# Recent progresses in the development of a new generation adaptive DG dynamical core for RegCM

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### Outline

- Motivation and introduction to the p-SISLDG formulation.
- Review of a novel SISL time integration approach.
- 1 st extension: mass conservative mixed Eulerian/semi-Lagrangian variant.
- 2nd extension: meshes of deformed quadrilaterals on the sphere and on a vertical plane.
- *p*-adaptivity.
- Numerical validation:
  - horizontal:
    - efficiency gain by TR-BDF2: unsteady flow with analytic solution
    - efficiency gain by p-adaptivity: Williamson's test 6
    - effects of the mesh deformation on the solution (mass conservative version): Williamson's test 2 and unsteady flow with analytic solution
  - p-adaptive tracers transport:
    - Solid body rotation
    - Deformational flow
    - Coupling with SWE solver: advection by Rossby-Haurwitz wave
  - vertical:
    - Interacting bubbles test
    - Linear hydrostatic lee waves
    - Nonlinear nonhydrostatic lee waves
- Where is the 3D dycore?? Current status and HPC requirements for using p-SISLDG as a three dimensional dynamical core.



## Motivation

Goal: use DG methods for the design of a new generation dynamical core for the *regional* climate modelling system RegCM of ICTP.

- This is challenging for:
  - stability restrictions with explicit time stepping:

"The RKDG algorithm is stable provided the following condition holds:

$$u\frac{\Delta t}{h} < \frac{1}{2p+1}$$

where p is the polynomial degree; (for the linear case this implies a CFL limit  $\frac{1}{3})"$ 

Cockburn-Shu, Math. Comp. 1989

- computational cost : DG requires more d.o.f. per element than CG .
- How to increase computational efficiency of DG ?
  - coupling DG to semi-implicit semi-Lagrangian (SI-SL) technique (no CFL)
  - introduction of p- adaptivity (flexible degrees of freedom)





### p-SISLDG: main features

Main novel features of the proposed p-SISLDG formulation:

- is the first unconditionally stable DG formulation for the shallow water and for the Euler equations,
- is based on the first fully second order two-time-level SISL time integrator,
- ▶ is the first extensive application of *p*-adaptivity strategies in NWP,
- employs a unified discretization approach for the horizontal and vertical.



### A novel approach for SISL time integration: TR-BDF2

Given a Cauchy problem for a system of ODEs:

the TR-BDF2 method is defined by the two following implicit stages (Bank et al. IEEE trans. 1985):

$$\mathbf{u}^{n+2\gamma} - \gamma \Delta t \mathbf{f}(\mathbf{u}^{n+2\gamma}, t_n + 2\gamma \Delta t) = \mathbf{u}^n + \gamma \Delta t \mathbf{f}(\mathbf{u}^n, t_n), \mathbf{u}^{n+1} - \gamma_2 \Delta t \mathbf{f}(\mathbf{u}^{n+1}, t_{n+1}) = (1 - \gamma_3) \mathbf{u}^n + \gamma_3 \mathbf{u}^{n+2\gamma},$$

with  $\gamma \in (0, 1/2]$  fixed implicitness parameter and

$$\gamma_2 = rac{1-2\gamma}{2(1-\gamma)}, \quad \gamma_3 = rac{1-\gamma_2}{2\gamma}.$$





### SL reinterpretation of TR-BDF2

If suitable semi-Lagrangian approximate evolution operators for scalar and vector valued functions are introduced:  $[E(t^n, \Delta t)G](\mathbf{x}) = G(t^n, \mathbf{x}_D)$ 

where  $\mathbf{x}_D = \mathbf{x} - \int_{t^n}^{t^{n+1}} \mathbf{u}^n \left( \mathbf{X}(t; t^{n+1}, \mathbf{x}) \right) dt$  and  $\mathbf{X}(t; t^{n+1}, \mathbf{x})$  is the solution of:

$$\begin{cases} \frac{d}{dt} \mathbf{X}(t; t^{n+1}, \mathbf{x}) = \mathbf{u}^n \Big( \mathbf{X}(t; t^{n+1}, \mathbf{x}) \Big) \\ \mathbf{X}(t^{n+1}; t^{n+1}, \mathbf{x}) = \mathbf{x} \end{cases}$$



- i.e. *two* steps are required to compute  $[E(t^n, \Delta t)G](\mathbf{x})$ :
  - 1. departure point  $\mathbf{x}_D$  computation (e.g. McGregor, Mon. Wea. Rev., 1993);
  - 2. interpolation of  $G^n$  at departure point.



