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**The k0-Method of Instrumental Neutron Activation Analysis
Irradiation Facility Characterization**

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The k_0 -method of Instrumental Neutron activation analysis

Irradiation facility characterization

Overview

- What we want to do in the end
- Standardization methods
- How to implement the k_0 -method
 - Gamma-ray spectrometry
 - Detector characterization (Monday afternoon)
 - Coincidence-summing based detector calibration
 - Advanced topic I (Tuesday morning)
 - Advanced topic II (Tuesday morning)
 - Irradiation facility characterization (Tuesday afternoon)
- The interpretation step

What we want to do in the end

- The measure peak area a is linearly proportional to the elemental concentration c . The proportionality constant is m .
- c is what we want to know, a is what we measure, m is what we get from the calibration and/or standardization process.
- So we want to determine m first, and then analyze samples
- m is the peak area that would be measured if the elemental concentration was 1 kg/kg

$$a = mc$$

How to calculate m

$$m = \frac{w\theta N_{avogadro}}{M} R \frac{(1 - e^{-\lambda t_{ir}})}{\lambda} e^{-\lambda t_d} (1 - e^{-\lambda t_m}) P$$

where w is the sample mass, θ the isotopic abundance, M the molar mass of the element, λ the decay constant, R the activation rate, and t_{ir} , t_d and t_m the irradiation, decay and measurement durations. P is the probability per disintegration of obtaining a count in the full-energy peak.

(This equation is only valid for the simplest activation case)

How to calculate R and P

- The activation rate R is calculated from the neutron spectrum shape parameters (Φ_s , Φ_e , α , T) and the capture cross-section parameters (σ , I_0 , E_r , $g(T)$).
- The detection probability P is calculated from the detector's **efficiency curves (full-energy and peak-to-total)**, the counting geometry and the decay scheme of the radionuclide.

Principles of the k_0 method

First conventional approach: adapted Høgdahl

$$\begin{aligned} R &= \int_0^{v_{Cd}} \sigma(v) \Phi(v) dv + \int_{v_{Cd}}^{\infty} \sigma(v) \Phi(v) dv \approx \\ &\int_0^{v_{Cd}} \frac{\sigma_0 v_0}{v} \Phi(v) dv + \int_{E_{Cd}}^{\infty} \sigma(E) \Phi(E) dE \approx \\ &\int_0^{v_{Cd}} \sigma_0 v_0 n(v) dv + \int_{E_{Cd}}^{\infty} \sigma(E) \frac{\Phi(E_{ref})}{\left(\frac{E}{E_{ref}}\right)^{1+\alpha}} dE = \\ &\sigma_0 \Phi_s + I_0(\alpha) \Phi_e = \sigma_0 \Phi_s \left(1 + \frac{Q_0(\alpha)}{f}\right) \end{aligned}$$

Principles of the k_0 method

First conventional approach: adapted Høgdahl

$$I_0(\alpha) \equiv \int_{E_{Cd}}^{\infty} \sigma(E) \frac{E_{ref}^{\alpha}}{E^{1+\alpha}} dE$$

$$\Phi_e \equiv \Phi(E_{ref}) E_{ref}$$

$$I_0(\alpha) = E_{ref}^{\alpha} \left\{ \frac{I_0(0) - 0.429\sigma_0}{\bar{E}_r^{\alpha}} + \frac{0.429\sigma_0}{(2\alpha + 1)E_{Cd}^{\alpha}} \right\}$$

$$f = \frac{\Phi_s}{\Phi_e}$$

Principles of the k_0 method

Second conventional approach: Westcott

Takes non $1/v$ (n,γ) reactions into account using $g(T)$.

Principles of the k_0 -IAEA software

Adapted² Høgdahl conventional approach: Blaauw

$$\begin{aligned} R &= \int_0^{\infty} \frac{\sigma_0 v_0}{v} \Phi(v) dv + \int_0^{\infty} \left\{ \sigma(v) - \frac{\sigma_0 v_0}{v} \right\} \Phi(v) dv \\ &\approx \int_0^{\infty} \sigma_0 v_0 n(v) dv + \int_0^{\infty} \left\{ \sigma(E) - \frac{\sigma_0 v_0}{v} \right\} \frac{\Phi(E_{ref})}{\left(\frac{E}{E_{ref}} \right)^{1+\alpha}} dE \\ &= \sigma_0 \Phi_t + I_0^*(\alpha) \Phi_e \\ &= \sigma_0 \Phi_t \left(1 + \frac{Q_0^*(\alpha)}{f^*} \right) \end{aligned}$$

Principles of the k_0 -IAEA software

Adapted² Høgdahl conventional approach: Blaauw

$$I_0^*(\alpha) \equiv \int_0^{\infty} \left\{ \sigma(E) - \frac{\sigma_0 v_0}{v} \right\} \frac{E_{ref}^{\alpha}}{E^{1+\alpha}} dE$$

$$\Phi_e \equiv \Phi(E_{ref}) E_{ref}$$

$$I_0^*(\alpha) = \frac{E_{ref}^{\alpha}}{\bar{E}_r^{\alpha}} I_0^*(0)$$

$$f^* = \frac{\Phi_t}{\Phi_e}$$

Principles of the k_0 -IAEA software

Conventional approach: Blaauw + Westcott + threshold

$$\begin{aligned} R &= \sigma_0 g(T) \Phi_t + I_0^*(\alpha) \Phi_e + \sigma_{fast} \Phi_{fast} \\ &= \sigma_0 \Phi_t \left(g(T) + \frac{Q_0^*(\alpha)}{f^*} \right) + \sigma_{fast} \Phi_{fast} \end{aligned}$$

$$g(T) = \frac{\int_0^\infty \sigma(v) \frac{2v^3}{v_T^4} e^{-\left(\frac{v}{v_T}\right)^2} dv}{\int_0^\infty \frac{\sigma_0 v_0}{v} \frac{2v^3}{v_T^4} e^{-\left(\frac{v}{v_T}\right)^2} dv}$$

