



**The Abdus Salam
International Centre for Theoretical Physics**



2240-5

**Advanced School on Scaling Laws in Geophysics: Mechanical and
Thermal Processes in Geodynamics**

23 May - 3 June, 2011

**Examples of a cooling lithosphere: both cooling plate and cooling half-space,
comparison of different boundary conditions
(fixed temperature and fixed heat flux).**

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(1)

Heat transfer

- 1) Derivation of equation
- 2) Features of solution
- 3) Space-time relationships
- 4) Effect of phase transformations

Fourier's law

$$q = -k \frac{dT}{dy}$$

units W/m^2

↗ why sign?

units
 $J/s (W)$

$$= k \frac{\Delta T}{l}$$

in 3D

$$q = -k \cdot \nabla T$$

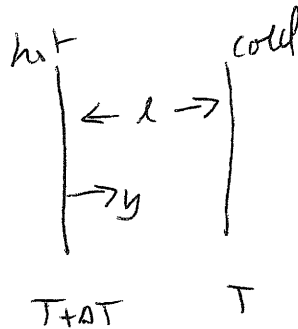
↗ need not be a scalar

typical numbers

$$dT/dy \sim 20-30 \text{ K/km}$$

$$k \sim 2-3 \text{ W/mK}$$

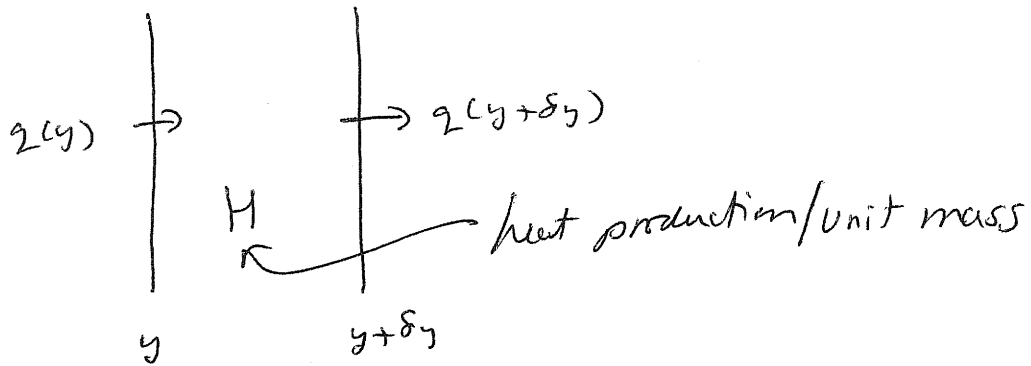
$$\Rightarrow q \sim 40-90 \text{ mW/m}^2$$



probl

(2)

1D heat conduction equation



$$q(y + \delta y) - q(y) = \rho H \delta y$$

$$\frac{q(y + \delta y) - q(y)}{\delta y} = \rho H$$

$\underbrace{\hspace{10em}}_{\partial q / \partial y}$

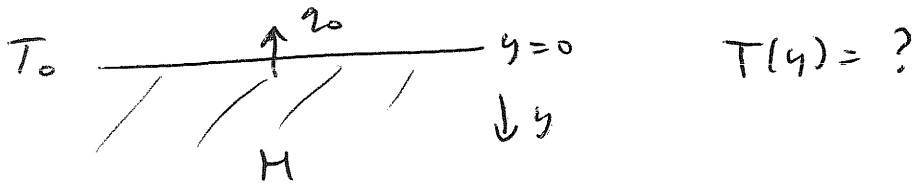
recall $q = -k dT/dy$

$$\frac{d}{dy} \left(k \frac{dT}{dy} \right) + \rho H = 0$$

if $H = 0$ $d^2T/dy^2 = 0$

in 3D $k \nabla^2 T + \rho H = 0$

(3)



