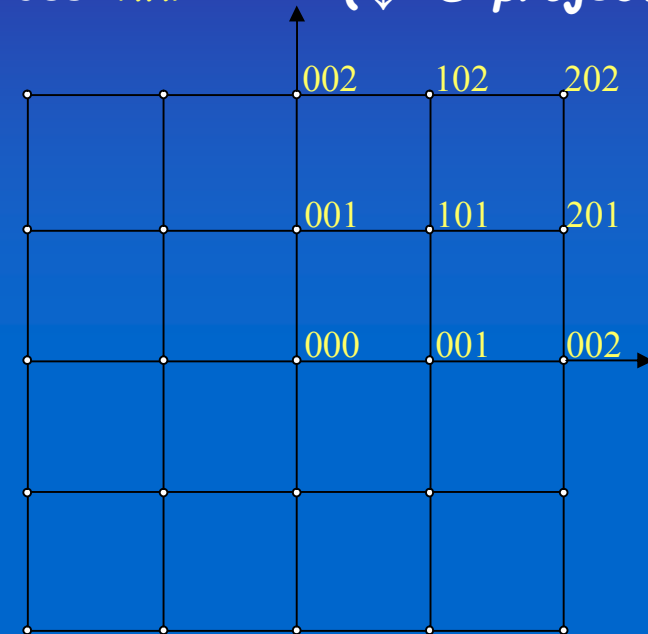
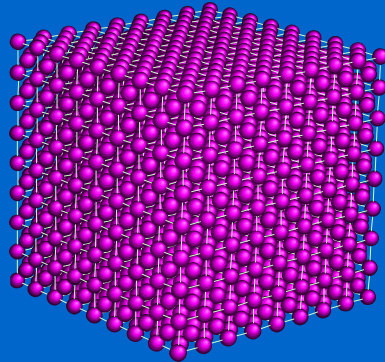
In diffraction conditions the scattered intensity is proportional to the square of the sum of the amplitudes

(all atoms are 'in phase')



DIRECT AND RECIPROCAL SPACE

For a perfect (infinite) crystal the **reciprocal lattice** is made of *infinitely small* points representing sets of planes of Miller indices hkl (\downarrow 2D projection)

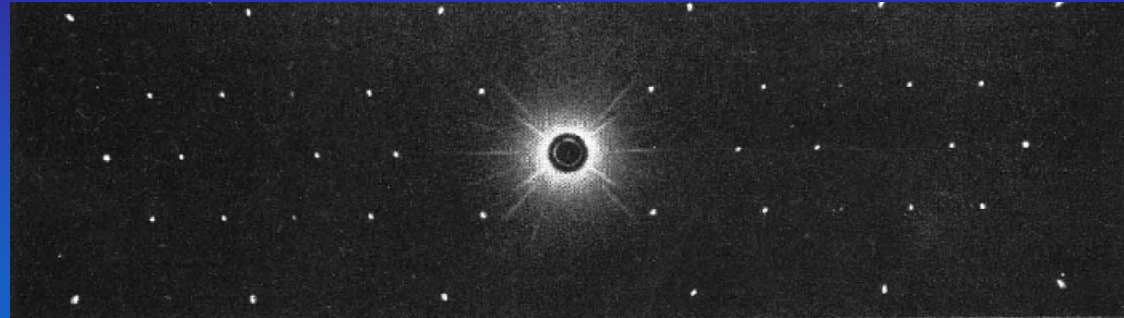
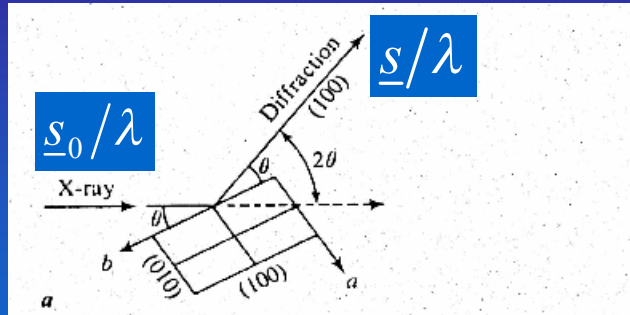


The distance d_{hkl}^* from the 000 origin to a hkl point is the **inverse of the interplanar distance**

$$d_{hkl}^* = \left| \underline{d}_{hkl}^* \right| = \frac{1}{d_{hkl}}$$



DIFFRACTION FROM A SINGLE CRYSTAL



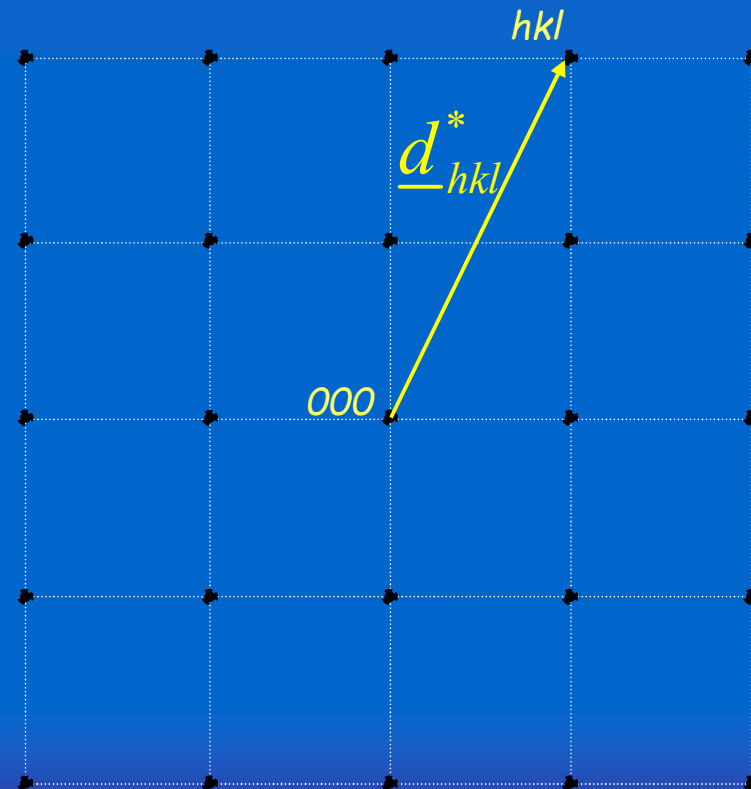
Diffraction conditions correspond to the scattering vector $(\underline{s} - \underline{s}_0)/\lambda$ being equal to:

$$\frac{\underline{s}}{\lambda} - \frac{\underline{s}_0}{\lambda} = \underline{d}_{hkl}^*$$



$$\lambda = 2 d_{hkl} \sin \theta$$

Bragg law





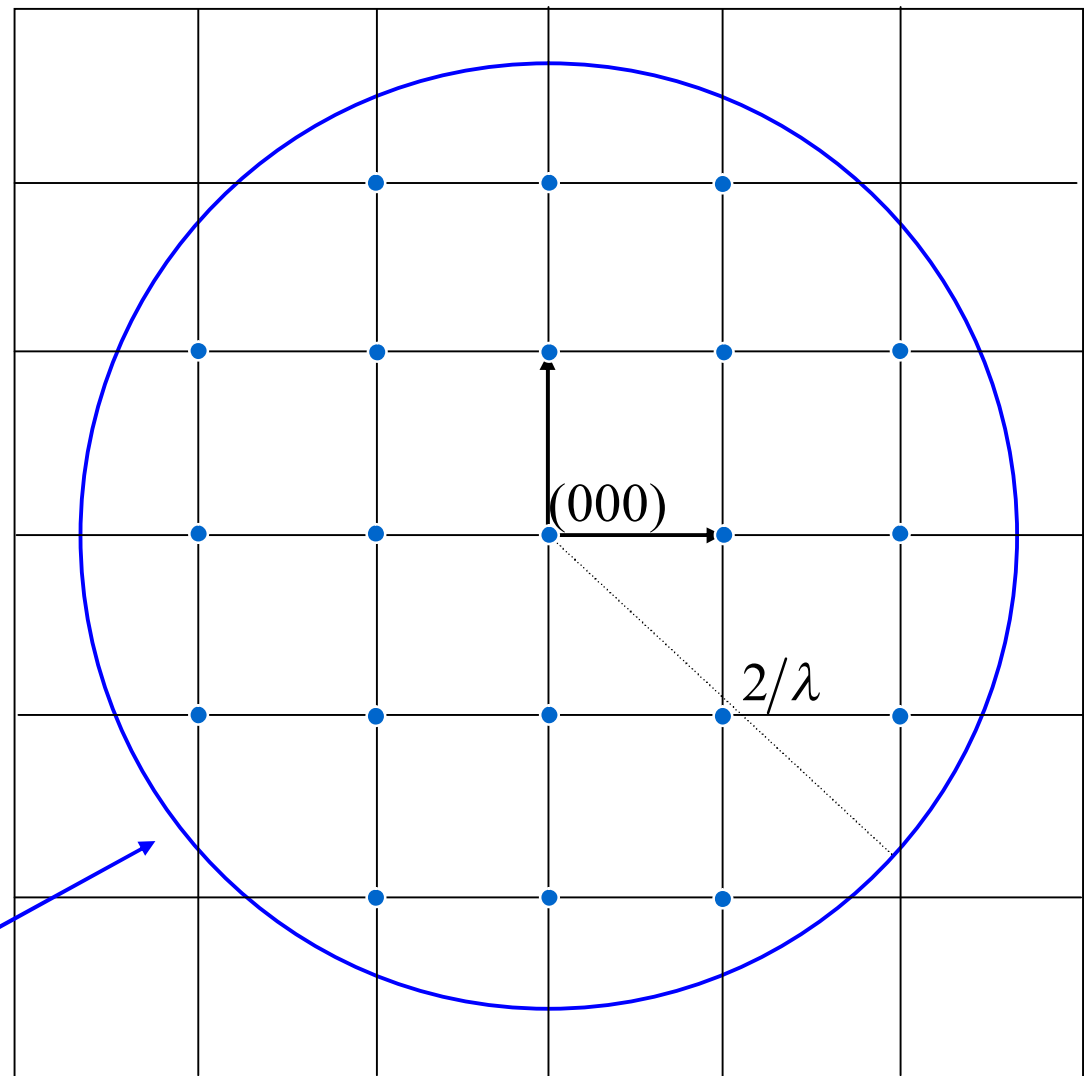
RECIPROCAL LATTICE: DIFFRACTION CONDITIONS

For a given wavelength, the Bragg law sets a limit to the interplanar distances for which diffraction is observed:

$$\sin \theta = \lambda/2d = \lambda d^*/2 \leq 1$$

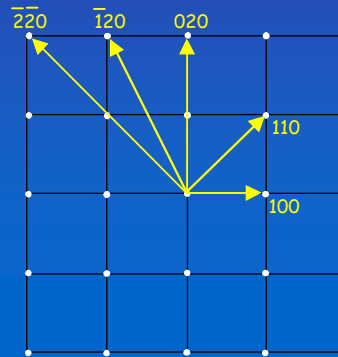
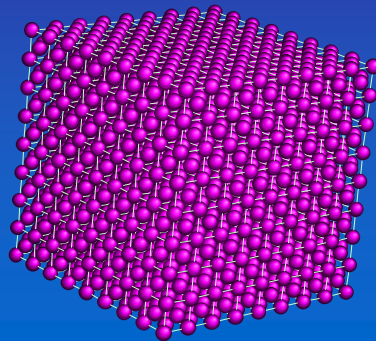
$$d^* \leq \frac{2}{\lambda}$$

All points representing planes that can diffract are inside a sphere of finite radius, $2/\lambda$ (*limiting sphere*)

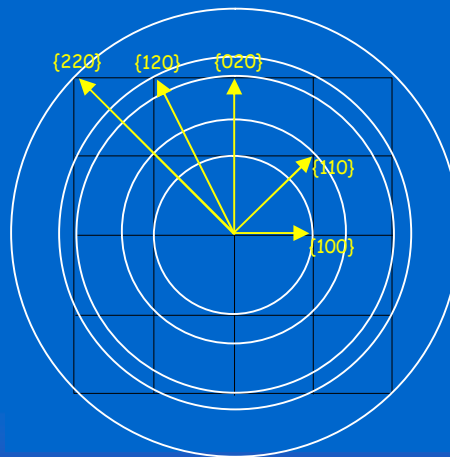
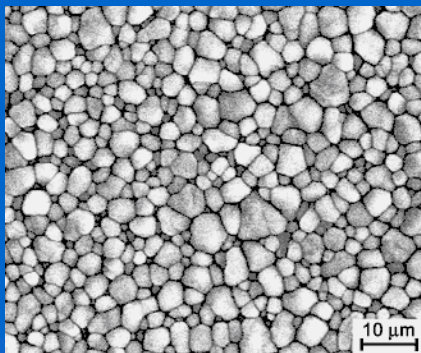




DIFFRACTION: SINGLE CRYSTAL AND POWDER



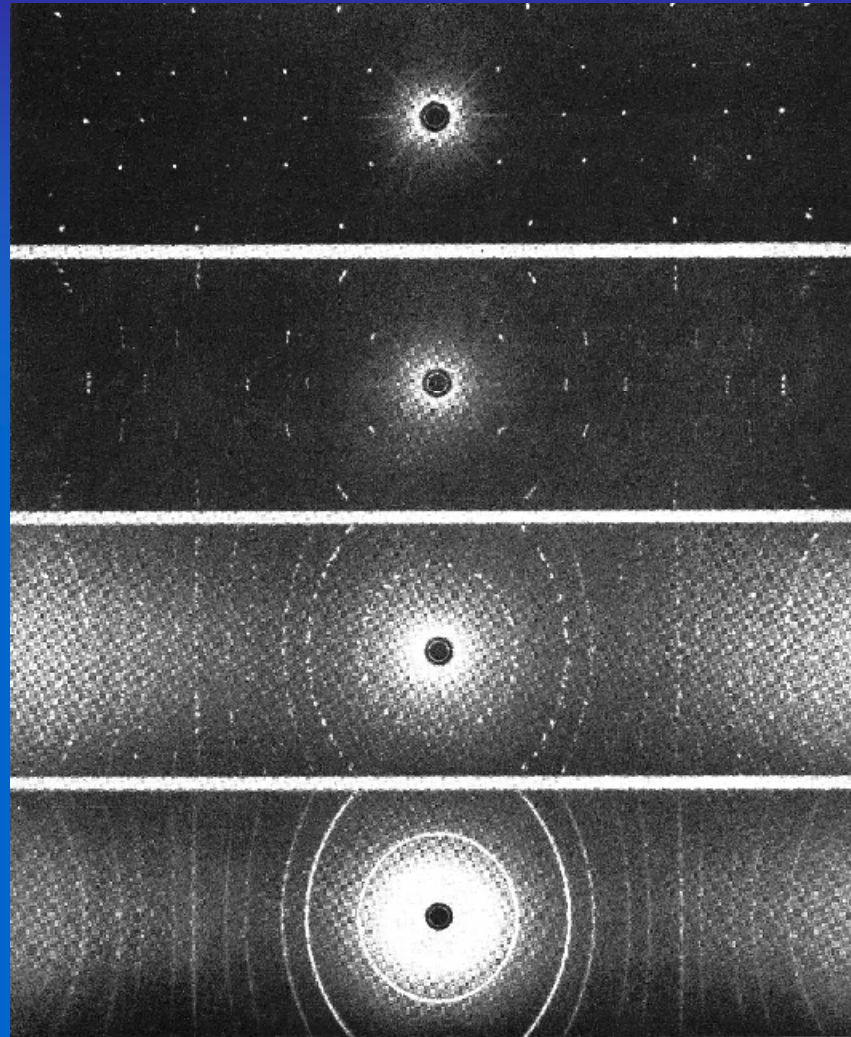
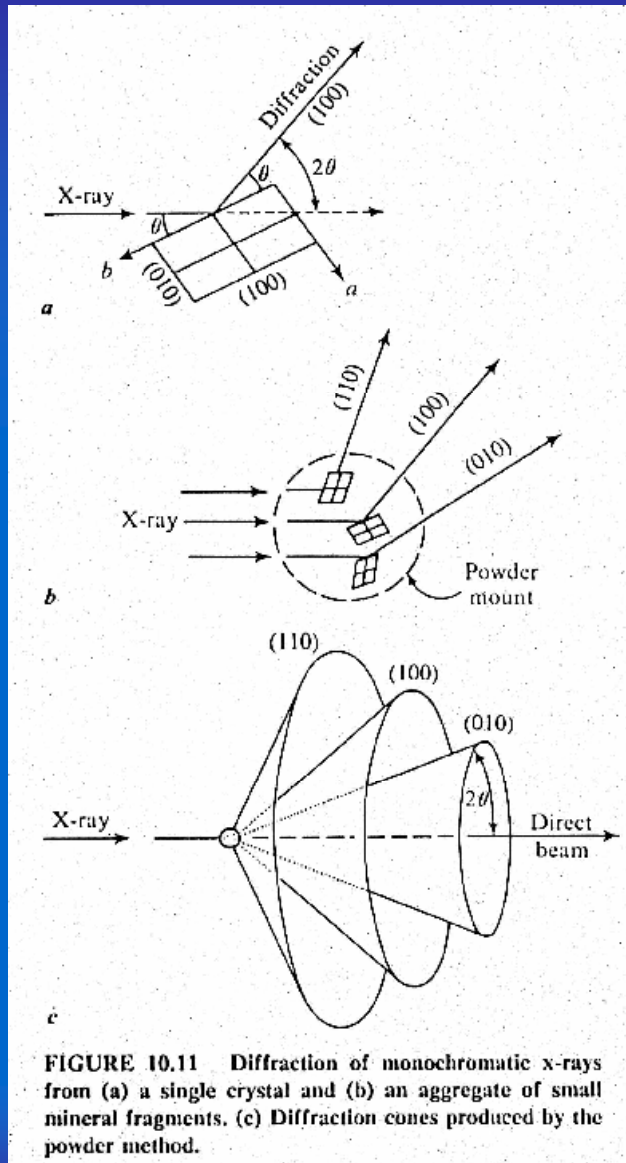
single crystal



powder
(bulk polycrystalline)



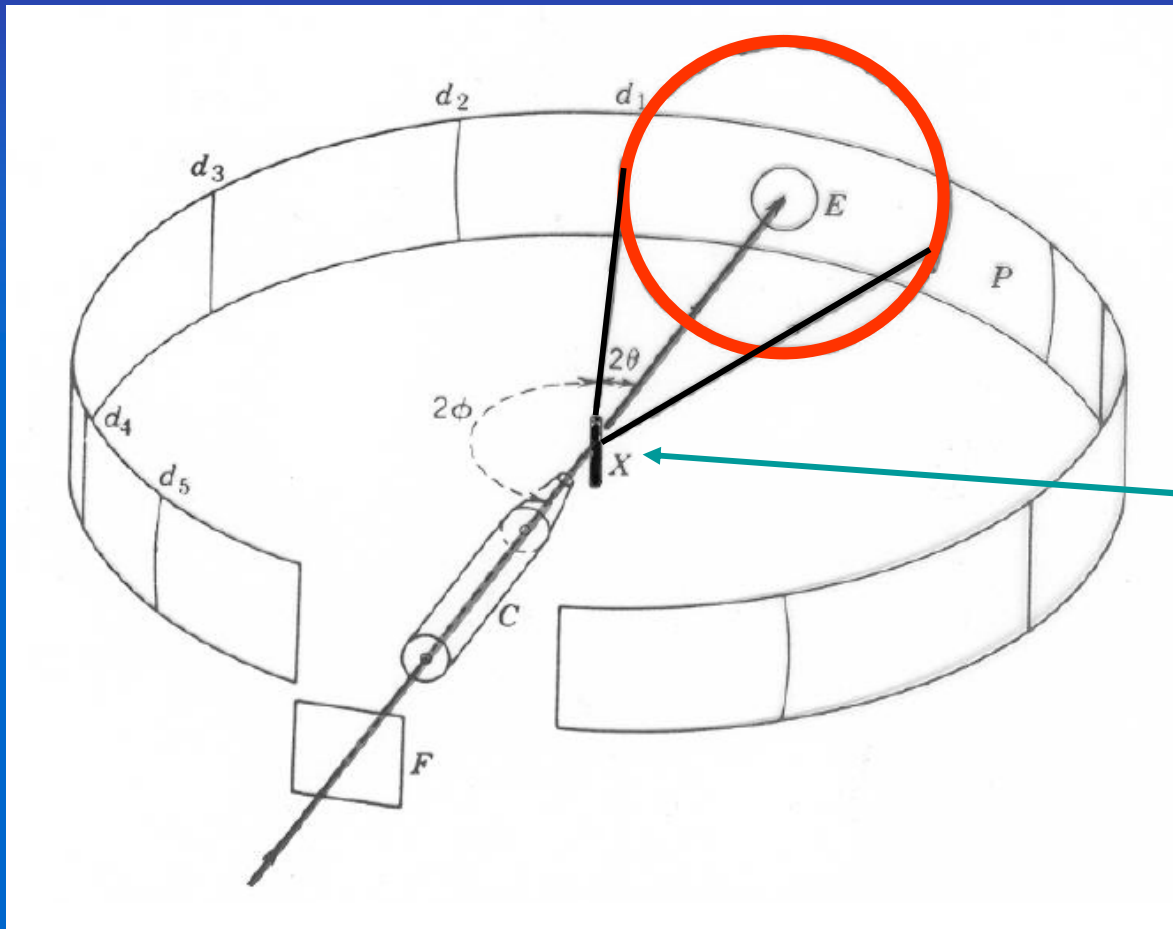
DIFFRACTION: SINGLE CRYSTAL AND POWDER



(From top to bottom). Fig. 197; Single-crystal rotation photograph of fluorite [100] vertical; Fig. 198; Single-crystal rotation photograph of fluorite [100] 2° to vertical; Fig. 199; X-ray photograph of five randomly oriented crystals of fluorite; Fig. 200; Powder photograph of fluorite.



DEBYE-SCHERRER GEOMETRY



POWDER



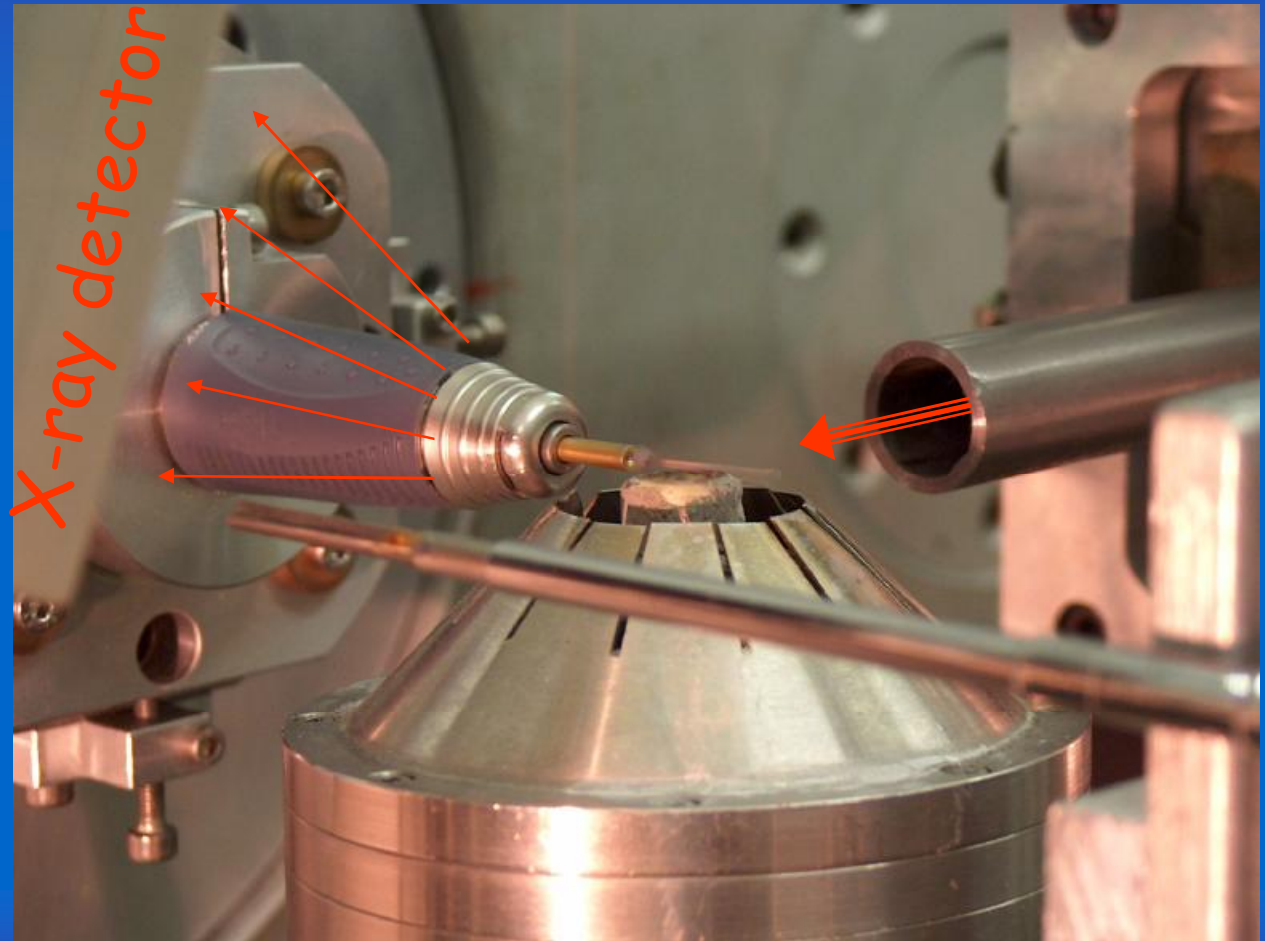
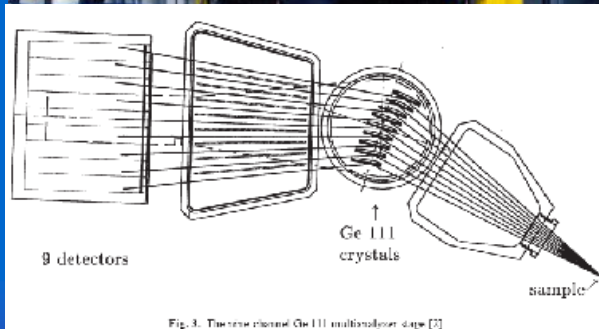
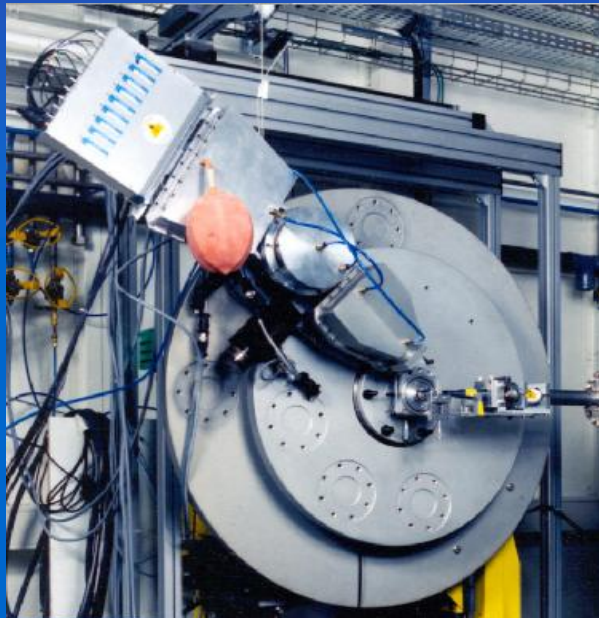


SRXRD POWDER GEOMETRY: A TYPICAL EXAMPLE

Parallel beam geometry at ID31 (ESRF)

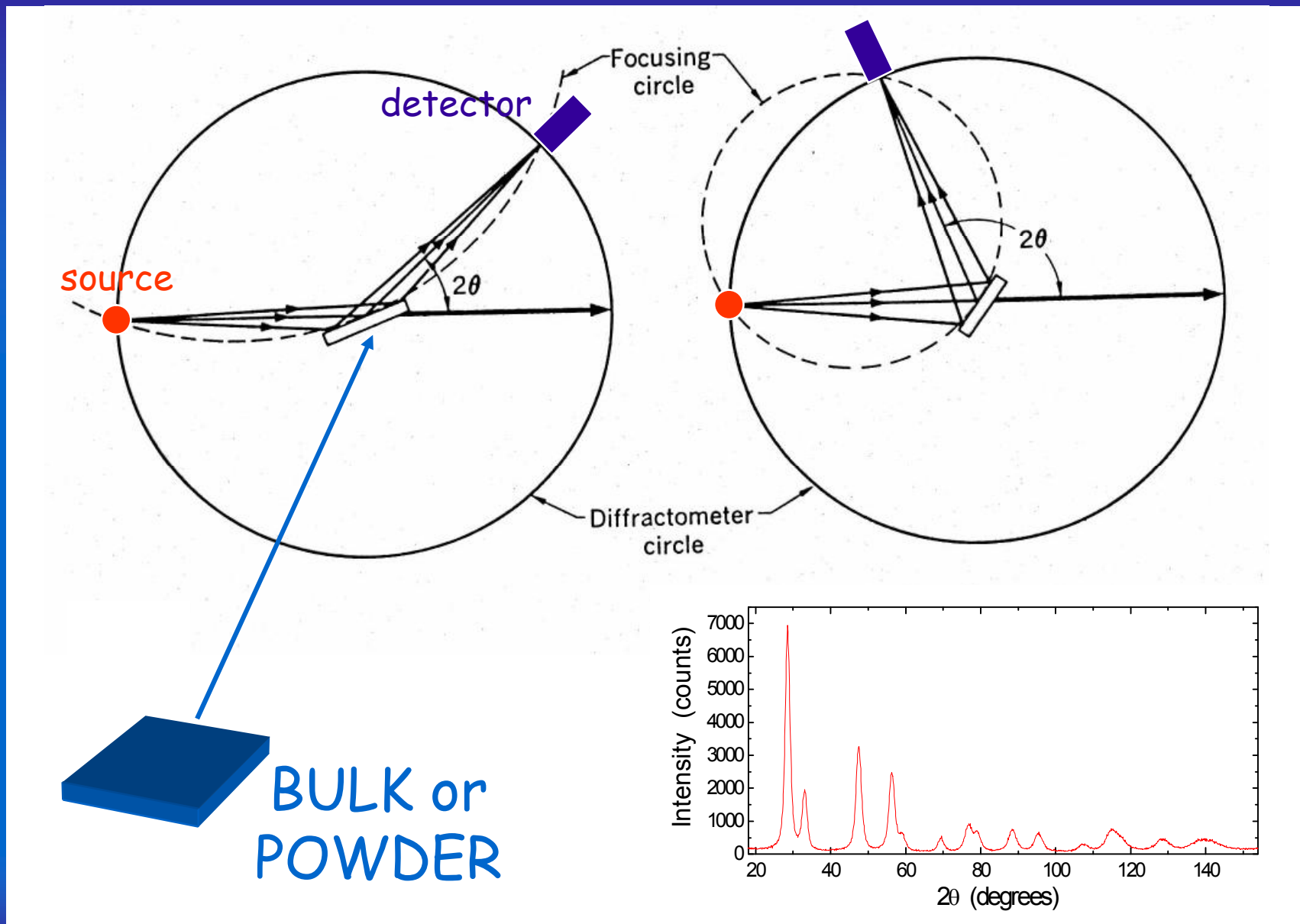
ID31 Goniometer and
nine-crystal analyzer

capillary holder / high temperature blower





TYPICAL LAB GEOMETRY: BRAGG-BRENTANO (POWDER)

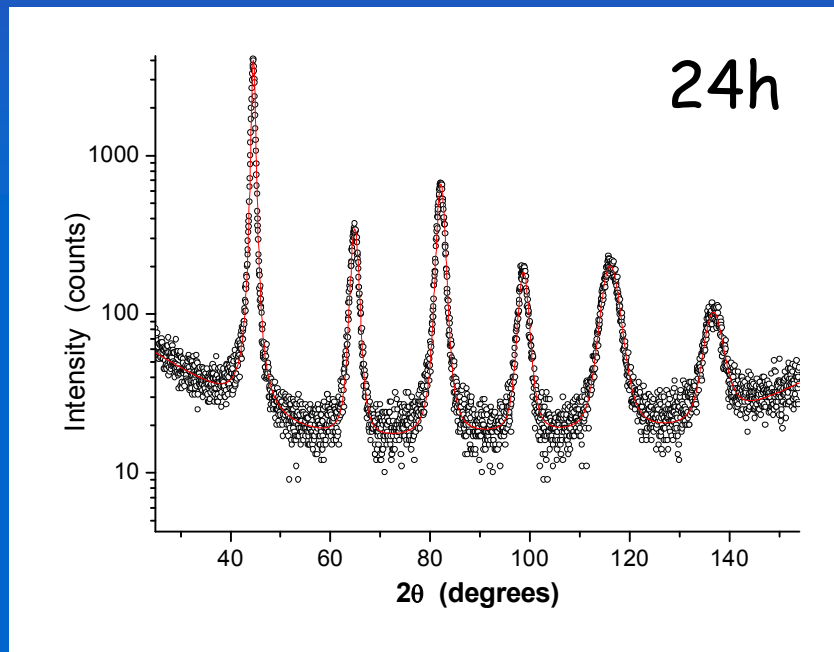




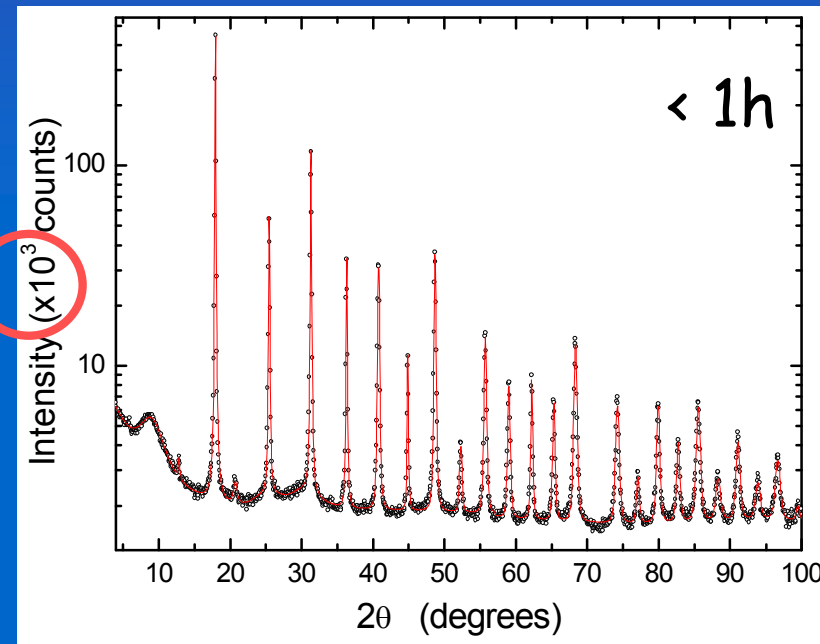
SOME ADVANTAGES OF SRXRD

1) High brilliance, much better counting statistics / shorter data collection time (→ fast kinetics, in situ studies)

Ball mille FeMo



CuK α $\lambda=0.15406$ nm

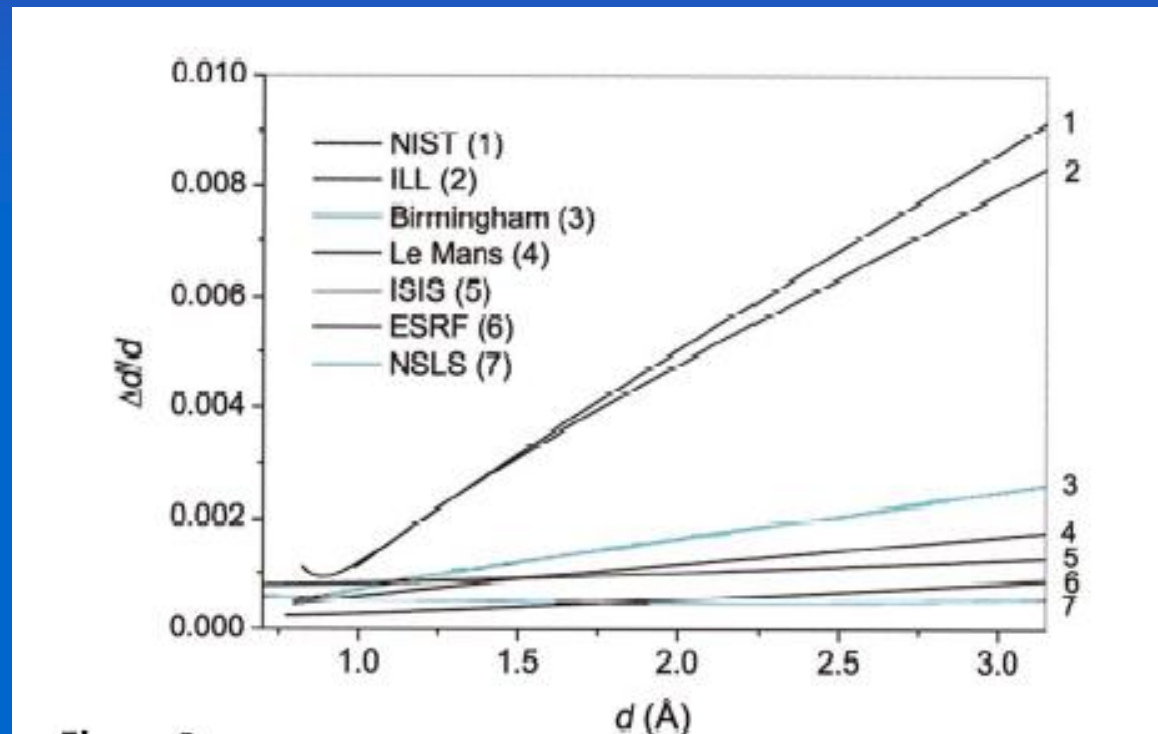


ESRF ID31 $\lambda=0.0632$ nm



SOME ADVANTAGES OF SRXRD

2) With proper selection of optics, very narrow instrumental profile: increased resolution and accuracy in the measurement of peak position, intensity and profile width/shape.



