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International Centre for Theoretical Physics**



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**Joint ICTP-IAEA Advanced Workshop on Multi-Scale Modelling for
Characterization and Basic Understanding of Radiation Damage
Mechanisms in Materials**

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Atomistic simulation of a swift ion track development in a model Ni-Al alloy

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Collaboration:

Christian Abromeit

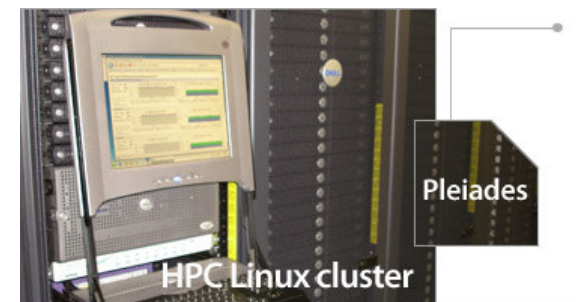
Helmholtz-Zentrum Berlin für Materialien und Energie

Rolf Gotthardt

École Polytechnique Fédérale de Lausanne

Robin Schäublin

EPFL SB CRPP Groupe Matériaux, PSI





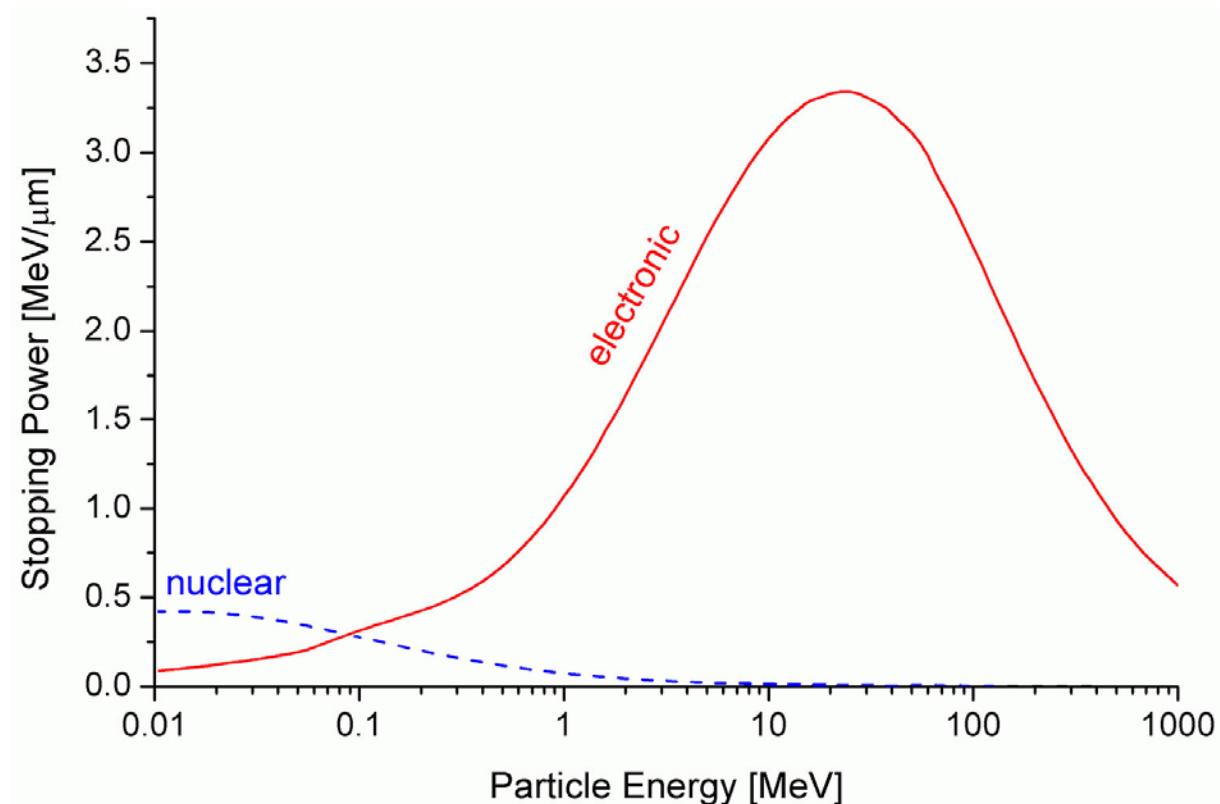
Outline

- Basic concepts of track formation
- MT and shape memory alloys
- Hysteretic behavior at reversible MT
- Kinetics of transformation
- Stress-controlled MT
- MT in ordered Ni_5Al_3 and Ni_7Al_5 alloys
- Grain Boundary Effect
- Phase transformations at track development



Nuclear and electronic stopping power

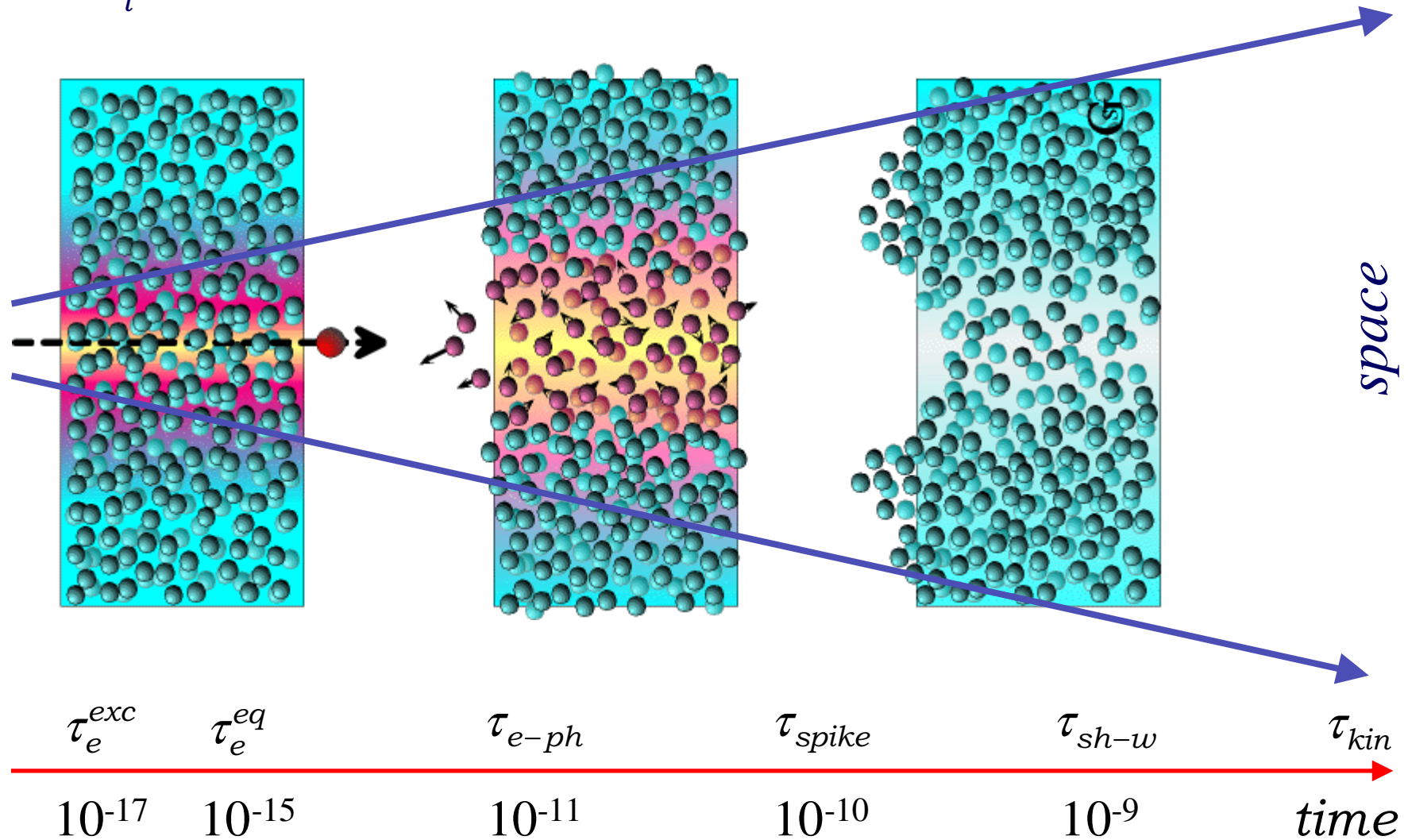
$$\frac{dE^{(total)}}{dx} = \frac{dE^{(nucl)}}{dx} + \frac{dE^{(electr)}}{dx}$$



Stopping power for Al ions in Al. The nuclear stopping curve typically reaches maximum at energies of ~1 keV/nucleon, the electronic one ~1MeV/ nucleon.

Track formation by swift heavy ion

$$E_i \sim 0.1-10 \text{ GeV}$$



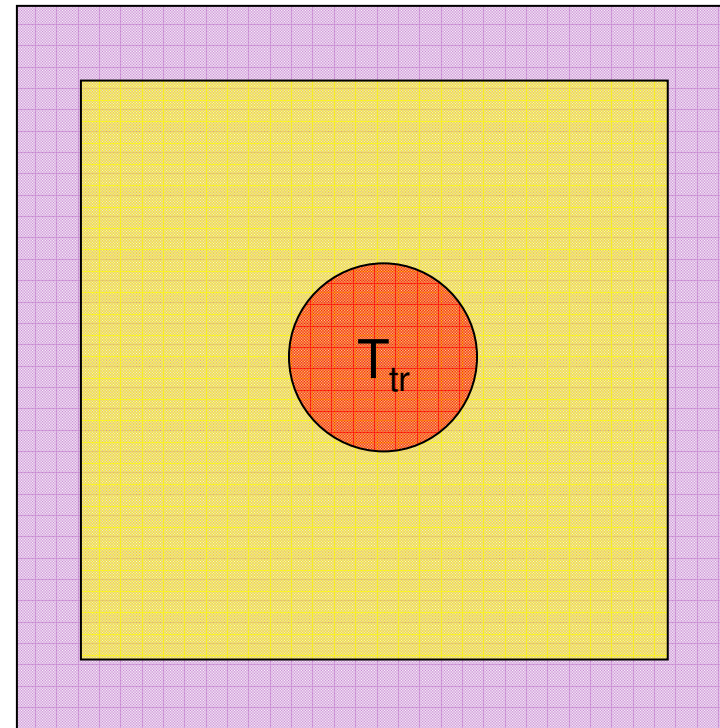
Thermal spike model: analytical description

M.I. Kaganov, I.M. Lifshits, L.V. Tanatarov, Sov. Phys. JETP 4 (1957) 175

$$C_e(T_e) \frac{\partial T_e}{\partial t} = \frac{1}{r} \frac{\partial}{\partial r} r K_e(T_e) \frac{\partial}{\partial r} T_e - g(T_e - T_a) + B(r, t)$$

$$C_a(T_a) \frac{\partial T_a}{\partial t} = \frac{1}{r} \frac{\partial}{\partial r} r K_a(T_a) \frac{\partial}{\partial r} T_a - g(T_a - T_c)$$

$$\frac{dE}{dx} = \iint B(r, t) dr dt$$





Experimental study of electronic temperatures in heavy ion tracks

M. Caron, H. Rothard, M. Toulemonde, B. Gervais, M. Beuve, NIMPR B245 (2006) 36–40

Values of the electron–phonon coupling g (in $10^{10} \text{ Wcm}^{-3}\text{K}^{-1}$) for different metals assuming $n_e/n_a = 1$ [25]

Metals ($\text{W/cm}^3/\text{K}$)	Kaganov et al. [26] ($\text{W/cm}^3/\text{K}$)	Swift heavy ions ($\text{W/cm}^3/\text{K}$)	Calculated threshold (keV/nm)	From experimen (keV/nm)
Cu	13×10^{10}			
Au	2.3×10^{10}			
Fe	119×10^{10}	144×10^{10} [16]	~ 45	~ 40 [30]
a- $\text{Fe}_{85}\text{B}_{15}$	2400×10^{10}	500×10^{10} [34,35]	~ 15	~ 13 [31]
Bi	20×10^{10}	13×10^{10} [33]	~ 30	~ 30 [25]
Ti	203×10^{10}	1000×10^{10} [16]	~ 12	~ 7 [32]
Graphite	2700×10^{10}	3000×10^{10}	~ 8	~ 7 [33]
Co	90×10^{10}	345×10^{10} [16]	~ 32	~ 35 [32]
Zr	85×10^{10}	260×10^{10} [16]	~ 29	~ 30 [32]



Swift ion track observations in the NiTi

A. Barbu, A. Dunlop, A. Hardouin Duparc, G. Jaskierowicz, N. Lorenzelli, NIMPR B145 (1998) 354.

Ion	E (GeV)	T	Fluence (cm^{-2})	$dE/dx _e$ (keV/nm)	Velocity (m/s)	Structure	Figures	Comments and mean track diameters D_m (nm)
Kr	0.71	85 K	5×10^{10} 5×10^{11}	17	4.0×10^7	M–M		No visible damage
Xe	0.82	85 K	1.3×10^{11}	32	3.5×10^7	M–M		No visible damage
		85 K	1.0×10^{12}			M–M		No visible damage
		85 K	2.6×10^{13}			M–M	17	Monoclinic \rightarrow B2 (X ray)
Ta	0.98	85 K	5×10^{10}	46	3.2×10^7	A–M	1c	$D_m = 4.2$
Pb	0.84	85 K	5×10^{10}	52	2.8×10^7	A–M	1b, 4c	$D_m = 5.7$
		85 K	5×10^{10}			M–M	5, 6, 7	$D_m = 12.8$
		85 K	1.8×10^{13}			M–M	13, 14	(am + B2)
		85 K	7.2×10^{13}			M–M	15	Totally am
Pb	0.84	300 K	5×10^{10}	52	2.8×10^7	A + M	9	Tracks only in M
			10^{12}			M	11, 12	Tracks (am + B2)
			10^{13}			A	16	No tracks but cascades
U	0.76	85 K	5×10^{10}	57	2.5×10^7	A–M	1a, 2, 4b, 10	$D_m = 13.1$
		85 K	5×10^{10}			M–M	8	$D_m = 17.5$
		85 K	5×10^{11}			A–M	3	$D_m = 13.1$
U	4.6	10 K	5×10^{10}	52	6.1×10^7	A–M	4a	$D_m = 6.5$

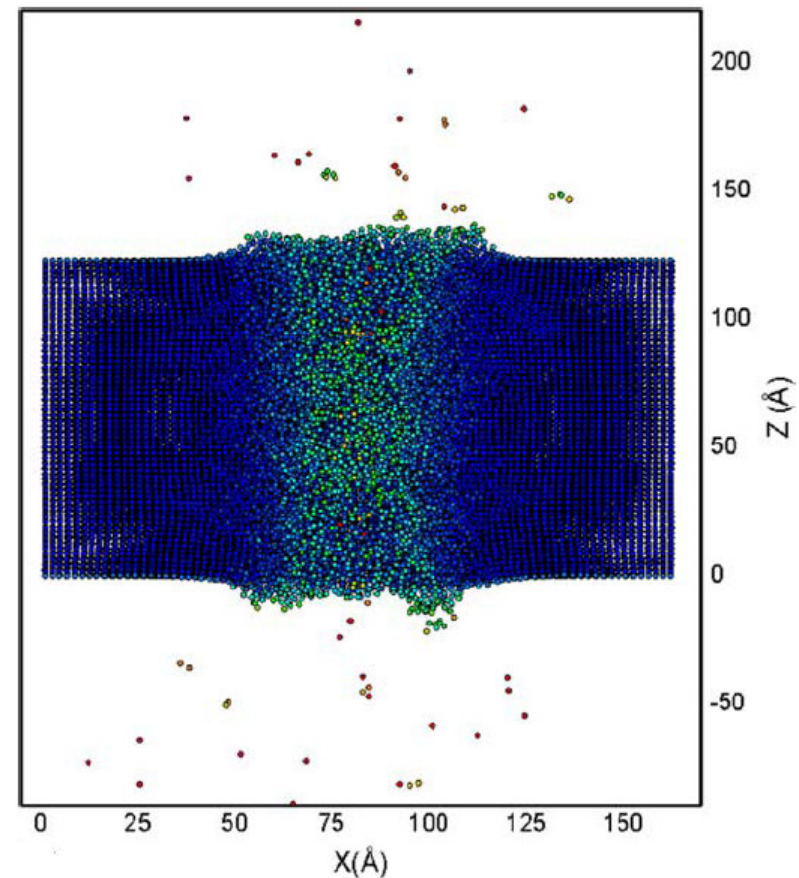
MD simulation of sputtering from a cylindrical track

O.J. Tucker, D.S. Ivanov, L.V. Zhigilei, R.E. Johnson, E.M. Bringa, NIMPR B 228 (2005) 163

Snapshots from simulations of thermal spike in Au.

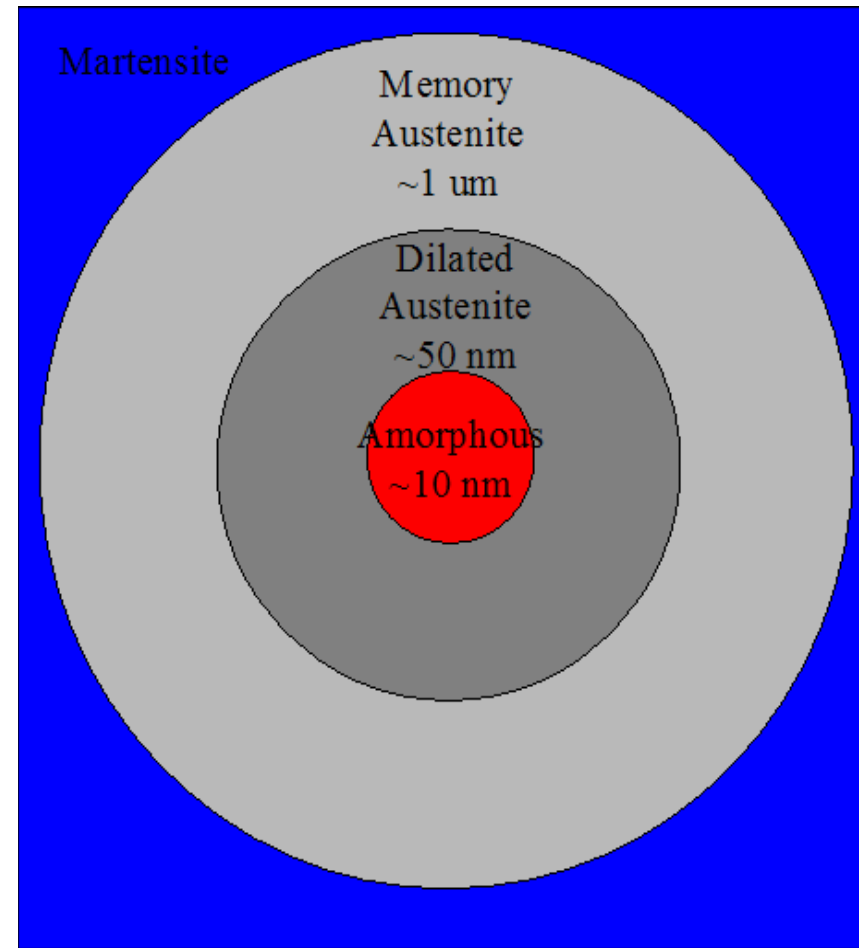
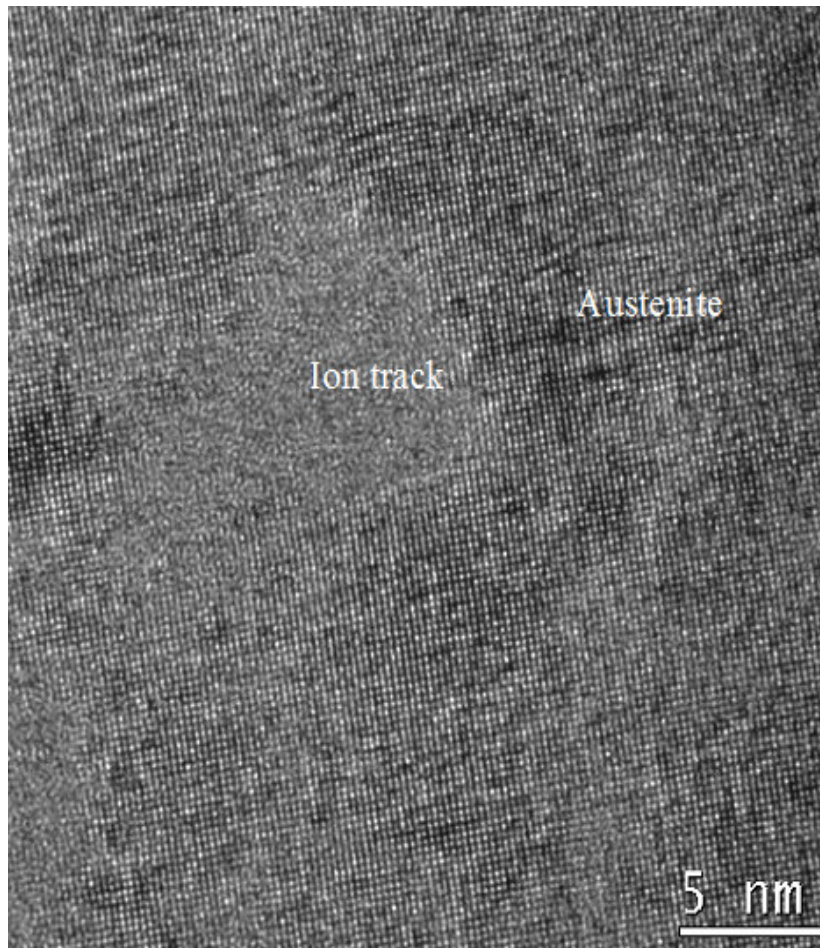
$$dE/dx = N_{\text{exc}} E_{\text{exc}} / d \sim n\pi R_{\text{cyl}}^2 E_{\text{exc}}$$

$$R_{\text{cyl}} = 10 \text{ \AA}, E_{\text{exc}} = 10 \text{ eV}, t = 4 \text{ ps}$$



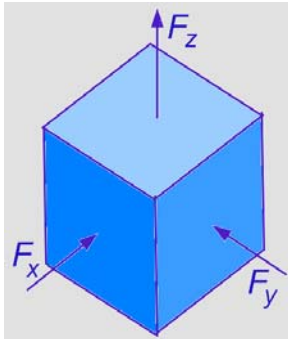
Microstructure of the 350 MeV Au ion irradiated Ti-Ni thin film

T. LaGrange, R. Schäublin, D. S. Grummon, C. Abromeit, R. Gotthardt, *Phil. Mag.* **85** (2005) 577

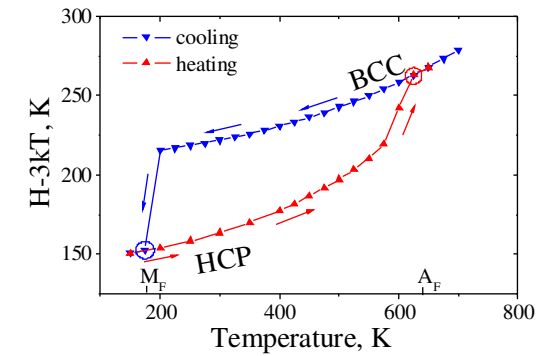


Problems

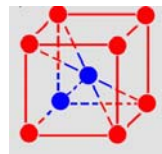
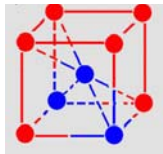
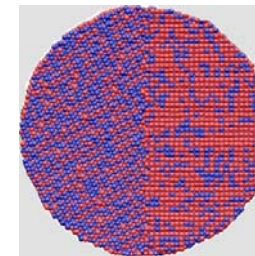
MT at fast heating/cooling



