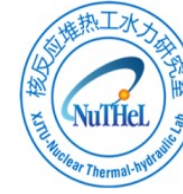


西安交通大学
XI' AN JIAOTONG UNIVERSITY



核反应堆热工水力研究室
Nuclear Thermal-hydraulic Lab

5th Joint ICTP-IAEA Workshop

Multiphysics modelling of Gen-IV reactors

Part 1 – OpenFOAM

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Xi'an Jiaotong University

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Aug. 2026

1

Overview of Gen-IV reactors

2

Brief review of frameworks

3

Part 1 – OpenFOAM

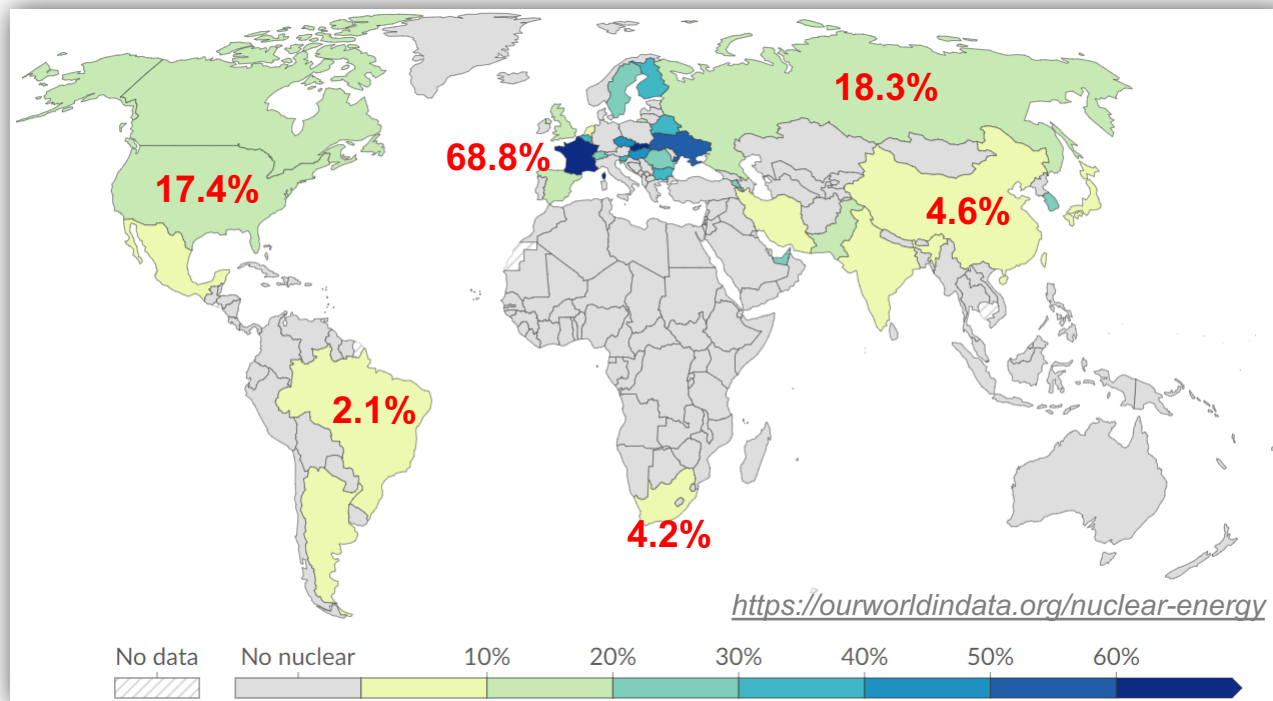
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Part 2 – MOOSE (Next talk)

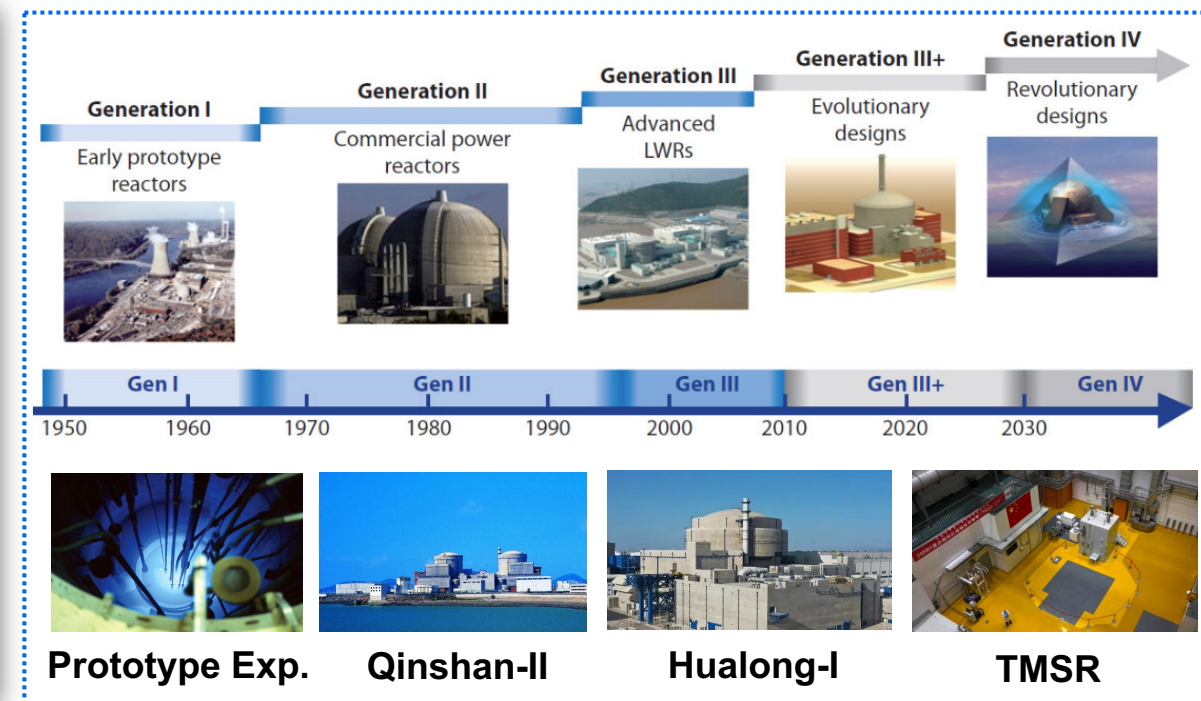
1.1 Development of nuclear energies

3/38

- Nuclear energy has a remarkable application in worldwide. **Its percentage of total power is increasing.** Particularly, the nuclear energy occupies **near 70% power supplement in France.**
- China proceeds a step-by-step development of nuclear energy. Gen-III+ reactors are used for main power generation, and **the Gen-IV advanced reactors are on-going in research and construction.**



Nuclear energy percentage of total power (in 2025)



Roadmap of nuclear power system in China

1.2 Proposal of Gen-IV reactors

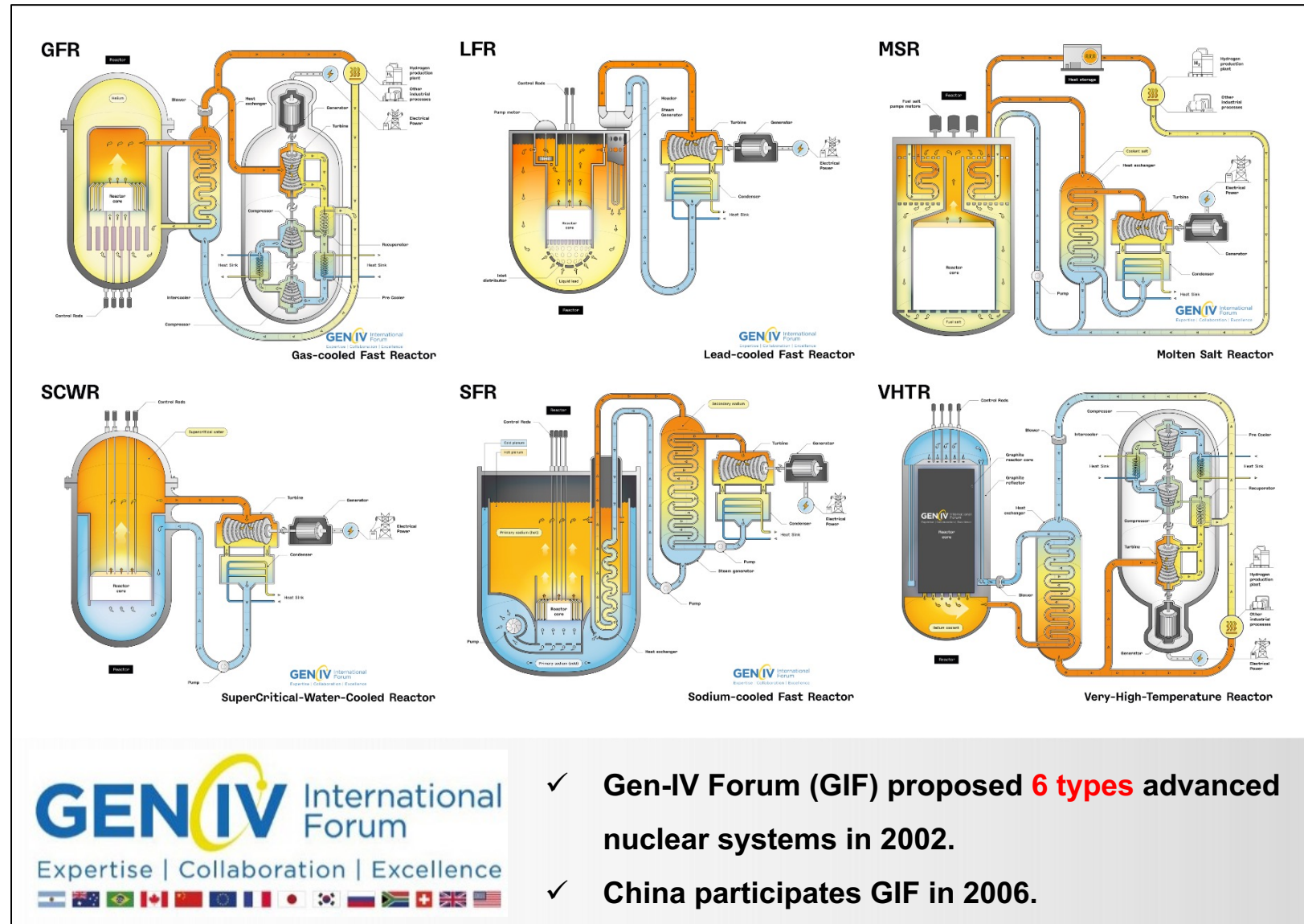
4/38

➤ Gen-IV advanced reactors

1. Gas-cooled fast reactor (GFR)
2. Lead-cooled fast reactor (LFR)
3. Molten salt reactor (MSR)
4. Supercritical water reactor (SCWR)
5. Sodium-cooled fast reactor (SFR)
6. Very high-temperature reactor (VHTR)

➤ Goals

- ✓ Sustainability
- ✓ Economics
- ✓ Safety and reliability
- ✓ Non-proliferation and protection



1.4 Why we need multiphysics?

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1. Inherent physical characteristics

- Gen-IV reactors exhibit the inherent physical coupling characteristics, e.g. Molten Salt Reactor.
- Molten fuel salt flows through the core, **strongly coupling the DNP transport and thermal-hydraulics.**

- Neutron transport

$$\frac{1}{V_g} \frac{\partial \psi_g}{\partial t} + \mathbf{\Omega} \cdot \nabla \psi_g = F_{P,g} + F_{D,g} + S_g - \underbrace{\frac{1}{V_g} \nabla \cdot (\mathbf{U} \psi_g)}_{V_g \gg |\mathbf{U}|, \approx 0}$$

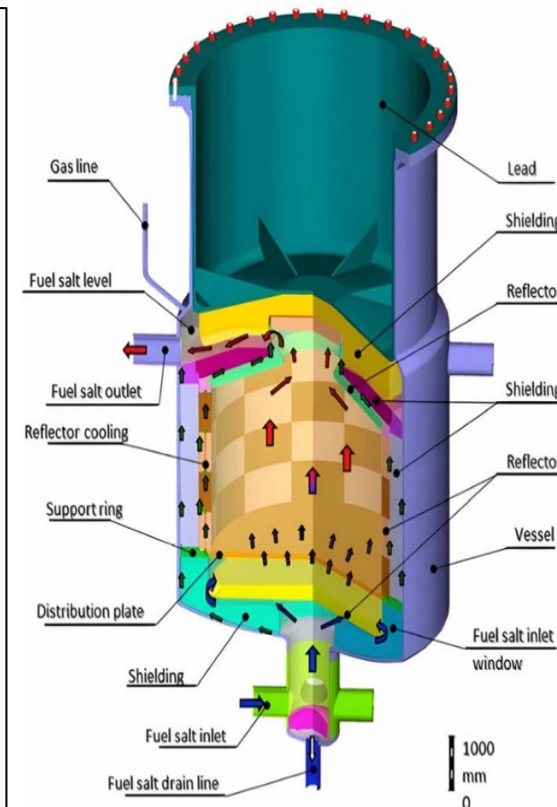
- DNP transport

$$\frac{\partial C_i}{\partial t} = \beta_i \sum_{g'=1}^G \left[\nu \Sigma_{f,g'} \sum_{m=1}^M \psi_{g'} \right] - \lambda_i C_i - \nabla \cdot (\mathbf{U} C_i)$$

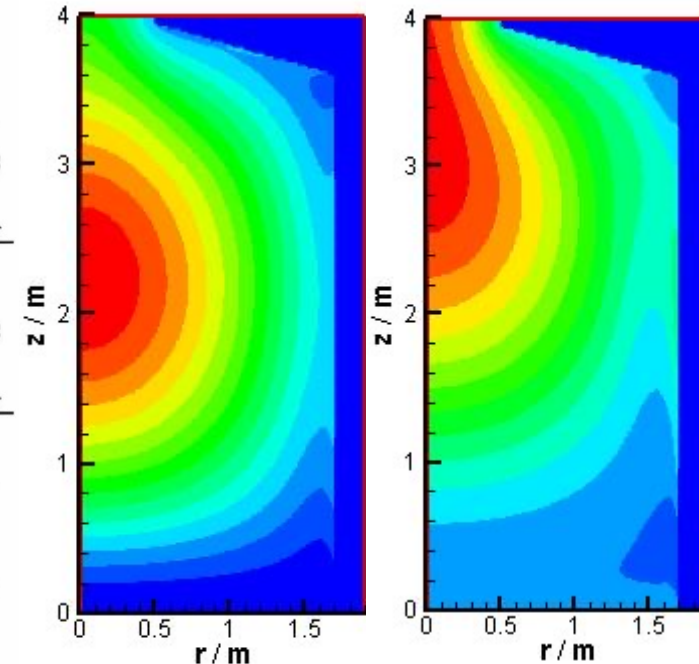
- Thermal-hydraulics

$$\frac{\partial \rho \Phi}{\partial t} + \nabla \cdot (\rho \mathbf{U} \Phi) = \nabla \cdot (\Gamma \nabla \Phi) + S$$

Couple



- DNP distribution in MOSART



No couple ✗

Couple ✓

1.4 Why we need multiphysics?

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2. Closer to reality, promoting safe operation

- Multiphysics coupling is **a hot research topic**, which is usually listed as a special track in conferences.
- It can help us to figure out a more realistic behavior of reactor, such as **SFR “blossom” effect**.



