# Beamline design 

Matteo Altissimo<br>Elettra Sincrotrone Trieste SCpA<br>S.S. 14, km163.5, Basovizza (TS)

Email: matteo.altissimo@elettra.eu

## Goal of beamline design

> Design a photon transport system connecting the light source to the experimental station within a set of specific parameters:

- Photon flux
- Photon energy
- Photon energy bandwidth
- Photon beam spatial size
- ...


## Beamline design process

## Requirements

Optics
Engineering

Thermal load

Beamline length

- Flux?
- Energy?
- Energy range?
- Energy resolution?
- Spatial size?
- ...



## Tools available

- Physics side: Photons' interactions with matter
- Refraction
- Reflection
- Diffraction
- Design side: Simulators
- Ray tracers
- Wave optics
- Finite Elements

Elettra
Sincrotrone

## Quick word about simulators


C. Welnak, P. Anderson, M. Khan, S. Singh, and F. Cerrina, "Recent developments in SHADOW," Review of Scientific Instruments, vol. 63, p. 865, 1992. O. Chubar, P. E. P. O. T. E. Conference, 1998, "Accurate and efficient computation of synchrotron radiation in the near field region," accelconf.web.cern.ch L. Rebuffi, M. Sanchez del Rio, "OASYS (OrAnge SYnchrotron Suite): an open-source graphical environment for x-ray virtual xperiments", Proc. SPIE 10388 ,

103880S (2017) . DOI: 10.1117/12.2274263
L. Rebuffi, M. Sanchez del Rio, "ShadowOui: A new visual environment for X-ray optics and synchrotron beamline simulations", J. Synchrotron Rad. 23 (2016).


# A quick recap 

just to set the scene...

# Handles available for "manipulating" x-ray photons 

## Usage

Diffraction<br>$2 d \cdot \sin \theta=m \lambda$<br>$d \cong \lambda$<br>Monochromatization Focussing

Reflection $\sin \phi^{\prime}=\frac{\sin \phi}{n} \cong \frac{\sin \phi}{1-\delta} \quad \begin{array}{ll}\theta_{C} \approx \sqrt{2 \delta} \quad(\mathrm{rad}) & \begin{array}{l}\text { Transport } \\ \theta_{C} \approx 81 \sqrt{\delta} \quad(\text { degrees })\end{array} \\ \begin{array}{l}\text { Divergence corrections } \\ \text { Focussing } \\ \text { Basic energy filtering }\end{array}\end{array}$

$$
\begin{array}{lll}
\text { Refraction } & n=1-\delta+i \beta & \begin{array}{l}
\delta=10^{-1} \div 10^{-6} \\
\beta=10^{-1} \div 10^{-8}
\end{array}
\end{array}
$$

Focussing

## Synchrotron beam emitted by source

$$
\gamma=1957 \mathrm{E}_{\mathrm{e}}[\mathrm{GeV}]
$$



$$
\text { For a typical experiment: required beam size } \sim 0.1 \text { to } 10 \text { 's of } \mu \mathrm{m} \text { or more }
$$

## A couple of undulator simulations $\mathrm{E}_{\mathrm{e}}=2.4 \mathrm{GeV}, \mathrm{N}=17$, period $=56 \mathrm{~mm}$, first harmonic only

Source Size



Divergence




Beam 20 m from source

M. Altissimo, 16th January 2024

## It's even more complicated...

$$
\mathrm{E}_{\mathrm{e}}=2.4 \mathrm{GeV}, \mathrm{~N}=17, \text { period }=56 \mathrm{~mm}
$$



Total flux $\sim 10^{19} \mathrm{ph} / \mathrm{s}$

## So what am I going to talk about??

- Mirrors for X-rays
- Basics of diffracting elements
- Monochromators for X-rays
- The thermal load issue


## Mirrors for x-rays

Transport<br>Divergence corrections<br>Focussing<br>Basic energy filtering

## Some nomenclature



Tangential/Meridian direction

## Mirror figures used in synchrotron beamlines

## Some numbers

| Plane | Re-direction/filtering | $R>100 \mathrm{~km}$ |
| :--- | :---: | :---: |
| Cylindrical | 1D focusing | $R \sim 100$ 's m |
| Spherical | 2D focusing | $R \sim 100$ 's m |
| Paraboloid | Infinity to point <br> (or viceversa) | $a \sim \mathrm{~cm}, \mathrm{f} \sim \mathrm{m}$ |
| Elliptical | Point to point focusing | $r \gg r^{`}$ |
| Toroidal | Astigmatic focusing | $R \sim 100 \mathrm{~m}, \rho \sim 10$ 's cm |