Stress-controlled MT

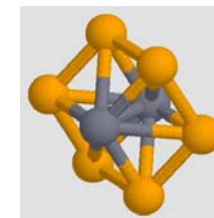


Effect of interfaces

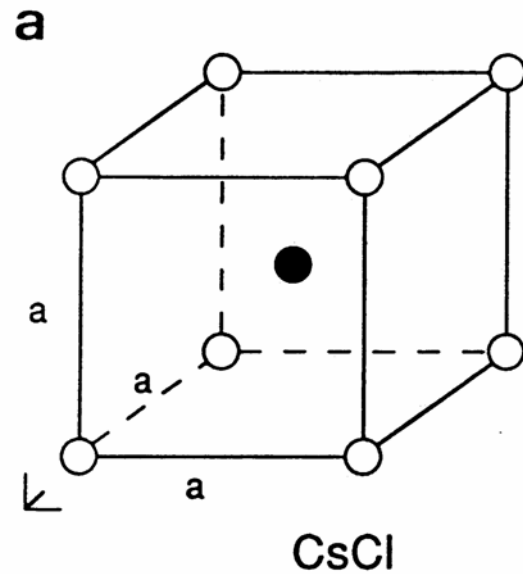


Compositional order-disorder

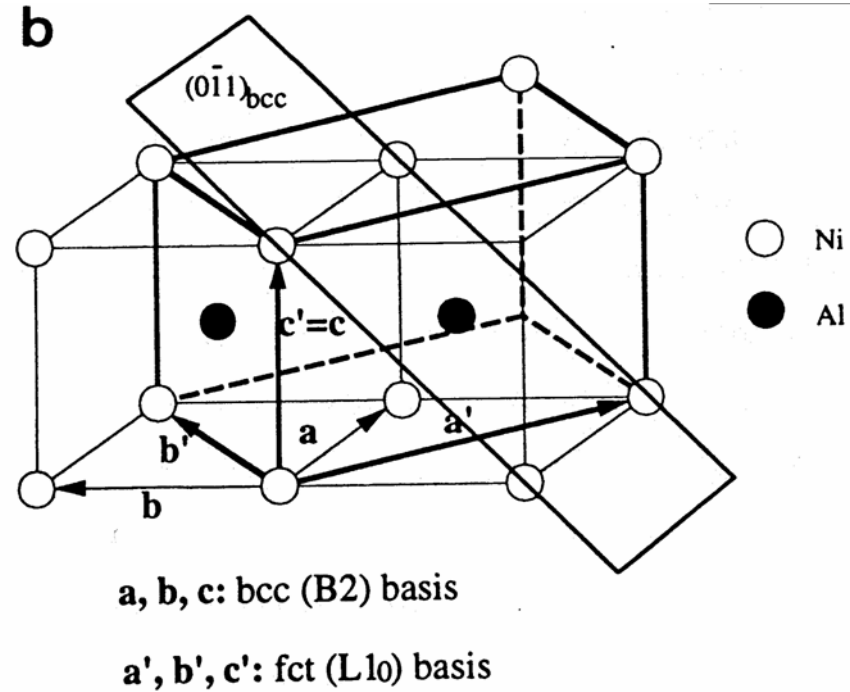
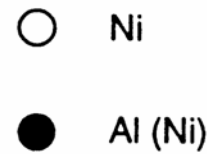
Local structure order



Lattice correspondence: austenite - martensite lattices



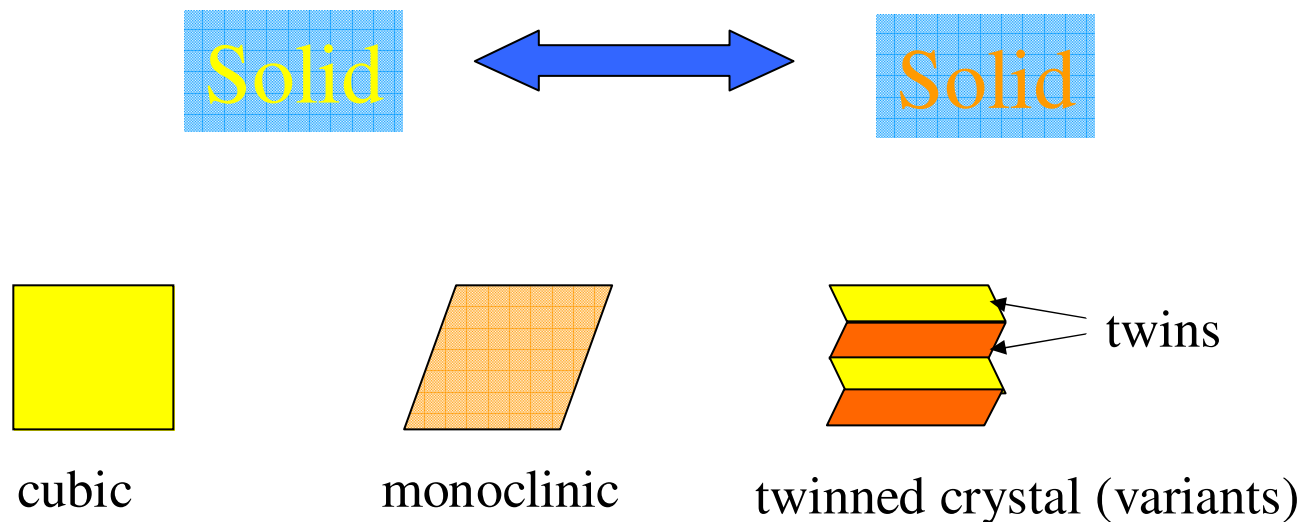
**austenite B2 structure
(CsCl ordering)**



martensite L1₀ lattices

Shape Memory Alloys

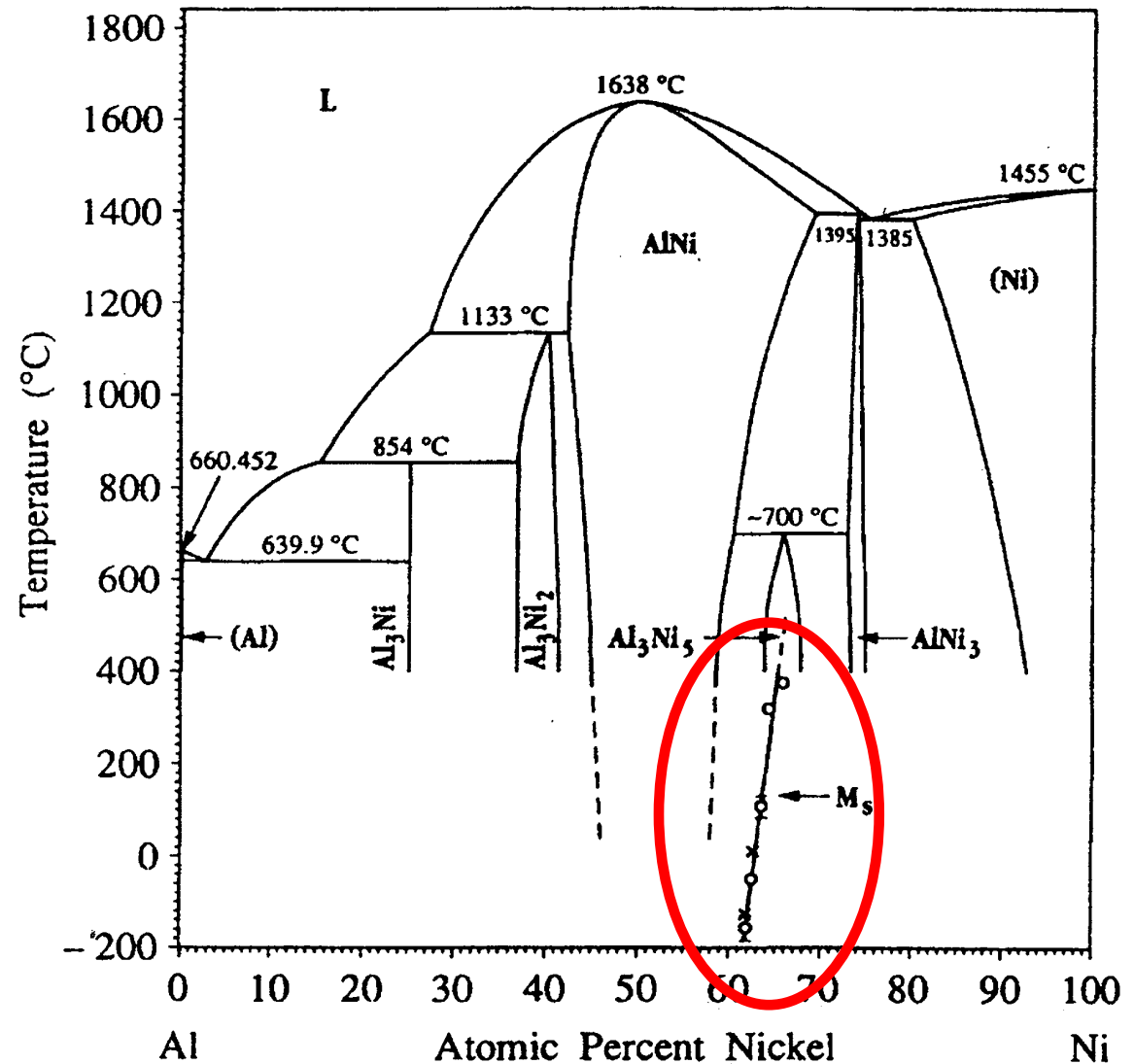
Ni-Ti, Cu-Zn-Al, Cu-Al-Ni, *Au-Cd*, *Fe-Pt*, *Ni-Al*



A non-diffusion transformation which can be induced by:

- temperature change
- applying stress

Phase diagram of Ni-Al system



H. Okamoto,
J. Phase Equilibria
14(2) (1993) 257



Simulation Setup



Molecular Dynamics with Empirical force-field

EAM potential:

$$U = \sum_{ij} V(r_{ij}) + \sum_i F(\rho_i)$$

Limitations:

System size

$$N = 10^4 \div 10^7$$

Time window

$$t = 1 \div 20 \text{ ns}$$



Potentials

A.F. Voter and S.P. Chen, *Accurate Interatomic Potentials for Ni, Al, and Ni₃Al*, Mat. Res. Soc. Symp. Proc. 82 (1987) 175.

D. Farkas, B. Mutasa, C. Vailhe, K. Ternes, *Interatomic potentials for B2 NiAl and martensitic phases*. Modeling Simul. Mater. Sci. Eng. 3 (1995) 201-214.

M. Yan, V. Vitek and S. P. Chen, *Many-body central force potentials and properties of grain boundaries in NiAl*, Acta Mater. 44 (1996) 4351-4365.

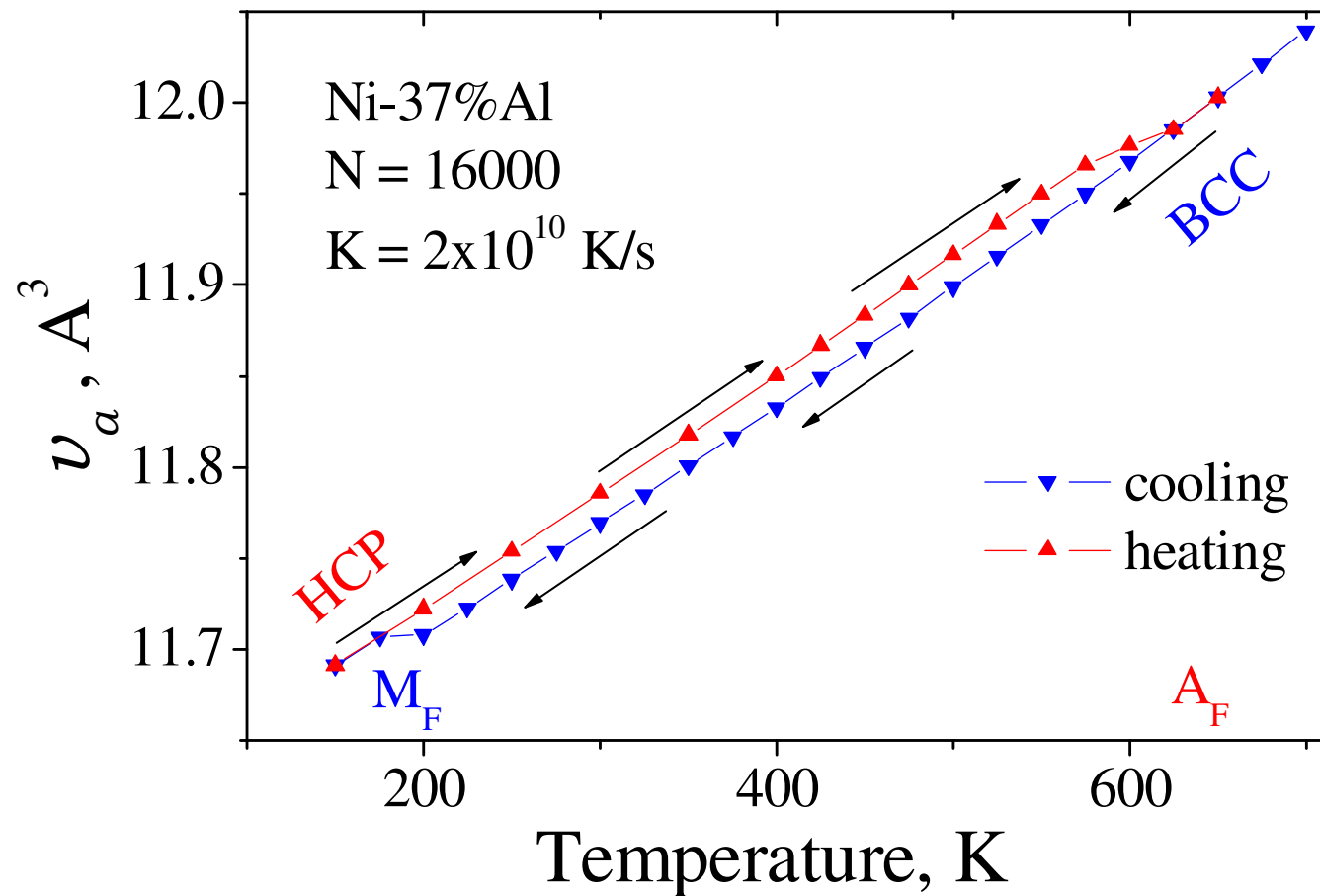
Y. Mishin, M. J. Mehl and D. A. Papaconstantopoulos, *Embedded-atom potential for B2-NiAl*, Phys. Rev. B65 (2002) 224114.

N. I. Papanicolaou, H. Chamatia, G. A. Evangelakisa, D. A. Papaconstantopoulos, *Second-moment interatomic potential for Al, Ni and Ni-Al alloys, and molecular dynamics application*, Comp. Mater. Sc. 27 (2003) 191-198.

Song Yua, Chong-Yu Wanga, Tao Yua, Jun Cai, *Self-diffusion in the intermetallic compounds NiAl and Ni₃Al: An embedded atom method study*, Physica B 396 (2007) 138–144.

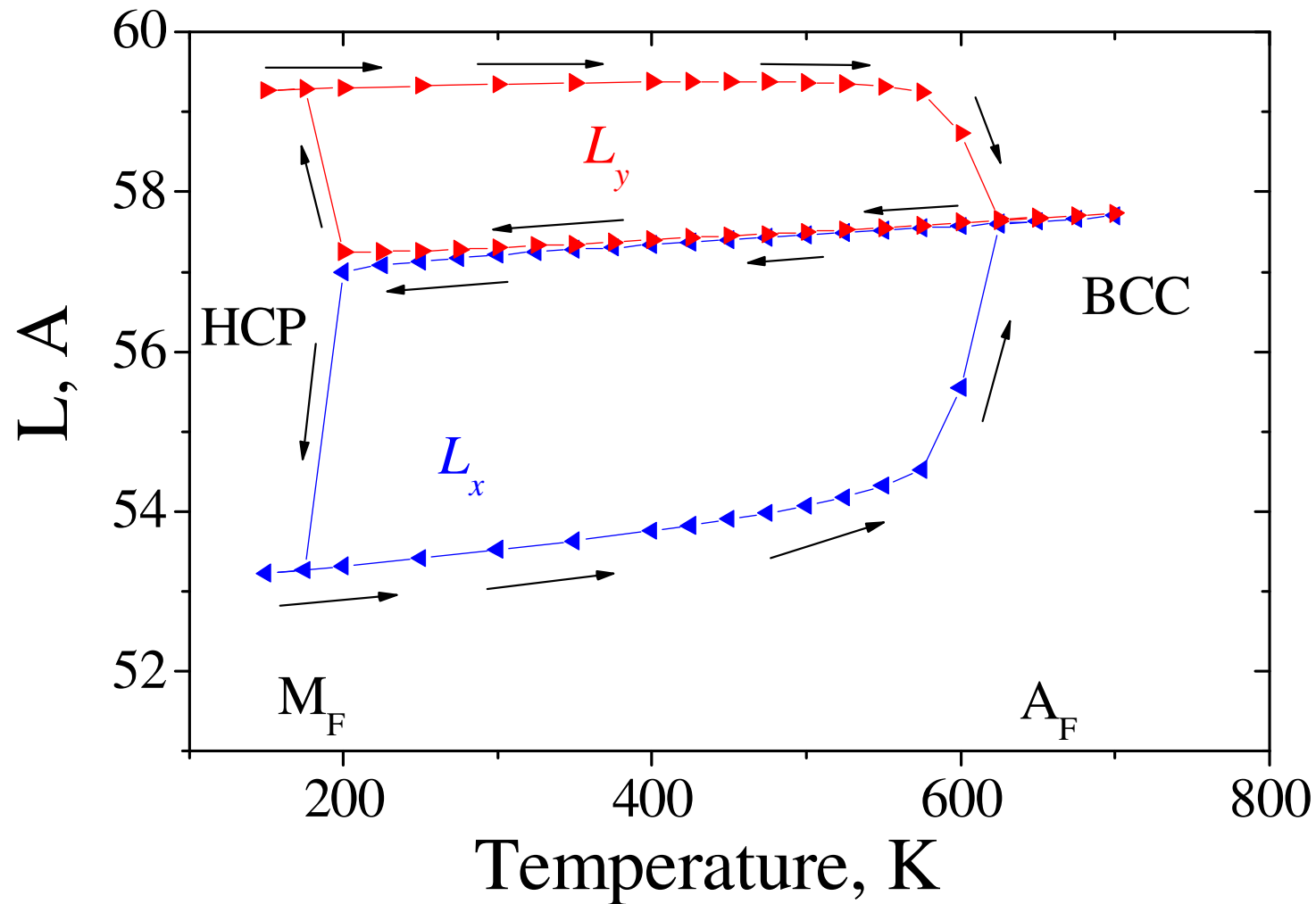
Temperature-controlled MT at constant external stress

N. P. Lazarev, C. Abromeit, R. Schäublin and R. Gotthardt, Solid-Solid Phase Transformations in Inorganic Materials, TMS publications, 2005, Vol. 2, p. 715.



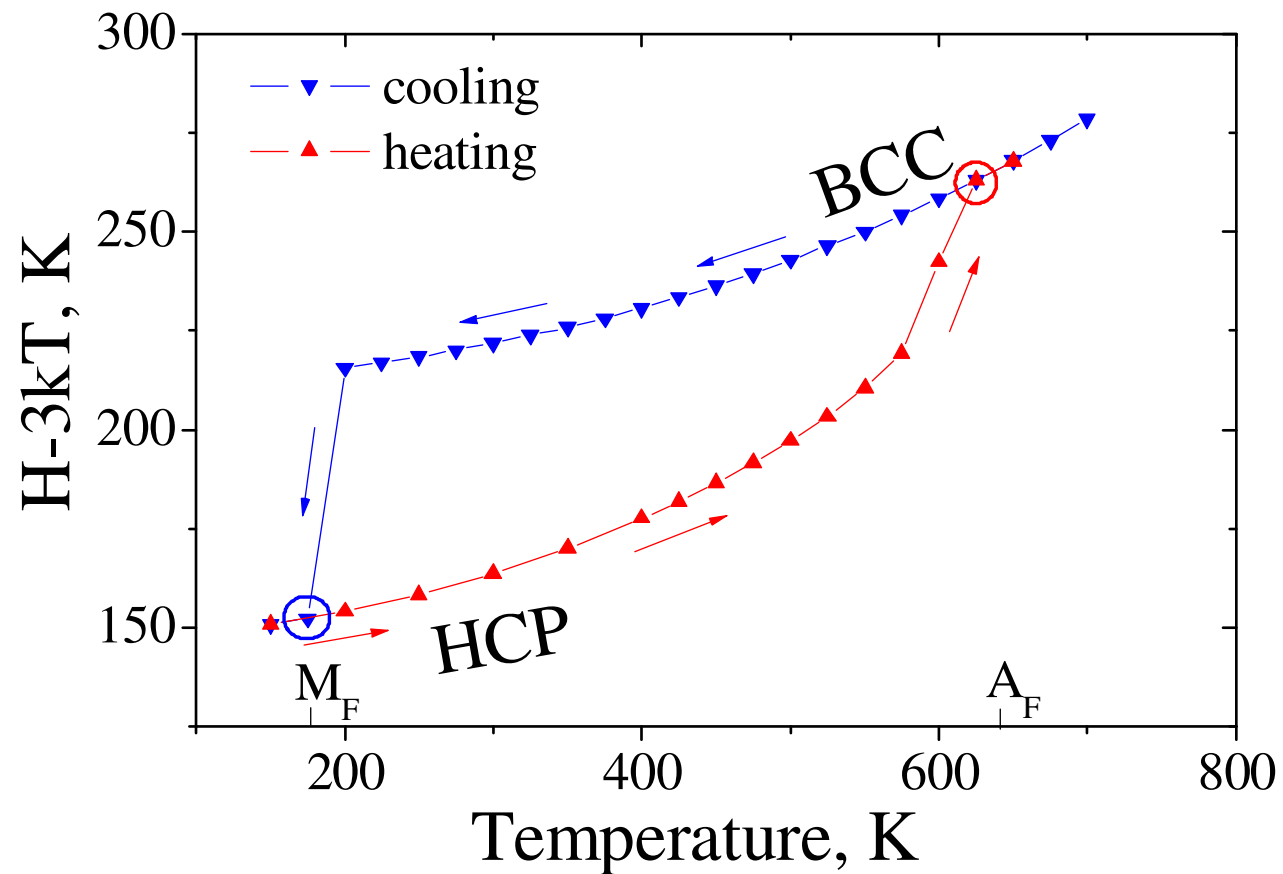
■ *Reversible phase transformation*

Shape Changes of Simulated Box



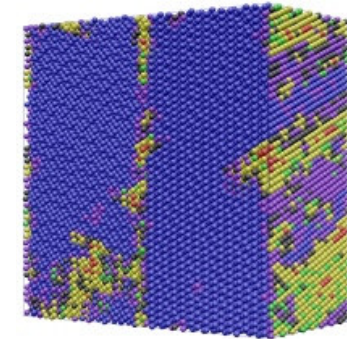
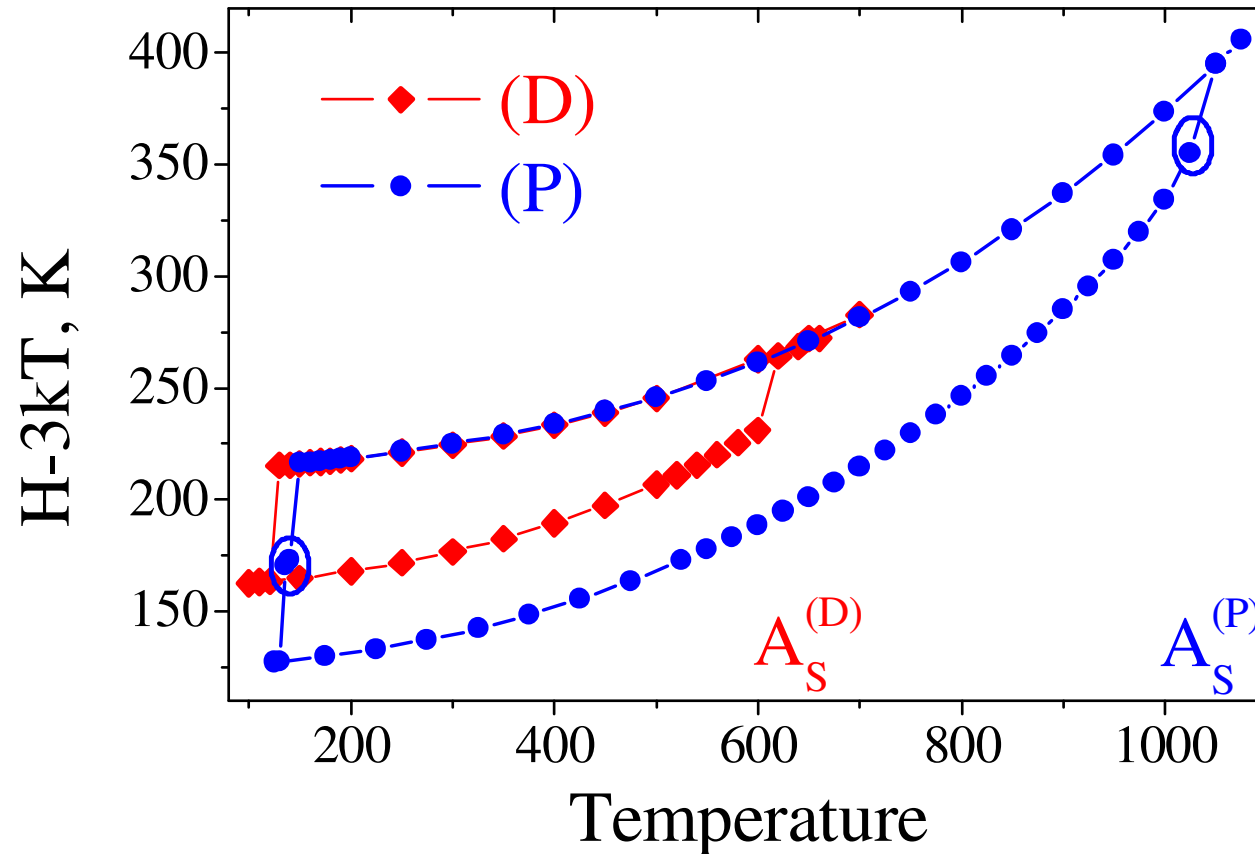
- *Linear dimensions are more sensitive to MPT than average volume*

Enthalpy at Reversible MTs

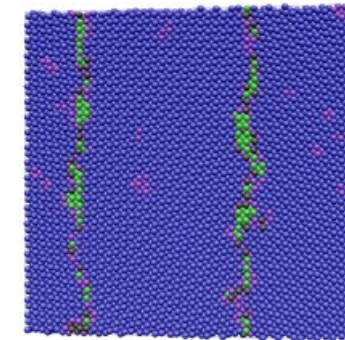


- *The 1-st order phase transformations: $A \rightarrow M \rightarrow A$*

Hysteretic behavior of different samples at equal composition Ni-37%Al.