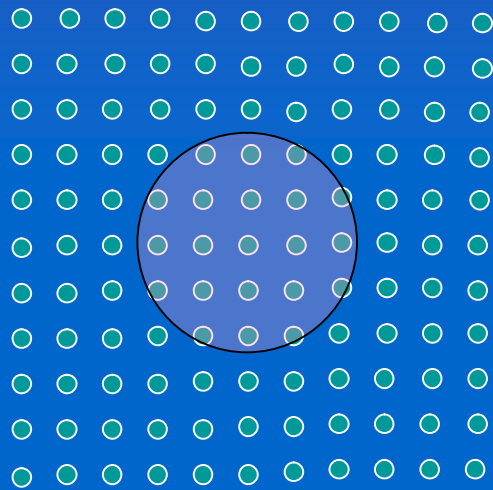
Lab instrument:
FWHM $\approx 0.05-0.1^\circ$

ID31 @ESRF:
FWHM $\approx 0.003-0.004^\circ$

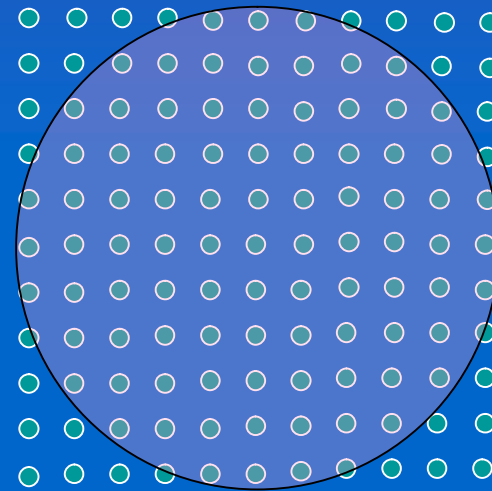


SOME ADVANTAGES OF SRXRD

3) Extending the accessible region of reciprocal space well beyond what traditional lab instruments can make



λ_1



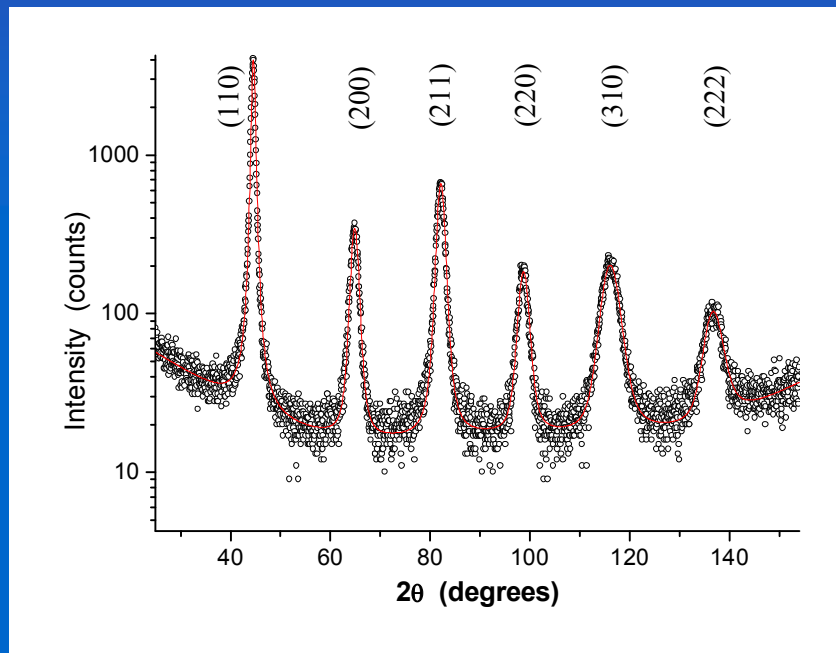
$\lambda_2 < \lambda_1$



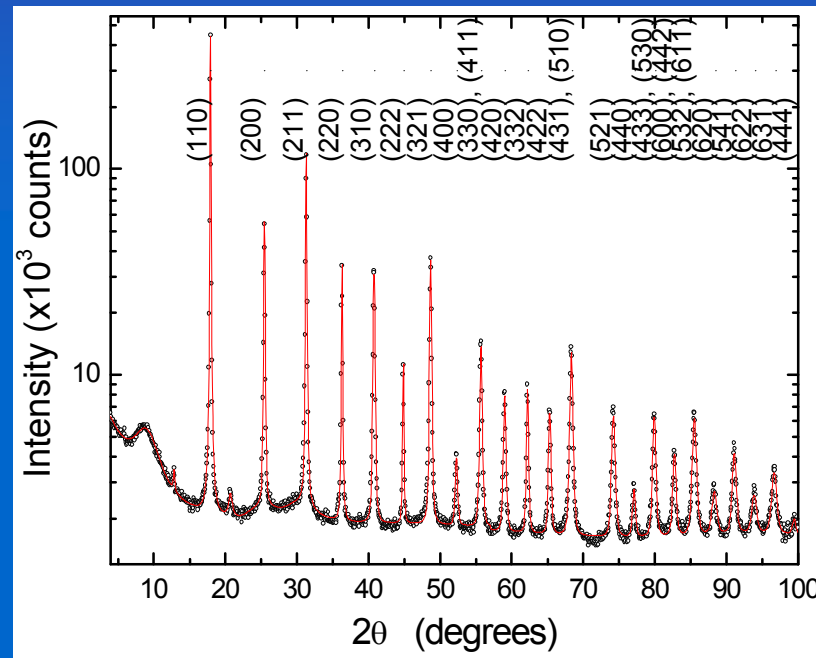
SOME ADVANTAGES OF SRXRD

3) Extending the accessible region of reciprocal space well beyond what traditional lab instruments can make

Ball mill FeMo



CuK α $\lambda=0.15406$ nm



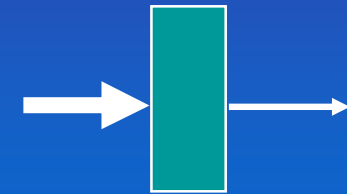
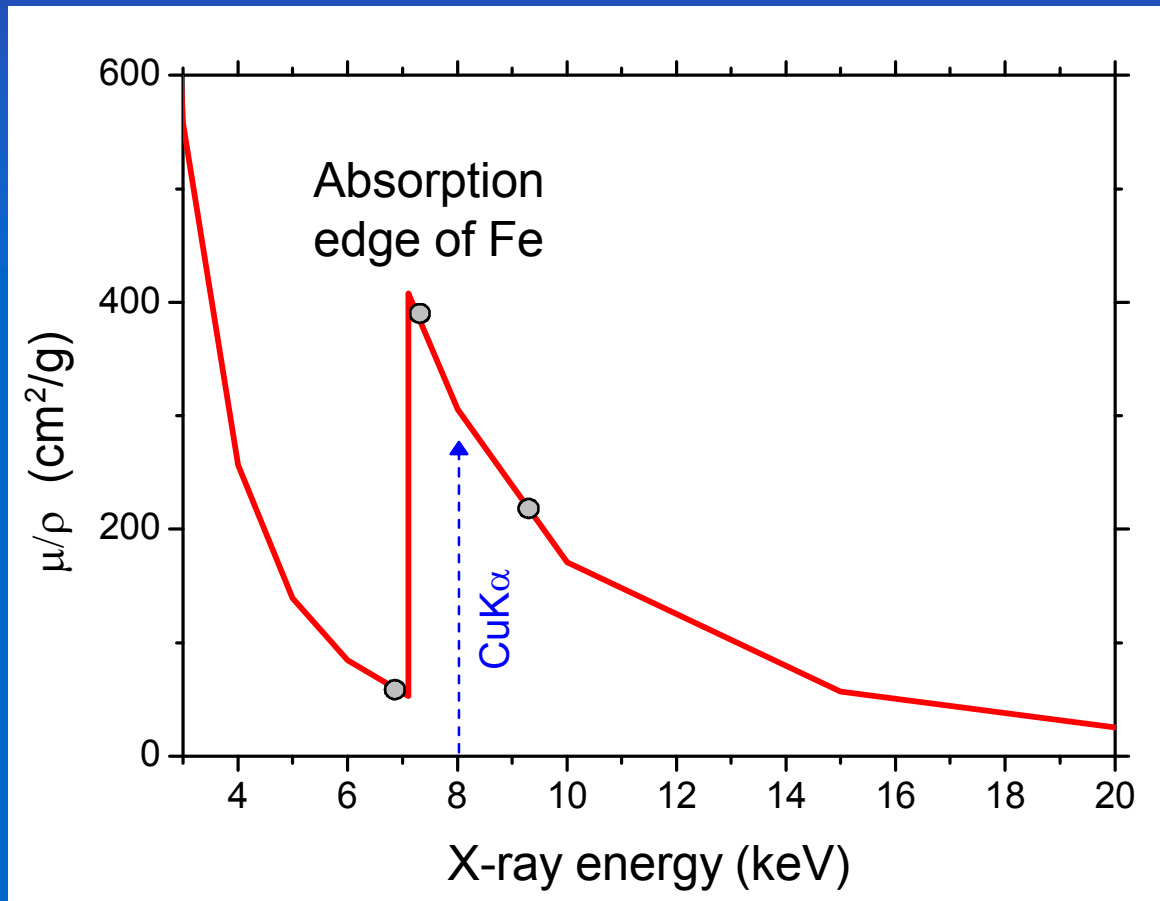
ESRF ID31 $\lambda=0.0632$ nm

M. d'Incau, Leoni & P. Scardi, J. Materials Research 22 (2007) 1744-1753.



SOME ADVANTAGES OF SRXRD

4) Tuning the energy according to adsorption edges. Resonant scattering, control of fluorescence emission and depth of analysis.



$$I = I_0 e^{-\left(\frac{\mu}{\rho}\right)\rho t}$$



X-RAY POWDER DIFFRACTION

Most frequent applications of powder diffraction

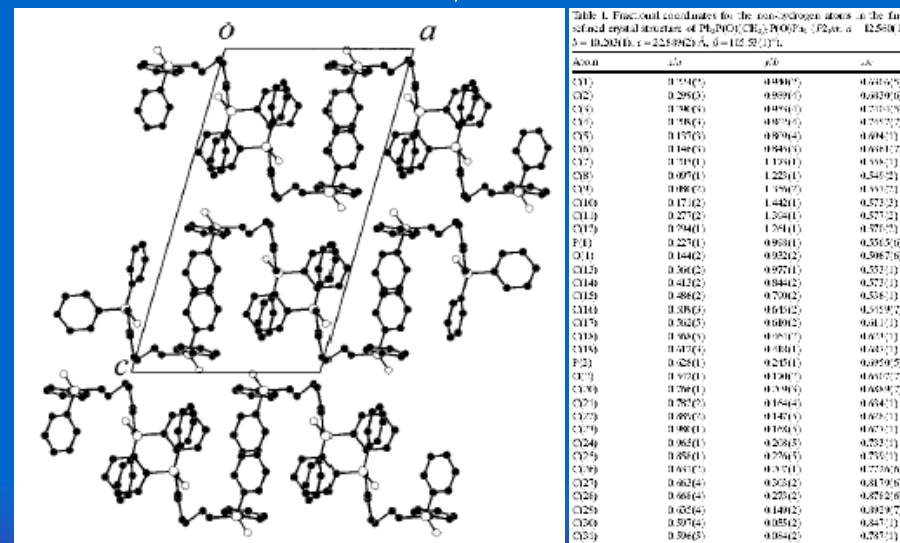
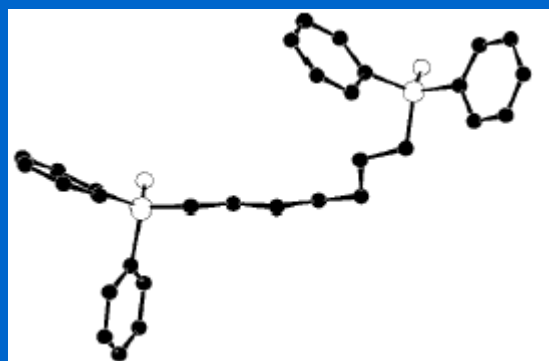
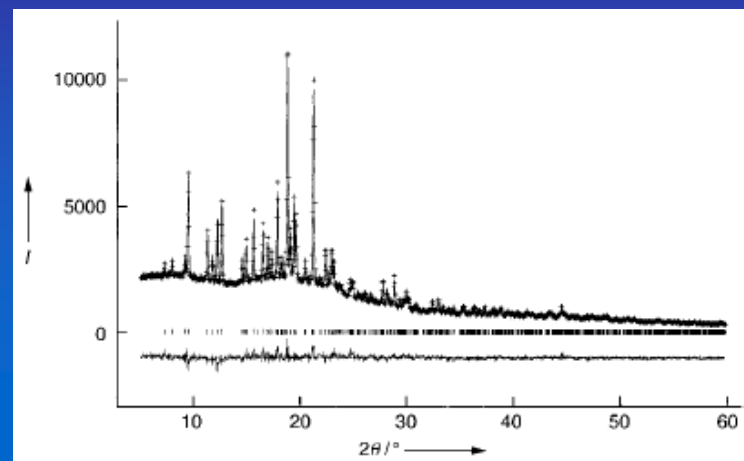
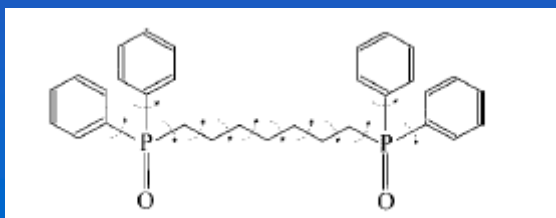
- Crystal structure determination
(Powder diffraction structure solution and refinement)
- Phase Identification - pure crystalline phases or mixtures
(Search-Match procedures)
- Quantitative Phase Analysis (QPA)
- Amorphous phase analysis (radial distribution function)
- Crystalline domain size/shape and lattice defect analysis
(Line Profile Analysis - LPA)
- Determination of preferred orientations (Texture Analysis)
- Determination of residual stress field (Residual Stress Analysis)



STRUCTURE SOLUTION: WHY POWDER ?

Structure solution of heptamethylene-1,7-bis(diphenylphosphane oxide)

Structural formula
 $\text{Ph}_2\text{P}(\text{O})(\text{CH}_2)_7\text{P}(\text{O})\text{Ph}_2$



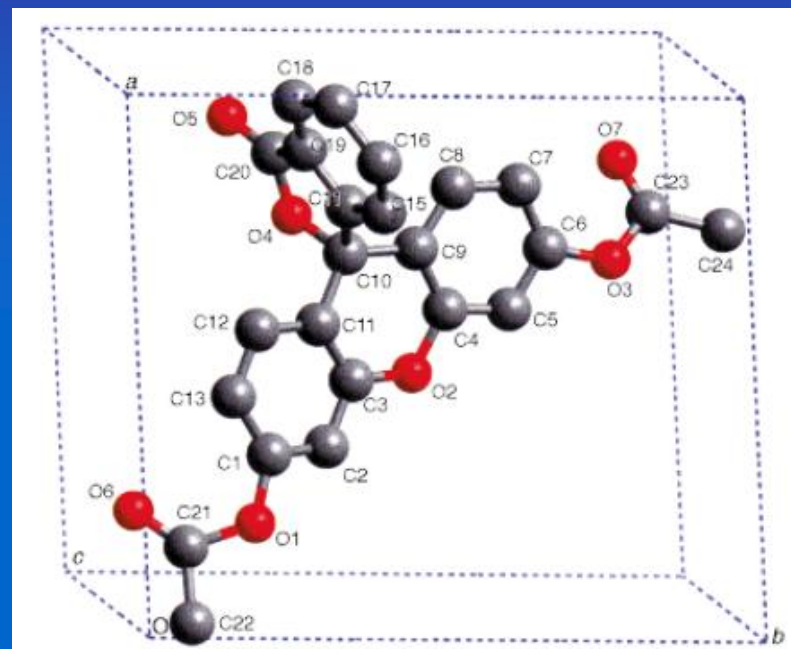
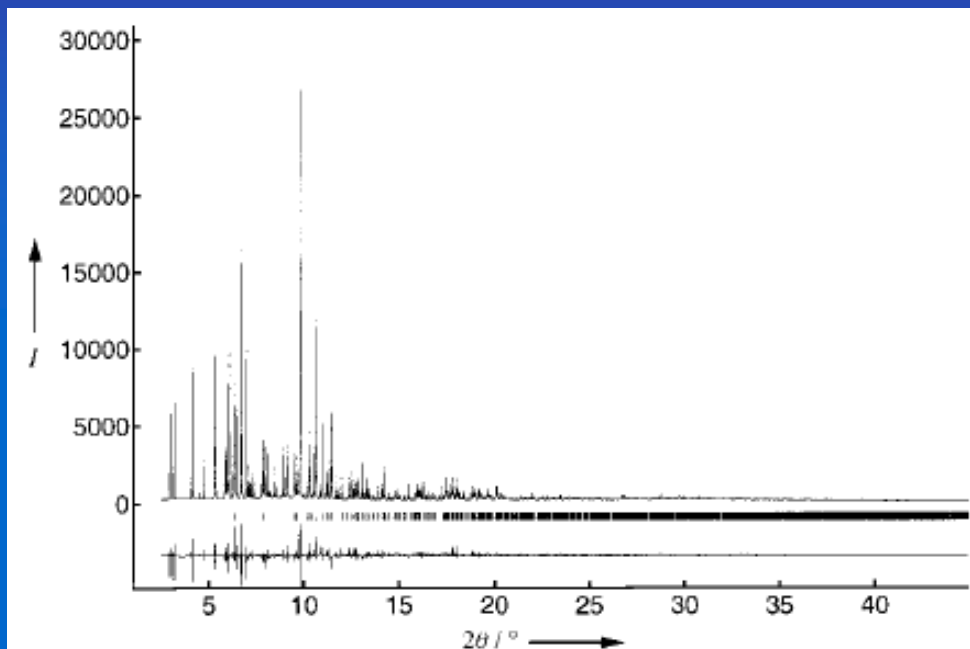
B.M. Kariuki, P. Calcagno, K. D. M. Harris, D. Philp and R.L. Johnston, *Angew. Chem. Int. Ed.* 1999, 38, No. 6, 831-835.



STRUCTURE SOLUTION & REFINEMENT: SRXRD

Structure solution/refinement of a complex triclinic organic compound ($C_{24}H_{16}O_7$)

K. D. Knudsen *et al.*, *Angew. Chem. Int. Ed.*, 37 (1998) 2340



- Narrow peak profiles
- Large number of measurable peaks
- Accurate peak position/intensity
- X-ray energy tuning to adsorption edges



STRUCTURE SOLUTION & REFINEMENT: SRXRD

Site occupancy in battery electrode material $\text{LaNi}_{3.55}\text{Mn}_{0.4}\text{Al}_{0.3}\text{Co}_{0.75}$

J.-M. Joubert *et al.*, J. Appl. Cryst. 31 (1998) 327

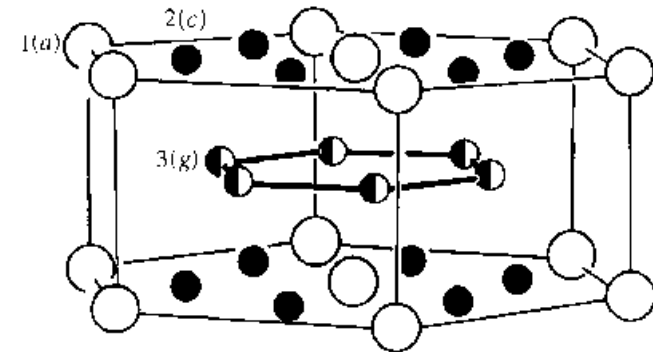
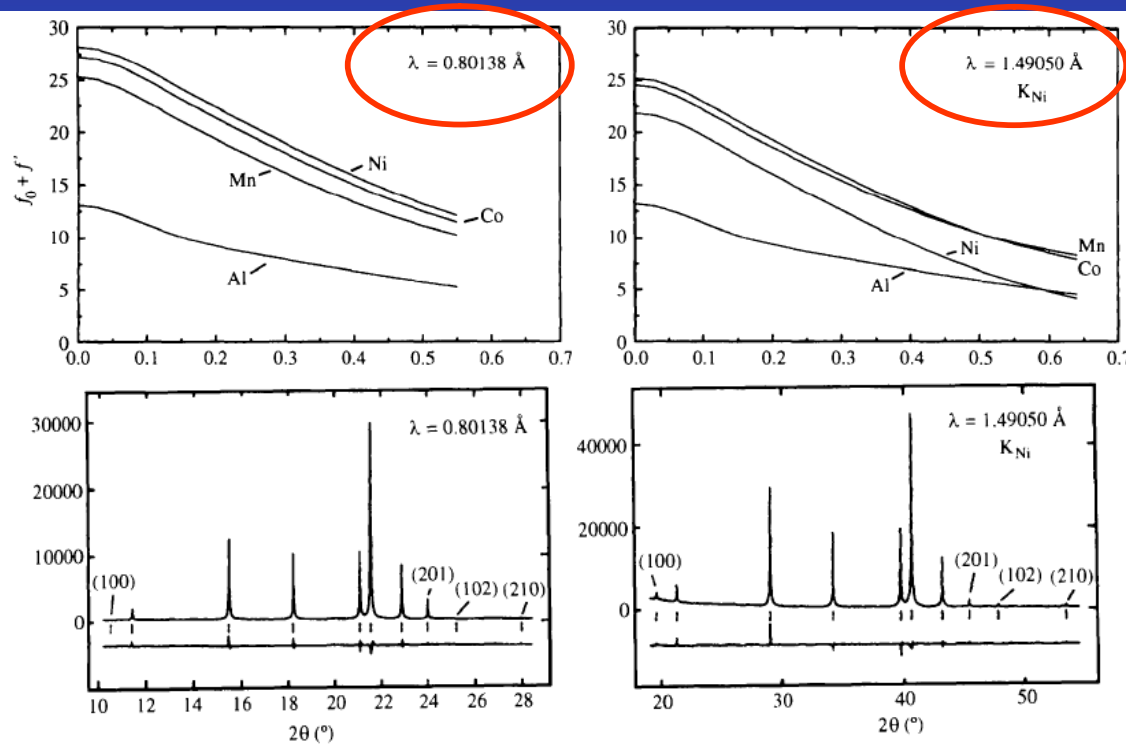


Fig. 1. The crystal structure of LaNi_5 : the large spheres are La on site 1(a); the small spheres are Ni on sites 2(c) and 3(g).

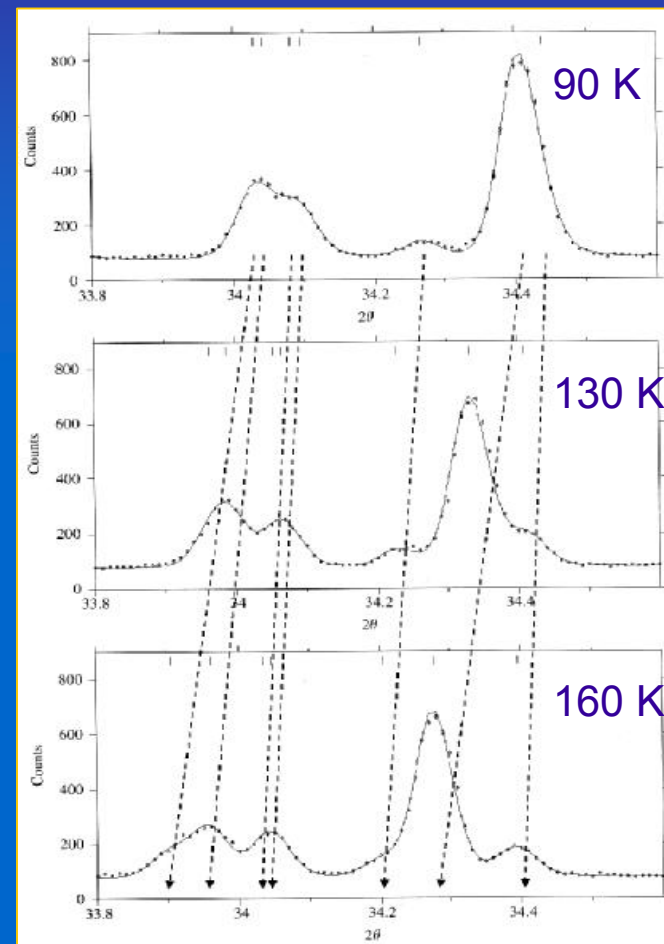
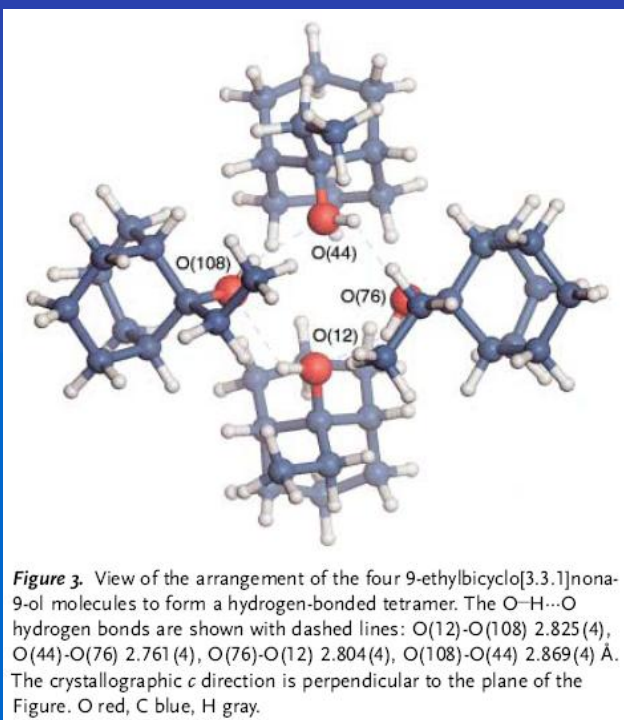
Atom	Site	x	y	z	B (\AA^2)	Occupancy (atoms site ⁻¹)
La	1(a)	0	0	0	2.06 (2)	1
Ni	2(c)	1/3	2/3	0	2.38 (2)	1.66 (2)
Mn						0.07 (1)
Al						0.032 (4)
Co						0.24 (1)
Ni	3(g)	1/2	0	1/2	1.97 (2)	1.89 (3)
Mn						0.33 (1)
Al						0.267 (6)
Co						0.51 (1)

- Narrow peak profiles
- Large number of measurable peaks
- Accurate peak position/intensity
- X-ray energy tuning to adsorption edges



STRUCTURE SOLUTION & REFINEMENT: SRXRD

Solving Larger Molecular Crystal Structures from Powder Diffraction Data by Exploiting Anisotropic Thermal Expansion, M. Brunelli et al., *Angew. Chem. Int. Ed.* 42, 2029, (2003)



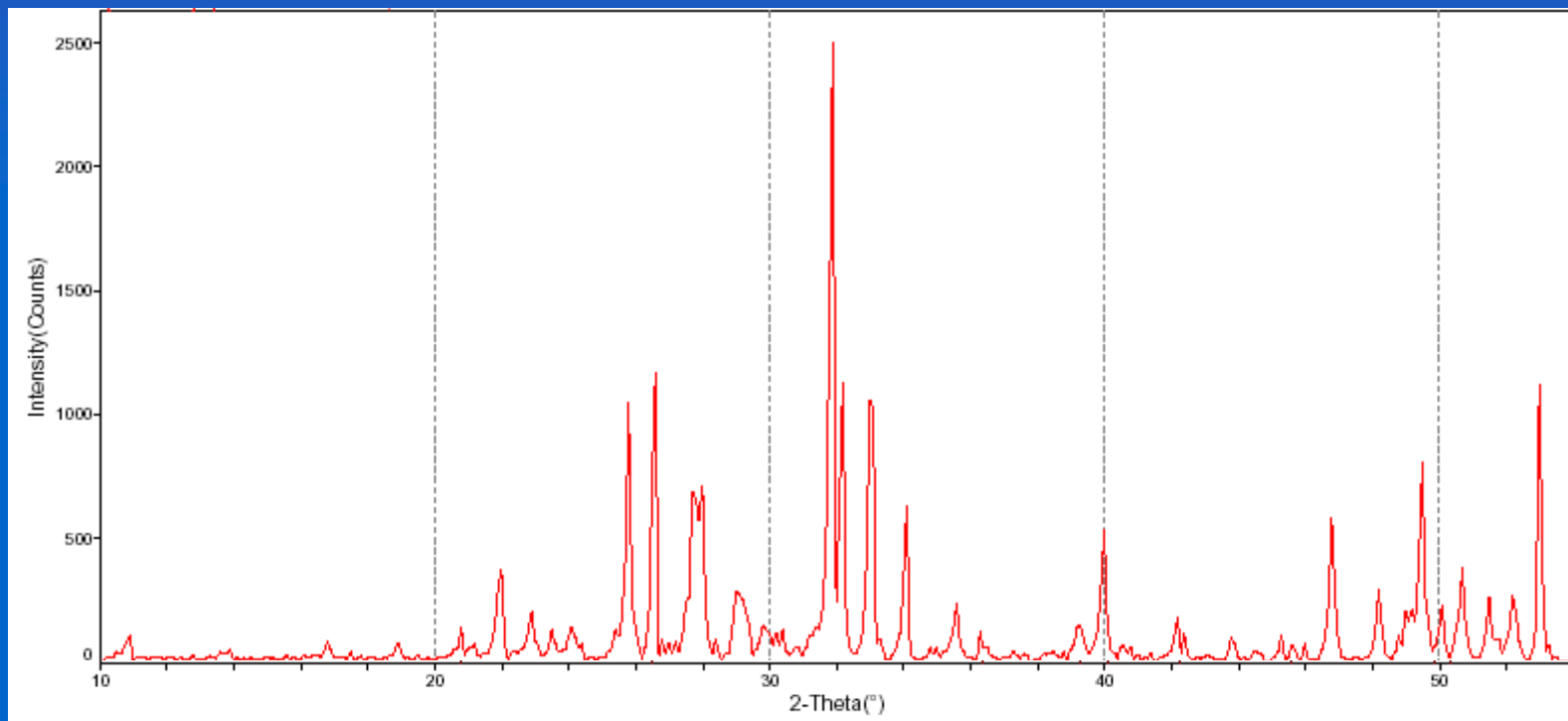
- Narrow peak profiles
- Large number of measurable peaks
- Accurate peak position/intensity
- X-ray energy tuning to adsorption edges
- Anisotropic thermal expansion



PHASE IDENTIFICATION

Phase identification is one of the first and most diffuse applications of powder diffraction, especially in industry for production, quality control and diagnostics, but also in research.