19th International Topical Meeting on Nuclear Reactor Thermal Hydraulics (NURETH-19)
March 6 - 11, 2022 • Brussels, Belgium • The Square

TECHNICAL TRACKS

2. COMPUTATIONAL THERMAL HYDRAULICS

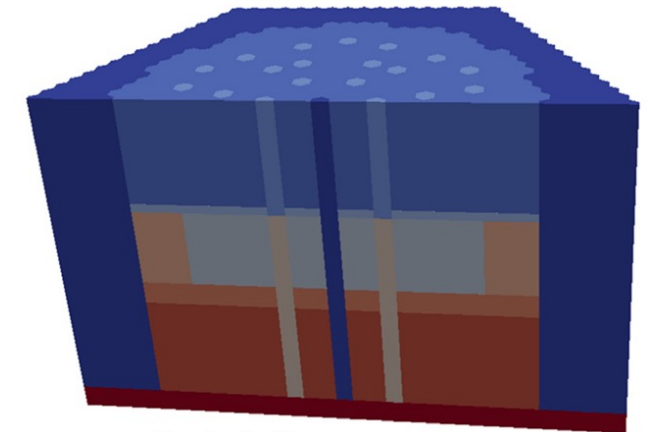
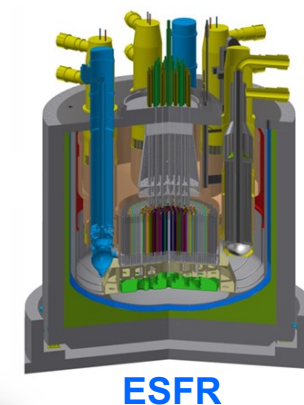
- 2a Thermal Hydraulics System Code Analysis
- 2b Computational Fluid Dynamics
- 2c Computational Multi-Fluid Dynamics
- 2d Multi-scale Analysis
- 2e Multi-physics Analysis**
- 2f

7. ADVANCED REACTORS

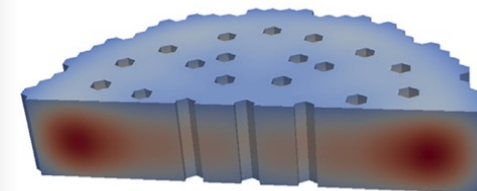
- 7a Advanced Reactors General
- 7b Small Modular Reactors
- 7c High-Temperature Gas-Cooled Reactors
- 7d Salt-Cooled High-Temperature Reactors

Proceedings of Advances in Thermal Hydraulics (ATH 2024)

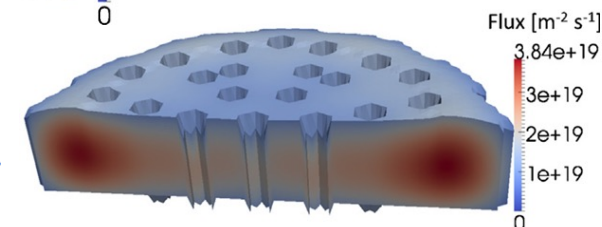
- | | |
|---|---|
| 1 Plenaries | 63 Performance Validation of the Passive Safety Features in Near Term PWRs in Korea— <i>Han-Gon Kim</i> |
| 3 ATH Plenary | 65 Keynotes: VI |
| 634 Effects of Upper Chimney Throttling on Two-Phase Flow in a Large-Scale Water-Based RCCS— <i>Matthew J. Jasica</i> , | 741 Multiphysics -Coupled and Microreactor Thermal Hydraulics |



Fiorina et al (2015)



SFR “blossom”



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Part 1 – OpenFOAM

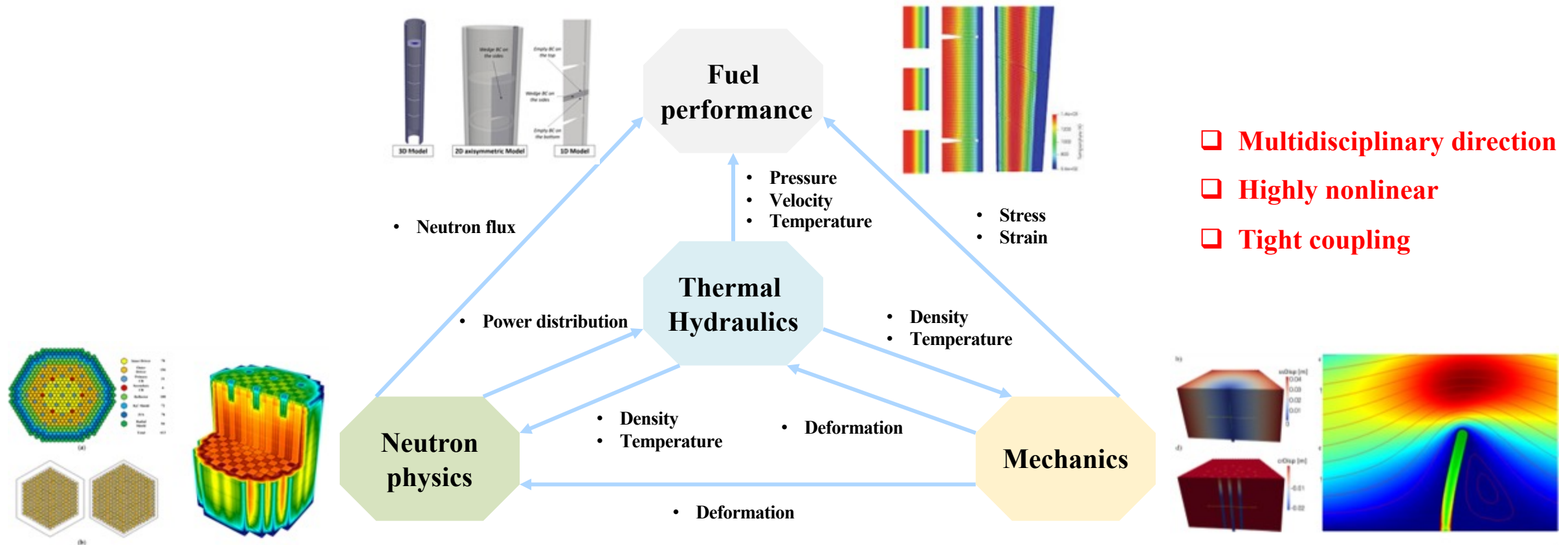
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Part 2 – MOOSE (Next talk)

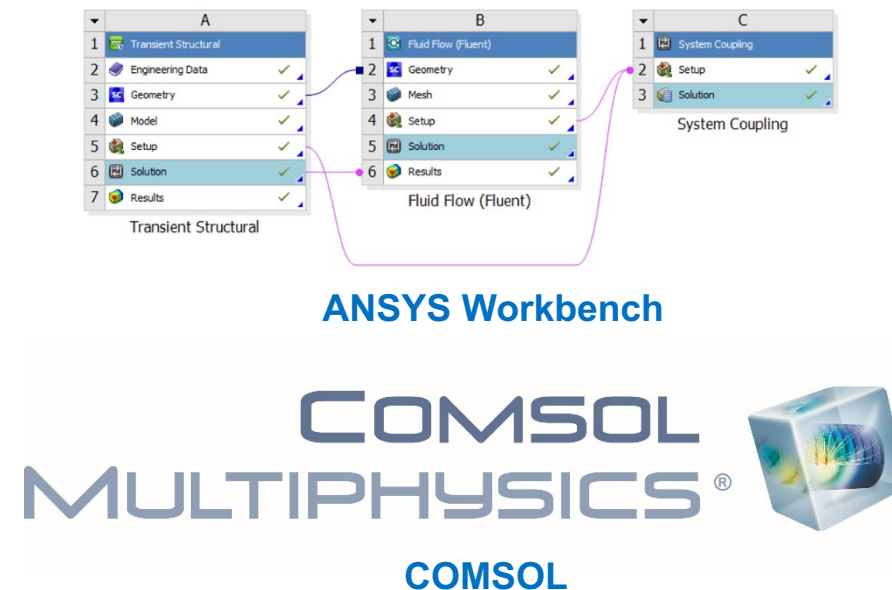
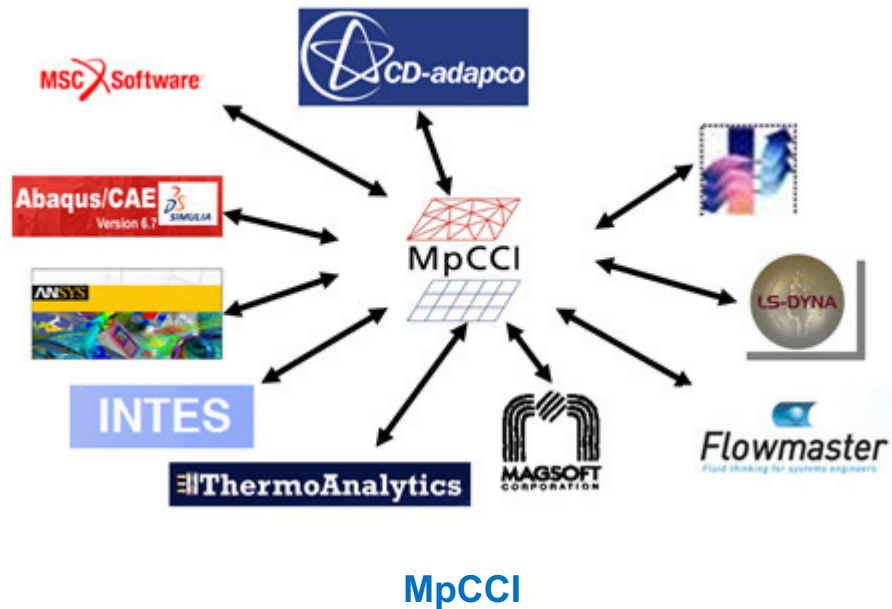
2.1 Technical routes to multiphysics

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- As an energy generation and transport system, a nuclear reactor system is a **multi-physics** system centered on **thermal-hydraulics** and coupled with **neutronics**, **mechanics**, and related disciplines
- The **high-fidelity** multi-physics computational tools represents a critical direction for next-generation numerical simulation platforms for nuclear power systems



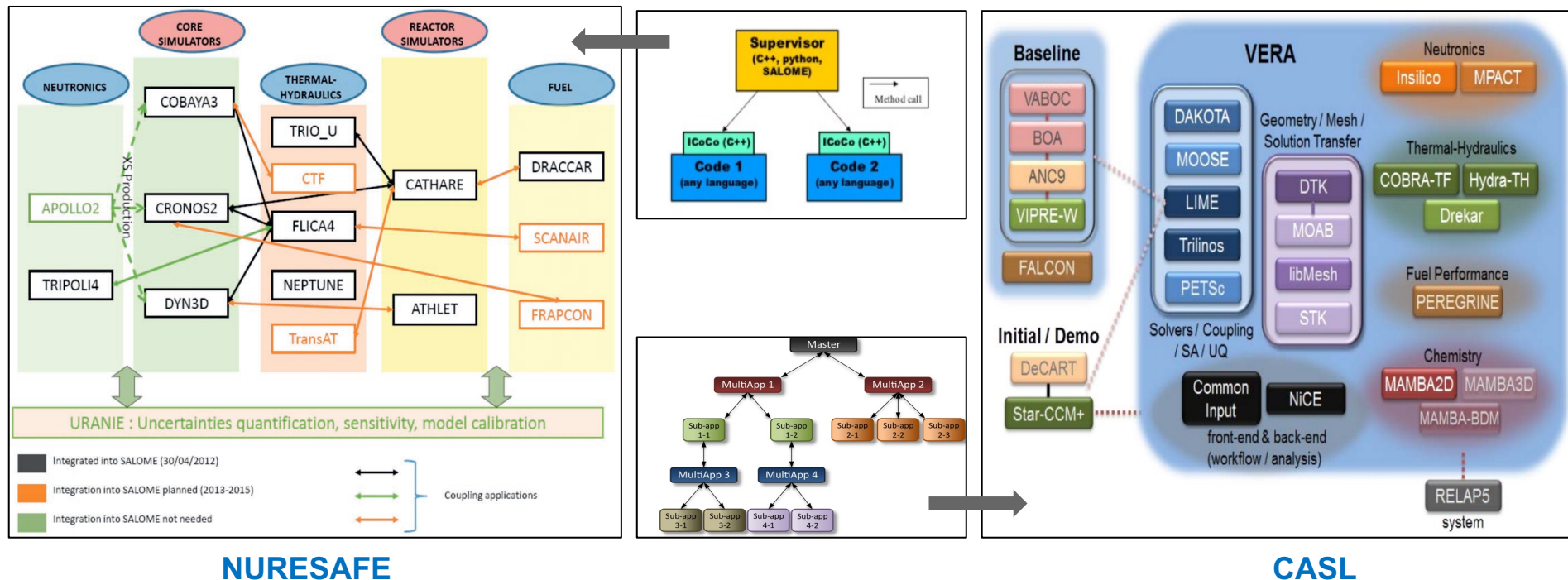
- ❑ **Features:** Limited development using commercial software, or external coupling with dedicated codes.
- ❑ **Advantages:** Strong thermal-hydraulics and mechanics modules; complete documentation; user-friendly operation.
- ❑ **Limitations:** Commercial software usually lacks neutronics solvers; external neutronics codes or embedded interfaces are required.
- ❑ **Applications:** MpCCI-based coupling; Workbench-based coupling; COMSOL-based coupling.



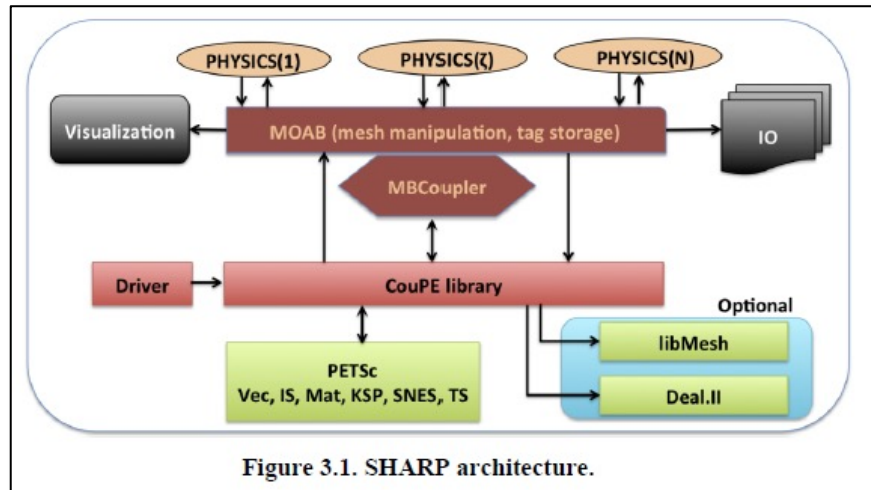
2.3 Route 2: Specified in-house codes

11/38

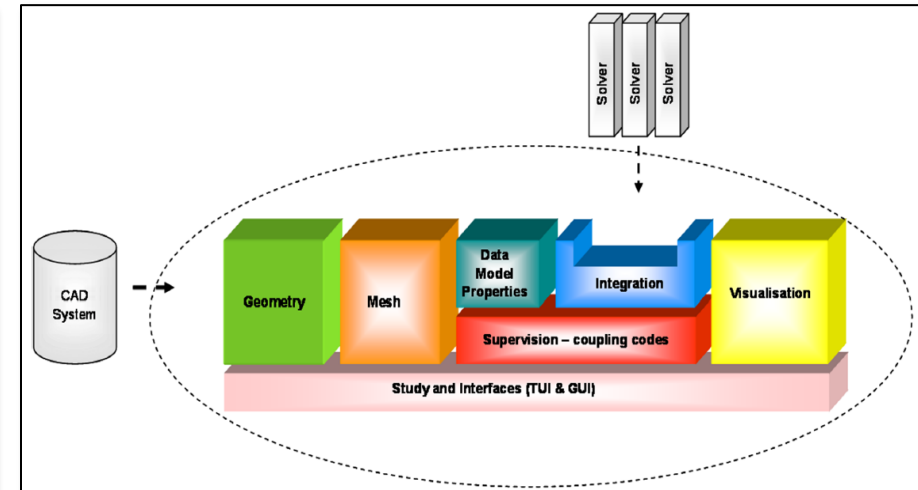
- ❑ **Features:** Adopts mature reactor codes with long-term V&V; only minor source-code changes are needed to build data-transfer interfaces.
- ❑ **Advantages:** Mature computational software system, with reliability verified over long-term use.
- ❑ **Limitations:** Three or more physics fields can create complex interaction logic; loose coupling converges slowly.
- ❑ **Applications:** The European NURES SAFE program uses the ICoCo data interface; the U.S. CASL program uses the LIME framework.