(D)

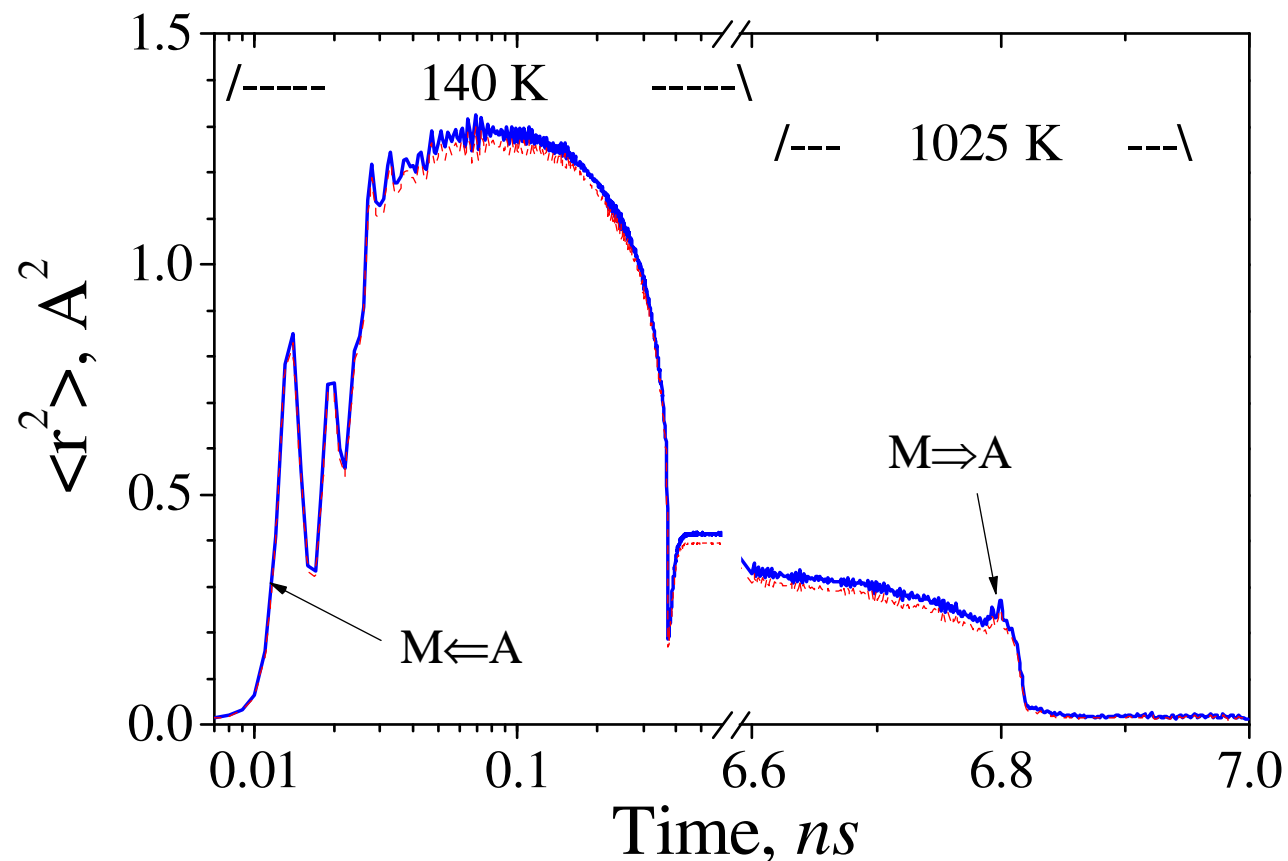


(P)

- *Hysteresis width essentially depends on defect structure of martensite state*

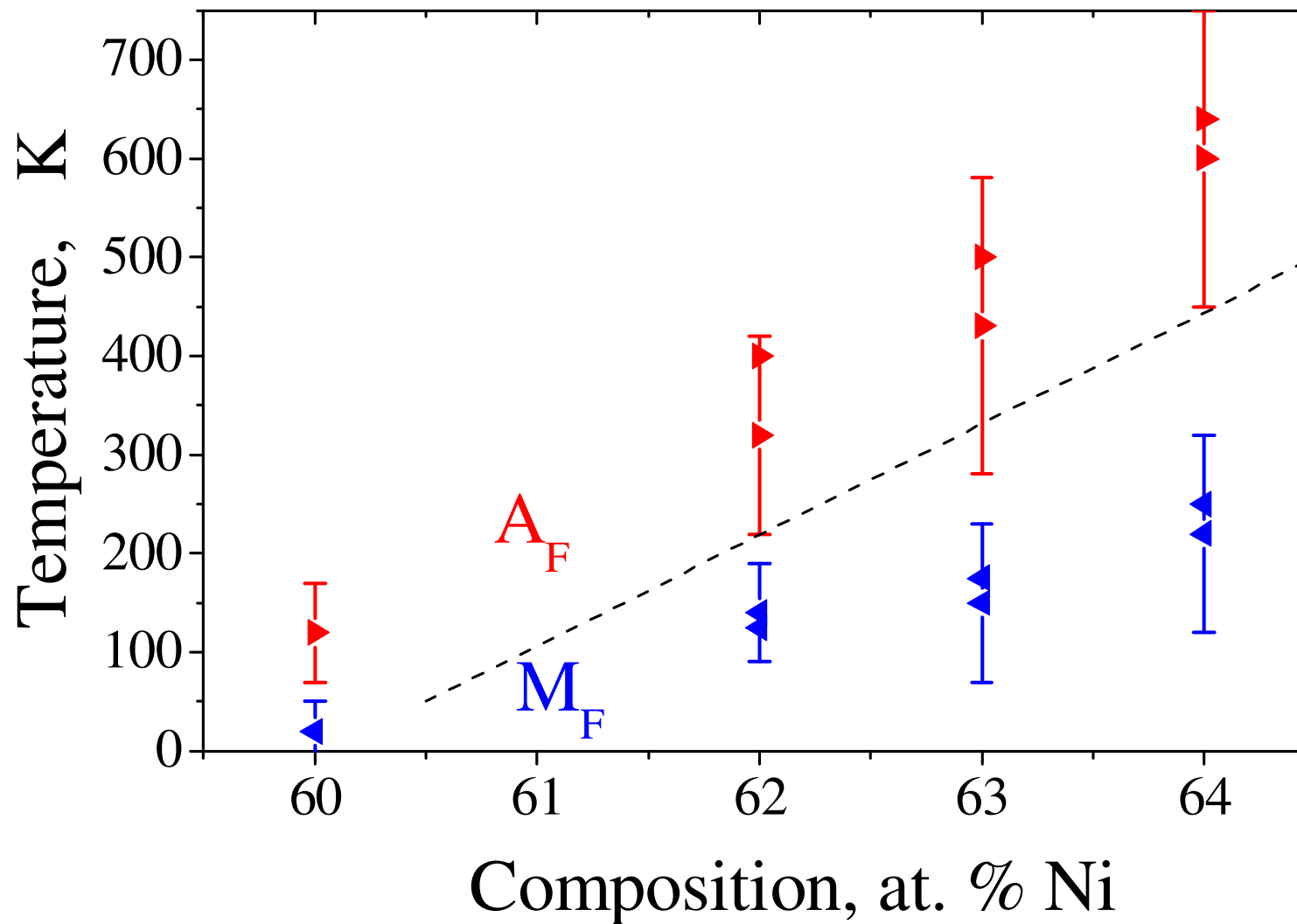
Atomic displacements during cycle $A \rightarrow M \rightarrow A$

N. P. Lazarev, C. Abromeit, R. Schäublin, R. Gotthardt, J. Appl. Phys. 100 (2006) 063520



- *Non-diffusional transformations and completely reversible*

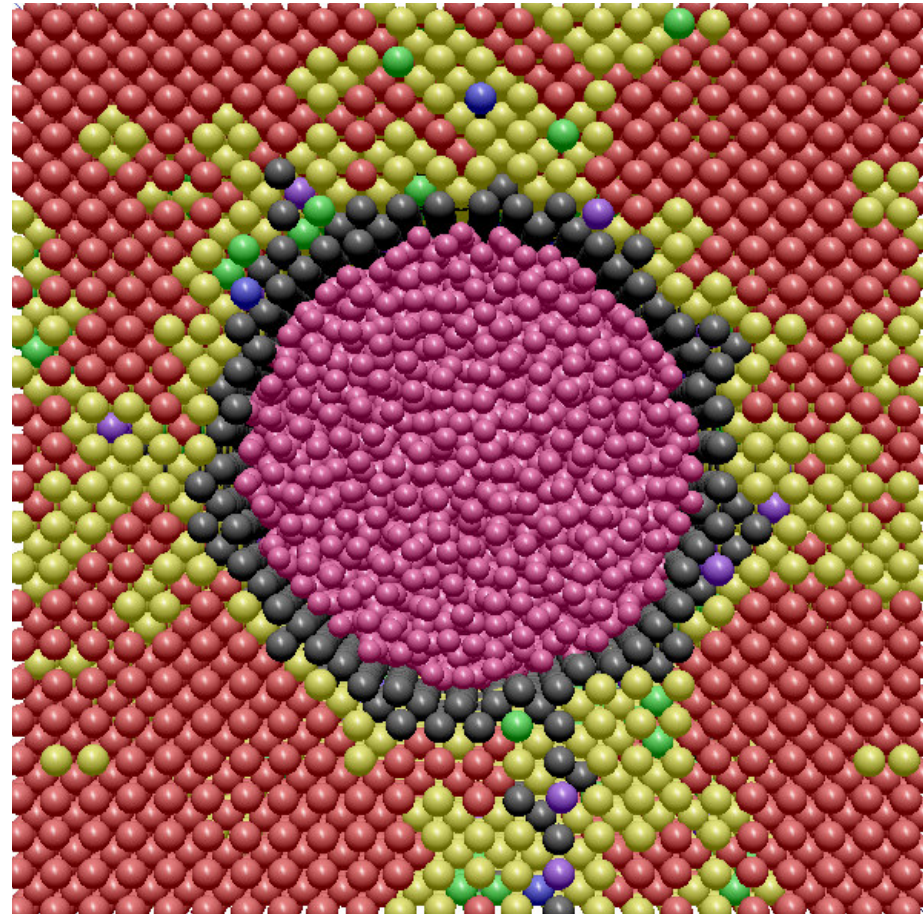
Composition dependent MPT

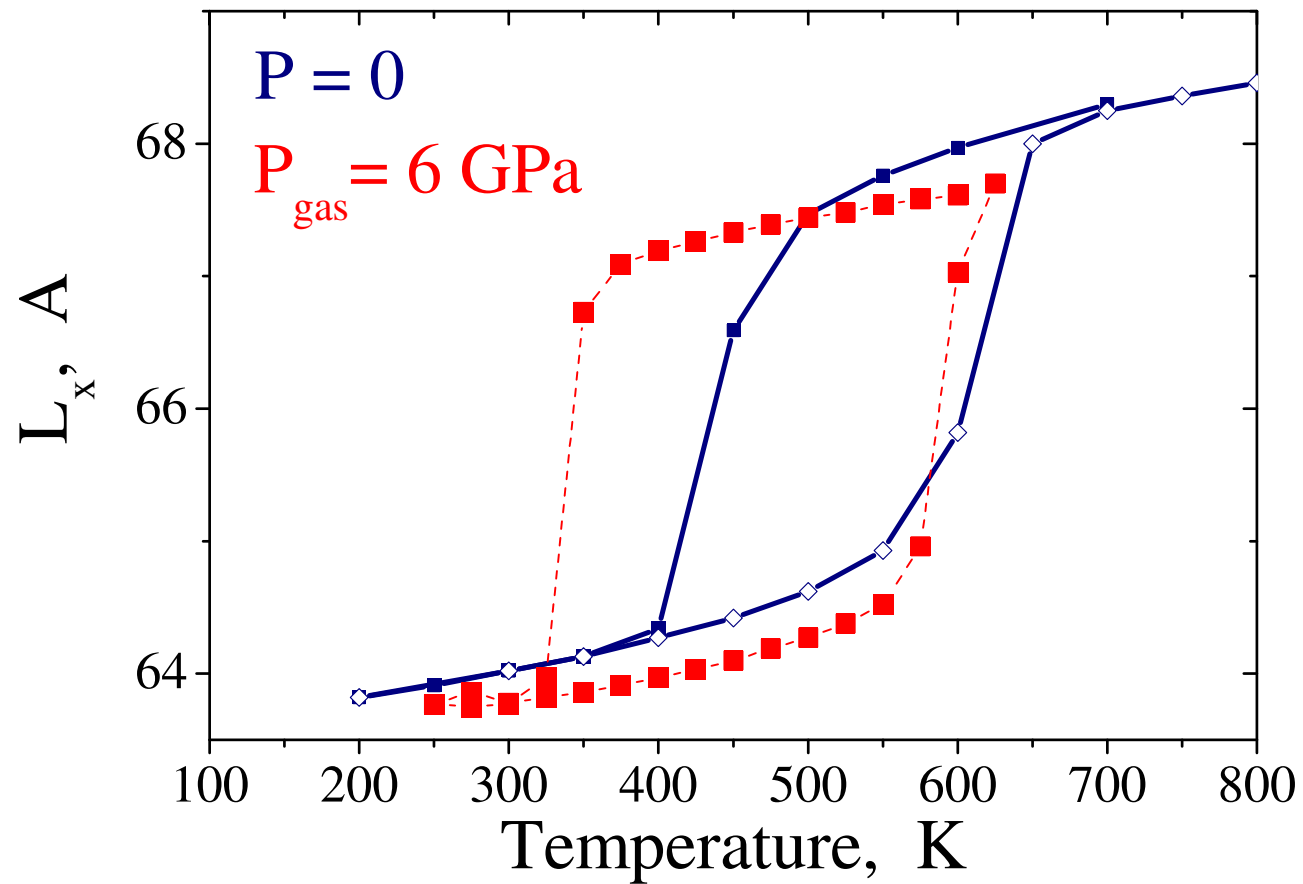


- *MPT is observed in narrow composition interval: 60-65 at. % Ni*

Cylinder under pressure, Ni₆₀Al₄₀

Perfect FCC + HCP
Distorted FCC + HCP
Perfect BCC
Distorted BCC
Perf. & Dist. ICO
Gas atoms
Unclassified

