

#### **Volcanic Processes: a Variety of Length and Time Scales**

# Rheology of Crystal-Rich Magmas

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Background and Summary



Database



Generalizing Costa et al. (2009) model



Application to test cases



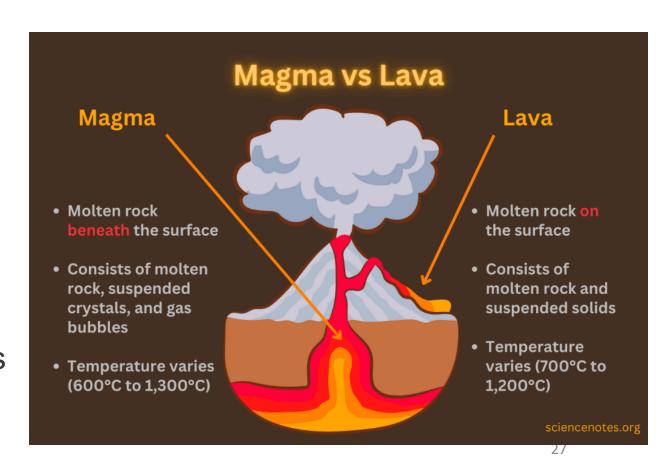
Conclusion

# Magma is liquid rock with crystals. Approaching the surface, gas bubbles form as pressure drops, so magma can contain solid, liquid, and gas.

Magma = liquid rock + crystals

 Pressure drops near surface → gases bubble out

Magma becomes solid + liquid + gas





#### It's all about *viscosity*

- Melt composition
- Temperature
- Crystals (content, shape, size distribution)
- Strain rate
- Vesicles

• ...

It can vary over 20 orders of magnitude!



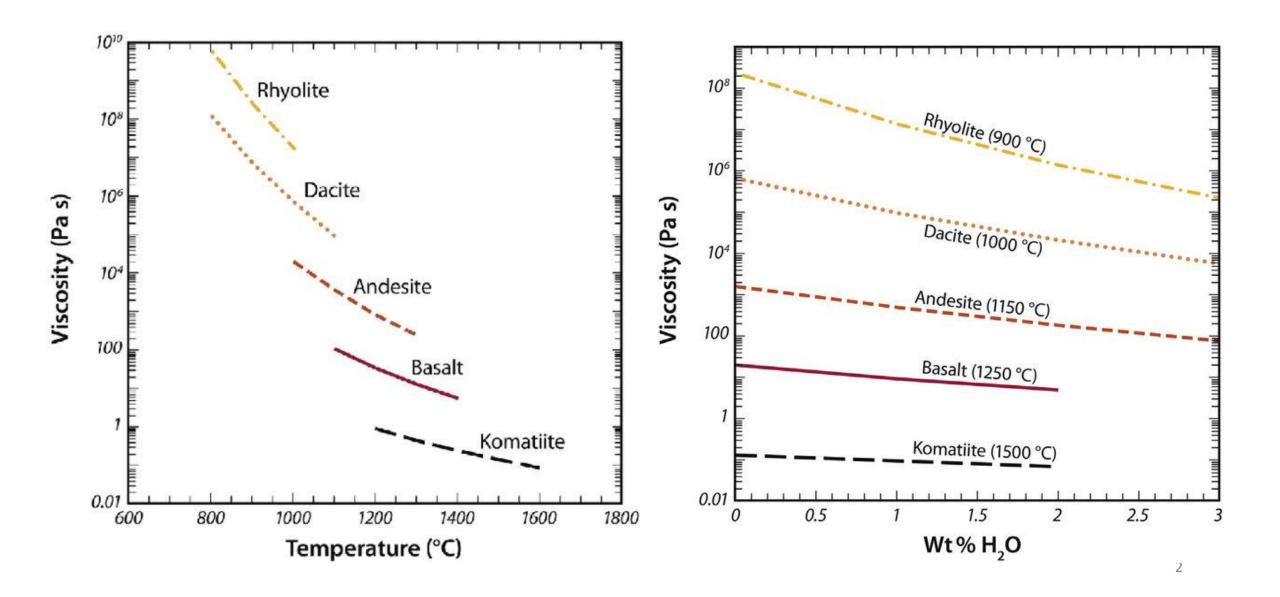
from Etna Volcano Live Webcam



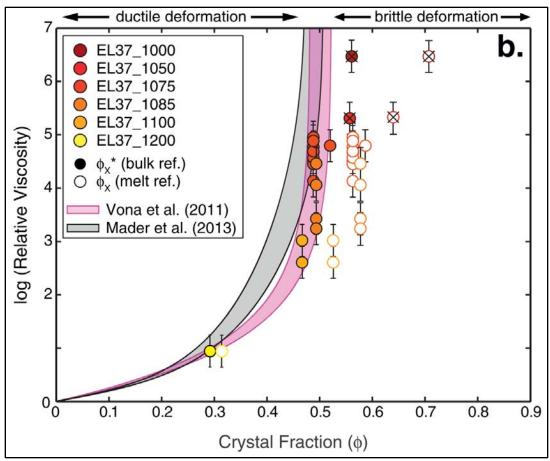


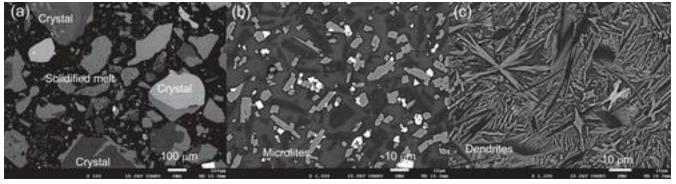
All this contributes to the different responses of magma rheology and eruption styles!