The k_0 method and the k_0 -IAEA software

Relations between standard k_0 and k_0 -IAEA parameters

$$Q_0^* = Q_0 - 0.429$$

$$f^* = f + 0.429$$

$$\Phi_t = \Phi_s + \Phi_e \left(\frac{1}{0.5 + \alpha} \right) \sqrt{\frac{E_0}{E_{ref}}} \left(\frac{E_{ref}}{E_{Cd}} \right)^{(0.5 + \alpha)}$$

$$= \Phi_s + 0.429\Phi_e \quad \text{if } \alpha = 0$$

and

$$E_0 = 25 \text{ meV}, E_{Cd} = 0.55 \text{ eV}, E_{ref} = 1 \text{ eV}$$

How to implement the k_0 method

- 1- Characterize the detector first
 - find or determine the detector dimensions
 - measure peak-to-total ratio curve
 - measure full-energy efficiency curve
 - measure escape ratio curves (k_0 -IAEA)
- 2- Characterize the irradiation facility second
 - determine T , f and α (and the fast flux)

How to implement the k_0 method - irradiation facility characterization

- determine T , f and α (and the fast flux)
 - use a suitable mix of elements, some with low Q_0 , some with high Q_0 , with various E_r 's, some showing (n,p) or other threshold reactions, some being non- $1/v$
 - for example: Zr, Au, Ni, Lu.

The trouble with the standard methods

- Cd-cover-method takes two samples of identical, complex composition - that's one too many.
- Bare triple-comparator method can only yield three parameters, we need five
- Adding Lu and e.g. Ni to the standard combination of Zr-Au seems a good option
- But foils and wires in one capsule are hard to count together (efficiency, decay, shielding)
- ^{97}Zr appear to be too extreme in its behavior, and not representative for the other high-Q nuclides

Possible alternatives

- Existing materials
 - available alloys that happen to be suitable
 - reference materials
 - SMELS
- Homemade mixtures
 - ground and mixed powders
 - solutions of suitable composition, pipetted on filter paper

An existing alloy

Element	Concentration	Uncertainty	
Mn	4100	41	
Ni	809300	8093	
Mo	151600	1516	
W	27600	276	
Au	2900	29	

NIST Montana soil

Element	Concentration	Uncertainty
Na	11400	148
Mg	10500	200
Al	65300	457
Si	304400	943
S	420	5
K	24500	392
Ca	28800	403
Sc	9	2.25
Ti	3060	116
V	81.6	1.5
Cr	47	11
Mn	638	14
Fe	28900	289
Co	10	2.5

Element	Concentration	Uncertainty
Ni	20.6	0.55
Cu	114	1
Zn	350.4	2.4
Ga	15	3.75
As	105	4
Se	1.52	0.07
Br	5	1.25
Rb	110	27.5
Sr	245.3	0.34
Y	25	6.25
Zr	230	57.5
Mo	1.6	0.4
Ag	4.63	0.19
Cd	41.7	0.13

Element	Concentration	Uncertainty
In	1.1	0.275
Sb	19.4	0.89
I	3	0.75
Cs	6.1	1.5
Ba	726	18.9
La	40	10
Ce	69	17.3
Nd	31	7.8
Sm	5.9	1.5
Eu	1.1	0.28
Dy	5.6	1.4
Ho	1	0.25
Yb	2.7	0.68
Hf	7.3	1.8

Element	Concentration	Uncertainty
W	3	0.75
Au	0.03	0.0075
Hg	6.25	0.094
Pb	1162	15
Th	14	3.5
U	2.6	0.65

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Home-made ground and mixed powders

- Too risky because of segregation
- To be tried only by experienced, trained, professional reference-material makers
- Don't even think of trying this at home!