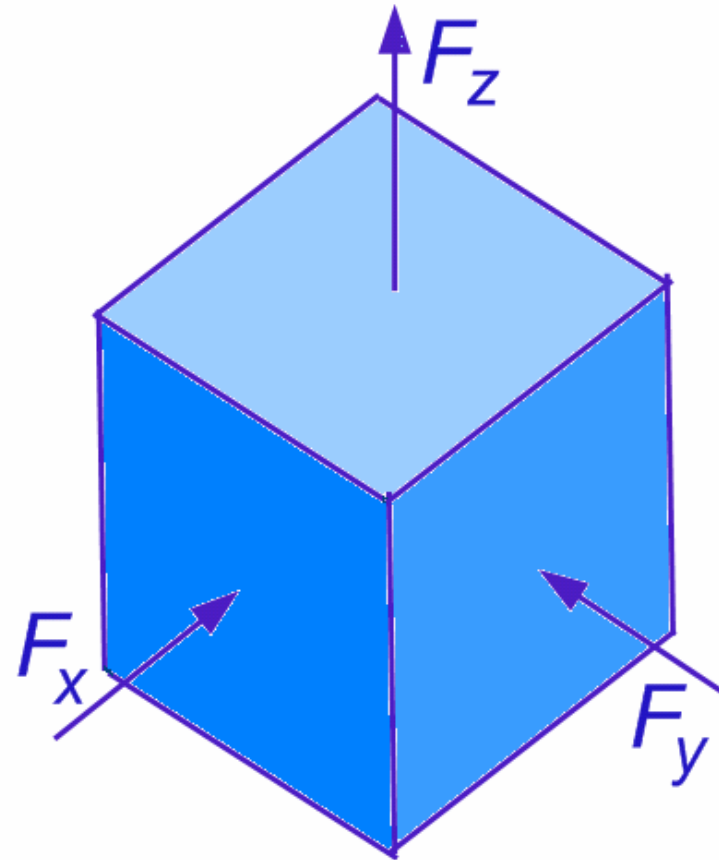


Cylinder under pressure, $\text{Ni}_{60}\text{Al}_{40}$ 

Stress-Controlled MPTs at Constant Temperature

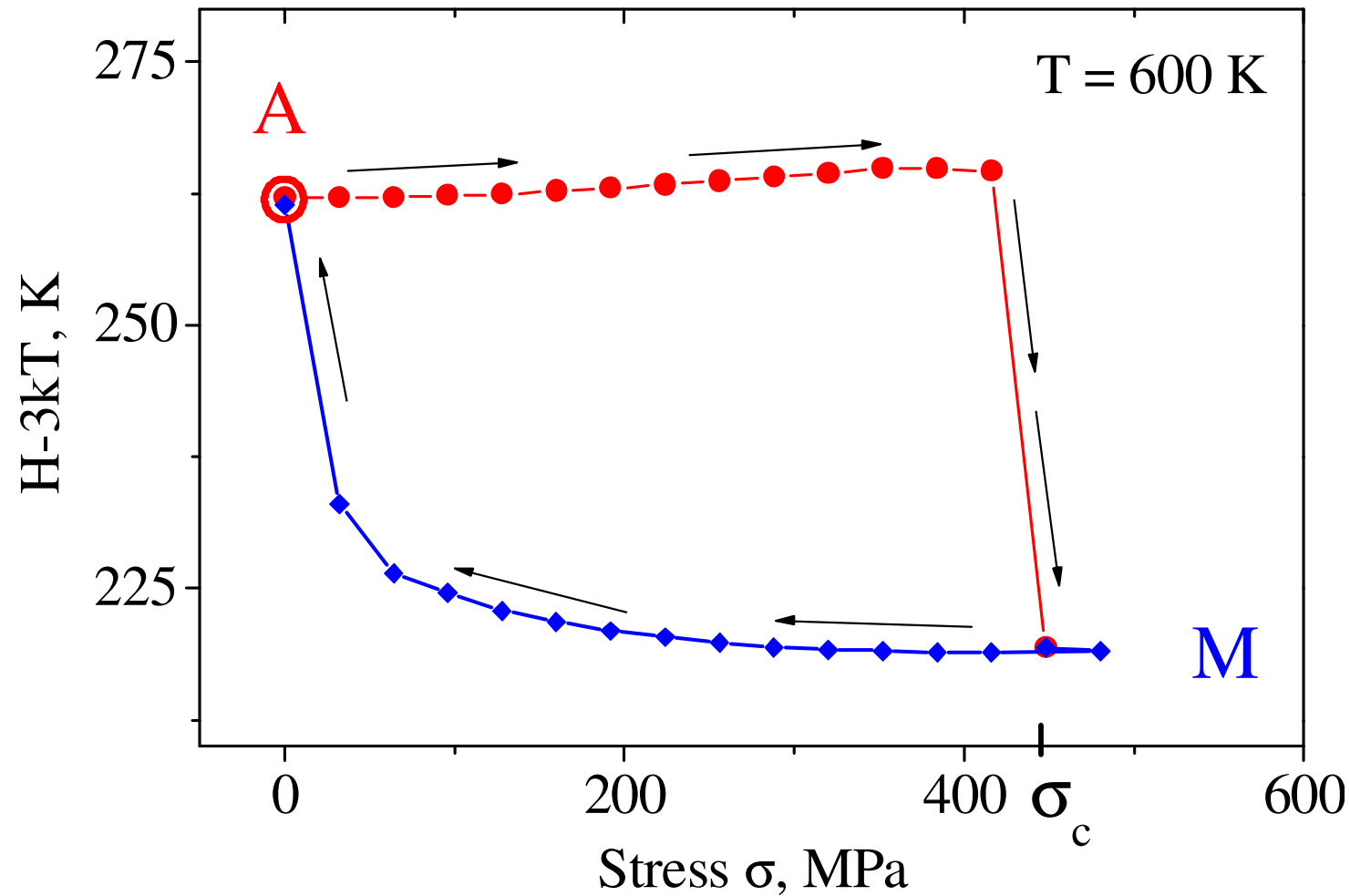
Multi-axial
compression/tension

$$\sigma_{xx} = \sigma_{yy} = -\sigma_{zz} / 2$$



Stress dependence

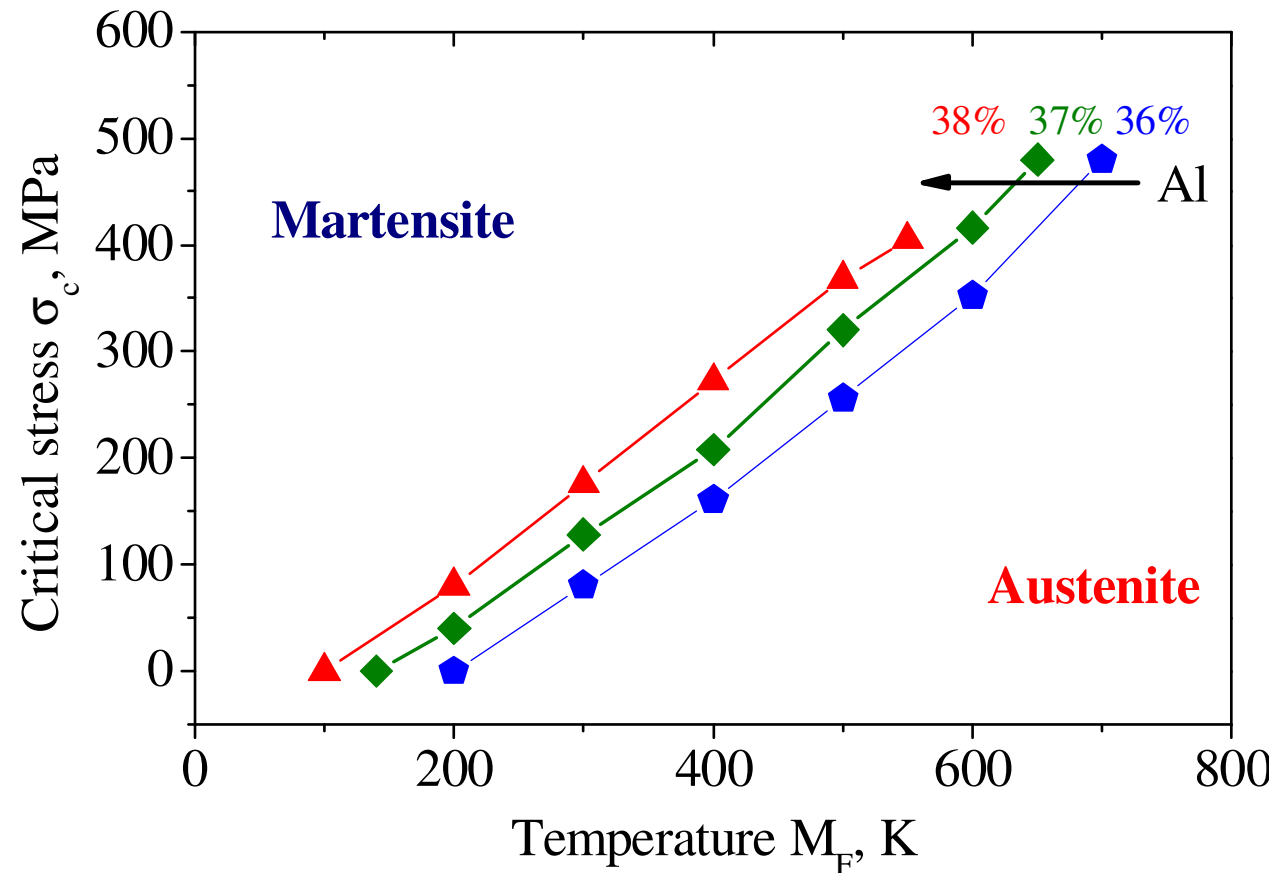
Ni-37%Al, N = 65536



■ *Reversibility on Stress*

Map of M_F -States

N. P. Lazarev, C. Abromeit, R. Schäublin, R. Gotthardt, Materials Science and Engineering A481–482 (2008) 205





Entropy of harmonic system

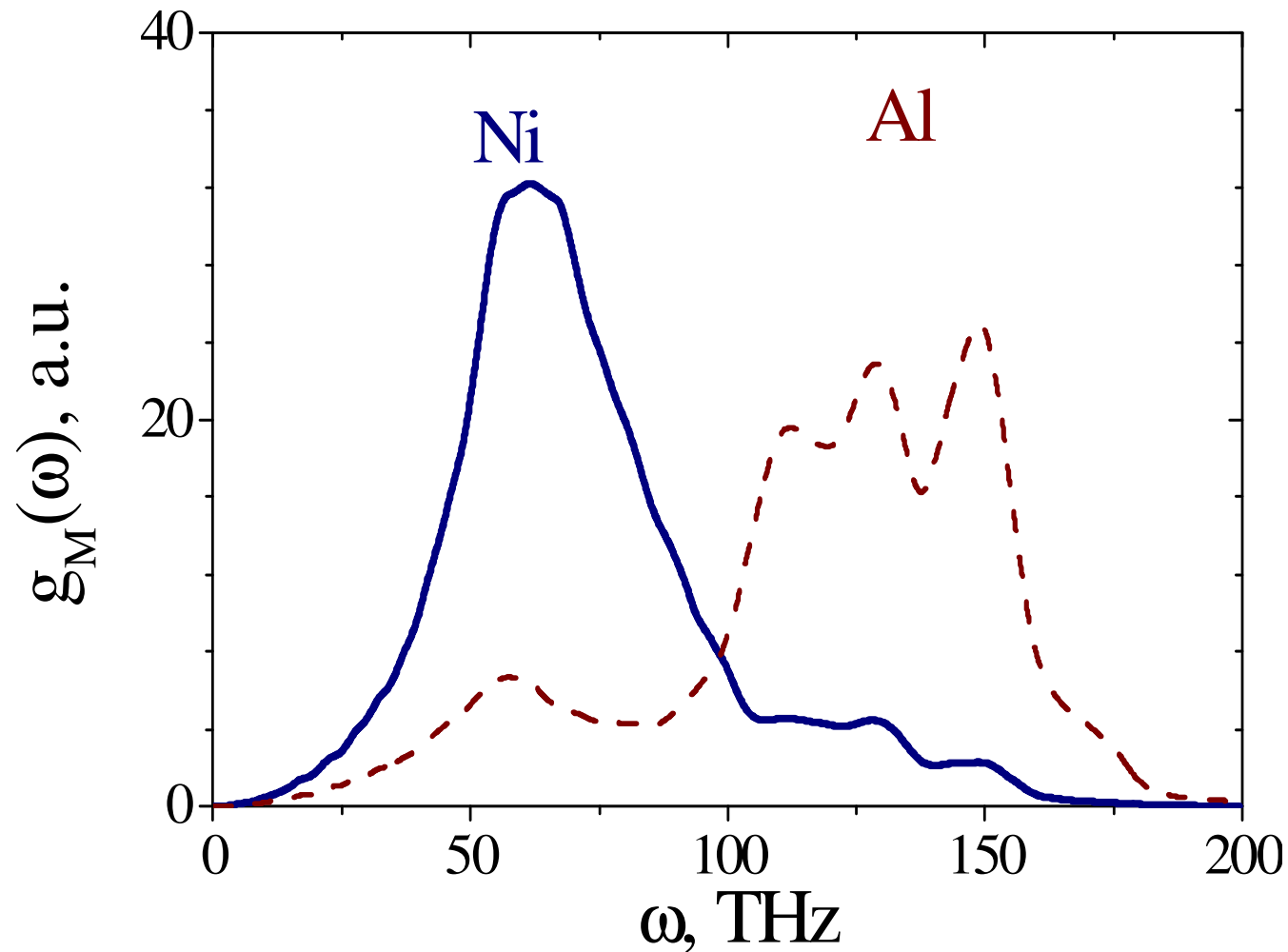
$$S_{har} = -k_B \sum_j \ln(\hbar \omega_j / k_B T) + S_0$$

$$\Delta S_{AM} = - \int_0^{\infty} \ln(\omega) [g_A(\omega) - g_M(\omega)] d\omega = - \ln \frac{\bar{\omega}_A}{\bar{\omega}_M}$$

$$A_{VV}(t) = \int_0^{\infty} V(\tau) V(\tau + t) d\tau$$

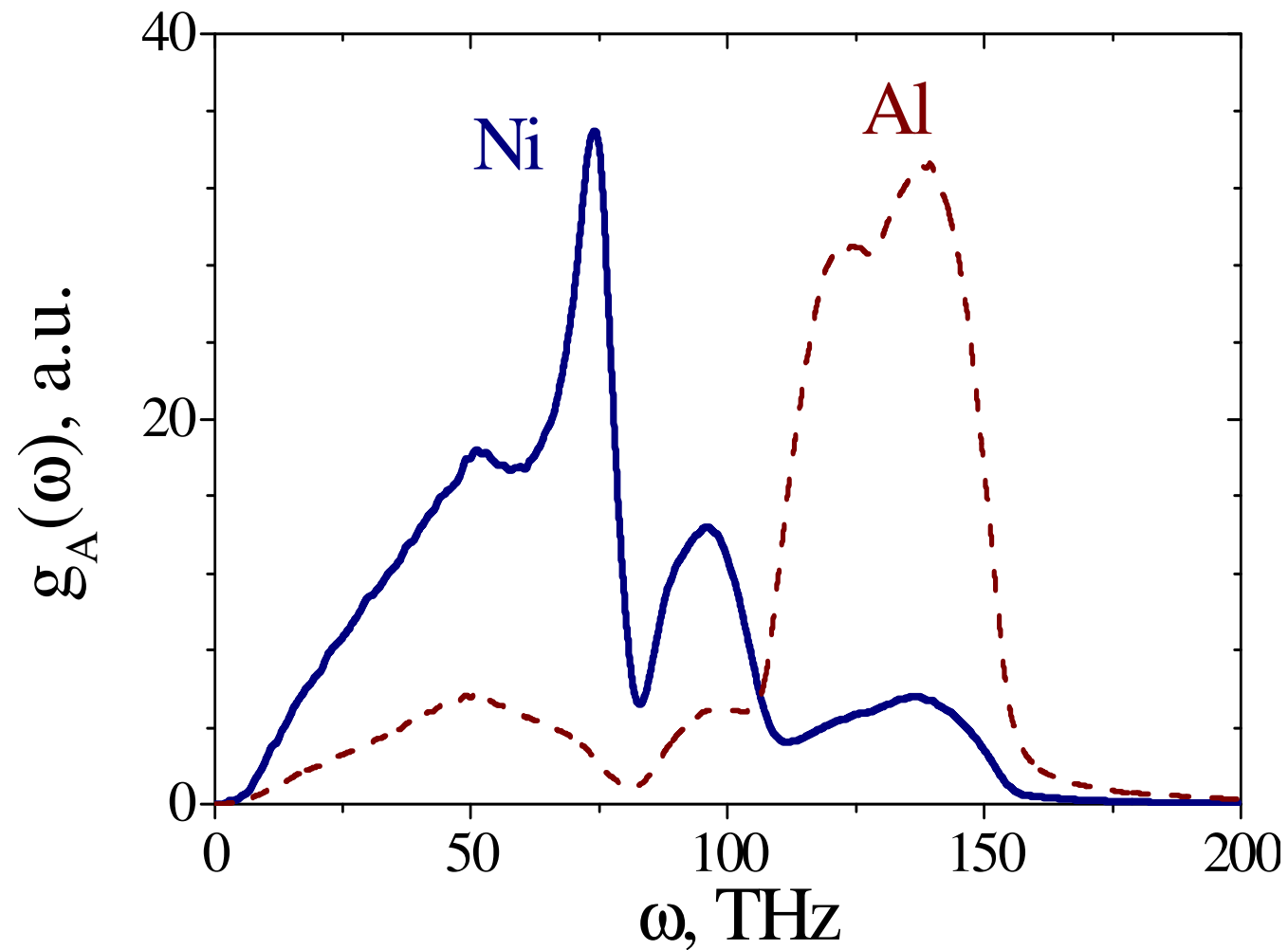
$$g(\omega) = \frac{1}{2\pi} \int_0^{\infty} e^{-\omega t} A_{VV}(t) dt$$

Spectral densities in martensite



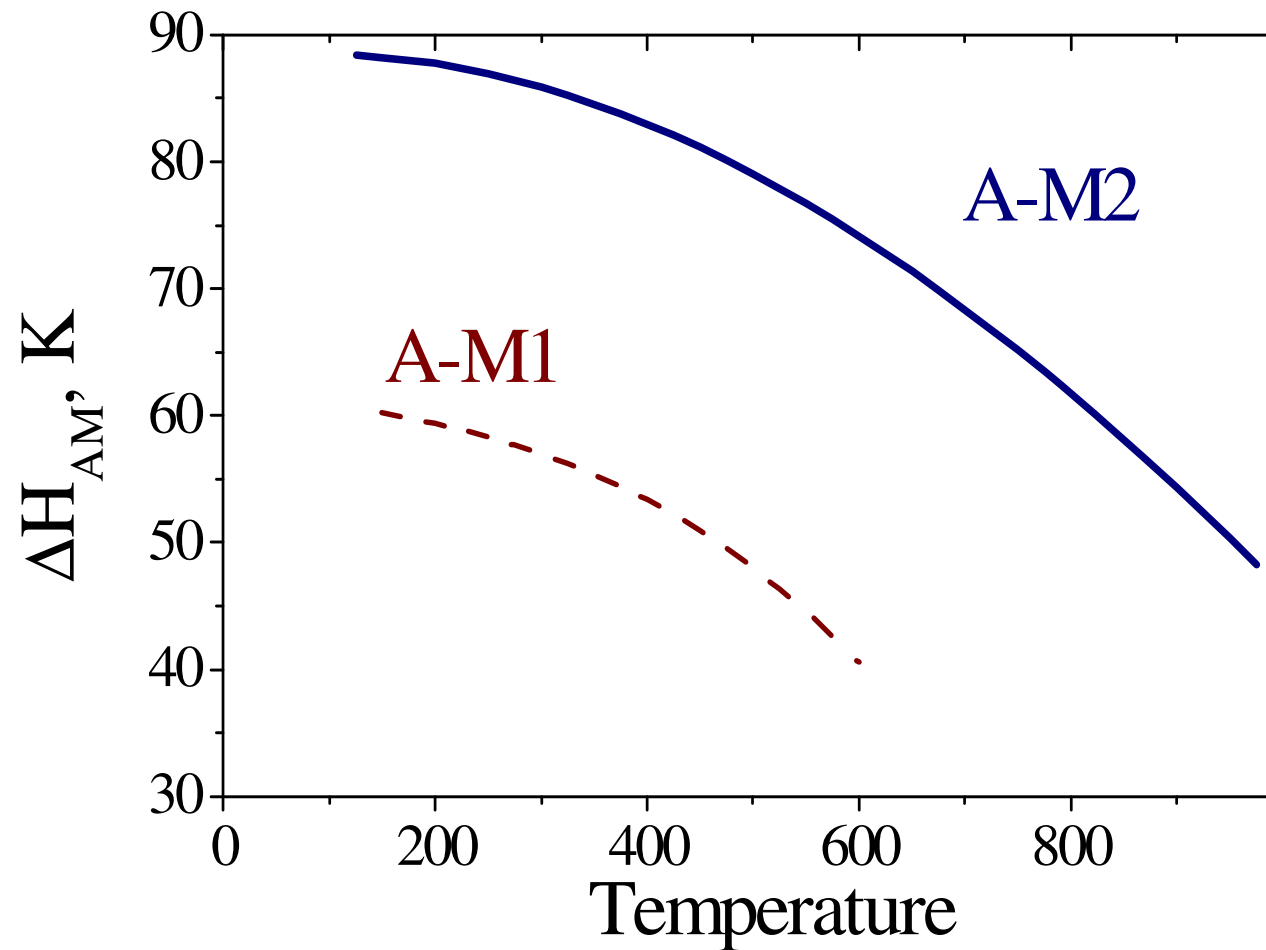
- *Low-frequency limit: $\sim \omega^2$*

Spectral densities in austenite

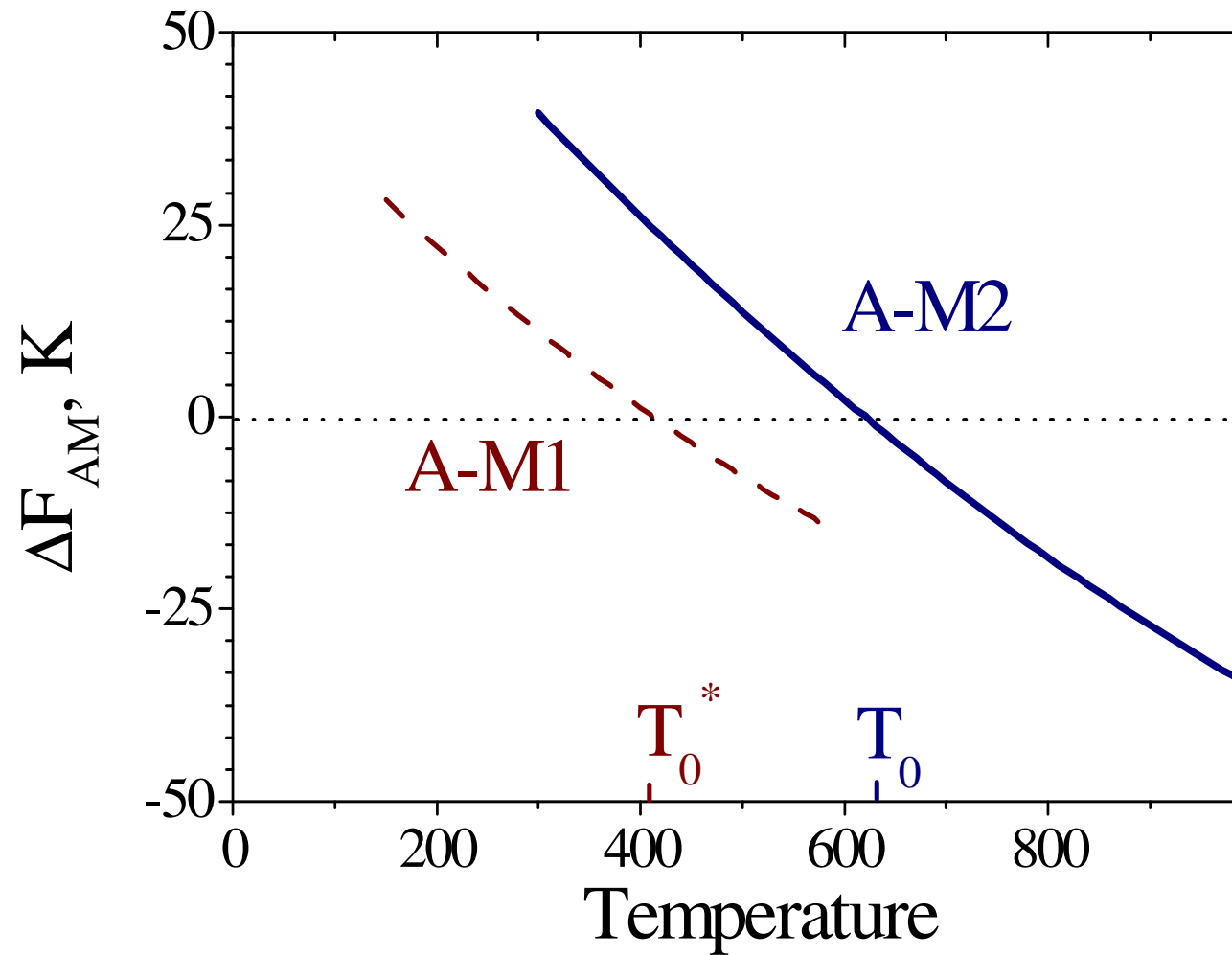


- *Soft modes at small ω ?*

Enthalpy difference, Ni-37%Al

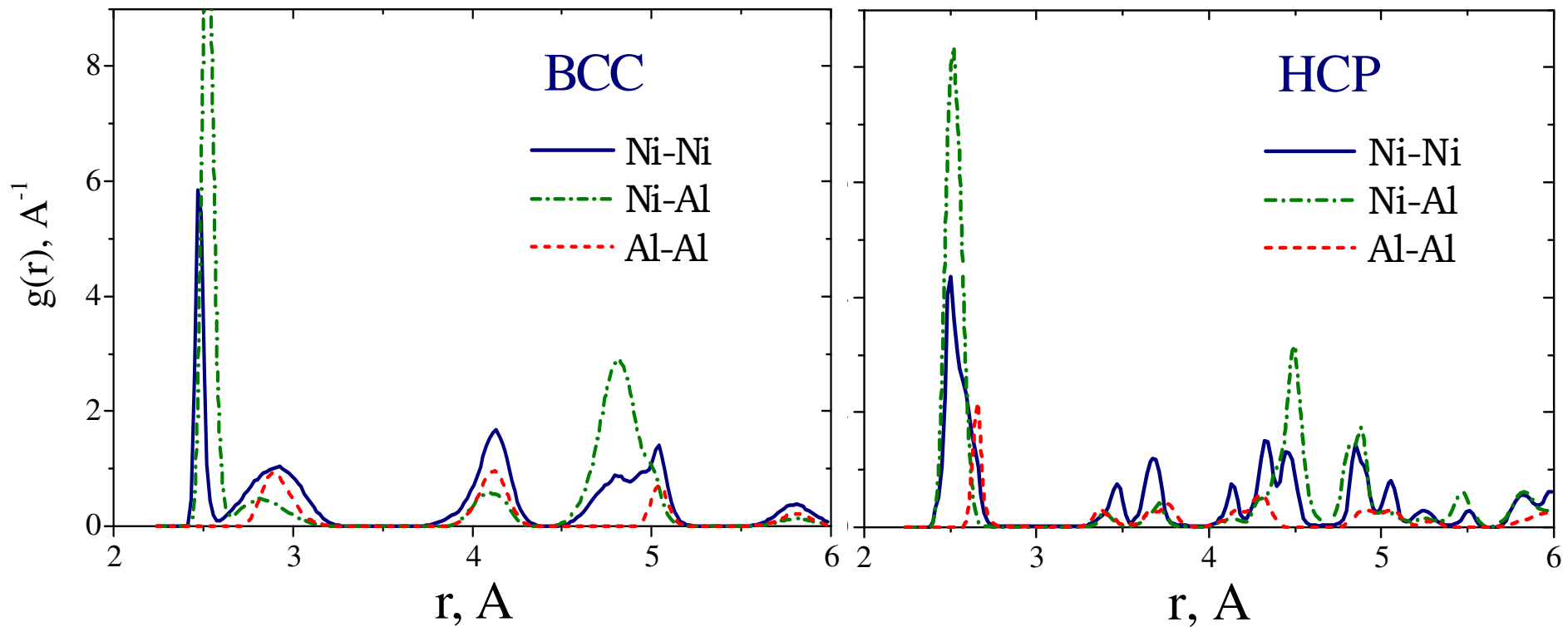


Free energy difference



Radial Distribution Function

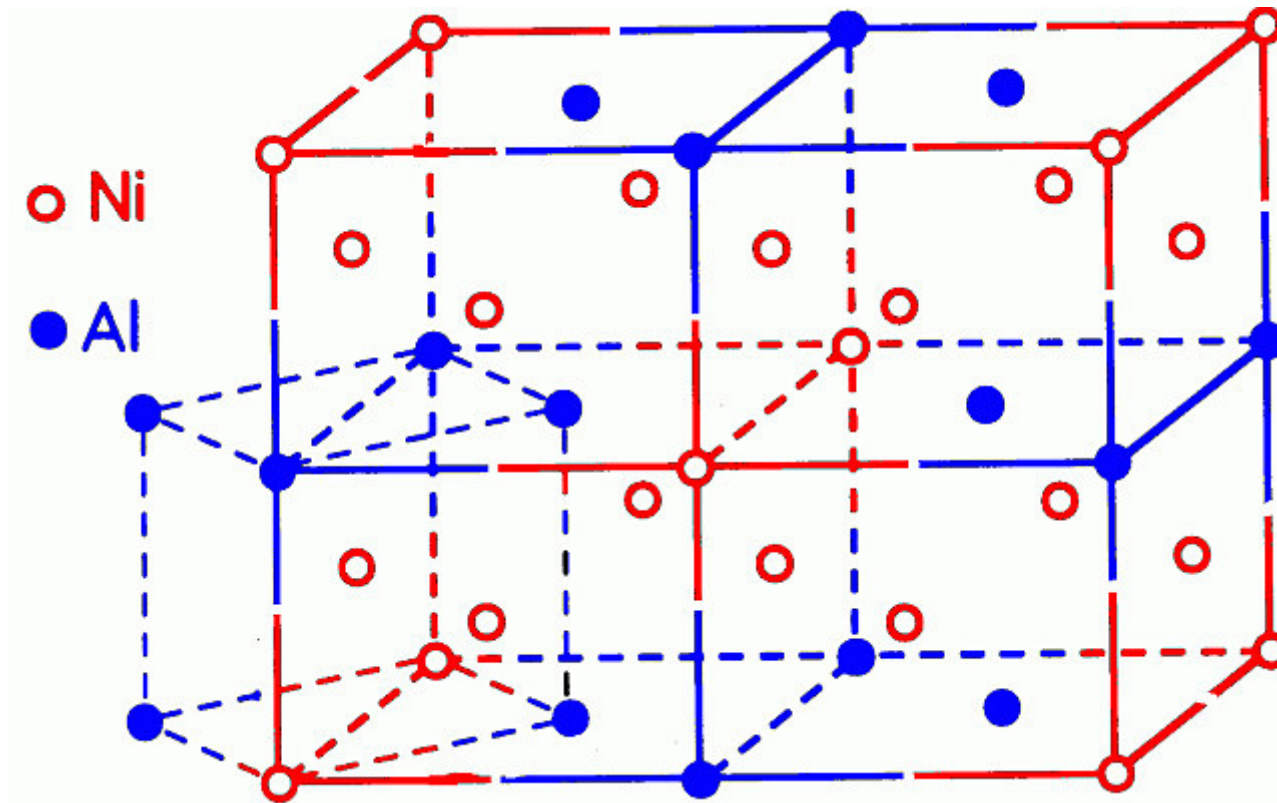
$$g(r) = \frac{V}{4\pi r^2 N^2} \left\langle \sum_i \sum_{j \neq i} \delta(r - r_{ij}) \right\rangle$$