#### Melt viscosity (e.g., Spera, 2000; Giordano, Russell, Dingwell, 2008)



Rheological literature





Namiki et al. (2025). Crystal-rich magma is solid-like and liquefies when deformed. J. Geophys. Res., 130, e2024JB030483.

Relative viscosity = magma viscosity/melt viscosity ( $\eta_m/\eta_l$ )

Relative viscosity increase with the solid phase concentration

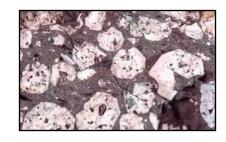
No focus on rheology above critical crystal fraction (e.g. maximum packing fraction)!

Many studies... but no systematic results on strain rate and Aspect Ratio!

Focusing on particle-bearing systems rheology:

- Database from rheological literature covering all the natural volcanic parameters.

Low R



High R



- Systematic model of relative viscosity  $(\eta_r)$  as function of :
- apparent viscosity  $\eta_a$
- melt viscosity  $\eta_l$
- crystal concentration  $\phi$
- crystal shape R
- and strain rate  $\dot{\varepsilon}$

Low  $\dot{\varepsilon}$ 



High ε



- Quantitative description of the rheological behavior of crystal-bearing magmatic systems.

Sigmoidal shape proposed by Lejeune and Richet (1995) and then described by Costa et al. (2007,2009):

$$\eta_r(\phi) = \frac{1 + \varphi^{\delta}}{[1 - F(\varphi, \varepsilon, \gamma)]^{B\phi_*}}$$

$$\eta_r(\phi) = \frac{1 + \varphi^{\delta}}{[1 - F(\varphi, \varepsilon, \gamma)]^{B\phi_*}} \qquad F = (1 - \xi) \operatorname{erf}\left[\frac{\sqrt{\pi}}{2(1 - \xi)}\varphi(1 + \varphi^{\gamma})\right] \qquad R = 1 \text{ only!}$$

B = Einstein coefficient = 2.5

 $\varphi = \phi/\phi_* \rightarrow \phi =$ solid fraction

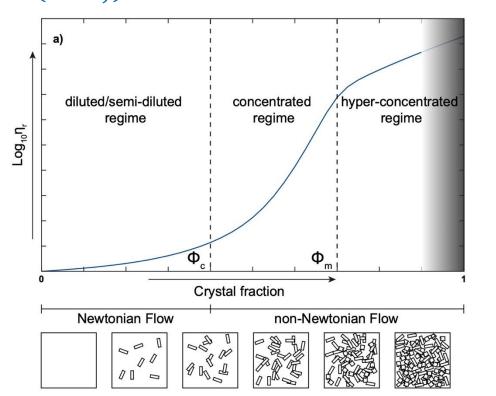
 $\phi_*$  = critical solid fraction

 $\gamma$  = steepness of the curve near  $\phi_*$ 

 $\delta$  and  $\xi$  = steepness and height

of the iper-concentrated region

erf = error function



Four different flow regimes: diluted, semi-diluted, concentrated and hyper-concentrated

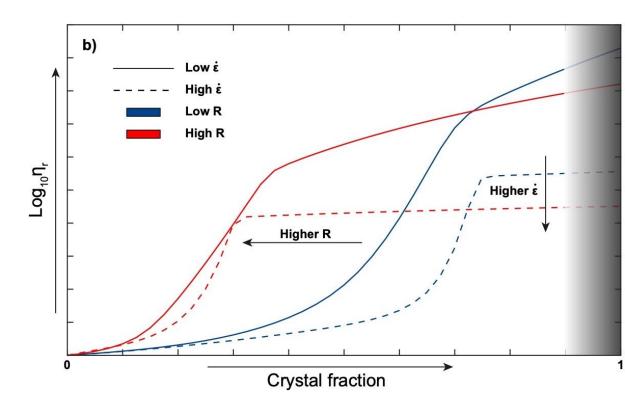
Viscosity varies with particles shape and strain rate!