- ❑ **Features:** Unified programming framework; different meshes for different physics fields; data transfer through mesh-mapping modules.
- ❑ **Advantages:** Shared framework facilitates extension and supports strong-coupling algorithms.
- ❑ **Limitations:** Mesh mapping introduces additional error sources; development effort is substantial.
- ❑ **Applications:** NEAMS uses MOOSE and MOBA for mesh management and mapping; NURESIM uses SALOME/MEDCoupling.



NEAMS-SHARP

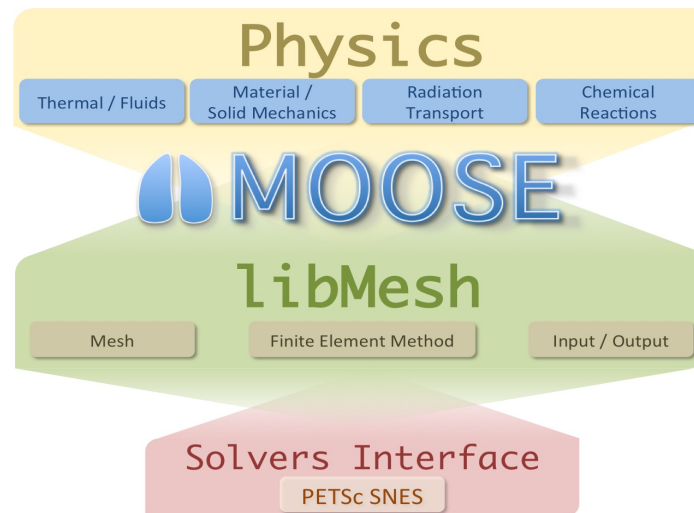


NURESIM-SALOME

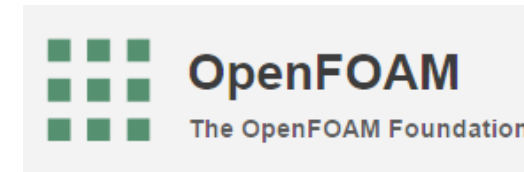
2.5 Route 4: All in one unified coupling frameworks

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- ❑ **Features:** Unified programming framework with the same mesh for all physics fields, where PDEs are discretized and solved on a common mesh.
- ❑ **Advantages:** No mesh-mapping error; supports high-accuracy strong or fully coupled schemes.
- ❑ **Limitations:** Development effort is difficult and substantial.
- ❑ **Applications:** No mature applications; two mainstream exploratory frameworks are MOOSE and OpenFOAM.



MOOSE (Next talk)



OpenFOAM

FOAM extend

OpenFOAM

Method	1. Commercial codes	2. In-house codes	3. General interface	4. Unified coupling framework
Coupling mode	Loose coupling	Loose coupling	Tight coupling	Tight coupling
Coupling method	OS (Operator separation)	OS	Picard	Picard/Newton
Coupling accuracy	Lower	Lower	Higher	Higher
Error	Errors introduced by data transfer and conversion between different programs		Grid interpolation errors	No grid interpolation error
Technical maturity	★★★★★	★★★★★	★★★	★★
Development difficulty	★	★★	★★★★★	★★★★★
V&V	★★★★★	★★★★★	★★	★★

Routes 3 and 4 have emerged as the principal directions for the development of next-generation multi-physics coupling codes

2.6 Summary

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		OpenFOAM	MOOSE	COMSOL	ANSYS	STAR-CCM+
Mode		Open source	Open source	Commercial		
Route		Route 2/3/4	Route 2/3/4	Route 1		
Discrete method		FVM	FEM	FEM	FVM/FEM	FVM/FEM
Multi-physics coupling platform		Unified framework / External data interface		Unified framework	External data interface based on the WorkBench platform	Internal data interface
Activity level in nuclear industry		★★★★★	★★★★★	★★★★	★★★★★	★★★★★
Scalability		★★★★★	★★★★★	★★	★★★	★★
Existing model maturity	Neutronics	★★★	★★★	--	--	--
	Thermal-hydraulics	★★★★★	★★★	★★★★	★★★★★	★★★★★
	Mechanics	★★★	★★★★	★★★	★★★★★	★★★
OpenFOAM and MOOSE constitute the technically mature, development-friendly, and legally low-risk open-source frameworks for strongly coupled multi-physics simulations						
Copyright risks		★	★	★★★★	★★★★	★★★★

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Part 1 – OpenFOAM

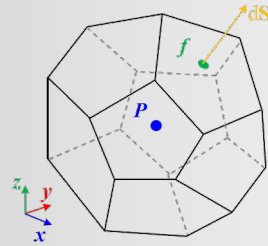
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Part 2 – MOOSE (Next talk)

3.1 Introduction to OpenFOAM

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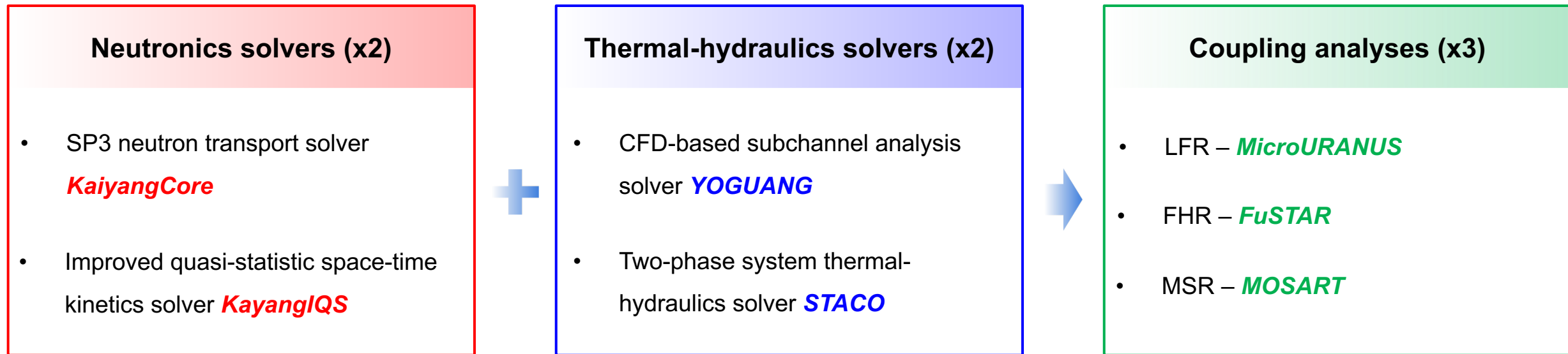
- OpenFOAM, developed in 1989, is the **most popular open-source CFD** platform in finite volume method.
- It is compatible with several open-source pre/post-process codes, **showing a healthy community**.
- Users can **freely and conveniently develop** their solvers for specified physical problems with OpenFOAM.

Pre-process	Solver	Post-process	
	 OpenFOAM The OpenFOAM Foundation https://openfoam.org/ Open  FOAM https://www.openfoam.com/ FOAM extend http://foam-extend.org		• FVM is naturally conservative. <pre data-bbox="2173 638 2486 895">fvVectorMatrix UEqn { fvm::ddt(U) + fvm::div(phi, U) - fvm::laplacian(nu, U) }; if (piso.momentumPredictor()) { solve(UEqn == -fvc::grad(p)); }</pre>
			
			
			
			
			• Highly extendable for user-defined solvers OpenFOAM finiteVolume Post-processing libraries Miscellaneous libraries Lagrangian particle tracking libraries Parallel libraries Solution and mesh manipulation libraries

3.2 Glance of our works on OpenFOAM

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- Based on OpenFOAM, we have developed 2 neutronics solvers and 2 thermal-hydraulics solvers, including the *neutron transport* and *space-time kinetics*, *subchannel analysis*, and *two-phase system thermal-hydraulics*. All the solvers are fully validated with experimental benchmarks.
- Besides, coupling analyses of 3 different types Gen-IV reactors (*LFR*, *FHR*, and *MSR*) are carried out.



3.3 SP3 neutron transport – KaiyangCore

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- **Our goal: use less computational workloads to get transport-like results – SP3 method.**
- **SP3 method is firstly proposed by *D. Geobard* in 1962, then *E. Larsen* strictly proved its theory in 1996.**

1. Diffusion-like transport

Approx: 3D operator to 1D operator

2. Heterogeneity revision

Approx: Even order to scalar

Approx: Odd order to vector

3. Scatter & fission sources

$$-D_g \nabla^2 (\psi_{0,g} + 2\psi_{2,g}) + \Sigma_{r,g} \psi_{0,g} = Q_g,$$

$$-\frac{27}{35} D_g \nabla^2 \psi_{2,g} + \Sigma_{t,g} \psi_{2,g} = \frac{2}{5} (\Sigma_{r,g} \psi_{0,g} - Q_g),$$

$$Q_g = \sum_{g' \neq g}^G \Sigma_{s,g' \rightarrow g} \psi_{0,g'} + \frac{\chi_g}{k_{eff}} \sum_{g'}^G \nu \Sigma_{f,g'} \psi_{0,g'},$$



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NUCLEAR ENERGY

Annals of Nuclear Energy 31 (2004) 1963–1986

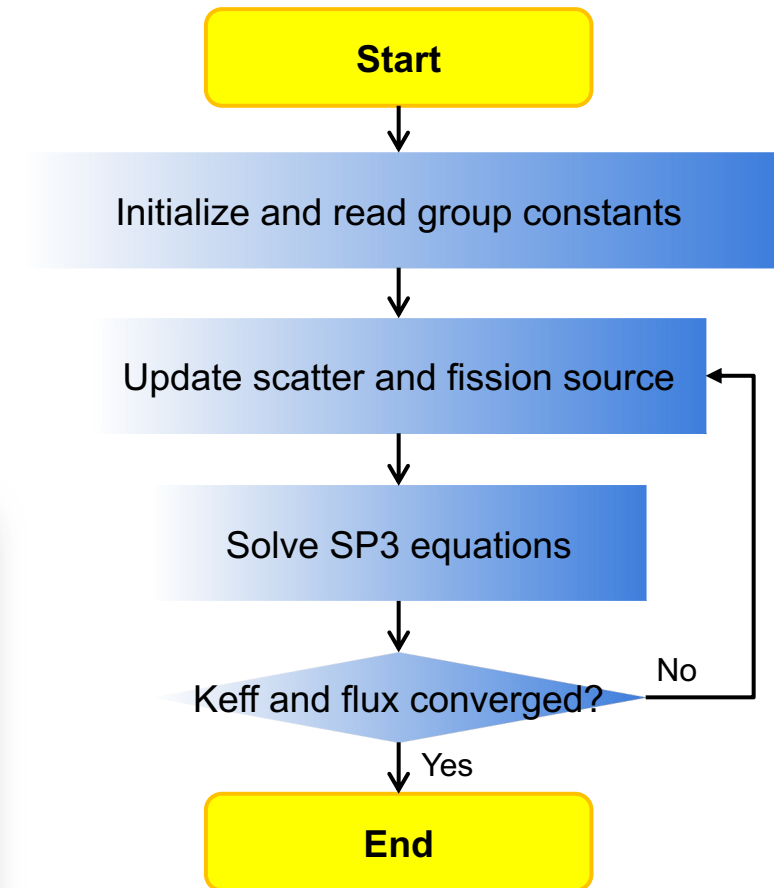
www.elsevier.com/locate/anucene

“I have an idea!” An appreciation of Edward W. Larsen’s contributions to particle transport

Marvin L. Adams *

Department of Nuclear Engineering, Texas A&M University, 129 Zachry, 3133 TAMU, College Station, TX 77843-3133, USA

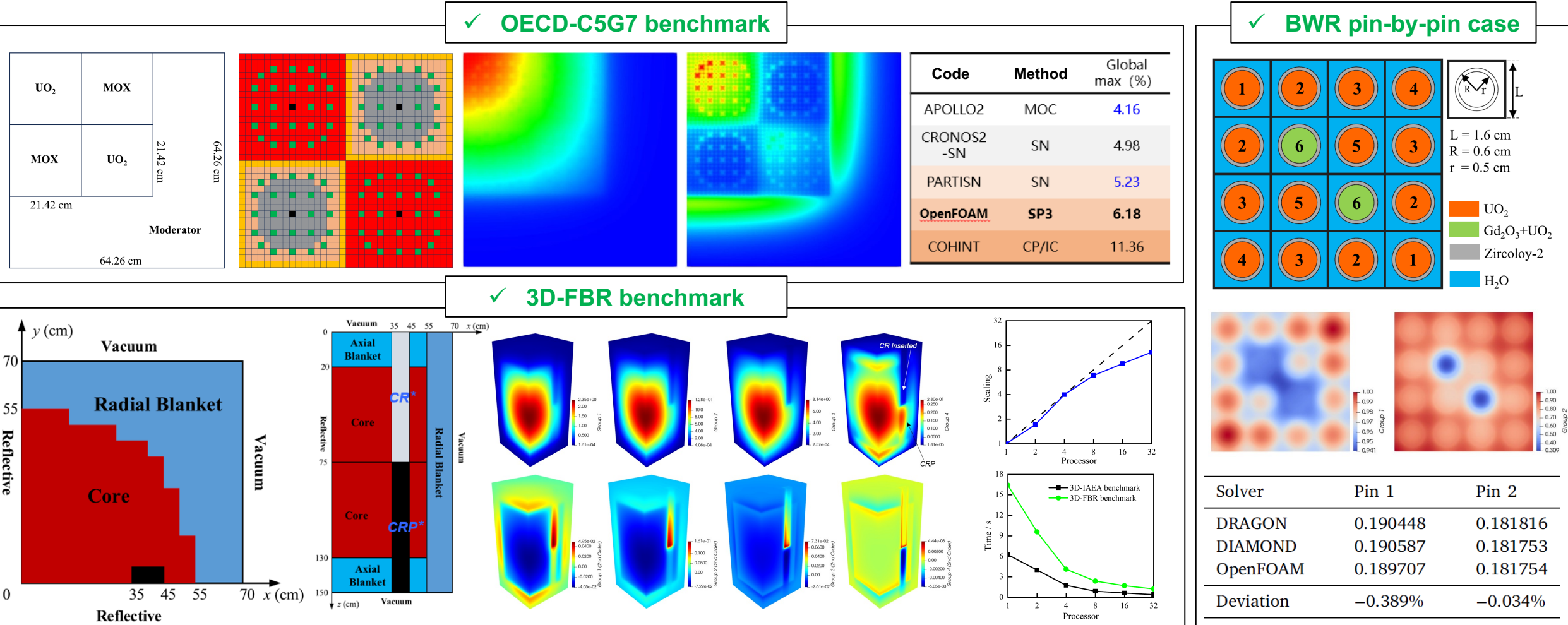
Courtesy of Univ. Michigan



Celebration of 60 years birthday of E. Larsen on the journal *Annals of Nuclear Energy* (2004) **gave the SP3 proof process introduction.**

3.3 SP3 neutron transport – KaiyangCore

➤ KaiyangCore has been validated by several neutron transport benchmarks, such as C5G7, 3D-FBR, and BWR pin-by-pin cases, **showing a comparable numerical accuracy with high-order transport solvers.**



3.4 Space-time kinetics – KaiyangIQS

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- Improved quasi-static method (IQS) decomposes the neutron scalar flux to **amplitude function (rapid)** and **shape function (slow)**, which allows us to use **small** and **large time steps** for space-time kinetics simulation coupling with **adjoint neutron transport equation**.