SL reinterpretation of TR-BDF2

... and if governing equations in advective form are to be solved:

(being  $\frac{D}{Dt}$  the Lagrangian derivative operator)

(SWE) Shallow Water Eqs. (no Coriolis force):

(VSE) Euler eqs. (no Coriolis force) on a Vertical Slice 
$$(\frac{\partial}{\partial y} = 0)$$
:

$$\frac{Dh}{Dt} + h\boldsymbol{\nabla}\cdot\mathbf{u} = \mathbf{0},$$

$$\frac{D\mathbf{u}}{Dt} + g\boldsymbol{\nabla}h = -g\boldsymbol{\nabla}b,$$

$$\frac{D\Pi}{Dt} + \left(\frac{c_{\rho}}{c_{v}} - 1\right) \Pi \nabla \cdot \mathbf{u} = 0,$$

$$\frac{Du}{Dt} + c_{\rho} \Theta \frac{\partial \pi}{\partial x} = 0,$$

$$\frac{Dw}{Dt} + c_{\rho} \Theta \frac{\partial \pi}{\partial z} - g \frac{\theta}{\theta^{*}} = 0,$$

$$\frac{D\theta}{Dt} + w \frac{d\theta^{*}}{dz} = 0.$$

with  $h, \mathbf{u} = (u, v)^T$  and *b* being fluid depth, horizontal velocity and bathymetry elevation respectively,

with  $\Theta = T(\frac{p}{p_0})^{-R/c_p}, \Pi = (\frac{p}{p_0})^{R/c_p}, p, T, \mathbf{u} = (u, w)^T$ , pressure, temperature and vertical velocity,  $c_p, c_v, R$  specific heats and gas constant of dry air, and

$$\Pi(x, y, z, t) = \pi^{*}(z) + \pi(x, y, z, t),$$
  

$$\Theta(x, y, z, t) = \theta^{*}(z) + \theta(x, y, z, t),$$

... then SISL-TR steps for SWE and VSE are isomorphic

$$h^{n+2\gamma} + \gamma \Delta t \ h^n \ \nabla \cdot \mathbf{u}^{n+2\gamma} = E\left(t^n, 2\gamma \Delta t\right) \left[h - \gamma \Delta t \ h \ \nabla \cdot \mathbf{u}\right],$$

 $\begin{aligned} \mathbf{u}^{n+2\gamma} + \gamma \Delta t \ g \boldsymbol{\nabla} h^{n+2\gamma} &= -\gamma \Delta t \ g \boldsymbol{\nabla} b \\ + E(t^n, 2\gamma \Delta t) \left\{ \mathbf{u} - \gamma \Delta t \left[ g(\boldsymbol{\nabla} h + \boldsymbol{\nabla} b) \right] \right\}. \end{aligned}$ 

$$\pi^{n+2\gamma} + \gamma \Delta t \ (c_{\rho}/c_{\nu} - 1) \Pi^{n} \nabla \cdot \mathbf{u}^{n+2\gamma} = -\pi^{*}$$
  