Spherical (Leucite)

Elongated (Plagioclase)





- Different elongation of crystals in nature
- Need to take into account the elongation (Aspect Ratio R)

Database: construction (over 1400 rheological data) and classification

- Material type (natural, synthetic or analogue)
- Chemical composition
- Experimental methodology
  - Temperature
  - Applied strain rate
  - Confining pressure
- The phase components
  - Crystal content and mean aspect ratio R

#### Results:

- Apparent viscosity  $\eta_a$
- Melt viscosity  $\eta_1$
- Relative viscosity  $\eta_r = \eta_a / \eta_1$

Data correction

Common issues in reporting data:

➤ Deformation mechanisms;

$$\eta_{eff} = \frac{\sigma}{\dot{\varepsilon}}$$
 VS  $\eta_{eff} = \frac{m g h^2}{3V \frac{\delta h}{\delta t}}$ 

➤ Relative viscosity of NATURAL SAMPLES experiments;

Natural vs residual melt

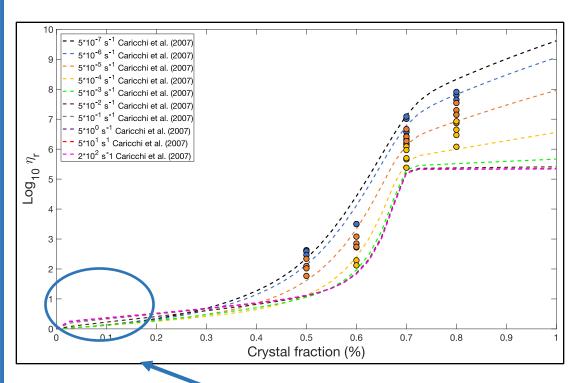
➤ Missing information

 $(R, \dot{\mathcal{E}}, Chemistry and/or T...)$ 

ightharpoonup Viscous heating For high particle fraction, high <math>R and high  $\dot{\mathcal{E}}$ 

Spherical particles and wide range of strain rates

$$\delta = \delta_m - \Delta \delta \longrightarrow \delta_m = 7.73$$
 (previously 6.78)



Avoid sharp increase at very low particle concentration

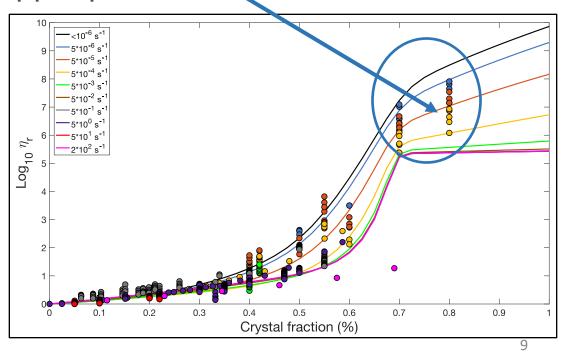
$$\phi_{\rm e}(\dot{\varepsilon}, R) = \left[\phi_{\rm en} + \Delta\phi \frac{(\dot{\varepsilon}/\varepsilon_{\rm c})^n - (\varepsilon_{\rm c}/\dot{\varepsilon})^n}{(\dot{\varepsilon}/\varepsilon_{\rm c})^n + (\varepsilon_{\rm c}/\dot{\varepsilon})^n}\right]$$

$$\delta(\dot{\varepsilon}, R) = \left[\delta_m - \Delta \delta \frac{(\dot{\varepsilon}/\varepsilon_c)^n - (\varepsilon_i/\dot{\varepsilon})^n}{(\dot{\varepsilon}/\varepsilon_c)^n + (\varepsilon_c/\dot{\varepsilon})^n}\right]$$

$$\xi(\dot{\varepsilon}, R) = \left[ \xi_m + \Delta \xi \frac{(\dot{\varepsilon}/\varepsilon_c)'' - (\varepsilon_c/\dot{\varepsilon})''}{(\dot{\varepsilon}/\varepsilon_c)'' + (\varepsilon_c/\dot{\varepsilon})''} \right]$$

$$\gamma(\dot{\varepsilon}, R) = \left| \gamma_m + \Delta \gamma \frac{(\dot{\varepsilon}/\varepsilon_c)^n - (\varepsilon_c/\dot{\varepsilon})^n}{(\dot{\varepsilon}/\varepsilon_c)^n + (\varepsilon_c/\dot{\varepsilon})^n} \right|$$

Better fit for the upper plateau

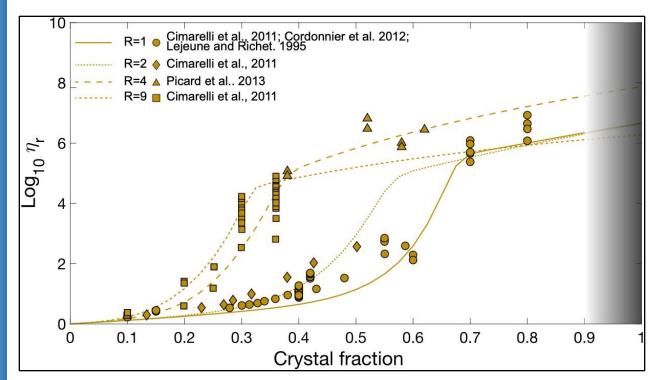


$$\phi_*(\dot{\varepsilon} = 10^{-4} \ s^{-1}; R) = \left(\frac{1}{R^{b_1}}\right) \phi_s \ (10^{-4} \ s^{-1})$$

$$\delta(\dot{\varepsilon} = 10^{-4} \, s^{-1}; R) = \delta_m e^{b_2(R-1)} (10^{-4} \, s^{-1})$$