■ BCC before MPT

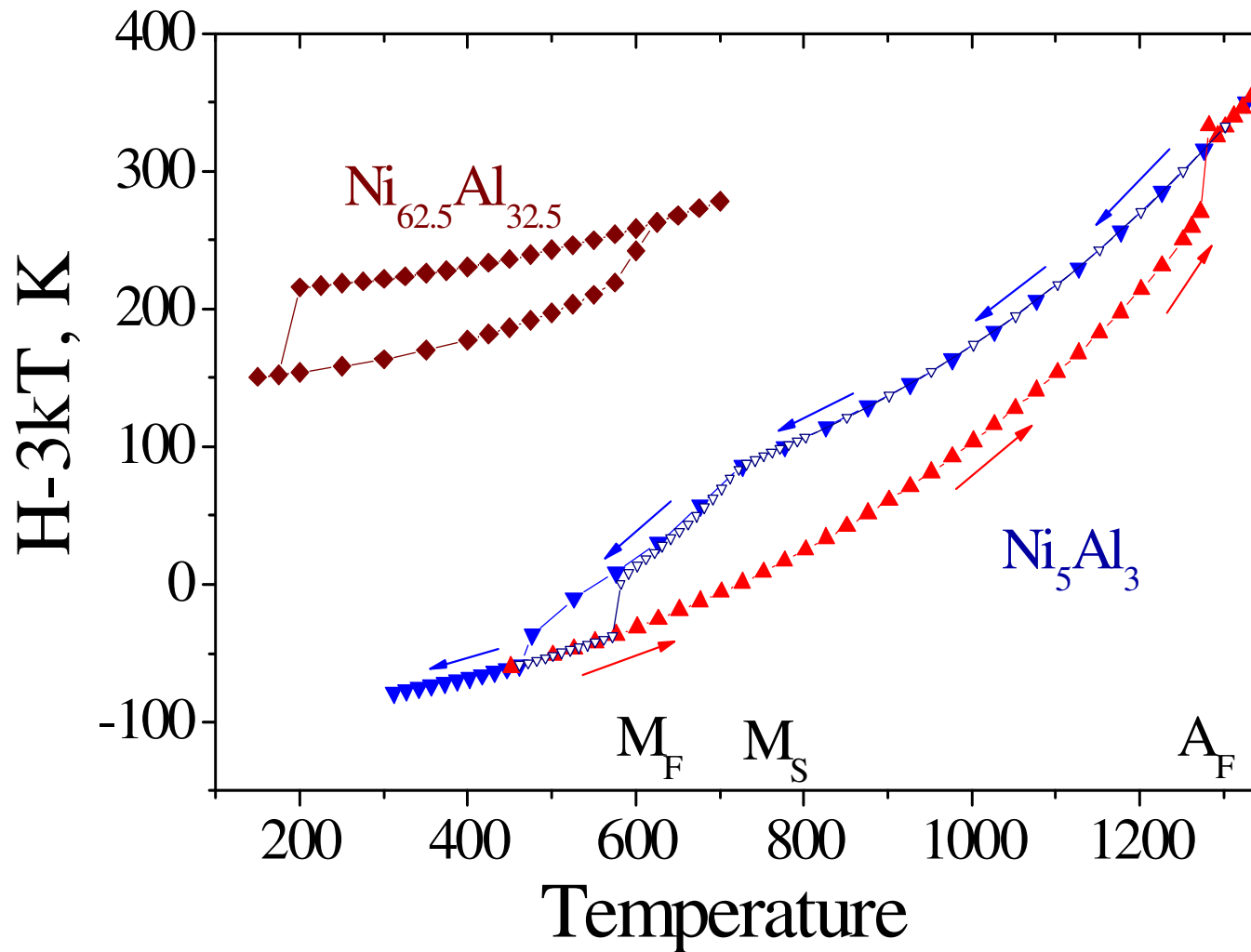
■ HCP after MPT

The Bainitic Ni_5Al_3 phase



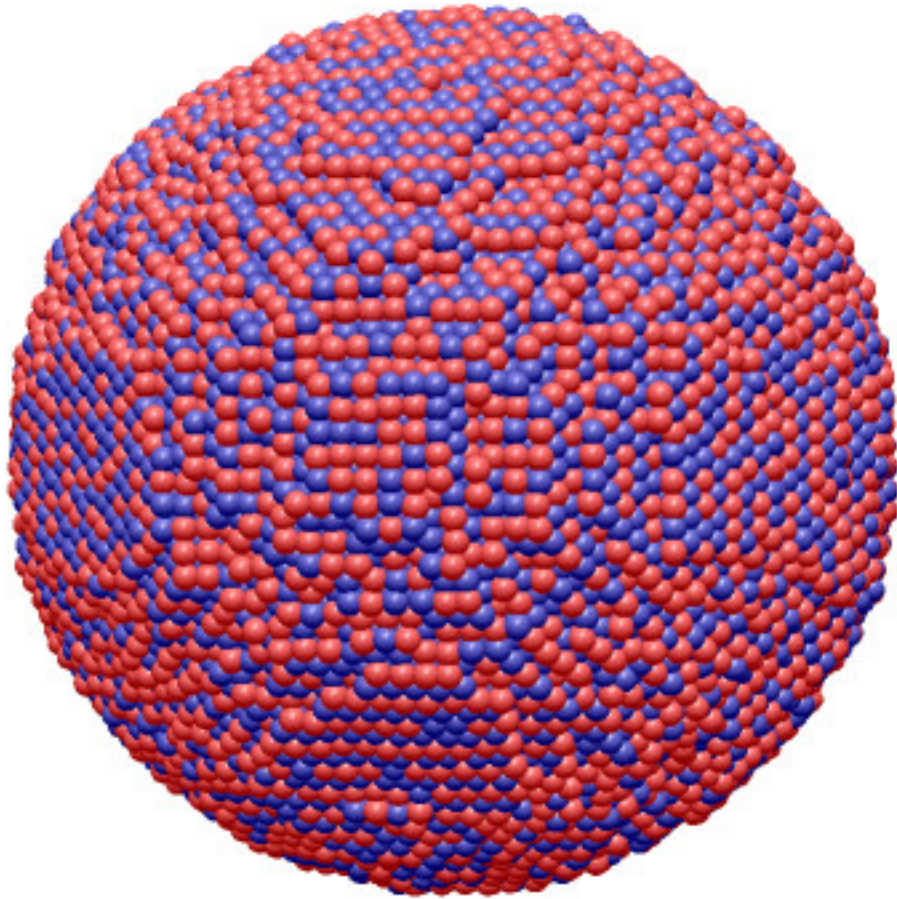
D. Schryvers et al,
J. de Physique IV, Vol. 5 (1995) Col. C8, p. 1029

MT in ordered alloy, Ni_5Al_3 (PBC): $B \rightarrow A \rightarrow B$

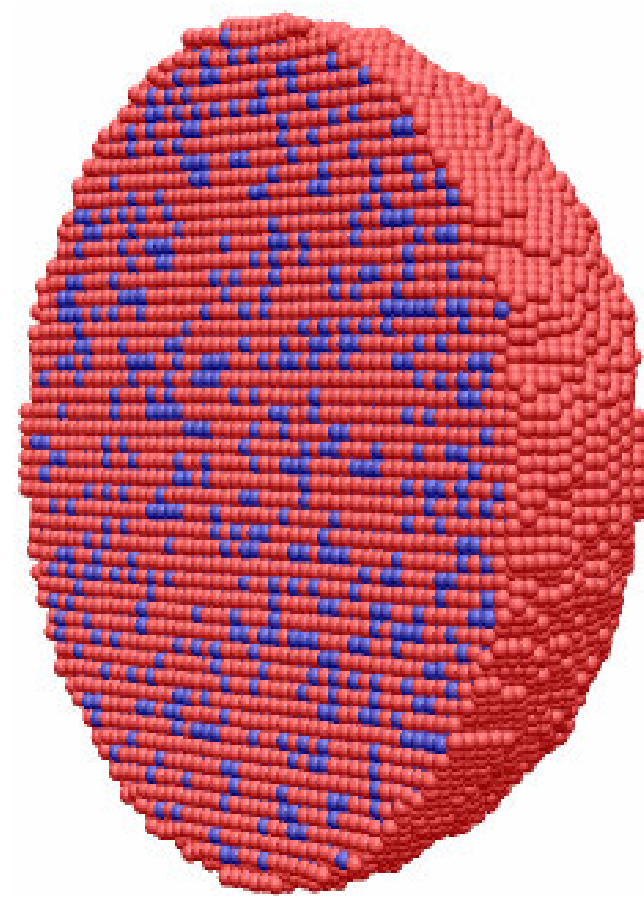


- *Compositional ordering facilitates to martensite (bainitic) phase*

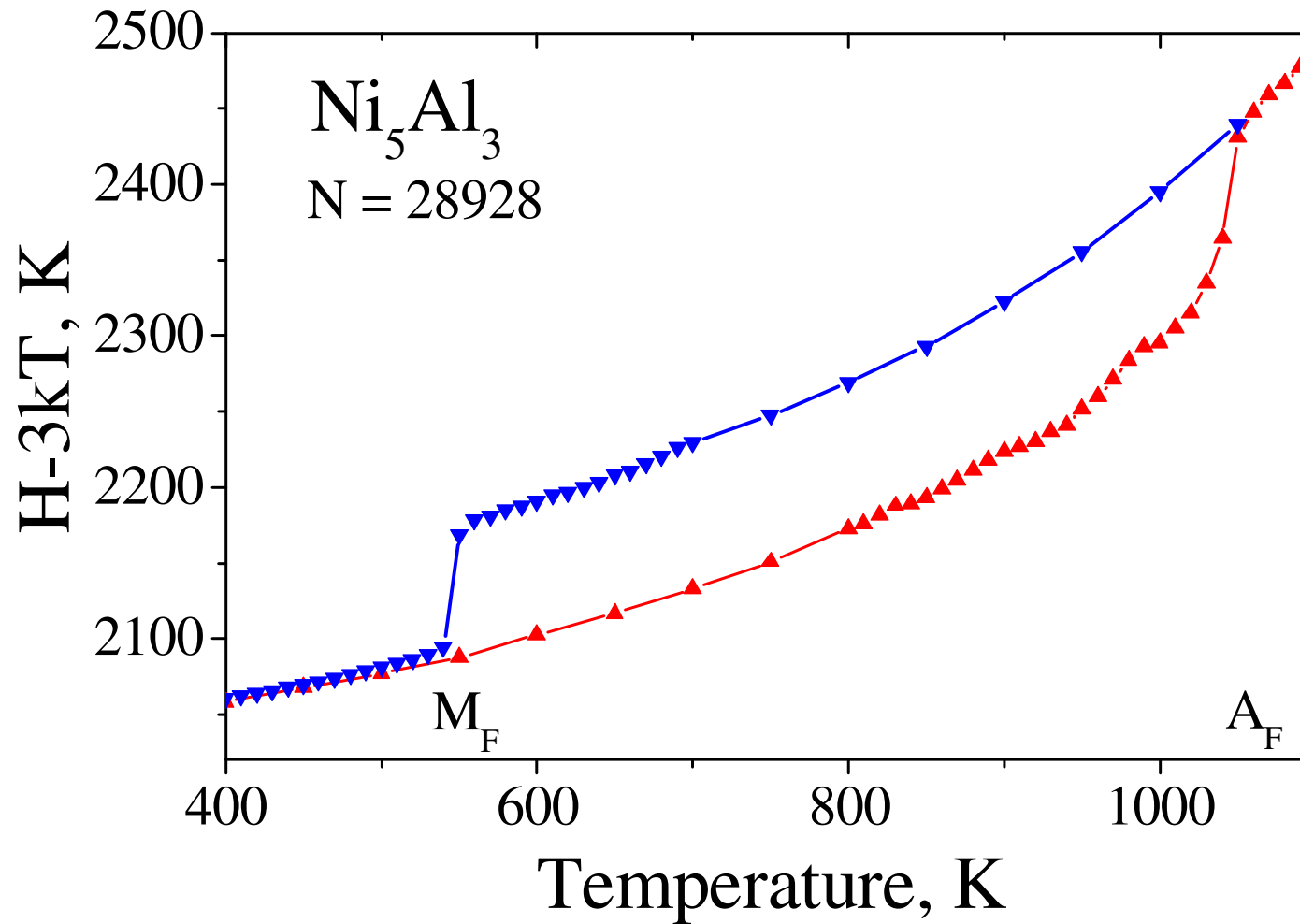
Free external surface



Ni62-Al38



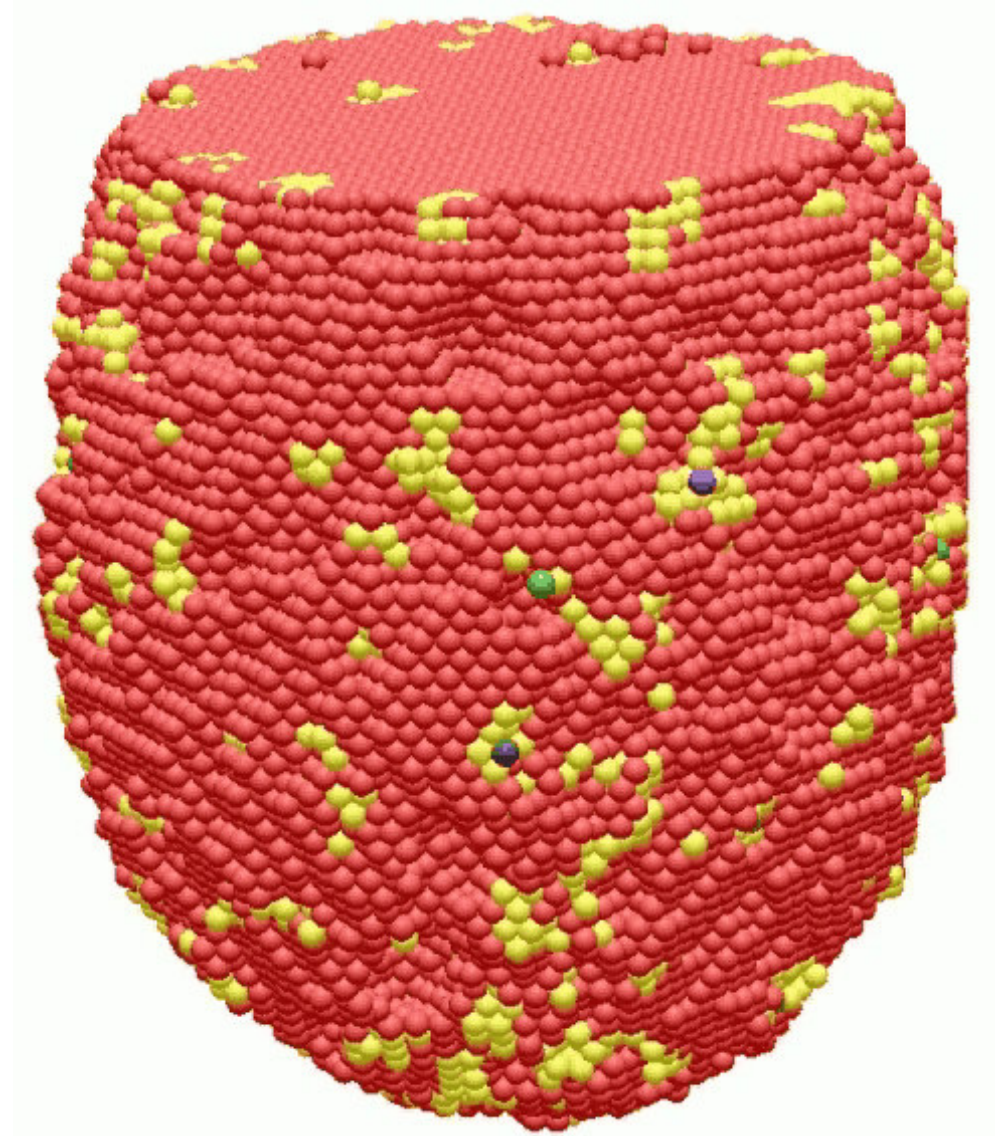
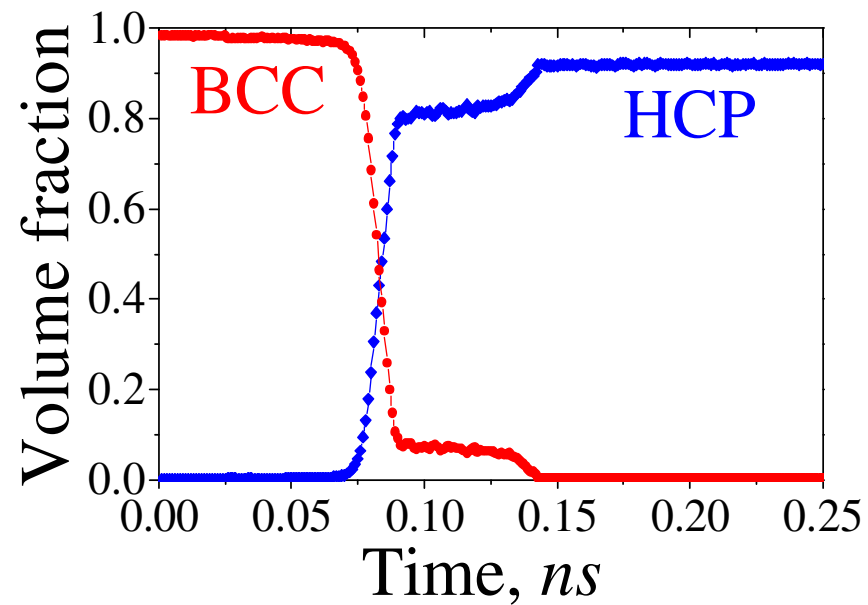
Al-Enriched

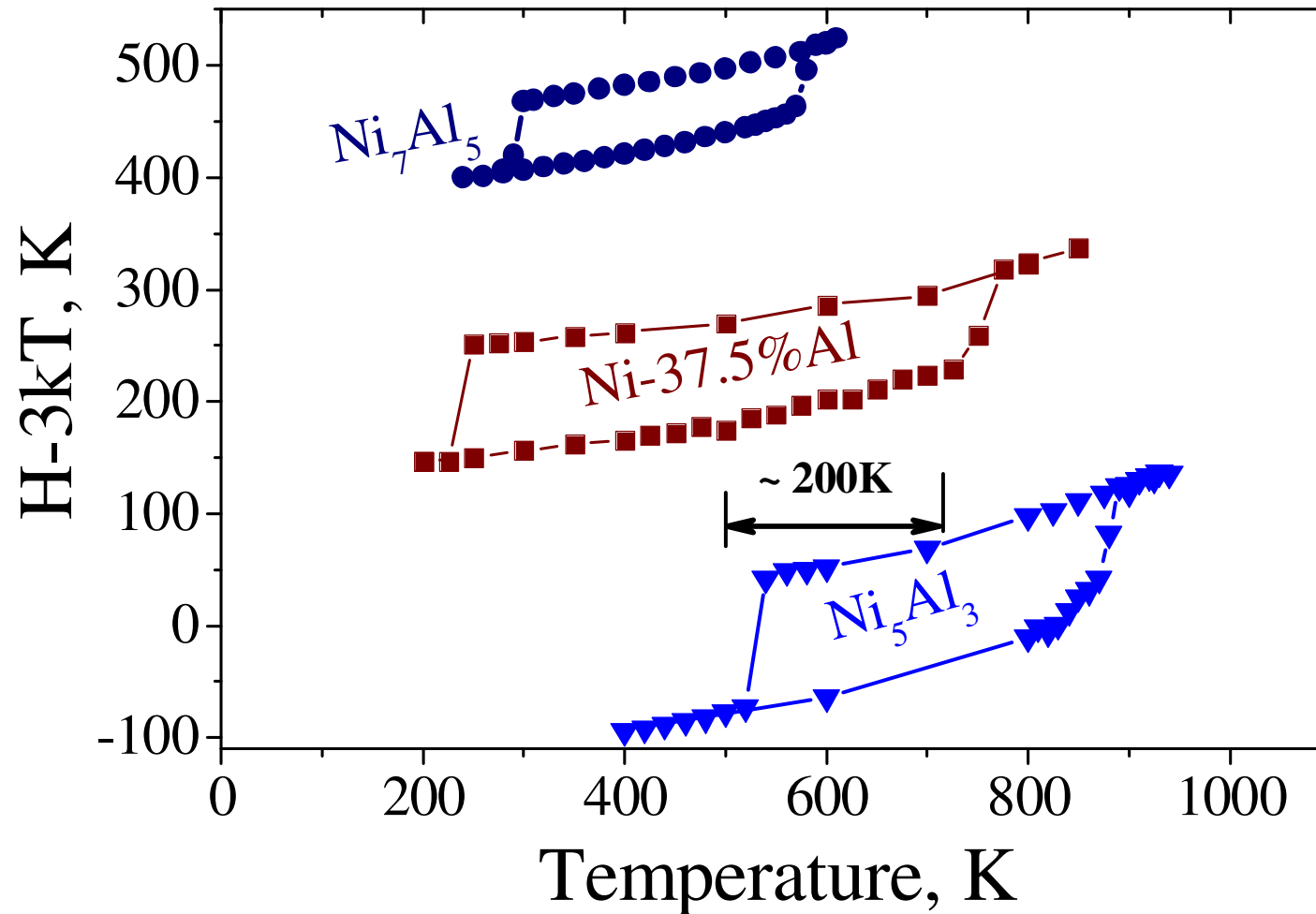
MT in finite-size Ni_5Al_3 : $B \rightarrow A \rightarrow B$ 

Dynamics of transformation $A \rightarrow B$ in Ni_5Al_3

$T = 635\text{K}$

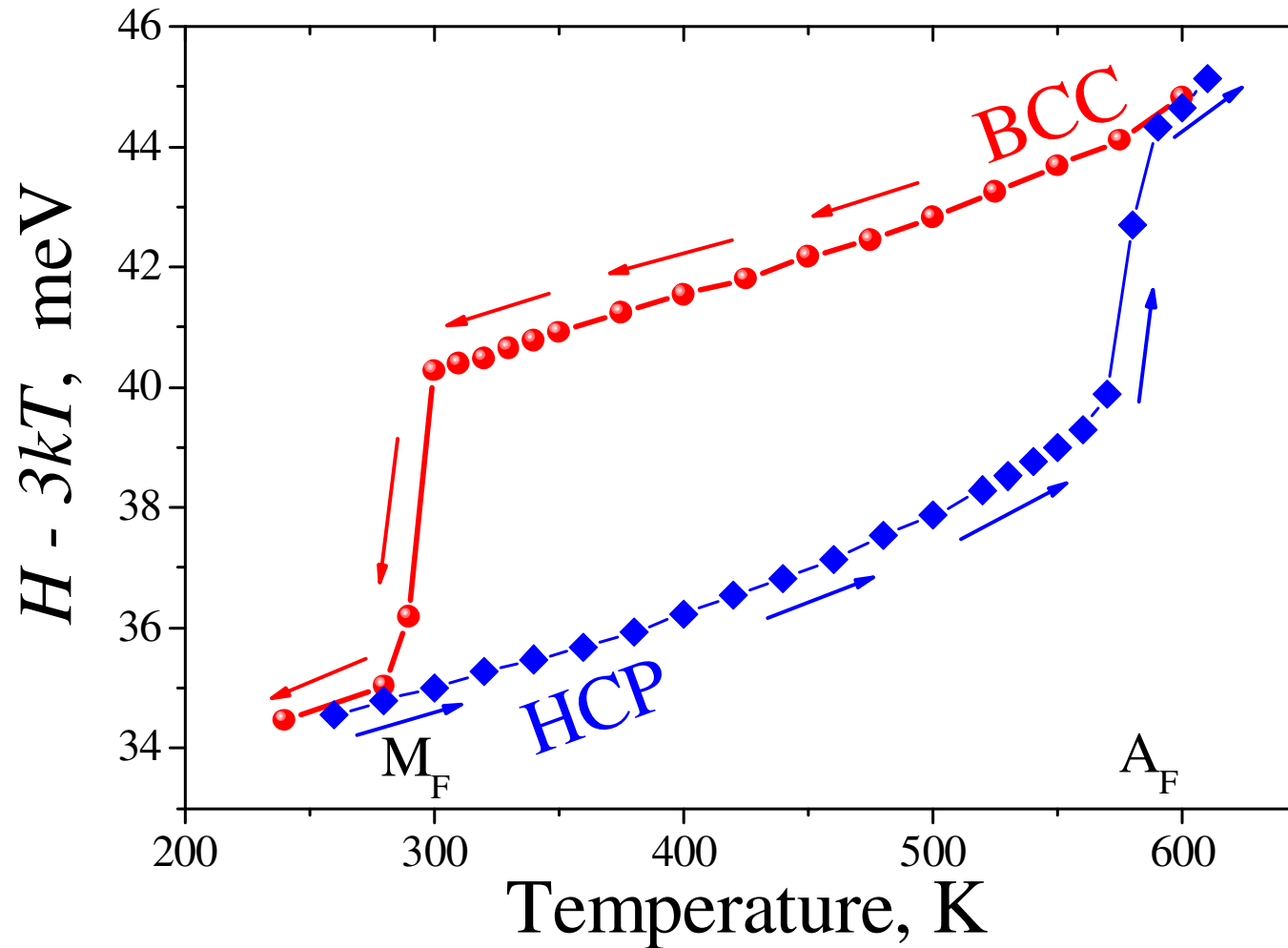
$N = 134048$



MT in finite-size ordered Ni_5Al_3 and Ni_7Al_5 

- *Composition disorder decreases transformation temperature up to $\sim 200\text{K}$*