Home-made solutions pipetted on filter paper

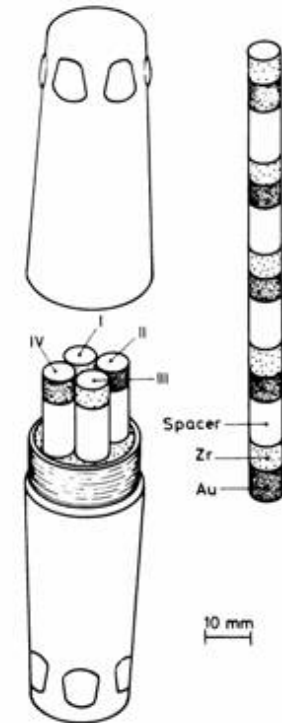
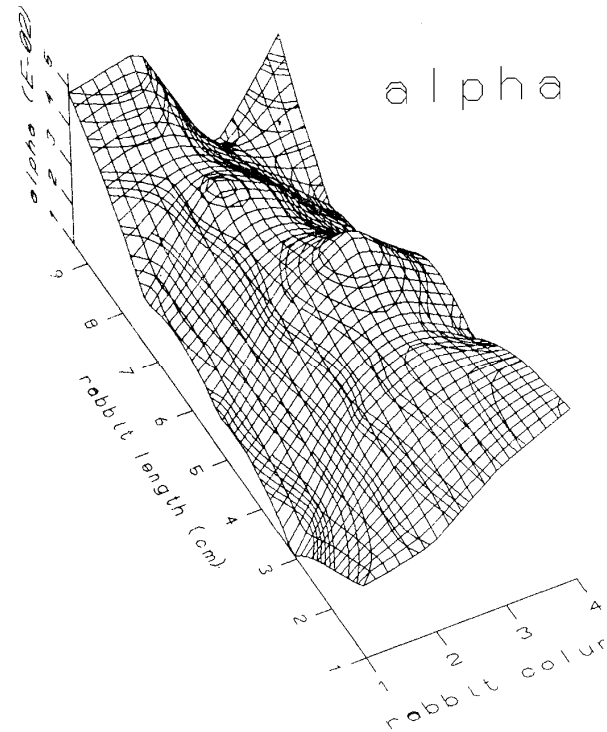
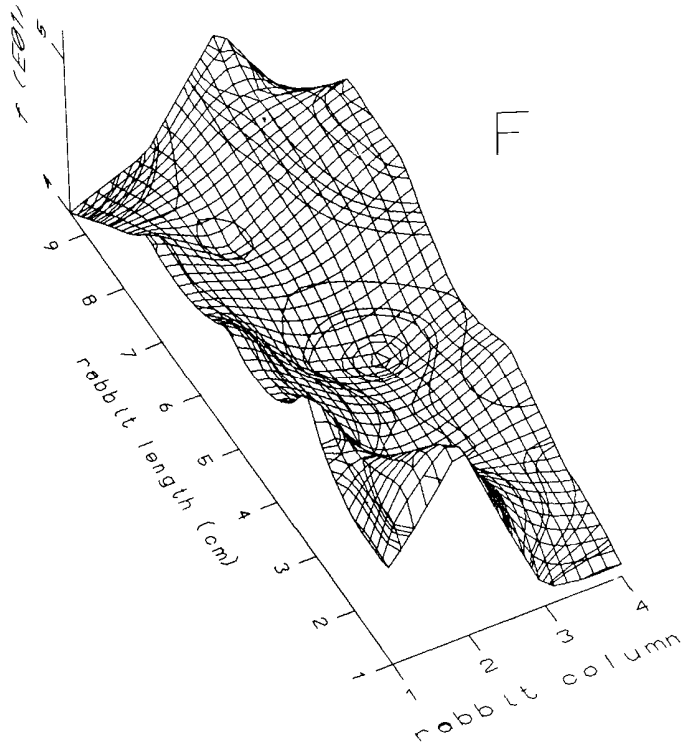
Delft - Sao Paolo example

Alternative methods for Thermal and Epithermal Flux Monitoring

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Trieste, Nov 8-10, 2010

Thermal and Epithermal Flux Monitoring



Thermal and Epithermal Flux Monitoring

Poor reproducibility of f and α in consecutive irradiations under stable reactor conditions:

1st series (n=5)

2nd series (n=5)

f 50 - 63

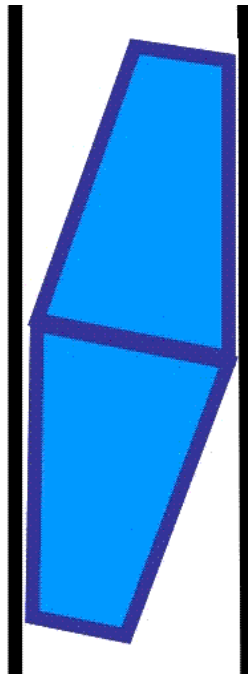
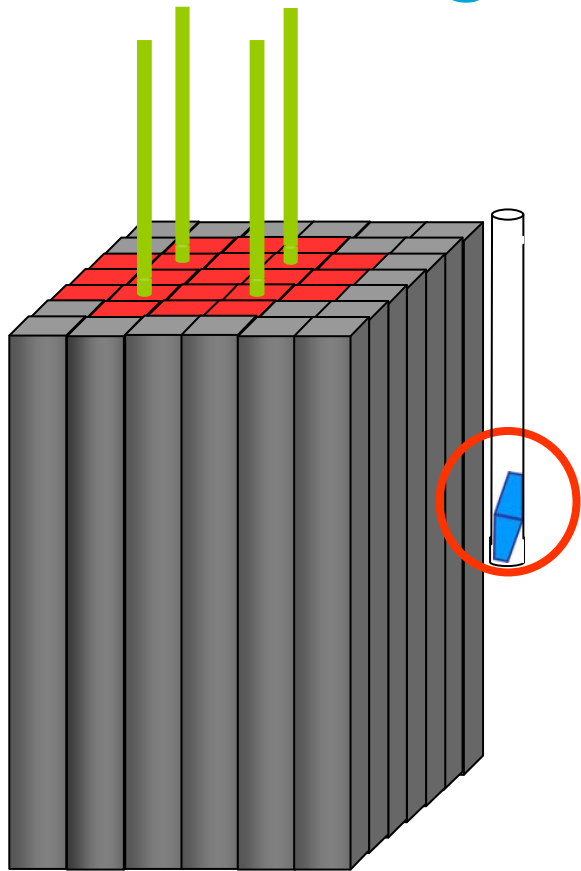
64 - 90

α 0,07 - 0,11

0,02 - 0,08

Temporarily solved at IRI by choosing $\alpha = 0.10$
and calculating the corresponding f values

Thermal and Epithermal Flux Monitoring



Thermal and Epithermal Flux Monitoring

Conclusions:

- Metrology requires to determine spectrum parameters in every irradiation for every position inside the rabbit.