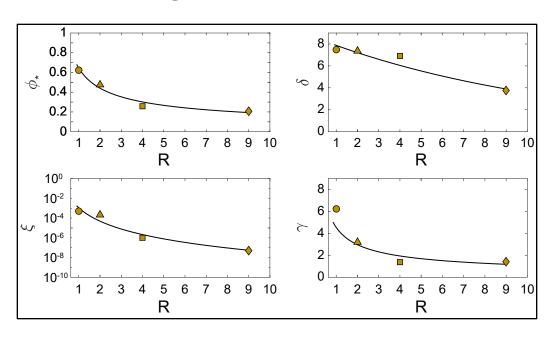
$$\xi(\dot{\varepsilon} = 10^{-4} \, s^{-1}; R) = \left(\frac{1}{R^{b_3}}\right) \xi_m \, (10^{-4} \, s^{-1})$$

$$\gamma(\dot{\varepsilon} = 10^{-4} \ s^{-1}; R) = \left(\frac{1}{R^{b_4}}\right) \gamma_m \ (10^{-4} \ s^{-1})$$



$$\dot{\varepsilon} = 10^{-4} \text{ s}^{-1}$$

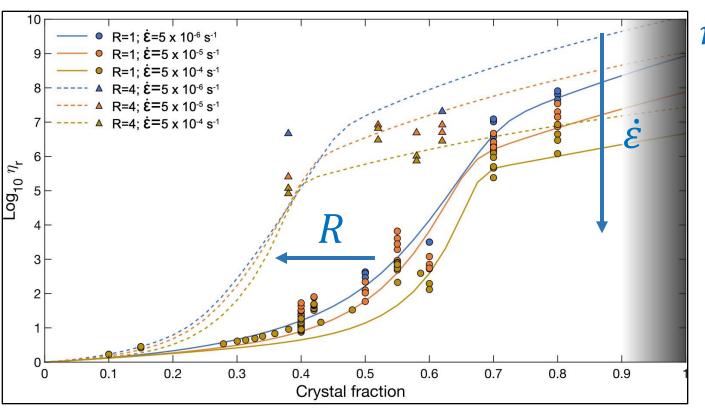
#### Entire range of R



$$b_1 = 0.538$$
  $b_2 = 0.092$ 

$$b_3 = 4.568$$
  $b_4 = 0.718$ 

- High crystal fraction plateau-like relative viscosity region
- For a given R, this plateau-like region is higher as the strain rate decreases
- For a given *strain rate*, the curves are shifted towards the lower crystal fractions as *R* increases.



$$\eta_r(\dot{\varepsilon}, R) = \frac{1 + \varphi^{\delta(\dot{\varepsilon}, R)}}{[1 - F(\dot{\varepsilon}, R)]^{B\phi_*(\dot{\varepsilon}, R)}}$$

$$\phi_{\rm e}(\dot{\varepsilon},R) = \left[\phi_{\rm en} + \Delta\phi \frac{(\dot{\varepsilon}/\varepsilon_{\rm c})^n - (\varepsilon_{\rm c}/\dot{\varepsilon})^n}{(\dot{\varepsilon}/\varepsilon_{\rm c})^n + (\varepsilon_{\rm c}/\dot{\varepsilon})^n}\right] * R^{-b_1}$$

$$\delta(\dot{\varepsilon}, R) = \left[\delta_m - \Delta \delta \frac{(\dot{\varepsilon}/\varepsilon_c)^n - (\varepsilon_c/\dot{\varepsilon})^n}{(\dot{\varepsilon}/\varepsilon_c)^n + (\varepsilon_c/\dot{\varepsilon})^n}\right] * e^{-\delta_2(R-1)}$$

$$\xi(\dot{\varepsilon}, R) = \left[ \xi_m + \Delta \xi \frac{(\dot{\varepsilon}/\varepsilon_c)'' - (\varepsilon_c/\dot{\varepsilon})''}{(\dot{\varepsilon}/\varepsilon_c)'' + (\varepsilon_c/\dot{\varepsilon})''} \right] * R^{-b_3}$$

$$\gamma(\dot{\varepsilon}, R) = \left[ \gamma_m + \Delta \gamma \frac{(\dot{\varepsilon}/\varepsilon_c)^n - (\varepsilon_c/\dot{\varepsilon})^n}{(\dot{\varepsilon}/\varepsilon_c)^n + (\varepsilon_c/\dot{\varepsilon})^n} \right] * R^{-b_4}$$

