



2254-1

Workshop on Sphere Packing and Amorphous Materials

25 - 29 July 2011

Ancient History: from Linear polymers to tethered surfaces

David NELSON

Harvard University Department of Physics 17 Oxford St., Cambridge, MA 02138 U.S.A.

Ancient History: from linear polymers to tethered surfaces

By the 1990's, theories of linear polymer chains in a good solvent had been generalized to include the statistical mechanics of flexible sheet polymers



Remarkably, "tethered surfaces" with a shear modulus are able to resist thermal crumpling and exhibit a low temperature flat phase!!





Pressurized Amorphous Shells, Pollen Grains and Thermal Fluctuations (D. Nelson, Harvard)

Shell theory: Foppl-von Karman equations and nonlinear elasticity theory

-- applicaton to crumpling and folding of pollen grains

Flat membranes: elasticity and statistical mechanics

--thermal fluctuations lead to scale-dependent elastic constants

Shells with thermal fluctuations: deformations of pressurized spherical shells

-- Renormalized bending rigidity, Young's modulus and pressure all diverge as sphere radius $R \rightarrow \infty$!

-- Anomalous height fluctuation and indentation experiments

J. Paulose G. Gompper G. Vliegenhart

E. KatiforiJ. DumaisE. CerdaS. Alben

Physics at T=0 is described by the Foppl-von Karman equations (~1904)





$$E = \frac{1}{2} \int d^2 x [\kappa (\nabla^2 f(\vec{x}))^2 + 2\mu u_{ij}^2(\vec{x}) + \lambda u_{kk}^2(\vec{x})]$$
$$u_{ij}(\vec{x}) = \frac{1}{2} \left[\frac{\partial u_i(\vec{x})}{\partial x_j} + \frac{\partial u_j(\vec{x})}{\partial x_i} + \frac{\partial f(\vec{x})}{\partial x_i} \frac{\partial f(\vec{x})}{\partial x_j} \right]$$

Take functional derrivatives and minimize to get ...

Foppl-von Karman equations

$$\kappa \nabla^4 f = \frac{\partial^2 \chi}{\partial y^2} \frac{\partial^2 f}{\partial x^2} + \frac{\partial^2 \chi}{\partial x^2} \frac{\partial^2 f}{\partial y^2} - 2 \frac{\partial^2 \chi}{\partial x \partial y} \frac{\partial^2 f}{\partial x \partial y} \qquad \sigma_{ij}(\vec{r}) = \varepsilon_{im} \varepsilon_{jn} \partial_m \partial_n \chi(\vec{r})$$
$$= \frac{1}{Y} \nabla^4 \chi = -\frac{\partial^2 f}{\partial x^2} \frac{\partial^2 f}{\partial y^2} + \left(\frac{\partial^2 f}{\partial x \partial y}\right)^2 \qquad Y = \frac{4\mu(\mu + \lambda)}{2\mu + \lambda} = Young's modulus$$

The limit of high FvK number, $\gamma = YR^2 / \kappa >> 1$, is singular, like high Reynold's number turbulence...

T = 0 F-vK equations: Cumpling of lily pollen grains (*Eleni Katifori, J. Dumais lab*)





It's reversible!!!

Helpful to avoid hysteresis associated with the "snap-through" or buckling transition



Modeling pollen crumpling with a weak sector



*model an amorphous shell with a weak sector using a triangular mesh

*minimize artificial effects of the 12 disclinations by compensating for different bond lengths:

$$\frac{\varepsilon}{2} \sum_{\langle ij \rangle} (|\vec{r}_i - \vec{r}_j| - a)^2 \rightarrow \frac{\varepsilon}{2} \sum_{\langle ij \rangle} (|\vec{r}_i - \vec{r}_j| - a_{ij})^2$$

*model dehydration by a soft constraint of ever decreasing volumes

*introduce spontaneous curvature

Simulation of crumpling/folding upon dehydration of the lily pollen grain



Renormalization of Elastic Parameters in Thermally Excited Sheet Polymers I

F.-von K.

fixed point

$$E = \frac{1}{2} \int d^2 x [\kappa (\nabla^2 f(\vec{x}))^2 + 2\mu u_{ij}^2(\vec{x}) + \lambda u_{kk}^2(\vec{x})]$$

$$u_{ij}(\vec{x}) = \frac{1}{2} \left[\frac{\partial u_i(\vec{x})}{\partial x_j} + \frac{\partial u_j(\vec{x})}{\partial x_i} + \frac{\partial f(\vec{x})}{\partial x_i} \frac{\partial f(\vec{x})}{\partial x_j} \right]$$

$$Z = \int \mathcal{D}\vec{u}(x_1, x_2) \int \mathcal{D}f(x_1, x_2) \exp(-F / k_B T)$$