Thermal and Epithermal Flux Monitoring

Cd-covered Zr-Au method:

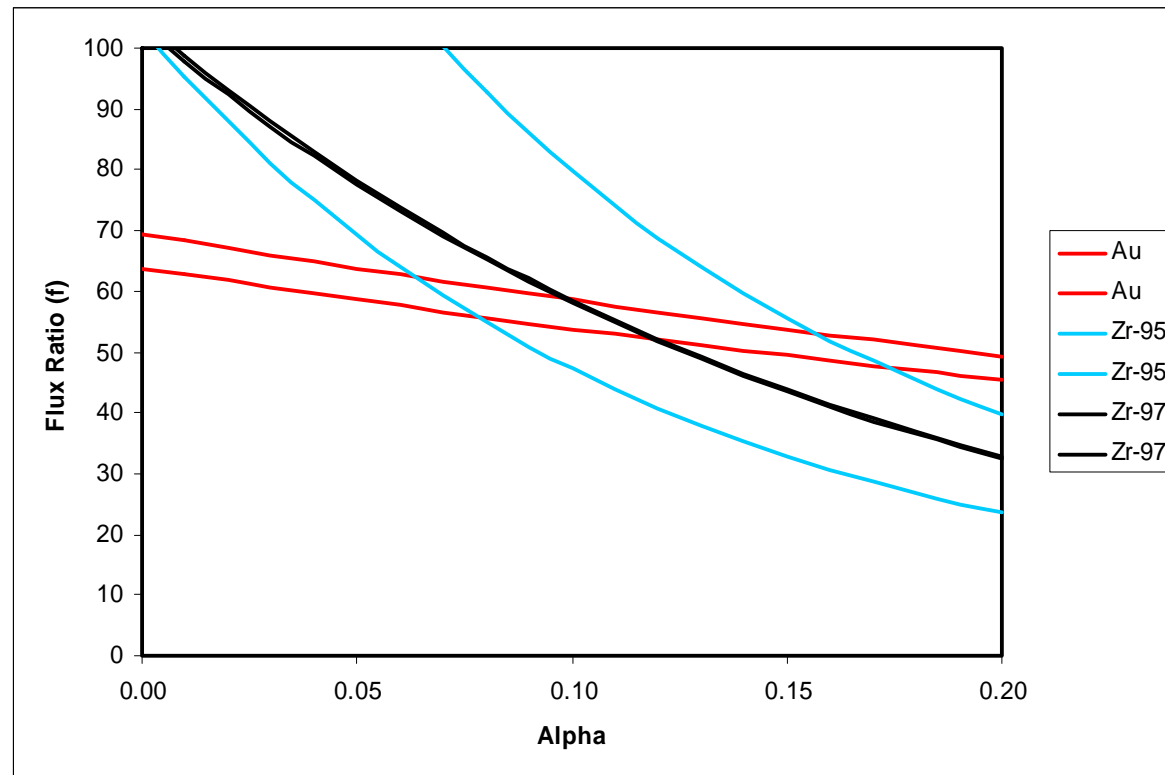
- Inapplicable due to thermal heating of Cd with a serious risk of damage to the plastic irradiation container.
- Inapplicable due to flux depressions in the real samples

Thermal and Epithermal Flux Monitoring

Bare triple method (Zr-Au):

- Poor counting statistics for ^{97}Zr under routine INAA conditions (t_{irr} : 1-4 h, t_{d} : 3-5 days, t_{c} : 1-4 h)
- Strong influence of counting statistics