$$\frac{1}{v_g} \frac{\partial \phi_g(\vec{r}, t)}{\partial t} = D_g \nabla^2 \phi_g(\vec{r}, t) - \Sigma_{t,g} \phi_g(\vec{r}, t) + \sum_{g'=1}^G \Sigma_{s,g' \rightarrow g} \phi_{g'}(\vec{r}, t) + \frac{(1-\beta)\chi_{p,g}}{k_{eff}^{(0)}} \sum_{g'=1}^G \nu \Sigma_{f,g'} \phi_{g'}(\vec{r}, t) + \sum_{i=1}^6 \chi_{d,i,g} \lambda_i \hat{C}_i(\vec{r}, t)$$

$$\frac{\partial \hat{C}_i(\vec{r}, t)}{\partial t} = \frac{\beta_i}{k_{eff}^{(0)}} \sum_{g=1}^G \nu \Sigma_{f,g} \phi_g(\vec{r}, t) - \lambda_i \hat{C}_i(\vec{r}, t), \quad i = 1, \dots, 6$$

➔

Quasi-static decomposition

$\phi_g(\vec{r}, t) = n(t) \cdot \psi_g(\vec{r}, t)$

Scalar flux

Shape

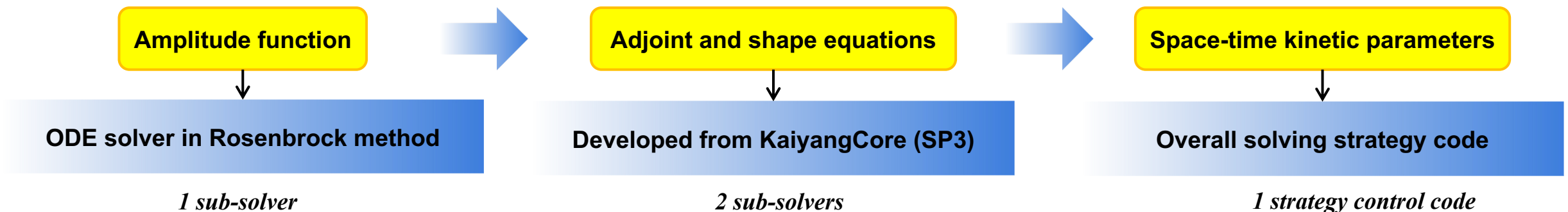
Amplitude

$$\frac{n}{v_g} \frac{\partial \psi_g}{\partial t} + \frac{\psi_g}{v_g} \frac{dn}{dt} - n \cdot D_g \nabla^2 \psi_g + n \cdot \Sigma_{t,g} \psi_g = n \cdot \sum_{g'=1}^G \Sigma_{s,g' \rightarrow g} \psi_{g'} + n \cdot \frac{(1-\beta)\chi_{p,g}}{k_{eff}^{(0)}} \sum_{g'=1}^G \nu \Sigma_{f,g'} \psi_{g'} + \sum_{i=1}^6 \chi_{d,i,g} \lambda_i \hat{C}_i$$

$$\frac{dn(t)}{dt} = \frac{\rho(t) - \bar{\beta}(t)}{\Lambda(t)} n(t) + \sum_{i=1}^6 \lambda_i \bar{C}_i(t)$$

$$\frac{d\bar{C}_i(t)}{dt} = \frac{\bar{\beta}_i(t)}{\Lambda(t)} n(t) - \lambda_i \bar{C}_i(t), \quad i = 1, \dots, 6$$

- **Implementation in OpenFOAM:** mainly consist of 3 sub-solvers, 1 process solving strategy code.

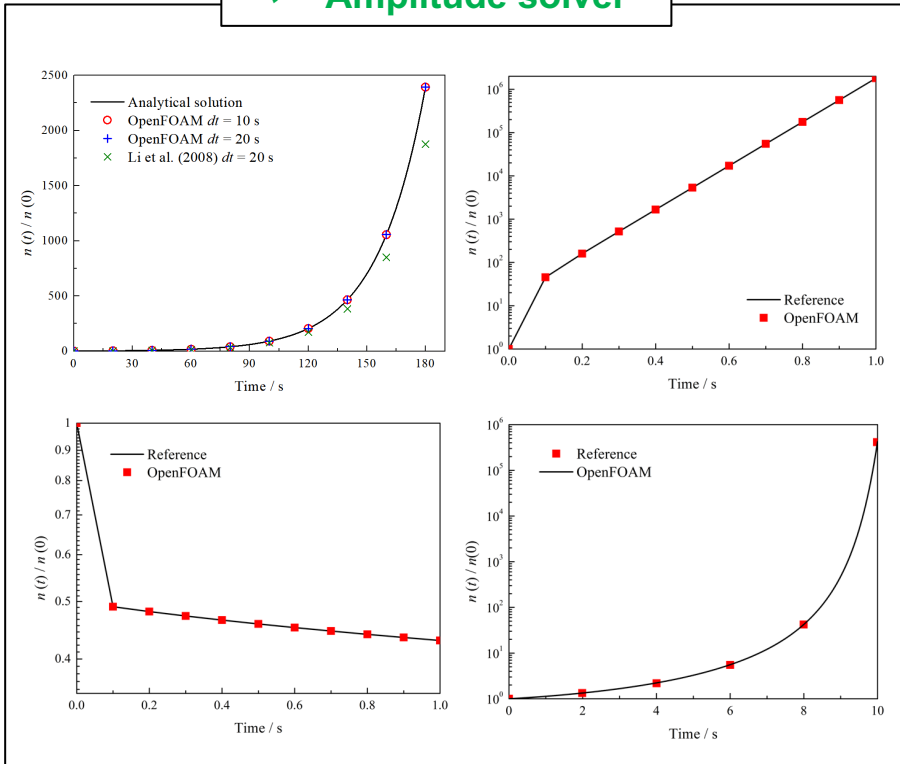


3.4 Space-time kinetics – KaiyangIQS

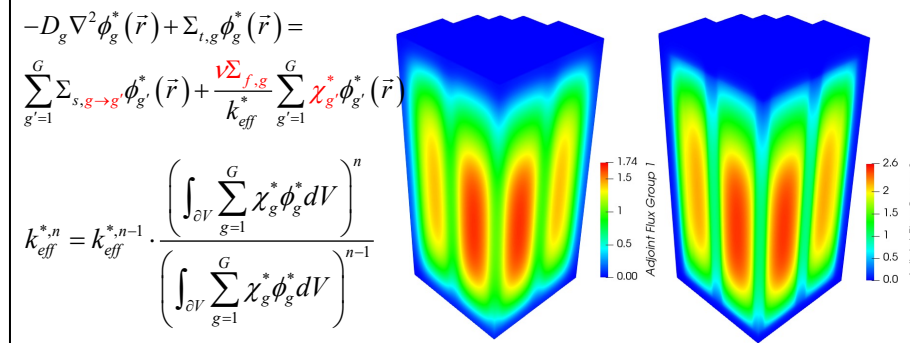
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- Sub-solvers in KaiyangIQS **are carefully verified first**, such as amplitude and adjoint neutronics solvers. The comprehensive validations of KaiyangIQS are carried out with **1D/2D/3D benchmarks**.
- We adopt **high-order Rosenbrock algorithm** to solve stiffness problems, the numerical accuracy of space-time kinetics is promising.

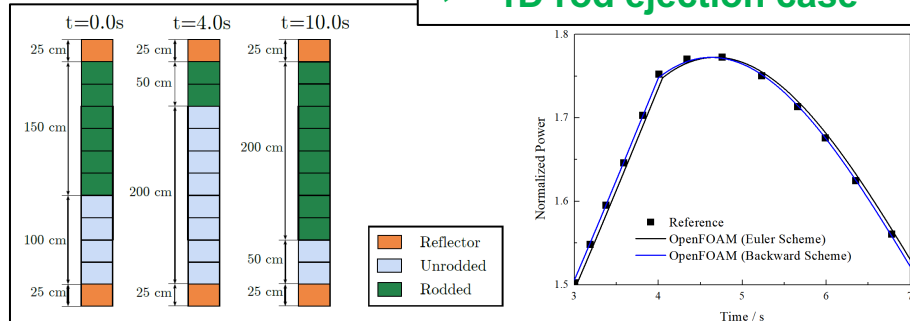
✓ Amplitude solver



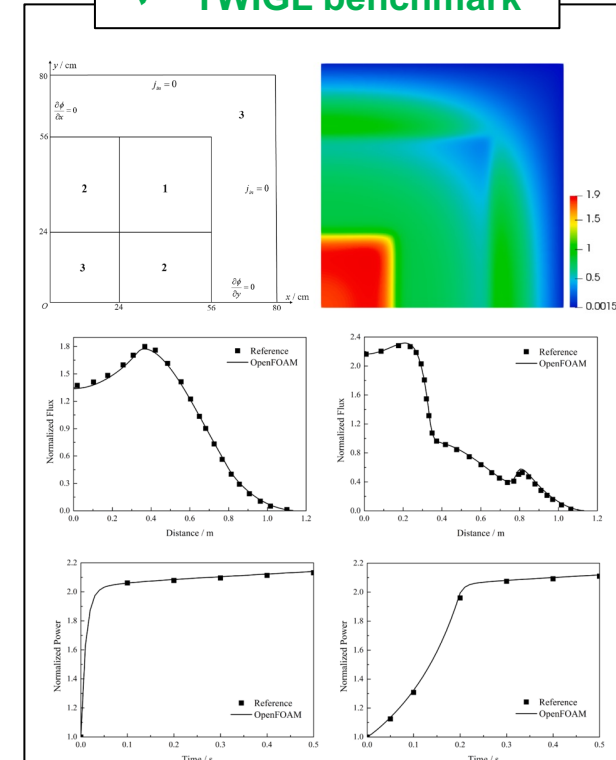
✓ Adjoint neutronics solver



✓ 1D rod ejection case



✓ TWIGL benchmark

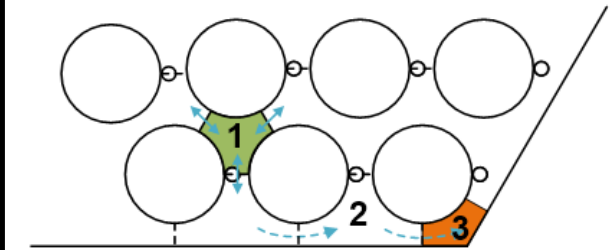


3.5 Subchannel analysis – YOGUANG

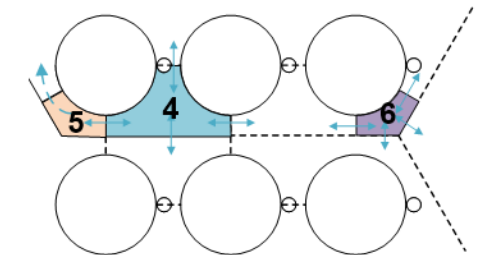
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- Considering the advantages of OpenFOAM, we develop a **CFD-based subchannel code** – YOGUANG for **Gen-IV wire-wrapped liquid metal cooled reactors**. General mesh system is adopted to solve a CFD-like thermal-hydraulics. The empirical models are supplemented to close the source terms.

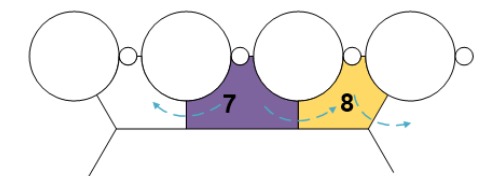
Continuity equation	$\nabla \cdot (\rho \mathbf{u}) = 0$	
Momentum equation	$\nabla \cdot (\rho \mathbf{u} \mathbf{u}) = -\nabla p + \nabla \cdot (\mu_t \nabla \mathbf{u}) + \nabla \cdot (\mu \nabla \mathbf{u}) - \mathbf{K} \cdot \mathbf{u} + \rho \mathbf{g}$	
Todreas-Nishimura model	$\kappa_t = f_{scale} \cdot \left[\underbrace{S(\text{Re}, \mathbf{u})}_{\text{sweep}} + \underbrace{P(\text{Re}, Gr, \mathbf{u})}_{\text{plume}} \right]$ $\mu_t = \rho \kappa_t \cdot \text{Pr}_t$ $-\rho \overline{\mathbf{u}'T'} = \Gamma_t \nabla T, \quad \text{Pr}_t = \frac{\mu_t}{\Gamma_t}$ $\kappa_t = \frac{\Gamma_t}{\rho}$	
Friction drag tensor	$\mathbf{M} = \begin{bmatrix} \mu \cdot f_x & & \\ & \mu \cdot f_y & \\ & & \mu \end{bmatrix}$	Cheng-Todreas model $\mathbf{K} = \begin{bmatrix} k_x & & \\ & k_y & \\ & & k_z \end{bmatrix}$ $\mathbf{k} = \frac{f_D \rho \mathbf{u} }{2D_h}$
Energy equation	$\nabla \cdot (\rho C_p \mathbf{u} T) = \nabla \cdot (\mathbf{A} \cdot \nabla \rho C_p T) + \nabla \cdot (\kappa_t \nabla \rho C_p T) + Q$	
Todreas-Nishimura model	$\kappa_t = f_{scale} \cdot \left[\underbrace{S(\text{Re}, \mathbf{u})}_{\text{sweep}} + \underbrace{P(\text{Re}, Gr, \mathbf{u})}_{\text{plume}} \right]$	Shape conduction $\mathbf{A} = \begin{bmatrix} \alpha \cdot f_x & & \\ & \alpha \cdot f_y & \\ & & \alpha \end{bmatrix}$



Inner, side, and corner subchannels

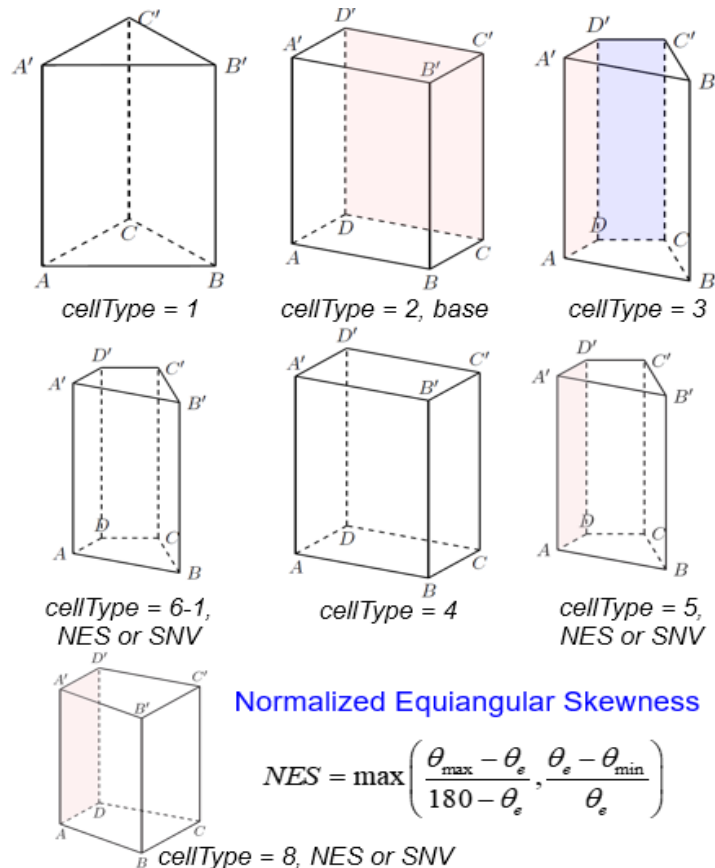


New-added open subchannels

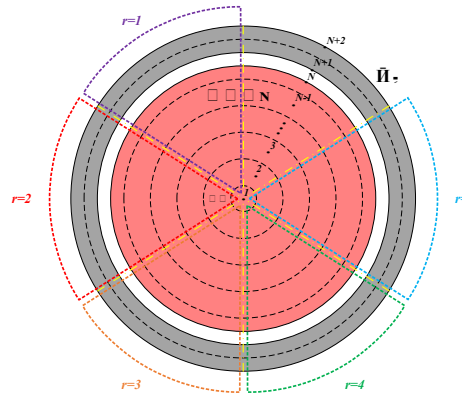


Irregular shape subchannels

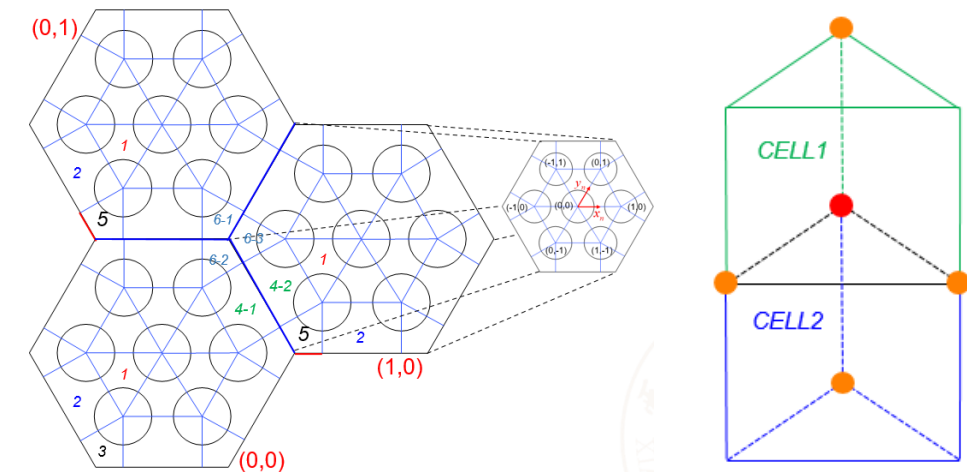
- **Three novel rapid modelling techniques** are proposed: 1. subchannel auto-identification, 2. fuel pin radial temperature calculation, and 3. fuel pin two-layer auto-location. The merits of YOGUANG allow to make a **quick core-level subchannel analysis with robust numerical methods** for Gen-IV reactors.