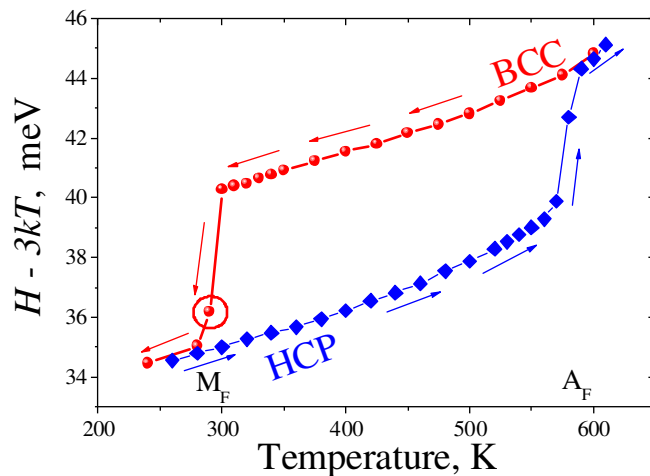
MT in finite-size ordered Ni₇Al₅



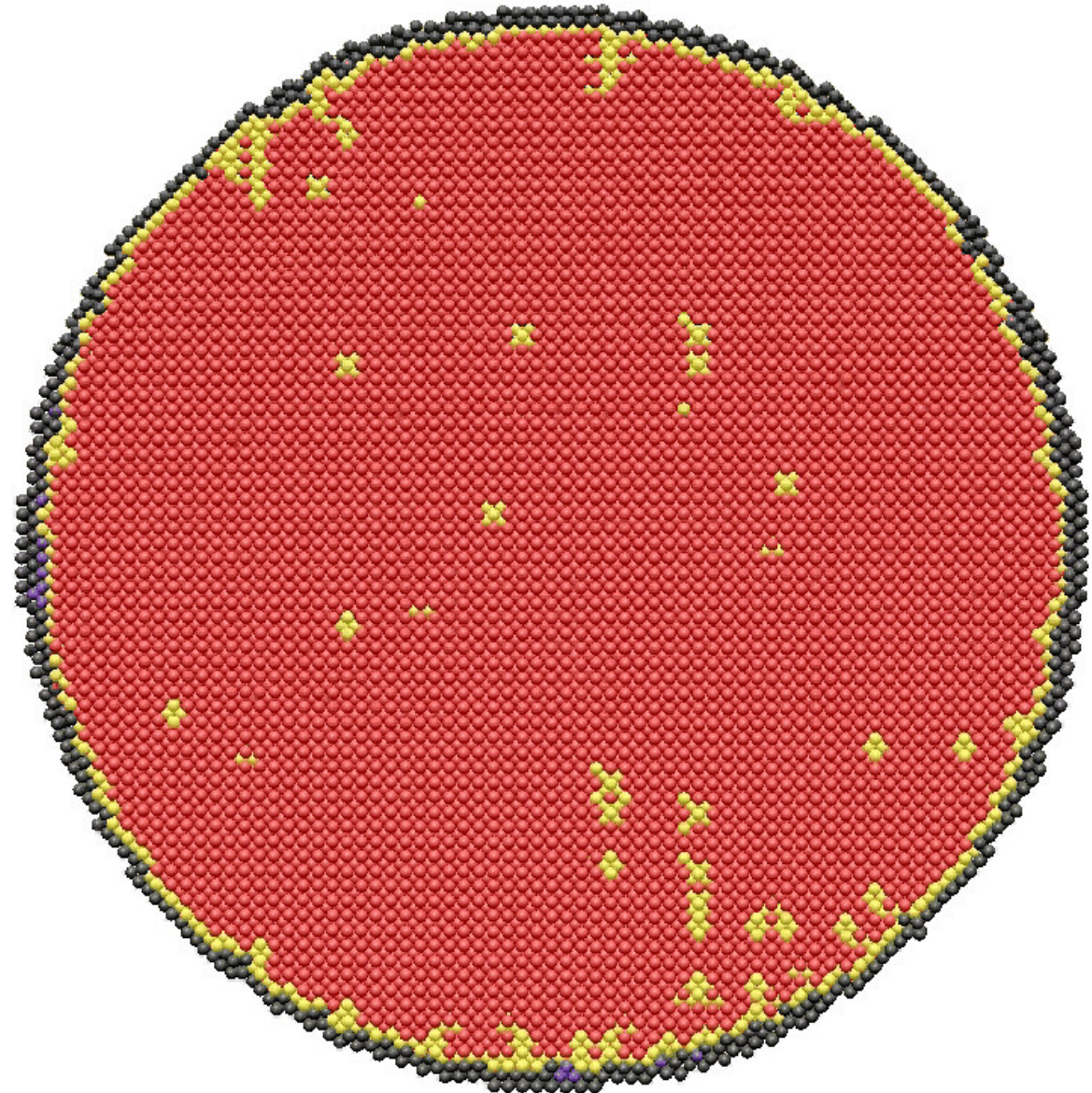
- *The 1-st order phase transformations: $A \rightarrow M \rightarrow A$*

Homogeneous transformation $A \rightarrow M$

Ni_7Al_5
 $T = 290\text{K}, N = 390948$



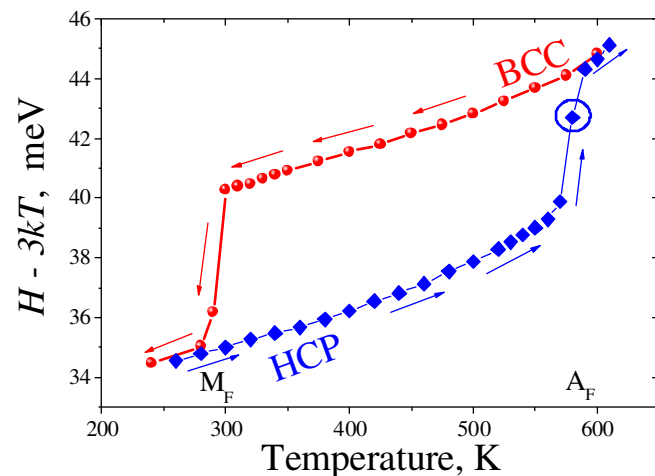
Perfect FCC+HCP
 Distorted FCC+HCP
 Perfect BCC
 Distorted BCC
 Perf. & Dist. ICO
 Unclassified



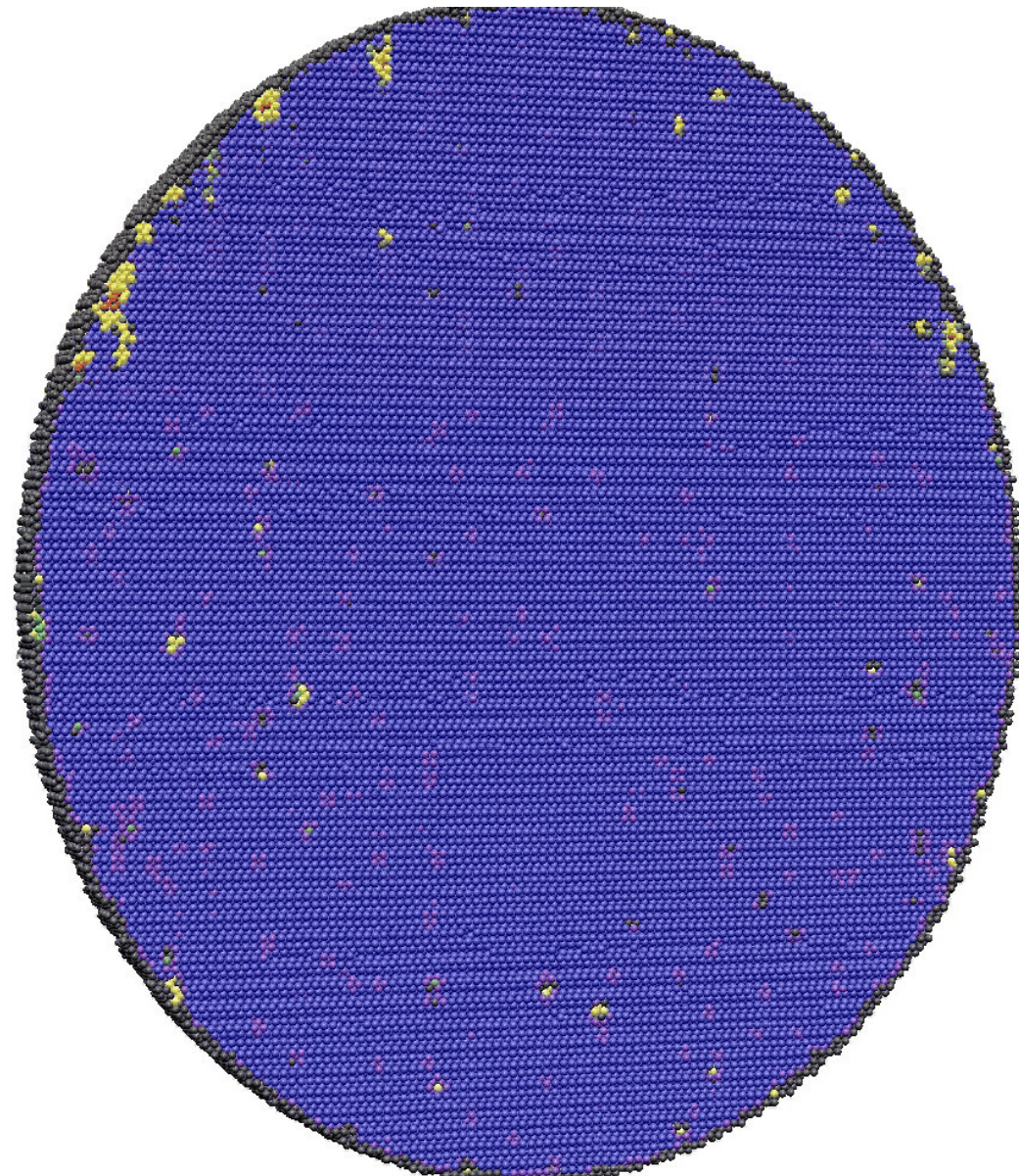
Heterogeneous transformation $M \rightarrow A$



$T = 580\text{K}$, $N = 1809648$

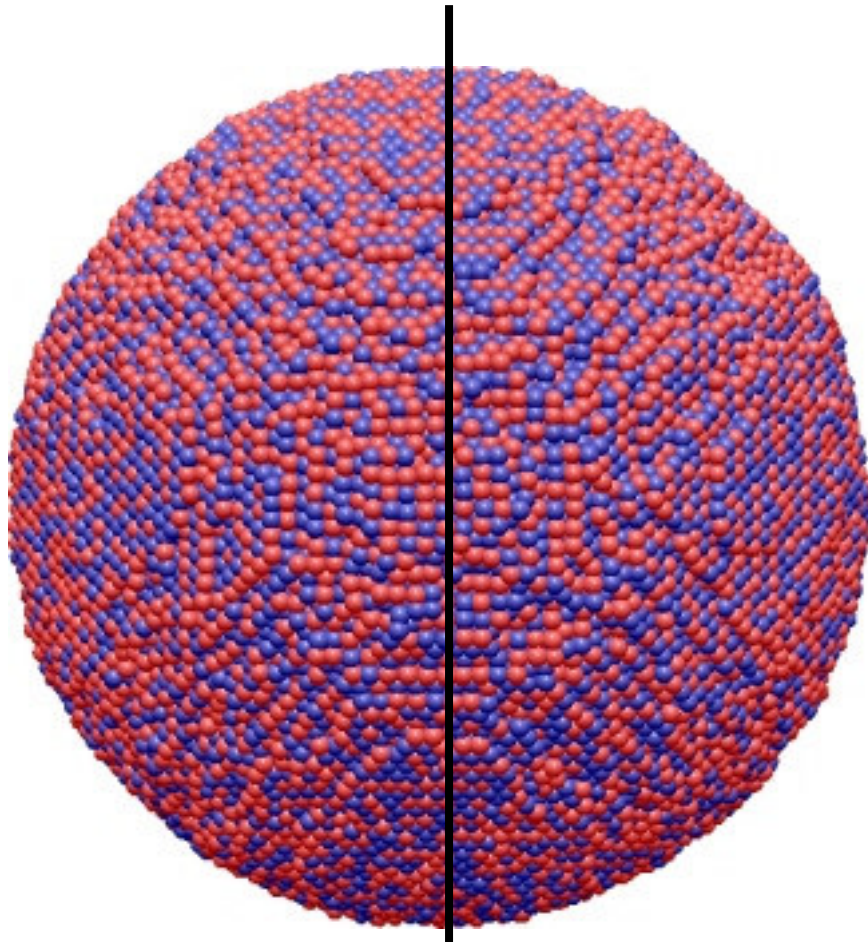


Perfect FCC+HCP
 Distorted FCC+HCP
 Perfect BCC
 Distorted BCC
 Perf. & Dist. ICO
 Unclassified

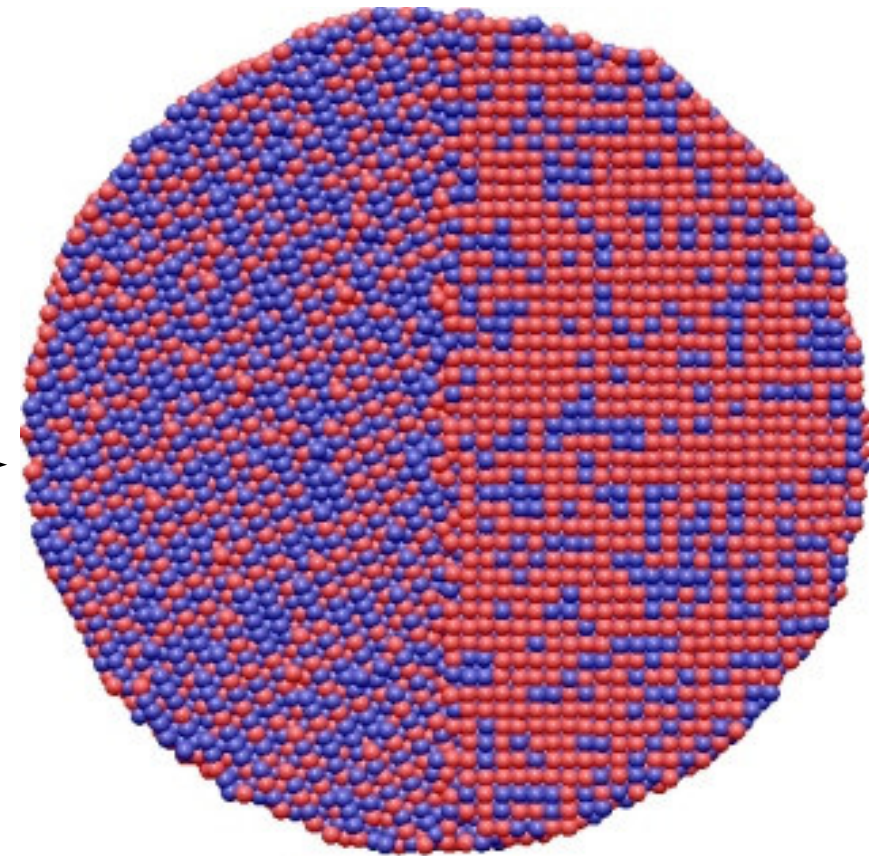


Grain boundary preparation

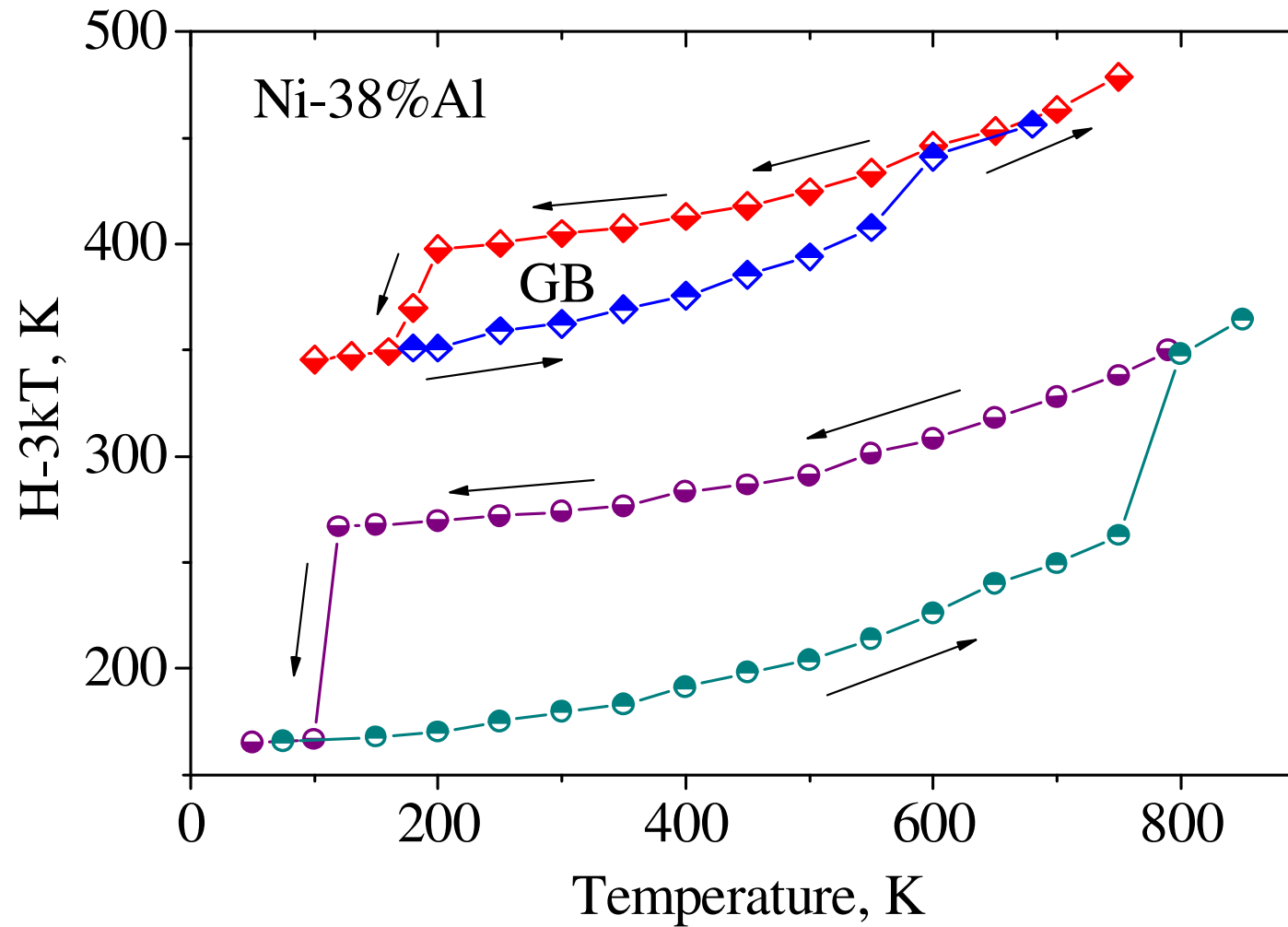
Cutting of init sphere



Cross-section of final state

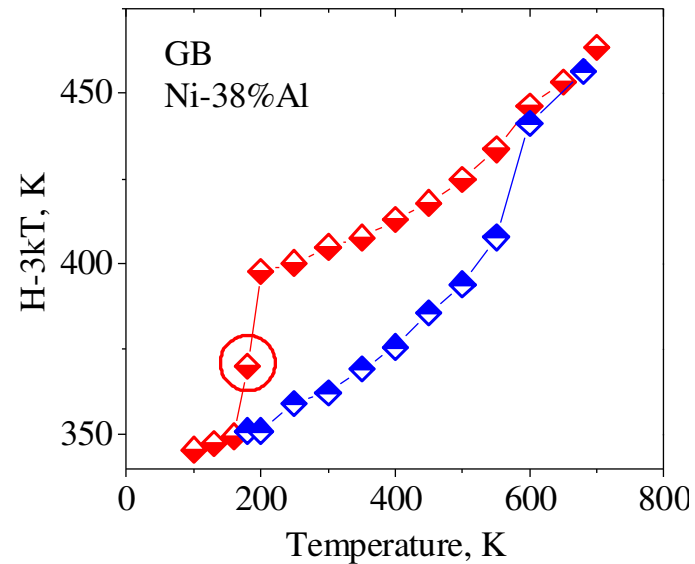


Grain boundary effect

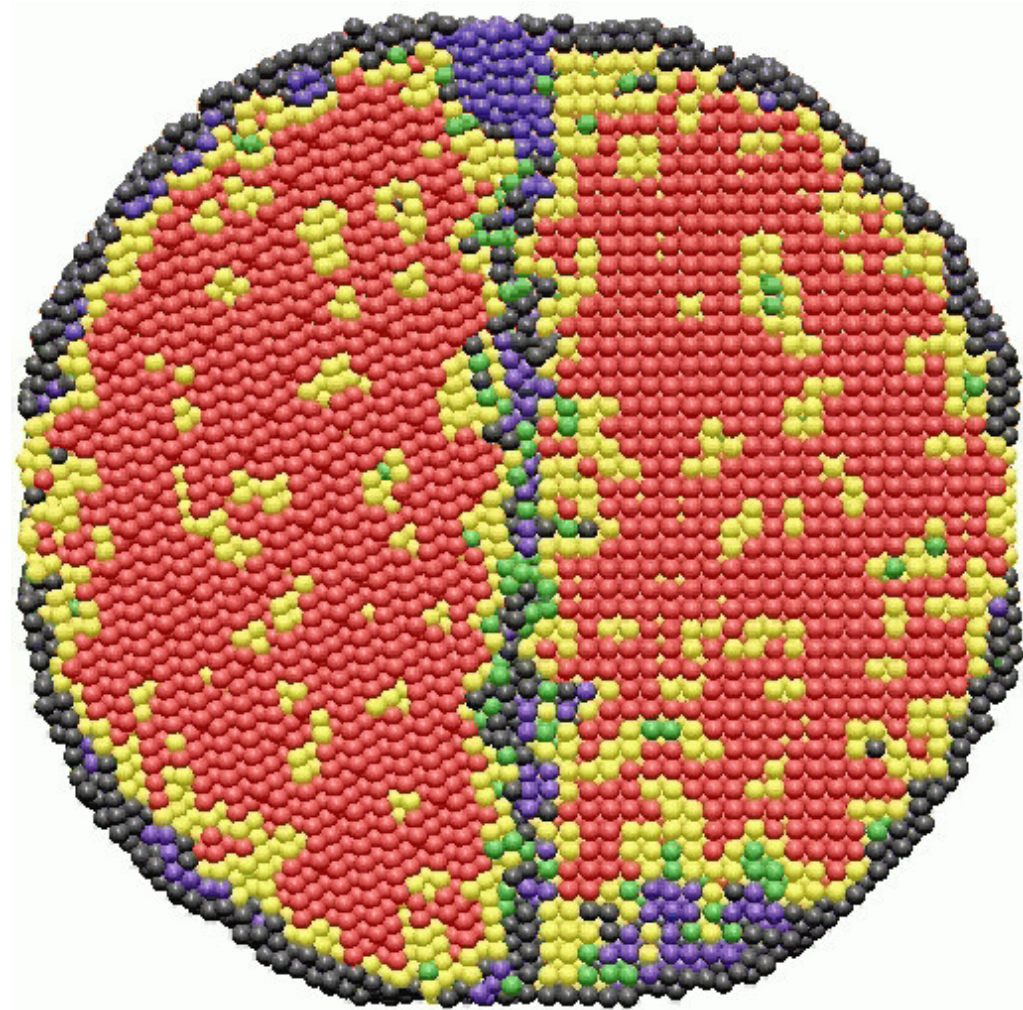


A → M heterogeneous transformation near GB

N = 130995



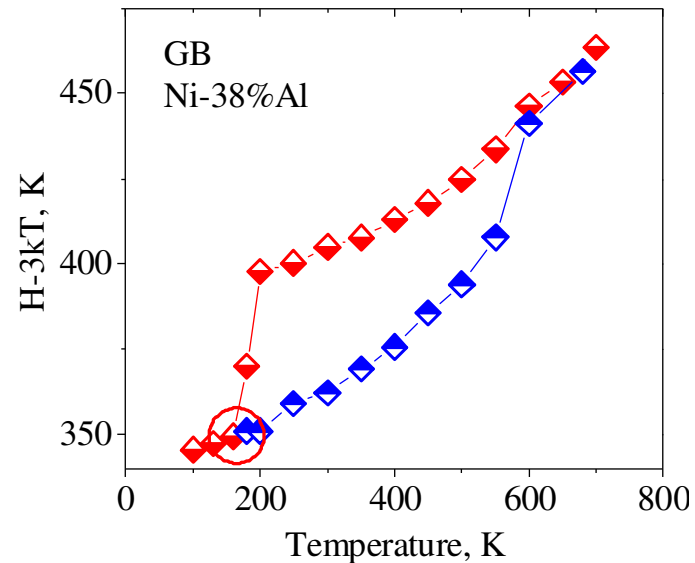
Perfect FCC + HCP
 Distorted FCC + HCP
 Perfect BCC
 Distorted BCC
 Perf. & Dist. ICO
 Unclassified