$$k \frac{d^2 T}{dy^2} = -\frac{\rho H}{k}$$

integrate $k \frac{dT}{dy} = -\rho H y + C_1$

at $y=0$, $C_1 = -2z_0$

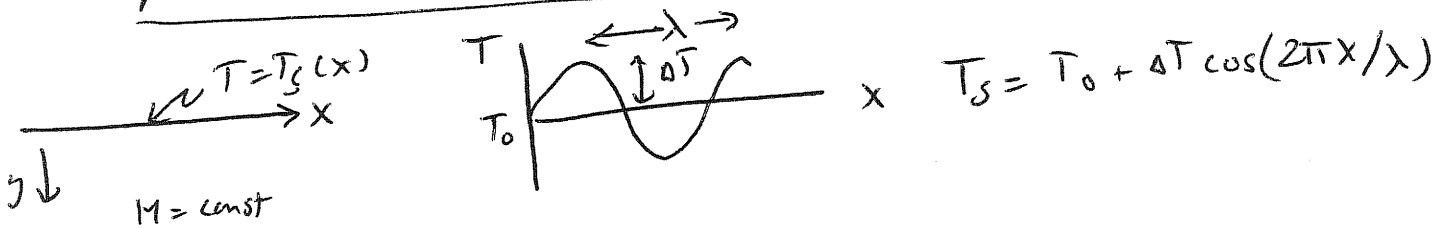
integrate again

$$\frac{\rho H}{2} y^2 = -kT + z_0 y + C_2$$

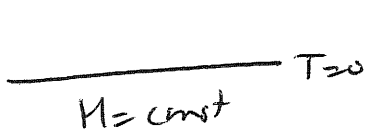
at $y=0$, $T=T_0$ so $C_2 = kT_0$

$$T = T_0 + \frac{z_0}{k} y - \frac{\rho H}{2k} y^2$$

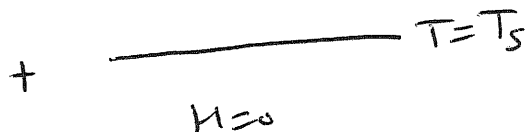
periodic variation in surface T



linear so ...



just solved



$$\frac{\partial^2 T}{\partial x^2} + \frac{\partial^2 T}{\partial y^2} = 0$$

Laplace's eq.

(4)

let $T(x, y) = T_0 + A(x)B(y)$ ← separation of variables (1)

to satisfy B.C. $A(x) = \cos(2\pi x/\lambda)$ (2)

sub (1) + (2) into $\nabla^2 T = 0$

$$-\frac{4\pi^2}{\lambda^2} A(x)B(y) + A(x) \frac{d^2 B}{dy^2} = 0$$

$$\frac{d^2 B}{dy^2} - \frac{4\pi^2}{\lambda^2} B = 0$$

$$B(y) = c_1 e^{-2\pi y/\lambda} + c_2 e^{2\pi y/\lambda}$$

as $y \rightarrow \infty$ $B(y)$ finite so $c_2 = 0$

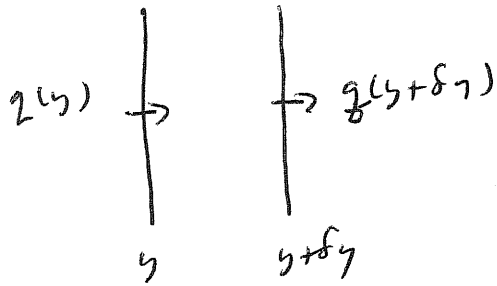
at $y = 0$ $T = T_0 + c_1 \cos(2\pi x/\lambda)$

$$\Rightarrow c_1 = \Delta T$$

$$\text{So } T(x, y) = T_0 + \underbrace{\Delta T e^{-2\pi y/\lambda}}_{\text{exponential decay of perturbation}} \cos(2\pi x/\lambda) + \frac{q_0}{k} y - \frac{\rho H}{2k} y^2$$

(5)

Unsteady heat conduction



$C \equiv$ specific heat
 (energy to raise T by
 1 degree)
 $\sim 10^3 \text{ J/kg}$

per unit area...

rate of internal energy change

$$\rho C \frac{\partial T}{\partial t} \delta y$$

rate at which heat is added

$$q(y) - q(y + \delta y) \quad (+ \rho H \delta y)$$

$$\therefore \rho C \frac{\partial T}{\partial t} = \underbrace{q(y) - q(y + \delta y)}_{-\partial q / \partial y \delta y}$$

but $q = -k \partial T / \partial y$

$$\rho C \frac{\partial T}{\partial t} = k \partial^2 T / \partial y^2$$

or

$$\frac{\partial T}{\partial t} = \kappa \partial^2 T / \partial y^2$$

thermal diffusivity $\sim 10^{-6} \text{ m}^2/\text{s}$

in 3D

$$\frac{\partial T}{\partial t} = \kappa \nabla^2 T (+ \rho H)$$

↑ if make heat

(6)

over what time t does $\frac{\Delta T}{T}$ change?

