

Callisto calibration

$$V = a + b \cdot \log(c)$$

General equation describing logarithmic detector, where

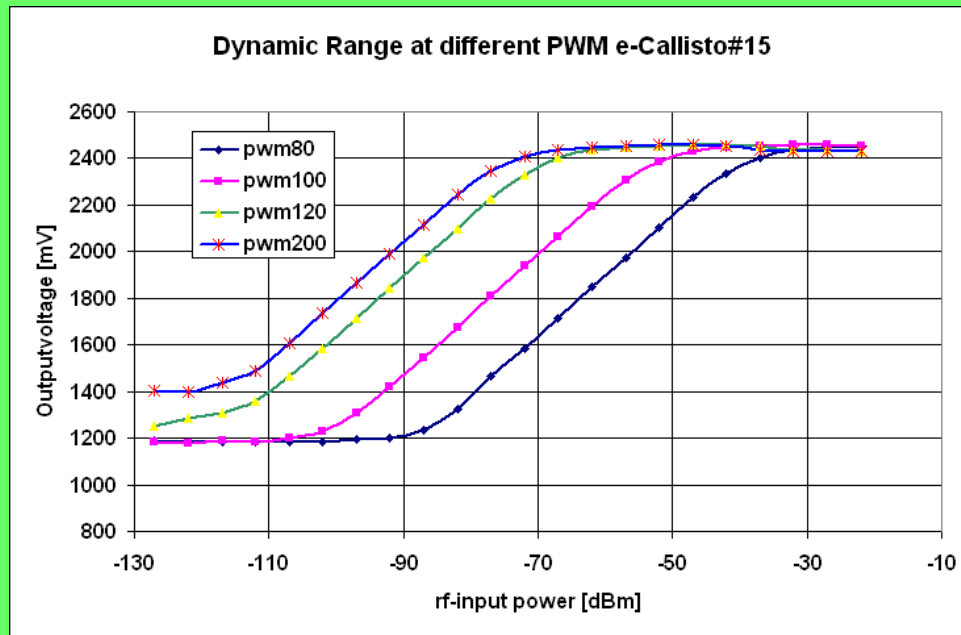
V = output voltage of the instrument -> FIT-file

a = offset voltage of the instrument

b = detector konversion constant (mV/dB)