Each crystalline phase has its own pattern that can be used as a 'fingerprint'



'Fingerprints' of unknown substances can be compared with those of known crystalline phases of a database → *Search-Match procedures*



PHASE IDENTIFICATION

The most powerful database is the PDF (Powder Diffraction File) by the ICDD (International Centre for Diffraction Data - www.icdd.com)



PDF-2
Peak pos/int



PDF-4
full structural information

ICDD DDView+ - PDF-4+ 2006 RDB

PDF Card - 04-001-2097

Wavelength: Cu Kα1 1.54056Å

2θ	d(Å)	I	h	k	l
28.5491	3.124	999	1	1	1
33.0829	2.7055	270	2	0	0
47.4886	1.913	450	2	2	0
56.3453	1.6315	327	3	1	1
59.094	1.562	59	2	2	2
69.4222	1.3527	52	4	0	0
76.7043	1.2414	103	3	3	1
79.0846	1.2099	64	4	2	0
88.4378	1.1045	85	4	2	2
95.4167	1.0413	68	5	1	1
107.2806	0.9565	25	4	4	0
114.7472	0.9146	69	5	3	1
117.3338	0.9018	31	6	0	0

Atomic Coordinates (2)

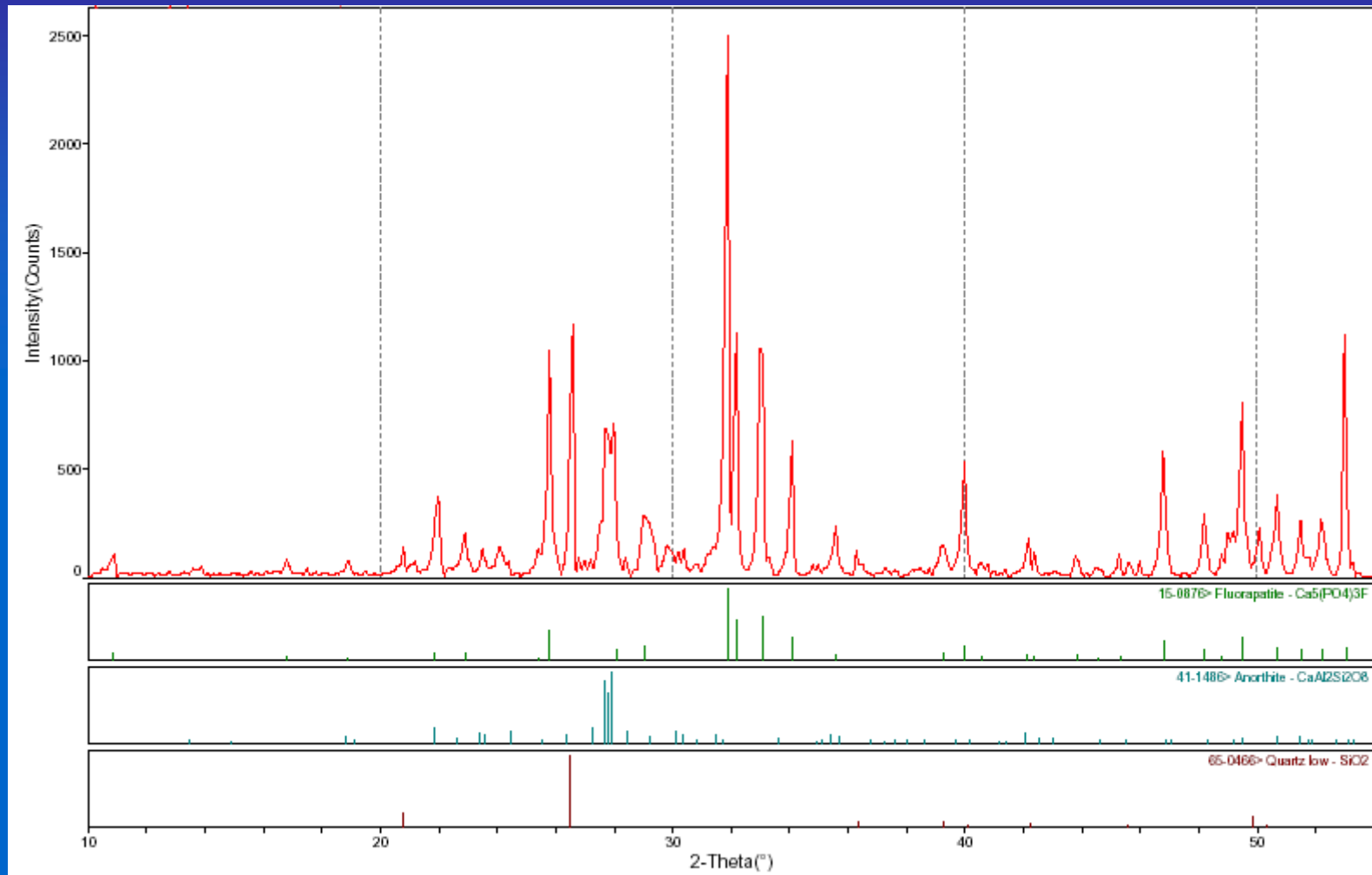
Atom	Num	Wyckoff	Symmetry	x	y	z	SOF	ITF	AET
Ce	1	4a	m-3m	0.0	0.0	0.0	1.0	0.7	8-a
O	2	8c	-43m	0.25	0.25	0.25	1.0	1	10-a

SG Symmetry Operators (48)

Seq	Operator
1	x,y,z
2	-x,-y,-z
3	z,x,y



PHASE IDENTIFICATION

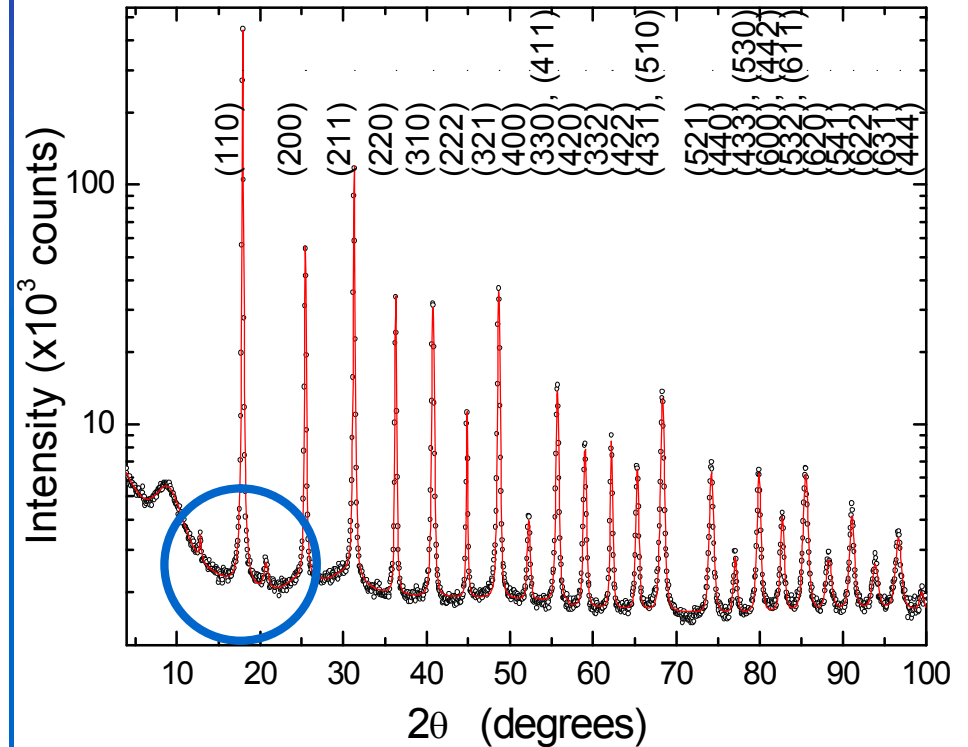
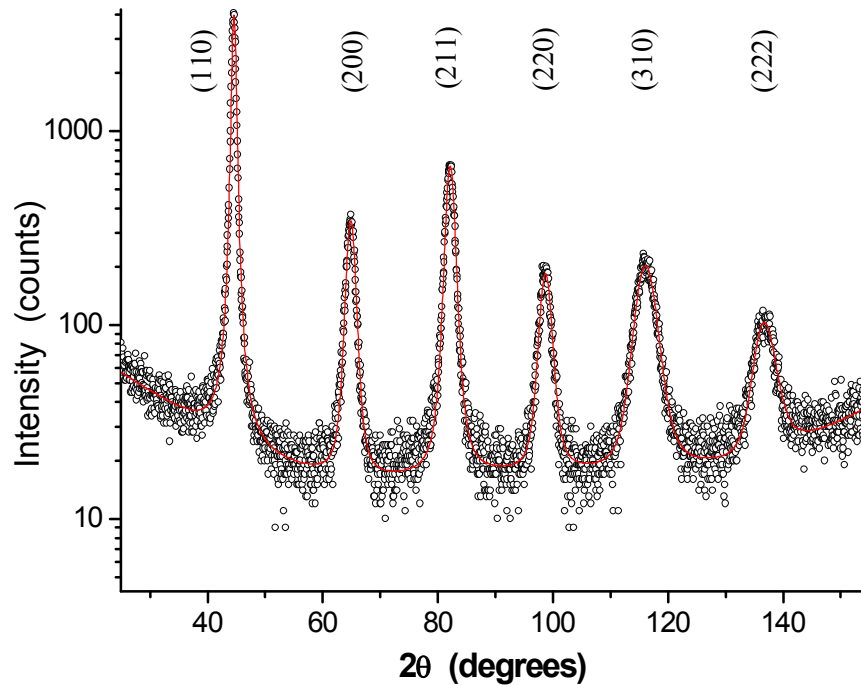


Automatic search-match procedures are based on peak position / intensity



MINOR PHASE IDENTIFICATION BY SRXRD

Iron oxide traces in ball milled α -Fe powder



$\text{CuK}\alpha$ $\lambda=0.15406$ nm

ESRF ID31 $\lambda=0.0632$ nm

M. d'Incau, Leoni & P. Scardi, J. Materials Research 22 (2007) 1744-1753.



QUANTITATIVE PHASE ANALYSIS (QPA)

The pattern of a phase mixture is the **WEIGHTED** sum of the patterns corresponding to the constituent phases. The weight depends of the specific scattering power and absorption of each phase in the mixture.

Several techniques exists for a quantitative determination of the phase content:

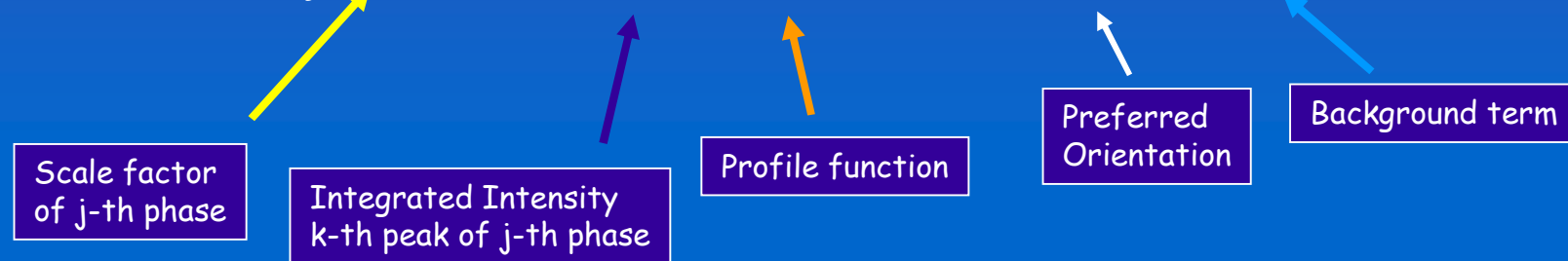
- **QPA with internal standard**
- **QPA with “virtual standard” (RIR method)**
- **QPA via the Rietveld method (virtual standard)**



THE RIETVELD METHOD

Intensity of the i -th point in the pattern

$$y_{ci} = \sum_j S_j \sum_k I_{k,j} \cdot \phi_{k,j}(2\theta) \cdot P_{k,j} + y_{bi}$$



Using the normalization condition: $\sum_k x_k = 1$ (not obvious !!)

it is possible to calculate the weight fraction x_j of the phase j in a polyphasic mixture as:

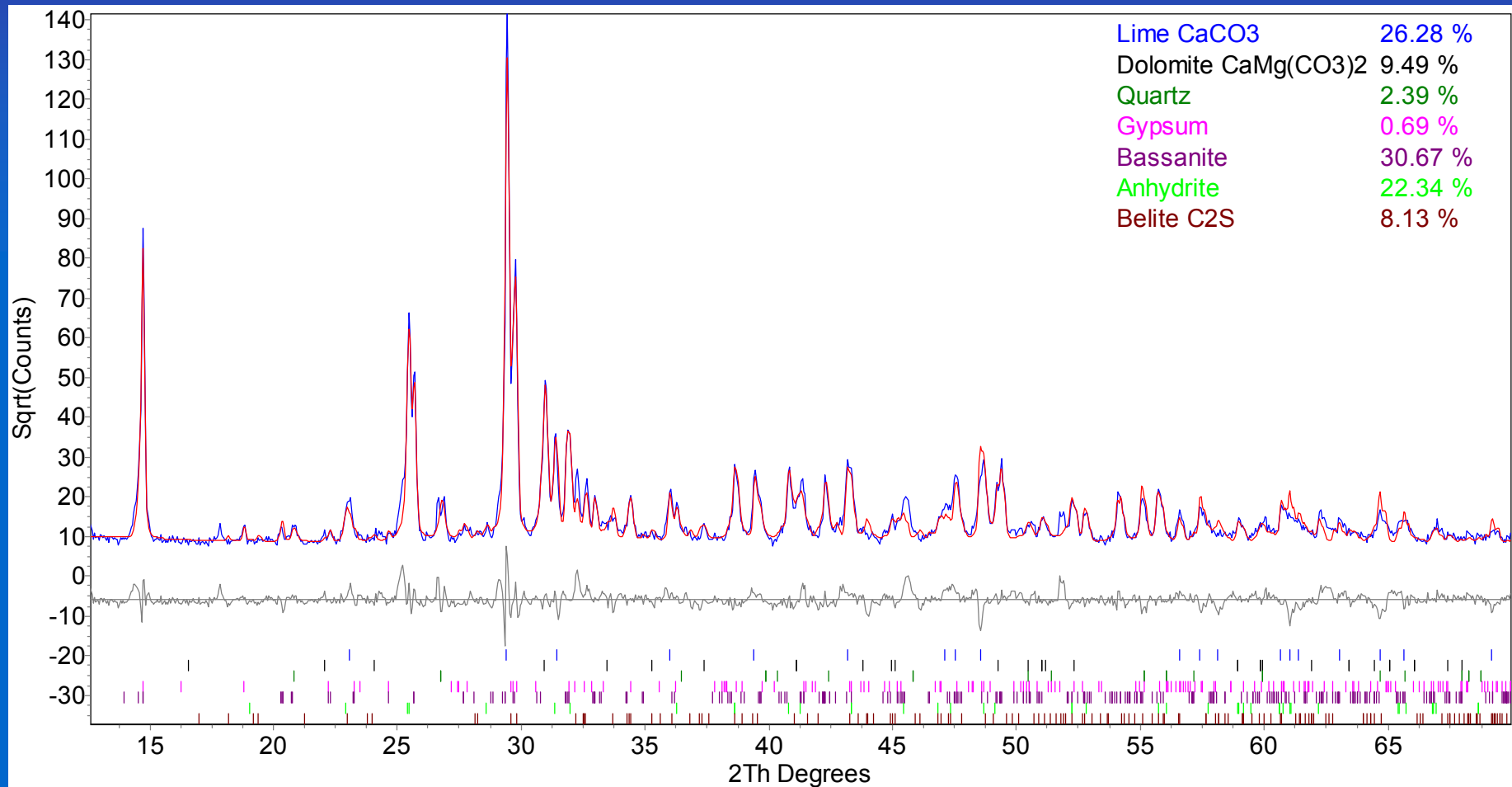
$$x_j = \frac{S_j \rho_j v_j}{\sum_l S_l \rho_l v_l}$$

→ J. Plasier



RIETVELD-BASED QPA

Example: mixture of mineral phases in a ligand





STRUCTURE SOLUTION IN MULTIPHASE SAMPLES

Structural and electronic properties of noncubic fullerides $A'_{40}C_{60}$ ($A'=Ba,Sr$)

C.M. Brown *et al.*, Phys. Rev. Let. 83 (1999) 2258

ESRF BM161 $\lambda=0.084884$ nm

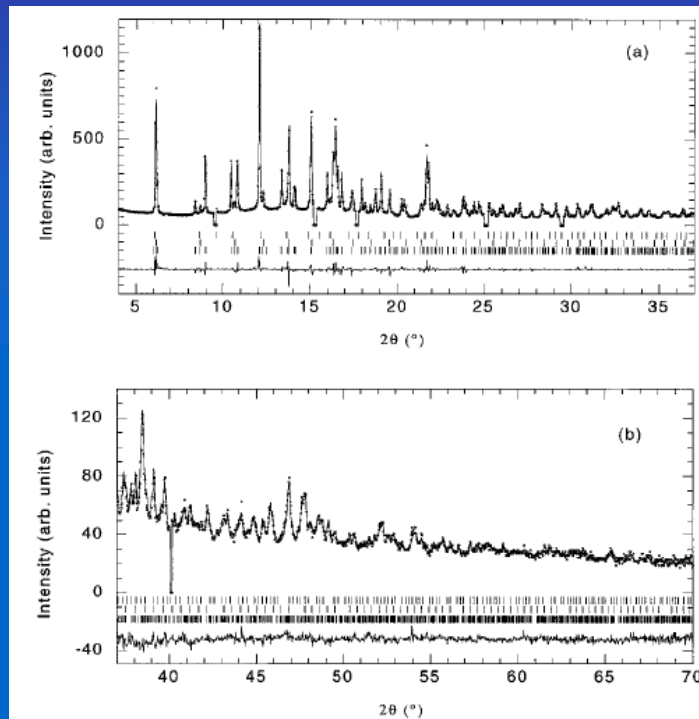


FIG. 2. Final observed (points) and calculated (solid line) synchrotron x-ray powder diffraction profiles for Ba_4C_{60} at 295 K in the range 4° to 70° ($\lambda = 0.84884 \text{ \AA}$). The lower panels show the difference profiles and the ticks mark the positions of the Bragg reflections of Ba_4C_{60} [majority phase: 86.1(2)%, lower most], Ba_6C_{60} [minority phase: 11.8(1)%, middle], and Ba_3C_{60} [minority phase: 2.1(1)% upper most]. Some sharp peaks originating from a nonfulleride phase were excluded from the refinement.

- Narrow peak profiles
- Large number of measurable peaks
- Accurate peak position/intensity
- X-ray energy tuning to adsorption edges



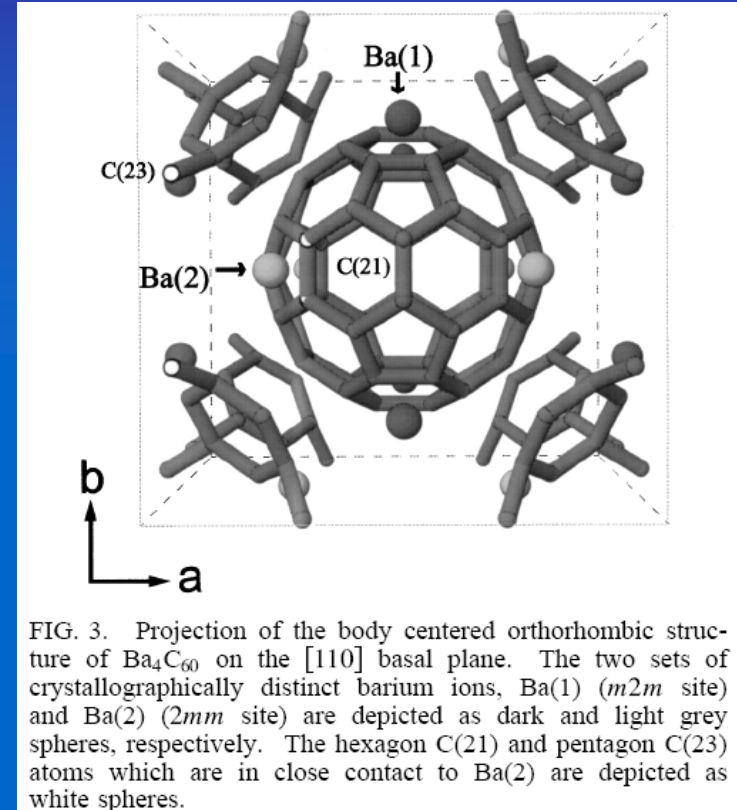
STRUCTURE SOLUTION IN MULTIPHASE SAMPLES

Structural and electronic properties of noncubic fullerides $A'_{40}C_{60}$ ($A'=Ba,Sr$)

C.M. Brown *et al.*, Phys. Rev. Let. 83 (1999) 2258

TABLE I. Refined parameters for orthorhombic Ba_4C_{60} obtained from Rietveld refinement of the synchrotron x-ray powder diffraction data at 295 K (space group $Immm$, $R_{wp} = 5.3\%$, $R_{exp} = 2.6\%$). The cell constants are $a = 11.6101(2)$, $b = 11.2349(2)$, and $c = 10.8830(2)$ Å, and the weight fraction of the Ba_4C_{60} phase is 86.1(2)%. The weight fractions of the minority phases, Ba_6C_{60} and Ba_3C_{60} are 11.8(1)% and 2.1(1)%, respectively. The cell constants of cubic Ba_6C_{60} (space group $Im\bar{3}$) and Ba_3C_{60} (space group $Pm\bar{3}n$) are 11.1959(2) and 11.338(1) Å, respectively.

Atom	x/a	y/b	z/c	$B_{iso}/\text{Å}^2$ ($\beta_{11}, \beta_{22}, \beta_{33}$)
Ba(1)	0.5	0.2034(2)	0.0	1.9(1), 2.9(2), 0.9(1)
Ba(2)	0.2488(1)	0.5	0.0	2.7(1), 3.7(2), 0.6(1)
C(11)	0.3005(2)	0.0	0.0652(1)	0.16(8)
C(12)	0.0	-0.063 88(4)	0.3206(2)	0.16(8)
C(13)	0.10014(6)	-0.127 86(7)	0.2798(2)	0.16(8)
C(21)	0.2003(1)	-0.63 88(4)	0.2389(1)	0.16(8)
C(22)	0.12373(7)	-0.271 0(2)	0.106 82(6)	0.16(8)
C(23)	0.06187(4)	-0.310 5(2)	0.0	0.16(8)
C(31)	0.2240(2)	-0.207 0(1)	0.066 00(3)	0.16(8)
C(32)	0.06187(4)	-0.231 4(1)	0.213 7(1)	0.16(8)
C(33)	0.2622(2)	-0.103 45(6)	0.131 99(8)	0.16(8)



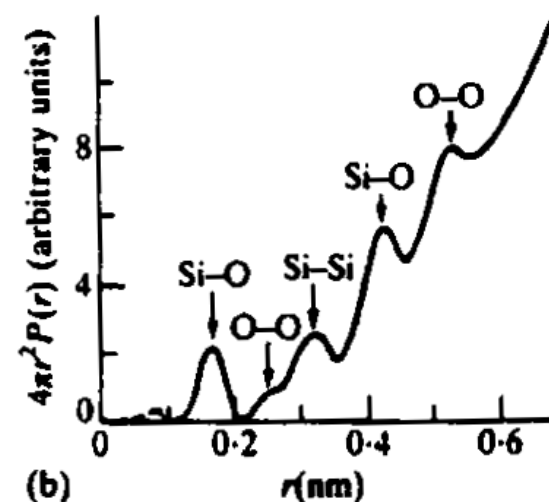
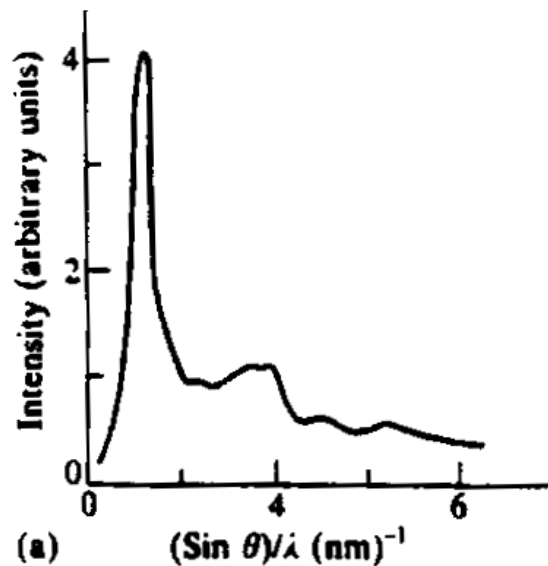
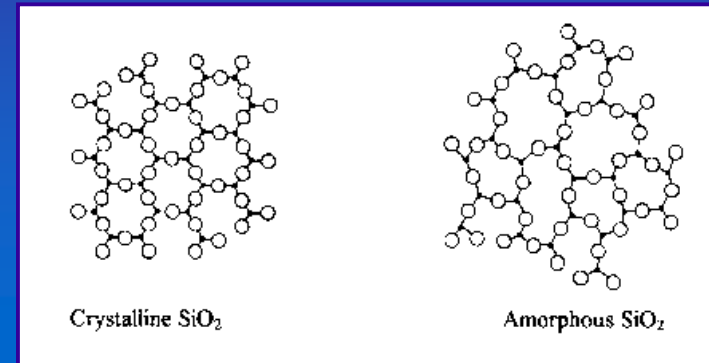
- Narrow peak profiles
- Large number of measurable peaks
- Accurate peak position/intensity
- X-ray energy tuning to adsorption edges



AMORPHOUS PHASE ANALYSIS

The long-range order typical of crystalline structures is absent in amorphous materials. However, a certain degree of short-range order is always present.

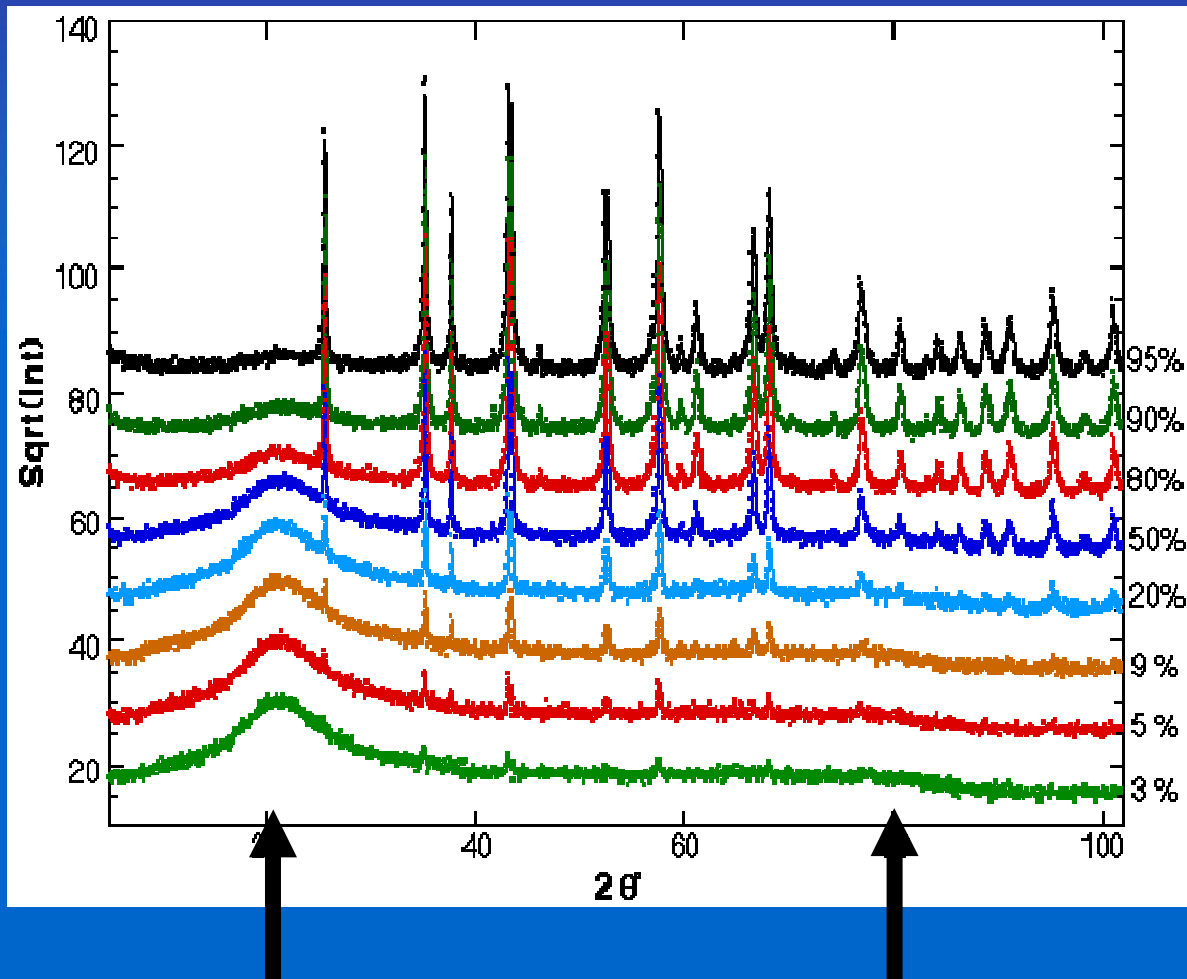
Diffraction can be used to measure the *radial distribution function*, i.e., the probability distribution to find an atom at a distance between r and $r+\delta r$ taken from a reference atom.





AMORPHOUS PHASE ANALYSIS

Mixture of (crystalline) corundum and amorphous silica



amorphous bands typical of the glass

Diffraction can provide:

- **fraction of amorphous phase** in mixtures
- **degree of crystallinity** (e.g. in glass-ceramics or in polymers)



PAIR DISTRIBUTION FUNCTION: USE OF SRXRD

Structure of nanocrystalline materials using atomic Pair Distribution Function (PDF) analysis: study of LiMoS_2 .

V. Petkov *et al.*, Phys. Rev. B 65 (2002) 092105

$$PDF : G(r) = 4\pi r [\rho(r) - \rho_0]$$

TABLE I. Structural parameters for MoS_2 . Space group is $P6_3/mmc$. Mo is at $(\frac{1}{3}, \frac{2}{3}, \frac{1}{4})$ and S at $(\frac{1}{3}, \frac{2}{3}, z)$.

	PDF	Rietveld	Single crystal ^a
a (Å)	3.169(1)	3.168(1)	3.1604(2)
c (Å)	12.324(1)	12.322(1)	12.295(2)
z	0.623(1)	0.625(1)	0.629(1)

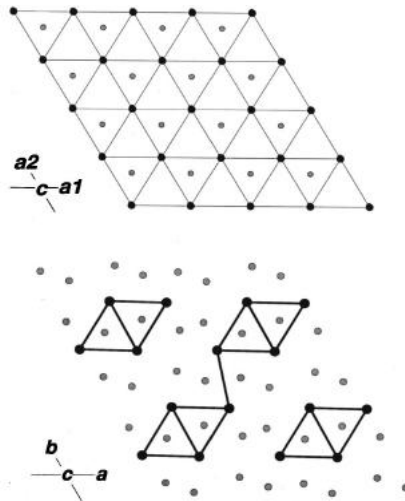


FIG. 4. Projection down the c axis of the crystal structures of hexagonal MoS_2 (up) and triclinic LiMoS_2 (down). The large black circles are Mo atoms and the small gray circles are the S atoms. Li atoms are not shown for the sake of clarity.

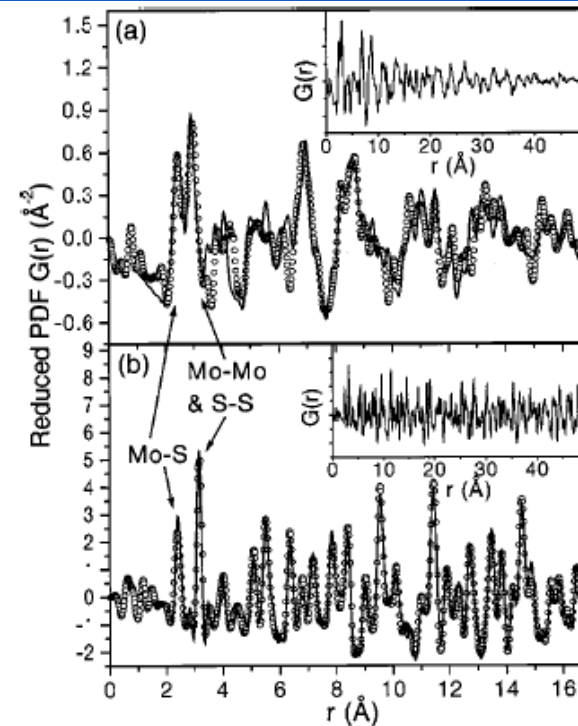
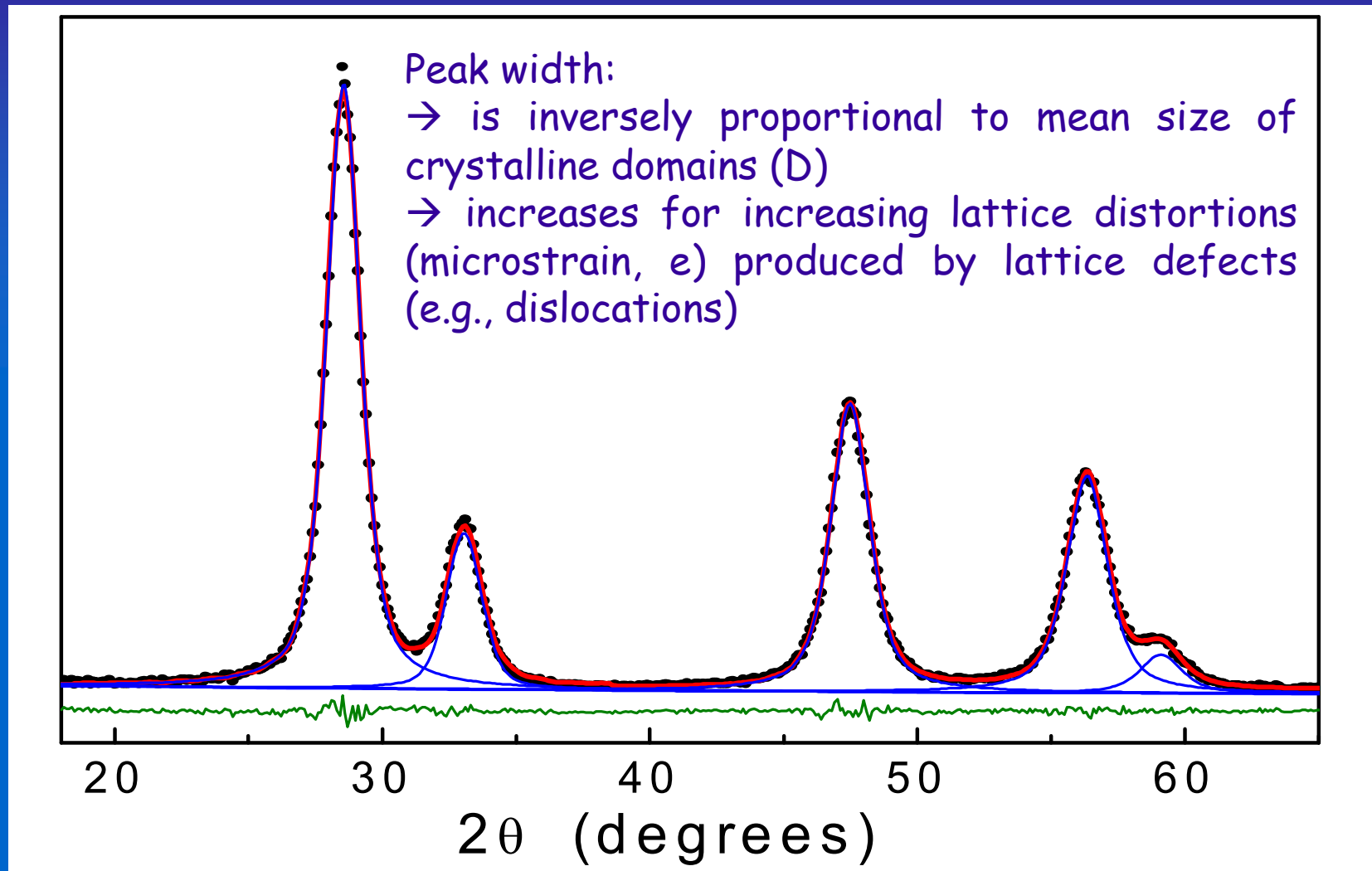


FIG. 2. Experimental (dots) and fitted (solid line) PDF's for LiMoS_2 (a) and MoS_2 (b). Note the different scale between (a) and (b). The first two peaks in the PDF's are labeled with the corresponding atomic pairs. The experimental data are shown in an expanded scale in the insets.



