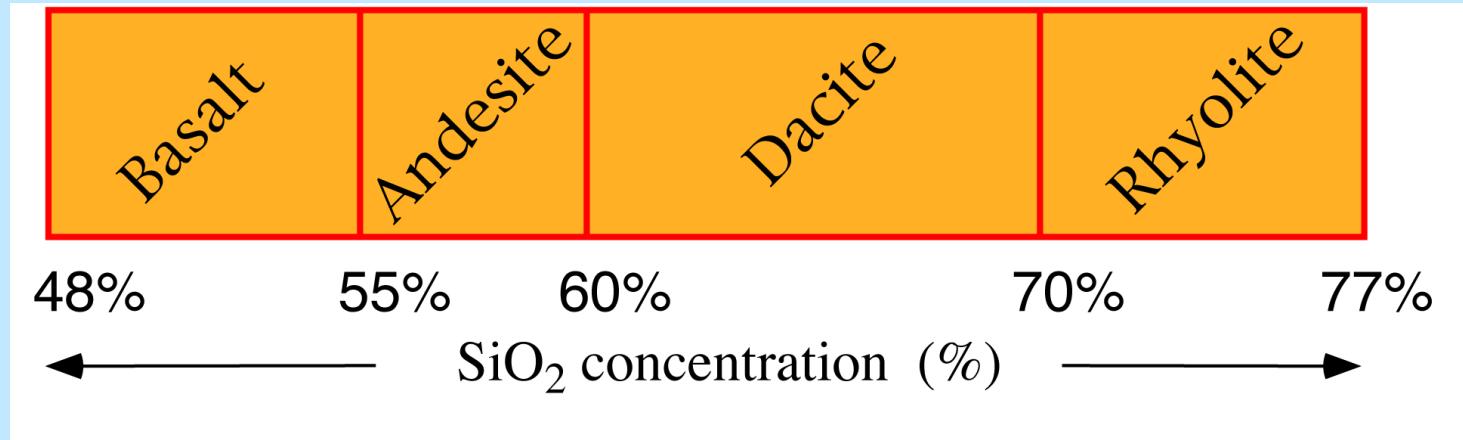
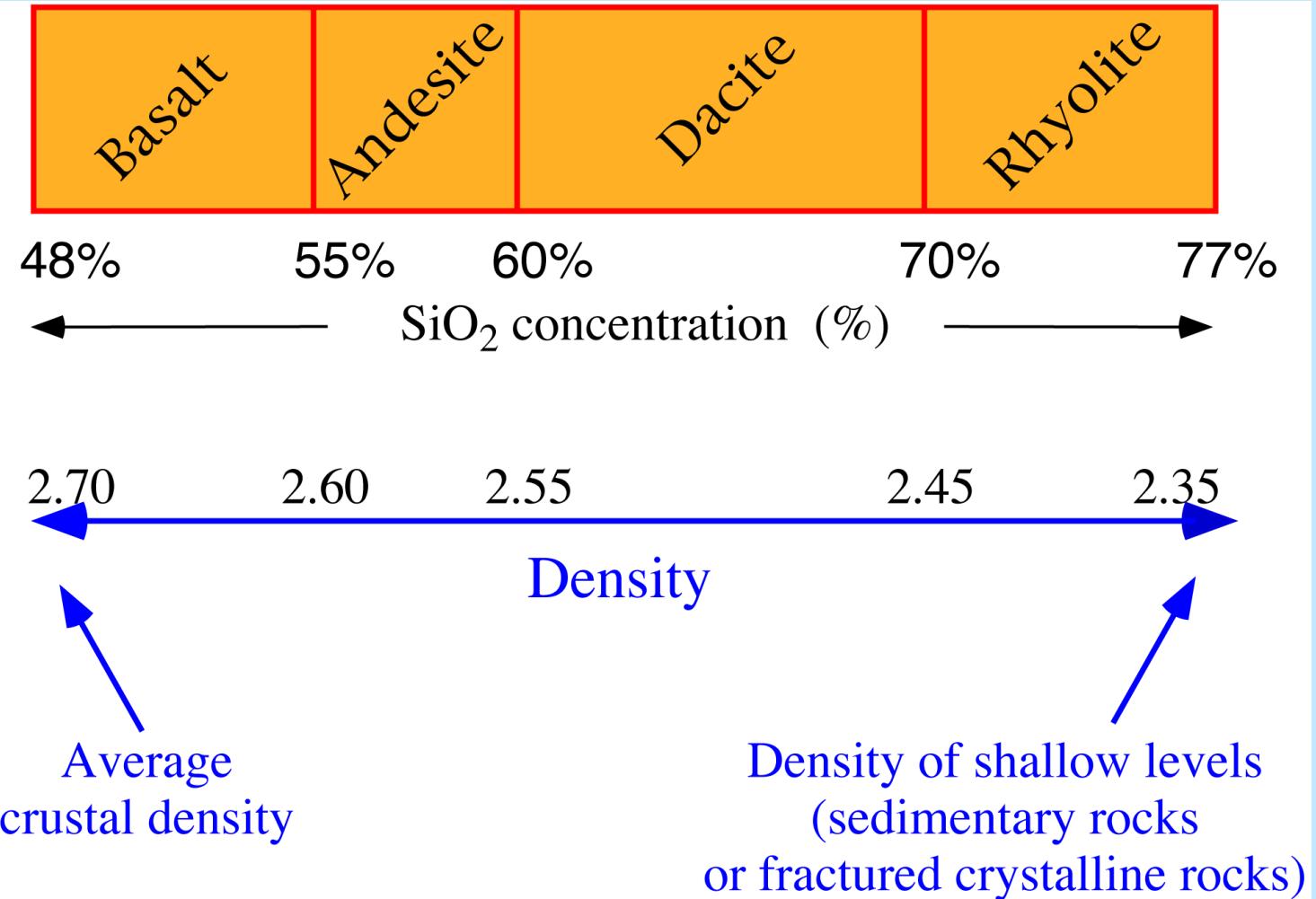


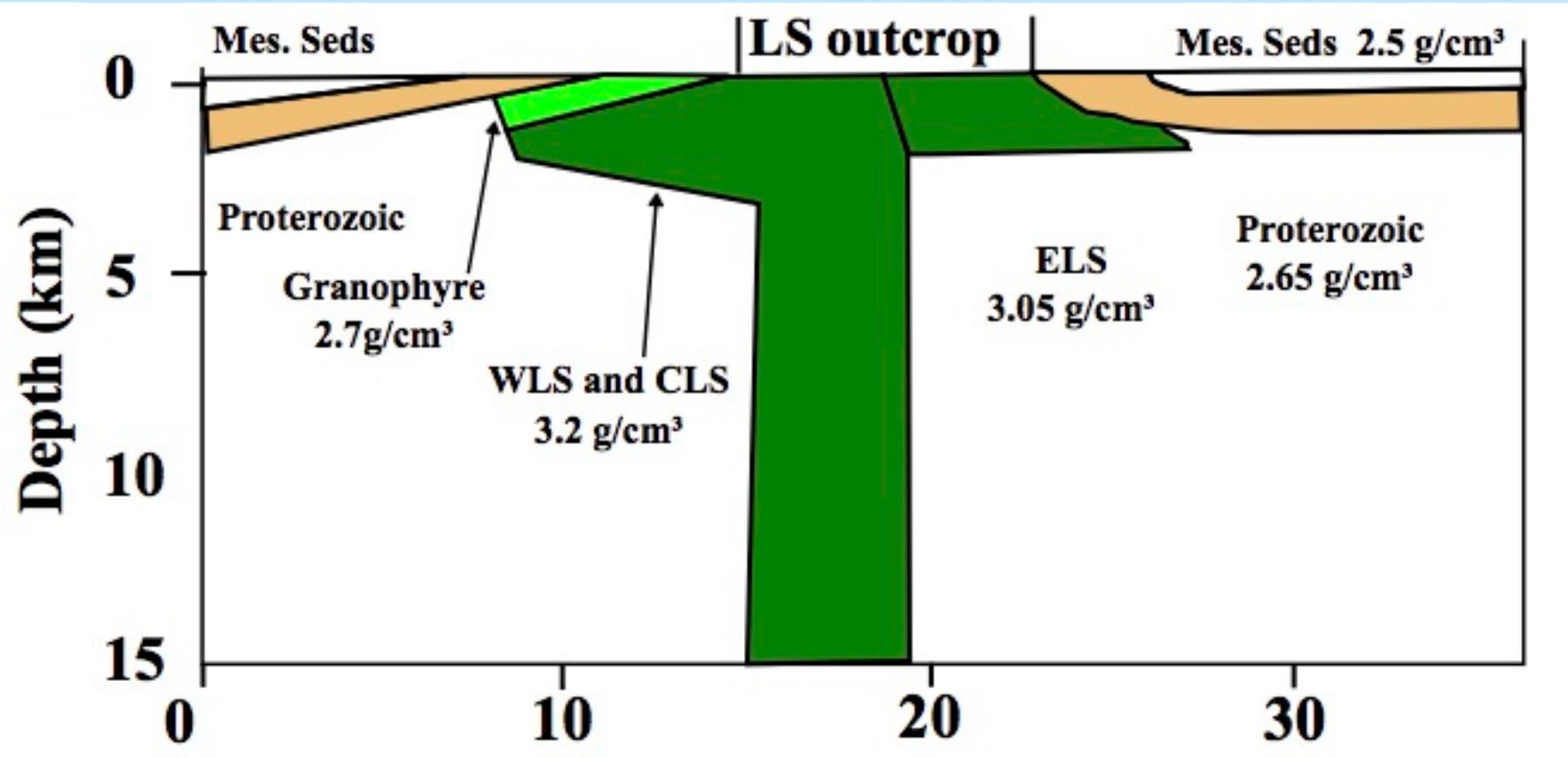
**MAGMA RESERVOIRS:  
EMPLACEMENT  
AND  
POST-EMPLACEMENT DYNAMICS**



Bulk composition of continental crust dictates that:

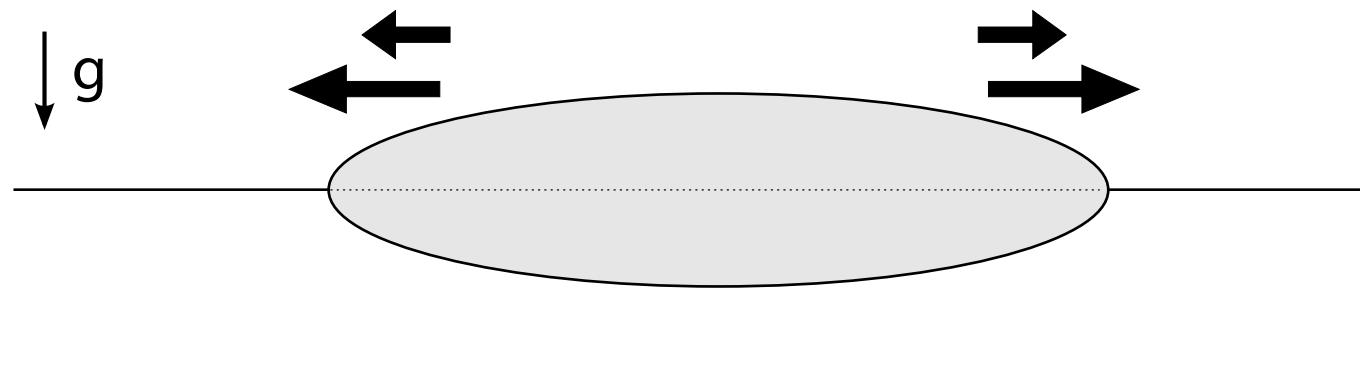
- mafic magmas differentiate (to produce evolved compositions),
- mafic cumulates founder or sink (out of the crust).