All this with a surface rms roughness $\sim \mathrm{nm}$ or less

## A quick look at reflectivities

$$
\theta_{c}=\sqrt{2 \delta} \propto \lambda \sqrt{Z}
$$

Au Reflectivity


Si Reflectivity


The higher the energy, the more grazing the incidence angle ( $1 \mathrm{mrad}=0.057^{\circ}, 1^{\circ}=17 \mathrm{mrad}$ )

## Source for examples

## Spatial Dimensions:

$$
\sigma_{x}=48 \mu m \quad \sigma_{z}=1.3 \mu m
$$

FWHM $(X)=105 \mu \mathrm{~m} \operatorname{FWHM}(Z)=3 \mu \mathrm{~m}$


## Angular dimensions:

$$
\sigma_{x}^{\prime}=3.8 \mu \mathrm{rad} \quad \sigma_{z}^{\prime}=1.82 \mu \mathrm{rad}
$$

FWHM $\left(X^{\prime}\right)=8.6 \mu \mathrm{rad} \operatorname{FWHM}\left(Z^{\prime}\right)=4.2 \mu \mathrm{rad}$


Plane mirror, $\mathrm{r}=20 \mathrm{~m}, \mathrm{r}^{\prime}=20 \mathrm{~m}, \theta=88^{\circ}$

Spatial Dimensions:



Angular dimensions:


FWHM $\left(X^{\prime}\right)=8.6 \mu \mathrm{rad} \operatorname{FWHM}\left(Z^{\prime}\right)=4.2 \mu \mathrm{rad}$

## Toroidal mirror: focussing properties

$\left(\frac{1}{r}+\frac{1}{r^{\prime}}\right) \frac{\cos \theta}{2}=\frac{1}{R} \quad$ Tangential focusing

$$
R>\rho
$$

$\left(\frac{1}{r}+\frac{1}{r^{\prime}}\right) \frac{1}{2 \cos \theta}=\frac{1}{\rho} \quad$ Sagittal focusing

Tangential focus

$$
\begin{aligned}
f_{t} & =\frac{R \cdot \cos \theta}{2} \\
f_{s} & =\frac{\rho}{2 \cos \theta}
\end{aligned}
$$

Condition for a stigmatic image of a point source:

$$
\frac{\rho}{R}=\cos ^{2} \theta
$$

## Toroidal mirror, $\mathrm{r}=20 \mathrm{~m}, \mathrm{r}^{\prime}=10 \mathrm{~m}, \theta=88^{\circ}$

$$
\begin{aligned}
& R=\left(\left(\frac{1}{r}+\frac{1}{r^{\prime}}\right) \frac{\cos \theta}{2}\right)^{-1}=382 \mathrm{~m} \rho=\left(\left(\frac{1}{r}+\frac{1}{r^{\prime}}\right) \frac{1}{2 \cos \theta}\right)^{-1}=0.23 \mathrm{~m} \\
& f_{t}=\frac{R \cdot \cos \theta}{2}=6.6 \mathrm{~m} \quad f_{s}=\frac{\rho}{2 \cos \theta}=3.3 \mathrm{~m} \\
& \text { Tangential focus } \\
& \text { Sagittal focus }
\end{aligned}
$$

$\operatorname{FWHM}(X)=333 \mu \mathrm{~m} \operatorname{FWHM}(Z)=1.5 \mu \mathrm{~m}$

## Spherical mirrors

## Same as toroidal mirrors with:

$$
\begin{array}{ccc}
R=\rho & f_{t}=\frac{R \cdot \cos \theta}{2} \\
\left(\frac{1}{r}+\frac{1}{r^{\prime}}\right) \frac{\cos \theta}{2}=\frac{1}{R} & \left(\frac{1}{r}+\frac{1}{r^{\prime}}\right) \frac{1}{2 \cos \theta}=\frac{1}{R} & f_{s}=\frac{R}{2 \cos \theta}
\end{array}
$$

A stigmatic image is only possible if:

$$
\frac{\rho}{R}=\cos ^{2} \theta=1
$$

i.e. this is possible only for normal incidence!

## Paraboloidal mirror

<- To source

$$
Y^{2}=4 \cdot a \cdot X
$$



$$
P\left(X_{0}, Y_{0}\right):
$$

$$
X_{0}=a \cdot \tan ^{2} \theta
$$

$$
Y_{0}=2 a \cdot \tan \theta
$$

$$
f=\frac{a}{\cos ^{2} \theta}
$$

## Parabola parameter $a=f \cos ^{2} \theta=0.02435 \mathrm{~m}$

## Source image @ 20 mt



FWHM (X) $=860 \mu \mathrm{~m}$ FWHM $(Z)=864 \mu \mathrm{~mm}$
FWHM ( $X^{\prime}$ )=8.6 $\mu \mathrm{rad} \operatorname{FWHM}\left(Z^{\prime}\right)=4.2 \mu \mathrm{rad}$