Thermal and Epithermal Flux Monitoring



Thermal and Epithermal Flux Monitoring

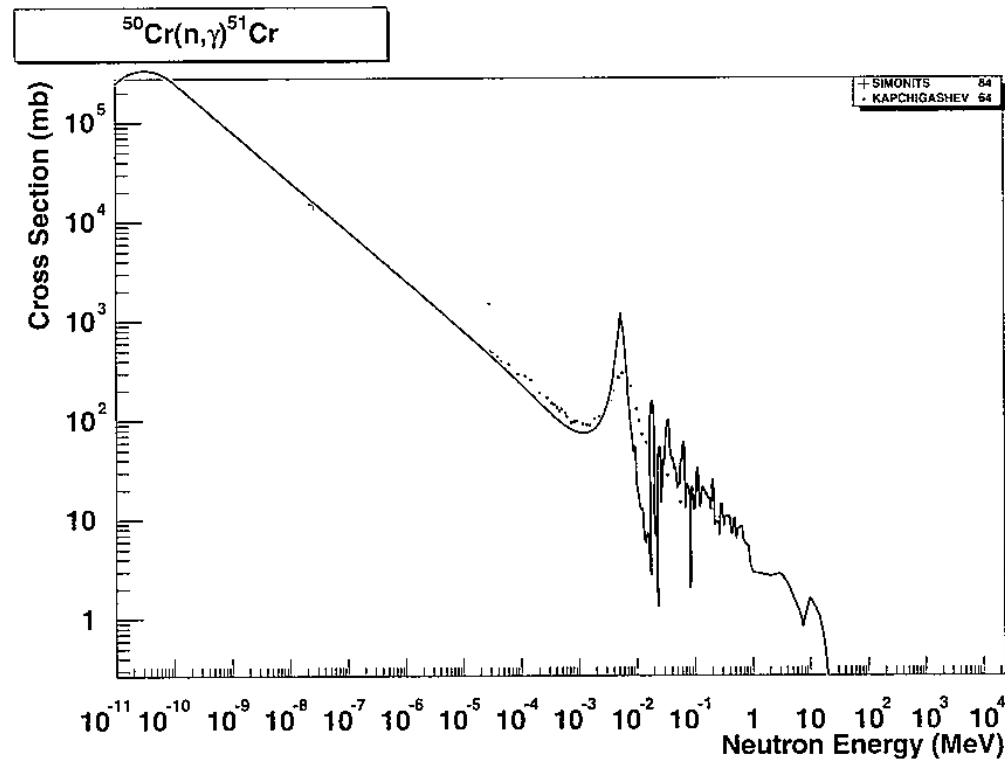
Search for alternative pairs of flux and spectrum monitors

Needed:

- High Q_0 , low E_r + High Q_0 , high E_r
- High σ_0
- No spectral interferences; minimal coincidence summing
- Easy to prepare in large batches
- $t_{1/2} > 1$ d

Thermal and Epithermal Flux Monitoring

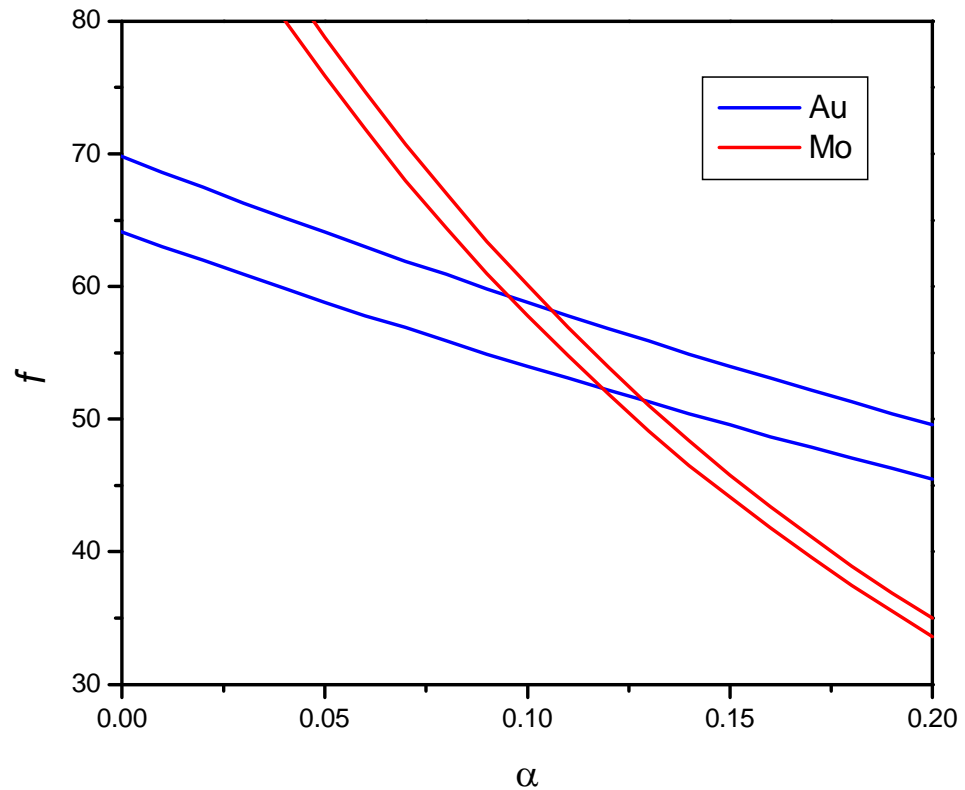
Epithermal flux can be neglected if $f > 50$



Thermal and Epithermal Flux Monitoring

Alternative set of monitors:

^{51}Cr , ^{99}Mo , ^{198}Au



Thermal and Epithermal Flux Monitoring

Verification in pool-side facility and AI-containers

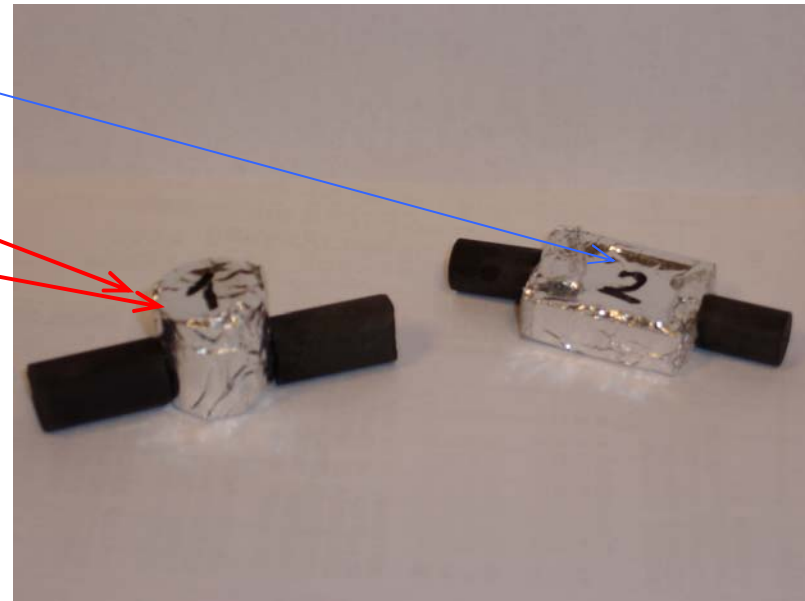
- Cd-covered Zr-Au-monitor
- Cr, Mo, Au monitor
- Zr, Au-monitor

Irradiation time: 30 minutes
(2 separate irradiations)