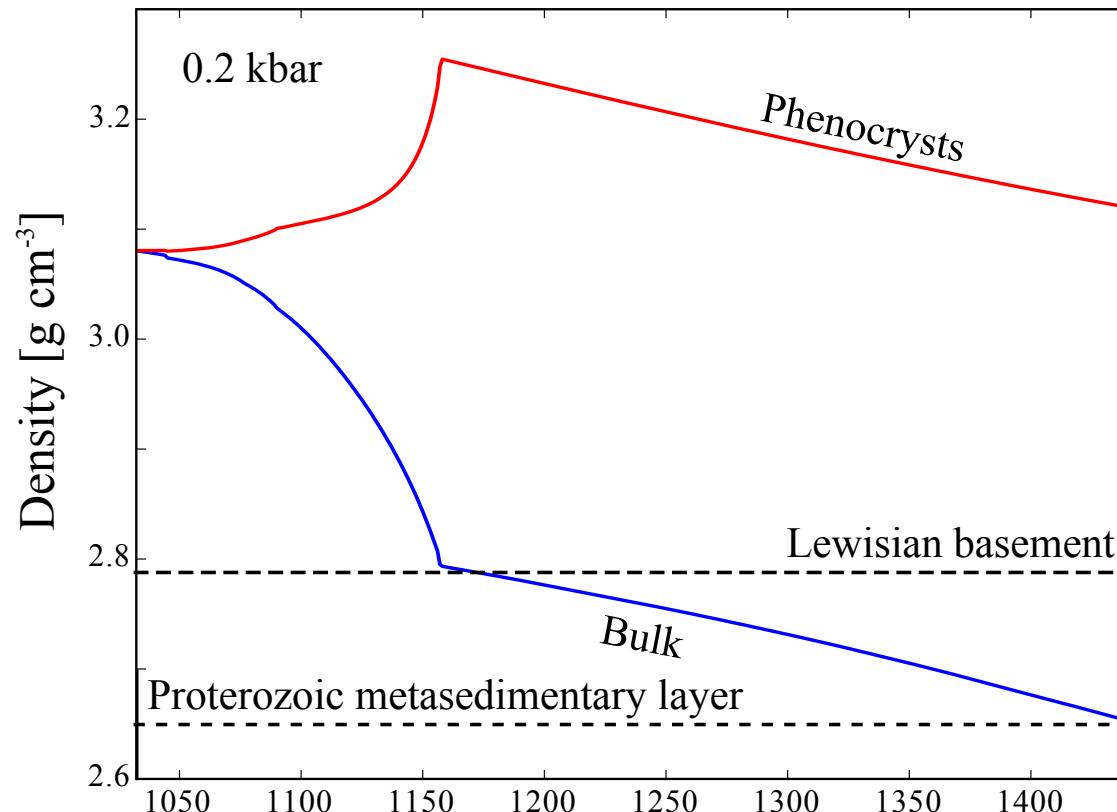




Rum intrusion, Scotland

## Phase 1 : emplacement

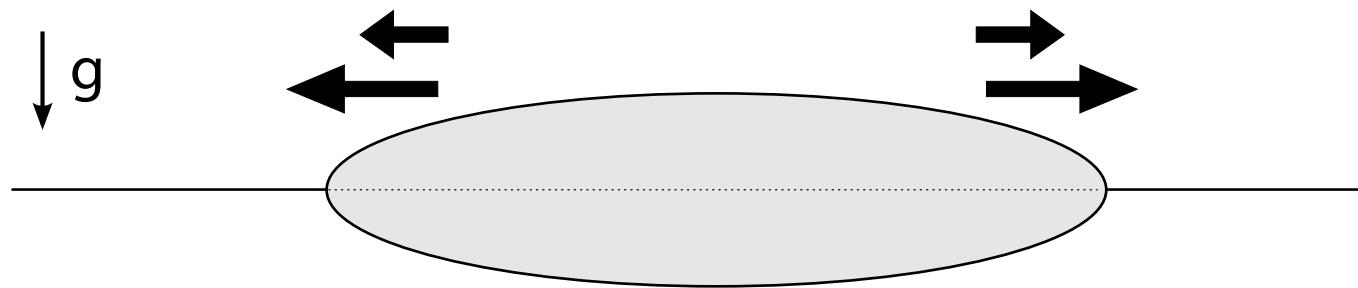


$T_S$  $T_l$ 

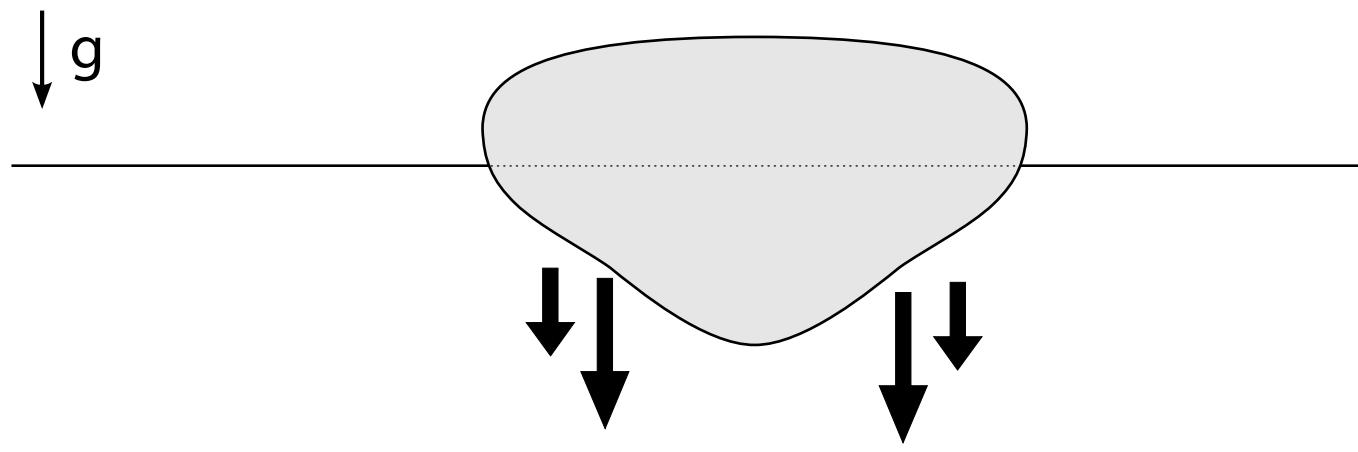
Rum intrusion, Scotland

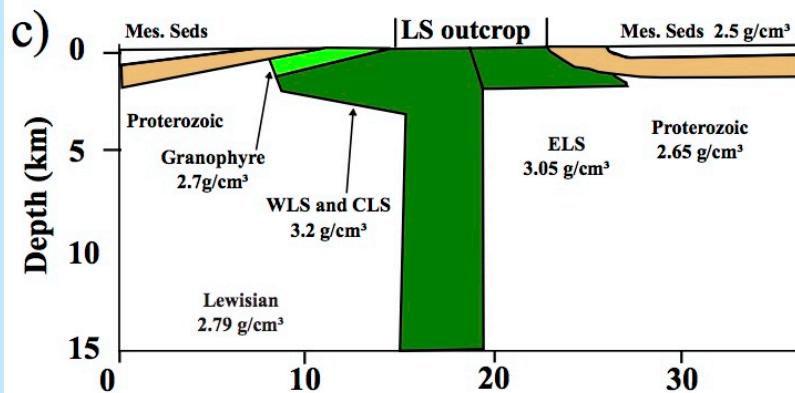
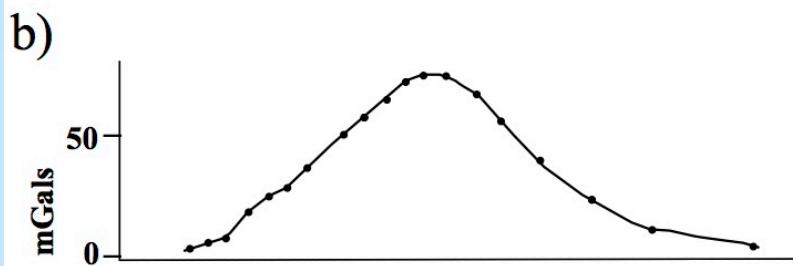
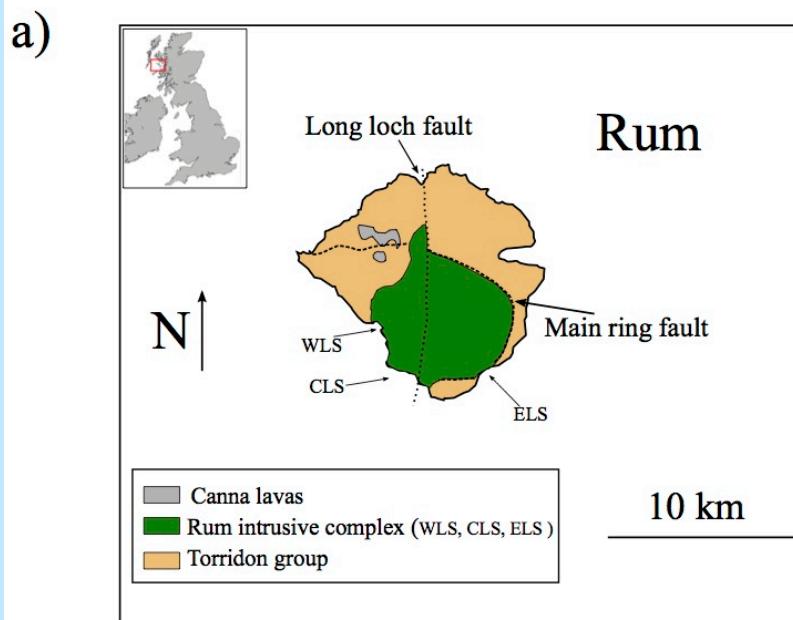
Intrusion	$\rho$ Mafics (kg m <sup>-3</sup> )	$\rho$ Host Rocks (kg m <sup>-3</sup> )	$\rho$ Magma (kg m <sup>-3</sup> )
Ardnamurchan			
Rum	3100-3200	2500-2650	2640
Sept-Iles	3000-3200	2760-2820	2680
Bushveld	3000-3200	2700-2870	2780

## Phase 1 : emplacement



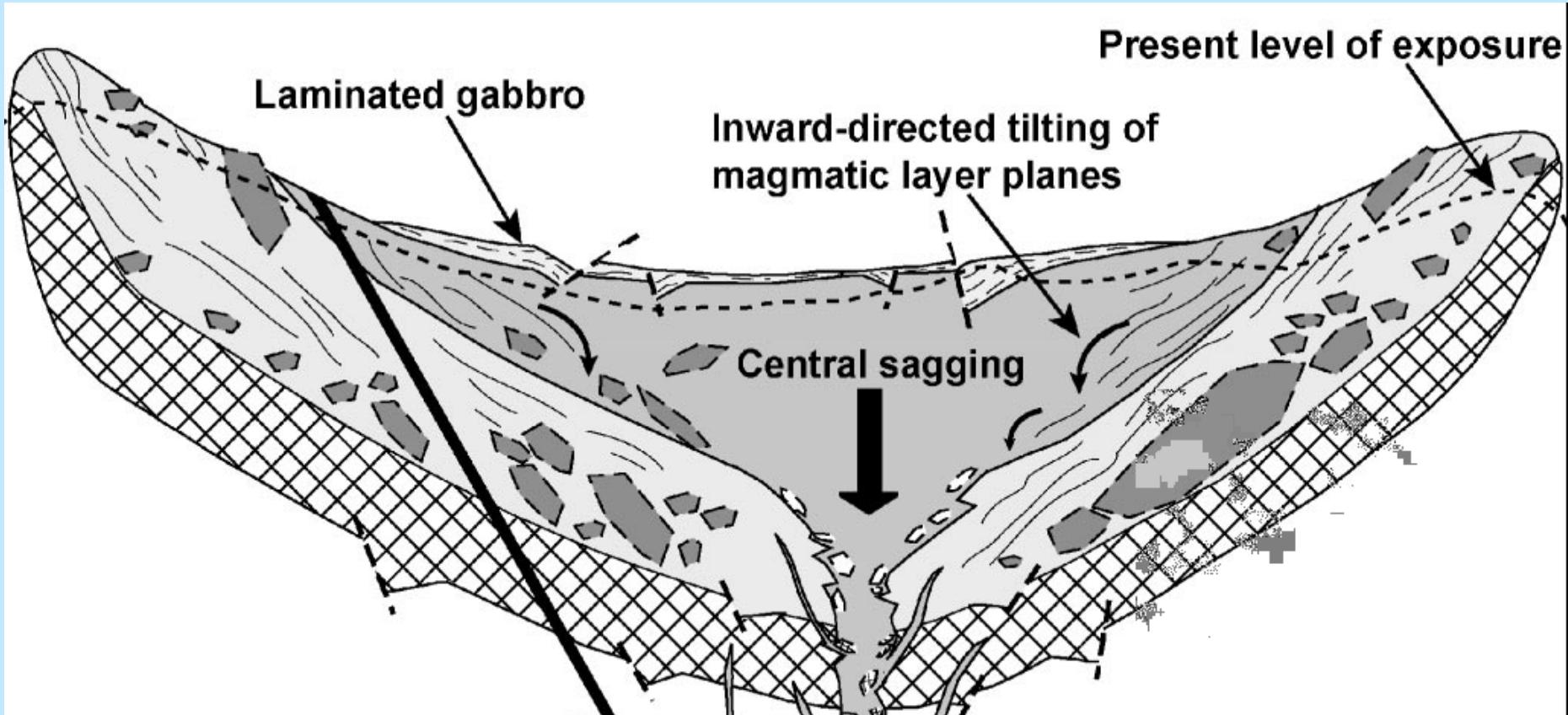
## Phase 2 : sagging and foundering







Ardnamurchan, Scotland



Sagging : evidence for dense material in the intrusion  
(not the initial magma)

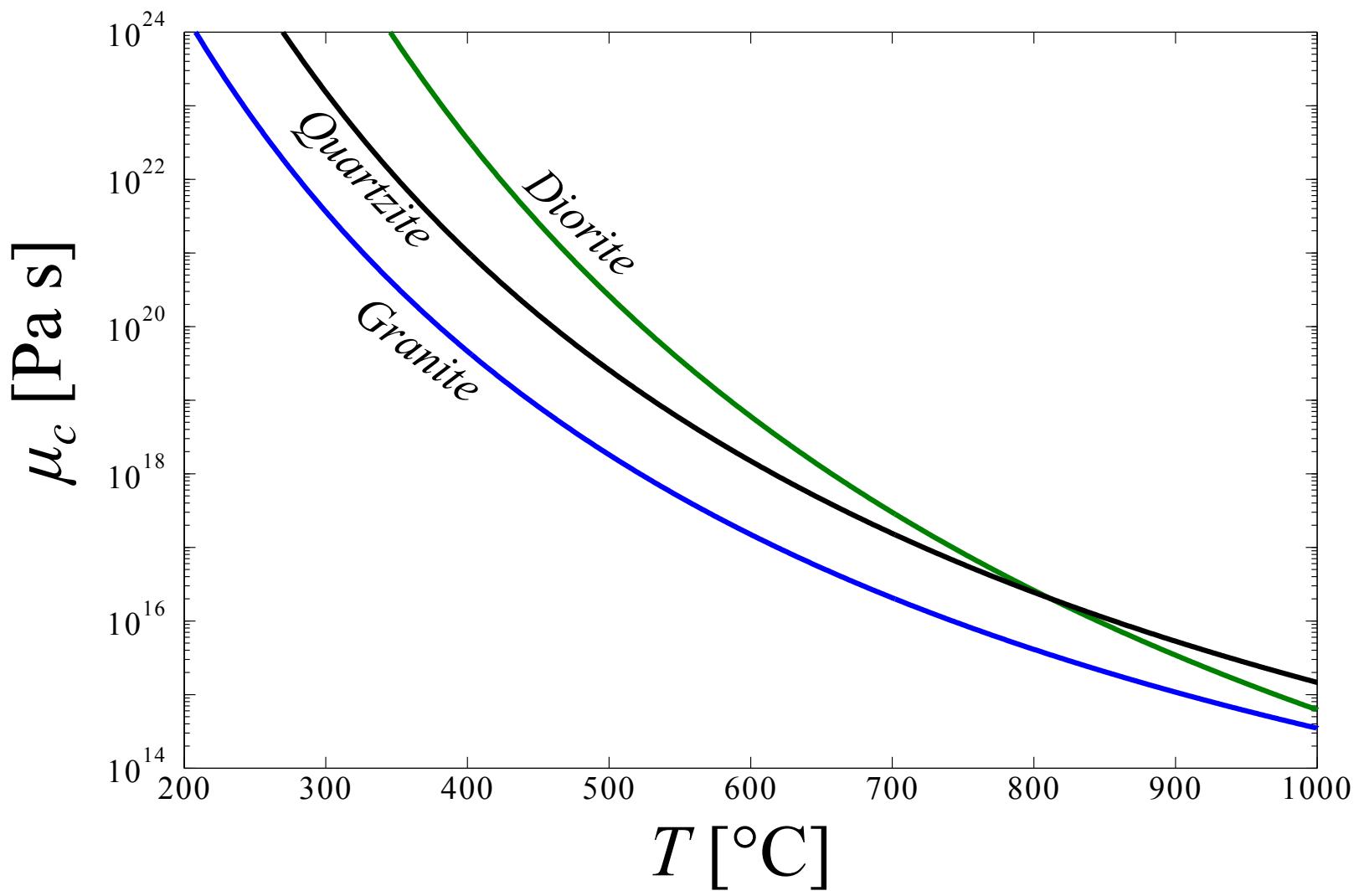
Rheological behaviour of crustal rocks: brittle and power-law creep.  
Stresses in post-crystallization phase: imposed by mafic cumulates.

$$\sigma \approx \Delta\rho gh$$

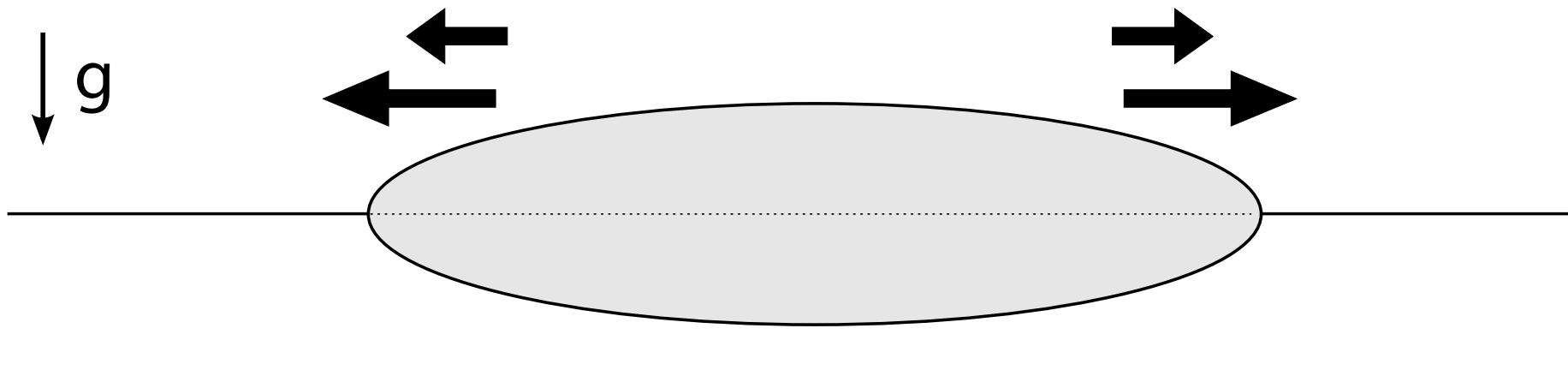
$\Delta\rho$  = density contrast between intrusion and host rocks  $300\text{-}400 \text{ kg m}^{-3}$ .