LINE PROFILE ANALYSIS

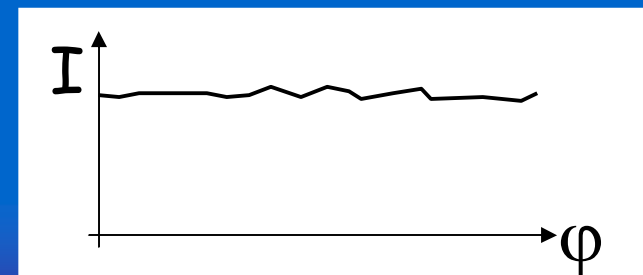
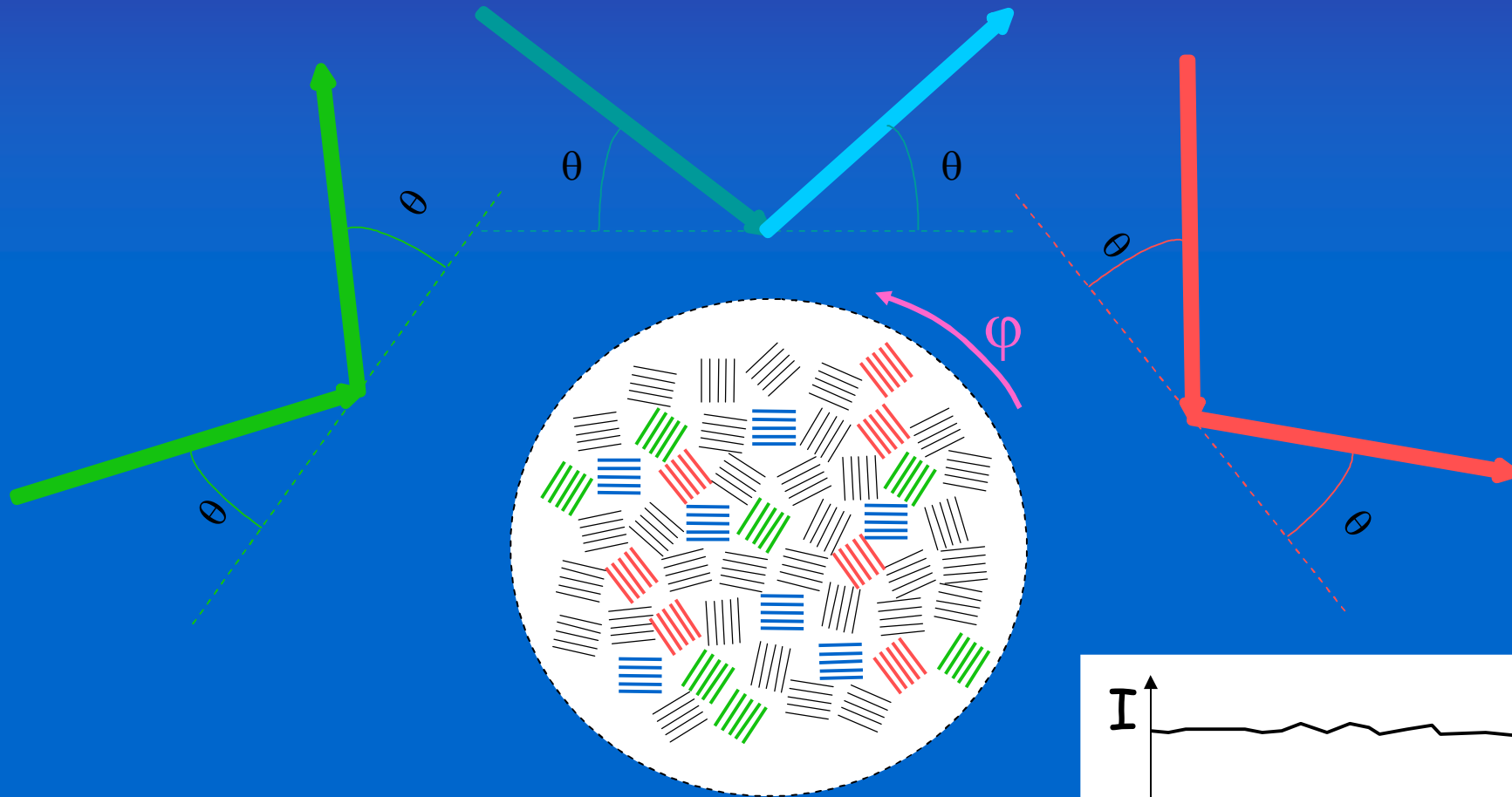


→ LPA: second part of this lecture



TEXTURE ANALYSIS

A 'true' powder has randomly oriented crystalline domains.
The diffracted intensity does not depend on the probing direction.



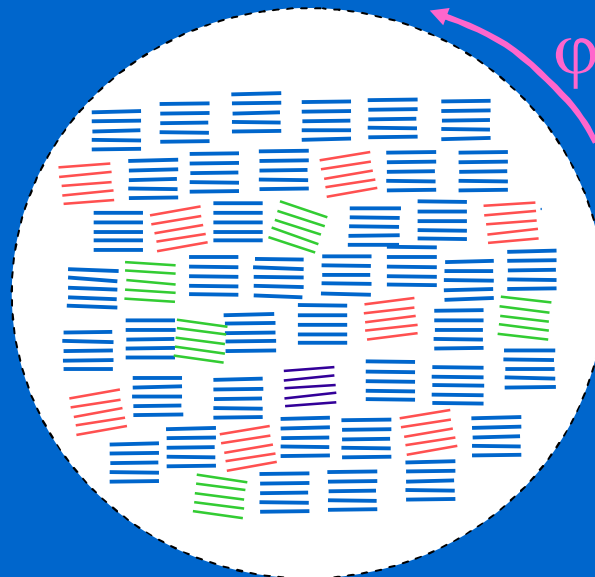
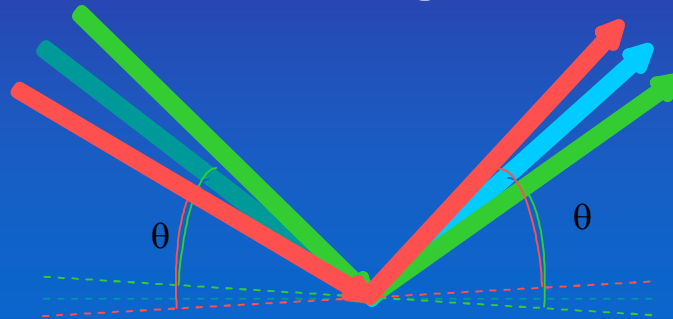
for any hkl

random orientation

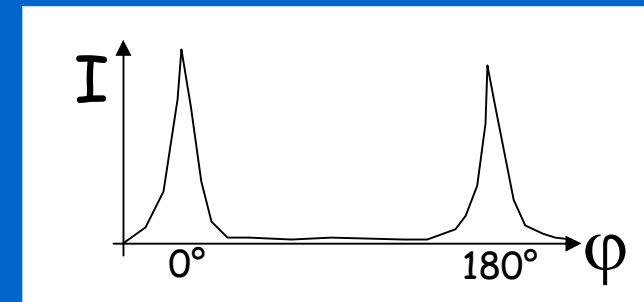


TEXTURE ANALYSIS

If the grain (crystal) orientation is not random, the diffracted signal depends on the incident angle.



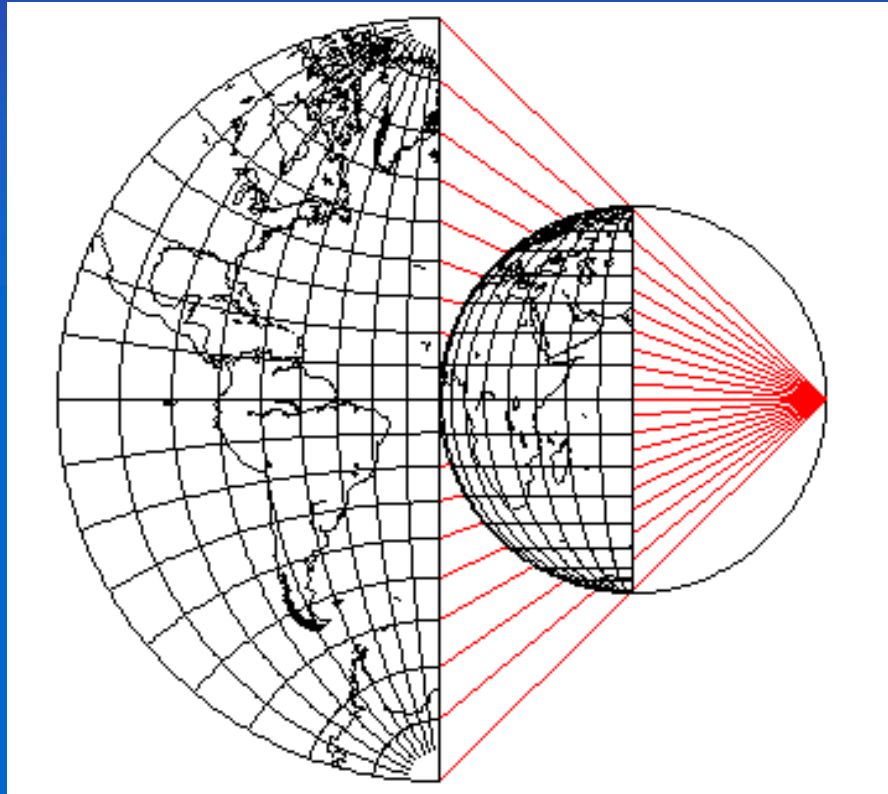
preferred orientation



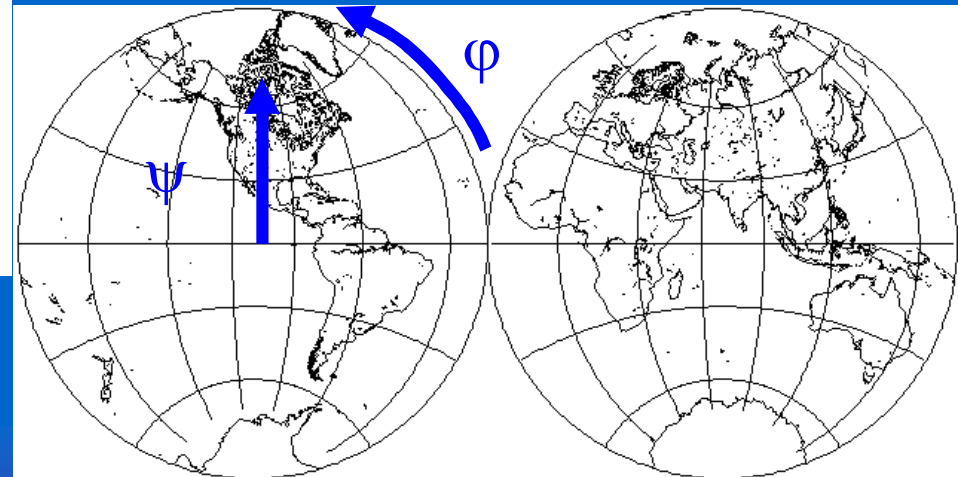


TEXTURE ANALYSIS

The information can be reported on suitable maps: pole figures.
The stereographic projection is adopted



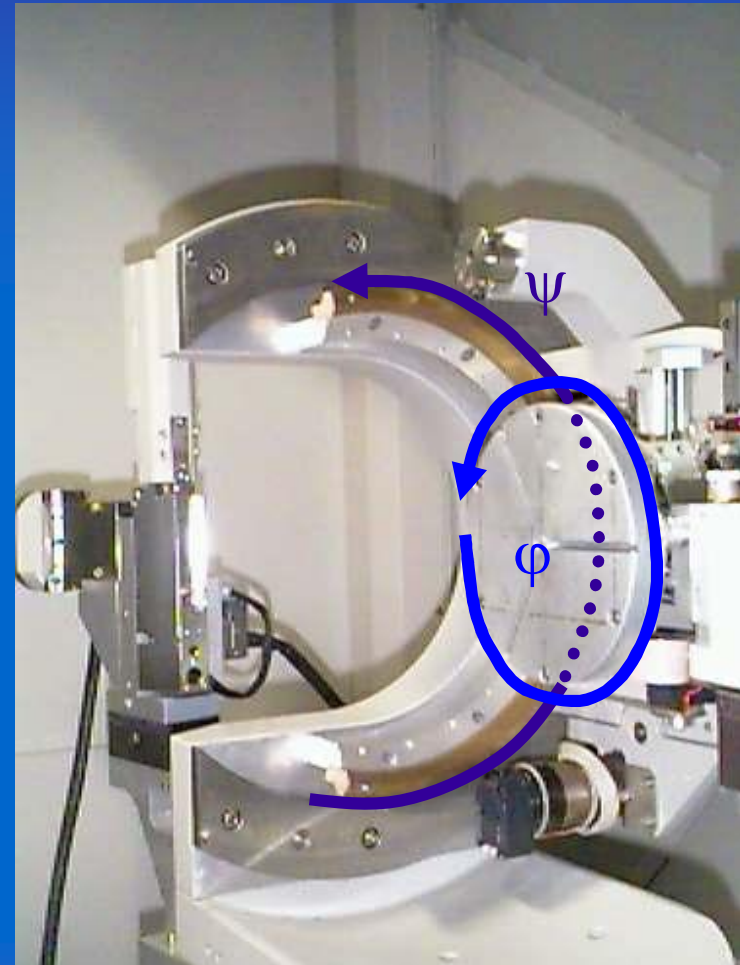
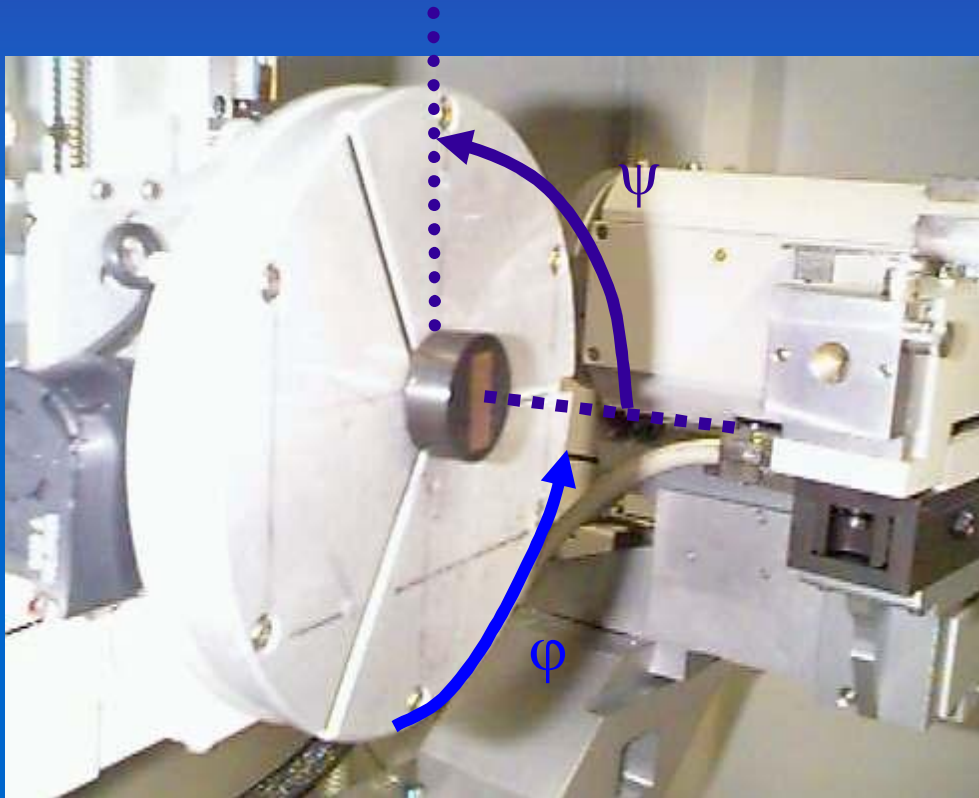
Two angles are used in the projection





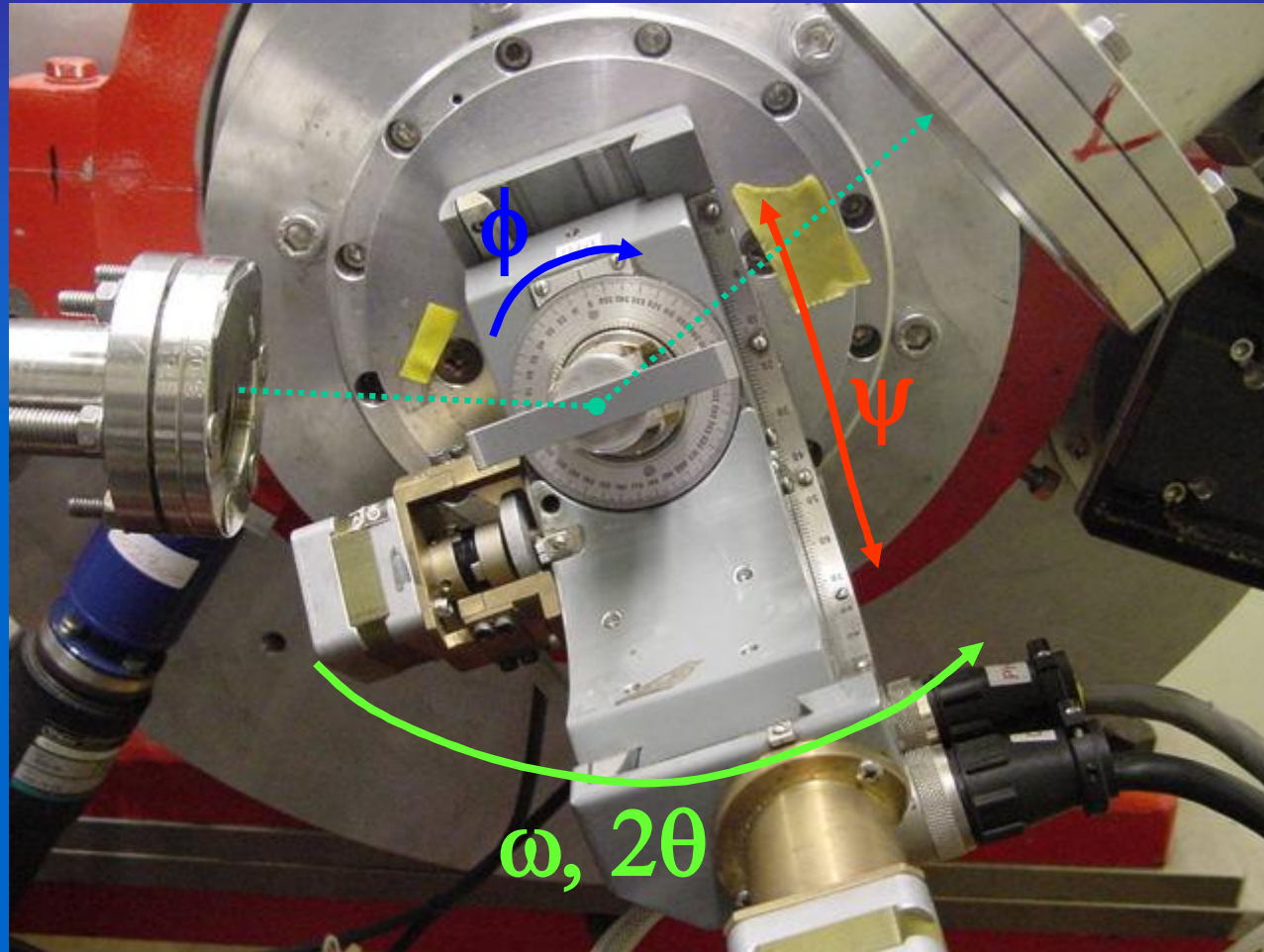
TEXTURE ANALYSIS

Eulerian cradle for stress/texture measurement: laboratory instrum.





TEXTURE & STRESS ANALYSIS BY SRXRD

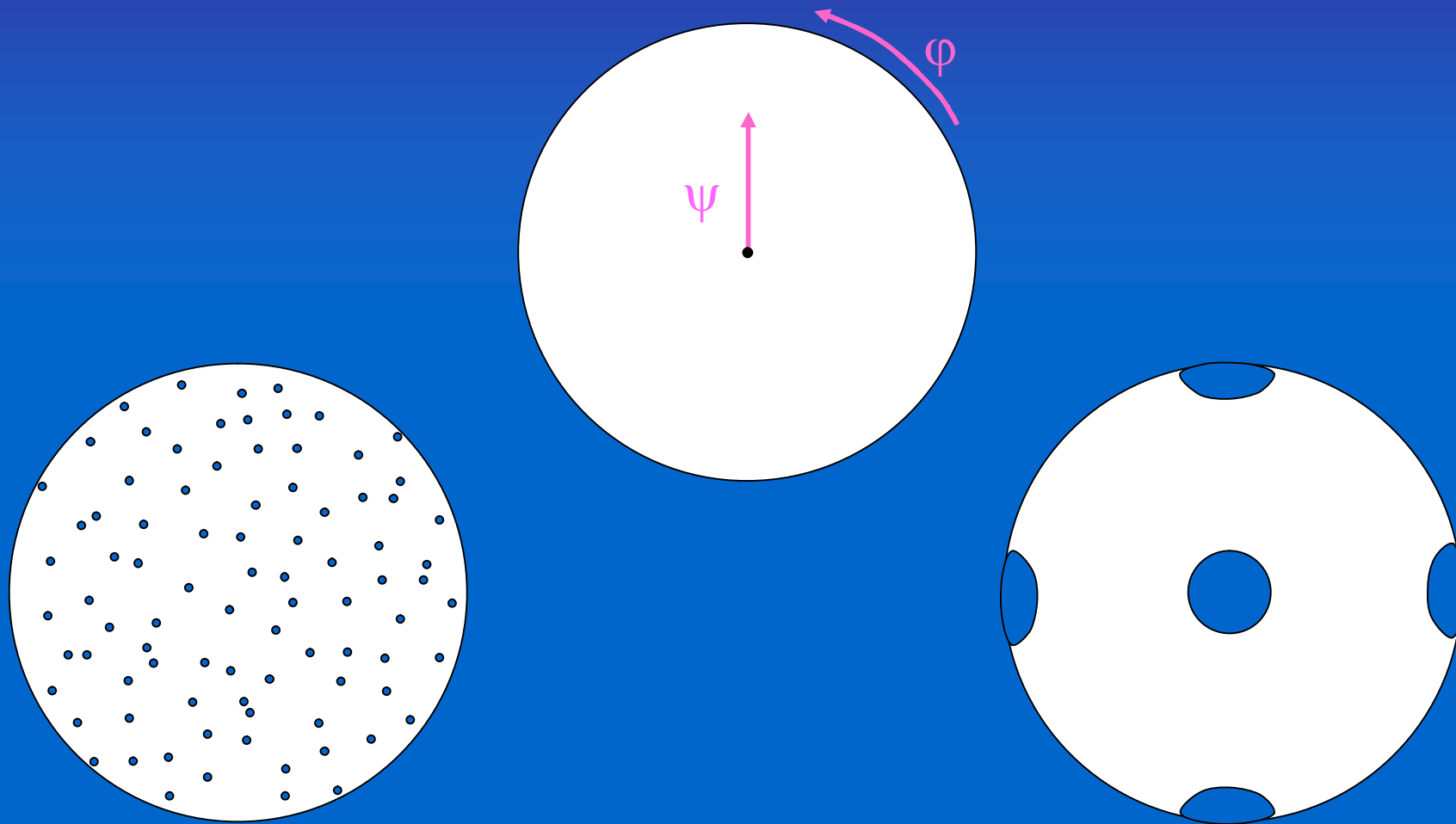


Eulerian cradle for stress/texture measurement: Daresbury beamline 2.3



TEXTURE ANALYSIS

Crystallographic texture: pole figures



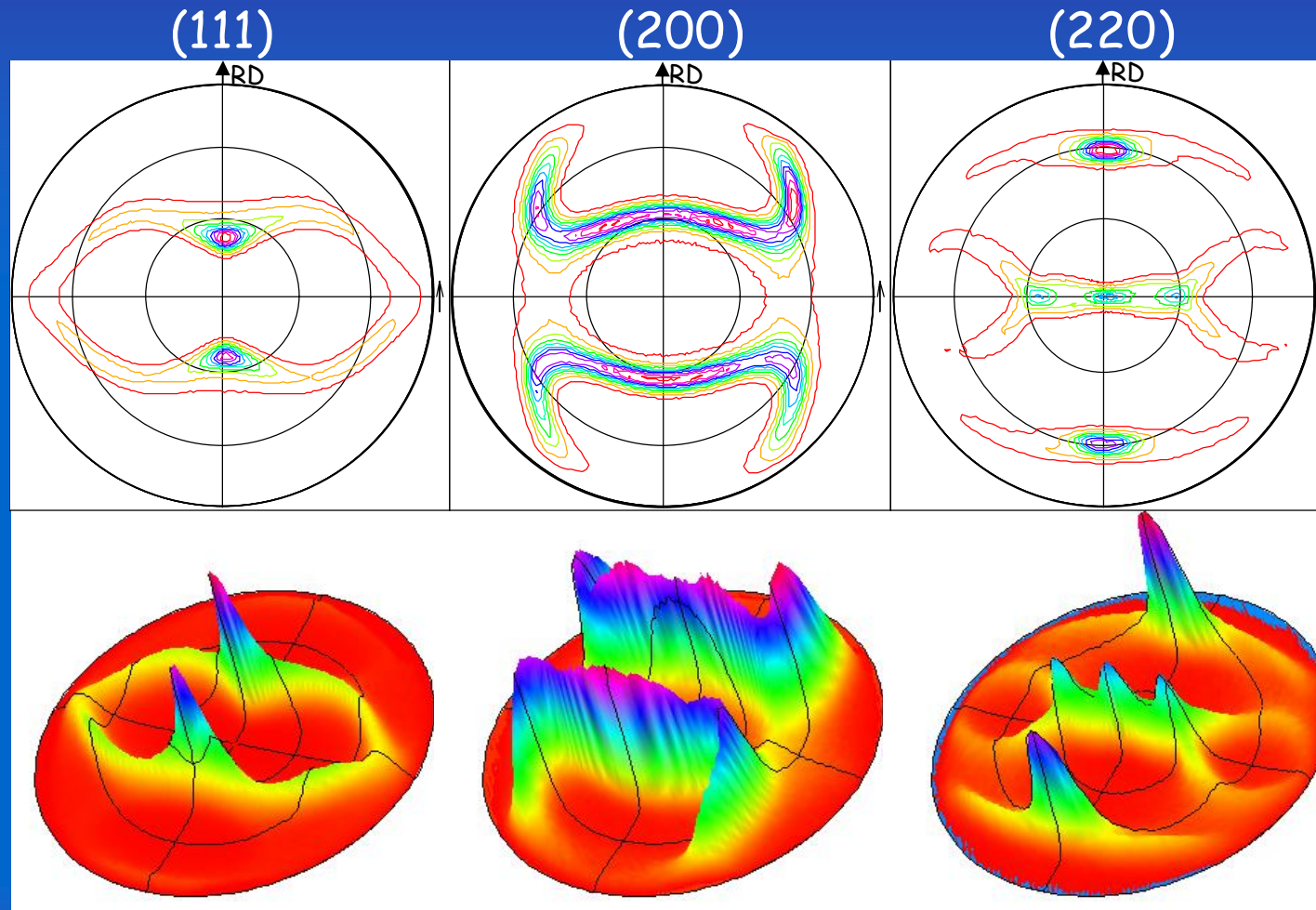
random orientation

preferred orientation



TEXTURE ANALYSIS

In general, texture can be quite complex. Several pole figures, for different (hkl), may be required to understand the orientation



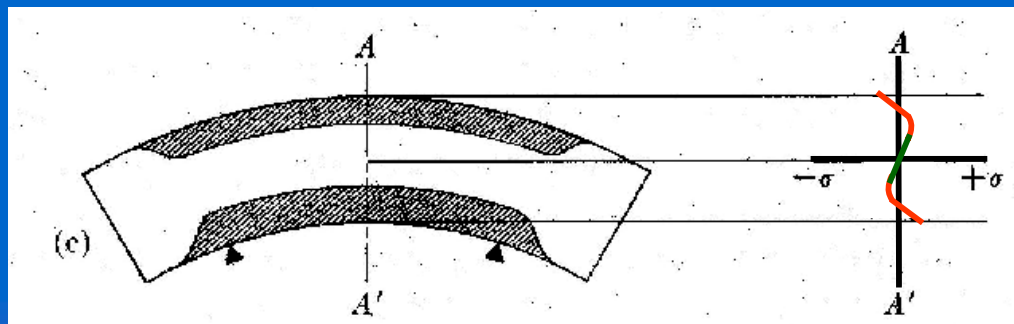
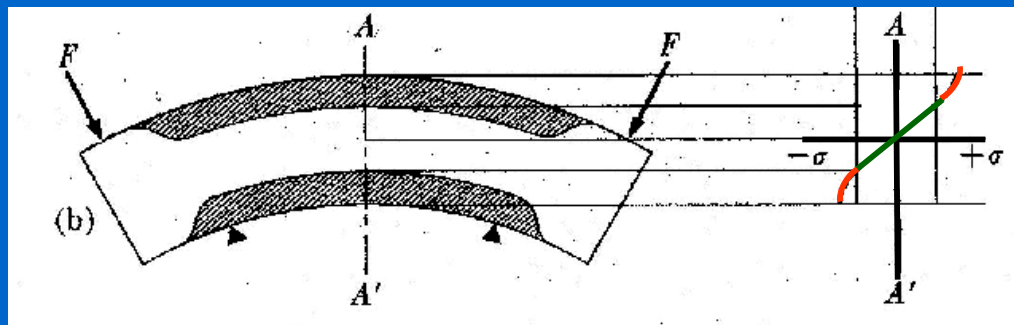
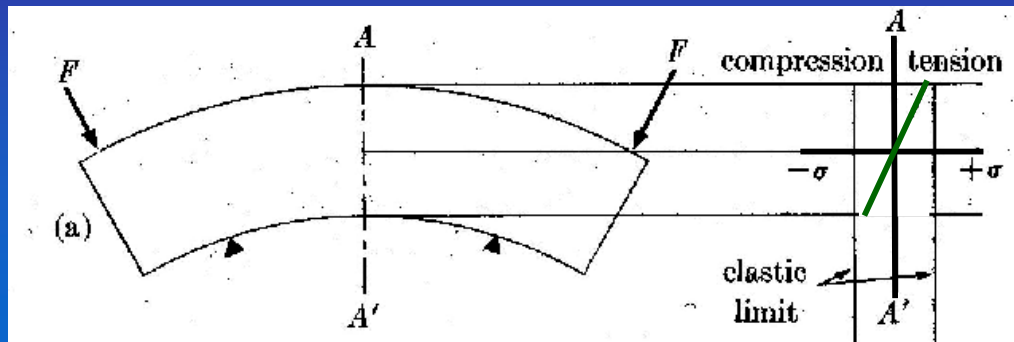
Cold-rolled Ni for high- T_c superconducting wires



RESIDUAL STRESS ANALYSIS

Why residual stresses?

Example: residual stress by plastic flow in bending:



(a) loaded **below** elastic limit

(b) loaded **above** elastic limit

(c) unloaded

Shaded regions have been plastically deformed

Source: B.D. Cullity "Elements of X-ray diffraction" II Edition. Addison-Wesley. Reading (1978)



RESIDUAL STRESS ANALYSIS

Crystalline domains can be used as strain gauges

grain deformation

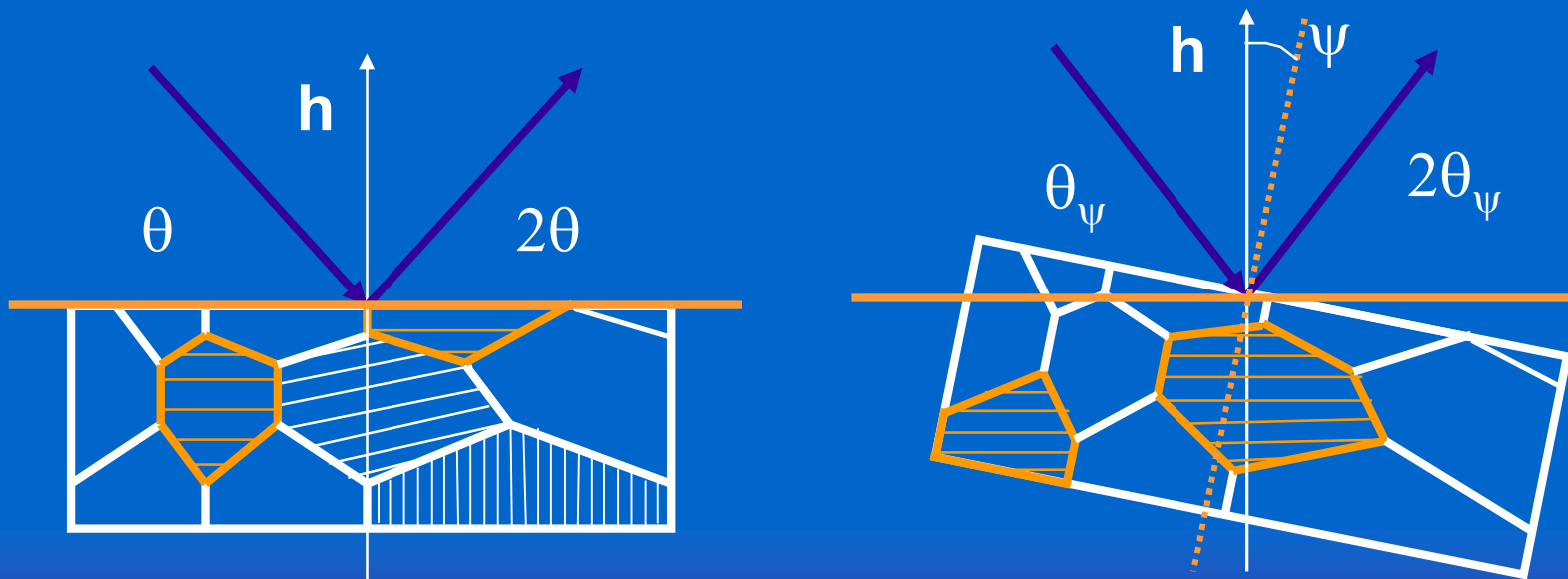
$$\varepsilon = \frac{\Delta l}{l}$$



lattice deformation

$$\varepsilon = \frac{\Delta d}{d}$$

The deformation is measured along different directions, by tilting the sample. The in-plane strain is obtained by measuring d along off-plane directions.