$$\frac{\partial T}{\partial t} = \kappa \frac{\partial^2 T}{\partial y^2}$$

$$O\left(\frac{\Delta T}{T}\right) \sim O\left(\kappa \frac{\Delta T}{L^2}\right)$$

$$\Rightarrow t \sim L^2/\kappa$$

time to cook a chicken (1 kg) is 1 hour
time to cook a turkey (10 kg)?

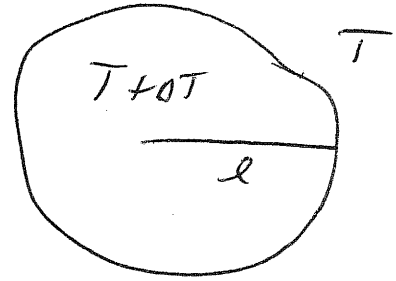
$$t \propto L^2 \quad L \propto M^{1/3}$$

$$t \propto M^{2/3}$$

$$\frac{t_1}{t_2} = \left(\frac{M_1}{M_2}\right)^{2/3}$$


$$t_{\text{turkey}} = (10)^{2/3} \sim 4.64 \text{ hours}$$

prob 2+3



(7)

periodic in time changes of surface T


 $T = T_0 + \Delta T \cos(\omega t)$
 $\frac{\partial T}{\partial t} = k \frac{\partial^2 T}{\partial y^2}$

again use separation of variables

$$T(y, t) = T_0 + A_1(y) B(t)$$

$$= T_0 + \underbrace{A_1(y) \cos \omega t}_{\text{in phase}} + \underbrace{A_2(y) \sin \omega t}_{\text{out of phase}}$$

sub. into $\frac{\partial T}{\partial t} = k \frac{\partial^2 T}{\partial y^2}$, apply B.C.

$$T = T_0 + \underbrace{\Delta T e^{-y \sqrt{\omega/2k}}}_{\text{amplitude}} \cos(\omega t - \underbrace{y \sqrt{\omega/2k}}_{\text{phase}})$$

decreases exponentially
by factor of e at

$$y_c = \left(\frac{2k}{\omega}\right)^{1/2}$$

if $\omega = 1/\text{day}$, $y_c = 17 \text{ cm}$

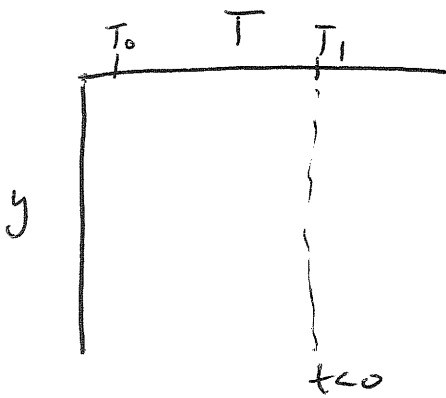
$\omega = 1/\text{year}$, $y_c = 3.2 \text{ m}$

$\omega = \frac{1}{10^4} \text{ years}$, $y_c = ?$ (320 m)

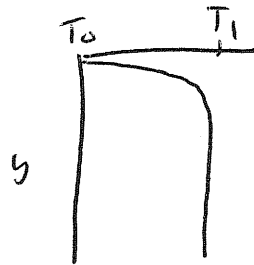
prob 4

(8)

Cooling of a half-space



at $t=0$ change T at $y=0$
from T_1 to T_0



$$t > 0 \quad \frac{\partial T}{\partial t} = k \frac{\partial^2 T}{\partial y^2} \quad (*)$$

$Q(t)$?