+  $E(t^{n}, 2\gamma \Delta t) [\Pi - \gamma \Delta t (c_{\rho}/c_{\nu} - 1) \Pi \nabla \cdot \mathbf{u}],$ 

$$u^{n+2\gamma} + \gamma \Delta t \ c_p \Theta^n \frac{\partial \pi}{\partial x}^{n+2\gamma} = \\ E(t^n, 2\gamma \Delta t) \left[ u - \gamma \Delta t \ c_p \Theta \frac{\partial \pi}{\partial x} \right],$$

$$\begin{split} & \left(1 + (\gamma \Delta t)^2 \frac{g}{\theta^*} \frac{d\theta^*}{dz}\right) w^{n+2\gamma} + \gamma \Delta t c_p \Theta^n \frac{\partial \pi}{\partial z}^{n+2\gamma} = \\ & E(t^n, 2\gamma \Delta t) \left[ w - \gamma \Delta t \left( c_p \Theta \frac{\partial \pi}{\partial z} - g \frac{\theta}{\theta^*} \right) \right] \\ & + \gamma \Delta t \frac{g}{\theta^*} E(t^n, 2\gamma \Delta t) \left[ \theta - \gamma \Delta t \frac{d\theta^*}{dz} w \right]. \end{split}$$

$$\begin{array}{cccc} h & \longleftrightarrow & \pi, \\ u & \longleftrightarrow & u, \\ v & \longleftrightarrow & W. \end{array}$$



 $h^{n+1} + \gamma_2 \Delta t \ h^{n+2\gamma} \ \nabla \cdot \mathbf{u}^{n+1} = (1 - \gamma_3) E(t^n, \Delta t) h \\ + \gamma_3 E(t^n + 2\gamma \Delta t, (1 - 2\gamma) \Delta t) h,$ 

 $+\gamma_3 E(t^n+2\gamma\Delta t,(1-2\gamma)\Delta t)\mathbf{u}.$ 

 $\mathbf{u}^{n+1} + \gamma_2 \Delta t \ g \nabla h^{n+1} =$ 

 $-\gamma_2 \Delta t \ g \nabla b$  $+(1-\gamma_3) E(t^n, \Delta t) \mathbf{u}$ 

$$\begin{aligned} \pi^{n+1} + \gamma_2 \Delta t \left( c_p / c_v - 1 \right) \Pi^{n+2\gamma} \nabla \cdot \mathbf{u}^{n+1} &= \\ -\pi^* + (1 - \gamma_3) [E \left( t^n, \Delta t \right) \Pi] \\ + \gamma_3 [E \left( t^n + 2\gamma \Delta t, (1 - 2\gamma) \Delta t \right) \Pi], \end{aligned}$$

$$u^{n+1} + \gamma_2 \Delta t \ c_{\rho} \Theta^{n+2\gamma} \frac{\partial \pi}{\partial x}^{n+1} = (1 - \gamma_3) [E(t^n, \Delta t) u] + \gamma_3 [E(t^n + 2\gamma \Delta t, (1 - 2\gamma) \Delta t) u],$$

$$\begin{pmatrix} 1 + (\gamma_2 \Delta t)^2 \frac{g}{\theta^*} \frac{d\theta^*}{dz} \end{pmatrix} w^{n+1} + \gamma_2 \Delta t \ c_\rho \Theta^{n+2\gamma} \frac{\partial \pi^{n+1}}{\partial z} = \\ (1 - \gamma_3)[E(t^n, \Delta t) \ w] + \gamma_3[E(t^n + 2\gamma \Delta t, (1 - 2\gamma)\Delta t) \ w] + \\ \gamma_2 \Delta t \frac{g}{\theta^*} \left\{ (1 - \gamma_3)[E(t^n, \Delta t) \ \theta] + \gamma_3[E(t^n + 2\gamma \Delta t, (1 - 2\gamma)\Delta t) \ \theta] \right\}$$

$$\begin{array}{cccc} h & \longleftrightarrow & \pi, \\ u & \longleftrightarrow & u, \\ v & \longleftrightarrow & W. \end{array}$$