#### **Conclusion and future work**

Building wide rheological database:

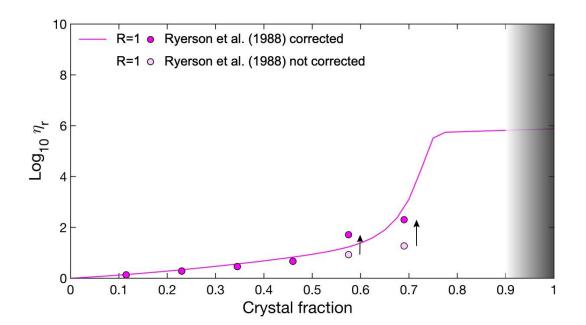
https://doi.org/10.6084/m9.figshare.16886155.v1

- Identification of issues in reporting data
- Extension of the model of Costa et al. (2009) to all the natural strain rates ( $\dot{\varepsilon}$ ) for spherical particles (R=1)
- Generalization of the model for all the aspect ratios (R) and strain rates ( $\dot{\varepsilon}$ ) pertinent to natural environment

#### **Conclusion and future work**

#### Scientific community should:

- adopt measurement standardization
- fill the gaps in the poorly characterized parameter space;
- carry experiments to characterize viscous dissipation effects (e.g. focusing on the regime explored by Ryerson et al., 1988)



$$T_{\text{max}} - T_0 = \ln (\text{Na})/b$$

 $T_{\text{max}}$ = max temperatura

 $T_0$  = considered temperature

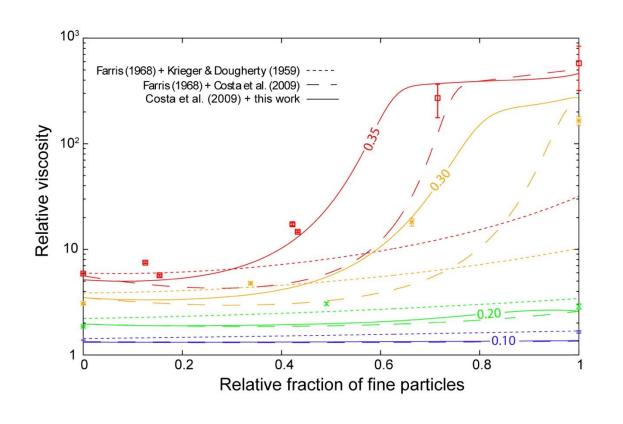
*Na* = Nahme number

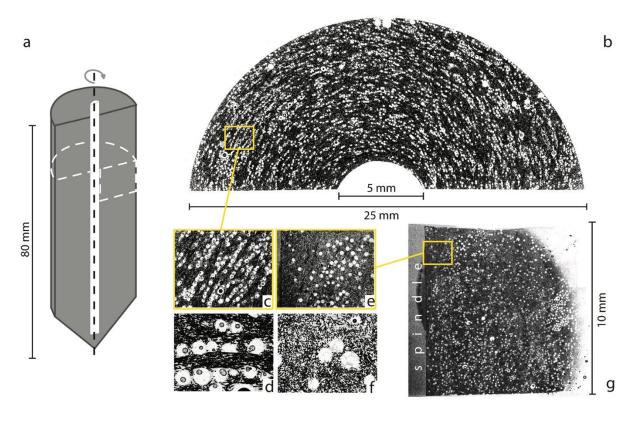
*b* = rheological sensitivity to temperature

#### **Conclusion and future work**

#### Scientific community should:

• better characterizing the effects of crystal-size distribution (fine vs coarse), fluid-solid interactions, and hysteresis relevant for elongated particles (Cimarelli et al., 2011)





# For further information:

www.nature.com/scientificdata

#### scientific data



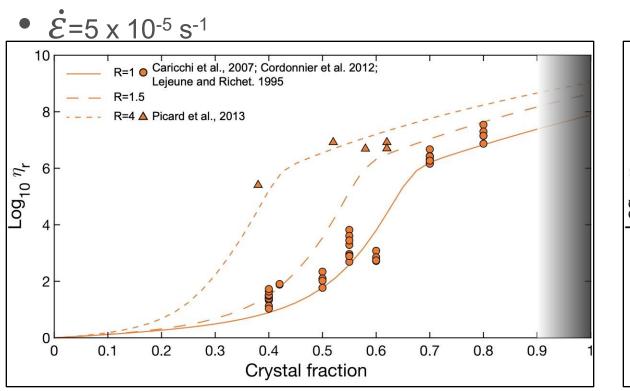


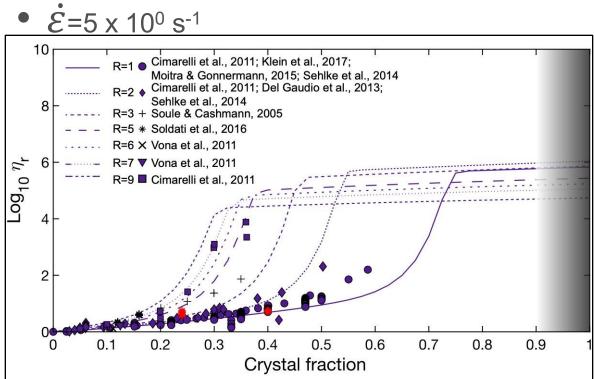
## **OPEN** A comprehensive database of DATA DESCRIPTOR crystal-bearing magmas for the calibration of a rheological model