Decay time: 4 days

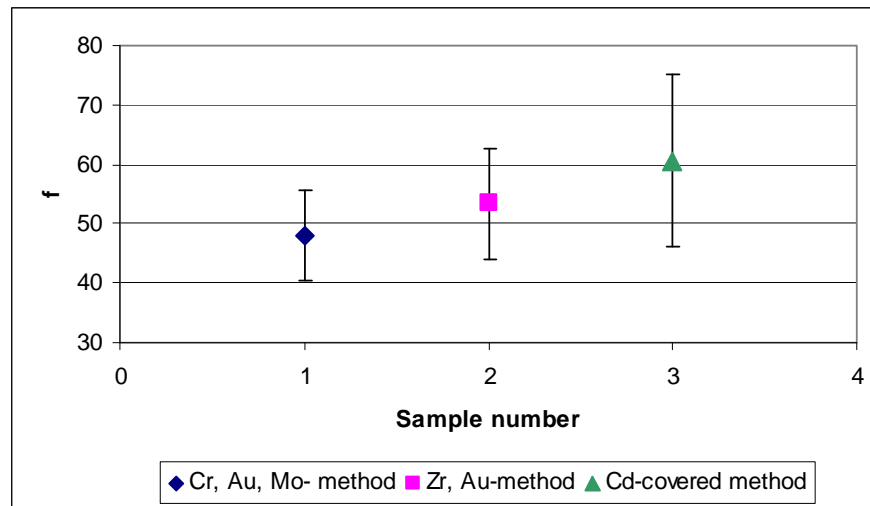
Counting time: 2 hours

Detector: 35 % Ge-detector

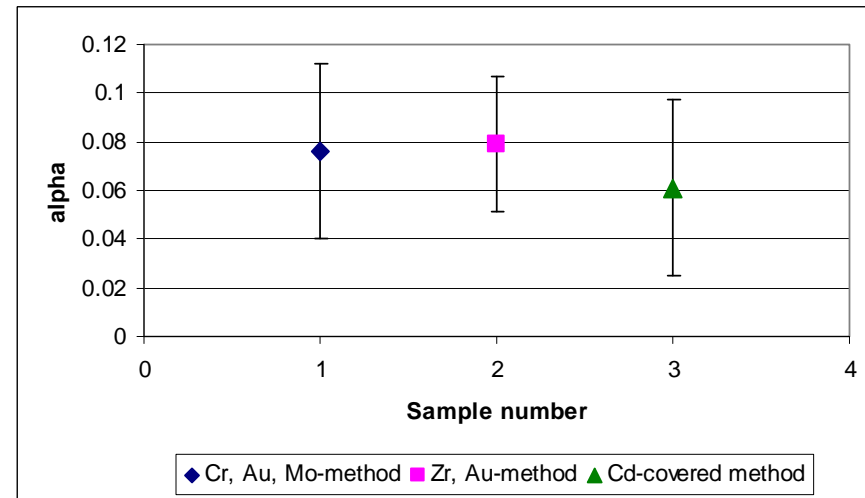


Thermal and Epithermal Flux Monitoring

f

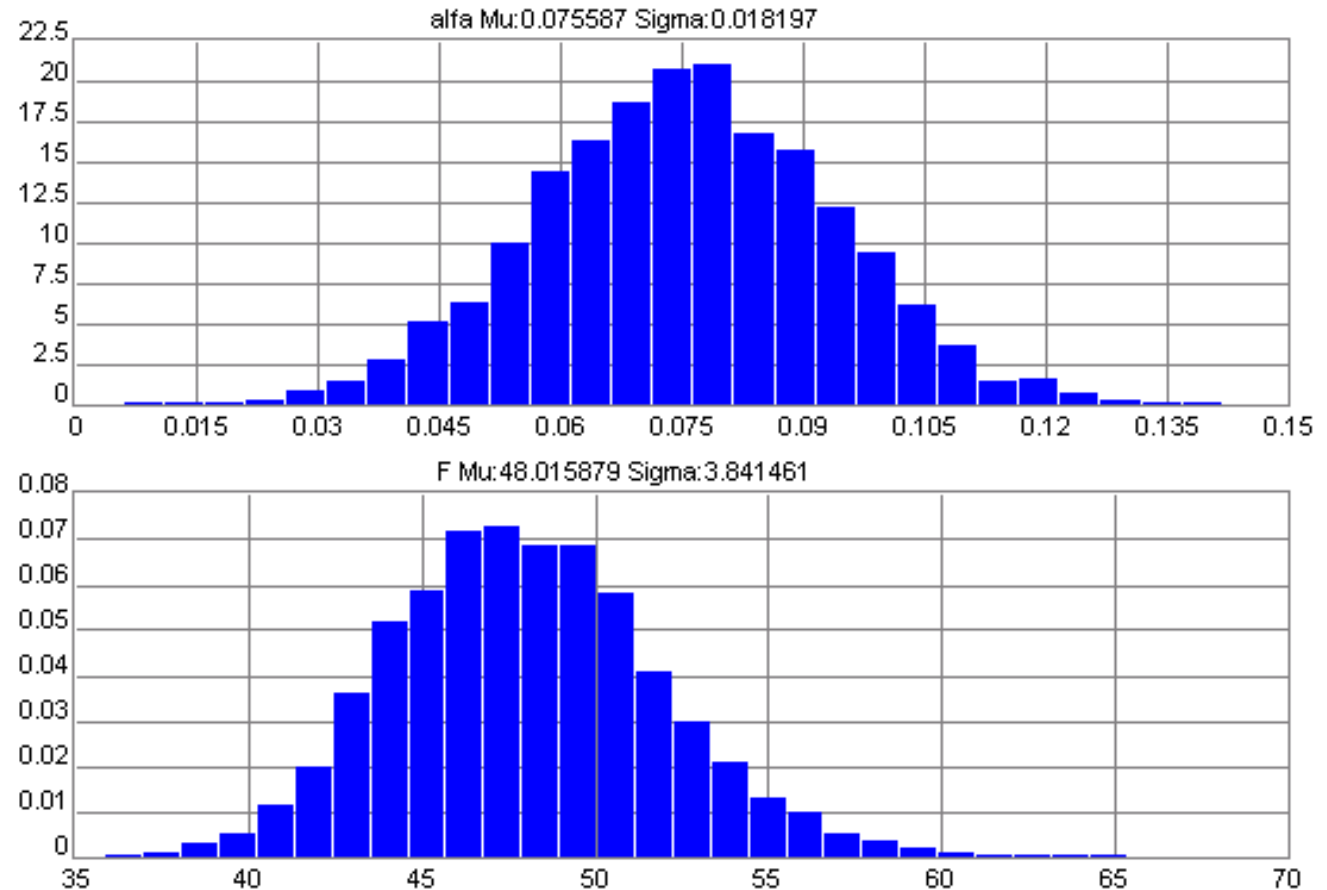


α

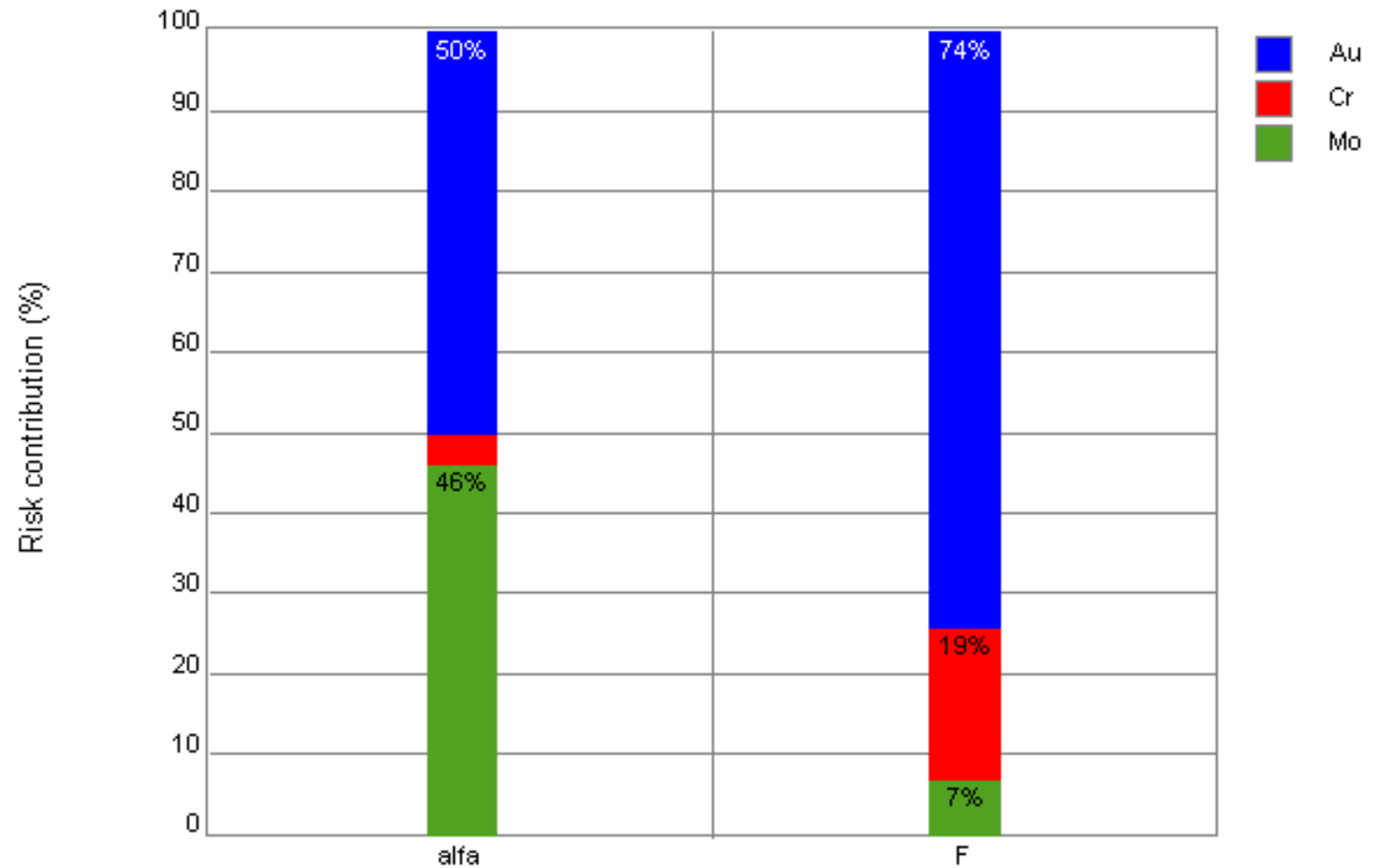


Thermal and Epithermal Flux Monitoring

	Activity uncertainty (%)
^{51}Cr	0.7
^{99}Mo	2.0
^{198}Au	1.1



Thermal and Epithermal Flux Monitoring



Thermal and Epithermal Flux Monitoring

Characterization of pneumatic facility