#### 1st Extension: mass conservation, SISL-TR-BDF2 time discretization

Considering the continuity equation in Eulerian flux form, while the momentum one in advective vector form:

$$rac{\partial \eta}{\partial t} = - \boldsymbol{\nabla} \cdot (h \mathbf{u}), \ rac{D \mathbf{u}}{D t} = -g \boldsymbol{\nabla} \eta - f \mathbf{k} imes \mathbf{u},$$

then, the TR stage of the SISL time discretization of previous equations is:

$$\eta^{n+2\gamma} + \gamma \Delta t \, \nabla \cdot \left( h^n \mathbf{u}^{n+2\gamma} \right) = \eta^n - \gamma \Delta t \, \nabla \cdot \left( h^n \mathbf{u}^n \right),$$
$$\mathbf{u}^{n+2\gamma} + \gamma \Delta t \left( g \nabla \eta^{n+2\gamma} + f \mathbf{k} \times \mathbf{u}^{n+2\gamma} \right)$$
$$= E(t^n, 2\gamma \Delta t) \left[ \mathbf{u} - \gamma \Delta t \left( g \nabla \eta + f \mathbf{k} \times \mathbf{u} \right) \right].$$

The TR stage is then followed by the BDF2 stage:

$$\eta^{n+1} + \gamma_2 \Delta t \, \nabla \cdot (h^{n+2\gamma} \mathbf{u}^{n+1}) = (1 - \gamma_3) \eta^n + \gamma_3 \eta^{n+2\gamma},$$
  
$$\mathbf{u}^{n+1} + \gamma_2 \Delta t \left( g \nabla \eta^{n+1} + f \mathbf{k} \times \mathbf{u}^{n+1} \right)$$
  
$$= (1 - \gamma_3) E(t^n, \Delta t) \mathbf{u} + \gamma_3 E(t^n + 2\gamma \Delta t, (1 - 2\gamma) \Delta t) \mathbf{u}.$$



### DG space discretization

Defined a tassellation T<sub>h</sub> = {K<sub>l</sub>}<sup>N</sup><sub>l=1</sub> of domain Ω and chosen ∀K<sub>l</sub> ∈ T<sub>h</sub> three integers p<sup>π</sup><sub>l</sub> ≥ 0, p<sup>θ</sup><sub>l</sub> ≥ 0, p<sup>θ</sup><sub>l</sub> ≥ 0, at each time level t<sup>n</sup>, we are looking for approximate solution s.t.

$$\begin{array}{rcl} h^n, \pi^n & \in & \mathcal{P}_h := \left\{ f \in L^2(\Omega) \, : \, f|_{\mathcal{K}_l} \in \mathbb{Q}_{p_l^n}(\mathcal{K}_l) \right\} \\ \theta^n & \in & \mathcal{T}_h := \left\{ f \in L^2(\Omega) \, : \, f|_{\mathcal{K}_l} \in \mathbb{Q}_{p_l^0}(\mathcal{K}_l) \right\} \\ u^n, v^n, w^n & \in & V_h := \left\{ g \in L^2(\Omega) \, : \, g|_{\mathcal{K}_l} \in \mathbb{Q}_{p_l^0}(\mathcal{K}_l) \right\}, \end{array}$$

- modal bases are used to span  $P_h$ ,  $T_h$ ,  $V_h$ ,
- L<sup>2</sup> projection against test functions (chosen equal to the basis functions),
- introduction of (centered) numerical fluxes,
- ► substitution of velocity d.o.f. from momentum eqs. into the continuity eq.,
- give raise, at each SI step, to a discrete (vector) Helmholtz equation in the fluid depth / pressure unknown only,

i.e. a sparse block structured nonsymmetric linear system is solved by GMRES with *block* diagonal (for the moment) preconditioning.





Potential of p-adaptivity for atmospheric modelling applications

- No remeshing required of many physical quantities like orography profiles, data on land use and soil type, land-sea masks.
- Completely independent resolution for each single model variable.
- Easier coupling with SL technique, especially on unstructured meshes (no need to store two meshes).
- Possibility also of static p-adaptation: e.g. reduced p as counterpart of reduced grid, i.e. locally imposed p controlling the local Courant number (=> significant #gmres-iterations reduction).
- Main potential problem: dynamic load balancing is mandatory for massively parallel implementations.