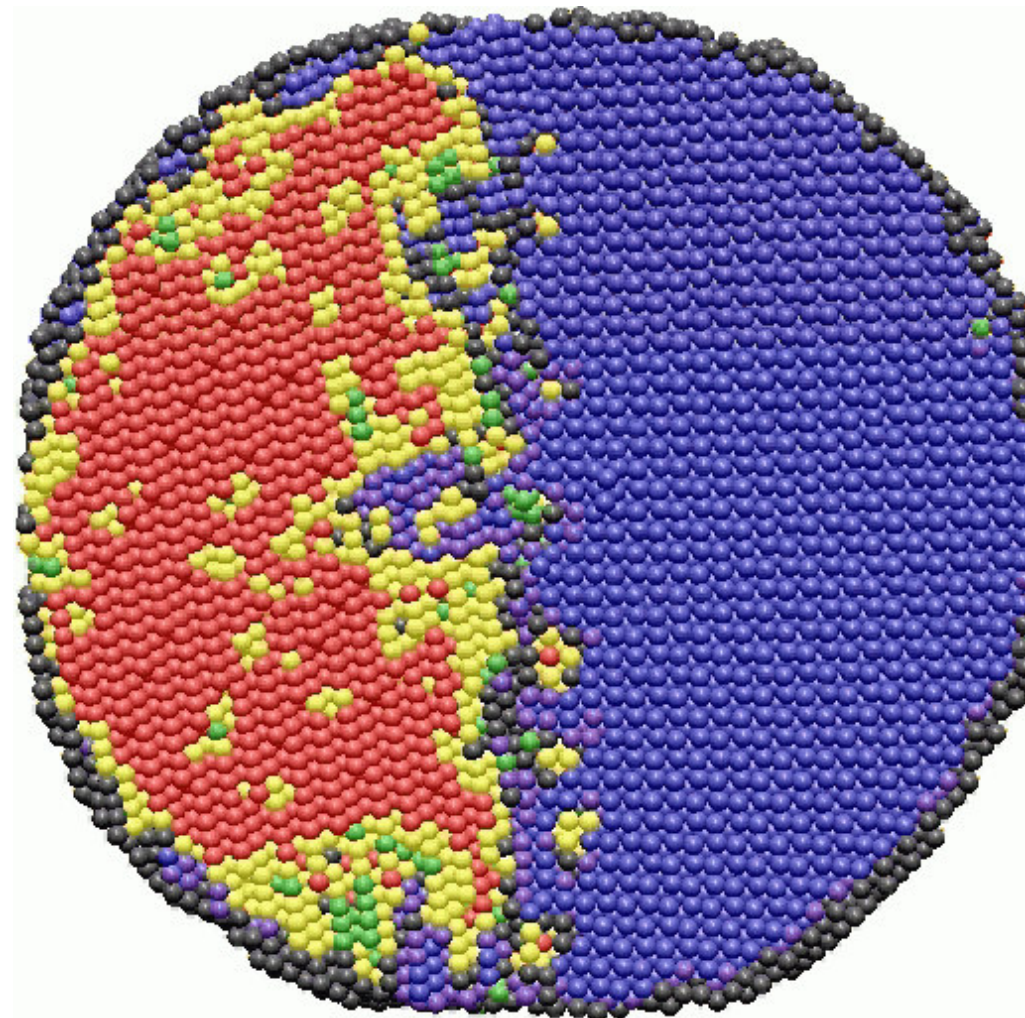
T = 180 K

A \rightarrow M heterogeneous transformation near GB

N = 130995



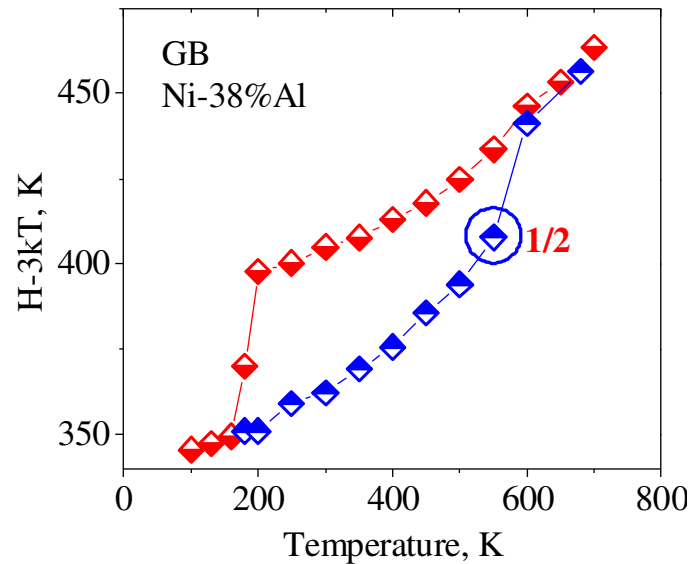
Perfect FCC + HCP
 Distorted FCC + HCP
 Perfect BCC
 Distorted BCC
 Perf. & Dist. ICO
 Unclassified



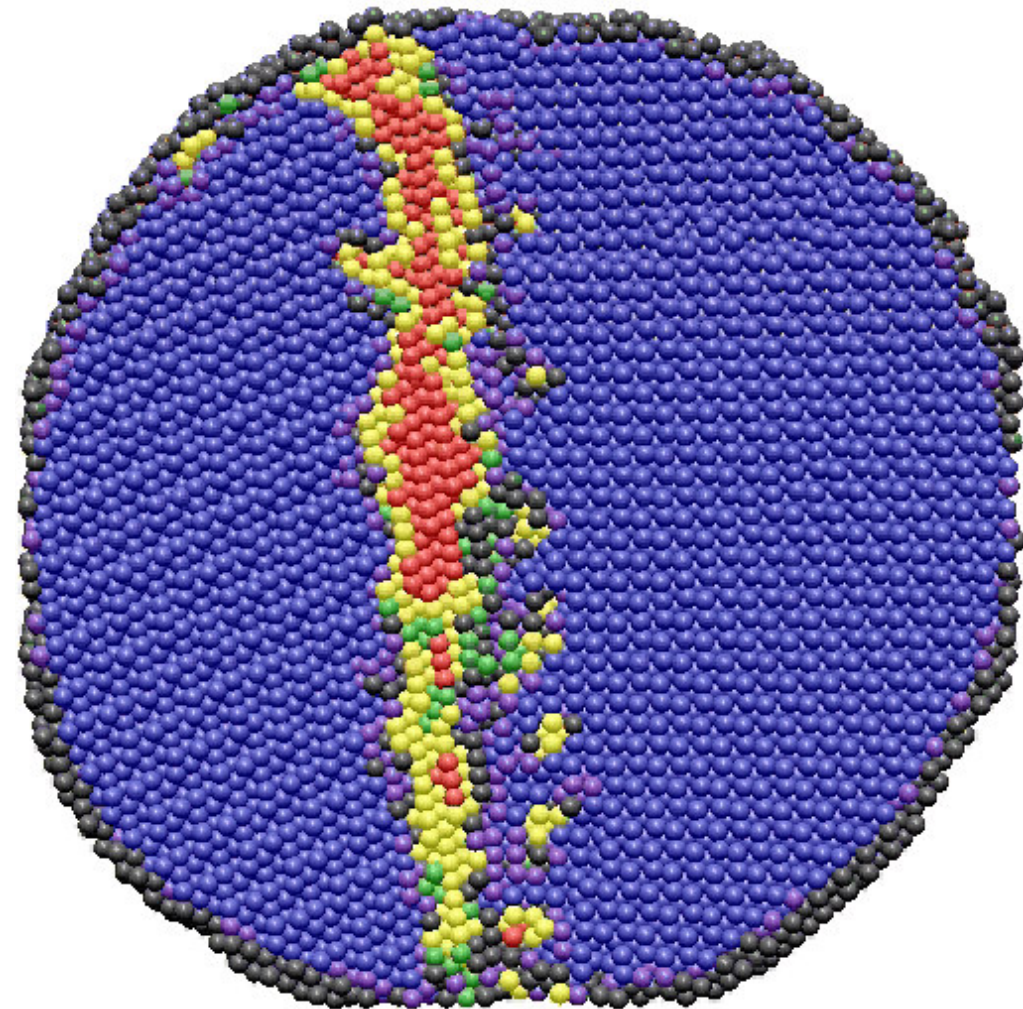
T = 160 K

M → A heterogeneous transformation near GB

N = 130995



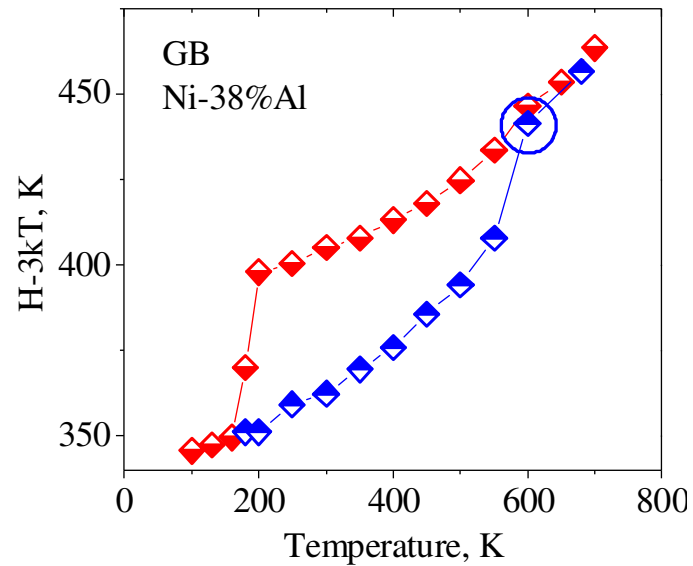
Perfect FCC + HCP
 Distorted FCC + HCP
 Perfect BCC
 Distorted BCC
 Perf. & Dist. ICO
 Unclassified



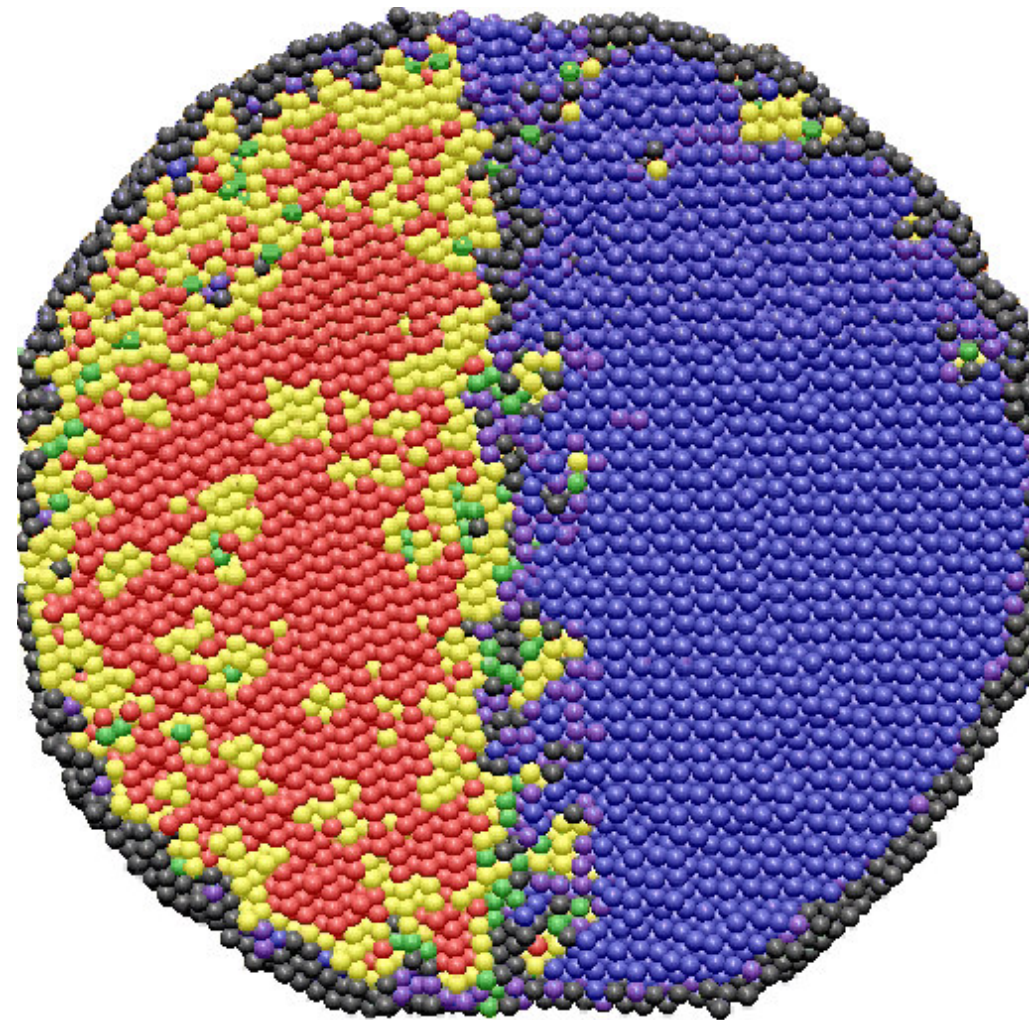
T = 550 K

M → A heterogeneous transformation near GB

N = 130995



Perfect FCC + HCP
 Distorted FCC + HCP
 Perfect BCC
 Distorted BCC
 Perf. & Dist. ICO
 Unclassified



T = 600 K



Atomistic simulation of track

Electronic system: Spike Model

$$C_e(T_e) \frac{\partial T_e}{\partial t} = \frac{1}{r} \frac{\partial}{\partial r} r K_e(T_e) \frac{\partial}{\partial r} T_e - g(T_e - T_a)$$

$$T_e(r, 0) = T_e^0 \exp(-r^2 / 2r_0^2)$$

$$\kappa_e = K_e / C_e$$

$$dE/dx = 25 \text{ keV/nm}, r_0 = 10 \text{ \AA} :$$

$$T_e^0 \sim 10^6 \text{ K}$$

Atomic system: MD

$$m_i \dot{\vec{v}}_i = \vec{F}_i + m_i \gamma \left(\frac{T_e(r)}{T_a(r)} - 1 \right) \vec{v}_i$$

$$T_a(r) = \frac{2}{3k_B N_r} \sum_{r-\delta < r_i < r+\delta} \frac{m_i \vec{v}_i^2}{2}$$

$$\frac{dT_a}{dt} = 2\gamma(T_e - T_a)$$

Simulation setup A

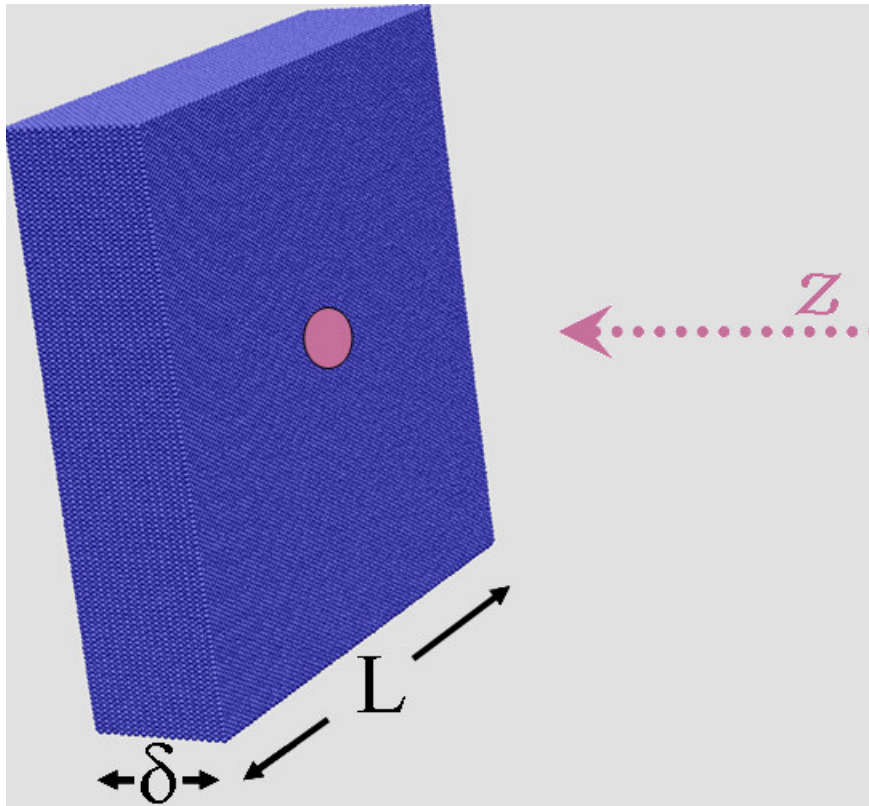
Ni-40%Al

$\delta = 7-10 \text{ nm}$

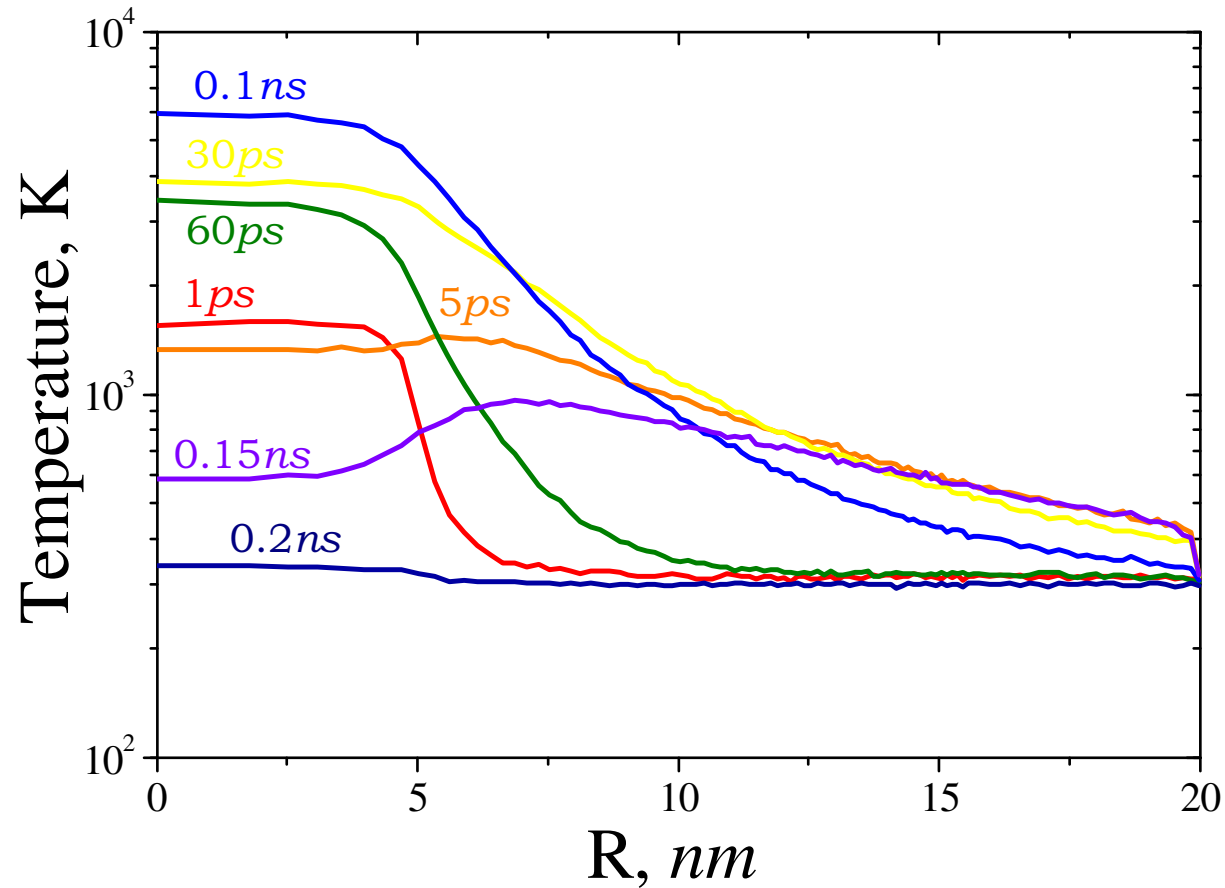
$L = 30-40 \text{ nm}$

$N = (0.6-1.4) \cdot 10^6$

$T = 300 \text{ K}$



Temperature development around track



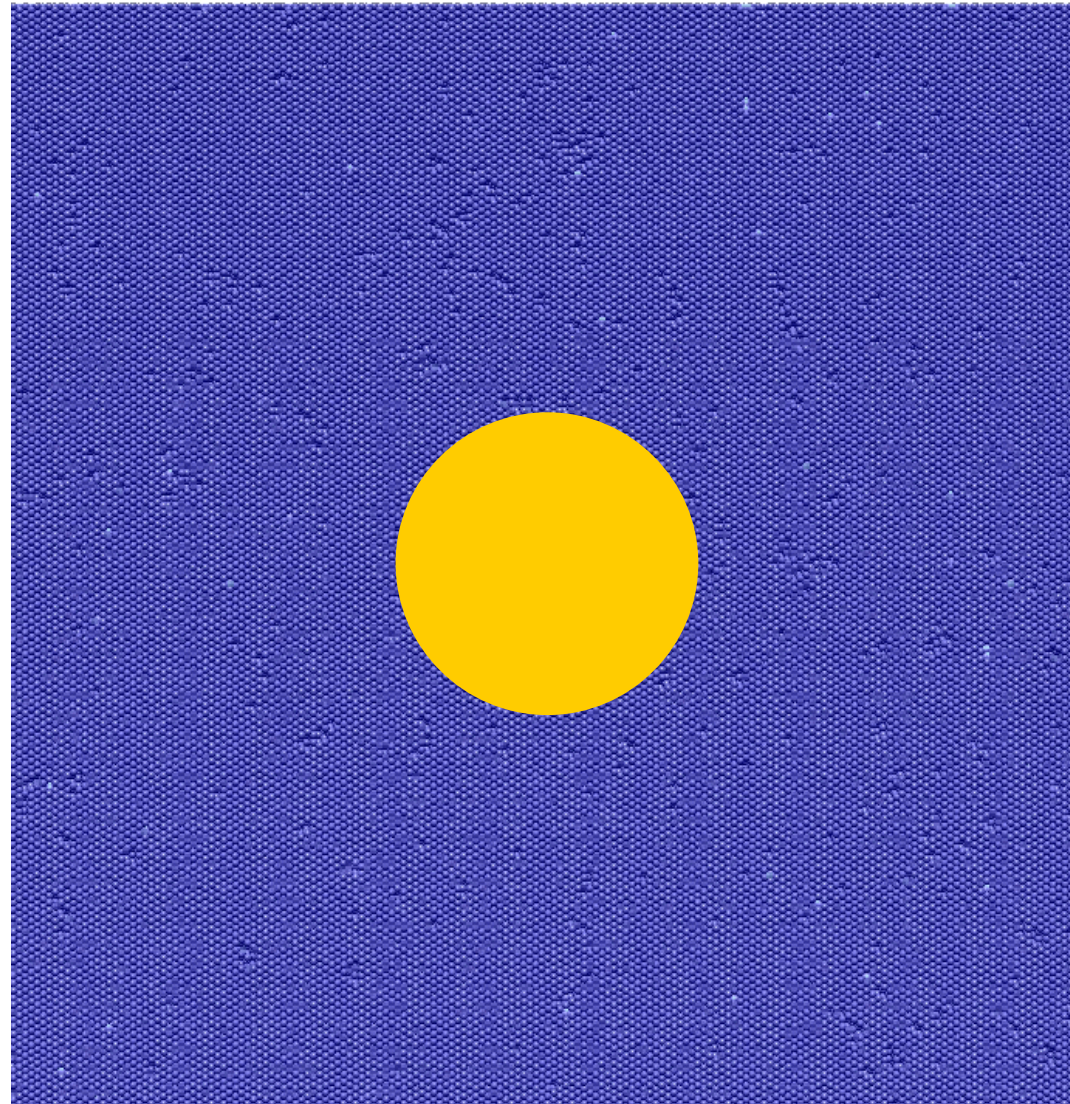
Phases Development in the Range of Swift Ion track