5 Cr, Mo, Au-monitors

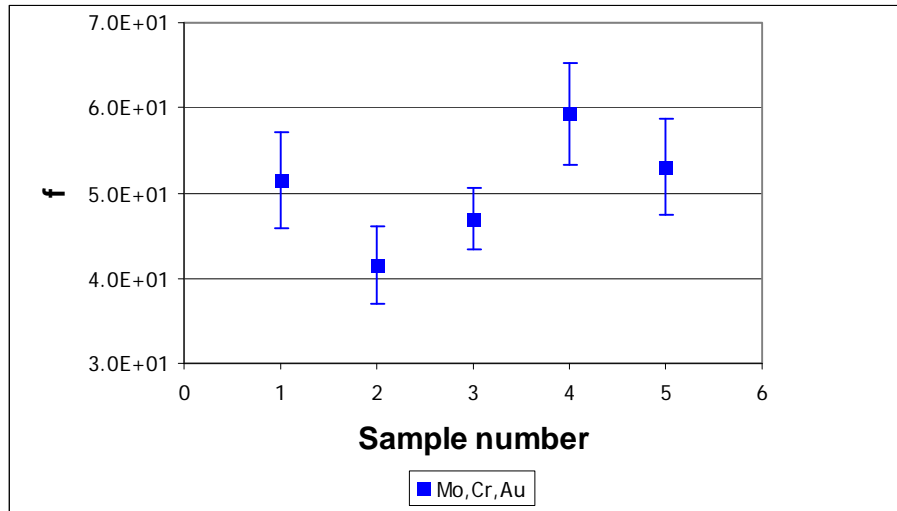
Irradiation time: 1 hour

Decay time: 4 days

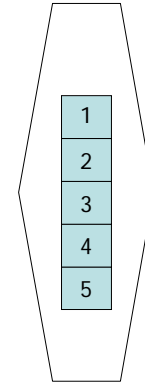
Counting time: 1 hours

Detector: 35 % Ge-detector

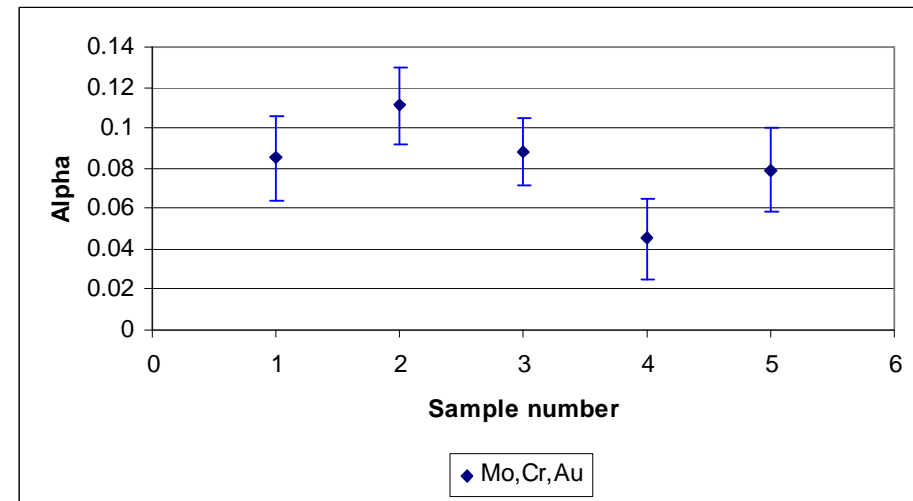
Thermal and Epithermal Flux Monitoring



f



α



Thermal and Epithermal Flux Monitoring

Conclusions:

- The Mo, Au, Cr- monitor is the solution for spatial f and α monitoring
- The monitor is easy to prepare in large batches
- The monitor will be used in routine INAA