L. Peliti & drn (~1987) J. Aronovitz and T. Lubenksy P. Le Doussal and L. Radzihovsky define running coupling constants.... $\overline{\mu}(l) = k_B T \mu a_0^2 / \kappa^2; \qquad \overline{\lambda}(l) = k_B T \lambda a_0^2 / \kappa^2$ Young's modulus is $Y(l) = \frac{4\mu(l)[\mu(l) + \lambda(l)]}{2\mu(l) + \lambda(l)}$ $\mathbf{\lambda}(l)$ $\overline{\mu}(l)$ Thermal fixed point



Consider, e.g., the size r(R) and crease energy E(R) of a bent surface....



without thermal fluctuations (F-vK limit) $r \propto R^{2/3}, E \propto R^{1/3}$, (T. Witten et al.)

with thermal fluctuations....

$$r \sim R^{0.76}, E \sim R^{0.74}$$

Anomalous Fluctuations in the Spectrin Skeleton of Red Blood Cells

C. Schmidt et al., <u>Science</u> 259, 952 (1993)



Power law scaling expected for the radially averaged structure of a dilute concentration of spectrin membranes

$$S(q) \sim 1/q^{2+\eta/2}$$

~ $1/q^{2.35}$
~ $\eta = 0.70 \ (\eta_{theory} = 0.75)$











Microfluidic fabrication of polymersomes

Shum et al., JACS 2008, 130, 9543

Start with "double emulsion" of ampiphillic diblock copolymers (PEG-b-PLA).

Tune wetting properties to eject thin *crystalline* bilayer shells.
Result is a delivery vehicle for dugs, flavors, colorings and fragrances that can be osmotically crushed.

> Polymersome Radius, $R = 30 \ \mu m$ Thickness, $h = 10 \ nm$

 $\gamma =$ Foppl-von Karman number $\approx 9(R/h)^2 = 10^7 !$ Initial shape: z = Z(x, y)

To address similar questions for spherical shells, we use shallow shell theory....



$$\begin{pmatrix} x \\ y \\ Z(x, y) \end{pmatrix} \rightarrow \begin{pmatrix} x + u_x(x, y) - \partial_x Z(x, y) f(x, y) \\ y + u_y(x, y) - \partial_y Z(x, y) f(x, y) \\ Z(x, y) + f(x, y) \end{pmatrix}$$

$$ds'^2 = ds^2 + 2u_{ij}dx_i dx_j$$

$$u_{ij}(\vec{x}) = \frac{1}{2} \left[\frac{\partial u_i(\vec{x})}{\partial x_j} + \frac{\partial u_j(\vec{x})}{\partial x_i} + \frac{\partial f(\vec{x})}{\partial x_i} \frac{\partial f(\vec{x})}{\partial x_j} \right]$$

$$u_{ij}(\vec{x}) = \frac{1}{2} \left[\frac{\partial u_i(\vec{x})}{\partial x_j} + \frac{\partial u_j(\vec{x})}{\partial x_i} + \frac{\partial f(\vec{x})}{\partial x_i} \frac{\partial f(\vec{x})}{\partial x_j} - \delta_{ij} \frac{f}{R} \right]$$

Membranes vs. shells: Curved is different



Bending rigidity Young's modulus



$$u_{ij}(\vec{x}) = \frac{1}{2} \left[\frac{\partial u_i(\vec{x})}{\partial x_j} + \frac{\partial u_j(\vec{x})}{\partial x_i} + \frac{\partial f(\vec{x})}{\partial x_i} \frac{\partial f(\vec{x})}{\partial x_j} \right] \quad VS. \quad u_{ij}(\vec{x}) = \frac{1}{2} \left[\frac{\partial u_i(\vec{x})}{\partial x_j} + \frac{\partial u_j(\vec{x})}{\partial x_i} + \frac{\partial f(\vec{x})}{\partial x_i} \frac{\partial f(\vec{x})}{\partial x_j} - \delta_{ij} \frac{f}{R} \right] \\ \int \frac{f}{\ell} \quad Strain \quad \sim \left[\frac{f}{\ell} \right]^2 \quad R$$