$h$  = intrusion thickness 3-8 km.

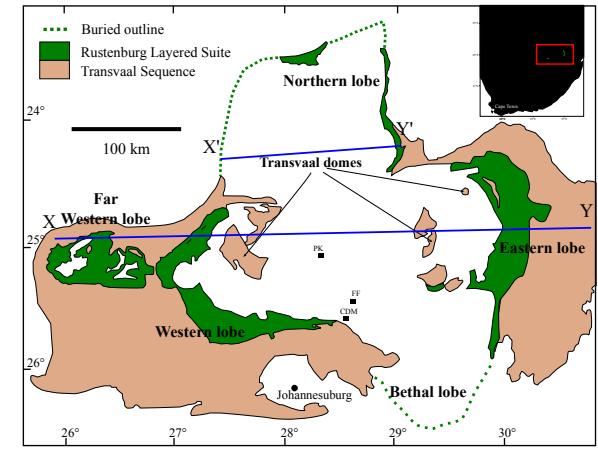
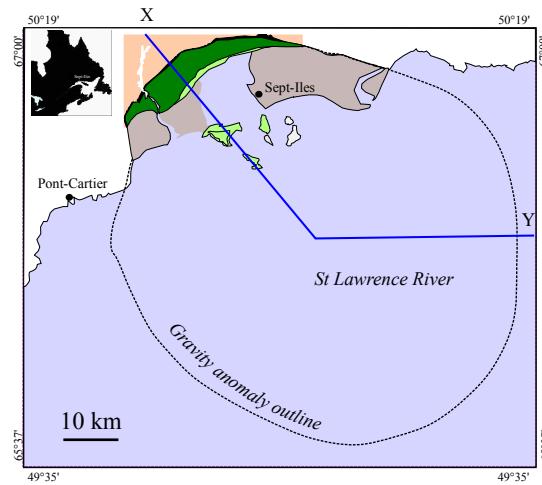
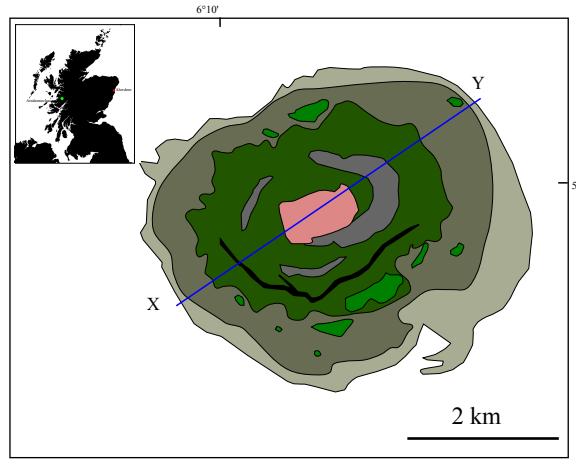
Effective viscosity  $10^{15} - 10^{20} \text{ Pa s}$  (strain rates  $> 10^{-13} \text{ s}^{-1}$ ).

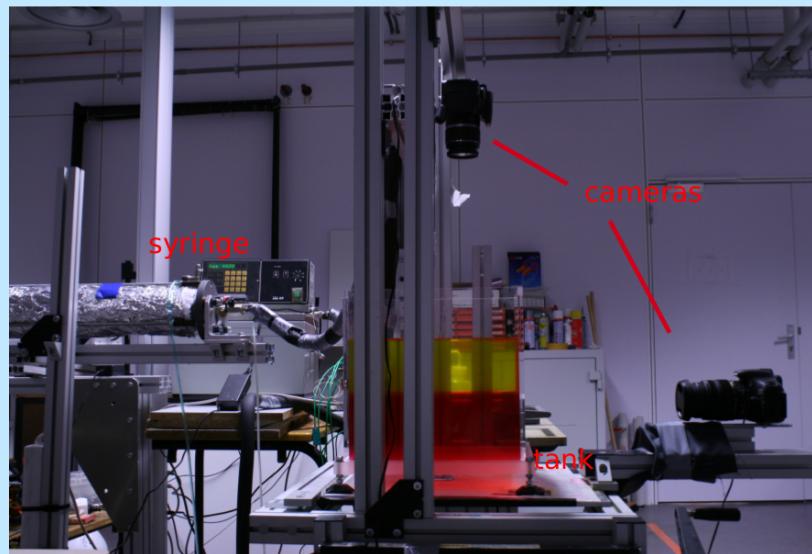
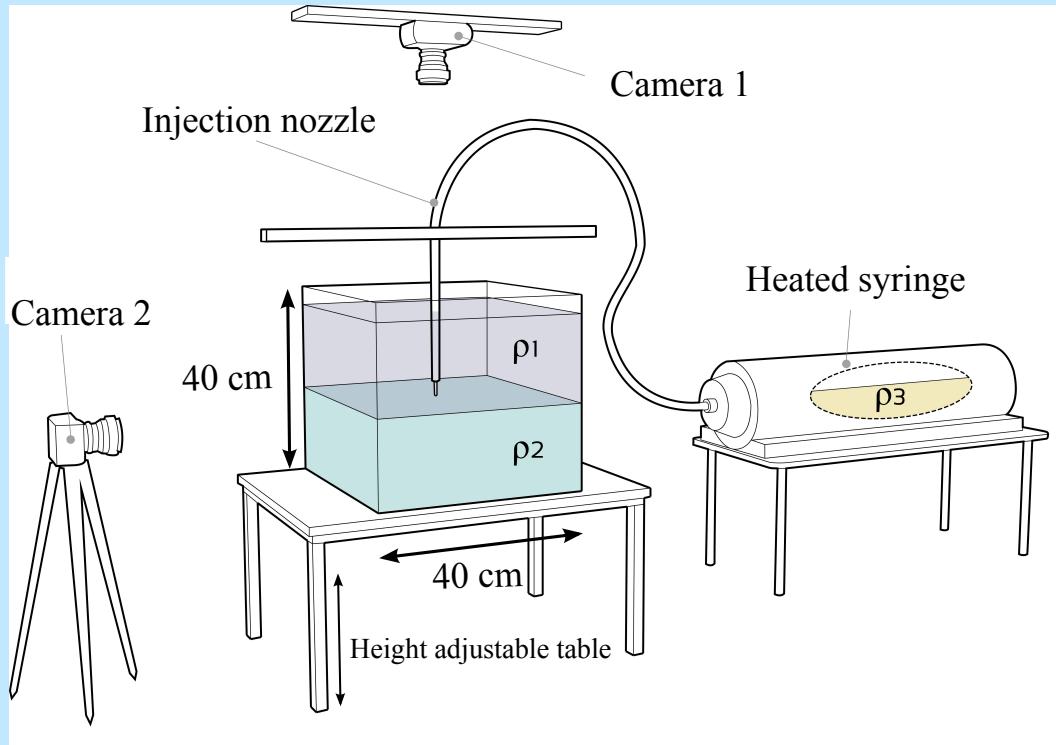


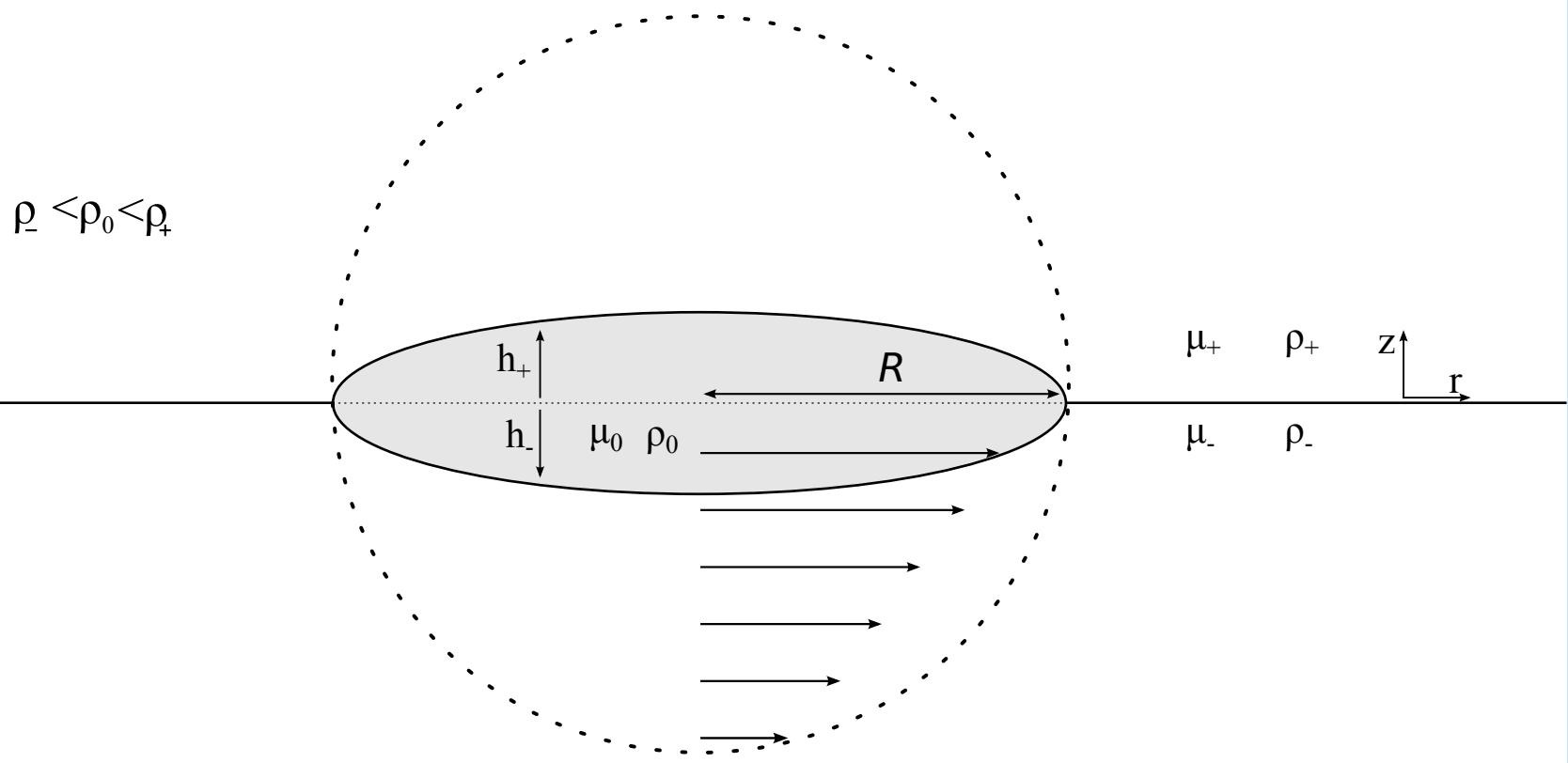
# Phase 1 : emplacement



Intrusion	Volume (km <sup>3</sup> )	Aspect ratio
Ardnamurchan	30	1
Rum	$5.4 \cdot 10^2$	0.5
Sept-Iles	$2.8 \cdot 10^4$	0.2
Bushveld	$10^6$	0.04







Driving = buoyancy.

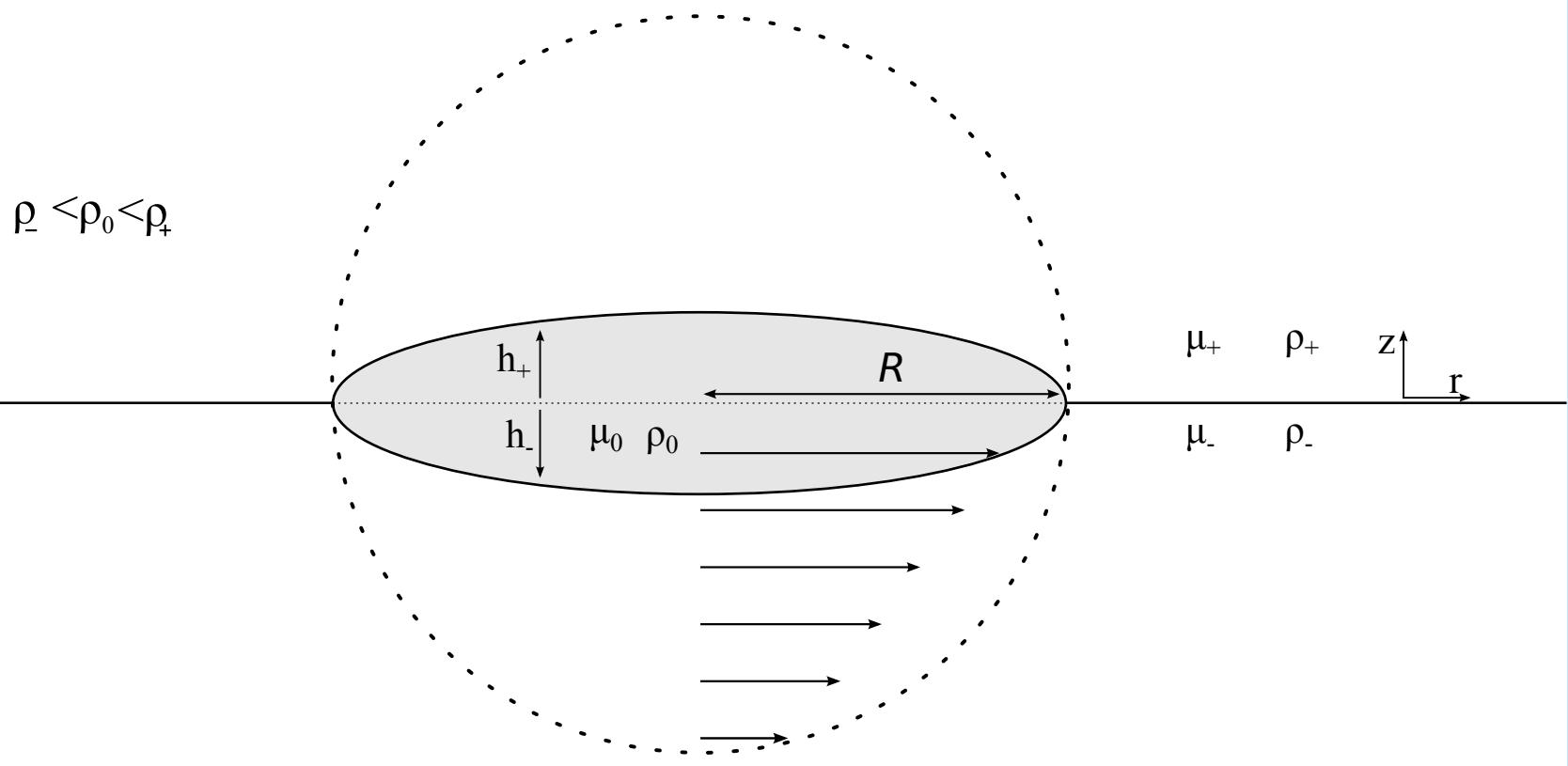
Resisting = viscous shear at top and bottom of intrusion.

Flow of radius  $R^*$ , thickness  $H^*$ .

For flow over radial distance  $R^*$ , kinematic boundary layer extends to distance  $\sim R^*$ .

Characteristic velocity (spreading rate)  $U_S$ .

Strain rate  $\sim U_S/R^*$ .



Bulk horizontal momentum balance:

$$(\rho_T g' H^*) H^* R^* \sim \left[ (\mu_- + \mu_+) \frac{U_s}{R^*} \right] R^{*2}$$

Add volume conservation.