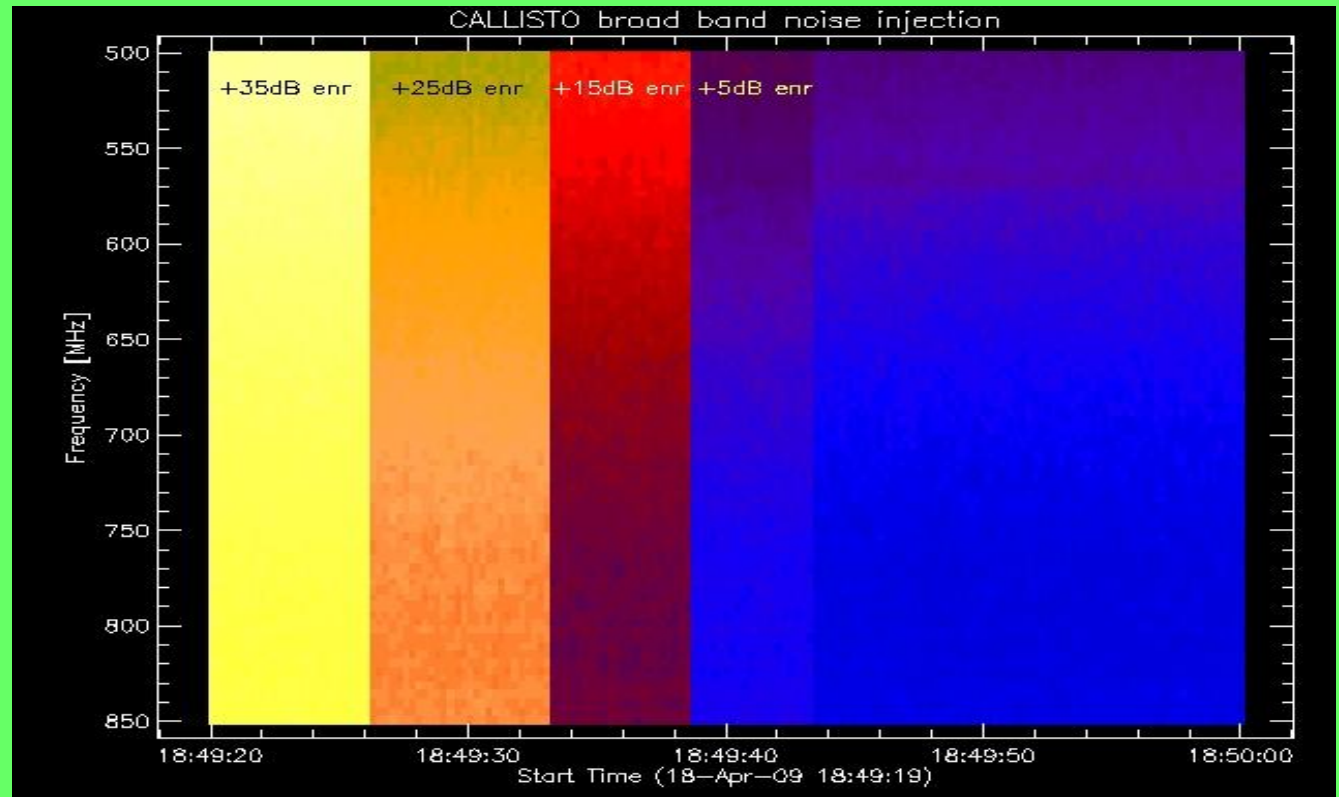
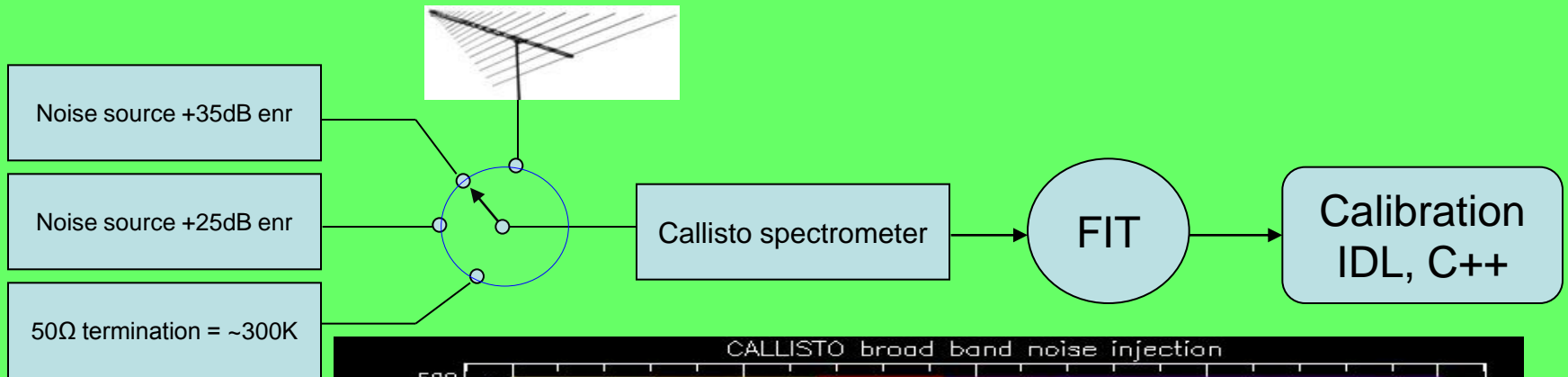
c = system temperature, where $c = T_{rx} + T_a = T_{rx} + S \cdot A_{eff} / (2 \cdot k)$ where $A_{eff} = \lambda^2 / (4\pi)$

$$c = 10^{\frac{(V-a)}{b}}$$



This equation above describes the function of the logarithmic detector. To solve this equation, we need in principle 3 independent measurements