$T(y, t)$?

let $\theta = (T - T_1) / (T_0 - T_1)$ so $0 < \theta < 1$

$$T = (T_0 - T_1)\theta + T_1$$

Sub into (*)

$$\frac{\partial \theta}{\partial t} = k \frac{\partial^2 \theta}{\partial y^2}$$

I.C. $\theta(y, 0) = 0$

B.C. $\begin{cases} \theta(0, t) = 1 \\ \theta(\infty, t) = 0 \end{cases}$

recall that k, t and length were related

hypothesize that θ depends on y, t being related

$$\eta = \frac{y}{2\sqrt{kt}}$$

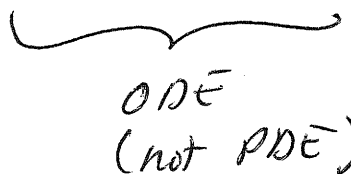
(9)

$$\frac{\partial \theta}{\partial t} = \frac{d\theta}{dn} \frac{\partial n}{\partial t} = \frac{\partial \theta}{\partial n} \left(-\frac{1}{4} \frac{y}{\sqrt{kt}} \frac{1}{t} \right) = -\frac{n}{2t} \frac{d\theta}{dn}$$

$$\frac{\partial \theta}{\partial y} = \frac{\partial \theta}{\partial n} \cdot \frac{\partial n}{\partial y} = \frac{1}{2\sqrt{kt}} \frac{\partial \theta}{\partial n}$$

$$\frac{\partial^2 \theta}{\partial y^2} = \frac{1}{2\sqrt{kt}} \frac{\partial^2 \theta}{\partial n^2} \cdot \frac{\partial n}{\partial y} = \frac{1}{4kt} \frac{\partial^2 \theta}{\partial n^2}$$

$$\therefore -2n \frac{d\theta}{dn} = \frac{d^2 \theta}{dn^2}$$



ODE
(not PDE)

B.C. $t=0 \Rightarrow n \rightarrow \infty$
 $y \rightarrow \infty \Rightarrow n \rightarrow \infty$
 $y=0 \Rightarrow n=0$

$\theta(n=\infty) = 0$
 $\theta(n=0) = 1$ } 2 B.C. for
 2nd order
 ODE

let $f = d\theta/dn \Rightarrow -2nf = df/dn$

integrate $-n^2 = \ln f + C$

$f = c_1 e^{-n^2} = d\theta/dn$

integrate again

$$\theta = c_1 \int_0^n e^{-z^2} dz + c_2$$

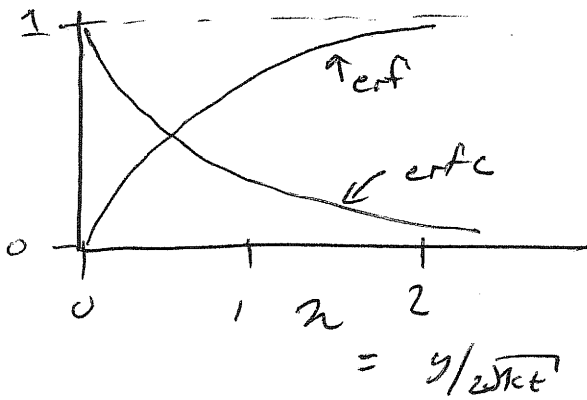
$\theta(0) = 1 \Rightarrow c_2 = 1$

$\theta(\infty) = 0$ so $\theta = c_1 \underbrace{\int_0^\infty e^{-z^2} dz}_{\sqrt{\pi}/2} + 1 = 0$
 $\Rightarrow c_1 = -2/\sqrt{\pi}$

(10)

$$\theta = \frac{T - T_1}{T_0 - T_1} = 1 - \underbrace{\frac{2}{\sqrt{\pi}} \int_0^{\eta} e^{-z^2} dz}_{\text{erf}(\eta)}$$

$$= \text{erfc}(\eta)$$



]} y, t related!!

Heat flow?

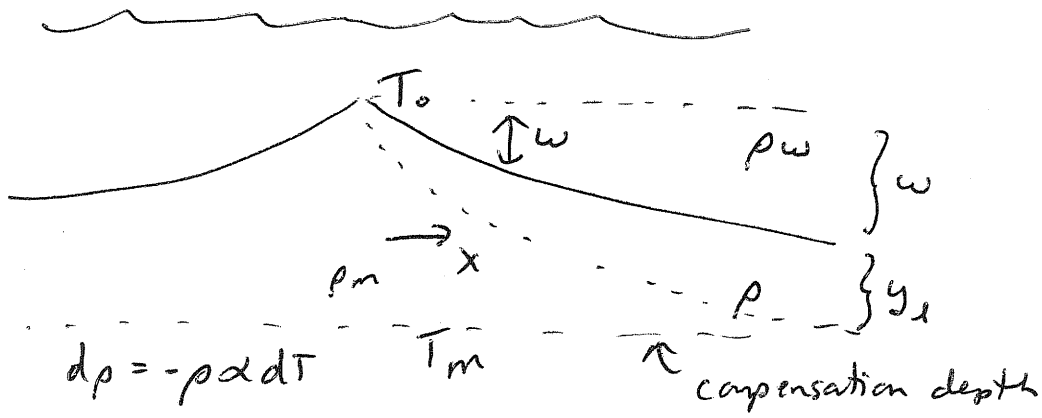
$$q = -k \frac{\partial T}{\partial y} = k \frac{(T_0 - T_1)}{\sqrt{\pi \alpha t}} \quad q \propto t^{-1/2}$$