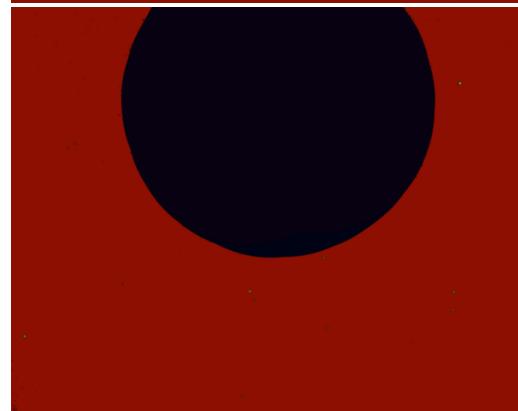
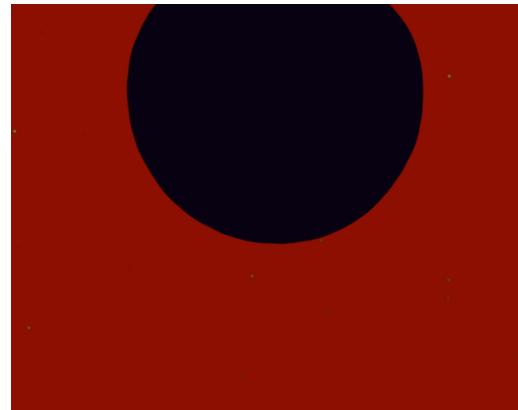
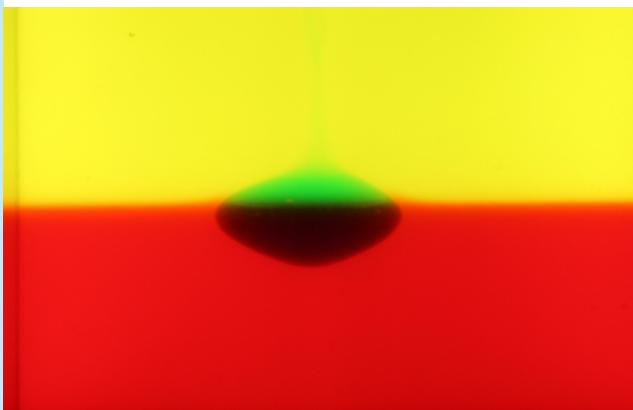
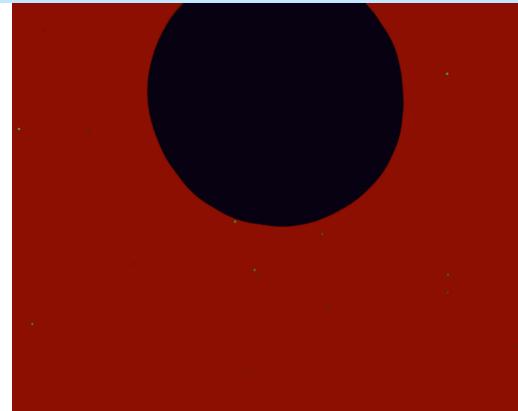
$$U_s \sim \frac{\rho_T g' H^{*2}}{\mu_- + \mu_+}$$

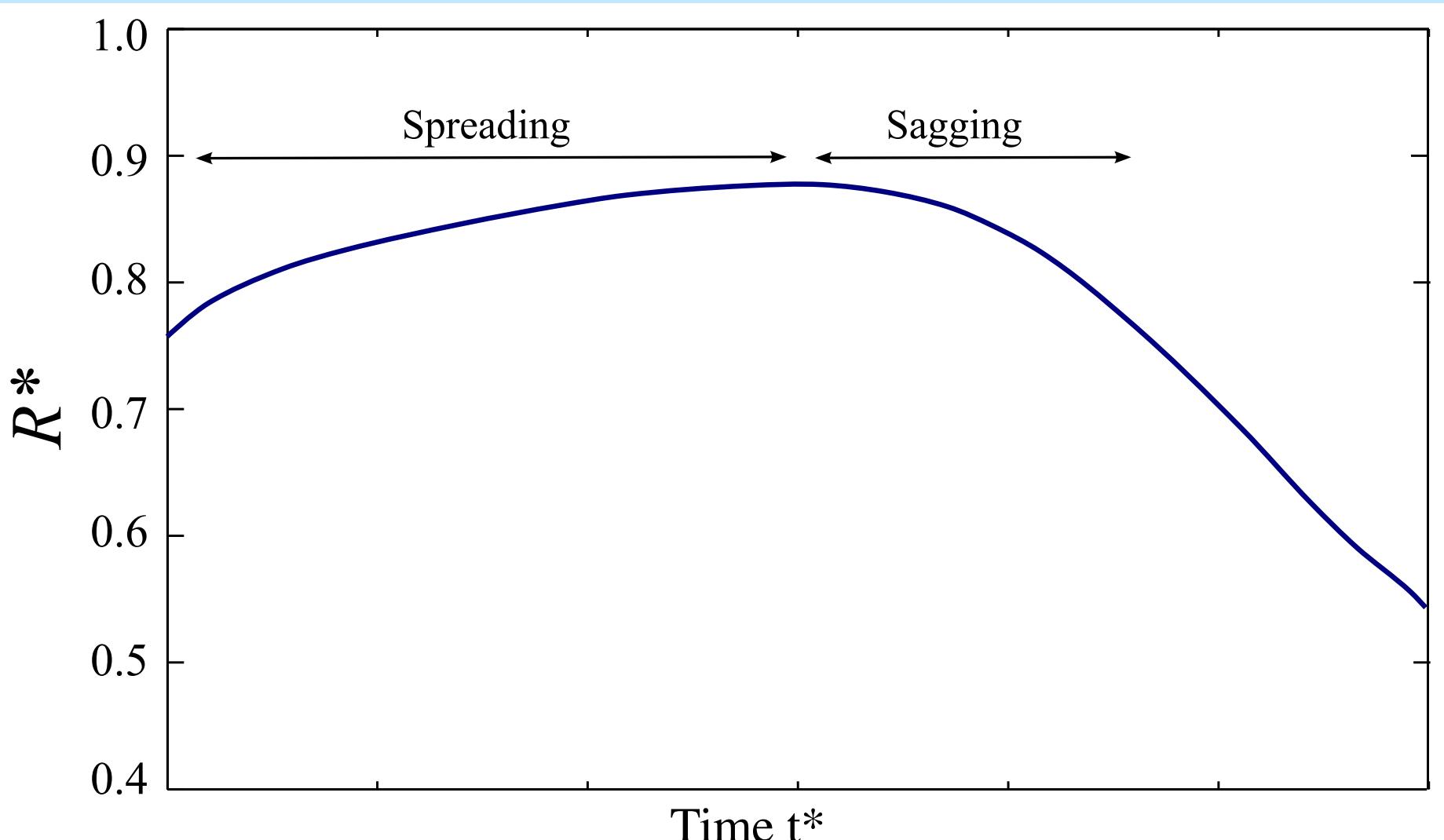
$$\begin{aligned} R(t) &\sim \left( \frac{\rho_T g' V^2}{\mu_+ + \mu_-} \right)^{1/5} t^{1/5} \\ h(t) &\sim \left( \frac{(\mu_- + \mu_+) V^{1/2}}{\rho_T g'} \right)^{2/5} t^{-2/5} \end{aligned}$$

Side view

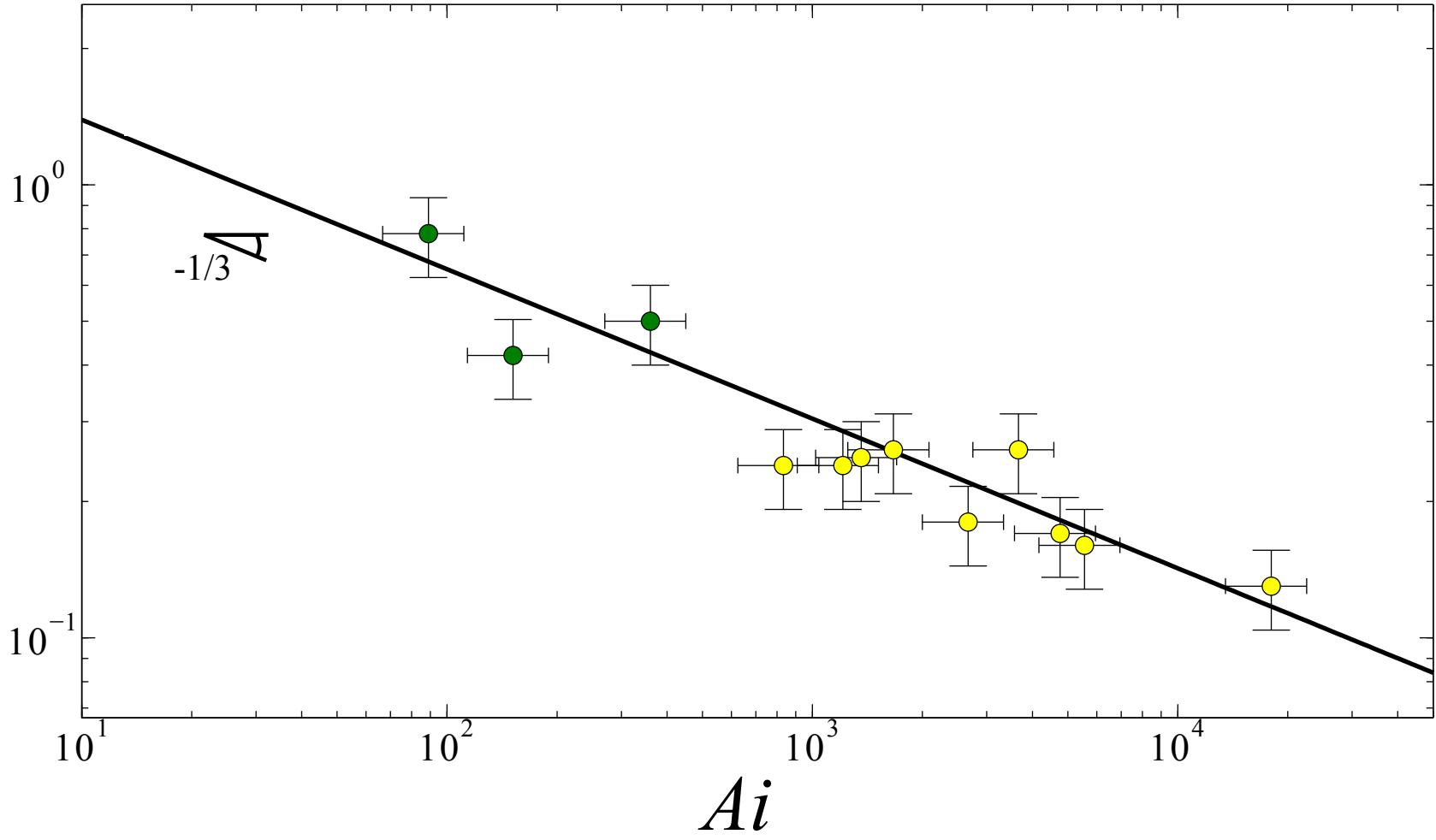


View from above





Aspect ratio H/R



End of the spreading phase such that cooling proceeds faster than spreading.

$$\text{Cooling rate} \sim \kappa/H.$$

$$\text{Spreading rate} \sim \frac{dR}{dt} \sim \left( \frac{\rho_T g' V^2}{\mu_+ + \mu_-} \right)^{1/5} t^{-4/5}$$

Thus, critical time for buoyancy reversal:

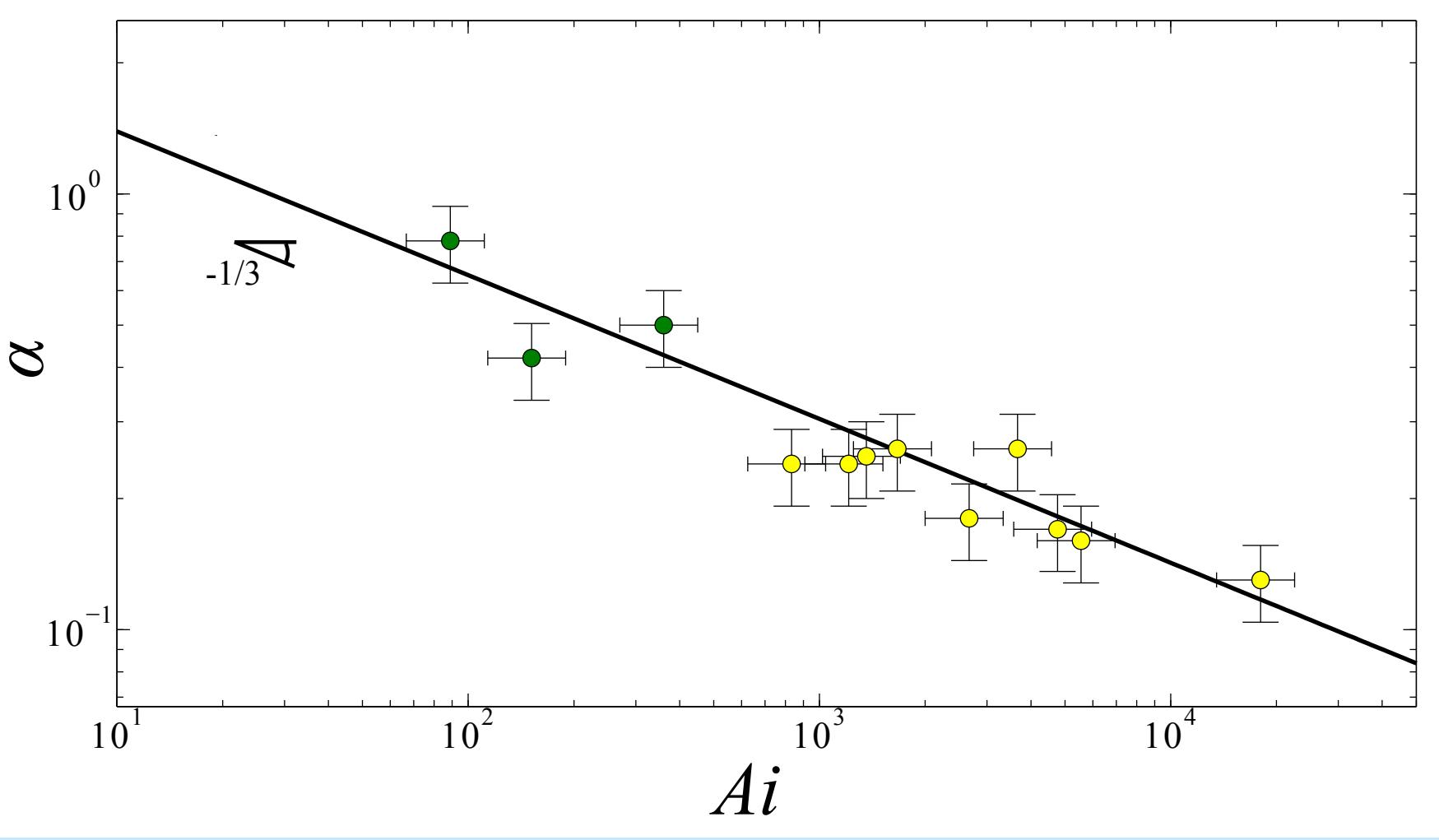
$$t_c \sim \left( \frac{(\mu_- + \mu_+) V^{1/2}}{\rho_T g' \kappa^{5/4}} \right)^{4/9}$$

At  $t = t_c$ ,  $H = H_c$  and  $R = R_c$ , corresponding to critical aspect ratio  $\alpha_c = H_c/R_c$ :

$$\alpha_c \sim \frac{H_c}{R_c} \sim \left( \frac{(\mu_- + \mu_+) \kappa}{\rho_T g' V} \right)^{1/3} = Ai^{-1/3}$$

Dimensionless number  $Ai$ :

$$Ai = \frac{\rho_T g' V}{(\mu_- + \mu_+) \kappa}.$$



$$\alpha_c = (2.8 \pm 0.10)Ai^{-1/3}.$$

$\alpha_c$  decreases with increasing volume  $V_*$ .