Subchannel auto-identification



1D fuel pin radial temperature calc.



Fuel pin two-layer auto-location

Advantages & advancements

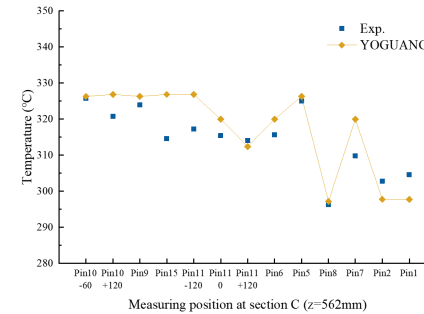
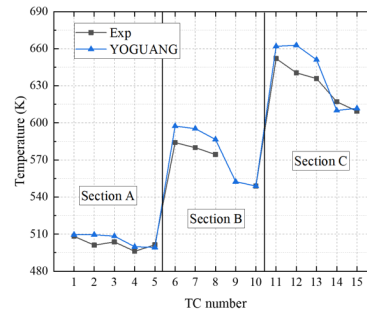
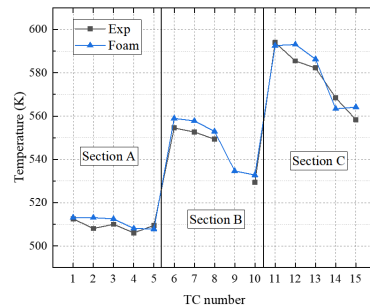
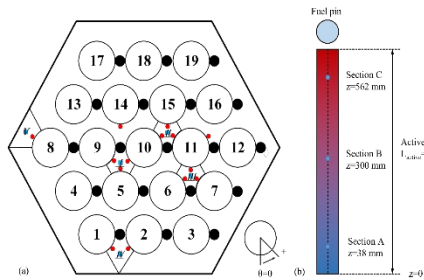
1. Quick core-level subchannel modeling ability.
2. More precise fuel pin temperature prediction.
3. More robust and flexible numerical scheme and solving algorithm.

3.5 Subchannel analysis – YOGUANG

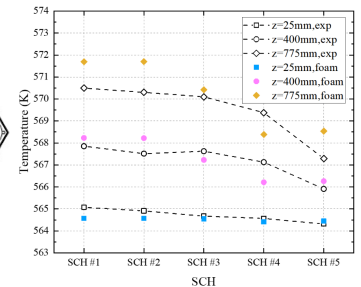
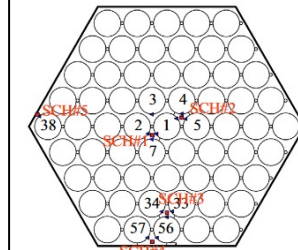
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- YOGUANG is validated with several well-known LBE experiments, such as NACIE-UP, KIT-THEADES, and KYLIN, **showing the good numerical predictions when compared with benchmark code – COBRA.**
- YOGUANG strongly supports the **coarse-mesh CFD subchannel method**, which is expected to give new insights on subchannel analysis of thermal-hydraulics.

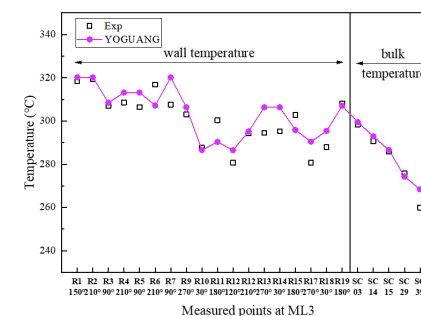
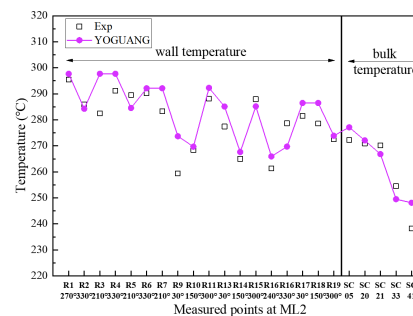
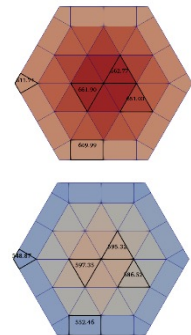
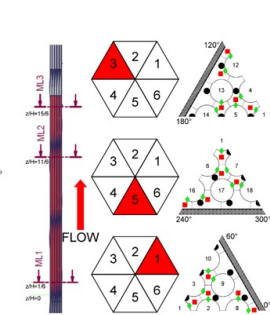
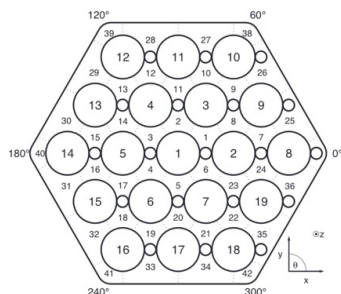
✓ NACIE-UP experiment



✓ KYLIN-61 experiment



✓ KIT-THEADES experiment

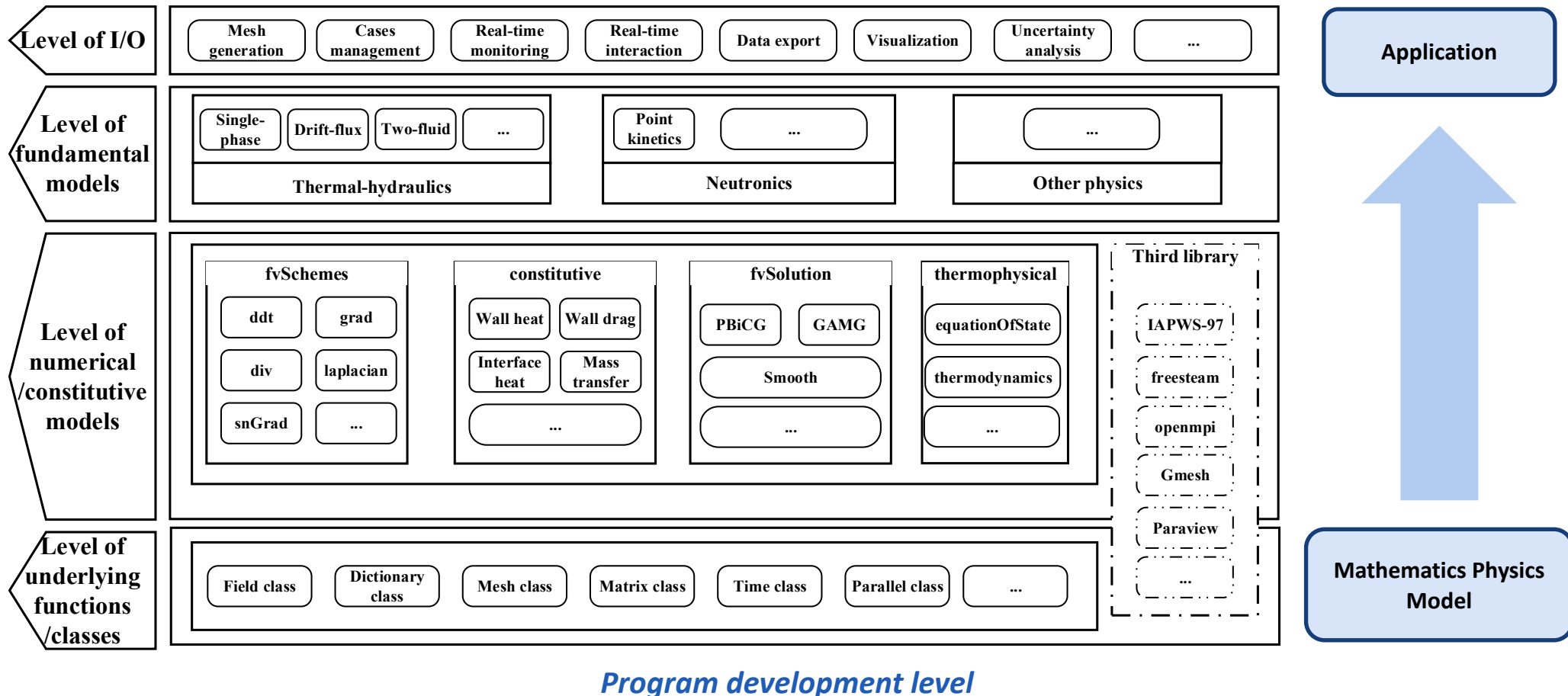


Error	MRE%	MAE(°C)	RMSE(°C)	MaxE(°C)
ML1				
SACOS	3.76	3.175	3.874	8.211
COBRA-YT	4.10	3.458	4.407	10.019
Foam	5.26	4.440	5.430	12.496
ML2				
SACOS	7.253	6.118	7.658	18.005
COBRA-YT	6.741	5.686	7.373	15.516
Foam	7.156	6.036	7.556	14.778
ML3				
SACOS	7.516	6.331	8.107	19.783
COBRA-YT	7.236	6.104	7.784	15.533
Foam	6.170	5.205	6.291	14.485

3.6 System-level two phase flow – STACO

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- We also develop a **CFD-based system code** – STACO (**S**ystem-level **T**hermal-hydraulic **A**nalysis **C**ode based on **O**penFOAM)
- This tool supports the partial non-equilibrium **drift-flux** model and the non-equilibrium **two-fluid** model



➤ Governing equations of two-fluid model

- Continuity equations $\frac{\partial(\alpha_k \rho_k)}{\partial t} + \nabla \cdot (\alpha_k \rho_k \mathbf{u}_k) = \Gamma_k$
- Momentum equations $\frac{\partial(\alpha_k \rho_k \mathbf{u}_k)}{\partial t} + \nabla \cdot (\alpha_k \rho_k \mathbf{u}_k \mathbf{u}_k) = -\alpha_k \nabla p + \mathbf{F}_{w,k} + \alpha_k \rho_k \mathbf{g} + \mathbf{F}_{i,k} + \Gamma_k \mathbf{u}_i$
- Energy equations $\frac{\partial(\alpha_k \rho_k h_k)}{\partial t} + \nabla \cdot (\alpha_k \rho_k \mathbf{u}_k h_k) = Q_{w,k} + \alpha_k \frac{Dp}{Dt} + h_{i,k} \Gamma_k + Q_{i,k}$
- Constitutive models

$\mathbf{F}_{w,k} = -C_{w,k} |\mathbf{u}_k| \mathbf{u}_k$
wall shear

$\mathbf{F}_{i,k} = C_i |\mathbf{u}_{1-k} - \mathbf{u}_k| (\mathbf{u}_{1-k} - \mathbf{u}_k)$
interphase shear

$Q_{i,k} = H_{i,k} A_i (T_i - T_k)$
interfacial heat transfer

$Q_{w,k} = H_{w,k} A_w (T_w - T_k) + H_{w,sat,k} A_w (T_w - T_{sat})$
wall heat transfer

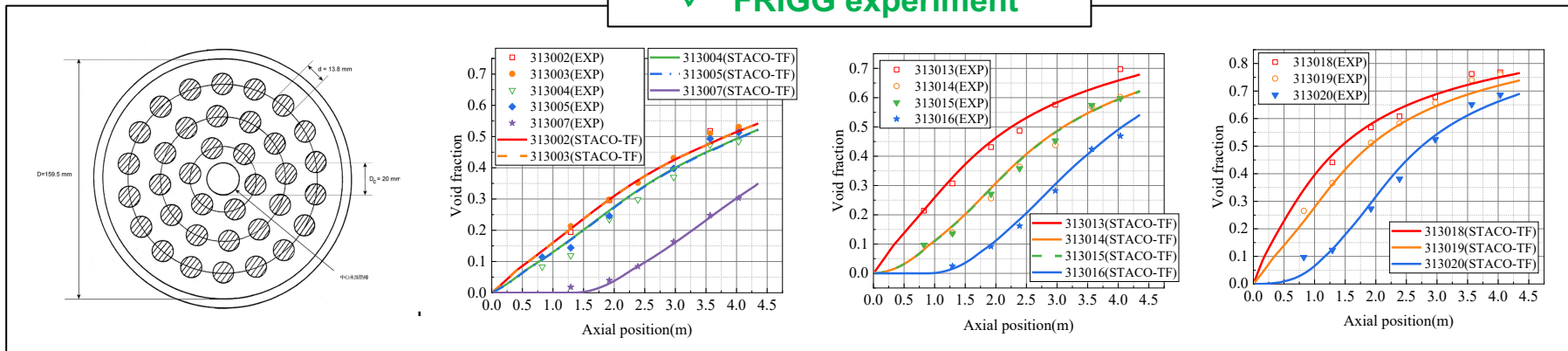
$\Gamma_k = \frac{Q_{i,k} + Q_{i,1-k}}{h_{i,k} - h_{i,1-k}} + \Gamma_w$
mass transfer

3.6 System-level two phase flow – STACO

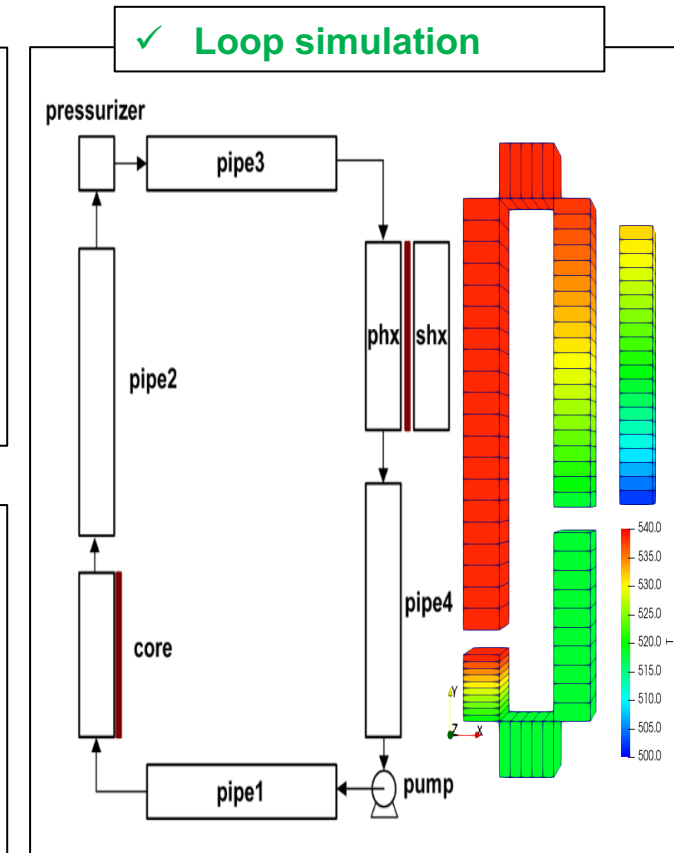
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- STACO is validated with several well-known two-phase experiments, such as **FRIGG**, **Bartolomei**, showing the good numerical predictions.
- STACO supports the **1D-mesh CFD system method**, which is expected to give new insights on system analysis of thermal-hydraulics.