Alessandro Frontoni 601 M., Antonio Costa 602, Alessandro Vona 601 & Claudia Romano1

In this work, we present a comprehensive rheological database including most of the existing data relevant for crystal-bearing magmas collected from the scientific literature, covering the entire range of natural volcanic conditions, in terms of crystal content (1–80%), crystal shape (aspect ratio R from 1 to 13), and strain rate (between  $10^{-7}$  and  $10^2$  s<sup>-1</sup>). Datasets were collected and discerned as a function of the information which we considered necessary for building a general systematic model describing relative viscosity of crystal-bearing magmas, such as the apparent and melt viscosity, the crystal concentration, crystal shape, and the strain rate. The selected dataset was then used for modelling the relative viscosity of a liquid-solid mixture having different concentrations of particles with different R, subjected to different strain rates. The proposed model allows us to quantitatively describe the rheological behaviour of crystal-bearing magmatic systems.

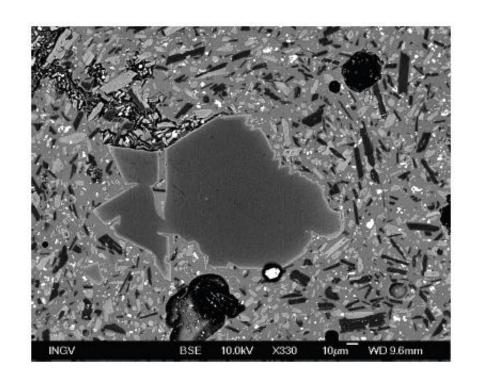
Thank you for your attention!

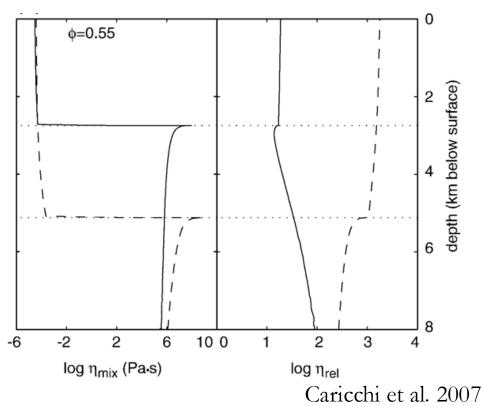




Application to <u>all the strain rates</u>, crystal content and aspect ratios of volcanological interest!

#### Rationale





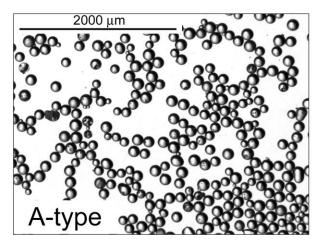
Complex history of crystallization (microlites + phenocrysts)

Increasing crystallinity changes rheology (non-Newtonian)

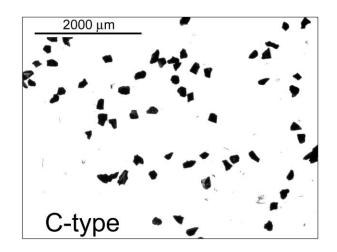
Influence on magma flow and eruptive style.

# Analogues

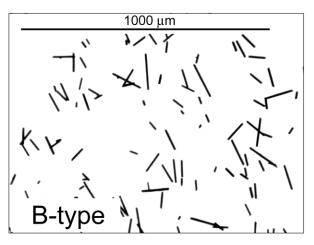
#### Suspensions of particles in Newtonian silicone oil



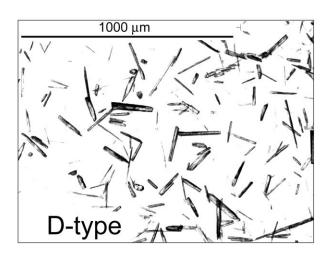
glass beads:  $\geq 2.448 \text{ g/cm}^3$ ; d=125 m