Callisto calibration



Callisto calibration

Given

$$V_{\text{cold}} = V_0 + b \cdot \log(\text{Trx} + T_{\text{cold}}) \quad \text{50 ohm termination} = 300 \text{ K}$$

$$V_{\text{warm}} = V_0 + b \cdot \log(\text{Trx} + T_{\text{warm}}) \quad \text{Noise source 10\%} = 25 \text{ dB enr} = 94'868 \text{ K}$$

$$V_{\text{hot}} = V_0 + b \cdot \log(\text{Trx} + T_{\text{hot}}) \quad \text{Noise source 100\%} = 35 \text{ dB enr} = 948'683 \text{ K}$$

Known: V_{cold} , V_{warm} , V_{hot} , T_{cold} , T_{warm} and T_{hot}

Unknown: V_0 , b and Trx

This set of non-linear equations can not be solved mathematically correct, it can only be solved numerically

But since $\text{Trx} \sim T_{\text{cold}} \ll T_{\text{warm}} < T_{\text{hot}}$, the set of equations can be simplified. This simplification leads to a set which can be solved straight forward.

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Given

$$V_{\text{cold}} = V_0 + b \cdot \log(\text{Trx} + T_{\text{cold}}) \quad \text{50 ohm termination} = 300 \text{ K}$$

$$V_{\text{warm}} = V_0 + b \cdot \log(T_{\text{warm}}) \quad \text{Noise source 10\%} = 25 \text{ dB enr} = 94'868 \text{ K}$$

$$V_{\text{hot}} = V_0 + b \cdot \log(T_{\text{hot}}) \quad \text{Noise source 100\%} = 35 \text{ dB enr} = 948'683 \text{ K}$$

$$\text{Find}(V_0, b, \text{Trx}) \rightarrow \left[\begin{array}{c} \frac{(-V_{\text{warm}} \cdot \ln(T_{\text{hot}}) + \ln(T_{\text{warm}}) \cdot V_{\text{hot}})}{(-\ln(T_{\text{hot}}) + \ln(T_{\text{warm}}))} \\ \ln(10) \cdot \frac{(-V_{\text{hot}} + V_{\text{warm}})}{(-\ln(T_{\text{hot}}) + \ln(T_{\text{warm}}))} \\ \exp \left[\frac{-(V_{\text{cold}} \cdot \ln(T_{\text{hot}}) - V_{\text{cold}} \cdot \ln(T_{\text{warm}}) - V_{\text{warm}} \cdot \ln(T_{\text{hot}}) + \ln(T_{\text{warm}}) \cdot V_{\text{hot}})}{(-V_{\text{hot}} + V_{\text{warm}})} \right] - T_{\text{cold}} \end{array} \right]$$

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Final equation for calibration:

$$S_{\lambda} = \frac{2 \cdot k}{\lambda^2} \cdot \frac{4 \cdot \pi}{G_{\lambda}} \cdot \left[10^{\frac{(V_{\lambda} - V_{o_{\lambda}})}{b_{\lambda}} \text{ K} - T_{rx_{\lambda}}} \right]$$

Still without taking into consideration second order effects like:

- Side lobes
- Spill over
- Cable loss (antenna – switch)
- Noise temperature enhancement by physical temperature of cables (antenna – switch)

To improve, do the same on the cold sky and take the difference $S = S(\text{sun}) - S(\text{sky})$

k = Boltzmann constant

K = 1 Kelvin

λ = wavelength = c/f [m]

G = antenna gain

Trx = receiver noise temperature [K]

V = voltage at one frequency on the sky

V_o = offset voltage at the same frequency

b = detector coefficient at the same frequency

S = radio flux of sky/sun at the same frequency [sfu]