$$\left(k \frac{\partial T}{\partial y} = (T_0 - T_1) \frac{\partial \theta}{\partial y} \right) \frac{1}{2\sqrt{\pi \alpha t}}$$

$$= \frac{k(T_0 - T_1)}{2\sqrt{\pi \alpha t}} \left(\frac{\partial \theta}{\partial \eta} \right) \left(\frac{\partial \eta}{\partial y} \right) \left(\frac{\partial \theta}{\partial \eta} \right) \propto e^{-\eta^2}$$

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Depth of oceans



What is $w(x)$?

at ridge

$$\rho_m(w + y_2) = \int_0^{y_2} \rho(y) dy + w\rho_w$$

$$w(\rho_w - \rho_m) + \int_0^{y_2} (\rho(y) - \rho_m) dy = 0$$

$$\rho_m \alpha (T_m - T_0)$$

we just solved for this

$$(T_m - T_0) \rho_m \alpha \int_0^{y_2} \text{erfc}\left(\frac{y}{2\sqrt{kt}}\right) dy$$

$$\therefore w = \frac{\rho_m \alpha (T_m - T_0)}{\rho_m - \rho_w} \int_0^{y_2} \text{erfc}\left(\frac{y}{2\sqrt{kt}}\right) dy$$

$$\text{if } y_2 \rightarrow \infty \int \rightarrow \frac{1}{\sqrt{\pi}}$$

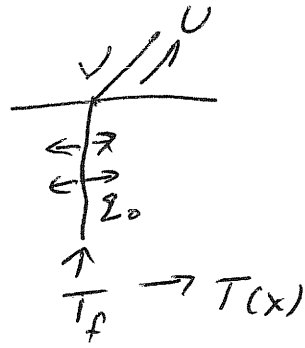
$$\text{let } u = \frac{y}{2\sqrt{kt}} \quad du/dy = \frac{1}{2\sqrt{kt}}$$

$$w(x) = \frac{\rho_m \alpha (T_m - T_0) 2\sqrt{kt}}{(\rho_m - \rho_w) \sqrt{\pi}}$$

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heating of faults

$Work = F \cdot d$
 rate of work = $F \cdot U$
 heat flow = τU



$$q_0 = U\tau/2$$

What is T_f ?

$$\frac{\partial T}{\partial t} = k \frac{\partial^2 T}{\partial x^2}$$

$$\frac{\partial}{\partial x} \left(\frac{\partial T}{\partial t} \right) = k \frac{\partial^3 T}{\partial x^3}$$

$$\frac{\partial q}{\partial t} = k \frac{\partial^2 q}{\partial x^2}$$

with B.C. $q(x=0) = \frac{U\tau}{2}$

$$q(x \rightarrow \infty) = 0$$

Solution $q = q_0 \operatorname{erfc} n$

$$\frac{\partial T}{\partial x} = -\frac{q_0}{k} \operatorname{erfc} n$$

$$T(x) = T_0 - \frac{q_0}{k} \int_0^x \operatorname{erfc} \left(\frac{x}{\sqrt{2kt}} \right) dx$$