Dimensionless number  $Ai$  = ratio between two velocity scales.  
Spreading rate versus and cooling rate (diffusion controlled).  
Cooling rate.

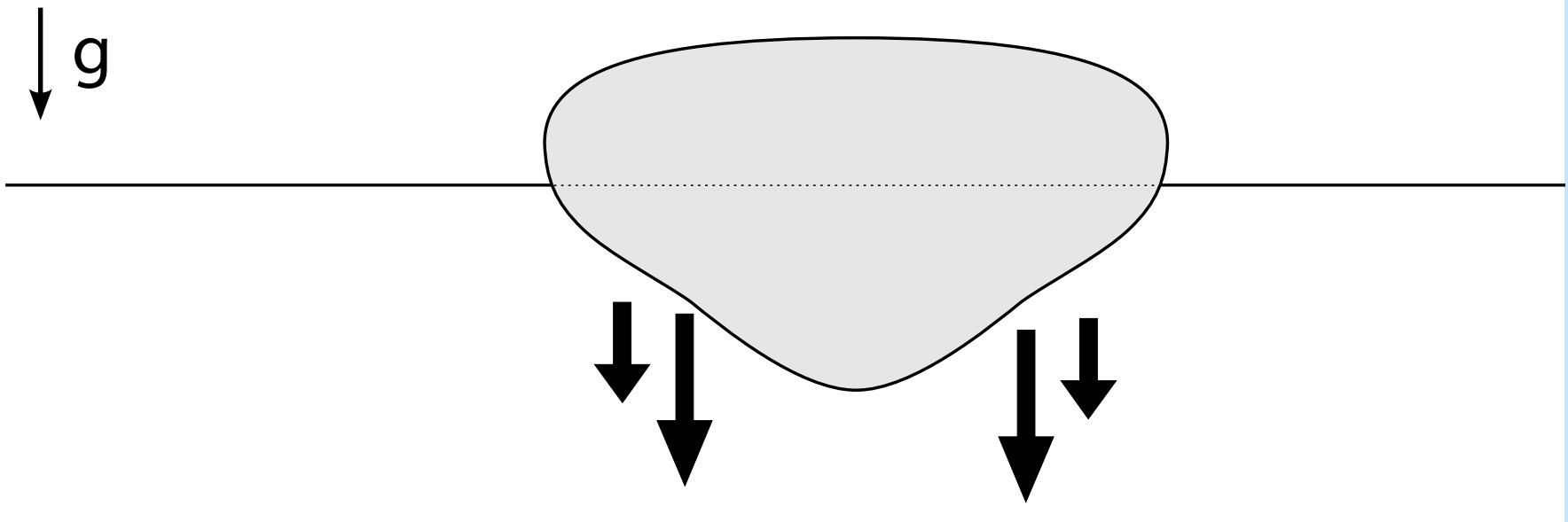
$$U_d = \frac{\kappa}{H^*}$$

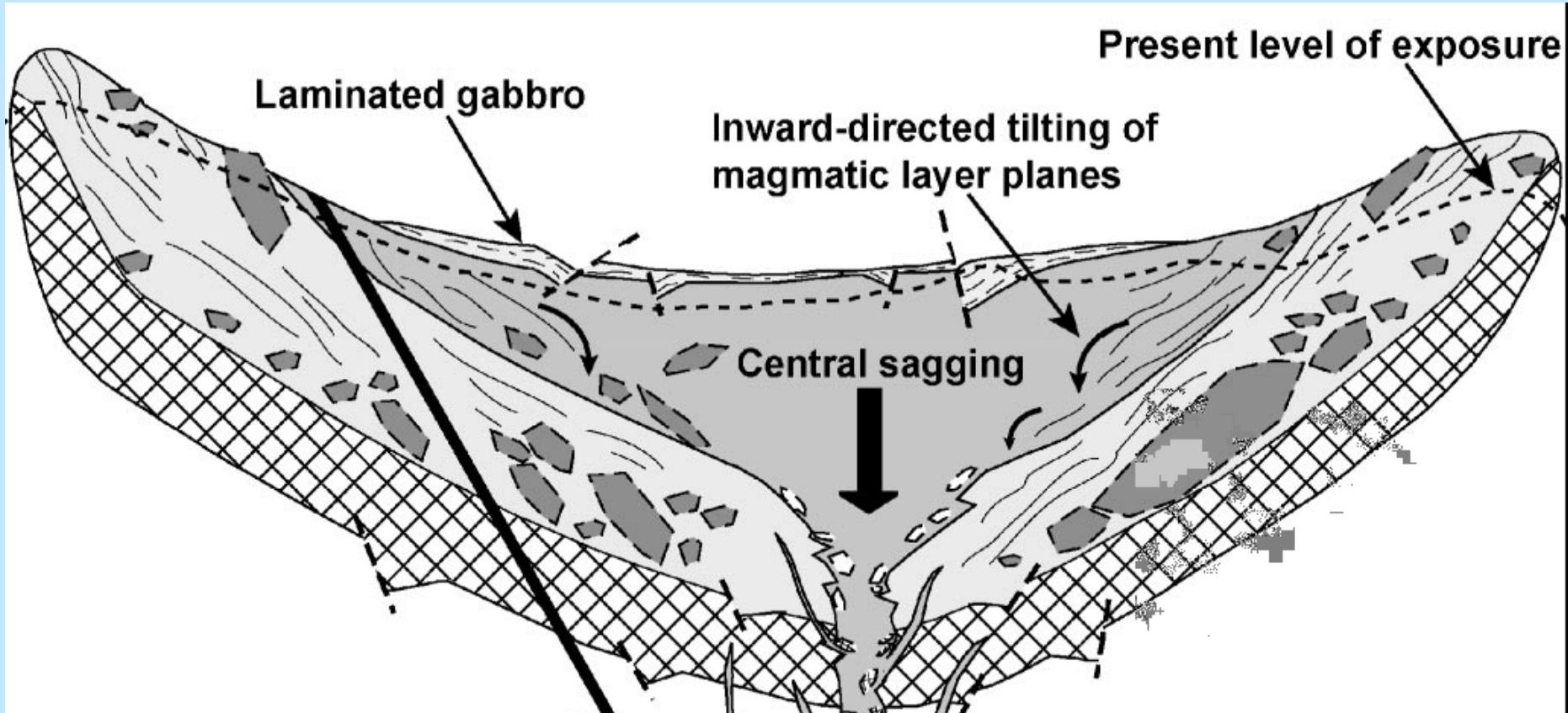
Set  $H^* \sim V^{1/3}$  and  $R^* \sim V^{1/3}$ :

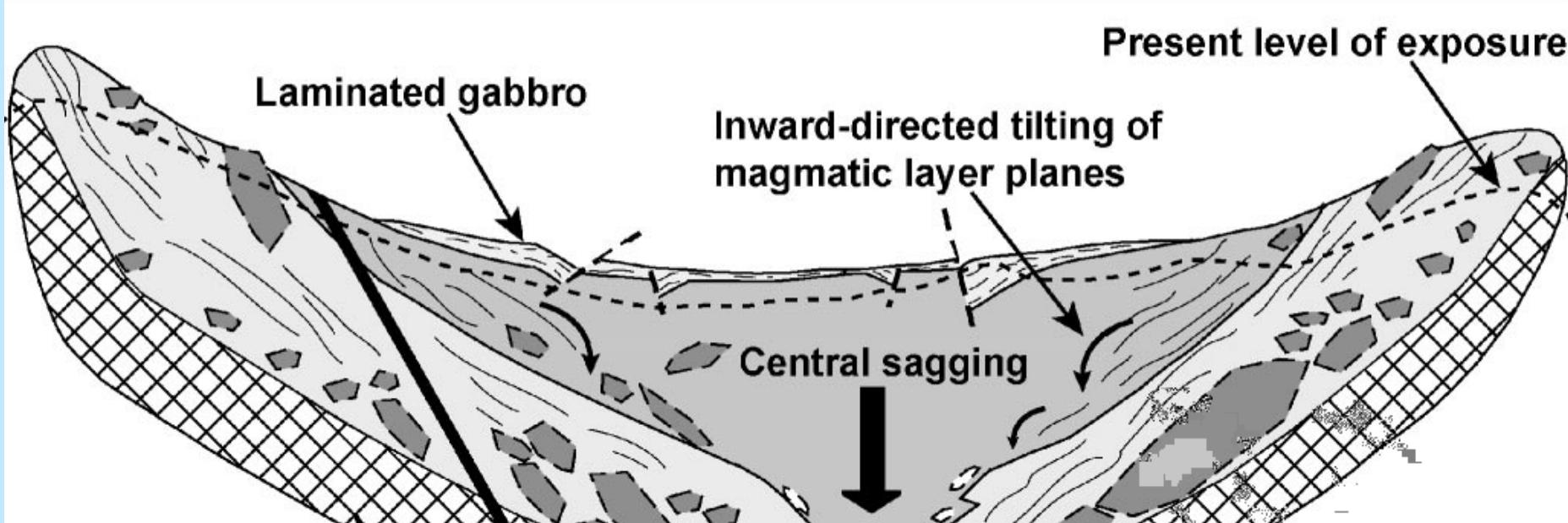
$$\frac{U_s}{U_d} = \frac{\rho_T g' V}{(\mu_- + \mu_+) \kappa} = Ai$$

Large  $Ai$  : spreading faster than cooling = intrusion extends to large distances.  
Small  $Ai$  : cooling faster than spreading = intrusion does not spread.