RESIDUAL STRESS ANALYSIS

If the stress field is plane and rotationally symmetric:

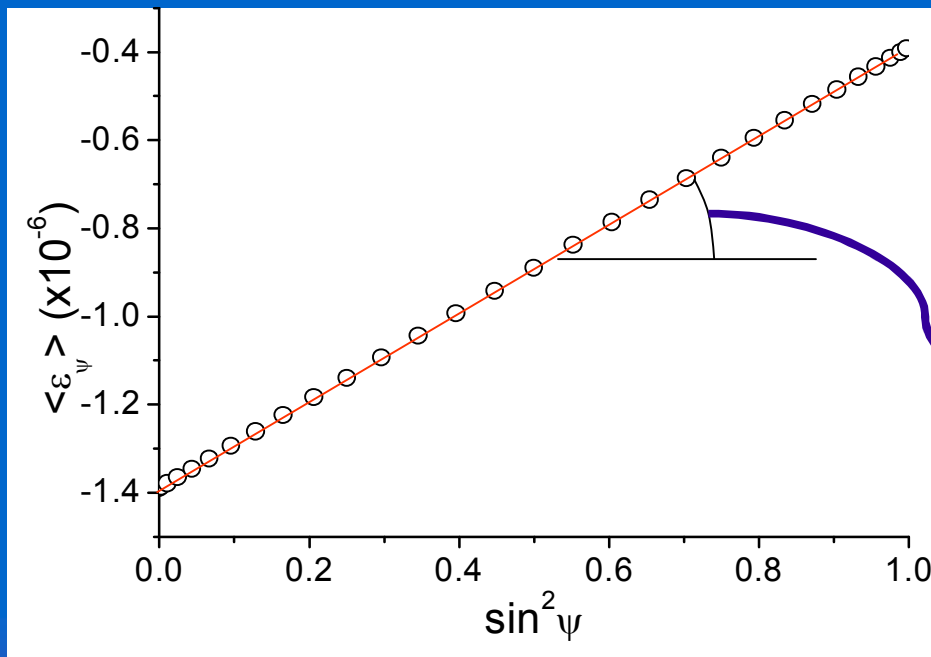
$$\sigma_{11} = \sigma_{22} = \sigma_{\parallel}, \quad \sigma_{12} = \sigma_{13} = \sigma_{23} = \sigma_{33} = 0$$



and if no gradient and no texture are present, then:

$$\langle \varepsilon_{\psi}^{hkl} \rangle = \left(2S_1^{hkl} + \frac{1}{2}S_2^{hkl} \sin^2 \psi \right) \sigma_{\psi}^S$$

"sin²ψ formula"



$$S_1^{hkl}, \quad \frac{1}{2}S_2^{hkl}$$

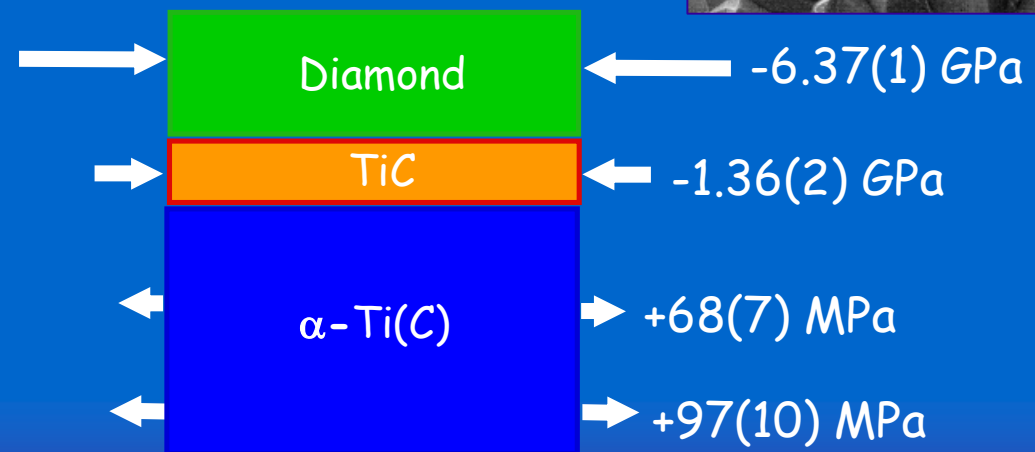
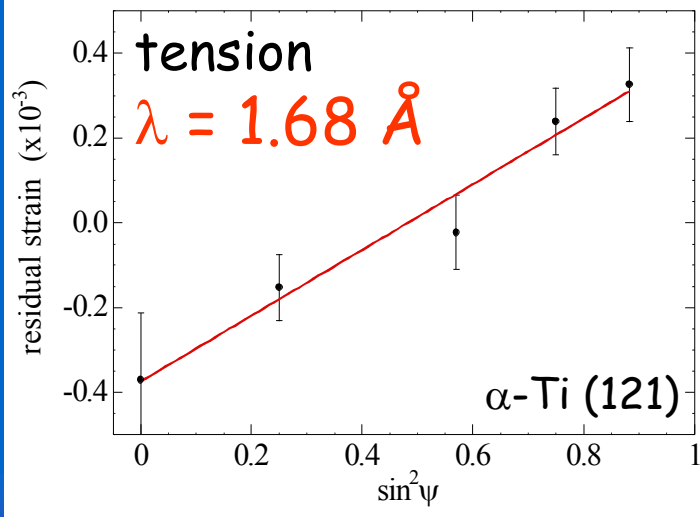
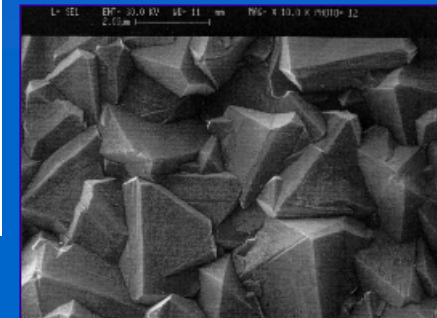
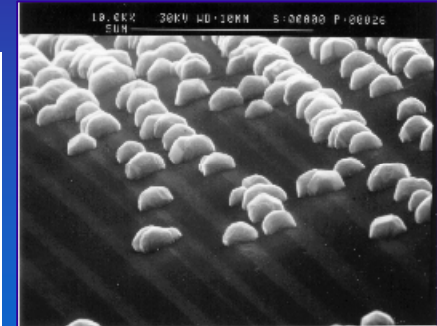
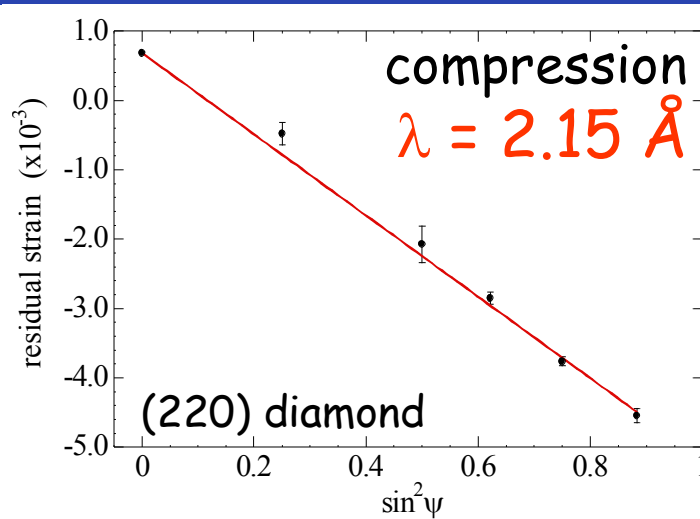
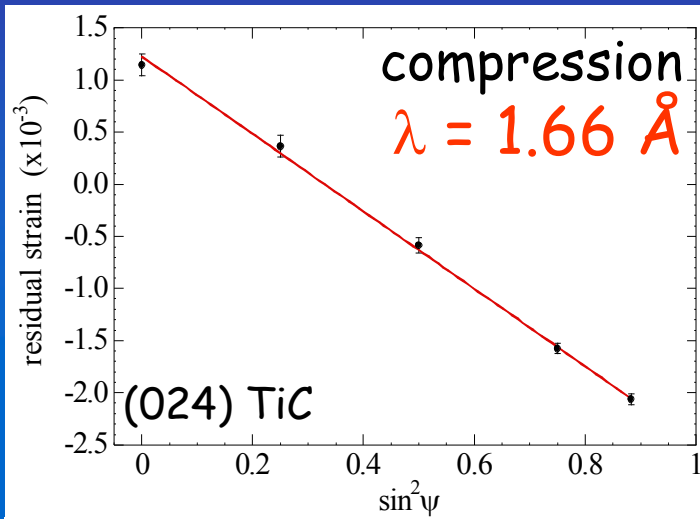
X-ray elastic constants (XECs)

slope related to
the average
in-plane stress



RESIDUAL STRESS GRADIENT BY SRXRD

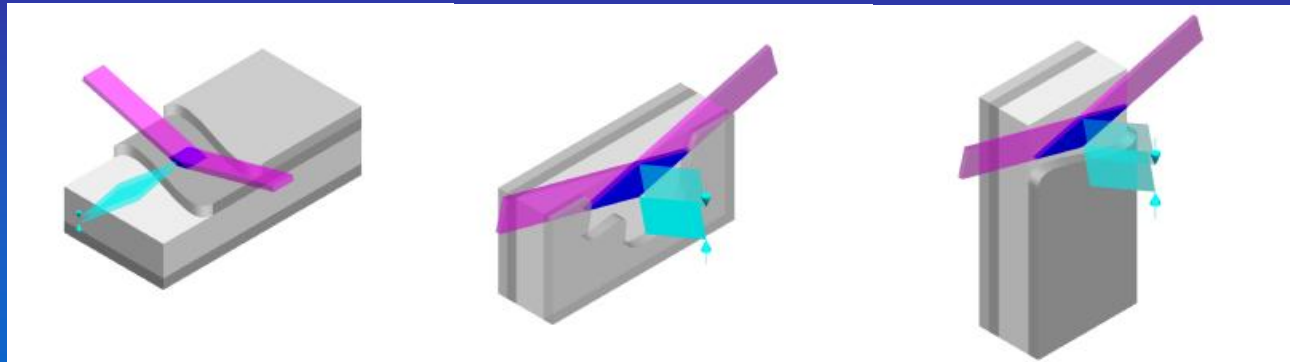
Residual stress in diamond coated components: multiple wavelength XRD



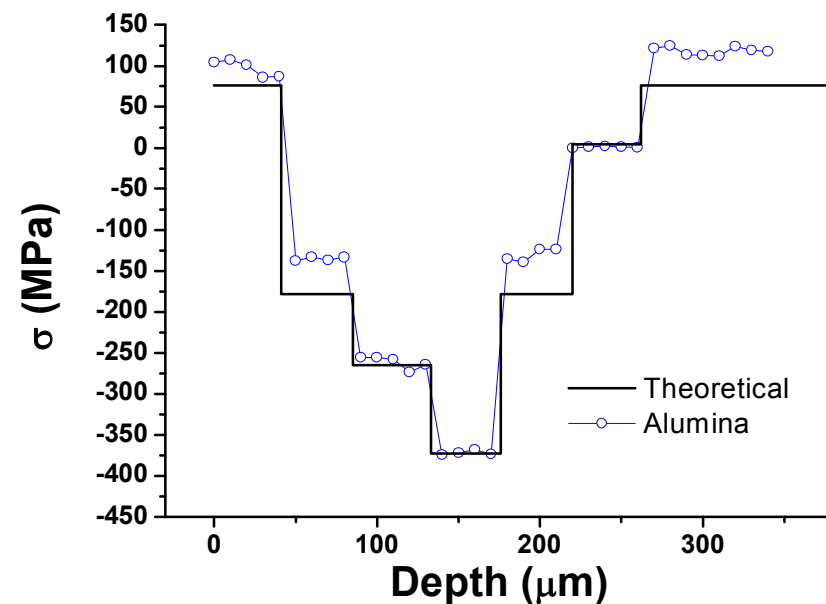
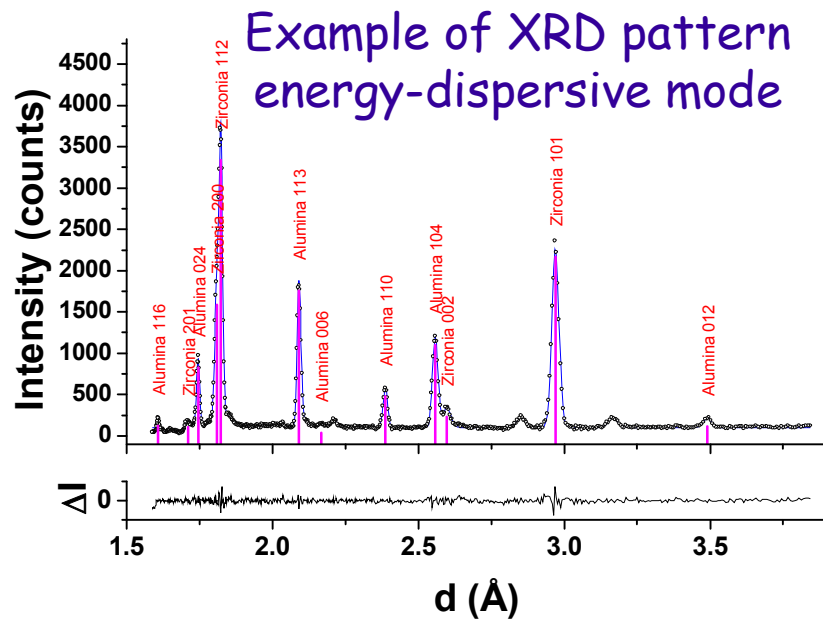


RESIDUAL STRESS GRADIENT BY SRXRD

Possible geometries for through-thickness stress mapping



Residual stress profile in a Alumina-Zirconia-Mullite ceramic laminates





PART 1: REFERENCES

- [1] B.D. Cullity, *Elements of X-ray Diffraction*, Addison-Wesley, Reading MA, 1978.
- [2] R. Jenkins & R. L. Snyder, *Introduction to X-ray Powder Diffractometry*, Wiley, New York, 1996
- [3] H.P. Klug & L.E. Alexander, *X-ray Diffraction procedures*, Wiley, New York, 1974.
- [4] B.E. Warren, *X-ray Diffraction*, Addison-Wesley, Reading, MA, 1969.
- [5] R.A. Young (Ed.), *The Rietveld method*, Oxford University Press, Oxford, 1993.
- [6] R.E. Dinnebier and S.J.L. Billinge (Eds.), *Powder Diffraction: Theory and Practice*, The Royal Society of Chemistry, Cambridge, 2008.
- [7] International Tables for X-ray Crystallography, 3rd series. [Kluwer Academic Publishers](http://www.kluweronline.com), Dordrecht, Boston, London. Vol.A (1983), Vol.B (1993), Vol.C (1992), "Brief Teaching Edition of Volume A" (1985).
- [8] P.P. Ewald, *Fifty years of X-ray Diffraction*, Reprinted in pdf format for the IUCr XVIII Congress, Glasgow, Scotland. Copyright © 1962, 1999 International Union of Crystallography, Chester, UK.
- [9] International Union of Crystallography: <http://www.iucr.org>
- [10] International Centre for Diffraction Data, Newtown Square, PA, USA. <http://www.icdd.com>



PRESENTATION OUTLINE

PART 1

- Basic elements of crystallography and X-ray diffraction (XRD) theory
 - Some advantages and peculiarities of synchrotron radiation XRD (SRXRD)
-

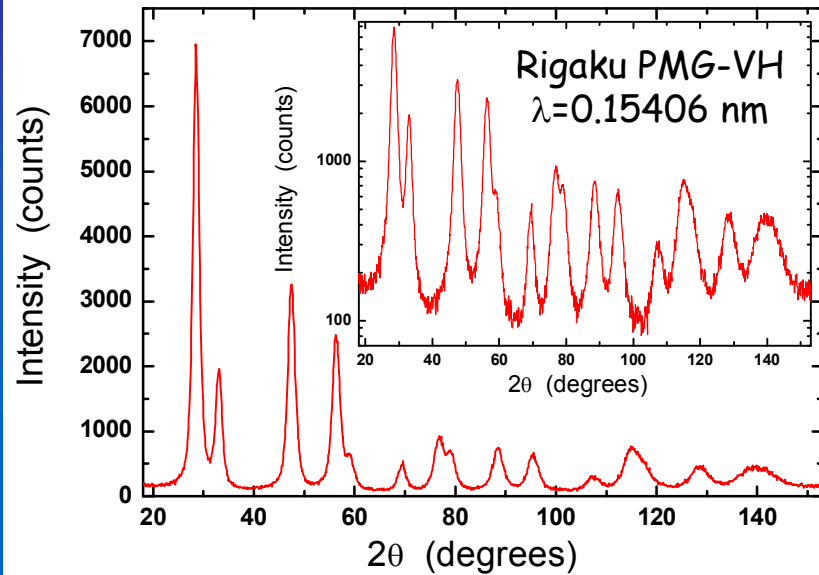
PART 2

- SRXRD from nanocrystalline and highly deformed materials

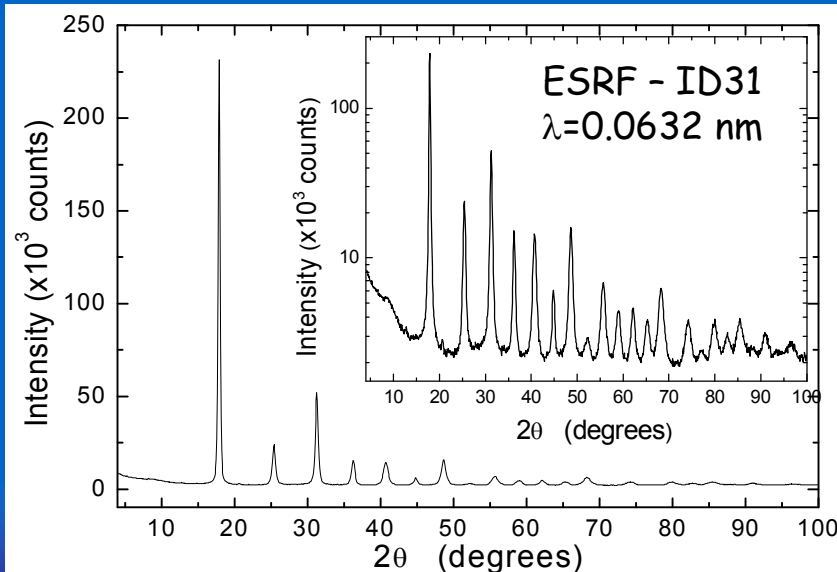
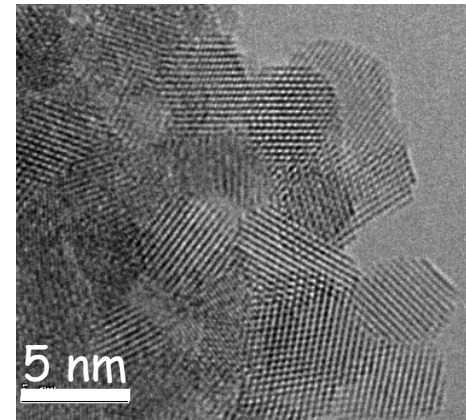


NANOCRYSTALLINE & HEAVILY DEFORMED MATERIALS

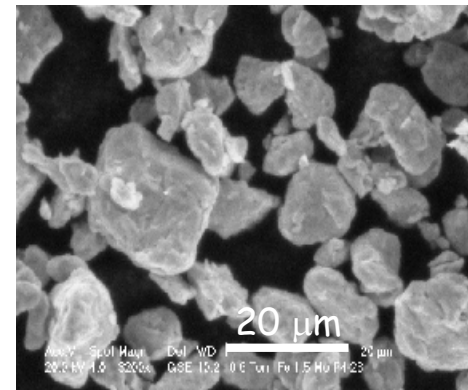
Two typical cases of study



Cerium oxide powder from xerogel



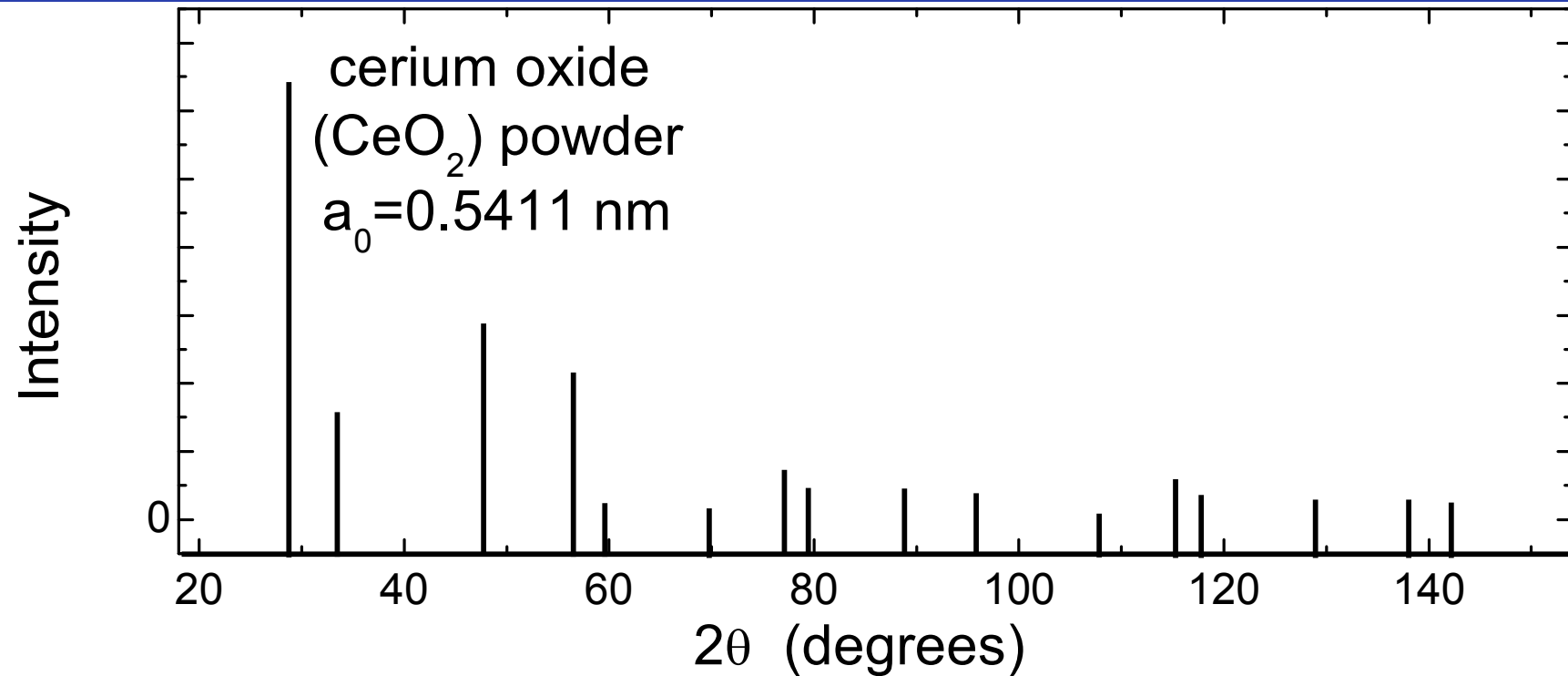
Ball milled Fe-1.5%Mo





DIFFRACTION PATTERN FROM A POLYCRYSTALLINE

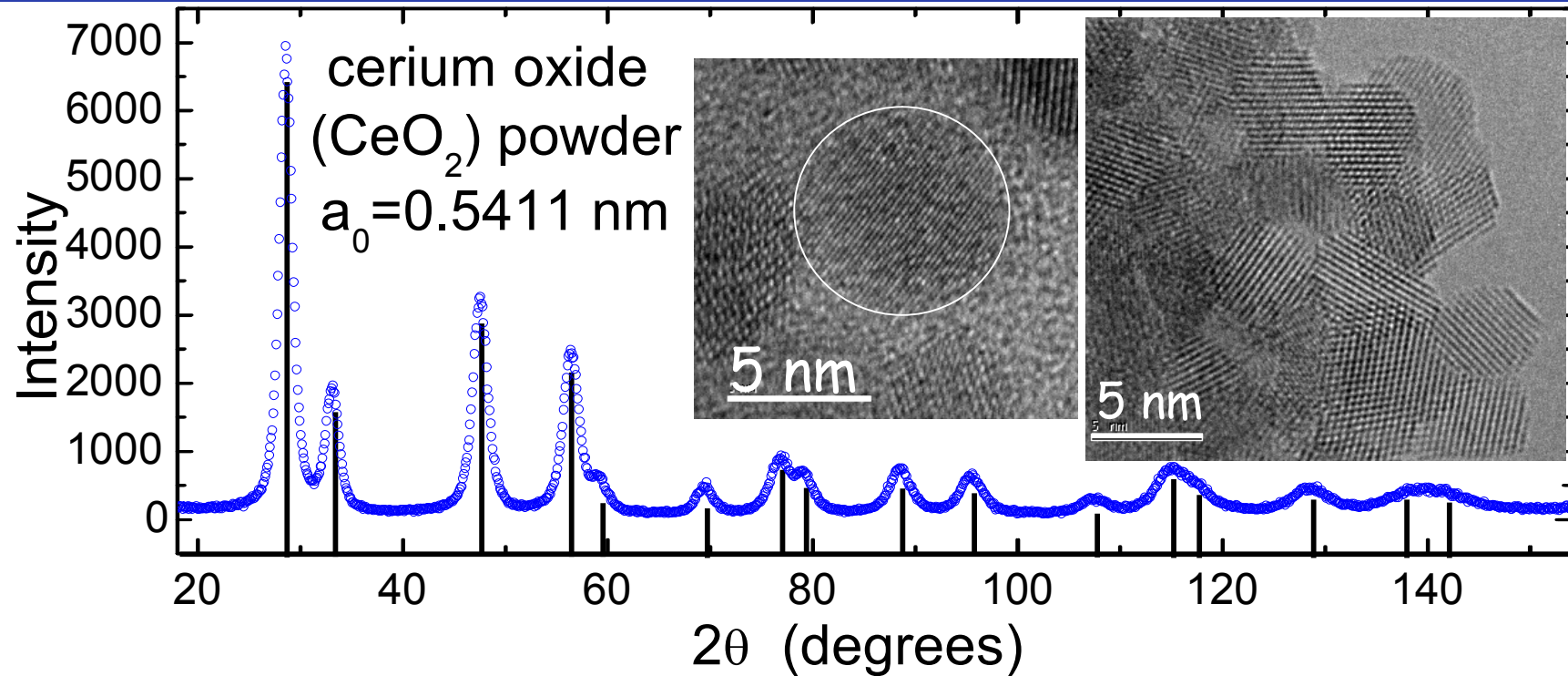
According to Bragg's law, peaks are δ -functions (infinitely narrow)





DIFFRACTION PATTERN FROM A POLYCRYSTALLINE

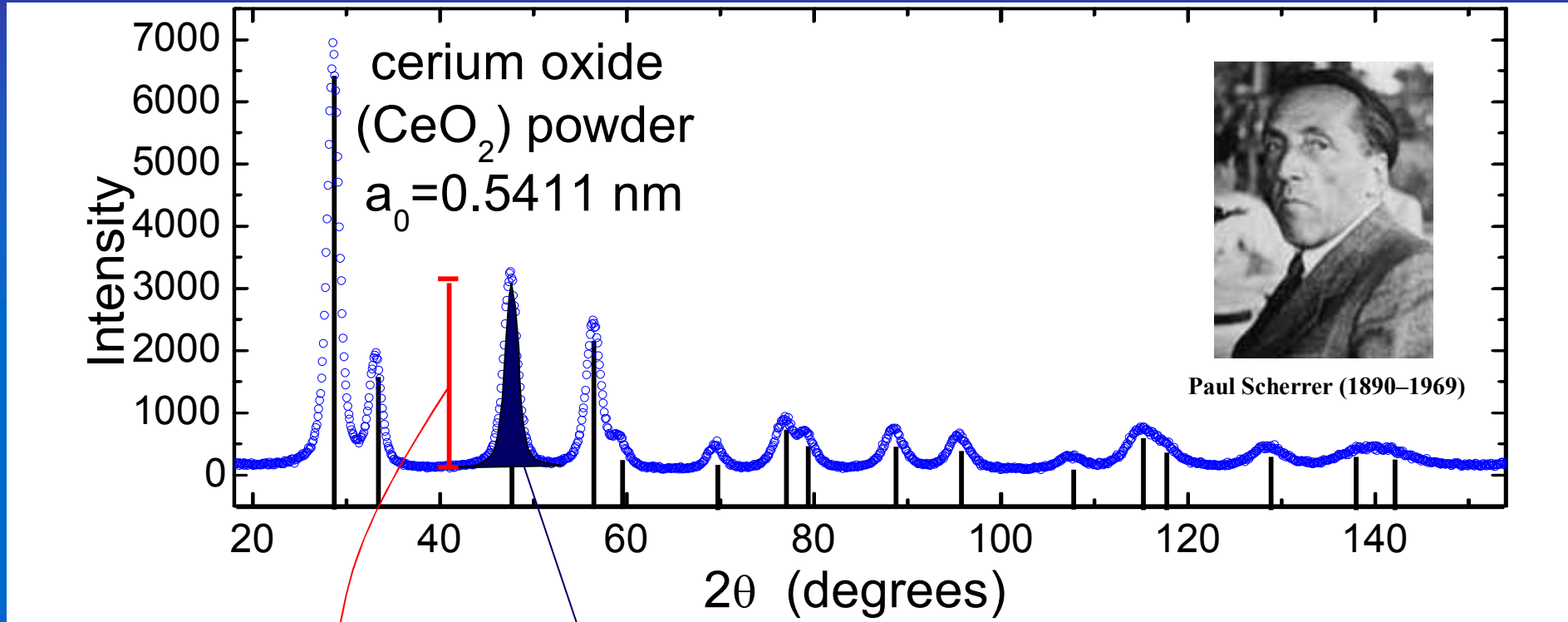
Actually, Bragg peaks from real (nanocrystalline) materials are broadened





DIFFRACTION PATTERN FROM A POLYCRYSTALLINE

Integral Breadth (area/intensity) as a measurement of peak broadening



Integral Breadth

$$\beta = \frac{\int I(2\theta) d2\theta}{I(2\theta_B)} = \frac{\lambda}{L \cos \theta}$$

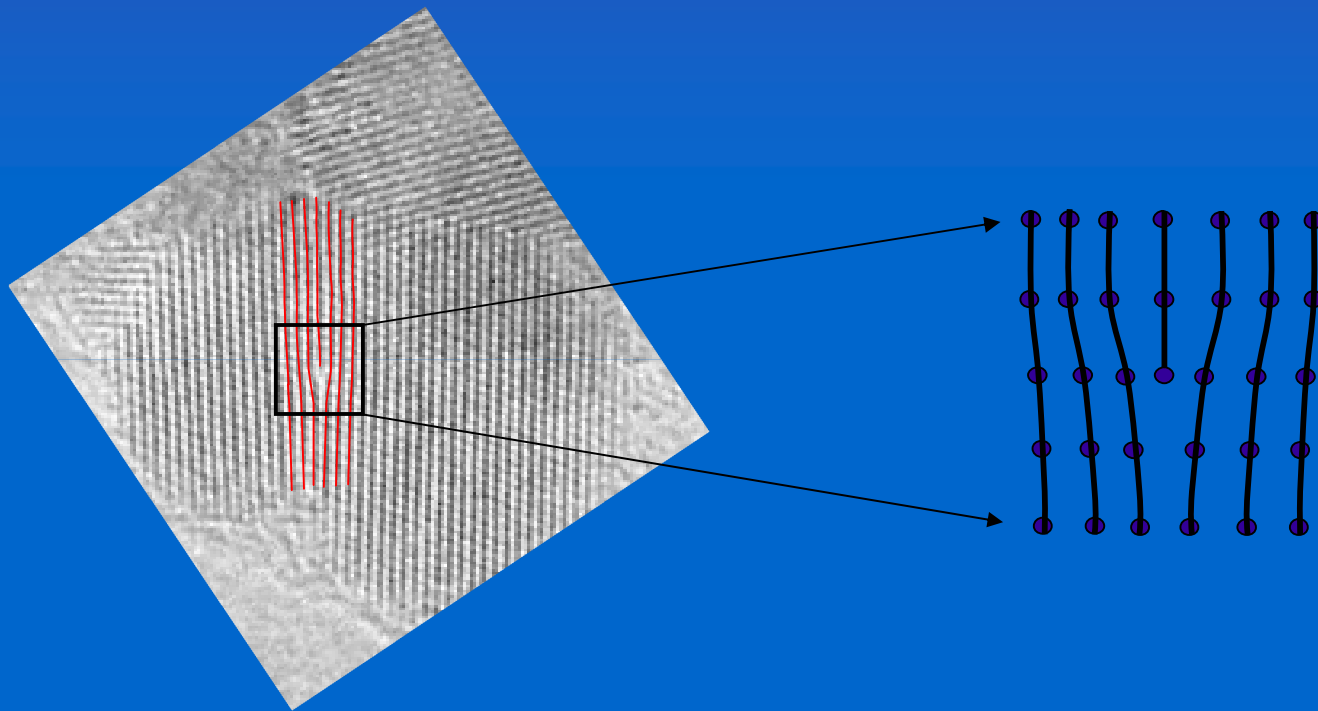
Scherrer formula
(1918)

L: effective crystalline domain size (*L* ≈ 1 - 200 nm)



STRAIN BROADENING: DISLOCATIONS

Lattice defects may also cause line broadening: e.g., dislocations

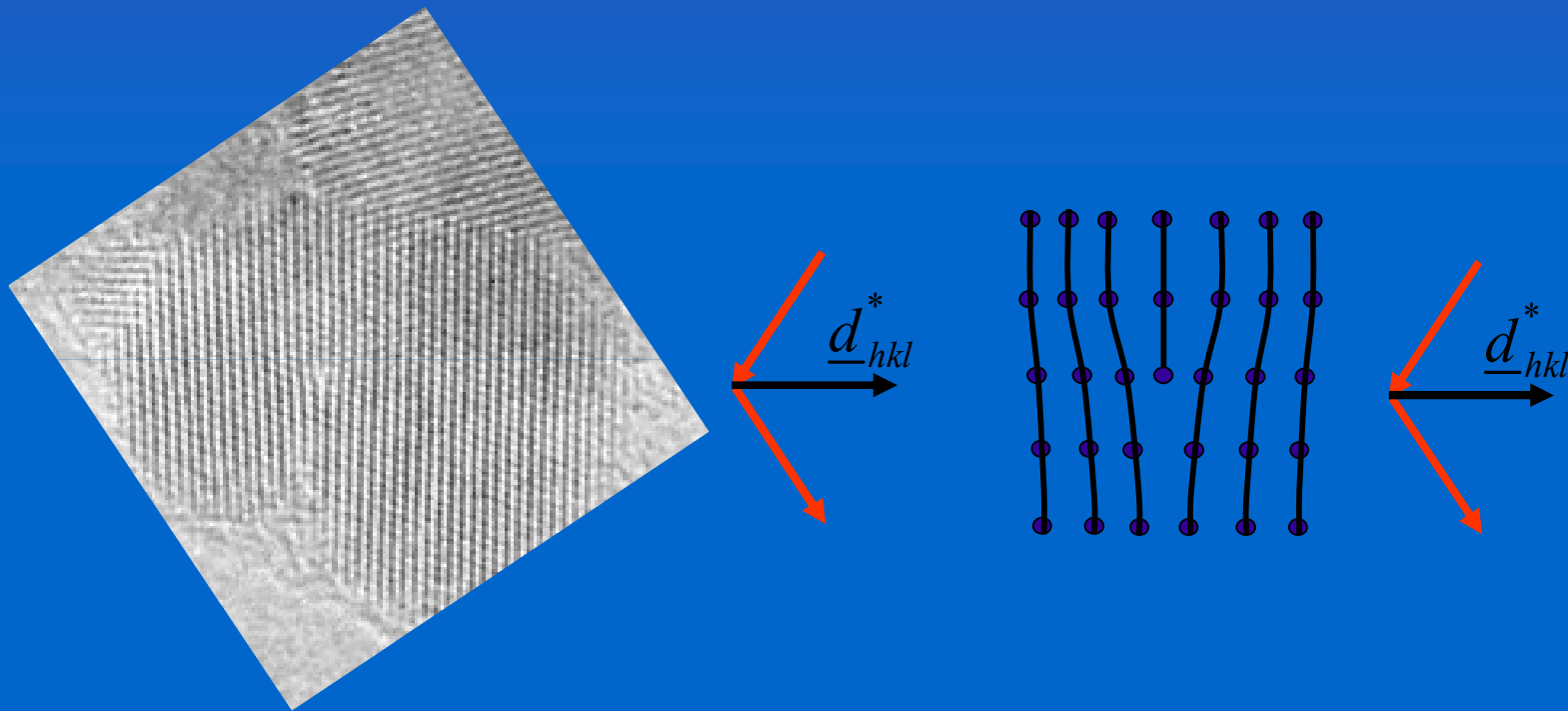


Edge dislocation in a crystalline nanograin



STRAIN BROADENING: DISLOCATIONS

Lattice defects may also cause line broadening: e.g., dislocations

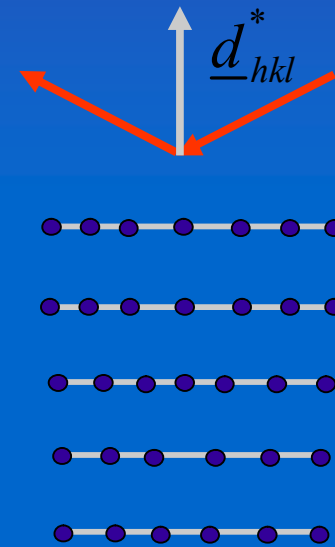
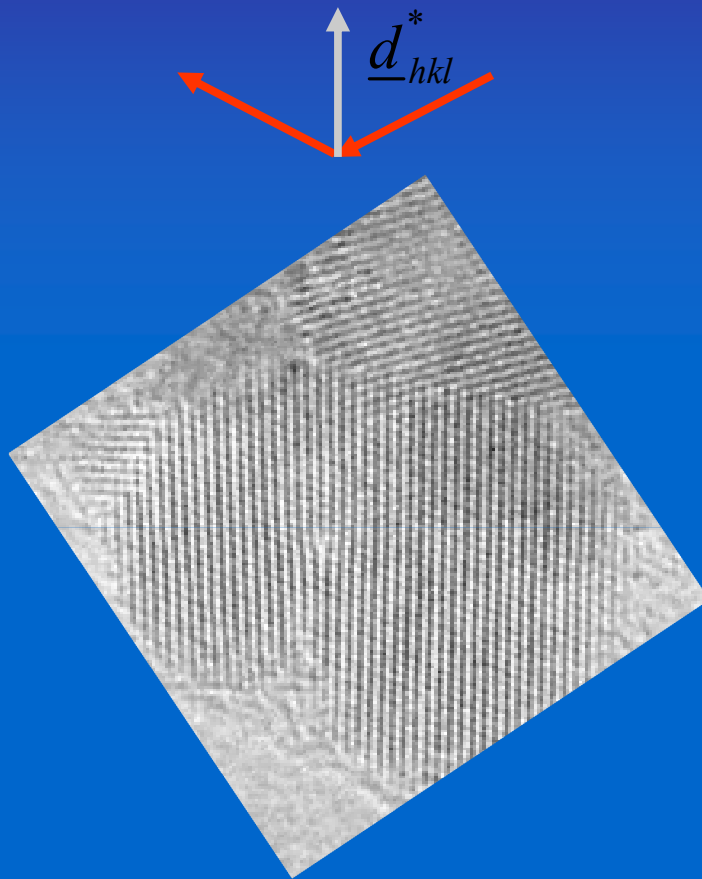