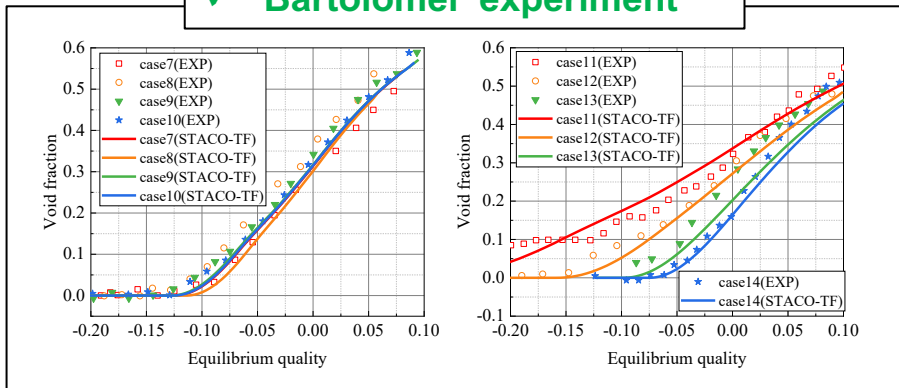
✓ FRIGG experiment



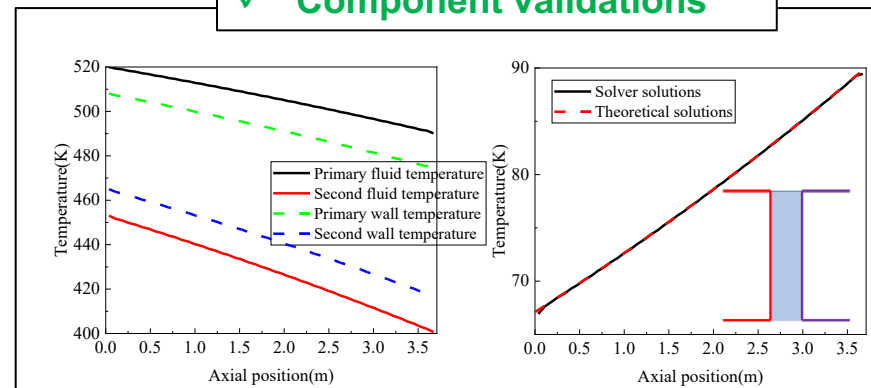
✓ Loop simulation



✓ Bartolomei experiment



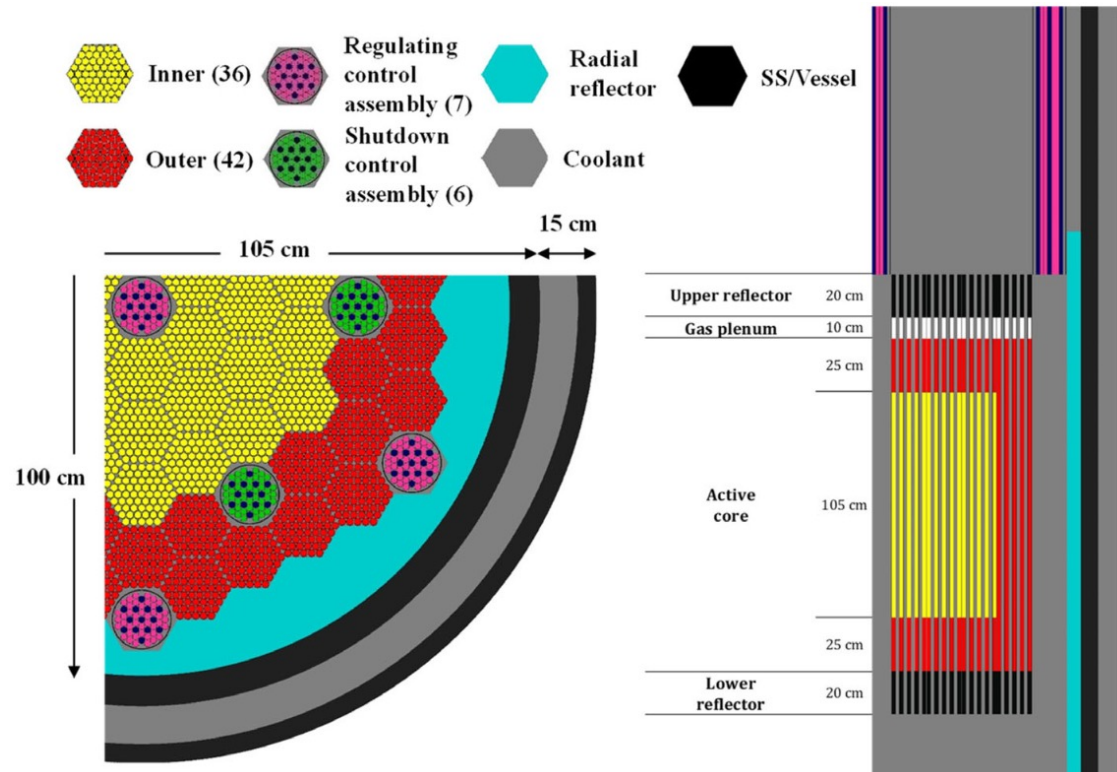
✓ Component validations



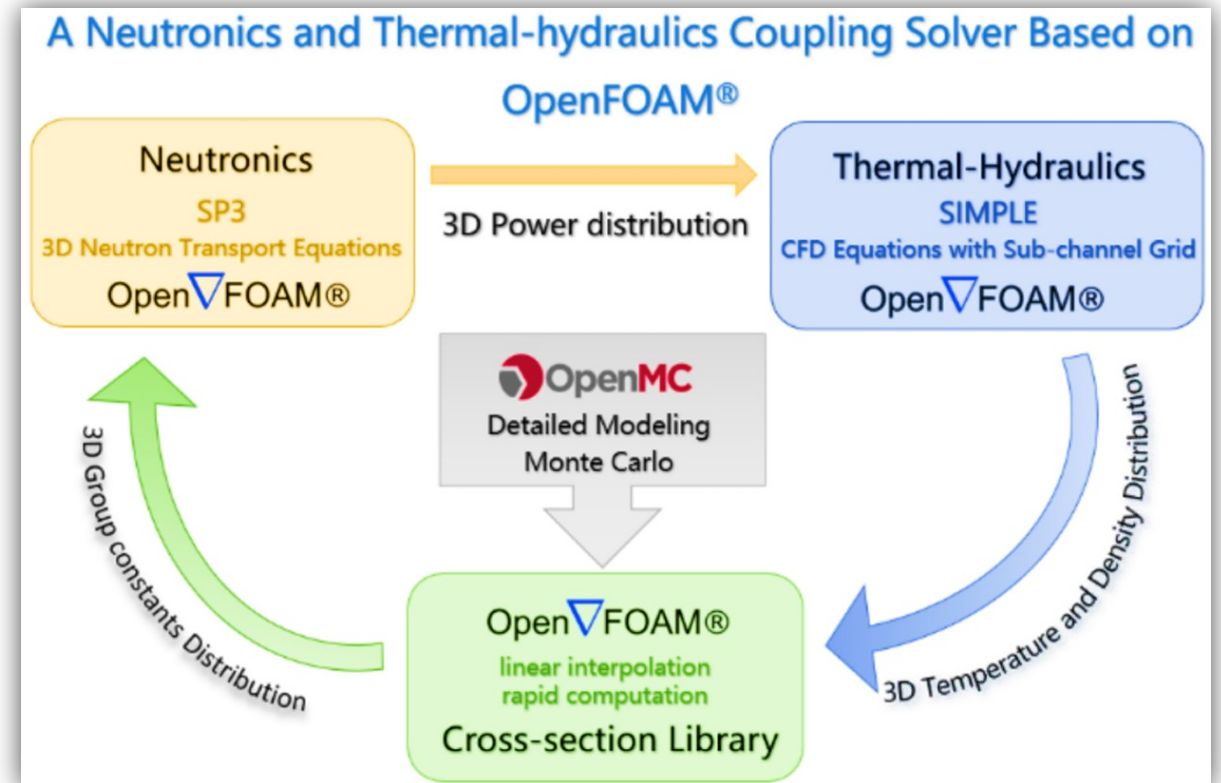
3.7 Coupling analysis for LFR

29/38

- MicroURANUS is a **small-modular LFR** for all-weather zero-carbon energy. However, the fission power distribution is coupled with thermal-hydraulics, required to be studied for safety assessment.
- We couple **KaiyangCore (SP3)** and **YOGUANG (subchannel)** to make the 3D core-level N/TH analyses. The group constants are generated from OpenMC.



MicroURANUS reactor layout (Nguyen et al 2021)

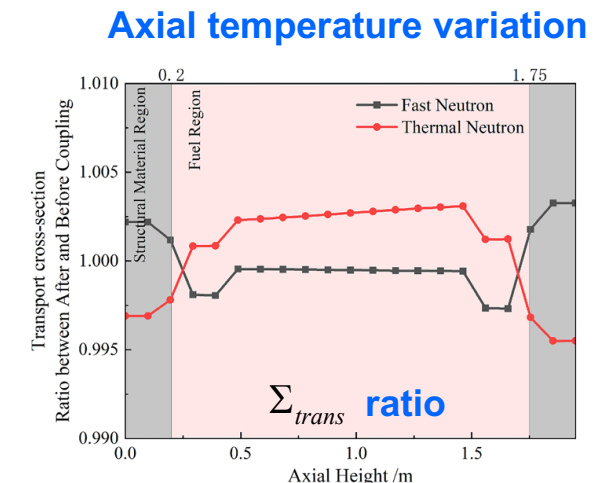
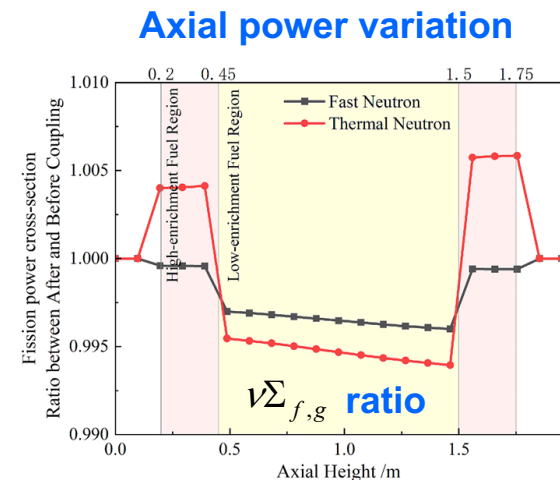
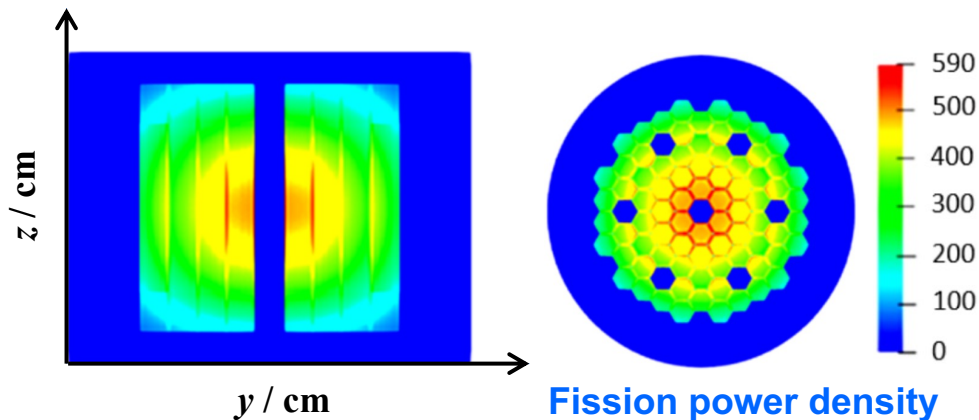
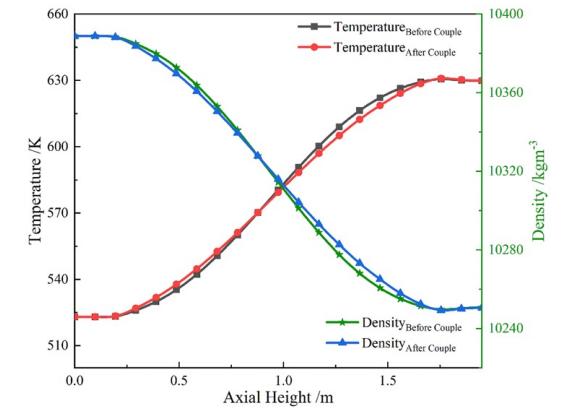
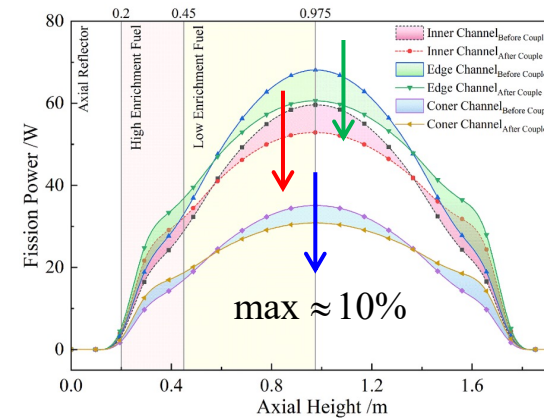
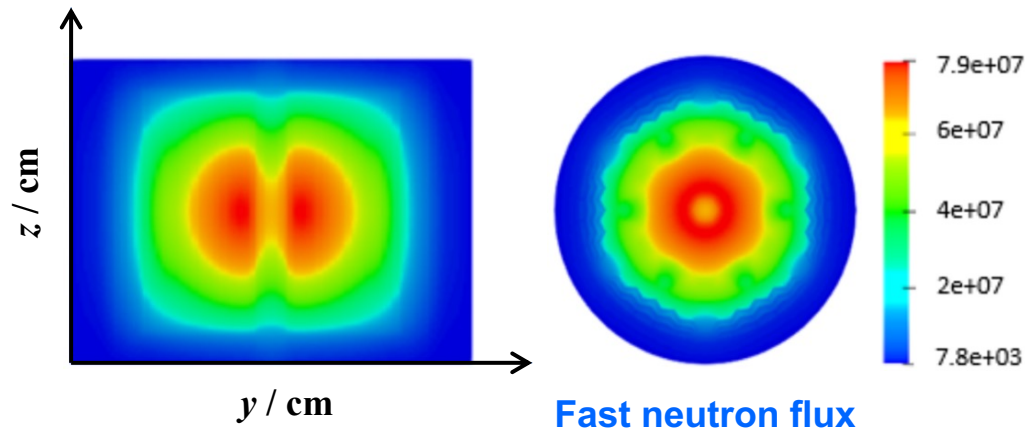


Neutronics/Thermal-hydraulics coupling strategy

3.7 Coupling analysis for LFR

30/38

- The neutronics behaviors solved by KaiyangCore are conducted and validated by Monte-Carlo method.
- The coupling effect of MicroURANUS is pronounced. The axial power is flattened with the max variation of 10% after the coupling, because of remarkable changes of fission and transport group constants.