Elastic length scale

$$E = \frac{1}{2} \int d^2 x [\kappa (\nabla^2 f(\vec{x}))^2 + 2\mu u_{ij}^2(\vec{x}) + \lambda u_{kk}^2(\vec{x})]$$

$$u_{ij}(\vec{x}) \approx \frac{1}{2} \left[\frac{\partial u_i(\vec{x})}{\partial x_j} + \frac{\partial u_j(\vec{x})}{\partial x_i} + \frac{\partial f}{\partial x_i} - \delta_{ij} \frac{f}{R} \right]$$
Bending energy $\sim \kappa \frac{f^2}{\ell^4}$
Stretching energy $\sim \frac{Y}{R^2} f^2$,
 $\left(Y = \frac{4\mu(\mu + \lambda)}{2\mu + \lambda} = \text{Young's modulus} \right)$

$$\frac{\kappa}{\ell^4} = \frac{Y}{R^2} \implies \ell^* = \left(\frac{\kappa R^2}{Y} \right)^{1/4} = R / \gamma^{1/4}$$
 $\left(\gamma = YR^2 / \kappa = \text{Foppl-von Karman number} \right)$

> The Föppl-von Kármán length scale l* provides an infrared cutoff for thermal fluctuations...

Shells under external pressure



 $f(x_1, x_2)$

Nonlinear Field Theory for Thermally Excited Shells...

Trace out in-plane phonons and upward radial shrinkage $f_0 \ldots$

$$\begin{split} F_{\text{eff}} &= -k_B T \ln \left(\int D\{u_x(x,y)\} \int D\{u_y(x,y)\} \int df_0 \, e^{-F/k_B T} \right) \\ & \text{New for curved membranes!} \\ F_{\text{eff}} &= \frac{\kappa}{2} \int d^2 x (\nabla^2 f)^2 + \frac{Y}{2} \int d^2 x \left(\frac{1}{2} P_{ij}^{\text{T}} \partial_i f \partial_j f - \frac{f}{R} \right)^2 - \frac{pR}{4} \int d^2 x |\nabla f|^2 \\ F_{eff} &= F_0 + F_1 \\ \begin{cases} F_0 &= \frac{1}{2} \int d^2 x \left[\kappa (\nabla^2 f)^2 - \frac{pR}{2} (\nabla f)^2 + \frac{Y}{R^2} f^2 \right] \\ F_1 &= \int d^2 x \left[\frac{1}{4} P_{ij}^T (\partial_i f \partial_j f)^2 - \frac{f}{R} P_{ij}^T \partial_i f \partial_j f \right] \end{cases}$$

Gaussian Fluctuation Spectrum in Fourier Space

$$F_{0} = \frac{1}{2} \int d^{2}x \left[\kappa (\nabla^{2}f)^{2} - \frac{pR}{2} (\nabla f)^{2} + \frac{Y}{R^{2}} f^{2} \right]$$

$$= \frac{1}{2} \int \frac{d^{2}q}{(2\pi)^{2}} \left(\kappa q^{4} - \frac{pR}{2} q^{2} + \frac{Y}{R^{2}} \right) \left| f_{q} \right|^{2}$$

$$F_{0} = \frac{\kappa}{2} \int \frac{d^{2}q}{(2\pi)^{2}} \omega(q) \left| f_{q} \right|^{2}, \quad \omega(q) = \frac{Y}{R^{2}} - \frac{pR}{2} q^{2} + \kappa q^{4}$$

$$F_{0} = \int d^{2}x e^{iqx} f(\mathbf{x})$$

$$Y/R^{2}$$

$$f_{q} = \int d^{2}x e^{iqx} f(\mathbf{x})$$

$$Y/R^{2}$$

$$q^{*} = \gamma^{1/4} / R = 1/l^{*} \qquad (\gamma = YR^{2}/\kappa)$$

Macroscopic Buckling Instability Arrested by a Wax Mandrel...

R. L. Carlson et al., Exp. Mech. 7, 281 (1962)

theory



Hutchinson, 1967

$$\ell^* = R / \gamma^{1/4} \propto \sqrt{Rh} << R$$



 $R = 4.25 in., R/h \sim 2000$

Singular Response to Thermal Fluctuations as $p \rightarrow p_c$

$$\left\langle \left| f_{\mathbf{q}} \right|^{2} \right\rangle_{0} = \frac{k_{B}T}{Y / R^{2} - pRq^{2} / 2 + \kappa q^{4}}$$

Modes with $q = 1/l^*$ unstable when

$$p \rightarrow p_c \equiv \frac{4\sqrt{\kappa Y}}{R^2}$$





Evaluate effect of nonlinearities with perturbation theory...



Effective theory including thermal corrections

$$k_{B}T\left\langle \left| f_{\mathbf{q}} \right|^{2} \right\rangle^{-1} = \kappa q^{4} + \frac{Y}{R^{2}} + \text{ corrections}$$
$$\equiv \kappa_{R}q^{4} - \sigma_{R}q^{2} + \frac{Y_{R}}{R^{2}}$$

$$Y_{R} = Y \left(1 - \frac{3}{256} \frac{k_{B}T}{\kappa} \sqrt{\frac{YR^{2}}{\kappa}} \right)$$
$$\kappa_{R} = \kappa \left(1 + \frac{61}{4096} \frac{k_{B}T}{\kappa} \sqrt{\frac{YR^{2}}{\kappa}} \right)$$
$$\sigma_{R} = \frac{1}{12\pi} \frac{k_{B}T}{\kappa} Y$$

Young's modulus is reduced

Bending rigidity is increased

A "negative surface tension" is generated from thermal fluctuations!