Dislocation "visibility" depends on the viewing direction (d_{hkl}^*)
→ line broadening anisotropy



STRAIN BROADENING: DISLOCATIONS

Lattice defects may also cause line broadening: e.g., dislocations



'invisible'

Dislocation "visibility" depends on the viewing direction (d_{hkl}^*)
→ line broadening anisotropy



MICROSTRAIN EFFECT IN POWDER DIFFRACTION

Heuristic approach: differentiate Bragg's law (with $\lambda = \text{constant}$):

$$0 = 2\Delta d \sin(\theta) + 2d \cos(\theta) \Delta(\theta)$$

Introducing the strain: $\varepsilon = \Delta d/d$

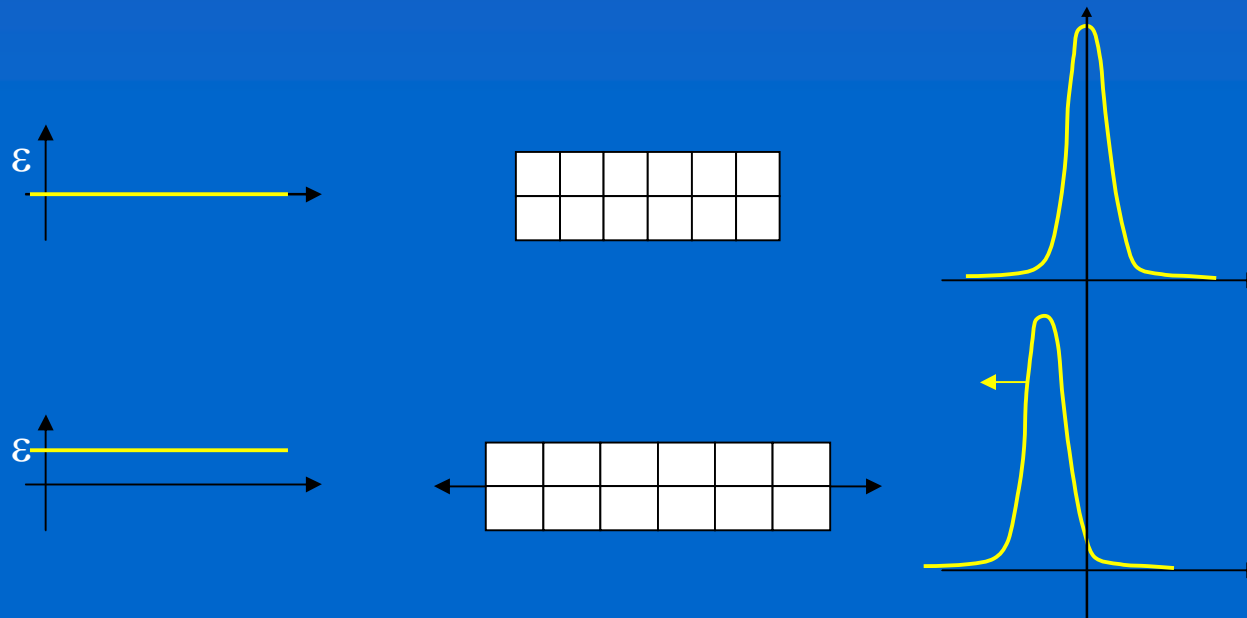
$$\Delta(2\theta) = -2 \tan(\theta) \frac{\Delta d}{d} = -2\varepsilon \tan(\theta)$$



MICROSTRAIN EFFECT IN POWDER DIFFRACTION

A uniform strain, gives a *shift* in diffraction peak position:

$$\Delta(2\theta) = -2\varepsilon \tan(\theta)$$



⇒ *Residual strain/stress analysis*

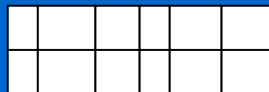
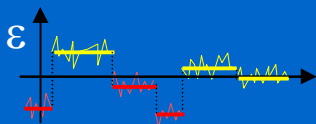
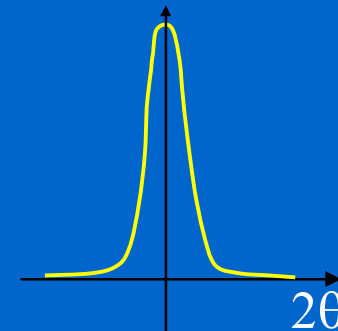
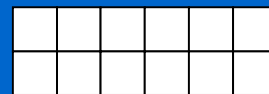


MICROSTRAIN EFFECT IN POWDER DIFFRACTION

Non-uniform strain gives a distribution $p_L(\varepsilon)$. Mean strain can be zero (e.g. in a powder), even if a microstrain (r.m.s. strain) is present:

$$\langle \varepsilon^2 \rangle^{1/2} = \langle (\Delta d/d)^2 \rangle^{1/2}$$

$$\Delta(2\theta) = -2\varepsilon \tan(\theta) \implies \beta(2\theta) \approx 2 \langle \varepsilon^2 \rangle^{1/2} \tan \theta$$

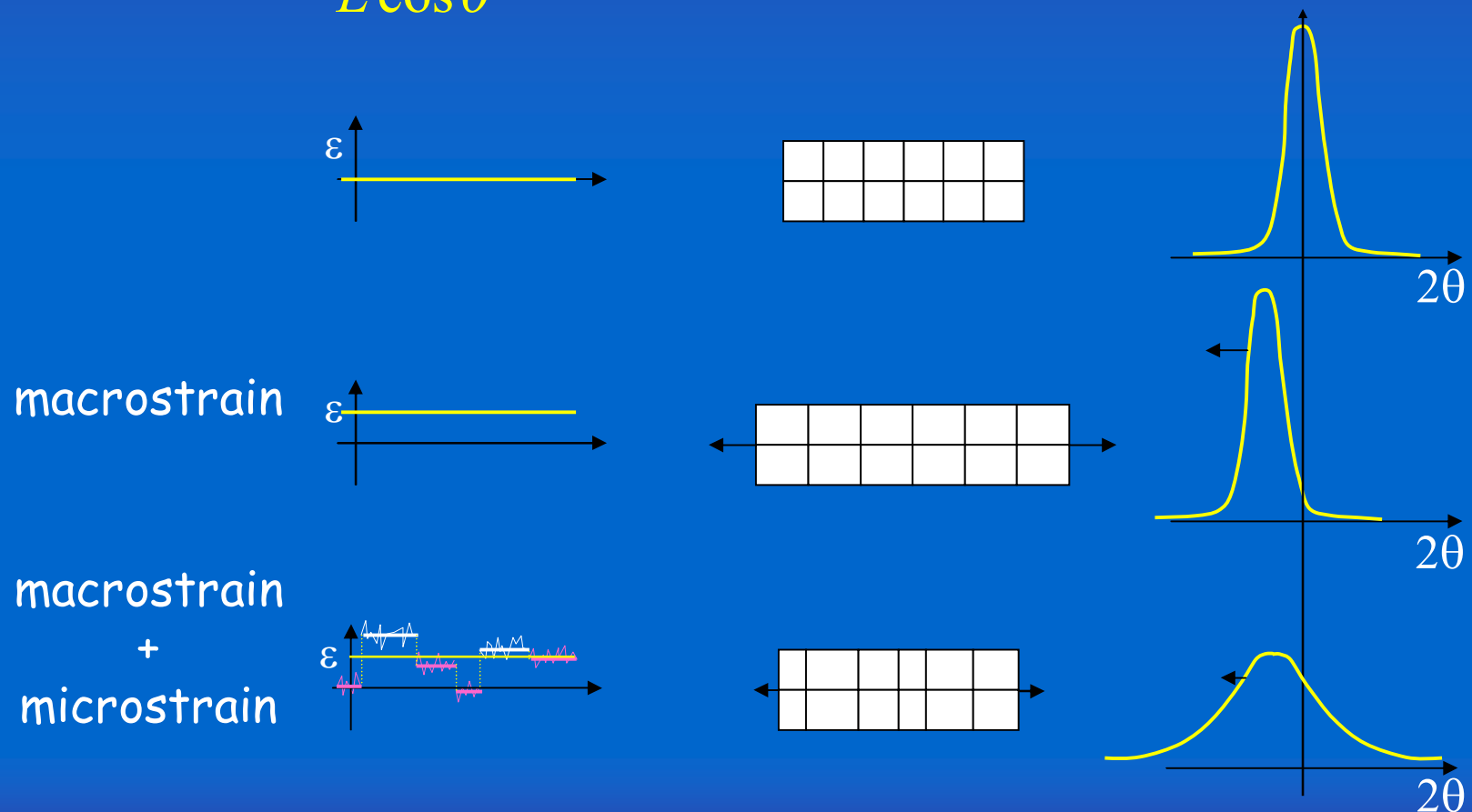




SIZE - STRAIN EFFECT IN POWDER DIFFRACTION

Combined effects - domain size and lattice distortions

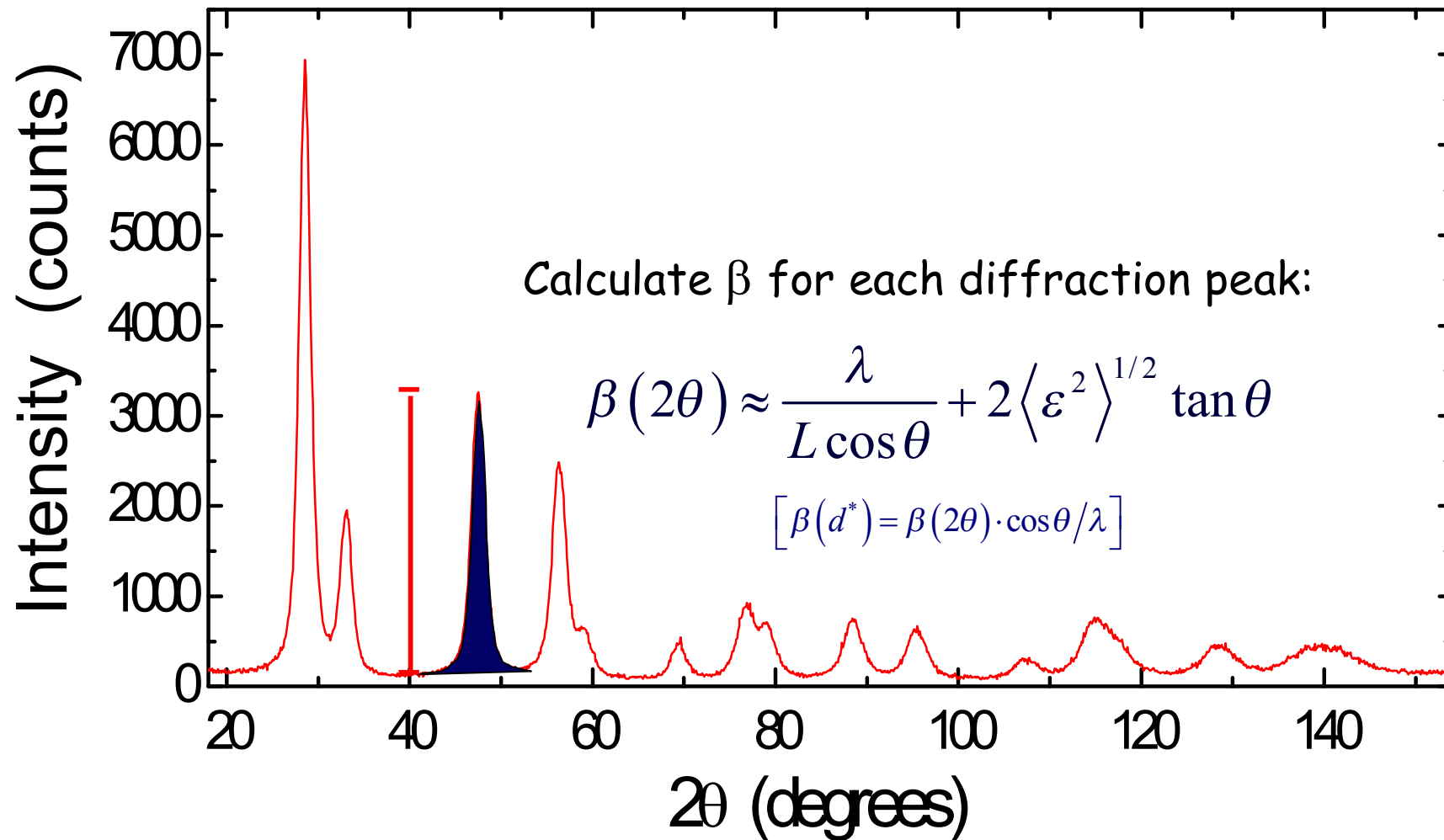
$$\beta(2\theta) \approx \frac{\lambda}{L \cos \theta} + 2 \langle \varepsilon^2 \rangle^{1/2} \tan \theta$$





INTEGRAL BREADTH METHODS

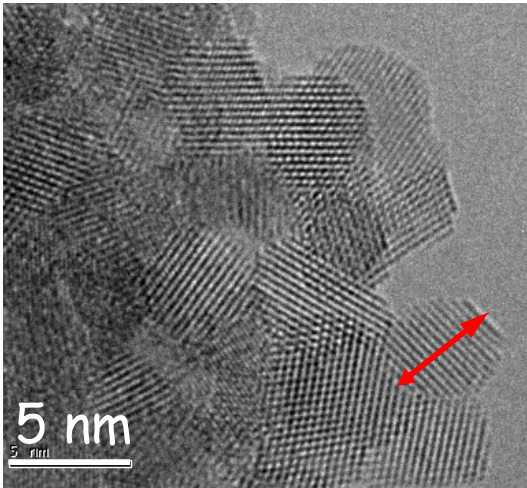
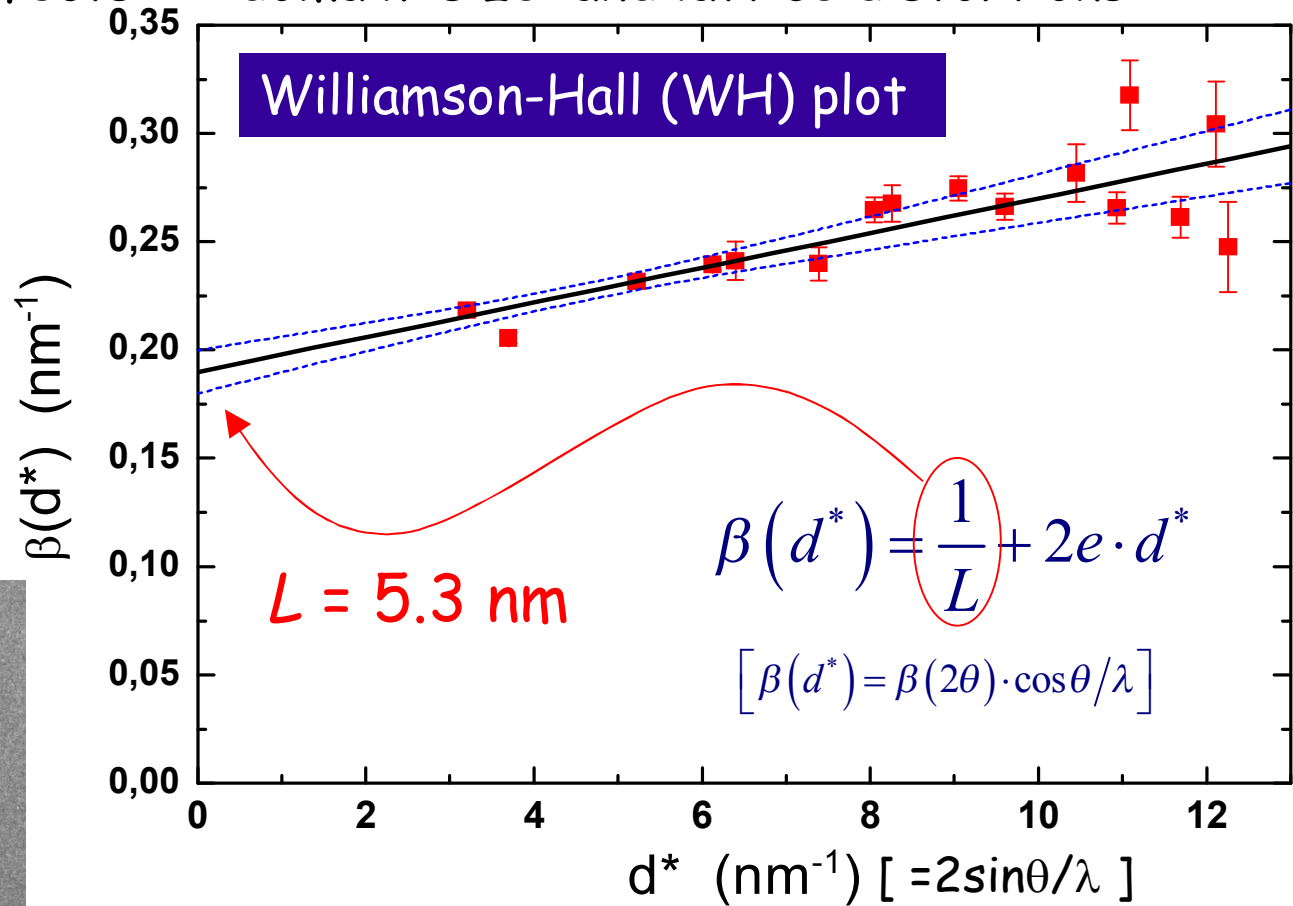
Combined effects - domain size and lattice distortions





INTEGRAL BREADTH METHODS

Combined effects - domain size and lattice distortions





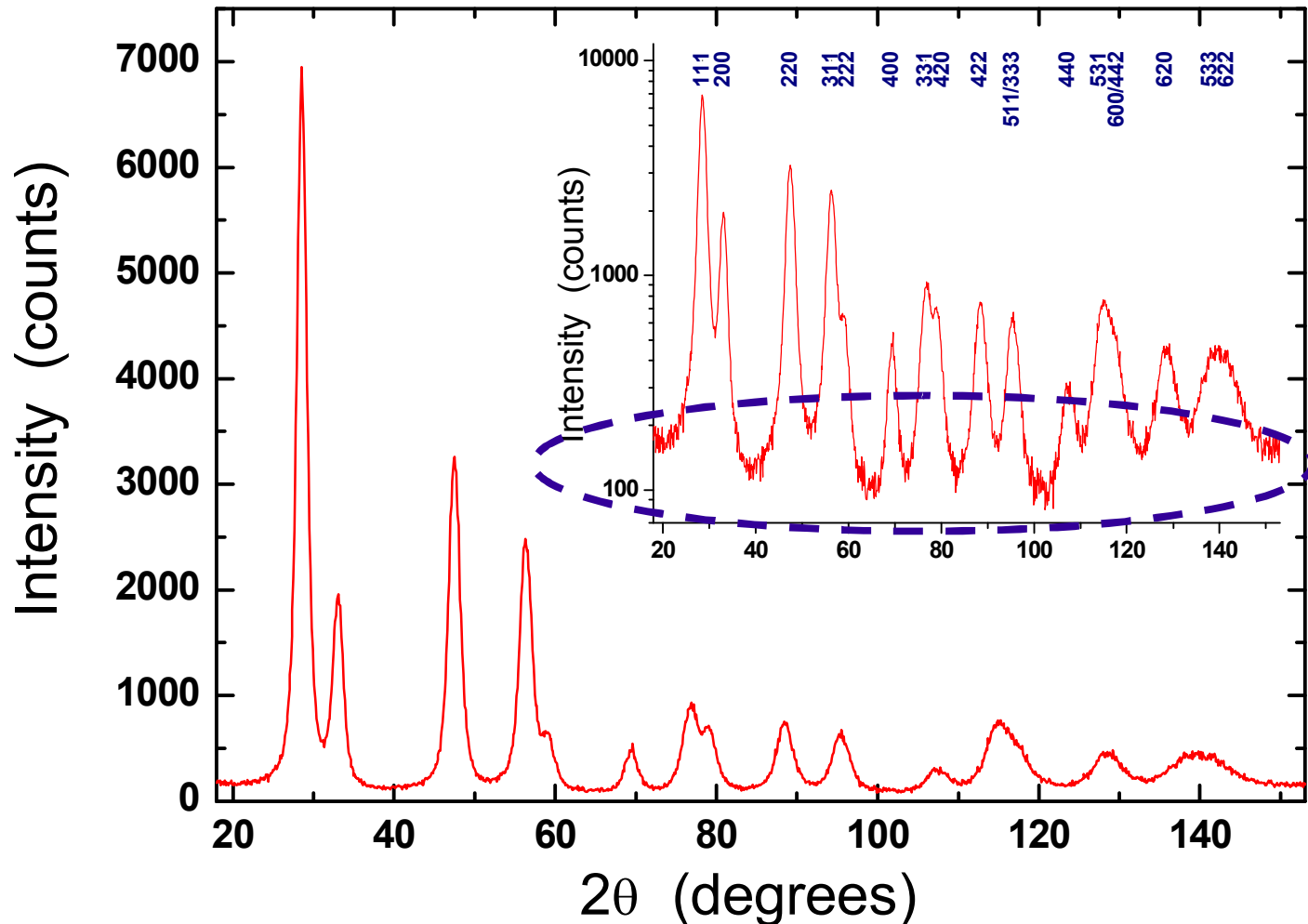
LINE PROFILE ANALYSIS

LIMITATIONS OF TRADITIONAL METHODS OF LINE PROFILE ANALYSIS

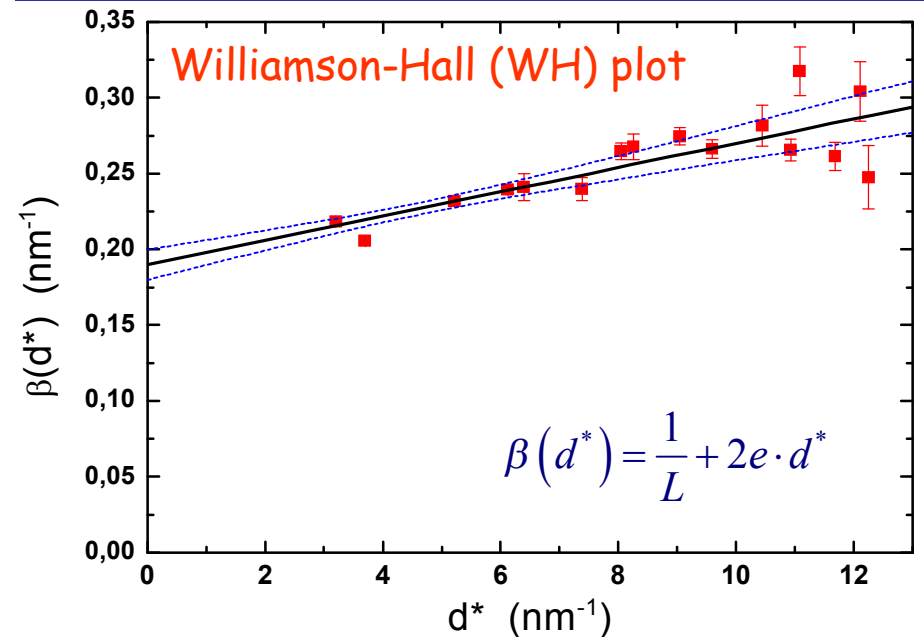
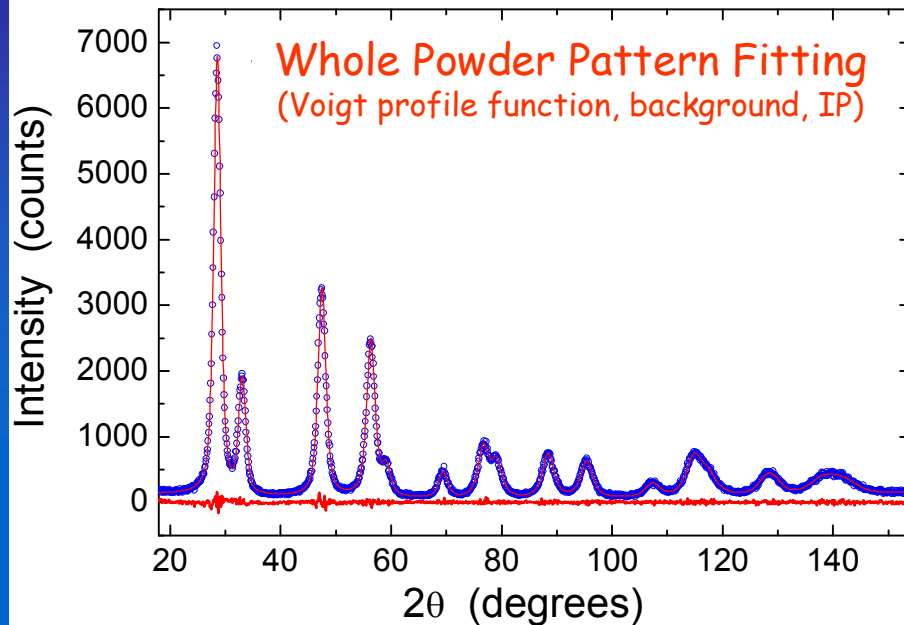


INTEGRAL BREADTH METHODS: LIMITATIONS

Peak profiles tend to overlap: difficult to obtain integral breadths



PROFILE FITTING AND LINE PROFILE ANALYSIS



MARQX software: Y.H. Dong & P. Scardi J. Appl. Cryst. 33 (2000) 184

Modern approach to LPA relies on peak profile fitting for

- Pattern decomposition
- Background separation
- Deconvolution / convolution with instrumental profile component

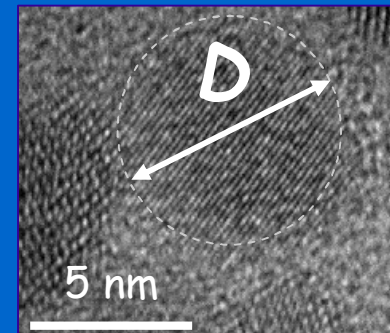
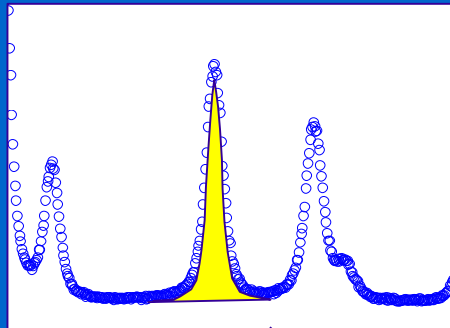
Although simple and flexible profile fitting is substantially arbitrary and controversial: no reason for adopting a given analytical shape !!!



INTEGRAL BREADTH METHODS: LIMITATIONS

What is the meaning of L ,
the 'size' value given by the Scherrer formula ??

$$\beta(2\theta) = \frac{\lambda}{L \cos \theta}$$

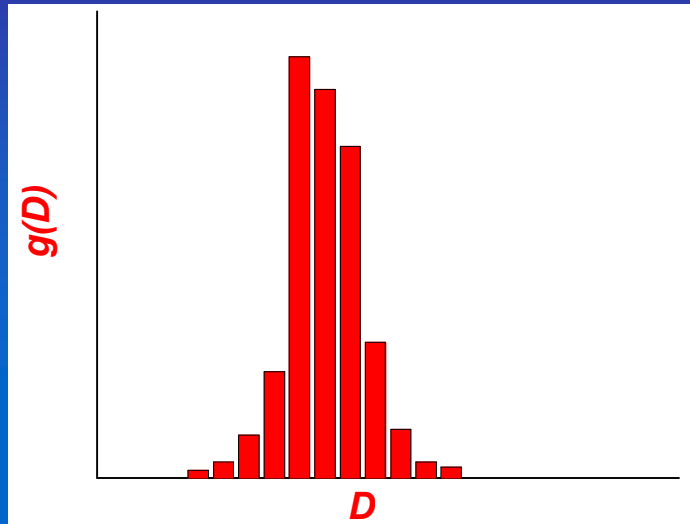


$L \neq D$



INTEGRAL BREADTH METHODS: LIMITATIONS

In most cases nano powders have a distribution of sizes (and shapes)



Distribution 'moments'

$$M_i = \int D^i g(D) dD$$

$M_1 \rightarrow$ mean

$M_2 - M_1^2 \rightarrow$ variance

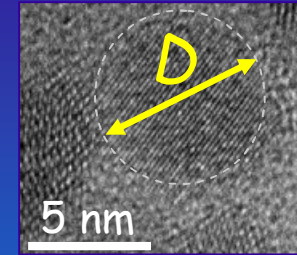
$$L \rightarrow \langle L \rangle_V = \frac{1}{K_\beta} \frac{M_4}{M_3}$$

K_β , a shape factor, generally function of hkl (4/3 for spheres)



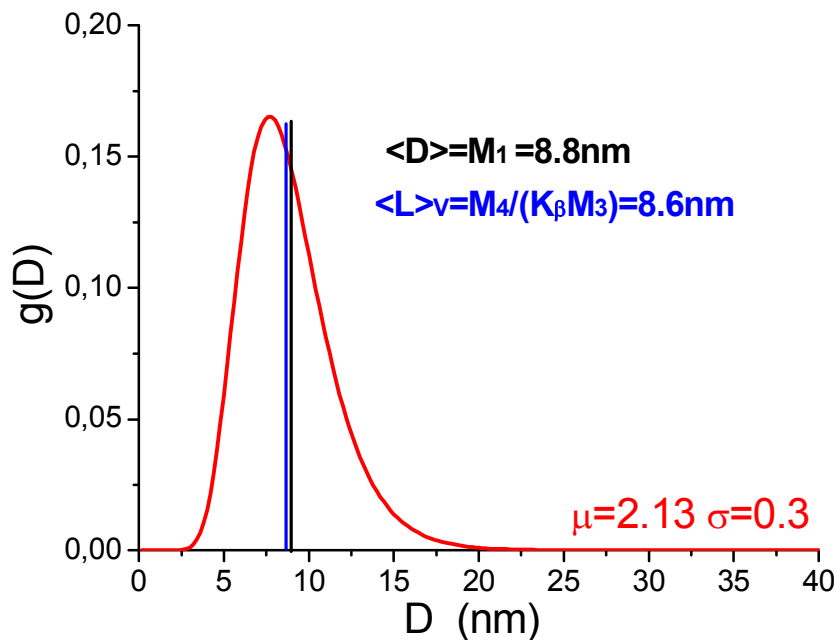
INTEGRAL BREADTH METHODS: LIMITATIONS

$$L \rightarrow \langle L \rangle_V = \frac{1}{K_\beta} \frac{M_4}{M_3} \neq D$$

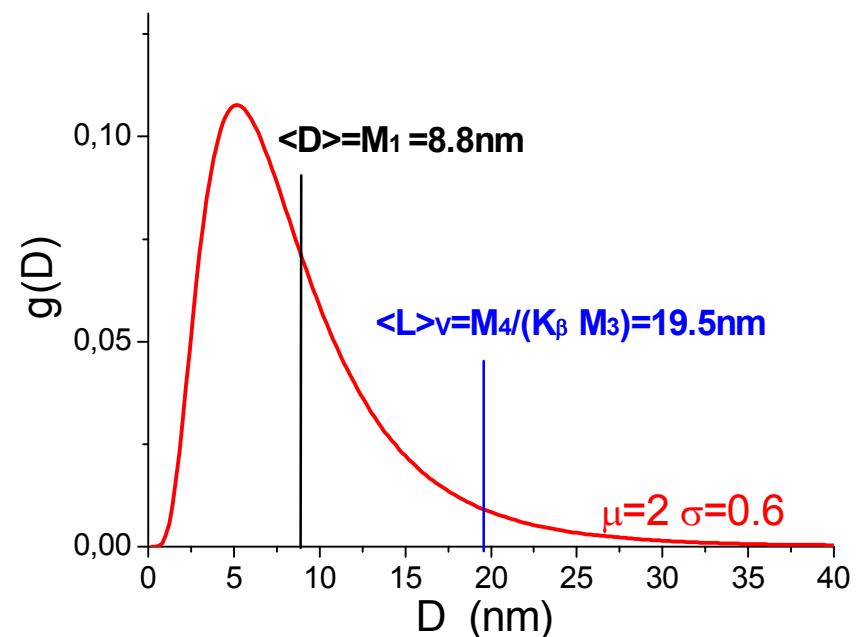


Example: lognormal distributions of spheres, $g(D)$ (mean μ , variance σ)

For little asymmetrical or narrow distributions



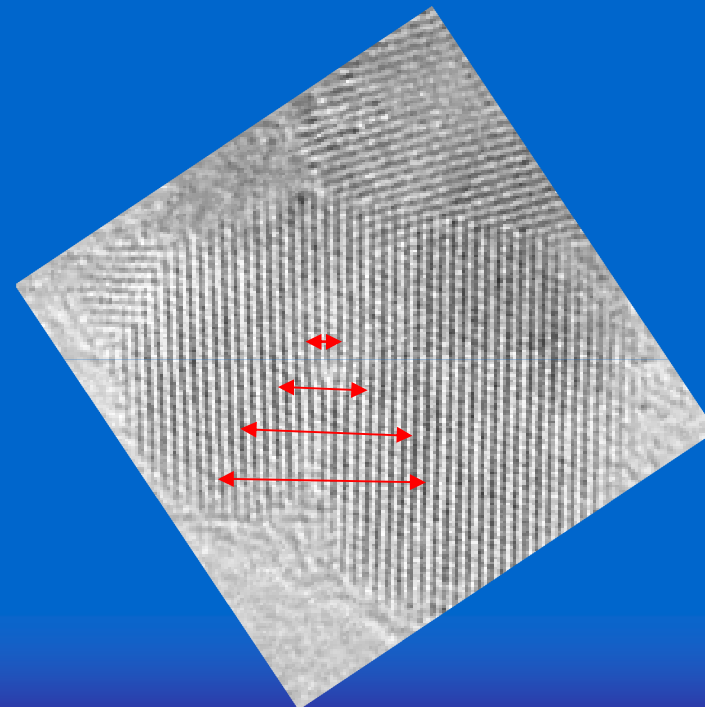
For broad, asymmetrical distributions





INTEGRAL BREADTH METHODS: MAIN LIMITATIONS

- Peak overlapping \rightarrow requires profile fitting with *arbitrary* profile functions
- Effective domain size, $L \rightarrow$ real information is the *size distribution*
- Microstrain ϵ is not a constant \rightarrow *microstrain distribution*