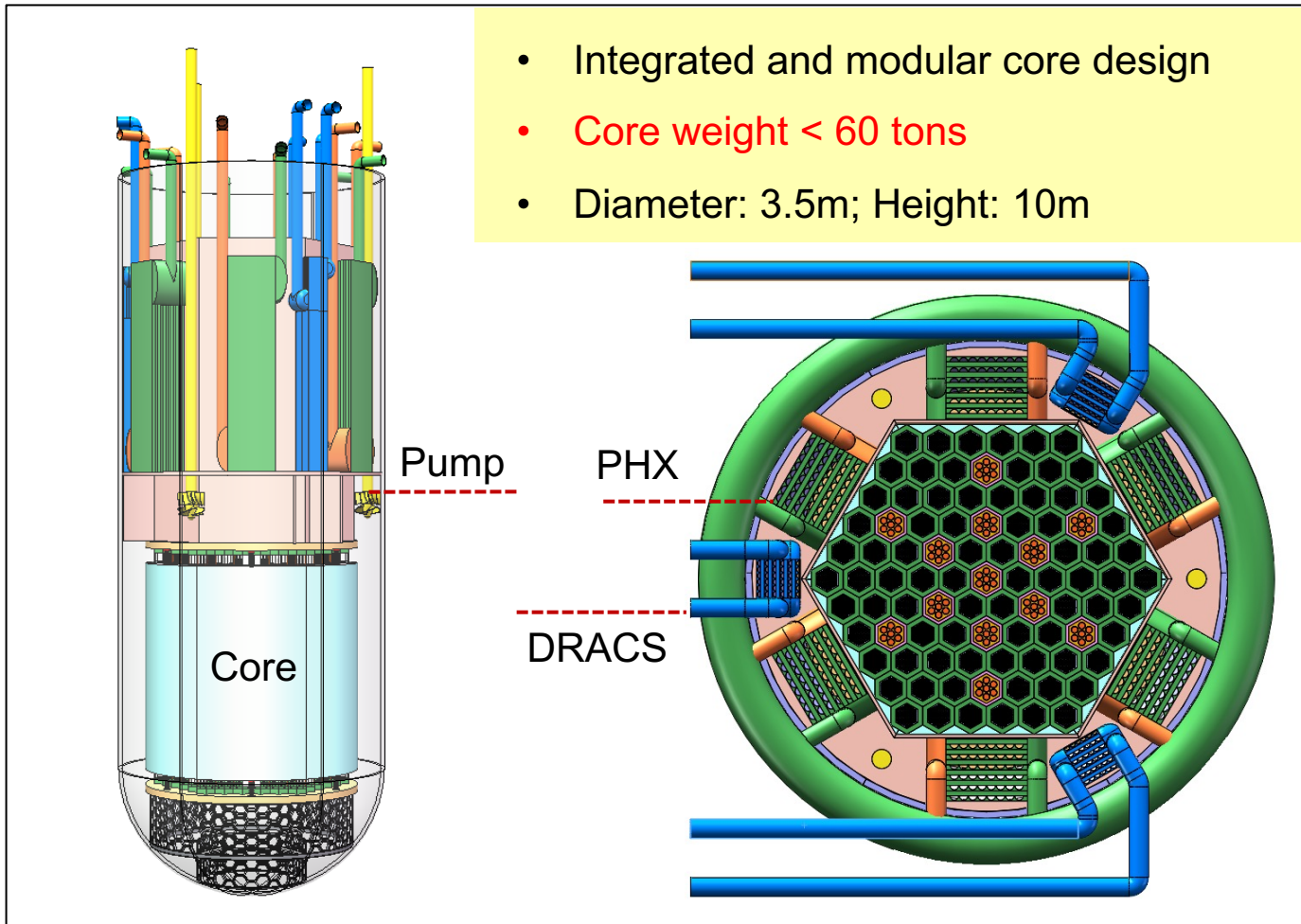


3.8 Coupling analysis for FHR

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固有安全一体化小型氟盐冷却高温堆 — “福星”

FLUORIDE-SALT-COOLED HIGH-TEMPERATURE ADVANCED REACTOR (FuSTAR)



➤ Highway



➤ Railway



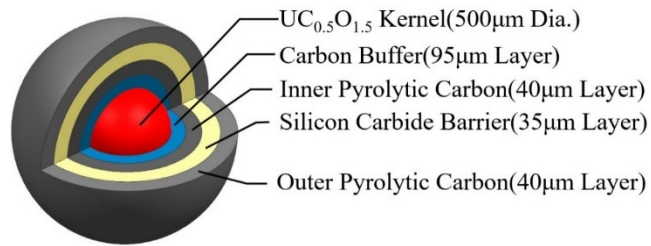
➤ 125 MWth with 973 K outlet



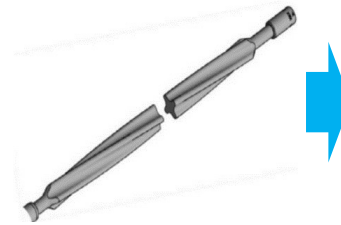
3.9 Coupling analysis for FHR

32/38

- **FUSTAR: A graphite-moderated thermal spectrum core scheme using TRISO particles as fuel, helical cruciform fuel elements, and FLiBe as coolant**



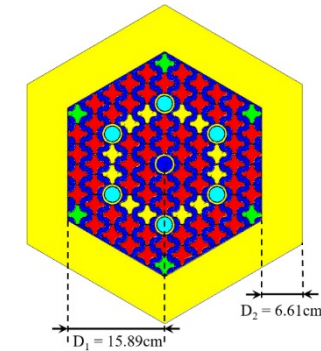
TRISO



Helical cruciform fuel element

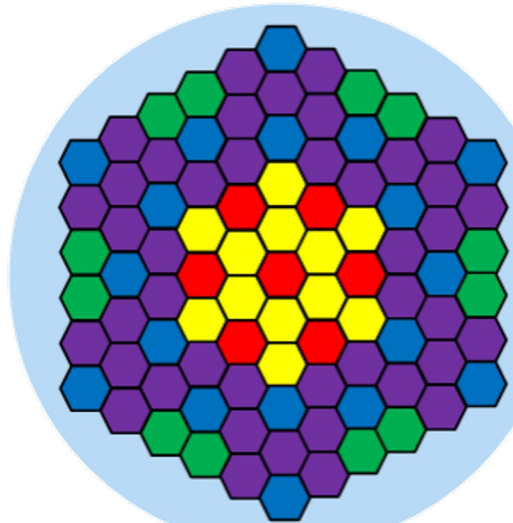


FLiBe

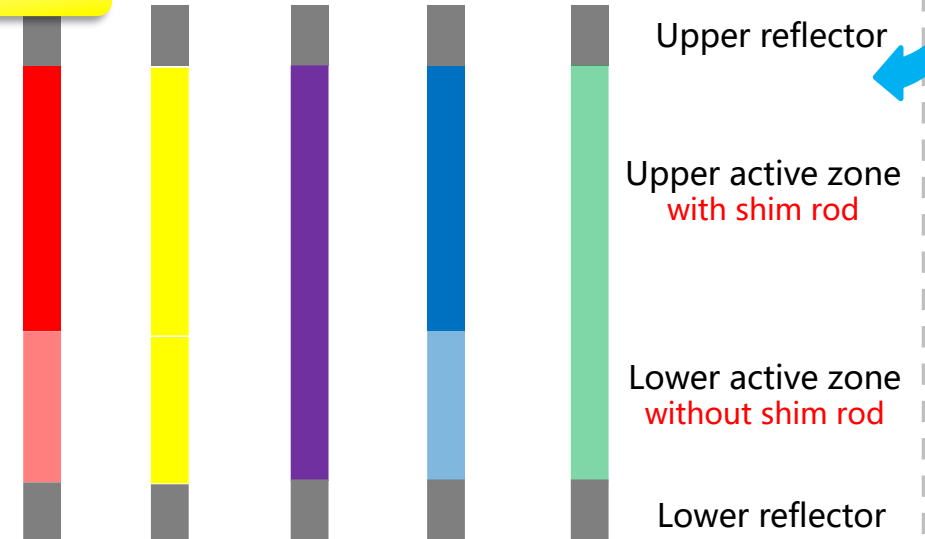


Graphite moderator

Core configuration



- Enrichment: 15%, shim rod
- Enrichment: 15%, without control rod
- Enrichment: 17.5%, without control rod
- Enrichment: 17.5%, shim rod
- Enrichment: 17.5%, safety rod



3.9 Coupling analysis for FHR

33/38

- GeN-FOAM is a **multi-physics** solver developed by **PSI** and **EPFL**, including **thermal-hydraulics**, **neutronics**, and **mechanics**.

$$\frac{\partial \gamma \rho}{\partial t} + \nabla \cdot (\gamma \rho \mathbf{u}) = 0$$

$$\frac{\partial \gamma \rho \mathbf{u}}{\partial t} + \nabla \cdot (\gamma \rho \mathbf{u} \mathbf{u}) = \nabla \cdot (\mu_{eff} \nabla \mathbf{u}) - \gamma \nabla p + \gamma \mathbf{F}_g + \gamma \mathbf{F}_{ss}$$

body force

drag force

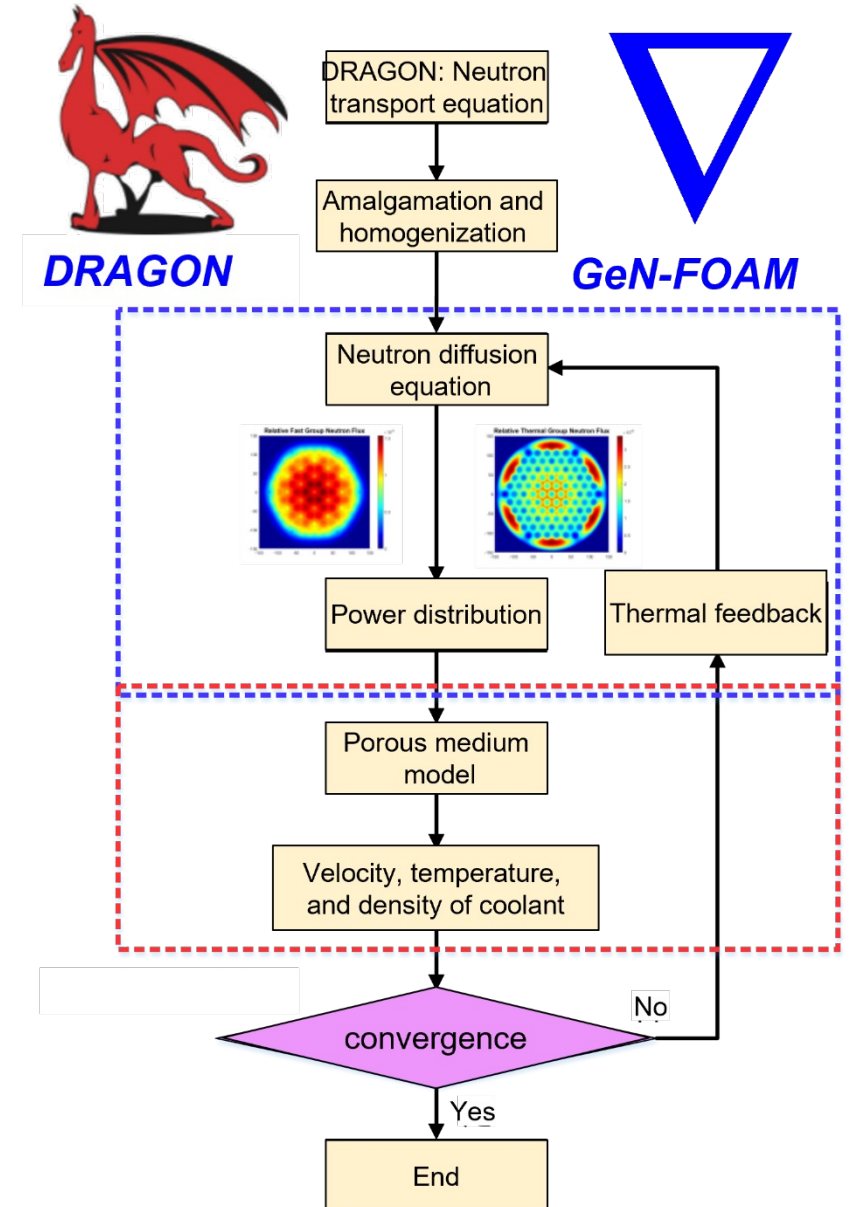
$$\frac{\partial \gamma \rho e}{\partial t} + \nabla \cdot (\gamma \rho \mathbf{u} (\rho e + p)) = \nabla \cdot (\gamma k_{eff} \nabla T) + \gamma Q_{ss} + Q_F + \gamma \mathbf{F}_{ss} \cdot \mathbf{u}$$

**heat source
from structure**

**heat source
from fuel salt**

$$\frac{1}{v_g} \left(\frac{\partial \phi_g}{\partial t} + \nabla \cdot \mathbf{u} \phi_g \right) = \nabla \cdot D_g \nabla \phi_g - \Sigma_{t,g} \phi_g + \sum_{g' \neq g}^G \Sigma_{g' \rightarrow g} \phi_{g'} + \chi_{p,g} (1 - \beta) \sum_{g'=1}^G v \Sigma_{f,g'} \phi_{g'} + \sum_{i=1}^I \chi_{d,i,g} \lambda_i C_i$$

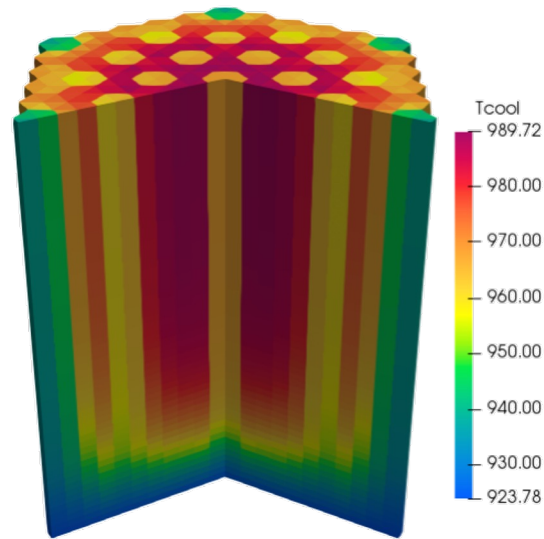
$$\frac{\partial C_i}{\partial t} + \nabla \cdot (\mathbf{u} C_i) = \nabla \cdot \left(\frac{v}{Sc} + \frac{v_t}{Sc_t} \right) \nabla C_i + \beta_i \sum_{g'=1}^G v \Sigma_{f,g'} \phi_{g'} - \lambda_i C_i$$



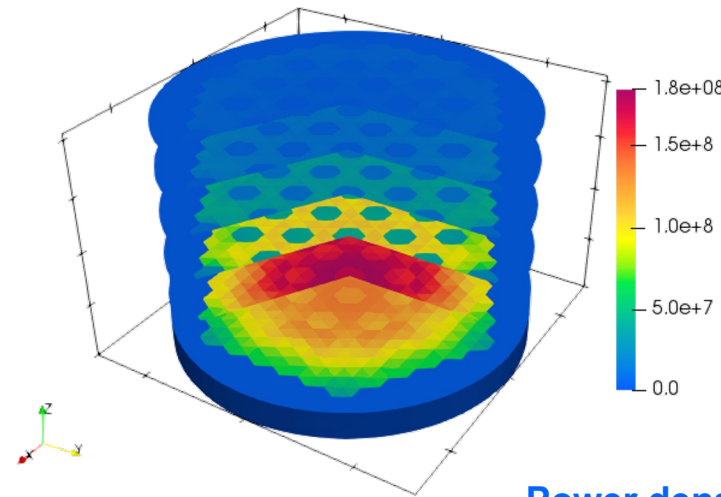
3.9 Coupling analysis for FHR

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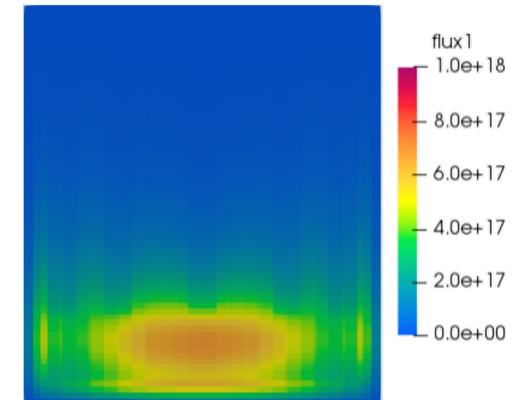
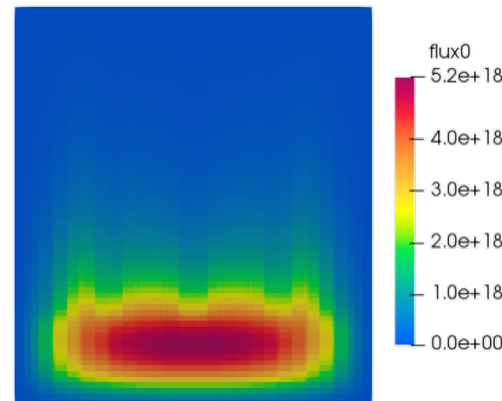
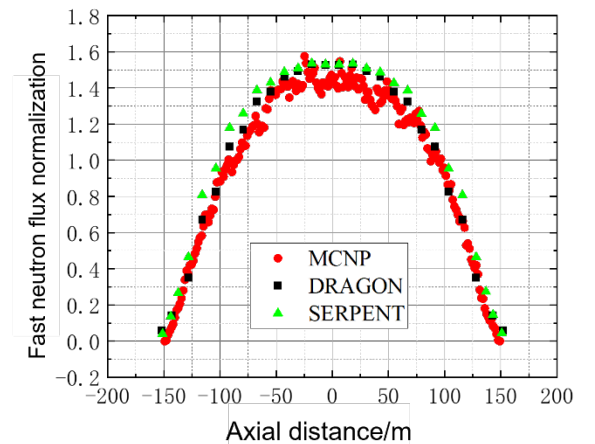
- The neutronics behaviors are conducted and validated by Monte-Carlo method.
- The overall temperature rise of the core was approximately **50K**, which met the design requirements.