Effective elastic constants

$$Y_R = Y \left[1 - \frac{3}{256} \frac{k_B T}{\kappa} \left(\sqrt{\gamma} + \frac{4}{\pi} \eta \right) \right] + O(\eta^2)$$

$$\kappa_R = \kappa \left[1 + \frac{k_B T}{\kappa} \left(\frac{61}{4096} \sqrt{\gamma} - \frac{49}{1920\pi} \eta \right) \right] + O(\eta^2)$$

$$\sigma_R = -\frac{pR}{2} - \frac{k_B T}{R^2} \sqrt{\gamma} \left(\frac{1}{12\pi} \sqrt{\gamma} - \frac{21}{512} \eta \right) + O(\eta^2)$$

Young's modulus is reduced

Bending rigidity is increased

A "negative surface tension" is thermally generated

$$\gamma = YR^2 / \kappa \qquad \eta = pR^3 / 4\kappa$$

- Long- wavelength elastic constants become temperature, pressure and system-size dependent.
- Corrections <u>diverge</u> as $\gamma, R \rightarrow \infty$!
- Corrections <u>diverge</u> as $\eta/\sqrt{\gamma} \rightarrow 1$, i.e. $p \rightarrow p_c$!



Preliminary simulation results

Mean square fluctuations averaged over the sphere:

$$\begin{split} \langle \overline{f^2} \rangle &= \frac{Rk_BT}{8\sqrt{\kappa Y}} \left[1 + \left(\frac{1}{12\pi^2} - \frac{13}{8192} \right) \frac{k_BT}{\kappa} \sqrt{\frac{YR^2}{\kappa}} \right] \\ &\approx \frac{Rk_BT}{8\sqrt{\kappa Y}} \left[1 + 0.0069 \frac{k_BT}{\kappa} \sqrt{\frac{YR^2}{\kappa}} \right] \end{split}$$



How thin is thin?







(a) Polymersomes Radius, R = 10-30μm

 $R = 2 \ \mu m, h = 10 \ nm$

(b) Polyelectrolyte capsules (c) Spider silk protein capsules $R = 15 \ \mu m, h = 6 \ nm$

Thickness, h = 10 nm Bending rigidity $\kappa \sim Eh^3$ 2D Young's modulus $Y \sim Eh$ Shell radius R

E: 3D elastic modulus h: Shell thickness

Föppl-von Kármán number

$$\gamma = \frac{YR^2}{\kappa} \sim \left(\frac{R}{h}\right)^2 ~~ \sim 10^7$$

Amplitude of thermal fluctuations

~10⁻³ for 10 nm thickness

• Thermal effects scale as
$$\frac{k_B T}{\kappa} \sqrt{\gamma} \sim \frac{k_B T R^2}{E h^4}$$
.

• Corrections significantly boosted by external pressure.

How thin is thin?







(a) Polymersomes Radius, R = 10-30μm Thickness, h = 10 nm

 $R = 2 \ \mu m, h = 10 \ nm$

(b) Polyelectrolyte capsules (c) Spider silk protein capsules $R = 15-30 \ \mu m, h = 6 \ nm$

Spider silk capsules (Bausch et al Adv Mater 19:1810): Point indentation correction: Reported: R = 30 microns, h = 6 nm \rightarrow corrections < 5% Half thickness: R = 30 microns, h = 3 nm \rightarrow corrections $\sim 50\%$

• Thermal effects scale as
$$\frac{k_B T}{\kappa} \sqrt{\gamma} \sim \frac{k_B T R^2}{E h^4}$$
.

• Corrections significantly boosted by external pressure.

Pressurized Amorphous Shells, Pollen Grains and Thermal Fluctuations

Shell theory: Foppl-von Karman equations and nonlinear elasticity theory

-- applicaton to crumpling and folding of pollen grains

Flat membranes: elasticity and statistical mechanics

--thermal fluctuations lead to scale-dependent elastic constants

Shells with thermal fluctuations: deformations of pressurized spherical shells

-- Renormalized bending rigidity, Young's modulus and pressure all diverge as sphere radius $R \rightarrow \infty$!

-- Anomalous height fluctuation and indentation experiments

E. Katifori J. Dumais E. Cerda S. Alben

J. Paulose G. Gompper G. Vliegenhart