#### 2nd extension: mesh deformation on the sphere







2nd extension: mesh deformation on a vertical plane, topography in z coordinate









**Numerical Validation** 



Shallow Water Equations (SWE) on the sphere



### Unsteady flow with analytic solution (Läuter 2005): TR-BDF2 vs off centerd Crank Nicolson

$N_x \times N_y$	$\Delta t$	l <sub>1</sub> (h)	$l_2(h)$	$I_{\infty}(h)$	$q_2^{emp}$
$ \begin{array}{cccc} 10 \times & 5 \\ 20 \times 10 \\ 40 \times 20 \\ 80 \times 40 \end{array} $	3600 1800 900	$5.46 \times 10^{-3}$ $1.25 \times 10^{-3}$ $3.04 \times 10^{-4}$ $7.55 \times 10^{-5}$	$6.12 \times 10^{-3} \\ 1.40 \times 10^{-3} \\ 3.41 \times 10^{-4} \\ 8.47 \times 10^{-5} \\ 10^{-5$	$9.54 \times 10^{-3} \\ 2.14 \times 10^{-3} \\ 5.21 \times 10^{-4} \\ 1.20 \times 10^{-4}$	- 2.1 2.0

Relative errors for TR-BDF2 at different resolutions, Δt in seconds:

• Relative errors for off-centered Crank Nicolson ( $\theta = 0.6$ ) at different resolutions:

$N_x \times N_y$	$\Delta t$	l <sub>1</sub> (h)	$l_2(h)$	$I_{\infty}(h)$	$q_2^{emp}$
10 × 5	3600	$1.44  imes 10^{-2}$	$1.63  imes 10^{-2}$	$2.40 imes10^{-2}$	-
20  imes 10	1800	$8.74 imes10^{-3}$	$9.89  imes 10^{-3}$	$1.44  imes 10^{-2}$	0.7
40  imes 20	900	$4.81  imes 10^{-3}$	$5.45  imes 10^{-3}$	$7.96  imes 10^{-3}$	0.9
80  imes 40	450	$2.53  imes 10^{-3}$	$2.86  imes 10^{-3}$	$4.18  imes 10^{-3}$	0.9

- At max. resolution in space and time (80 × 40 el., Δt = 450s) error norms for TR-BDF2 are around 34 times smaller than those of off-centered Crank Nicolson, while CPU time is equivalent (104.3s for a time step of TR-BDF2 vs 99.9s for a time step of off centerd CN).
- At fixed resolution in space (40 × 20 el.), off centered Crank Nicolson needs to be run with a 16 times smaller Δt in order to reach same level of accuracy of TR-BDF2 with Δt = 900s. ⇒ CPU time for TR-BDF2 is around 20% that of off-centered CN for same accuracy.



### Combination of static + dynamic p-adaptation: Williamson's test 6

 $64 \times 32$  elements,  $\max p^h = 4$ ,  $\Delta t = 900s$  ( $C_{cel} \approx 83$  without adaptivity).

$$\frac{\text{\#gmres-iterations}(p^h = \text{adapted})}{\text{\#gmres-iterations}(p^h = \text{uniform})} \approx 13\%, \quad \Delta_{dof}^n = \frac{\sum_{l=1}^N (p_l^n + 1)^2}{N(p_{max} + 1)^2} \approx 45\%.$$



### Williamson's test 6: time convergence rate and p-adaptation efficiency

Relative errors at t<sub>f</sub> = 15 days for different number of elements, with respect to NCAR spectral model solution at resolution T511:

$N_x  imes N_y$	$\Delta t$ [min]	$l_1(h)$	$l_2(h)$	$I_{\infty}(h)$	$q_{\scriptscriptstyle 2}^{\scriptscriptstyle emp}$
10 × 5	60	$2.92\times10^{-2}$	$3.82  imes 10^{-2}$	$6.75 imes10^{-2}$	-
20  imes 10	30	$5.50  imes 10^{-3}$	$6.80  imes 10^{-3}$	$1.11  imes 10^{-2}$	2.4
$40\times 20$	15	$1.40  imes 10^{-3}$	$1.80  imes 10^{-3}$	$3.20 imes10^{-3}$	2.0