$$= T_0 + \frac{2q_0 \sqrt{kt}}{k} \int_n^{\infty} \operatorname{erfc} n' dn'$$

$\int_n \rightarrow \frac{1}{\sqrt{\pi}}$

$$T(x=0) = T_0 + \frac{2q_0 \sqrt{kt}}{k} \frac{1}{\sqrt{\pi}}$$

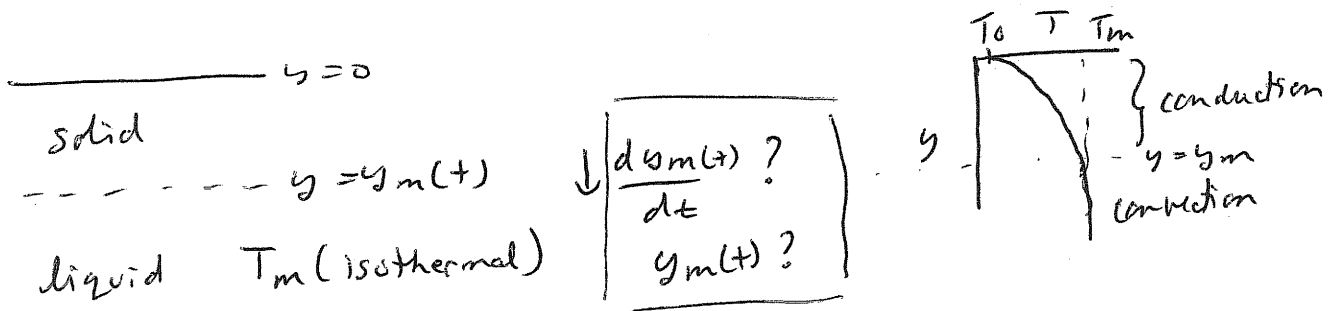
ans

Phase changes (solidification)

Latent heat: heat liberated by solidification of 1 kg
(L)

2 complications: Where is boundary? Accounting for L?

Stefan (1891) problem



again $\Theta = (T - T_0) / (T_m - T_0)$

$n = y / \sqrt{2\sqrt{\lambda k t}}$

define $n_m = y_m / \sqrt{2\sqrt{\lambda k t}} = \lambda_1$ (Answer already!)

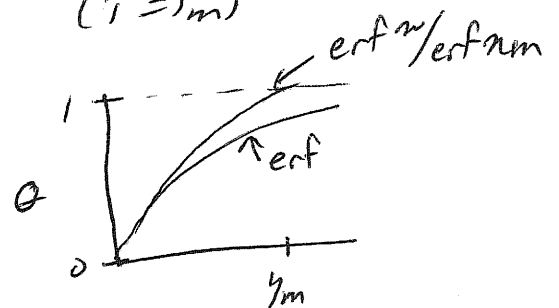
what is λ_1 ?

$2n \frac{d\Theta}{dn} = \frac{d^2\Theta}{dn^2}$ from before

B.C. $\Theta(n=0) = 0$ ($T = T_0$)

$\Theta(n = n_m = \lambda_1) = 1$ ($T = T_m$)

$\Theta = \frac{\text{erf } n}{\text{erf } (n_m)}$



prob 5

(14)

to get λ_1 ,

in time δt , boundary moves down $\frac{dy_m}{dt} \delta t$

solidifying $\rho \left(\frac{dy_m}{dt} \right) \delta t / \text{area}$

releasing heat $L \rho \left(\frac{dy_m}{dt} \right) \delta t / \text{area}$

heat must be conducted $-k \frac{\partial T}{\partial y} \Big|_{y=y_m} \delta t$

$$\therefore -k \frac{\partial T}{\partial y} \Big|_{y=y_m} = \rho L \frac{dy_m}{dt}$$

$$\text{since } y_m = 2\lambda_1 \sqrt{\pi k t}$$

$$\frac{dy_m}{dt} = \lambda_1 \sqrt{\frac{\pi k}{t}}$$

$$\frac{\partial T}{\partial y} \Big|_{y=y_m} = -\frac{T_m - T_0}{2\sqrt{k t}} \frac{2}{\sqrt{\pi}} e^{-\lambda_1^2} \frac{1}{\text{erf } \lambda_1}$$

$$\frac{k(T_m - T_0)}{\rho L k \sqrt{\pi}} \frac{e^{-\lambda_1^2}}{\text{erf } \lambda_1} = \rho L \lambda_1 \sqrt{\frac{\pi k}{t}}$$

$$\frac{e^{-\lambda_1^2}}{\lambda_1 \text{erf } \lambda_1} = \frac{\rho L k}{k \rho C (T_m - T_0)} \quad \text{known - get } \lambda_1$$

plot