Coolant temperature field



Power density distribution

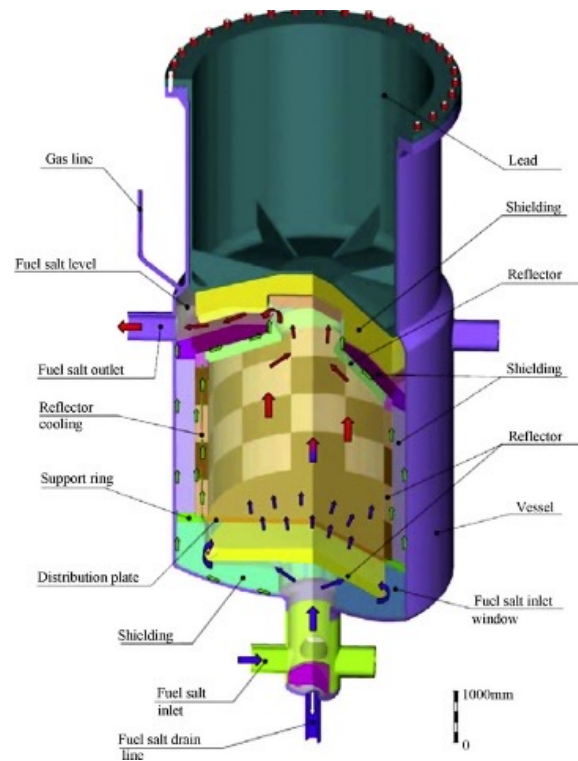


Neutron flux distribution

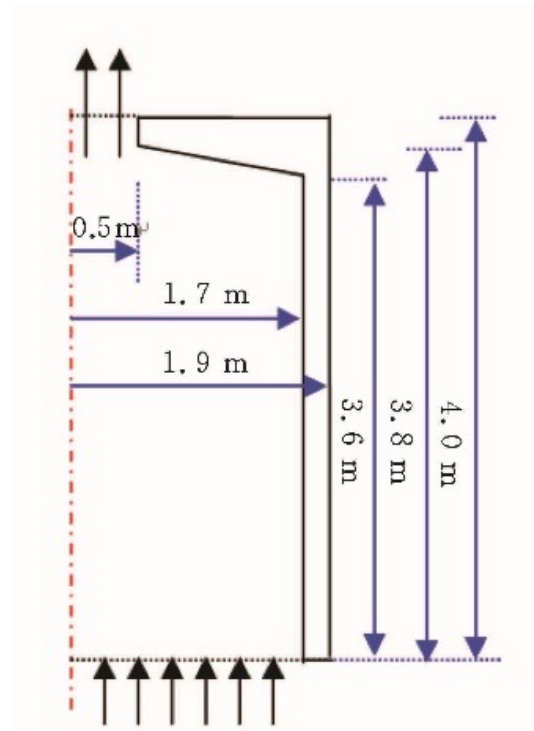
3.9 Coupling analysis for MSR

35/38

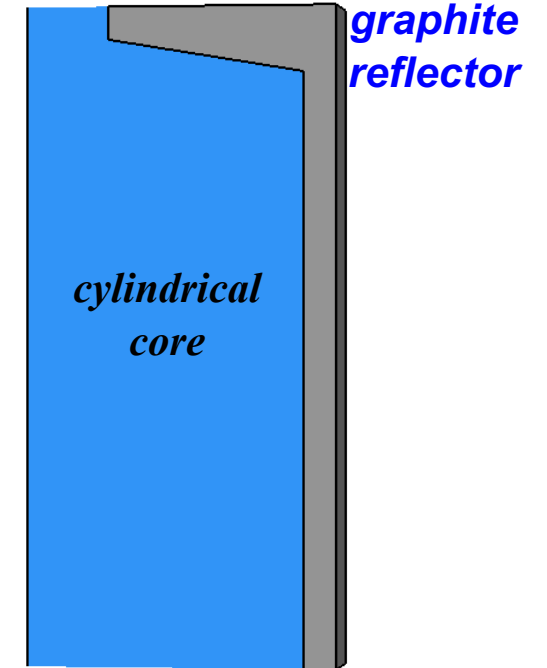
- The concept of **MOSART** was first proposed by the Russian RPC-KI
- MOSART is a **fast spectrum** reactor with a cylindrical core surrounded by a graphite reflector



MOSART



**Simplified
structure**

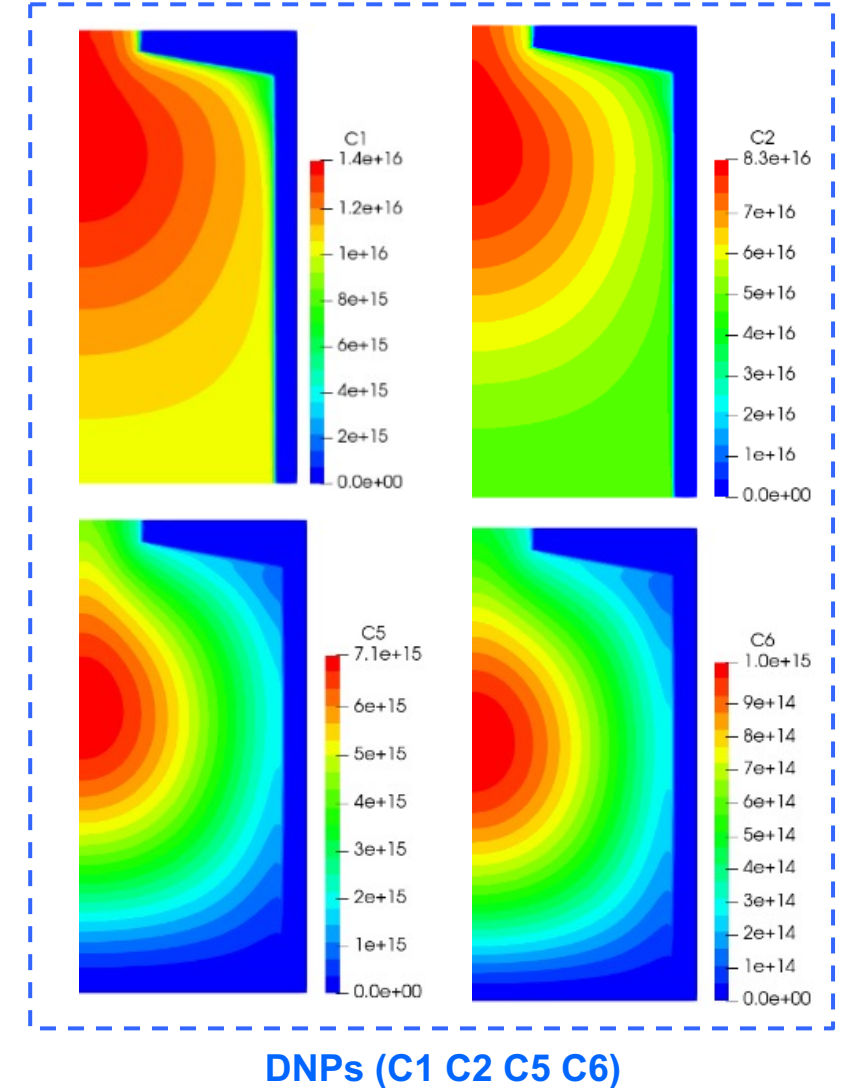
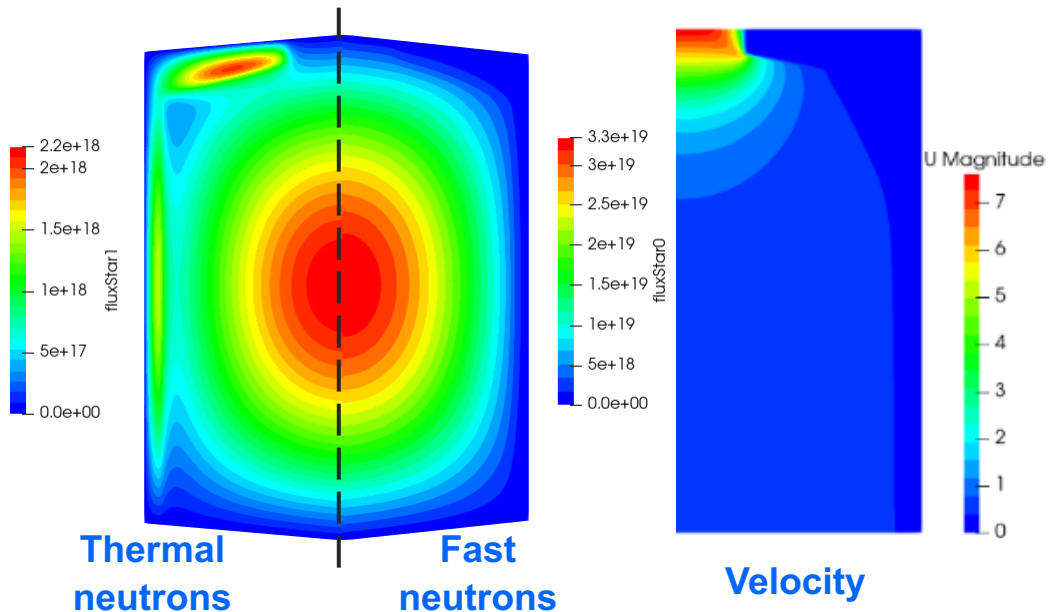


**2D axisymmetric
model**

3.9 Coupling analysis for MSR

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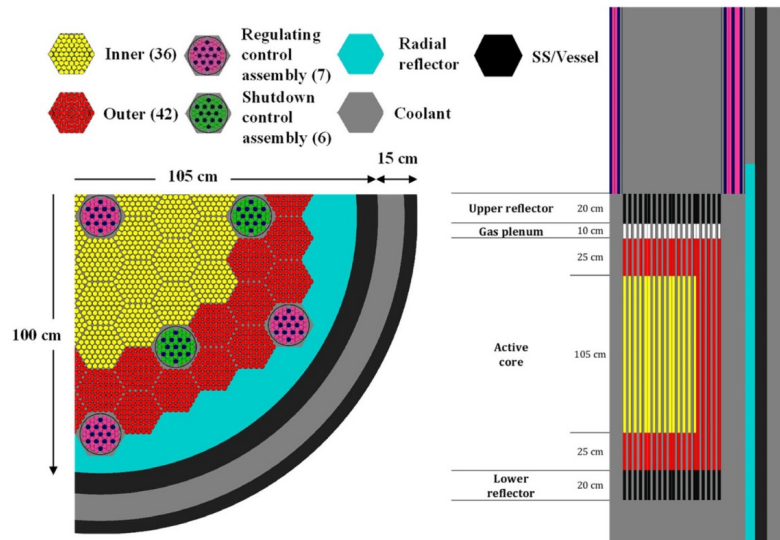
- The **peaks** of both fast and thermal neutron flux occur at the center of the reactor core.
- The flow of molten salt is uniform with the **recirculation** zone forming at the corner.
- **DNPs** move downstream along the flow.



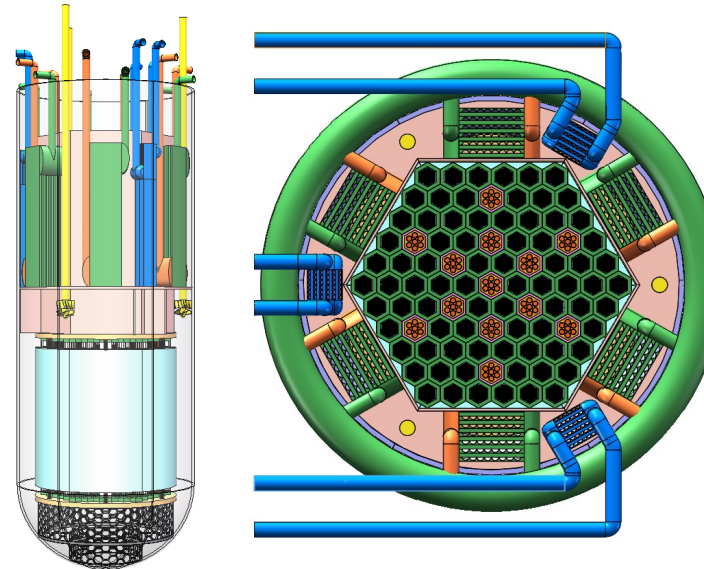
3.10 Summary

37/38

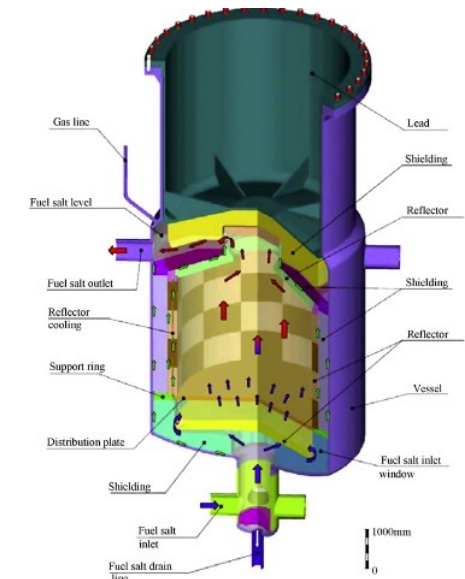
- In the first talk, we mainly focus on the multiphysics modeling of Gen-IV reactors based on **OpenFOAM**.
- Given the merits of powerful FVM operator, equation discretization, and matrix solver, we can flexibly develop our own **neutronics and thermal-hydraulics solvers**.
- Coupling under a unified framework shows advantages on compact and high-fidelity solving, which is practical and conducted on the examples of **LFR**, **FHR**, and **MSR**.



MicroURANUS



FuSTAR



MOSART



Thank You!