► Relative differences btw adaptive (tol. 
equal = 10<sup>-2</sup>) and nonadaptive solution at t<sub>f</sub> = 15 days:

adaptivity	<i>l</i> <sub>1</sub> ( <i>h</i> )	$l_2(h)$	$I_{\infty}(h)$
static static + dynamic	$\begin{array}{c} 2.182 \times 10^{-4} \\ 3.407 \times 10^{-4} \end{array}$	$\begin{array}{c} 3.434 \times 10^{-4} \\ 4.301 \times 10^{-4} \end{array}$	$\begin{array}{c} 2.856 \times 10^{-4} \\ 7.484 \times 10^{-4} \end{array}$

 CPU time: static and dynamic p-adaptive solution execution time is around 24% of that for nonadaptive solution.



#### Williamson's test 6: deformed vs. aligned mesh

 $p^{\eta} = 4$ ,  $p^{u} = 5$ ,  $N_x \times N_y = 32 \times 16$ ,  $t_f = 15$  days



Mass conservative formulation on deformed mesh: convergence rate, Williamson's test 2

$$p^{\eta} = p^{u} = 3$$

$N_x \times N_y$	$\Delta t[s]$	$I_1(\eta)$	$I_2(\eta)$	$I_\infty(\eta)$	$q_2^{emp}$
20 × 10	1800	$5.59 imes10^{-5}$	$8.39 imes10^{-5}$	$1.20 imes10^{-3}$	-
$40\times 20$	900	$5.84 imes10^{-6}$	$8.66 imes10^{-6}$	$1.67 imes10^{-4}$	3.3
80  imes 40	450	$7.50  imes 10^{-7}$	$1.02  imes 10^{-6}$	$6.88  imes 10^{-6}$	3.1
$N_x  imes N_y$	$\Delta t[s]$	$l_1(u)$	$I_2(u)$	$I_{\infty}(u)$	$q_2^{emp}$
20  imes 10	1800	$7.72  imes 10^{-4}$	$1.51  imes 10^{-3}$	$1.35 imes10^{-2}$	-
40 imes 20	900	$7.46 imes10^{-5}$	$2.78 imes10^{-4}$	$6.77 imes10^{-3}$	2.5
$80\times40$	450	$4.69 imes10^{-6}$	$1.00  imes 10^{-5}$	$2.03 imes10^{-4}$	4.8
$N_x  imes N_y$	$\Delta t[s]$	$l_1(v)$	$l_2(v)$	$I_{\infty}(v)$	$q_2^{emp}$
20  imes 10	1800	$8.23\times10^{-4}$	$1.09  imes 10^{-3}$	$9.98 imes10^{-3}$	-
40 imes 20	900	$7.87 imes10^{-5}$	$1.58 imes10^{-4}$	$2.66 imes10^{-3}$	2.8
$80\times40$	450	$8.12 imes10^{-6}$	$1.84 imes10^{-5}$	$4.70 imes10^{-4}$	3.1



Mass conservative formulation: errors for deformed vs. aligned mesh, unsteady flow with analytic solution (Läuter 2005)

$$p^{\eta} = 4$$
,  $p^{u} = 5$ ,  $N_{x} \times N_{y} = 20 \times 10$ ,  $t_{f} = 5$  days

mesh	$h_1(\eta)$	$l_2(\eta)$	$I_{\infty}(\eta)$
distorted	$1.574439  imes 10^{-3}$	$2.015191  imes 10^{-3}$	$6.223918  imes 10^{-3}$
aligned	$1.574433  imes 10^{-3}$	$2.015189  imes 10^{-3}$	$6.220938  imes 10^{-3}$
mesh	$l_1(u)$	$l_2(u)$	$I_{\infty}(u)$
distorted	$3.062825  imes 10^{-2}$	$3.816815  imes 10^{-2}$	$7.295160  imes 10^{-2}$
aligned	$3.062796  imes 10^{-2}$	$3.816801  imes 10^{-2}$	$7.293568  imes 10^{-2}$
mesh	$l_1(v)$	$l_2(v)$	$I_{\infty}(v)$
distorted	$2.105254  imes 10^{-2}$	$2.195037  imes 10^{-2}$	$3.832416  imes 10^{-2}$
aligned	$2.105328  imes 10^{-2}$	$2.195039  imes 10^{-2}$	$3.833373  imes 10^{-2}$