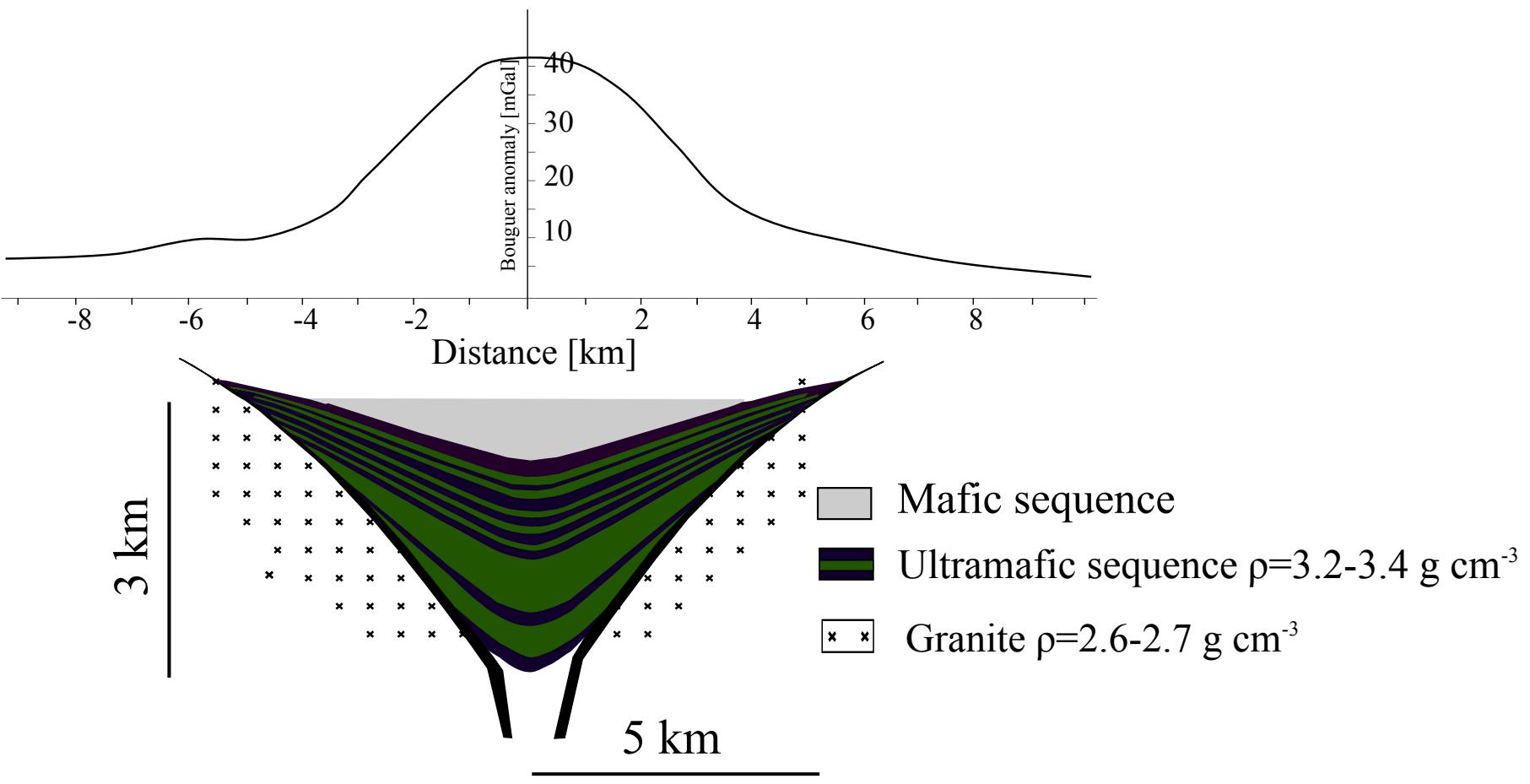
## Phase 2 : sagging and foundering



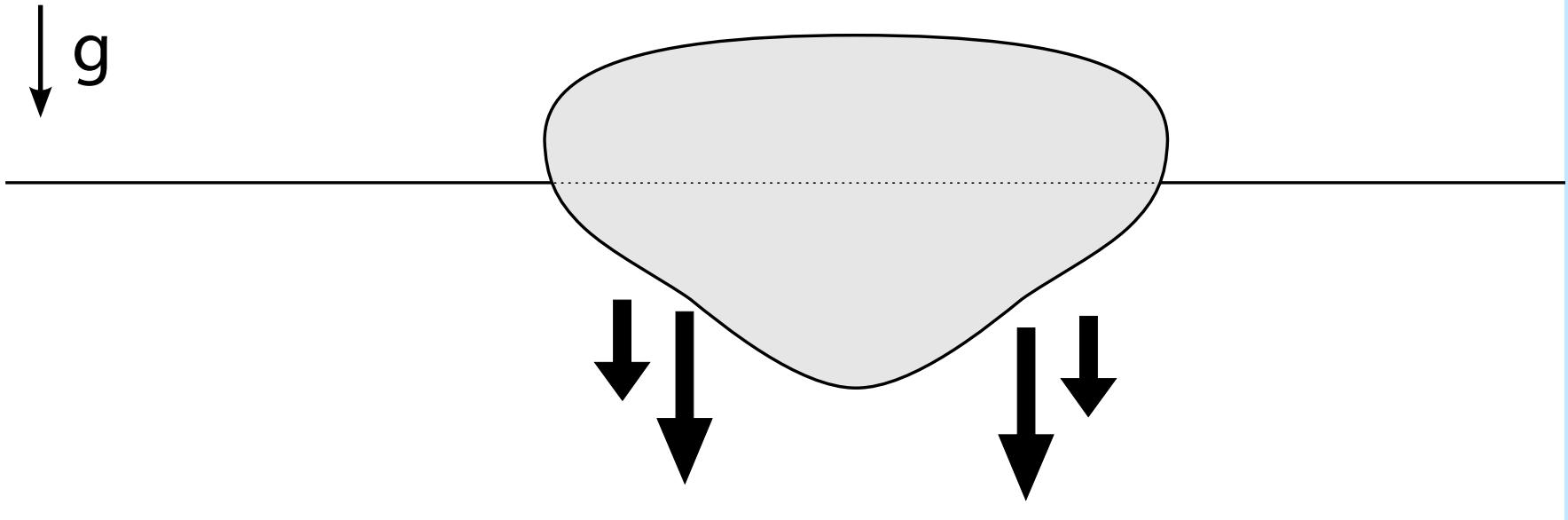




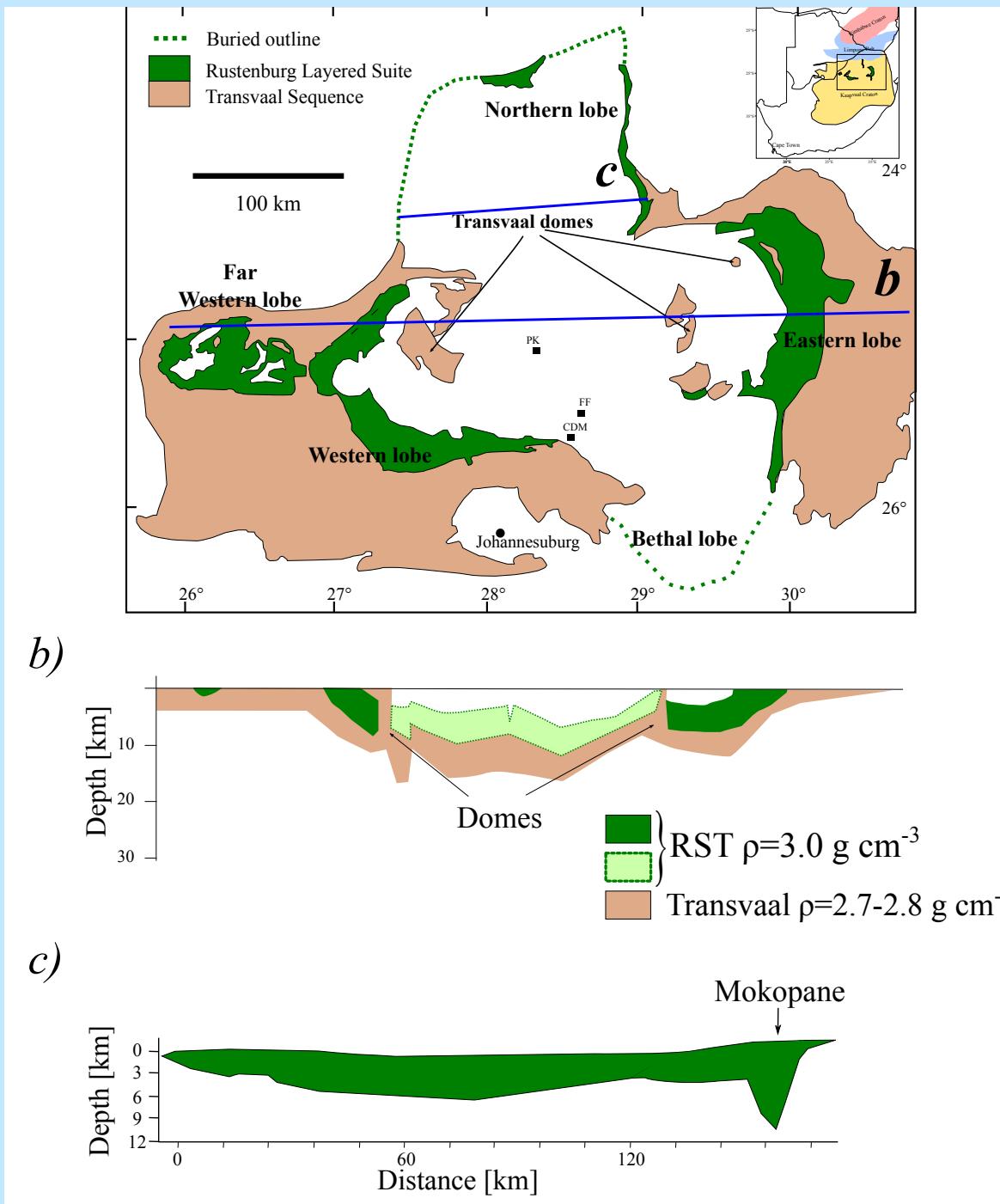
Sagging ?  
inward dips increase towards axial zone:  
not consistent with sagging (flexural behaviour)  
suggests incipient foundering



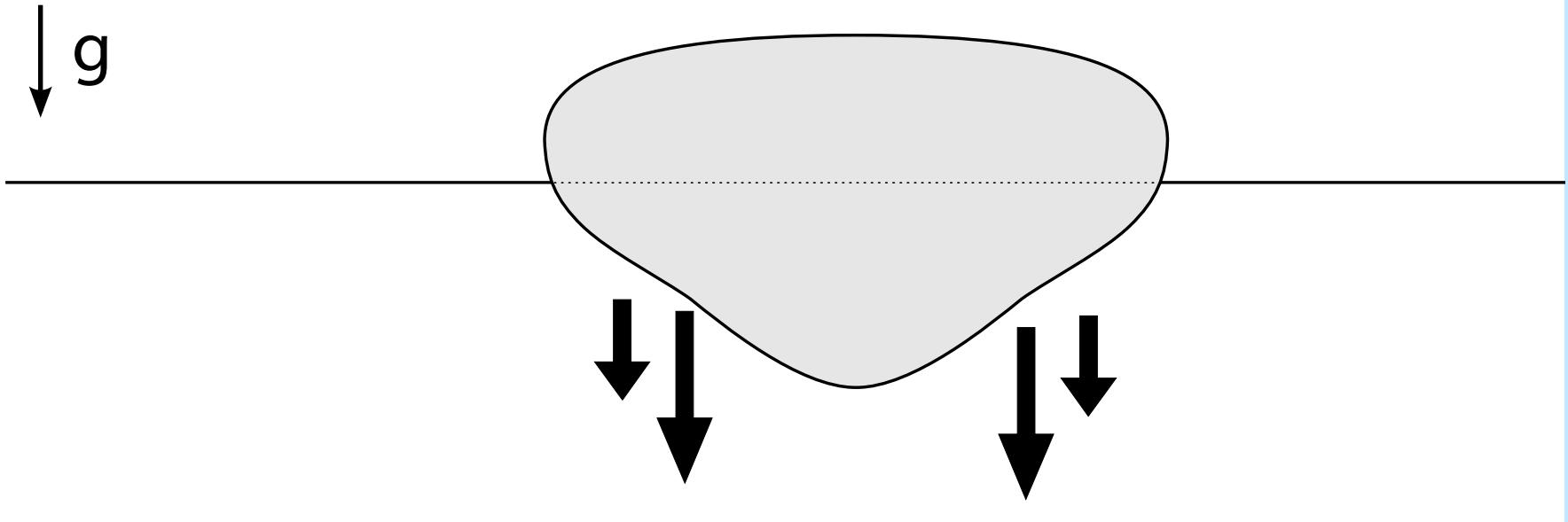
## Phase 2 : sagging and foundering



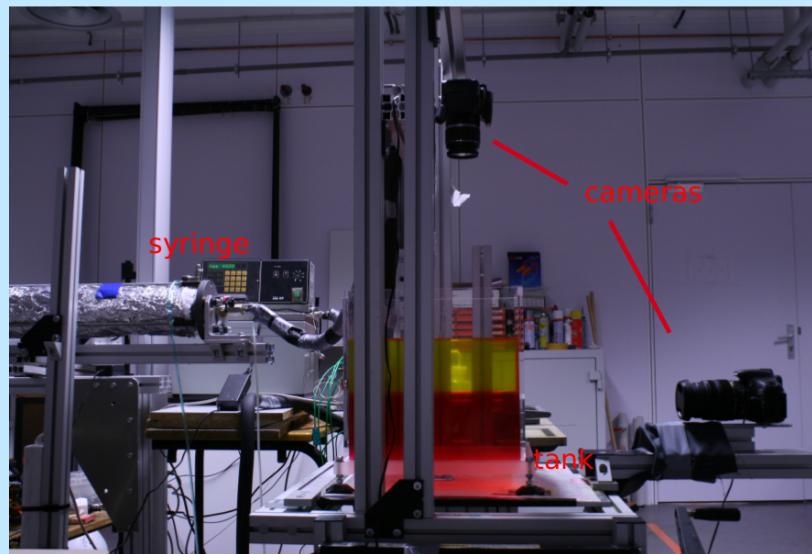
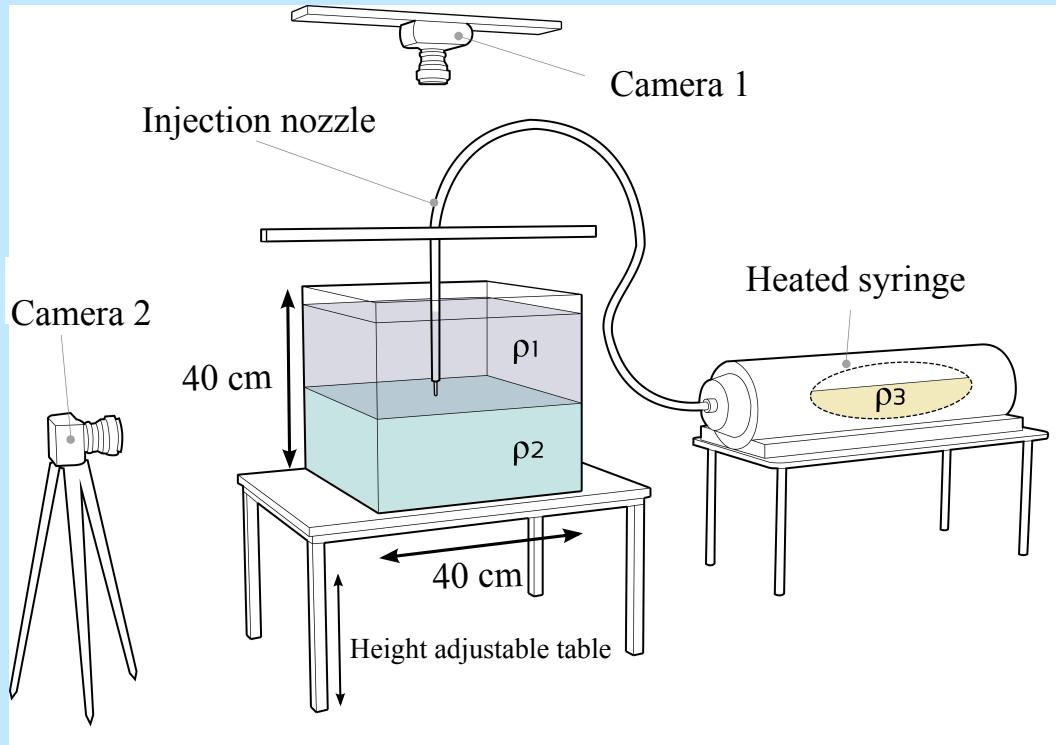
Sequence of increasing deformation with increasing volume.  
Sagging – funnel structure – sinking (?)



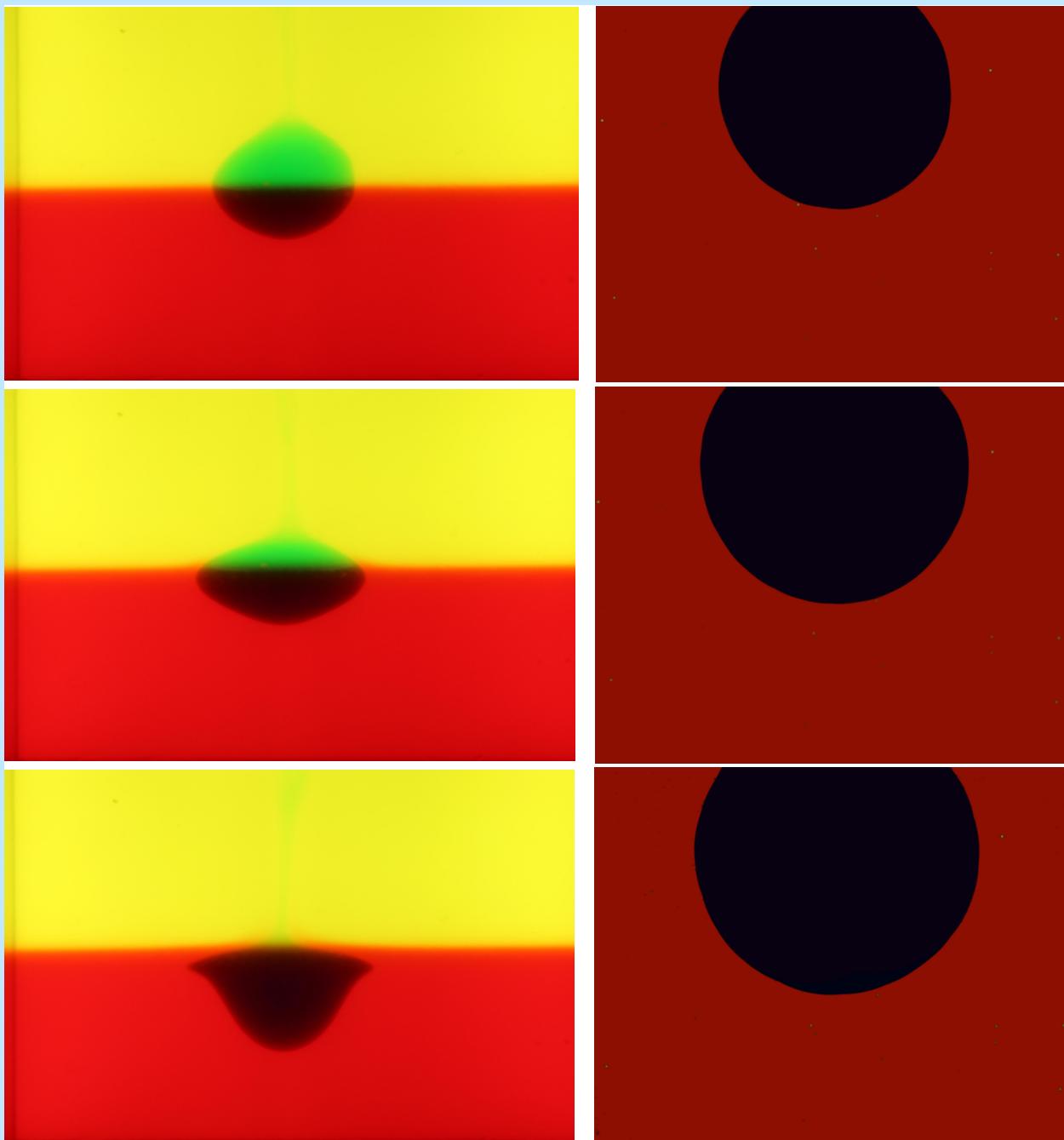
## Phase 2 : sagging and foundering



Sequence of increasing deformation with increasing volume.  
Complex shapes for small aspect-ratio intrusions.