Paraboloidal Mirror image


FWHM $(X)=172 \mu \mathrm{~m}$ FWHM $(Z)=83 \mu \mathrm{~m}$
FWHM $\left(X^{\prime}\right)=5.2 \mu \mathrm{rad}$ FWHM $\left(Z^{\prime}\right)=0.1 \mu \mathrm{rad}$

## Ellipsoidal mirror



Ellipsoidal mirror, $\mathrm{r}=20 \mathrm{~m}, \mathrm{r}^{\prime}=5 \mathrm{~m}, \theta=88^{\circ}$

$$
\mathrm{a}=12.5 \mathrm{~m}, \mathrm{~b}=0.349 \mathrm{~m}, \mathrm{e}=0.999610
$$

Our source dimensions are: $\operatorname{FWHM}(X)=105 \mu \mathrm{~m} \operatorname{FWHM}(Z)=3 \mu \mathrm{~m}$

$$
M=\frac{r^{\prime}}{r}=0.25
$$

i.e. we expect a focus of $\sim 26 \times 0.75 \mu \mathrm{~m}$ (FWHM)

$\operatorname{FWHM}(X)=26 \mu \mathrm{~m} \operatorname{FWHM}(Z)=0.7 \mu \mathrm{~m}$

## WARNING!

All the simulations above are for educational purposes!

- Reflectivity set to 1 , and independent of energy
- Ideal source
- No mirror errors (roughness, figure errors, etc)


Elettra
Sincrotrone
Trieste

http://www.esrf.eu/home/UsersAndScience/Experiments/ CBS/ID09/OpticsHutch/mirror.html

http://www.crystal-scientific.com/ mirror_plano.html
R. Radhakirshnan et al, DOI 10.1149/07711.1255ecst

School on Synchrotron Light Sources and their Applications, ICTP Trieste (remote)


# Diffracting elements 

Gratings<br>Crystals<br>Multilayers<br>Zone Plates

Monochromatization Focussing

# Usage: <br> Overwhelmingly for monochromatization 

| Micro <br> wave | I.R. | Visible | U.V. | Soft <br> X-ray | Hard <br> X-ray |
| :--- | :---: | :---: | :---: | :--- | :--- |


| Micro <br> wave | I.R. | Visible | U.V. | Soft <br> X-ray | Hard <br> X-ray |
| :--- | :--- | :--- | :--- | :--- | :--- |



Grating


## Diffraction gratings

Artificial periodic structure, with a precisely defined period d.


Grating equation
$\sin \alpha+\sin \beta=L m \lambda$
$m$ is the diffraction order
$\alpha$ and $\beta$ have opposite signs if on opposite side of the surface normal

## Grating resolving power

Angular dispersion of a grating with line density $\mathrm{L}: \quad \Delta \lambda=\frac{s^{\prime} \cos \beta}{L m r^{\prime}}$
Resolving power $\mathrm{R}: \quad R=\frac{E}{\Delta E}=\frac{\lambda}{\Delta \lambda}=\frac{\lambda L m r^{\prime}}{s^{\prime} \cos \beta}$


## Crystals

Based on Bragg's law: $\quad 2 d \sin \theta=m \lambda$


Since $\sin \theta \leq 1, \lambda \leq \lambda_{\text {MAX }}\left(E \geq E_{\text {MIN }}\right)=2 \mathrm{~d}$
$\operatorname{Si}(111): d=3.13 \AA\left(E_{\text {Min }} \sim 2 k e V\right) \quad S i(311): d=1.64 \AA\left(E_{\text {MIN }} \sim 3.8 k e V\right)$ $\operatorname{lnSb}(111): d=3.74 \AA\left(E_{\text {MIN }} \sim 1.7 \mathrm{keV}\right)$

## Crystals' resolving power



$$
\begin{aligned}
& \frac{\Delta E}{E}=\frac{\Delta \lambda}{\lambda}=\Delta \theta \frac{\cos \theta}{\sin \theta} \\
& \text { Angular spread }
\end{aligned}
$$

Where does $\Delta \theta$ come from?
$\Delta \theta_{\text {beam }} \quad$ Angular divergence of the incoming beam
$\omega_{\text {crystal }} \quad \begin{gathered}\text { Intrinsinc width of Bragg reflection, } \\ \text { the Darwin curve }\end{gathered}$

* more on this later...


## Multi-layer mirrors



$$
\omega_{s}=\omega_{i}+\omega_{d}
$$

$\mathbf{k}_{\mathrm{s}}=\mathbf{k}_{\mathbf{i}}+\mathbf{k}_{\mathrm{d}}$
But $\omega_{d}=0$, therefore:

$$
\begin{aligned}
& \left|\mathbf{k}_{\mathbf{s}}\right|=\left|\mathbf{k}_{\mathbf{i}}\right|=2 \pi / \lambda \\
& \sin \theta=\frac{k_{d} / 2}{k_{i}}
\end{aligned}
$$

## $\lambda=2 d \sin \theta$

D. Attwood, $X$-Rays and Extreme Ultraviolet Radiation,Cambridge University Press, 2017

## Multi-layer mirrors

What if $n_{a}(z)$ is still periodic, but not a simple sinusoid?