*p*-adaptive tracers advection



### Solid body rotation on the sphere

 $120 \times 60$  elements, max  $p^c = 4$ ,  $\Delta t = 7200$ s,  $C_{vel,x} \approx 400$ ,  $C_{vel,y} \approx 4$ 



#### Deformational flow on the sphere (adapted from Nair, Lauritzen 2010)

 $80 \times 40$  elements, max  $p^c = 4$ ,  $\Delta t = 1800$ s



#### Rossby Haurwitz wave velocity field

 $120 \times 60$  elements, max  $p^c = 4$ ,  $\Delta t = 900s$ ,  $C_{vel,x} \approx 1$ 



Euler equations on a Vertical Slice (VSE)



#### Warm bubble test (Carpenter et al., MWR 1990) 49 × 60 elements, $p^{\pi} = 4$ , $p^{u} = 5$ , $\Delta t = 1$ s, $C \approx 18$ .

variable	<i>I</i> 1	<i>l</i> <sub>2</sub>	$I_{\infty}$
π	$2.744  imes 10^{-3}$	$4.92  imes 10^{-3}$	$3.86 \times 10^{-2}$
$\theta$	$1.70  imes 10^{-2}$	$4.38  imes 10^{-2}$	$9.34 imes10^{-2}$
и	$3.64 imes10^{-4}$	$1.14  imes 10^{-3}$	$3.60  imes 10^{-2}$



### Interacting bubbles test (Robert, 1993)

 $50 \times 50$  elements,  $p^{\pi} = 4$ ,  $p^{u} = 5$ ,  $\Delta t = 1$  s,  $C \approx 87$ .



#### Linear hydrostatic lee waves

 $60 \times 50$  elements,  $p^{\pi} = 4$ ,  $p^{u} = 5$ ,  $\Delta t = 7$  s,  $C_{V} \approx 7$ ,  $C_{H} \approx 9$ .

(maximum space resolution 2 km)



#### Linear hydrostatic lee waves

 $60 \times 50$  elements,  $p^{\pi} = 4$ ,  $p^{u} = 5$ ,  $\Delta t = 7$  s,  $C_{V} \approx 7$ ,  $C_{H} \approx 9$ .





#### Linear hydrostatic lee waves: adaptive run

 $60 \times 50$  elements,  $p^{\pi} = p^{u} = 4$ ,  $\Delta t = 7$  s,  $C_{V} \approx 7$ ,  $C_{H} \approx 9$ .

(maximum space resolution 2 km)



#### Nonlinear nonhydrostatic lee waves

 $60 \times 50$  elements,  $p^{\pi} = 4$ ,  $p^{u} = 5$ ,  $\Delta t = 2$  s,  $C_{V} \approx 25$ ,  $C_{H} \approx 13$ .

(maximum space resolution 200m)



#### Nonlinear nonhydrostatic lee waves

 $60 \times 50$  elements,  $p^{\pi} = 4$ ,  $p^{u} = 5$ ,  $\Delta t = 2$  s,  $C_{V} \approx 25$ ,  $C_{H} \approx 13$ .





#### Nonlinear nonhydrostatic lee waves: adaptive run

 $100 \times 50$  elements,  $p^{\pi} = p^{u} = 4$ ,  $\Delta t = 2$  s,  $C_{V} \approx 25$ ,  $C_{H} \approx 13$ .

(maximum space resolution 200m)



## Main challenges towards p-SISLDG parallelization

 semi-implicit stencil requires communication



 semi-Lagrangian advection stencil requires communication as well



 dynamic p-adaptivity requires dynamic load balancing



Where is the 3D dynamical core ??