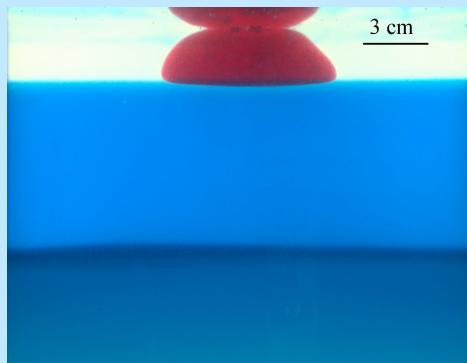


## Teardrop regime



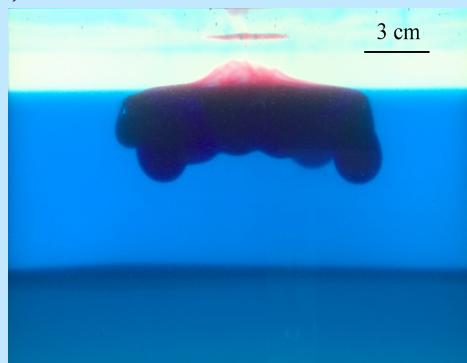
“Jellyfish”  
regime

a)



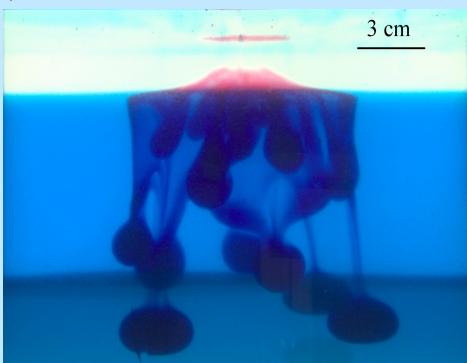
$t=10\text{ s}$

b)

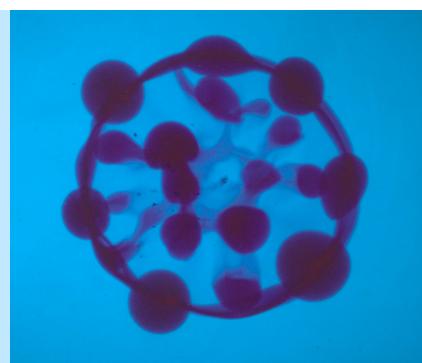
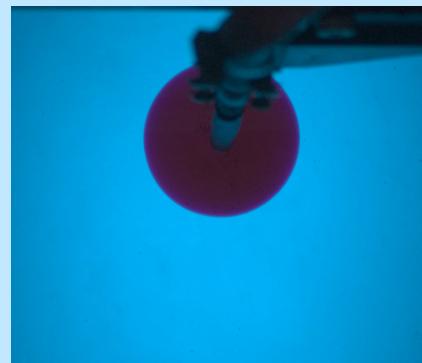


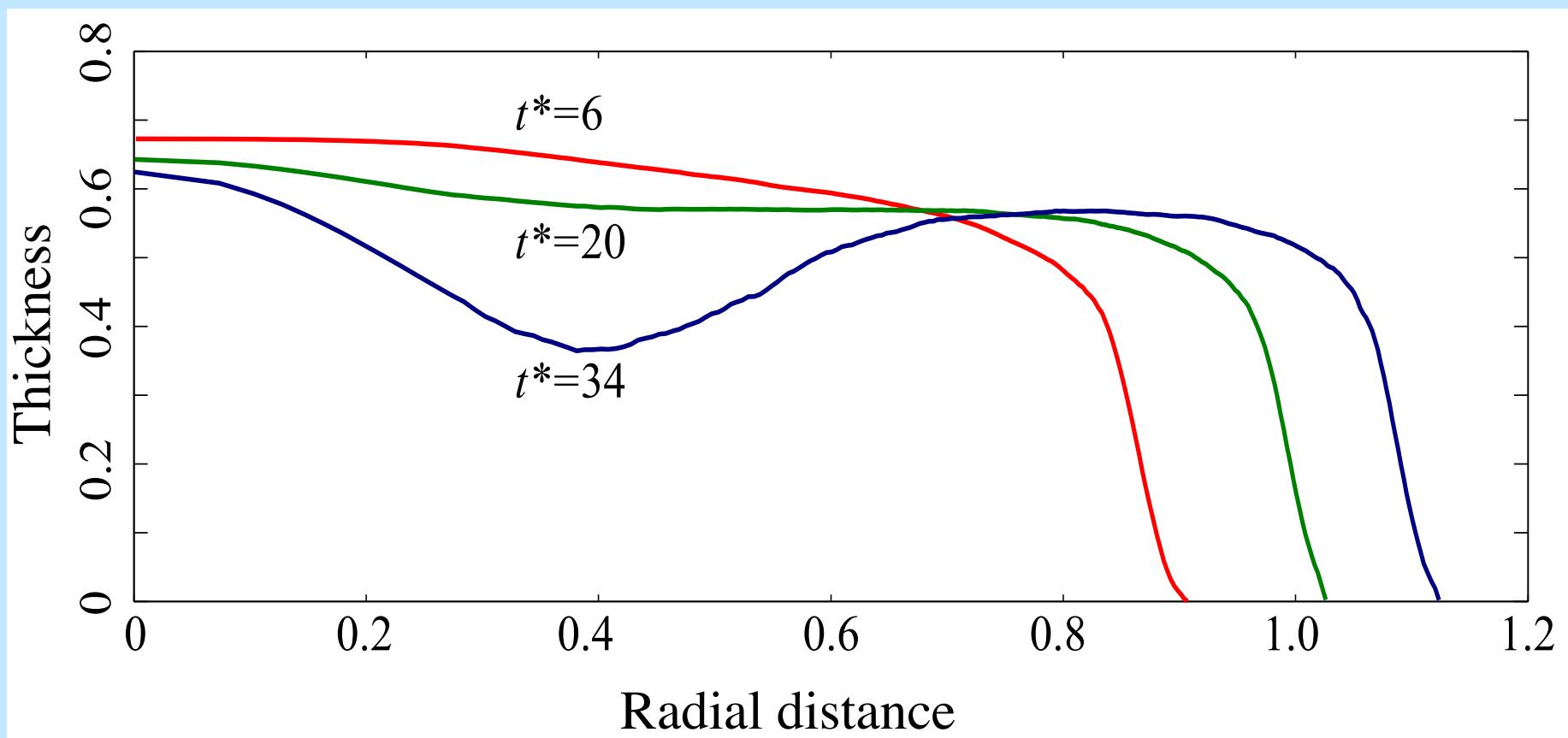
$t=480\text{ s}$

c)



$t=710\text{ s}$





$V = 28 \text{ cm}^3$

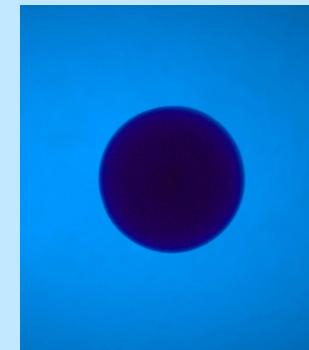
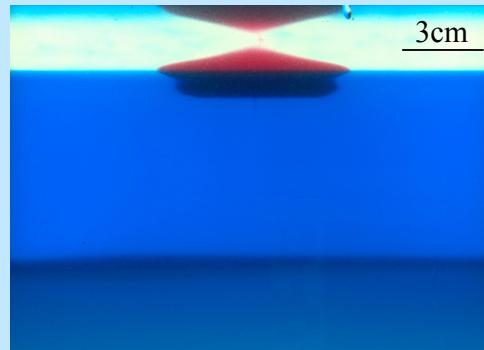
*3cm*

$V = 157 \text{ cm}^3$

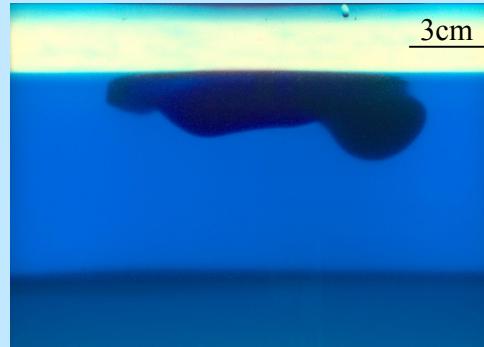
*3cm*

## Annular regime

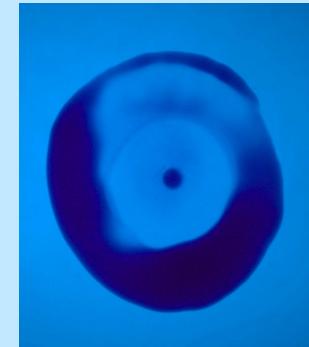
a)



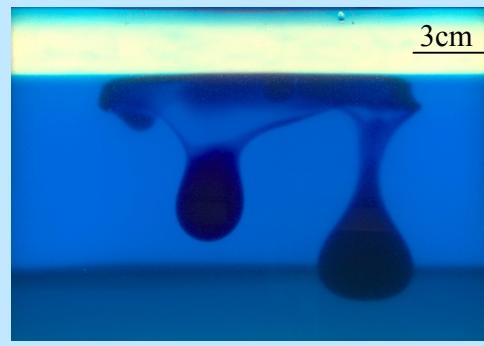
b)



$t=60\text{ s}$



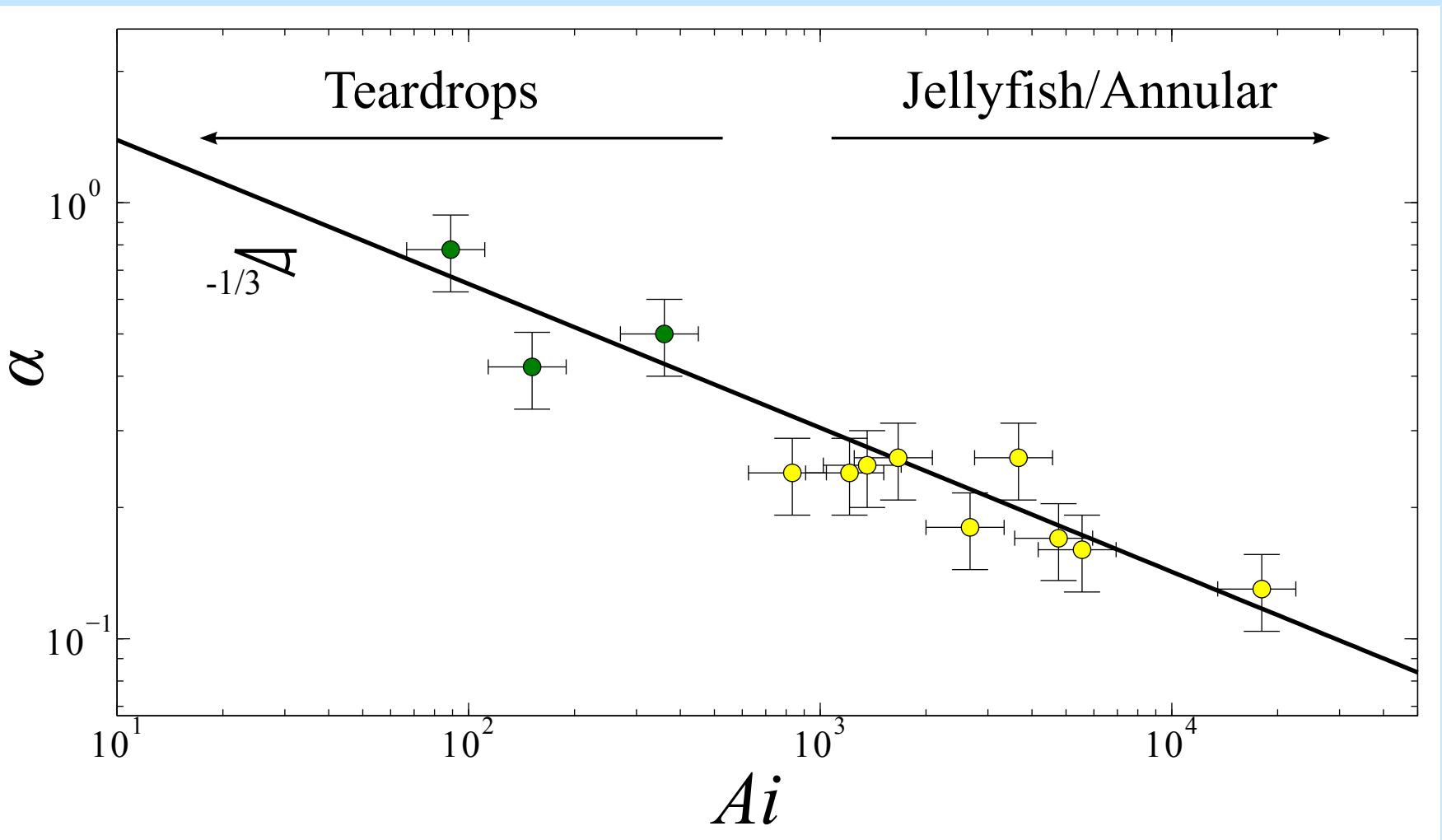
c)