Ni - 40%Al

$N = 1\,400\,000$

$T = 300\text{ K}$

Perfect FCC + HCP
Distorted FCC + HCP
Perfect BCC
Distorted BCC
Perf. & Dist. ICO
Compositionally
Disordered
Unclassified



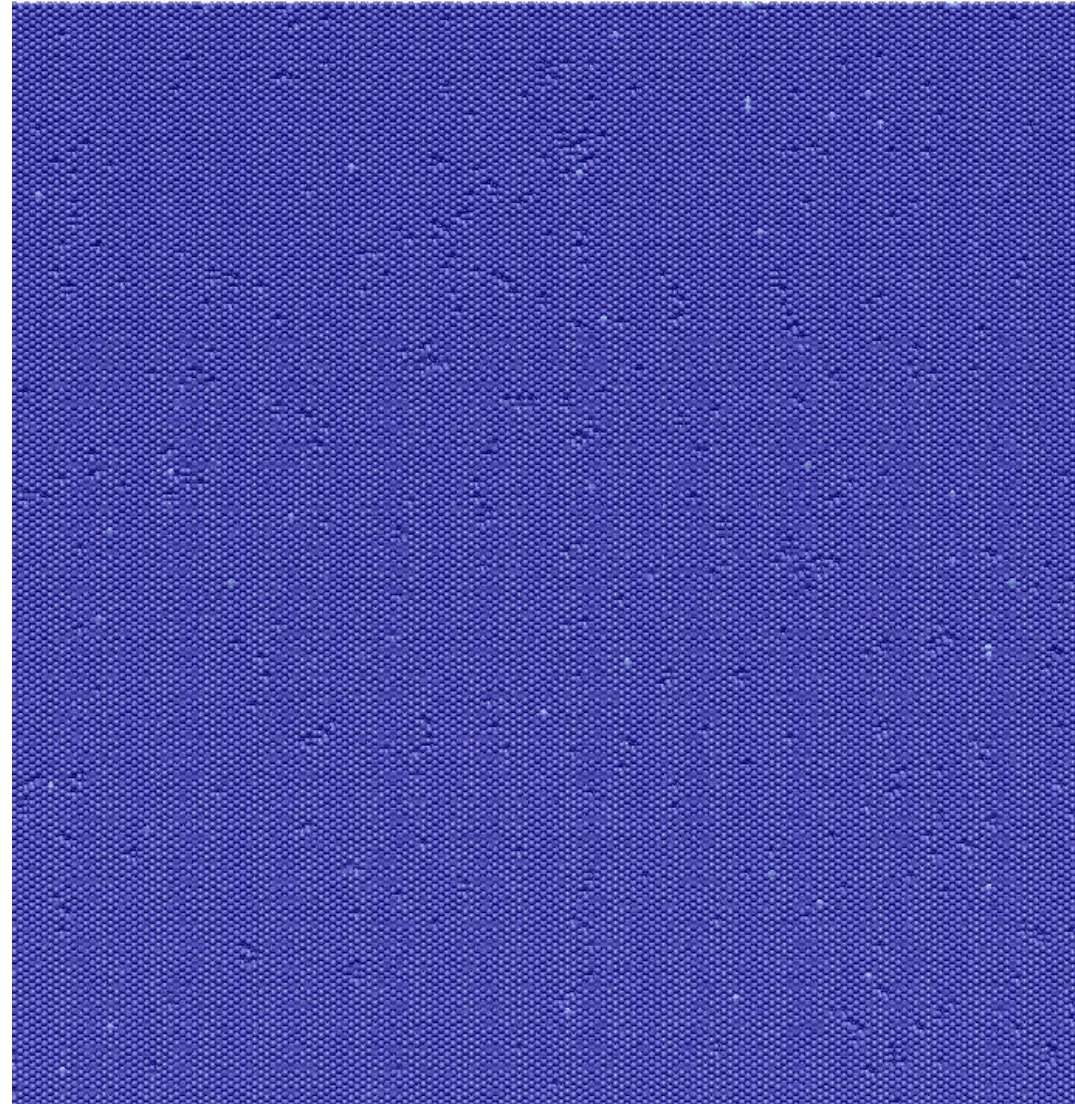
Phases Development in the Range of Swift Ion track

Ni - 40%Al

$N = 1\,400\,000$

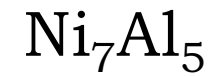
$T = 300\text{ K}$

Perfect FCC + HCP
Distorted FCC + HCP
Perfect BCC
Distorted BCC
Perf. & Dist. ICO
Compositionally
Disordered
Unclassified



Melting, Martensitic Transformations, Order-Disorder

Simulation setup B

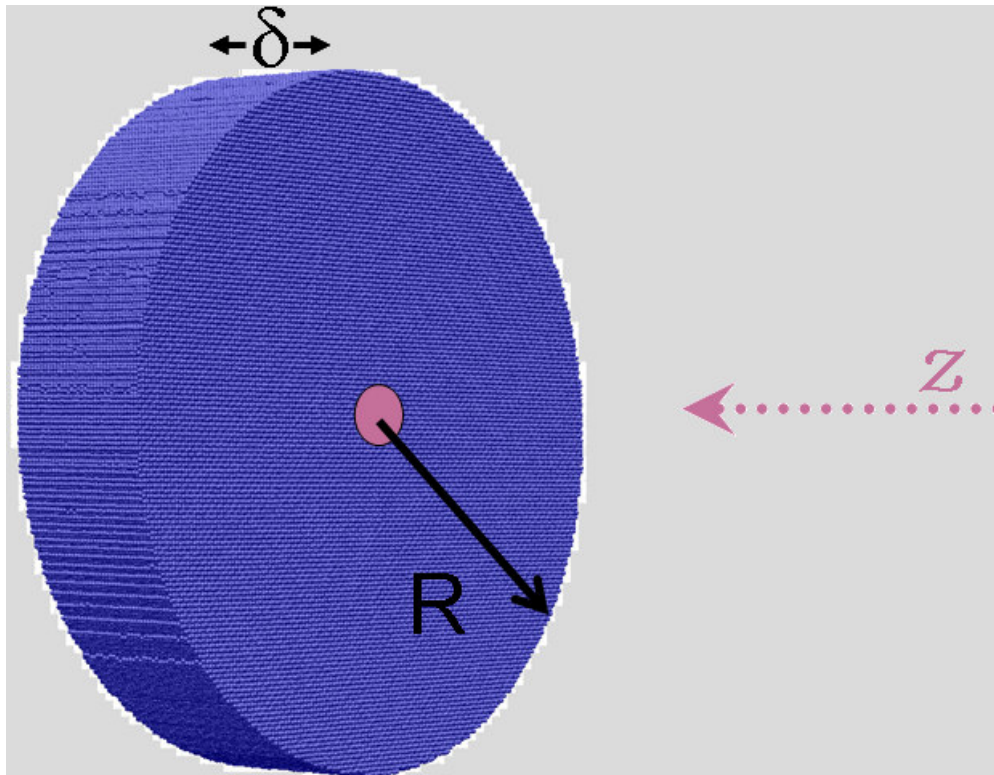


$$\delta = 10 \text{ nm}$$

$$R = 22\text{-}44 \text{ nm}$$

$$N = (1\text{-}5) \cdot 10^6$$

$$T = 300\text{-}400 \text{ K}$$



Development of Swift Ion Track

Ni_7Al_5

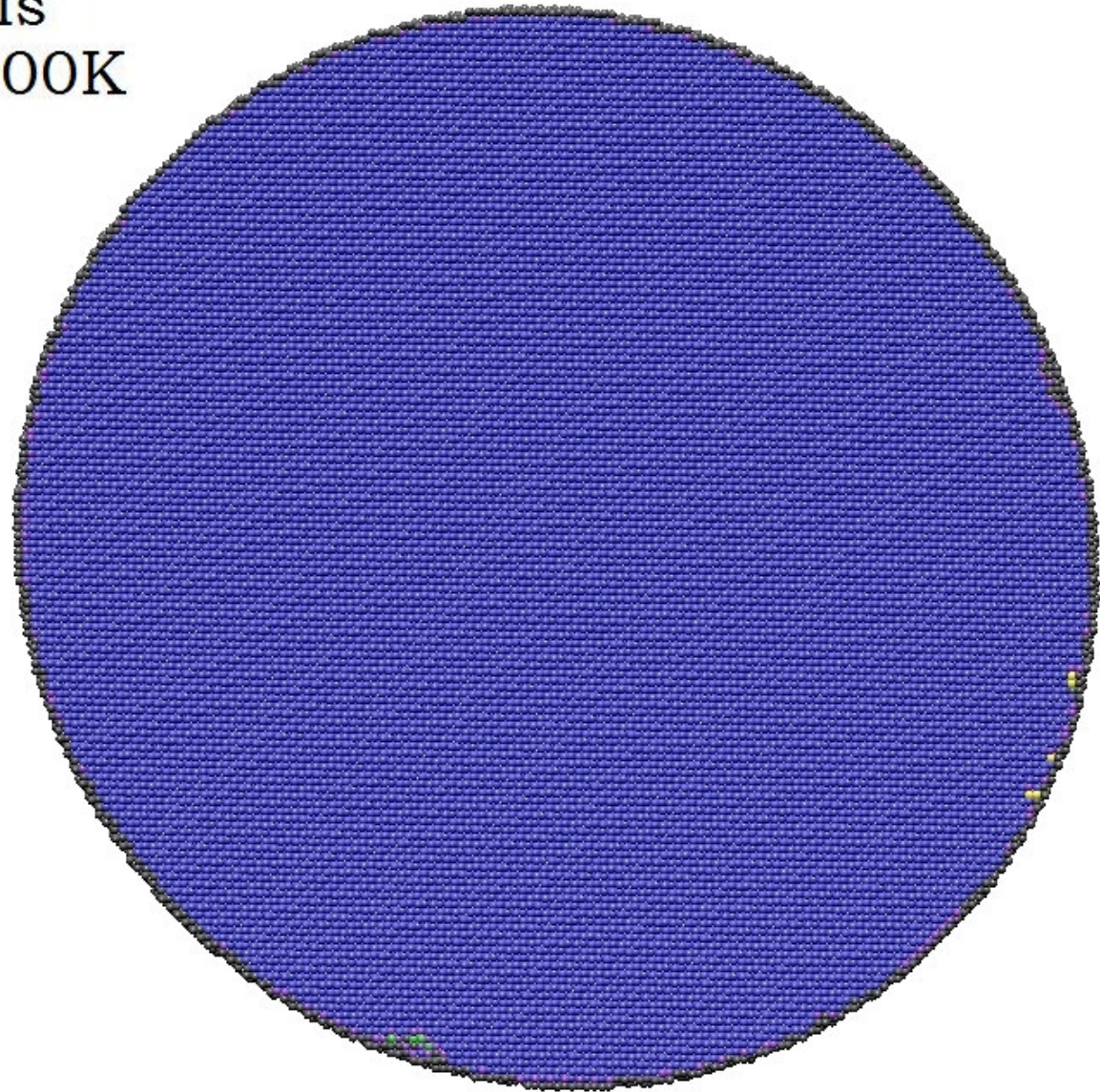
8fs
1300K

$N = 1\,200\,000$

$T = 300\text{ K}$

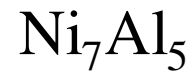
$k_e = 10\text{ A}^2/\text{fs}$

Perfect FCC + HCP
Distorted FCC + HCP
Perfect BCC
Distorted BCC
Perf. & Dist. ICO
Compositionally
Disordered
Unclassified





Development of Swift Ion Track



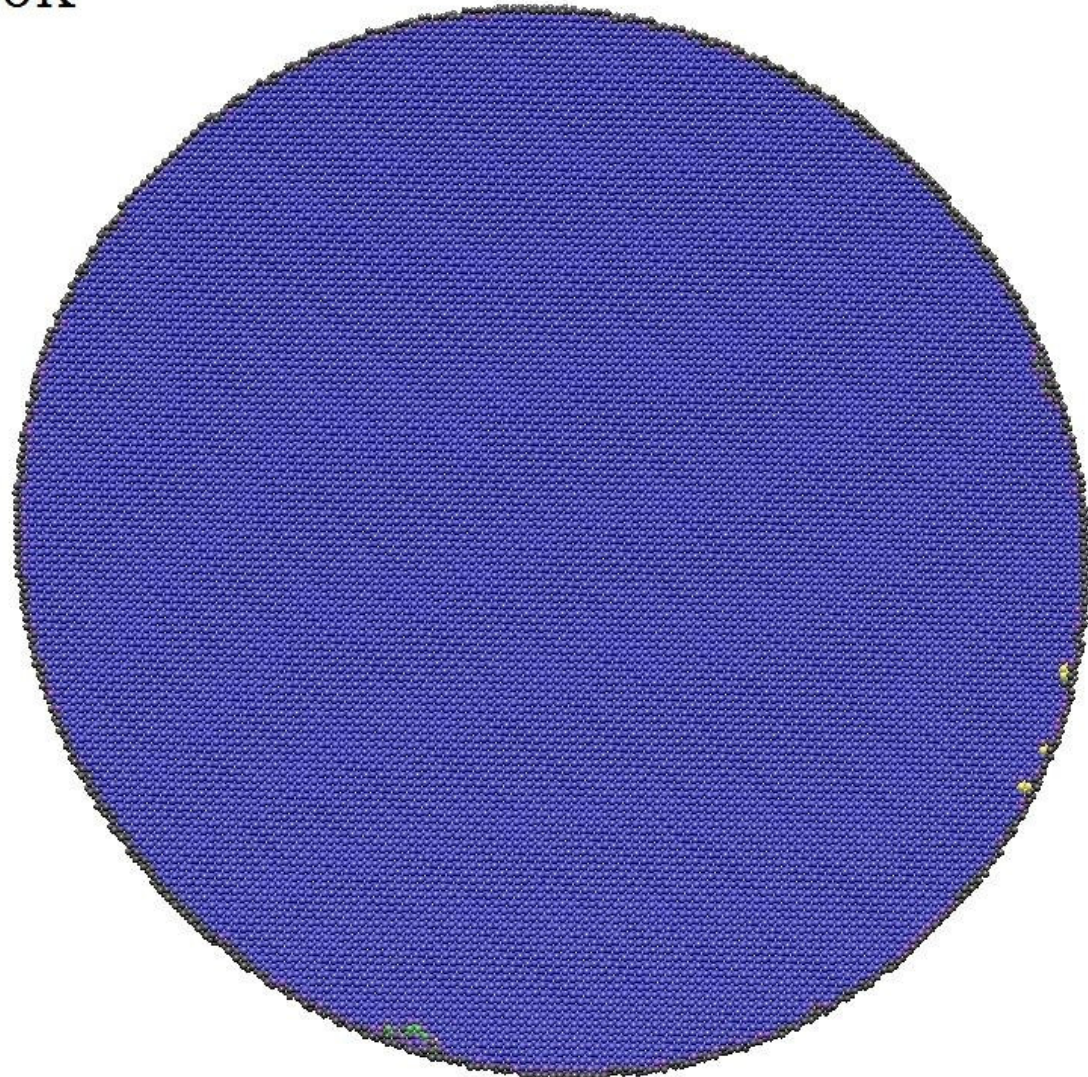
8fs
1400K

$$N = 1\,200\,000$$

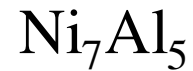
$$T = 300\text{ K}$$

$$k_e = 5\text{ A}^2/\text{fs}$$

Perfect FCC + HCP
Distorted FCC + HCP
Perfect BCC
Distorted BCC
Perf. & Dist. ICO
Compositionally
Disordered
Unclassified



Development of Swift Ion Track

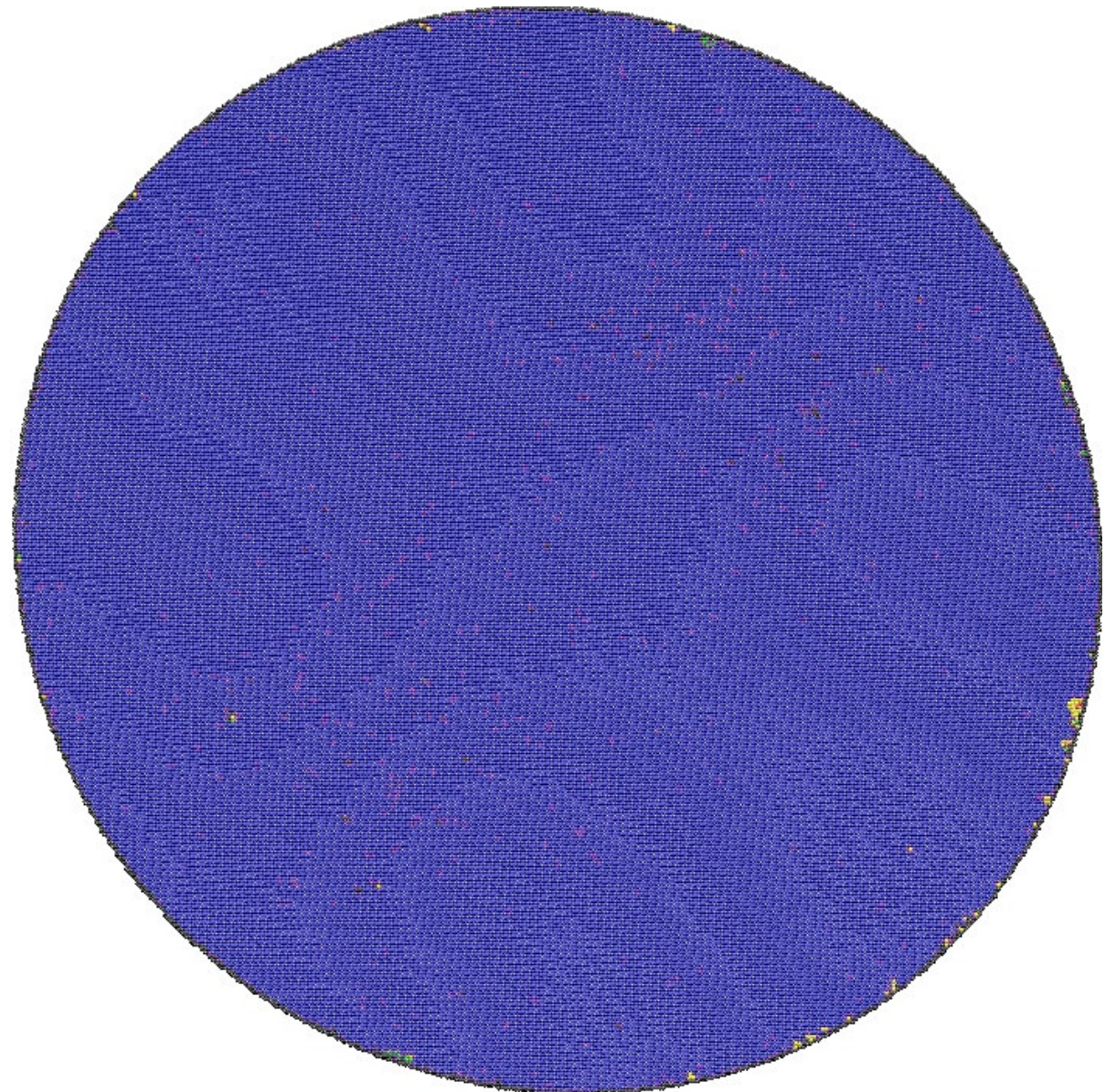


$$N = 4\,900\,000$$

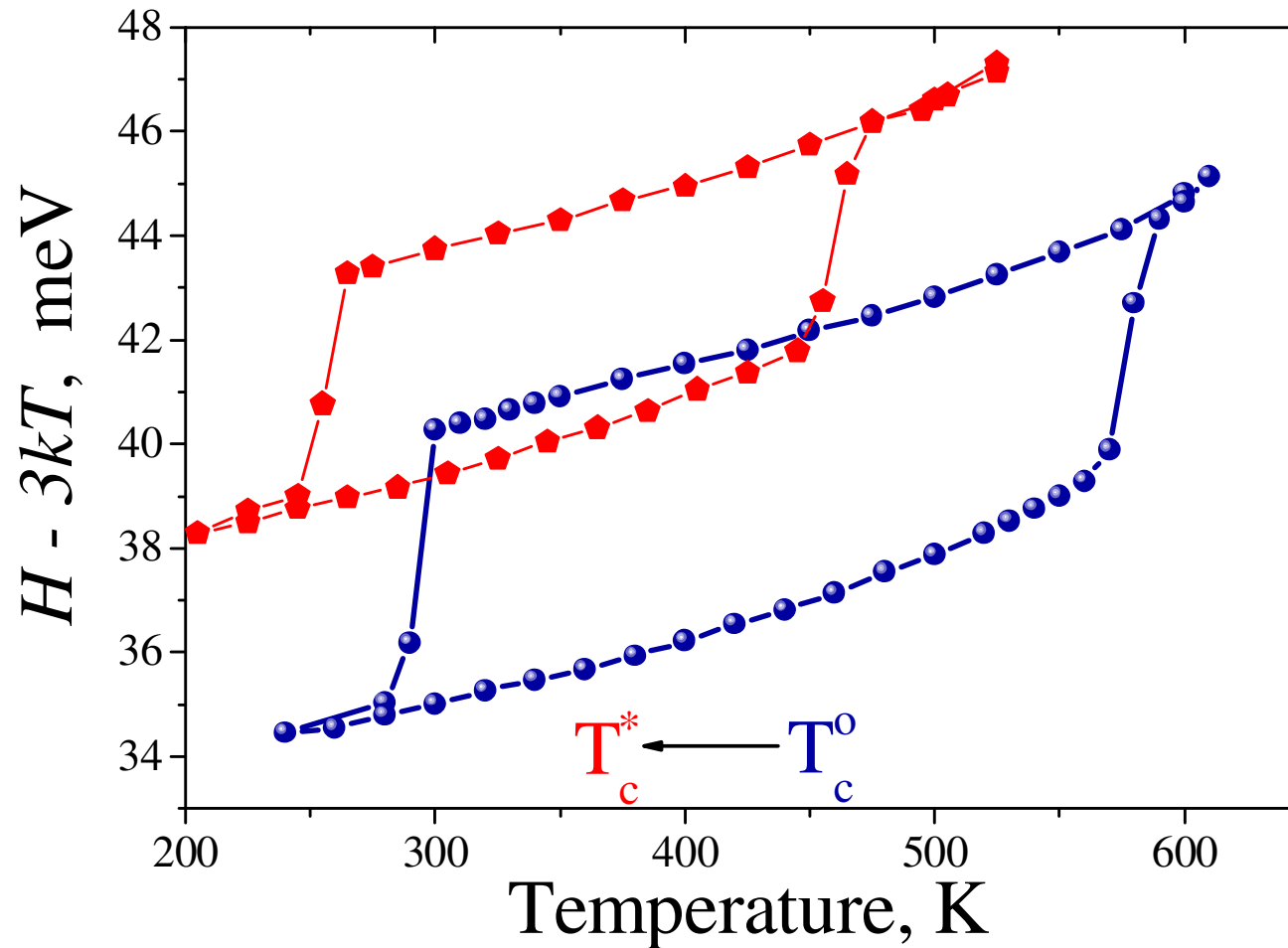
$$T_0 = 400\text{ K}$$

$$k_e = 10\text{ A}^2/\text{fs}$$

Perfect FCC + HCP
Distorted FCC + HCP
Perfect BCC
Distorted BCC
Perf. & Dist. ICO
Compositionally
Disordered
Unclassified



Compositional disordering favours austenitic phase



- *Shift of T_c*



Conclusions

- The reversibility of both temperature- and stress-controlled MTs was observed at MD simulation of model NiAl alloy
- Stress-controlled MPTs have features of shape memory effect
- External surface and GG affect the behavior of MTs indicating heterogeneous nucleation of new phase on extended defects
- Compositional disordering is the dominant cause of track formation in ordered NiAl alloy