SiC grit:  $\geq 3.166 \text{ g/cm}^3$ ; r=1.8



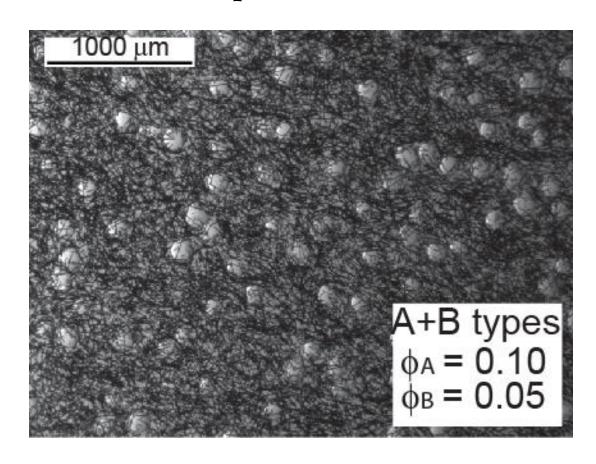
carbon fibres:  $\geq 1.740 \text{ g/cm}^3$ ; r=9.05



wollastonite:  $\geq 2.750 \text{ g/cm}^3$ ; r=8.50

# **Analogues**

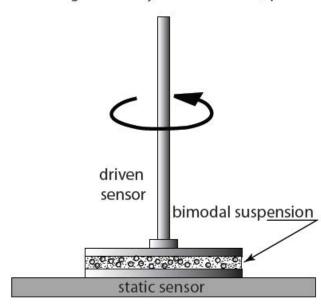
Bimodal suspensions of particles with different shape and size

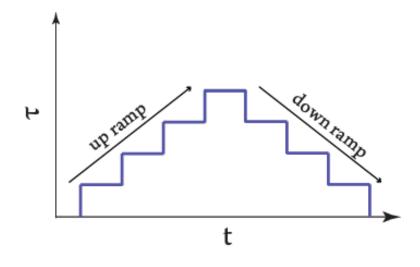


#### Measurements

#### Parallel Plate sensor system

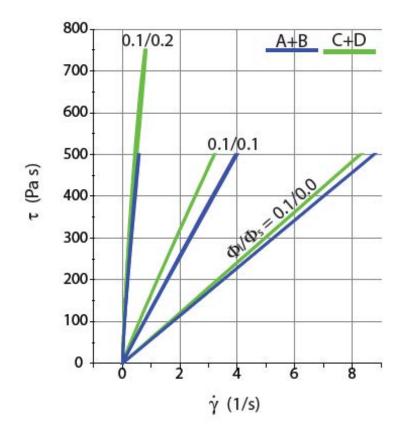
Torque, M  $\rightarrow$  Stress,  $\tau$ Angular velocity,  $\Omega \rightarrow$  Strain rate,  $\dot{\gamma}$ 





#### Measurements

Flow curve 
$$\tau = f(\gamma)$$



$$\boldsymbol{\tau} = \boldsymbol{\tau}_0 + \boldsymbol{K} \dot{\boldsymbol{\gamma}}^n$$

Herschel-Bulkley model

 $l_0$ : yield strength (Pa)

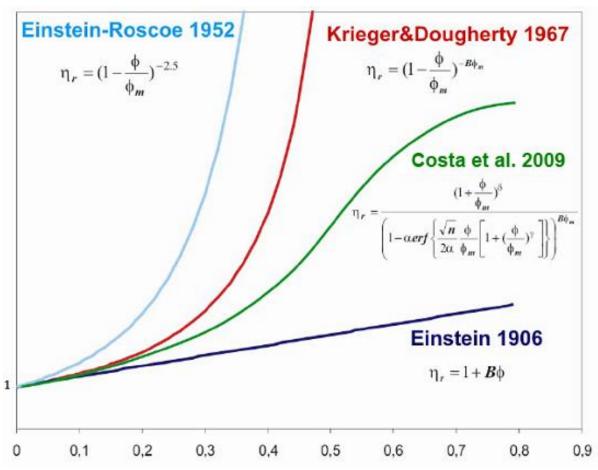
K: consistency (Pa s<sup>n</sup>)

n: flow index

effective relative viscosity

$$\eta_r \equiv \frac{1}{\mu_l} \left( \frac{\tau - \tau_0}{\dot{\gamma}} \right) = \frac{K \dot{\gamma}^{n-1}}{\mu_l}$$

# Models for $/r(\phi)$



#### Monodisperse suspensions:

#### Einstein 1906

Theoretical, linear, dilute suspensions B 'intrinsic viscosity' = 2.5 for spheres