INTEGRAL BREADTH METHODS: MAIN LIMITATIONS

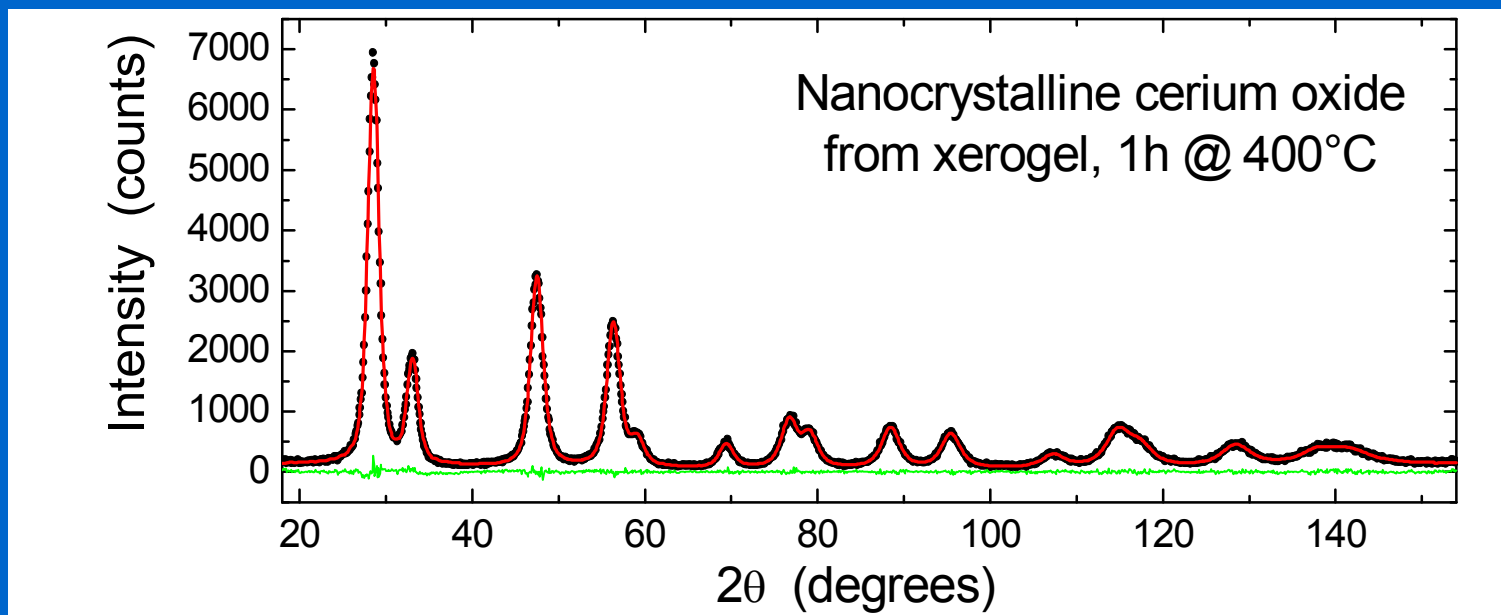
- Peak overlapping → profile fitting with *arbitrary* profile functions
- Effective domain size, L → real information is the *size distribution*
- Microstrain e is not a constant → *microstrain distribution*
- Line broadening effects *do not* simply “add” as in the Williamson-Hall formula

$$\beta(d^*) = \underbrace{\frac{1}{L}}_{\text{'size'}} + \underbrace{2e \cdot d^*}_{\text{'strain'}}$$



WHOLE POWDER PATTERN MODELLING - WPPM

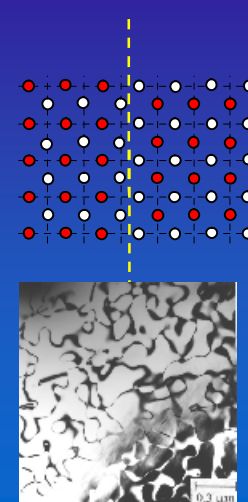
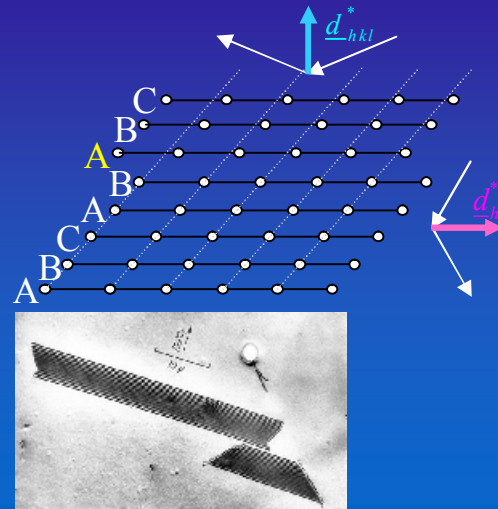
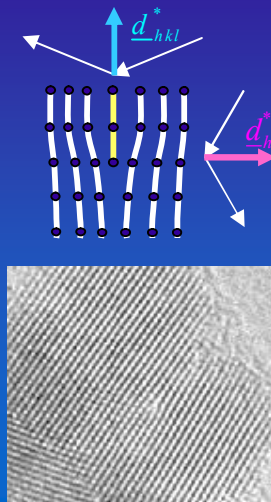
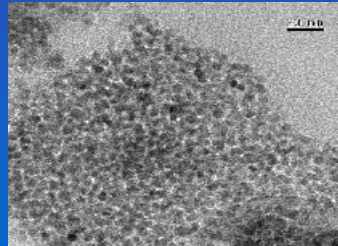
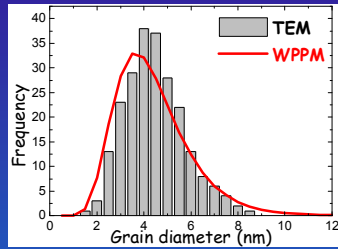
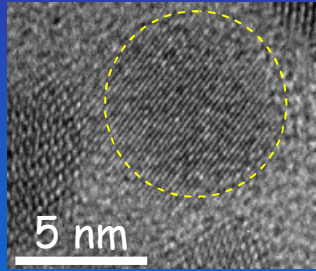
Modelling of the experimental pattern based on physical models of the microstructure and lattice defects:



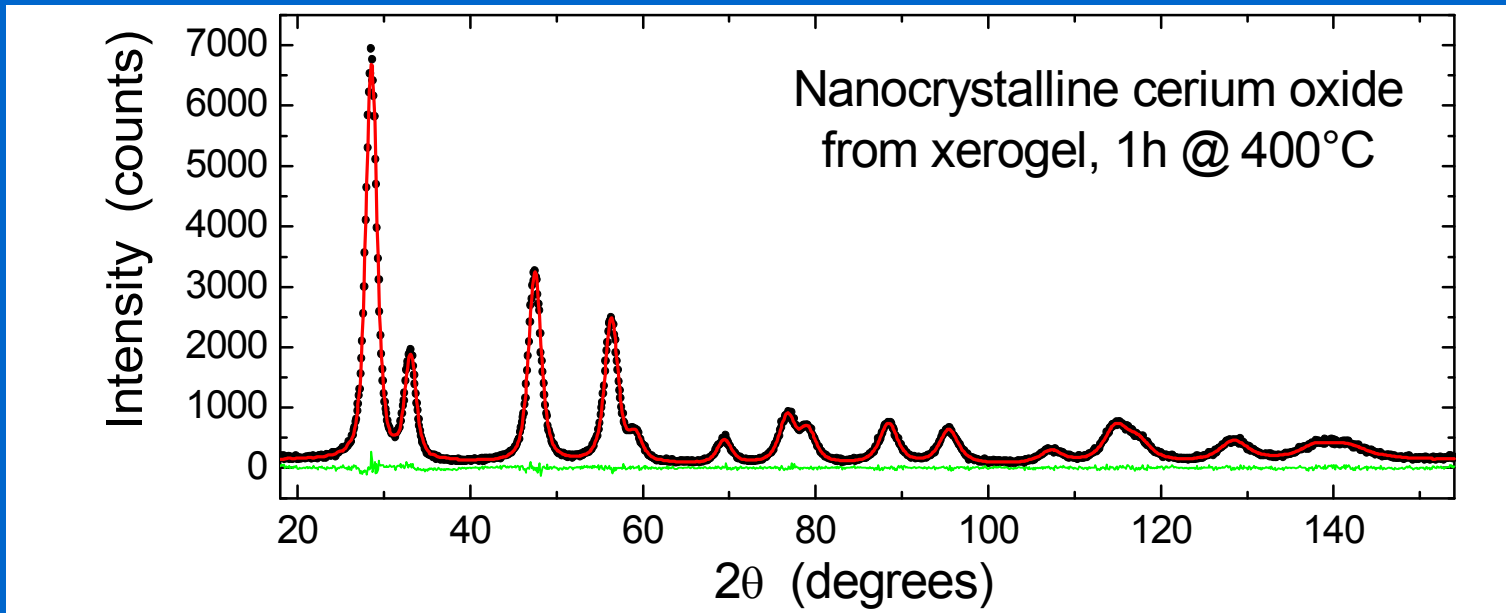
M. Leoni, R. Di Maggio, S. Polizzi & P. Scardi, *J. Am. Ceram. Soc.* 87 (2004) 1133.

P. Scardi & M. Leoni, *Acta Cryst. A* 57 (2001) 604. P. Scardi & M. Leoni, *Acta Cryst. A* 58 (2002) 190

WHOLE POWDER PATTERN MODELLING



(...)



M. Leoni, R. Di Maggio, S. Polizzi & P. Scardi, *J. Am. Ceram. Soc.* 87 (2004) 1133.

P.Scardi & M. Leoni, *Acta Cryst. A* 57 (2001) 604. P.Scardi & M. Leoni, *Acta Cryst. A* 58 (2002) 190



WHOLE POWDER PATTERN MODELLING

Modelling of the experimental pattern based on physical models of the microstructure and lattice defects:



How does it work ??



DIFFRACTION LINE PROFILE: CONVOLUTION OF EFFECTS

The diffraction peak is a **convolution** (\otimes) of *profile components* :

instrumental profile (IP), domain size (S), microstrain (D), faulting (F), anti-phase domain boundaries (APB), stoichiometry fluctuations (C), grain surface relaxation (GSR), etc.

$$I(s) = I^{IP}(s) \otimes I^S(s) \otimes I^D(s) \otimes I^F(s) \otimes I^{APB}(s) \otimes I^C(s) \otimes I^{GRS}(s) \dots$$

$$h = g$$

Instrument

$$\otimes$$

$$f$$

Specimen-related

What is the difference between *convolution* and *sum of effects* ??



DIFFRACTION LINE PROFILE: CONVOLUTION OF EFFECTS

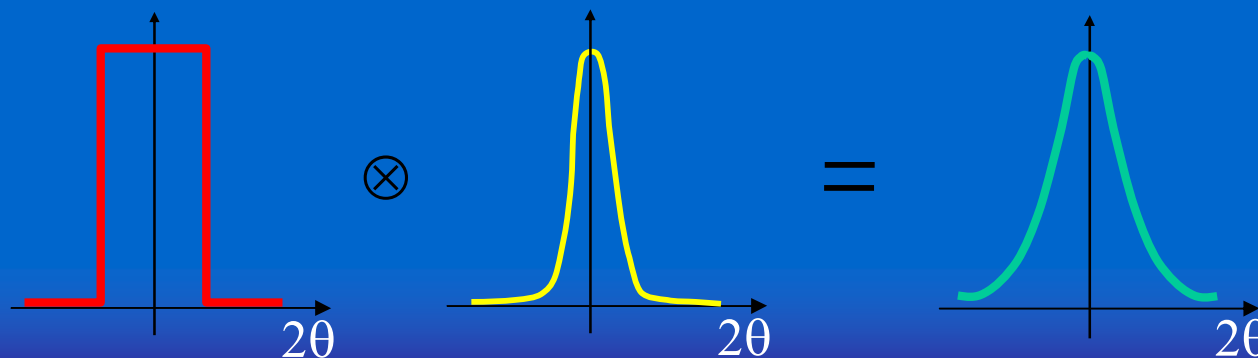
Example: consider instrument (IP) and domain size (S):

$$I(s) = I^{IP}(s) \otimes I^S(s)$$



$$I(s) = \int I^{IP}(t) I^S(s-t) dt$$

g profile, slit (box) function; f profile, bell-shape function (e.g. gaussian)





WPPM : HOW DOES IT WORK ??

The diffraction profile results from a convolution of effects:

$$I(s) = I^{IP}(s) \otimes I^S(s) \otimes I^D(s) \otimes I^F(s) \otimes I^{APB}(s) \otimes I^C(s) \otimes I^{GRS}(s) \dots$$

the Fourier Transform of $I(s)$ is the product of the FTs of the single profile components

$$I(s) \propto \int_{-\infty}^{\infty} C(L) e^{2\pi i L \cdot s_{hkl}} dL$$

$$C = \prod_i A_i = \underbrace{T_{pV}^{IP}}_{\text{instr. profile}} \cdot \underbrace{A_{\{hkl\}}^S}_{\text{domain size/shape}} \cdot \underbrace{A_{\{hkl\}}^D \cdot (A_{hkl}^F + iB_{hkl}^F) \cdot A_{\{hkl\}}^{APB}}_{\text{lattice defects / strain}} \cdot \dots$$



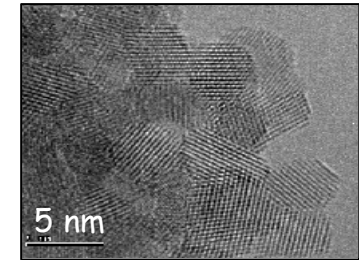
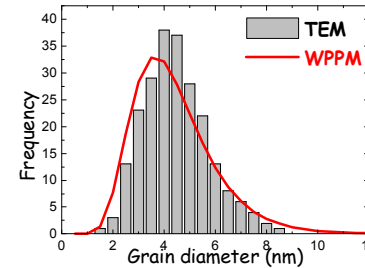
$A_i(L)$ EXPRESSIONS (ANALYTICAL OR NUMERICAL FORM)

$$T_{pV}^{IP}(L) = (1-k) \cdot \exp(-\pi^2 \cdot \sigma_s^2 L^2 / \ln 2) + k \exp(-2\pi \cdot \sigma_s L)$$

Instrumental profile

Domain size effect: μ, σ

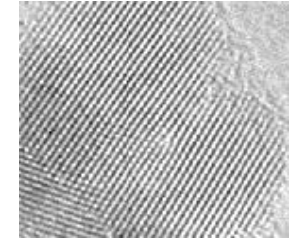
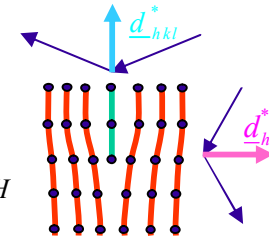
$$A^S(L) = \sum_{n=0}^3 H_n^c \cdot \text{Erfc} \left[\frac{\ln(L \cdot K^c) - \mu - (3-n)\sigma^2}{\sigma\sqrt{2}} \right] \frac{M_{l,3-n}}{2M_{l,3}} \cdot L^n$$



Dislocation (strain) effect: $\rho, R_e, (\bar{C}_{hkl})$

$$A_{\{hkl\}}^D(L) = \exp \left[-\frac{1}{2} \pi |b|^2 \bar{C}_{hkl} \rho d_{\{hkl\}}^{*2} \cdot L^2 f^*(L/R_e) \right]$$

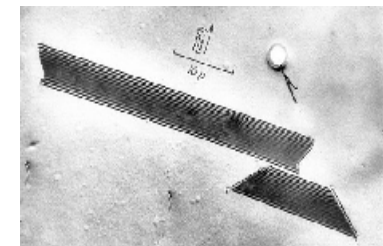
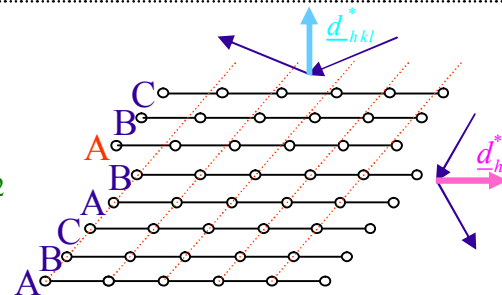
$$\bar{C}_{hkl} = A + B \cdot \frac{h^2 k^2 + k^2 l^2 + l^2 h^2}{(h^2 + k^2 + l^2)^2} = A + B \cdot H$$



Faulting: α (def.), β (twin)

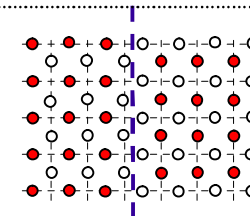
$$A_{hkl}^F(L) = (1 - 3\alpha - 2\beta + 3\alpha^2) \left| \frac{1}{2} L d_{\{hkl\}}^* \cdot \frac{L_o}{h_o^2} \sigma_{L_o} \right|$$

$$B_{hkl}^F(L) = -\sigma_{L_o} \cdot \frac{L}{|L|} \cdot \frac{L_o}{|L_o|} \cdot \beta / (3 - 6\beta - 12\alpha - \beta^2 + 12\alpha^2)^{1/2}$$



Anti-Phase Domains: γ

$$A_{\{hkl\}}^{APB}(L) = \exp \left[-\frac{-2\gamma (|h| + |k|) \cdot L}{d_{hkl} (h^2 + k^2 + l^2)} \right]$$





WHOLE POWDER PATTERN MODELLING

- Diffraction profiles are modelled directly in terms of relatively few microstructural parameters: $\mu, \sigma - \rho, Re - \alpha, \beta - \gamma \dots$
- No arbitrary profile functions (Voigt, pseudo-Voigt, Pearson VII, etc.)

WPPM : based on physical models of microstructure and lattice defects



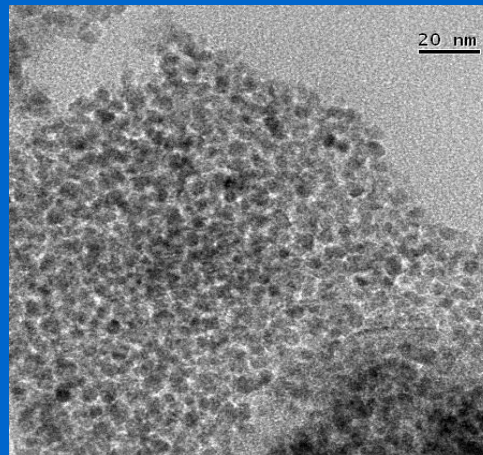
More Theory: see REFERENCES



WPPM APPLICATIONS



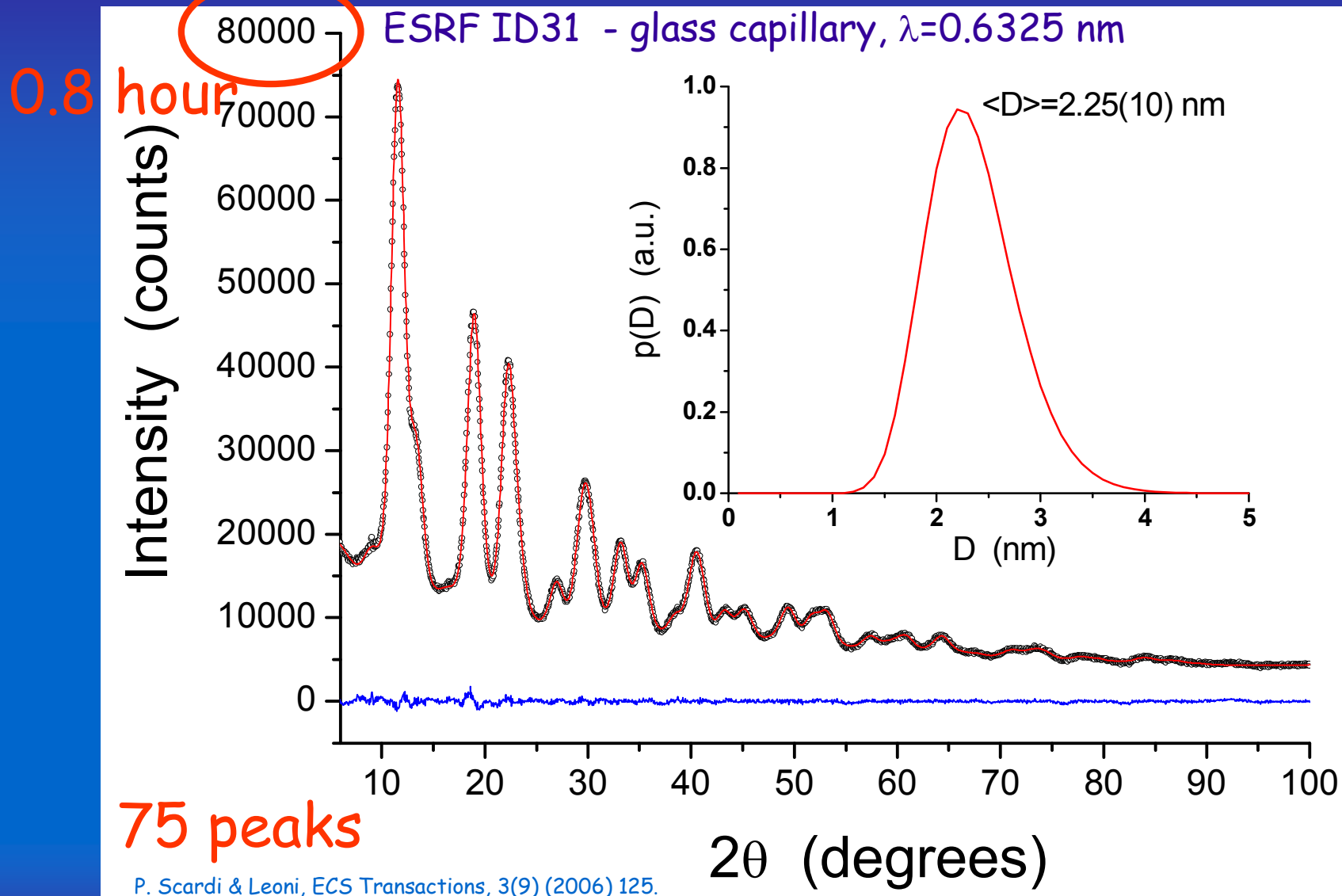
Nanocrystalline cerium oxide: growth kinetics of a xerogel





WPPM APPLICATIONS: NANOCRYSTALLINE CERIA

Xerogel obtained by vacuum-drying: broad diffraction lines of nanocrystalline fcc phase



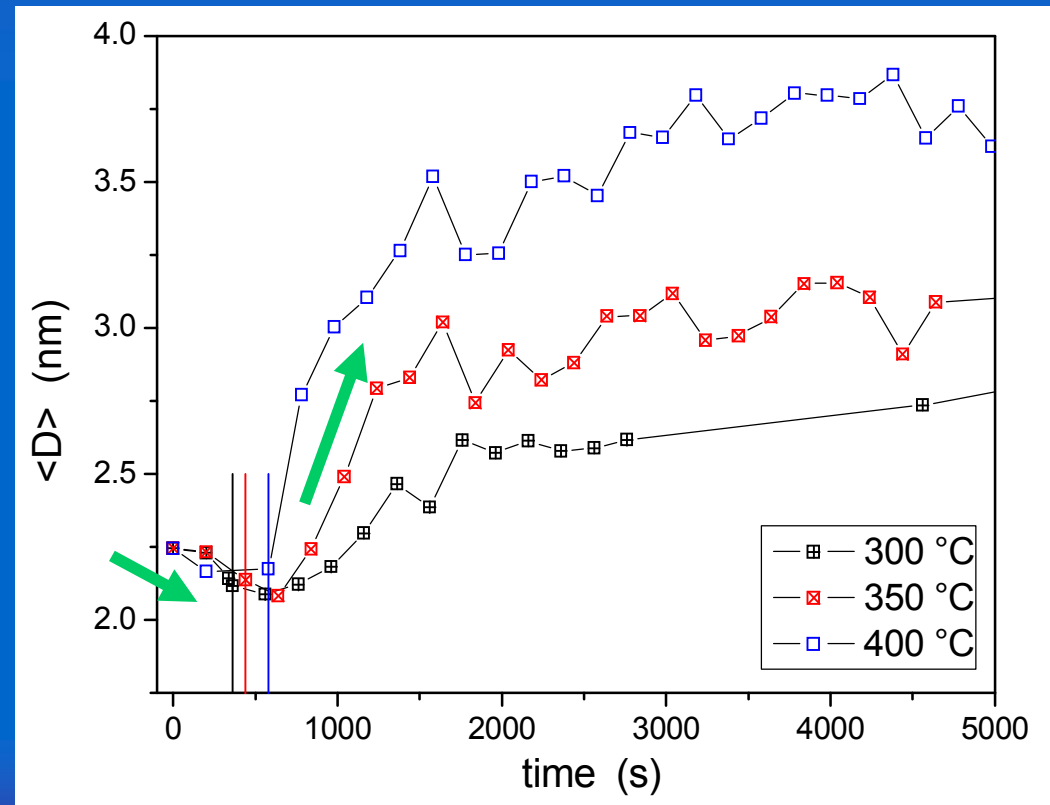
P. Scardi & Leoni, ECS Transactions, 3(9) (2006) 125.



WPPM APPLICATIONS: NANOCRYSTALLINE CERIA

Evolution of line profiles during isothermal treatment: 300°C, 350°C, 400°C

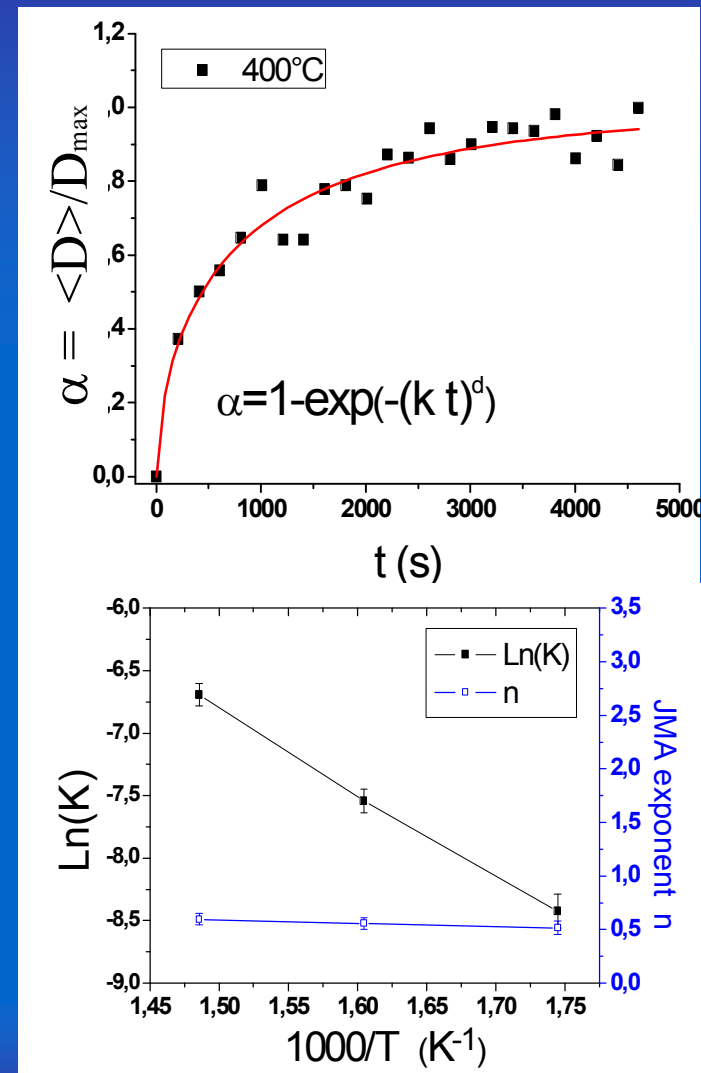
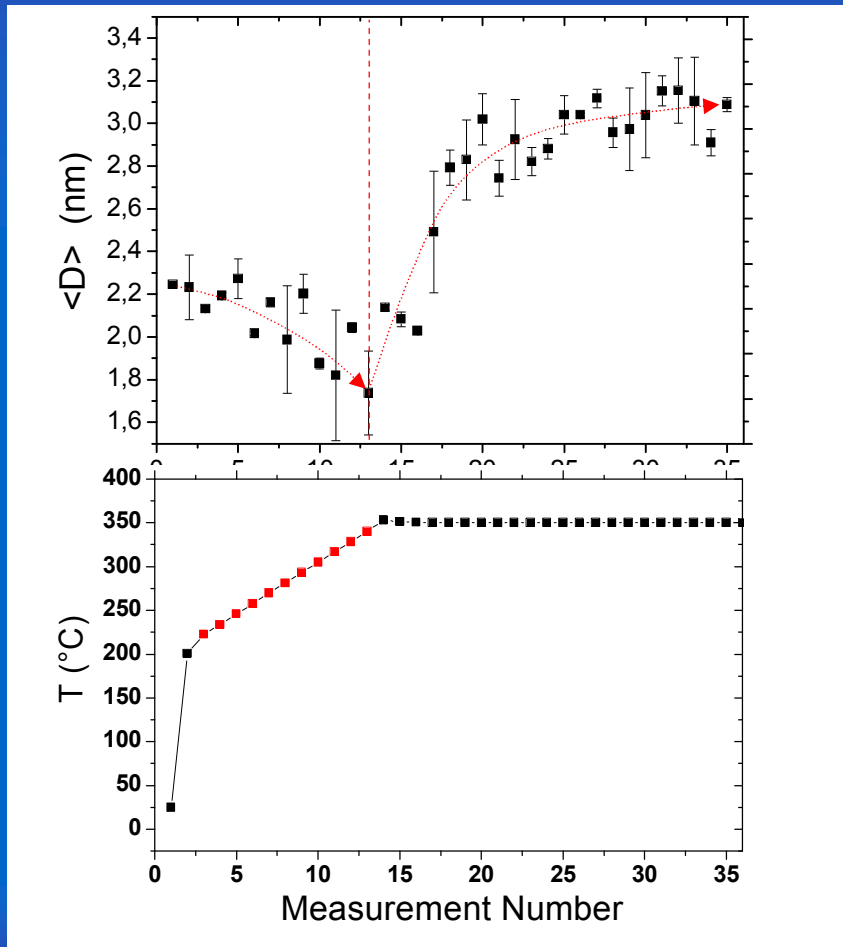
High temperature blower on ID31 at ESRF





WPPM APPLICATIONS: NANOCRYSTALLINE CERIA

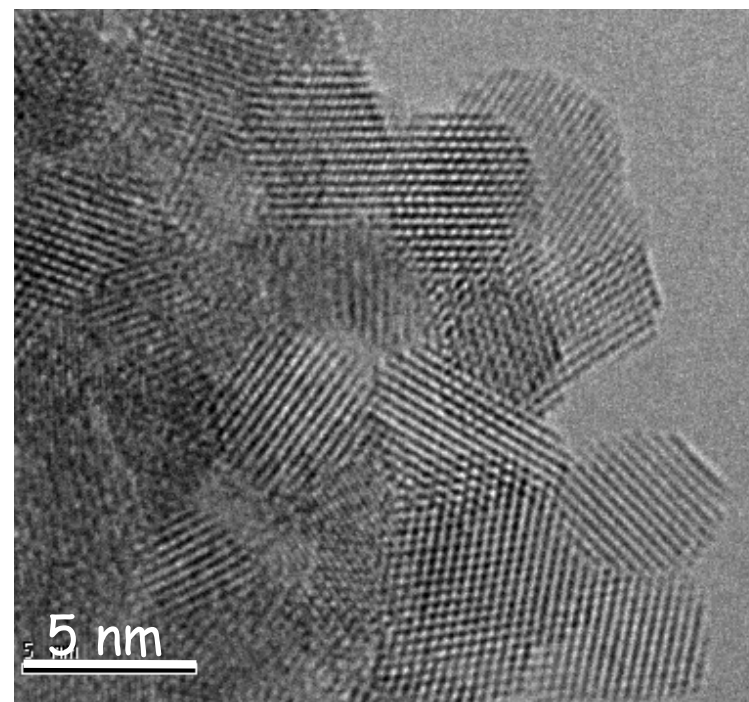
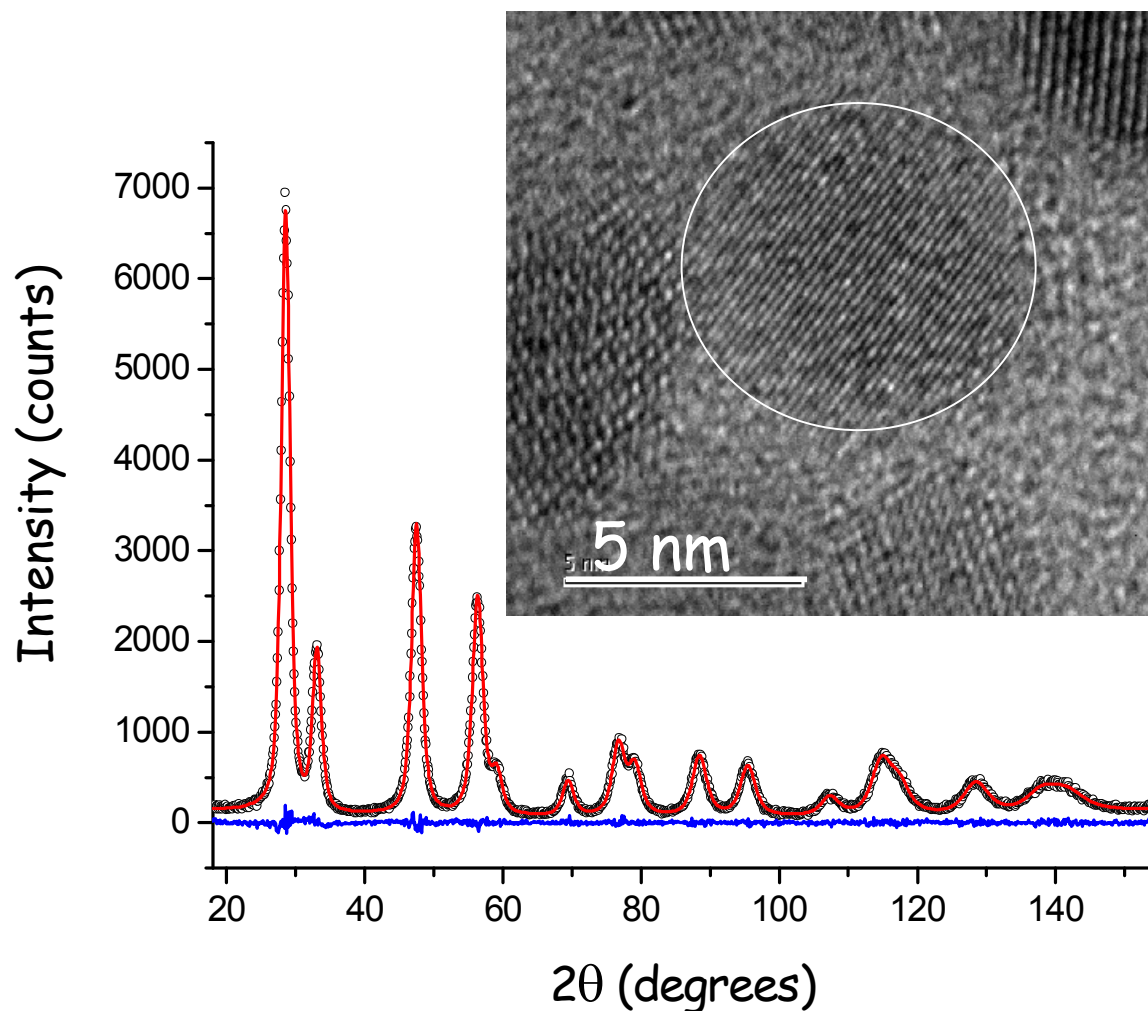
Nucleation during the heating stage: mean domain size initially decreases, before the grain growth starts