### Preliminary results with the 3D dycore

Solid body advection of a tracer concentration:

Eulerian formulation,

explicit Runge-Kutta 4 time integrator.



### Towards a three dimensional dynamical core

- Up to now, no general HPC infrastructures for efficient and natively p-adaptive implementations of DG methods on massively parallel were available;
- hence a new design of the three dimensional code was needed by using
  - indirect adressing for the elements;
  - direct adressing for element degrees of freedom;
  - advanced data types (object-oriented programming);
  - global arrays of pointers to local data structures to avoid the use of linked lists and to make easier the migration of elements between processes;
- this is the basis for the parallel programming design of p-SISLDG around these criteria:
  - SPMD style programming (like MPI + OpenMP);
  - dynamic load balancing based for example on the use of Space Filling Curves (SFCs) (under evaluation as other options like collection of adaptive octrees);
  - overlap between computation and communication;
  - adoption of standards / reduction use of external libraries (for example by use of Fortran coarrays).



### Open issues and future perspectives

- Improvement of the linear solver for the SI step: hierachical Krylov solver;
- introduction of the SL discretization of diffusive terms; (see L. Bonaventura and R. Ferretti, SIAM J. Sci. Comp. 2014);
- development of a conservative fully semi-Lagrangian version (along the lines of M. Restelli, M. Bonaventura, R. Sacco, J. Comput. Phys., 2006);
- from next October available a new resource (provided by Politecnico di Milano and OGS whithin the HPC-TRES framework) working on related topics.



### Conclusions

- a novel TR-BDF2-based SISL discretization has been presented within the DG framework for the rotating SWE as well as for the Euler equations on a vertical slice, that can be effectively applied to all geophysical scale flows.
  - The resulting scheme is
    - unconditionally stable,
    - full second order accurate in time,
    - arbitrary high order in space,
    - adapting the number of degrees of freedom in each element in order to balance accuracy and computational cost,
    - extended to deformed meshes with no grid imprinting and extendable to arbitrary non-structured even non-conforming meshes,
    - equipped with mass conservative version,
    - multiscale i.e. the same unified model (and therefore architecture) can be successfully run at a range of scales from global to regional (self generation of BC's).
  - Numerical experiments confirm the potential of the proposed formulation.
  - Parallel 3D version at advanced stage of development (nontrivial challenge from the HPC side).



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# THANK YOU FOR YOUR ATTENTION!

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### Dynamic p-adaptation: the strategy

- p-adaptivity easier by the use of modal bases: here tensor products of Legendre polynomials;
- hence, the representation for a model variable  $\alpha$  becomes  $(I = (I_x, I_y)$  multi-index):

$$\alpha(\mathbf{x})\big|_{K_{l}} = \sum_{k=1}^{p_{l}^{\alpha}+1} \sum_{l=1}^{p_{l}^{\alpha}+1} \alpha_{l,k,l} \psi_{l_{x},k}(x) \psi_{l_{y},l}(y).$$

and its 2-norm is given by (in planar geometry):



- while the quantity  $w_l^r = \sqrt{\frac{\varepsilon_l^r}{\varepsilon_l^{rot}}}$  will measure the relative 'weight' of the *r* degree modes
- Given an error tolerance ε<sub>I</sub> > 0 for all I = 1,..., N, at each time step repeat following steps:
   1) compute w<sub>pj</sub>
  - 2.1) if  $w_{p_i} \ge \epsilon_i$ , then 2.1.1) set  $p_i(\alpha) := p_i(\alpha) + 1$ 2.1.2) set  $\alpha_{i,p_i} = 0$ , exit the loop and go the next element

#### 2.2) if instead $w_{p_i} < \epsilon_i$ , then 2.2.1) compute $w_{p_i-1}$ 2.2.2) if $w_{p_i-1} \ge \epsilon_i$ , exit the loop and go the next element 2.2.3) else if $w_{p_i-1} < \epsilon_i$ , set $p_i(\alpha) := p_i(\alpha) - 1$ and go back to 2.2.1.