#### Einstein-Roscoe 1952

Power-law,  $\phi_m = \text{max. particle}$  concentration

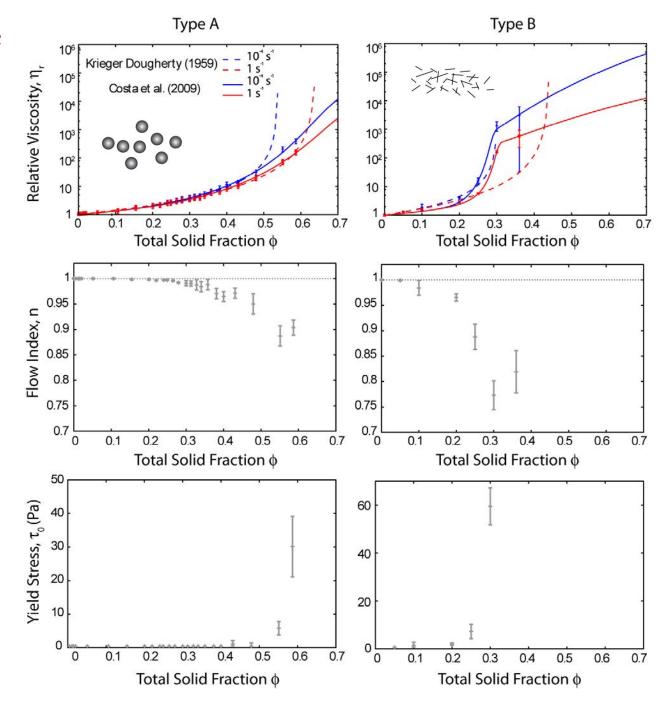
#### Krieger & Dougherty 1967

Power-law, exponent modified by  $\varphi_{\rm m}$ 

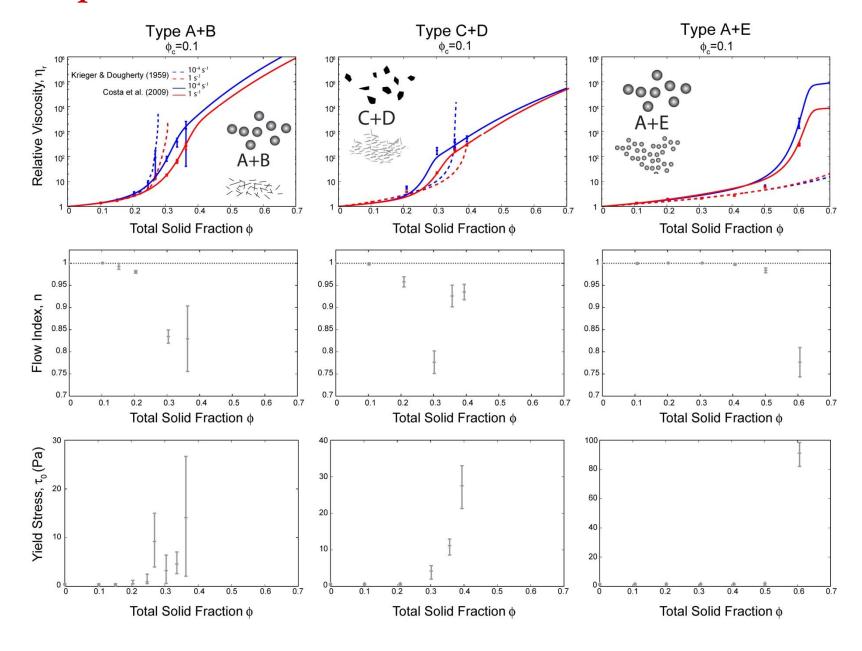
#### Costa et al. 2009

sigmoidal semi-empirical 3-parameter equation

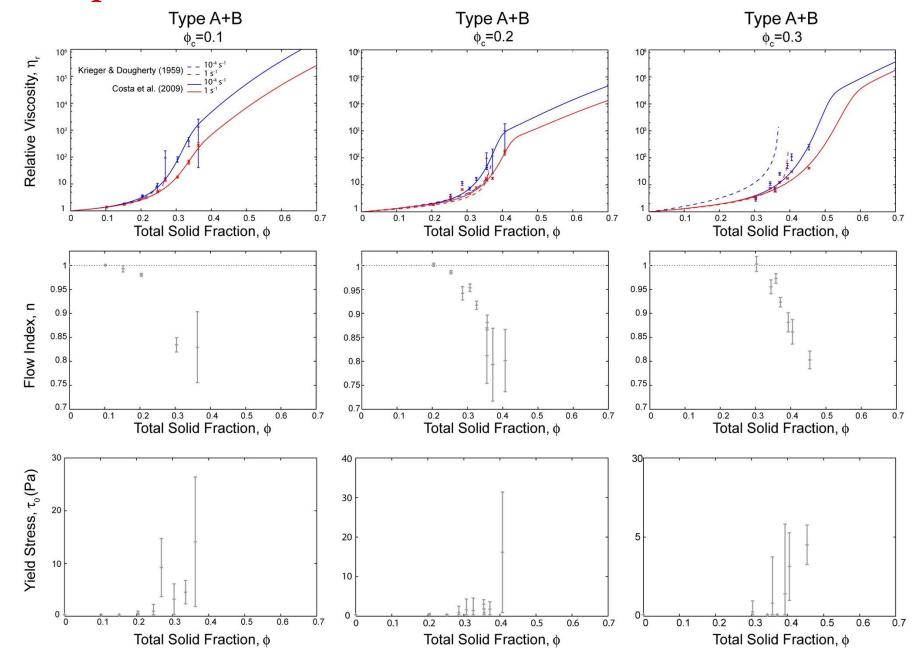
#### Monodisperse



#### **Bidisperse**



#### **Bidisperse**



#### Monodisperse