WPPM APPLICATIONS: NANOCRYSTALLINE CERIA

Heat treated 1h @ 400°C

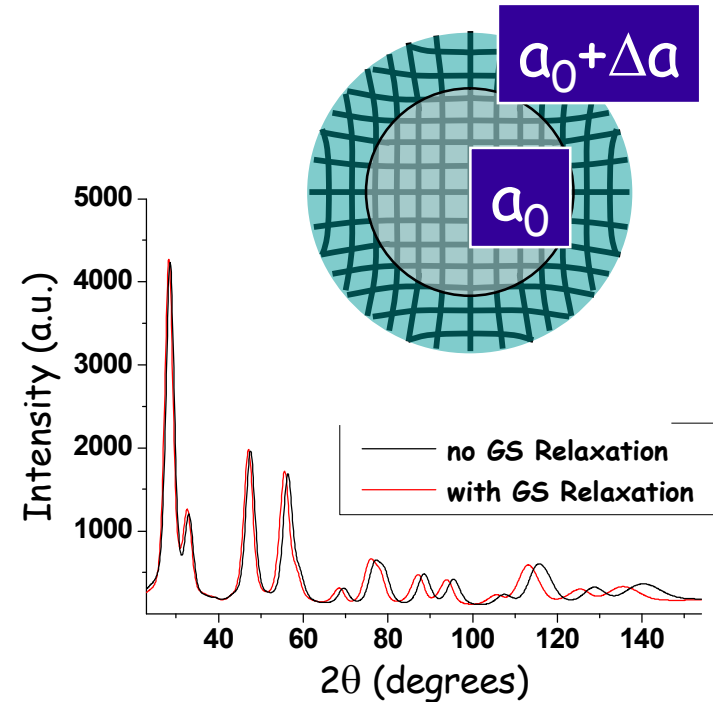
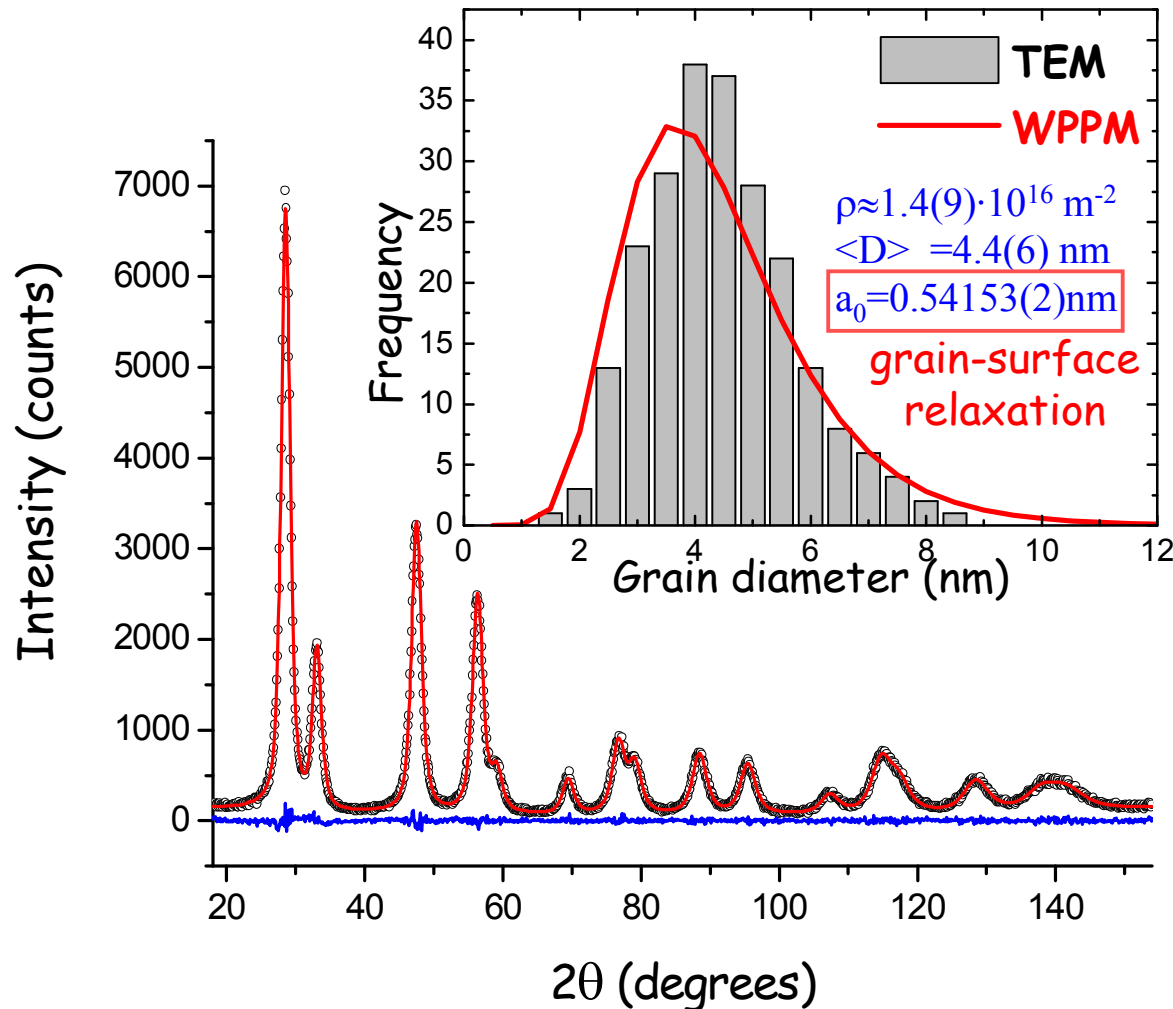


M. Leoni & P. Scardi, in *Diffraction Analysis of Materials Microstructure*. E.J. Mittemeijer & P. Scardi, editors. Berlin: Springer-Verlag, 2004



WPPM APPLICATIONS: NANOCRYSTALLINE CERIA

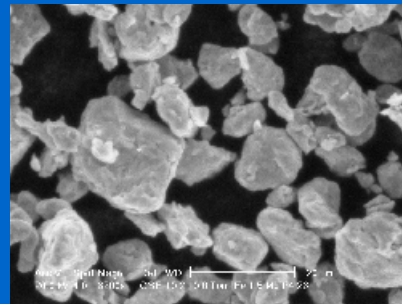
Heat treated 1h @ 400°C



M. Leoni & P. Scardi, in *Diffraction Analysis of Materials Microstructure*. E.J. Mittemeijer & P. Scardi, editors. Berlin: Springer-Verlag. 2004



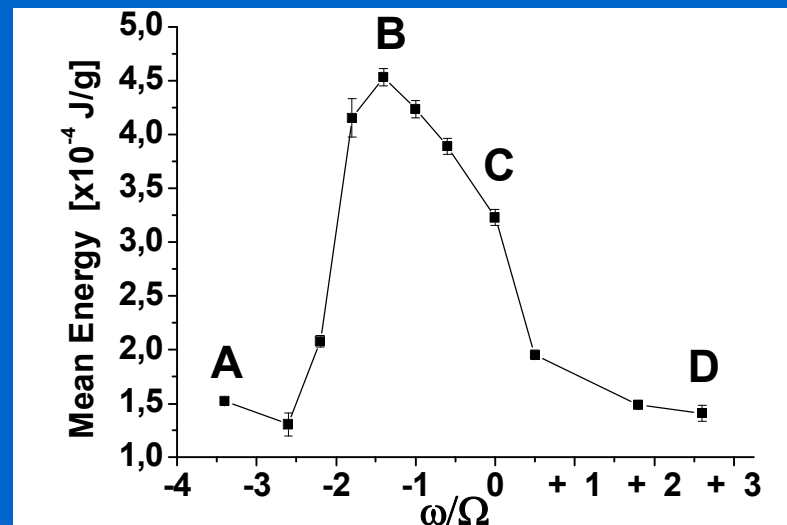
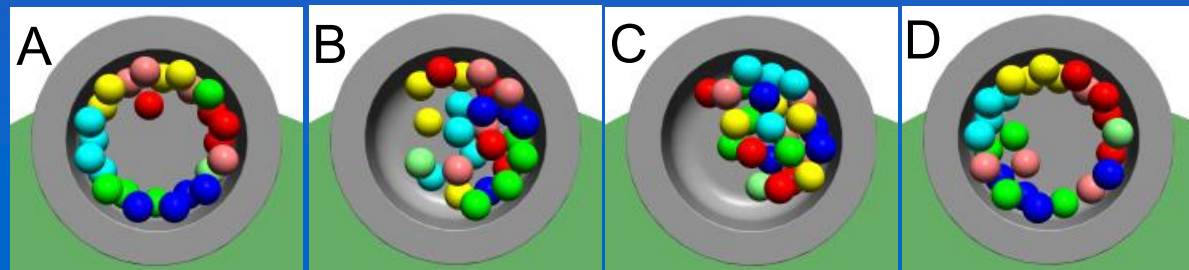
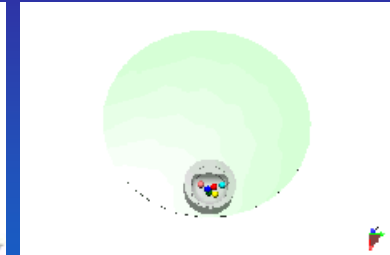
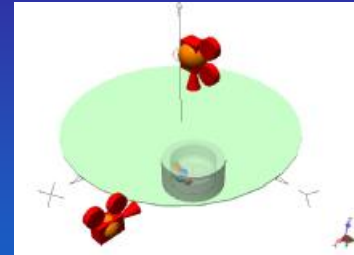
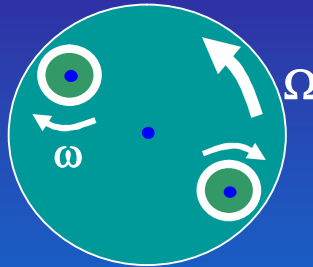
Highly-energy mechanical grinding ball-milled Fe-1.5%Mo





NANOCRYSTALLINE Fe-1.5%Mo POWDER

Planetary ball mill - process modelling & production

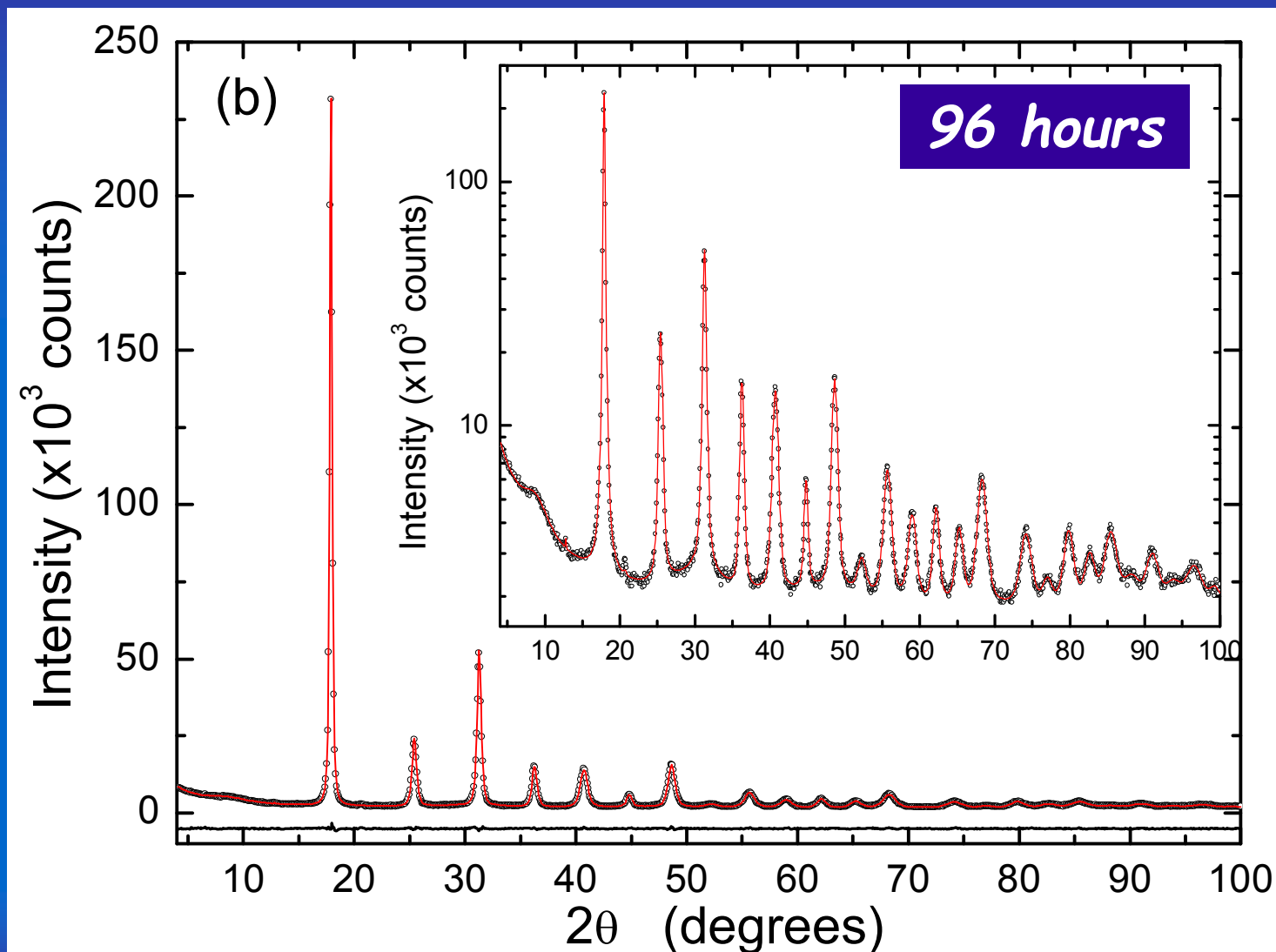


M. d'Incau, Leoni & P. Scardi, J. Materials Research 22 (2007) 1744-1753.



NANOCRYSTALLINE Fe-1.5%Mo POWDER

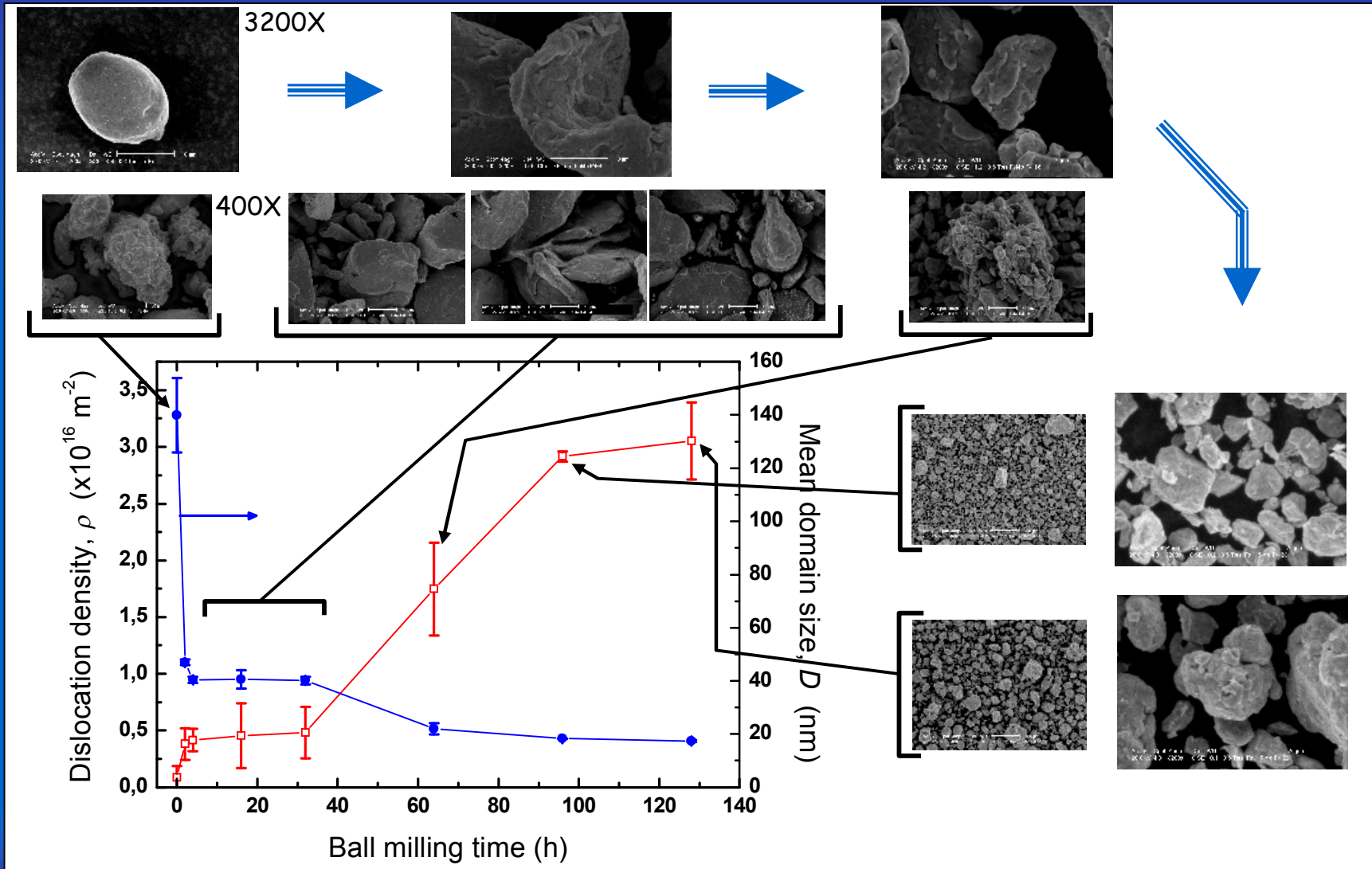
Ball milled Fe1.5Mo (Fritsch P4) - data collected at ESRF - ID31 $\lambda=0.0632$ nm





NANOCRYSTALLINE Fe-1.5%Mo POWDER

Ball milled Fe1.5Mo (Fritsch P4) - data collected at ESRF - ID31 $\lambda=0.0632$ nm
 dislocation density/domain size vs. morphology





NANOCRYSTALLINE Fe-1.5%Mo POWDER

Ball milled Fe1.5Mo (Fritsch P4) - data collected at ESRF - ID31 $\lambda=0.0632$ nm
 dislocation density/domain size vs. morphology

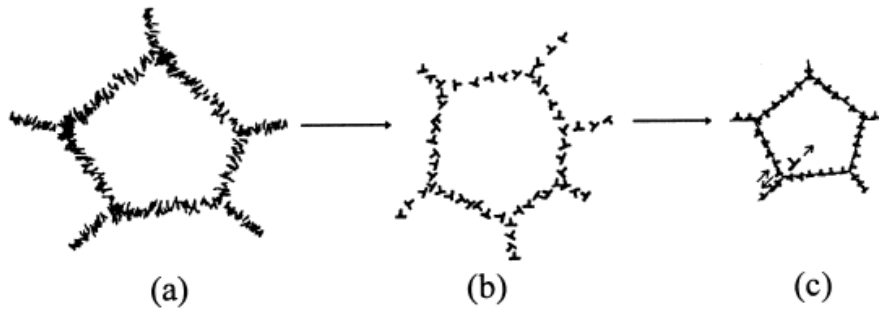


Fig. 15. Schematic model of dislocation structure evolution at different stages during severe plastic deformation.

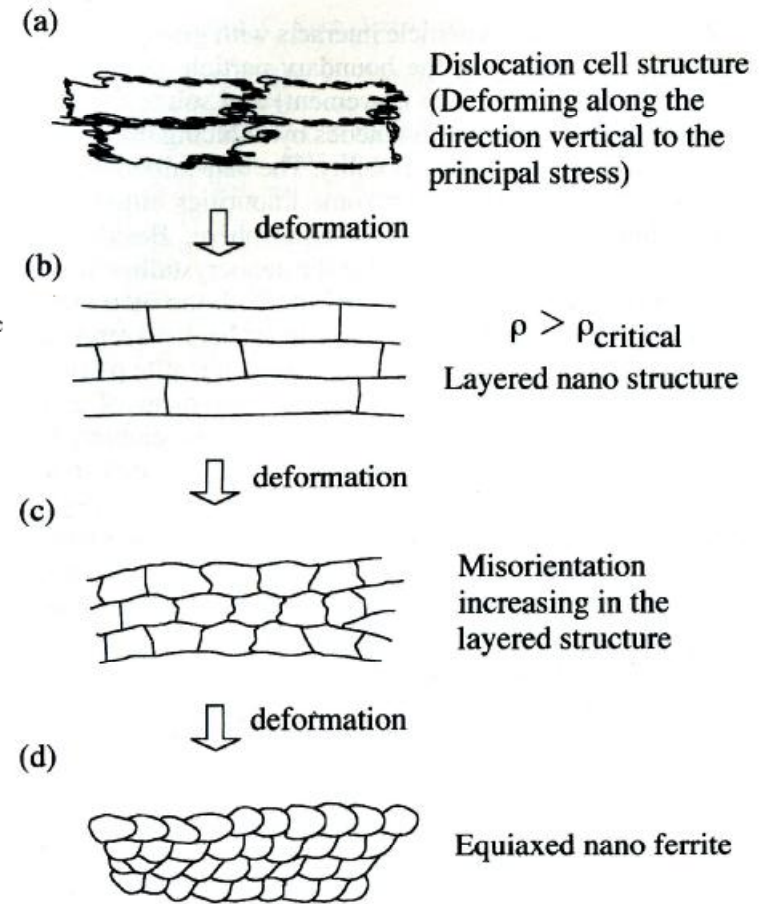
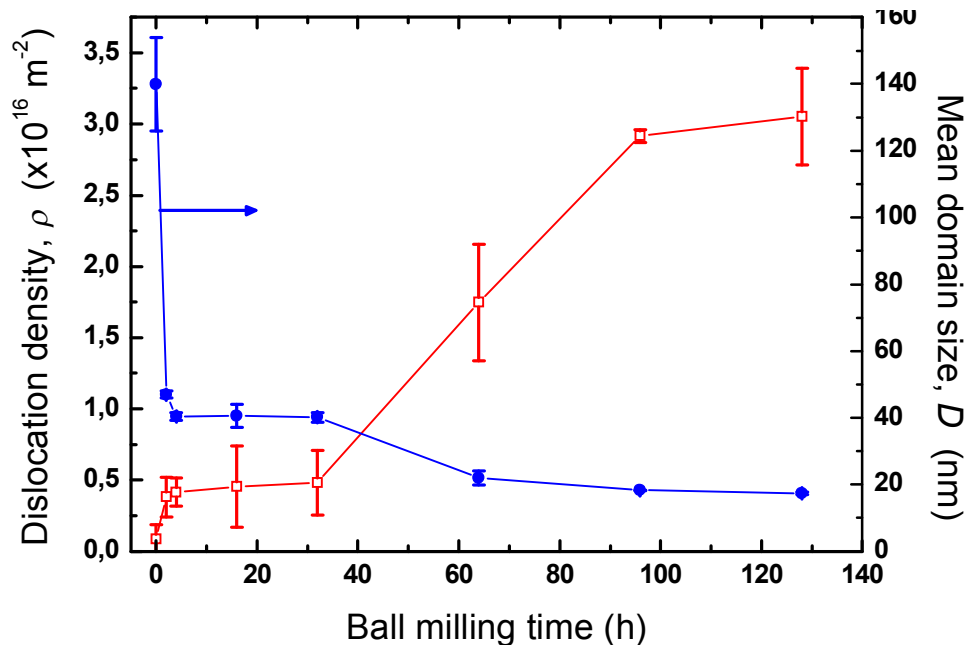


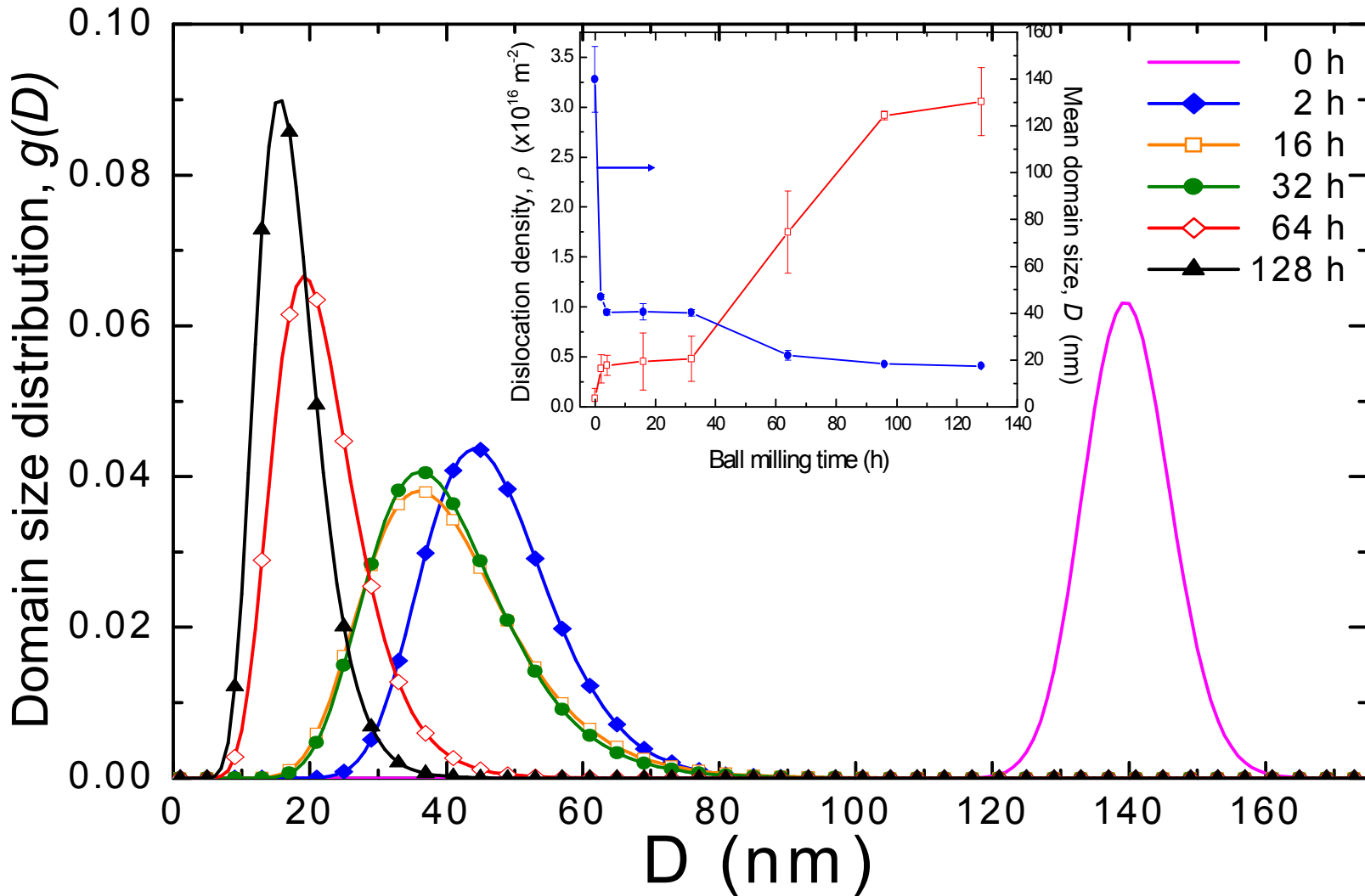
Fig. 11—(a) through (d) A schematic drawing of nanocrystalline ferrite formation by ball milling.



NANOCRYSTALLINE Fe-1.5%Mo POWDER

Ball milled Fe1.5Mo (Fritsch P4) - data collected at ESRF - ID31 $\lambda=0.0632$ nm

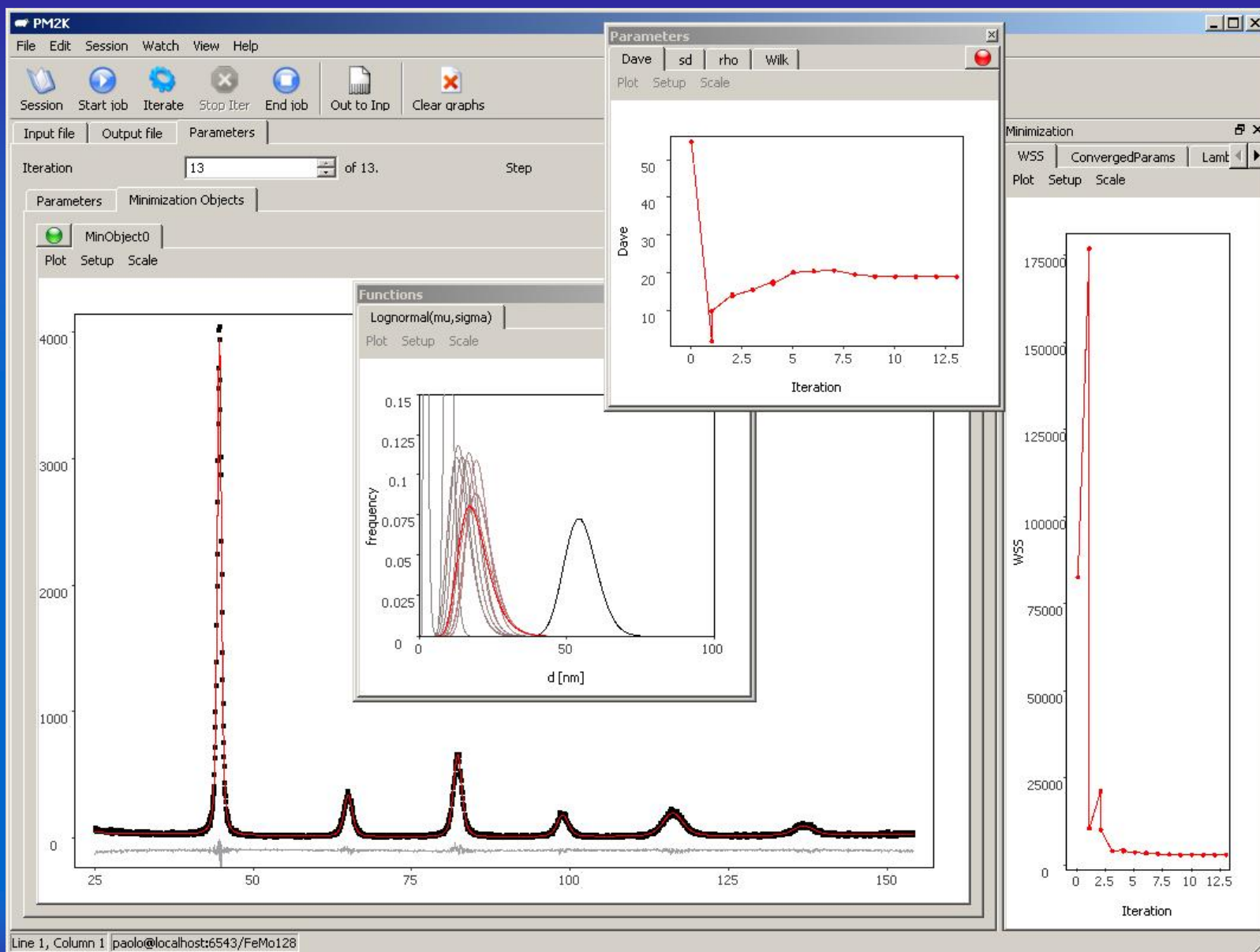
In addition to mean values, WPPM provides the size distribution



M. d'Incau, M. Leoni & P. Scardi, J. Materials Research 22 (2007) 1744-1753.



PM2K SOFTWARE - email to: Paolo.Scardi@unitn.it





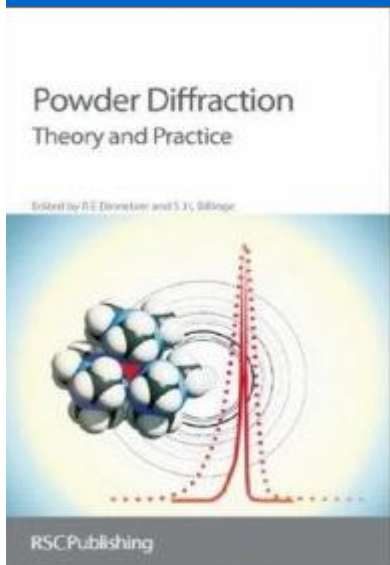
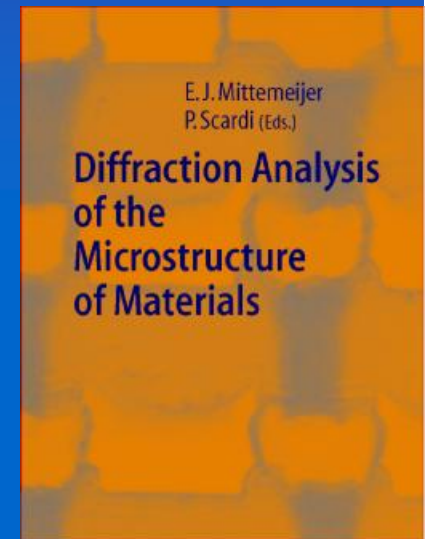
PART 2: REFERENCES - Paolo.Scardi@unitn.it

- P.Scardi & M. Leoni, *Acta Cryst. A* 57 (2001) 604
- P.Scardi & M. Leoni, *Acta Cryst. A* 58 (2002) 190
- P.Scardi, M. Leoni, R. Delhez *J. Appl. Cryst.* 37 (2004) 381
- M. Leoni, P. Scardi *J. Appl. Cryst.* 37 (2004) 629
- P. Scardi & M. Leoni, *Acta Mater.* 53 (2005) 5229.
- P. Scardi & M. Leoni *J. Appl. Cryst.* 39 (2006) 24.

Diffraction Analysis of Materials Microstructure

E.J. Mittemeijer & P. Scardi, editors.

Berlin: Springer-Verlag, 2004.



Powder Diffraction: Theory and Practice

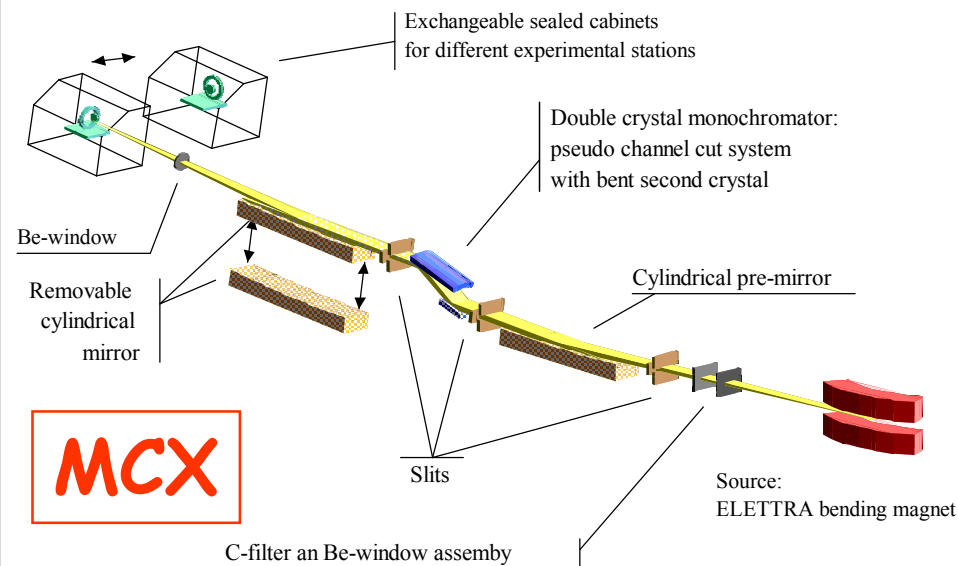
R.E. Dinnebier & S.J.L. Billinge, editors.

Cambridge: Royal Society of Chemistry, 2008.





MCX - A new beamline for Materials Characterization by XRD at ELETTRA (Trieste, Italy)
G. Paolucci, E. Busetto, A. Lausi, J. Plasier (Sincrotrone Trieste), P. Scardi (Univ. Trento & INSTM)



Examples of typical applications

- Residual stress and texture analysis in thin films by multiple wavelength XRD
- Surface analysis by grazing incidence XRD and reflectivity
- Medium-low energy (3.5÷20 keV) anomalous scattering XRD
- Line Profile Analysis (e.g., nanocrystalline, highly defected materials)
- Non-ambient studies (controlled atmosphere, high temperature kinetics)
- Surface mapping by microdiffraction (diffraction on small area)

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Information and applications:

<http://www.mse.unitn.it>

Paolo.Scardi@unitn.it