Elettra
Sincrotrone
Trieste

## Multi-layer mirrors

W/C, d=22.3 A, $\Gamma=0.5, N=100$




## Monochromator

## The need for collimated illumination

Crystals Energy resolution:

$$
\frac{\Delta E}{E}=\frac{\Delta \lambda}{\lambda}=\Delta \theta \frac{\cos \theta}{\sin \theta}
$$

Same for multilayers
Gratings

$$
\frac{\Delta E}{E}=\frac{\Delta \lambda}{\lambda}=\frac{\cos \beta}{\lambda L m r^{\prime}} \Delta \beta
$$




Undulator

5th Harmonic ( $\sim 1 \mathrm{keV}$ ) $\Delta \mathrm{E}=500 \mathrm{eV}$

## The need for collimated illumination

Collimating mirror before monochromator


Mirror calculated setting virtual source distance (r) very far (~100s m)

* more on this later...


## Double Crystal Monocromator (DCM)

$$
2 d \sin \theta=m \lambda
$$

$$
\frac{\Delta E}{E}=\frac{\Delta \lambda}{\lambda}=\Delta \theta \frac{\cos \theta}{\sin \theta}
$$

## Parallel geometry

All rays accepted by first crystal are accepted also by the second

Second crystal acts merely as a mirror

## DCM in parallel configuration



Elettra
Sincrotrone
Trieste

## DCM in parallel configuration



Elettra
Sincrotrone
Trieste

## DCM in parallel configuration



## DCM in parallel configuration



## 2 X DCM in parallel configuration



## Plane grating monochromator

Concept of the plane grating monochromator


## Plane grating monochromator



## Something to keep in mind: thermal loads!

Source


Spectrum



~ 100's W
~few kW
~0.1-1 kW

From first mono element standpoint: kW in, NOTHING out!

## Thermal load issues (besides melting)

$Q$ is the incoming power, $D$ the mirror/crystal thickness


## Silicon vs Copper Thermal conductivity



M White et al 2014 Metrologia 51 S245

## ... finally a couple of examples

## TwinMic Beamline @ Elettra

## Photon energy: 400 eV to 2 keV X-ray microscopy and microFluorescence

Undulator source $\mathrm{N}=17$
Period $=56 \mathrm{~mm}$
Min gap: 25 mm

| Cylindrical mirror |
| :--- |
| 16 m from source |
| Au coated |
| $\rho=0.56 \mathrm{~m}$ |
| $\theta=1 \mathrm{deg}$ |

Toroidal mirror
20 m from source
Au Coated
$\mathrm{R}=211 \mathrm{~m}$
$\rho=0.07 \mathrm{~m}$
$\theta=1 \mathrm{deg}$

Entrance slit
12.6 m from source
$\mathrm{D}=1 \mathrm{~mm}$

PGM with plane pre-mirror 18 m from source
Blazed grating, $\theta_{b}=1.1 \mathrm{deg}$ Au coated
$\mathrm{L}=600 \mathrm{I} / \mathrm{mm}$

Secondary source 22 m from source $5-100 \mu \mathrm{~m}$ diameter

Zone Plate $\mathrm{D}=600 \mu \mathrm{~m}$
Res 50 nm
24 m from source

Experiment
$\sim 24.5 \mathrm{~m}$ from source
Focal spot dia:
100 nm to $1.5 \mu \mathrm{~m}$

## Diffraction Beamline @ Elettra

## Photon energy: 4 to 21 keV

Cylindrical mirror for vertical collimation
22 m from source
Pt Coated
$\mathrm{R}=14 \mathrm{~km}$
$\theta=0.172 \mathrm{deg}$

Multi-pole wiggler
$\mathrm{N}=54$, 1.5 T mag field
Period $=140 \mathrm{~mm}$
Critical Energy: 5.8keV @ 2.4GeV 5 kW total power @ 140 mA

Toroidal focussing mirror 28 m from source
Sagittally cylindrical, bendable $\mathrm{R}=9 \mathrm{~km}$ ( 5 km to $\infty$ )
$\rho=0.055 \mathrm{~m}$

Experiment 41.5 m from source Focal spot:
$0.7 \times 0.2 \mathrm{~mm}^{2}$
$\Delta \mathrm{E} / \mathrm{E} \sim 4000$

Double crystal mono
24 m from source
$\mathrm{Si}(111), \omega_{\mathrm{s}}=25 \mu \mathrm{rad} @ 8 \mathrm{keV}$

## Thank you!