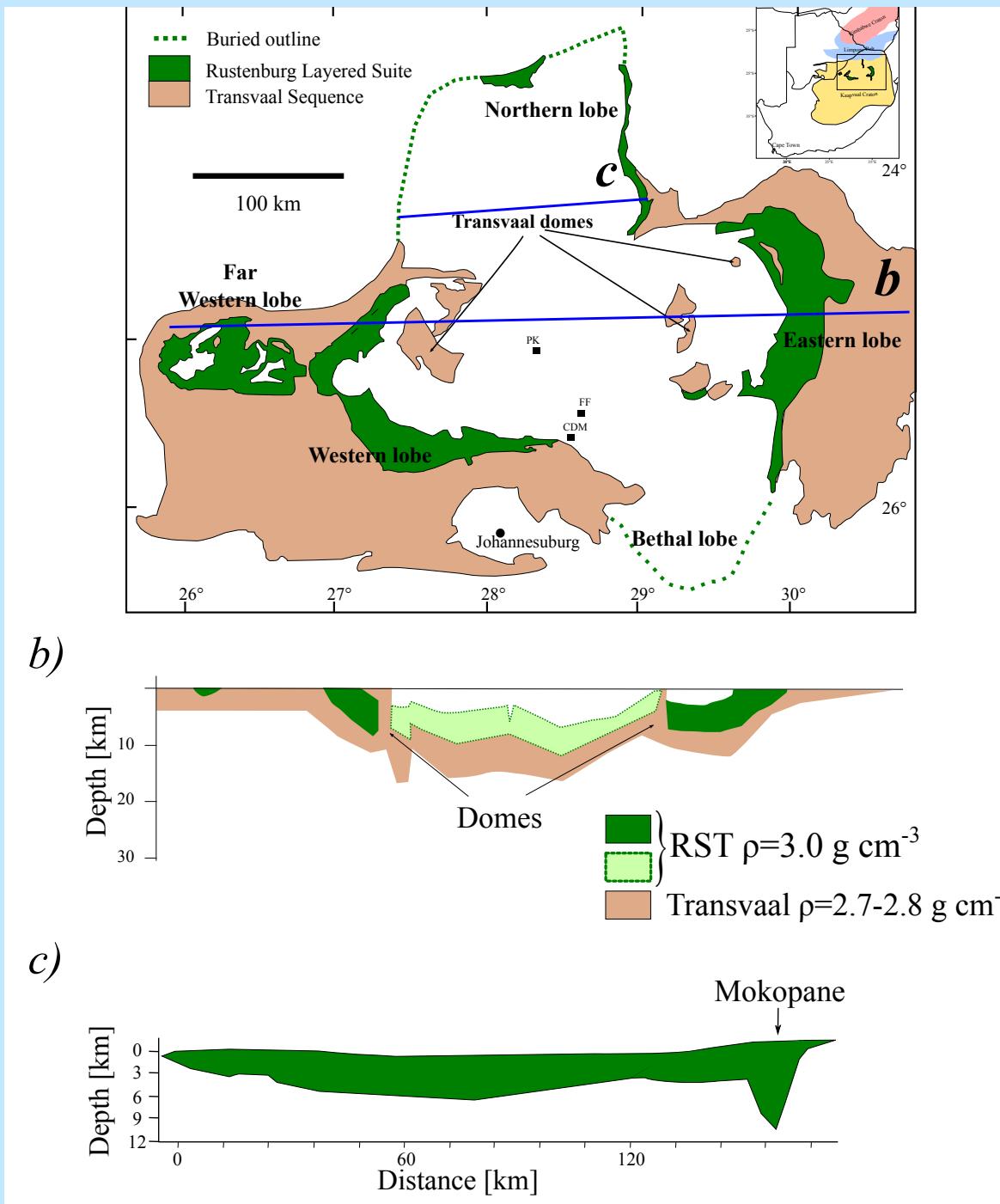


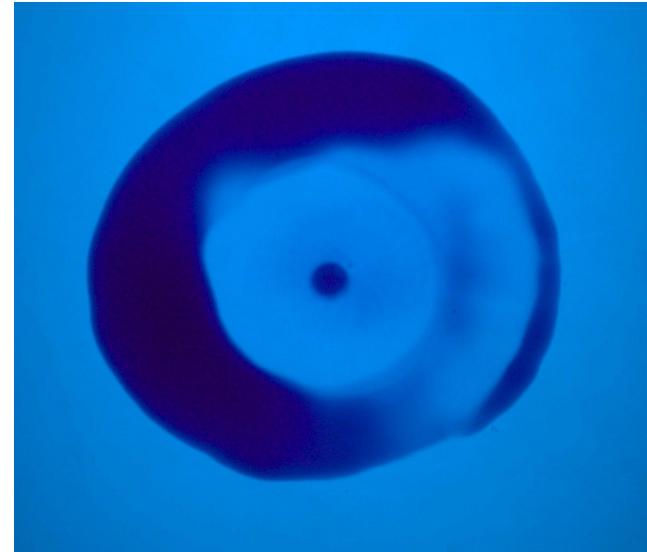
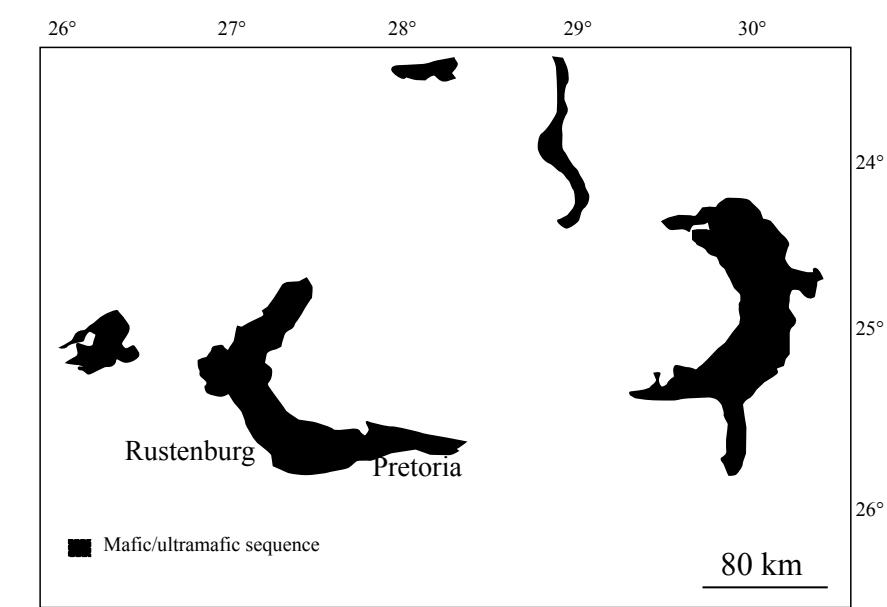
$t=580\text{ s}$



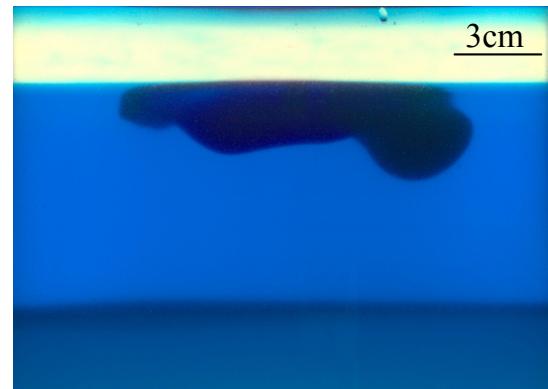
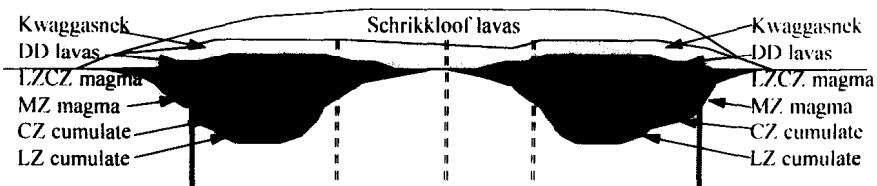
$t=870\text{ s}$

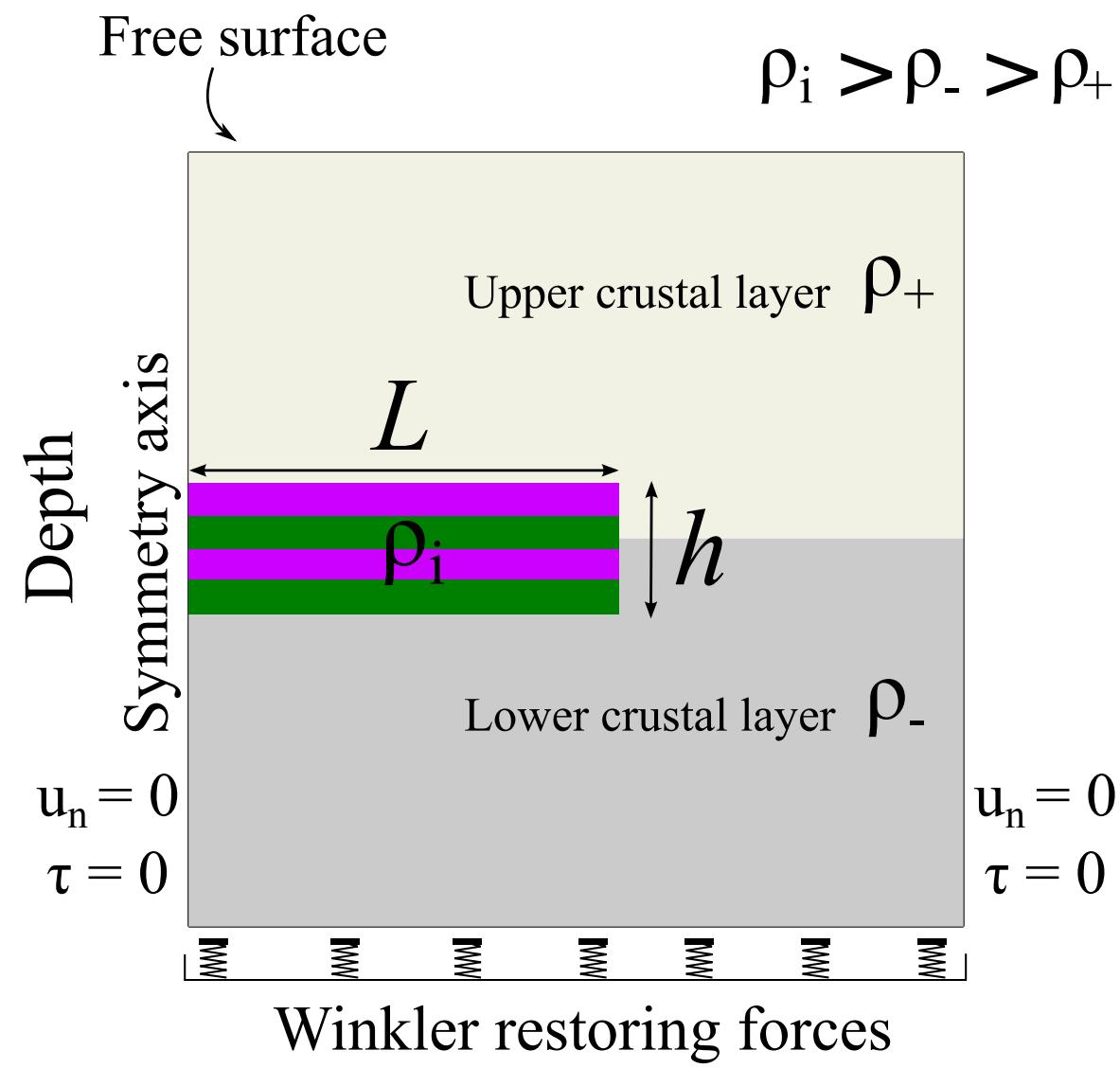




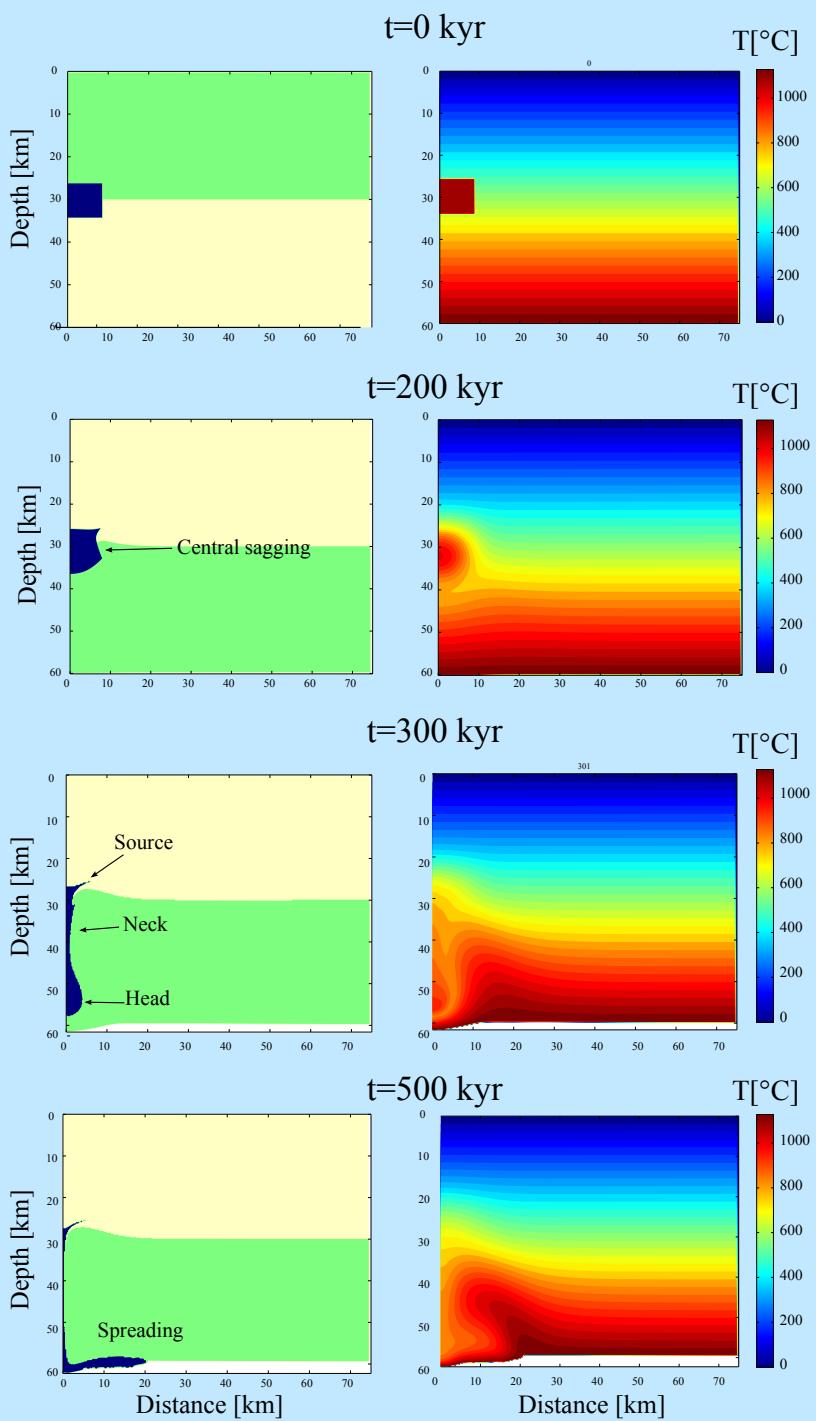


## Idealized cross-section

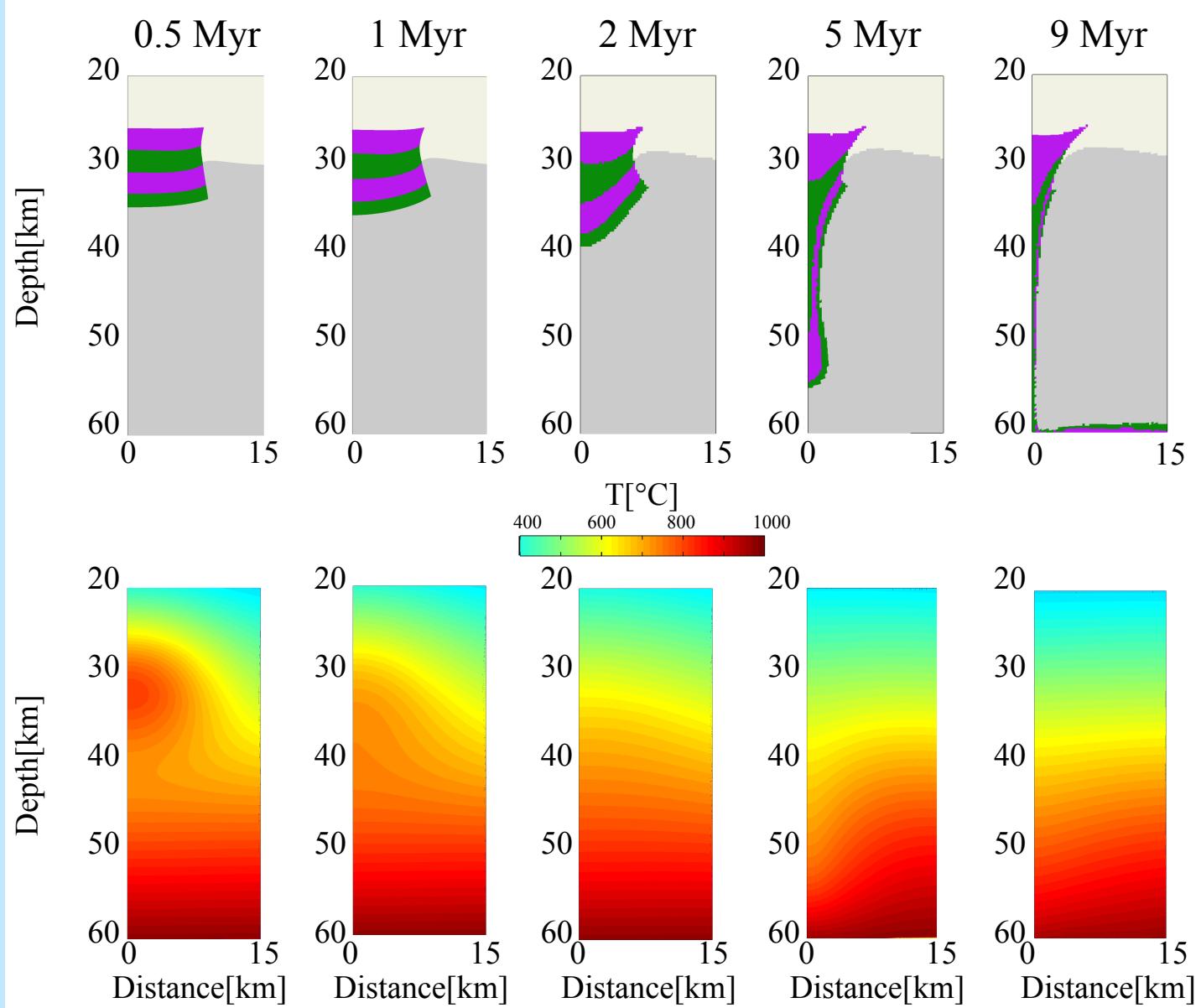


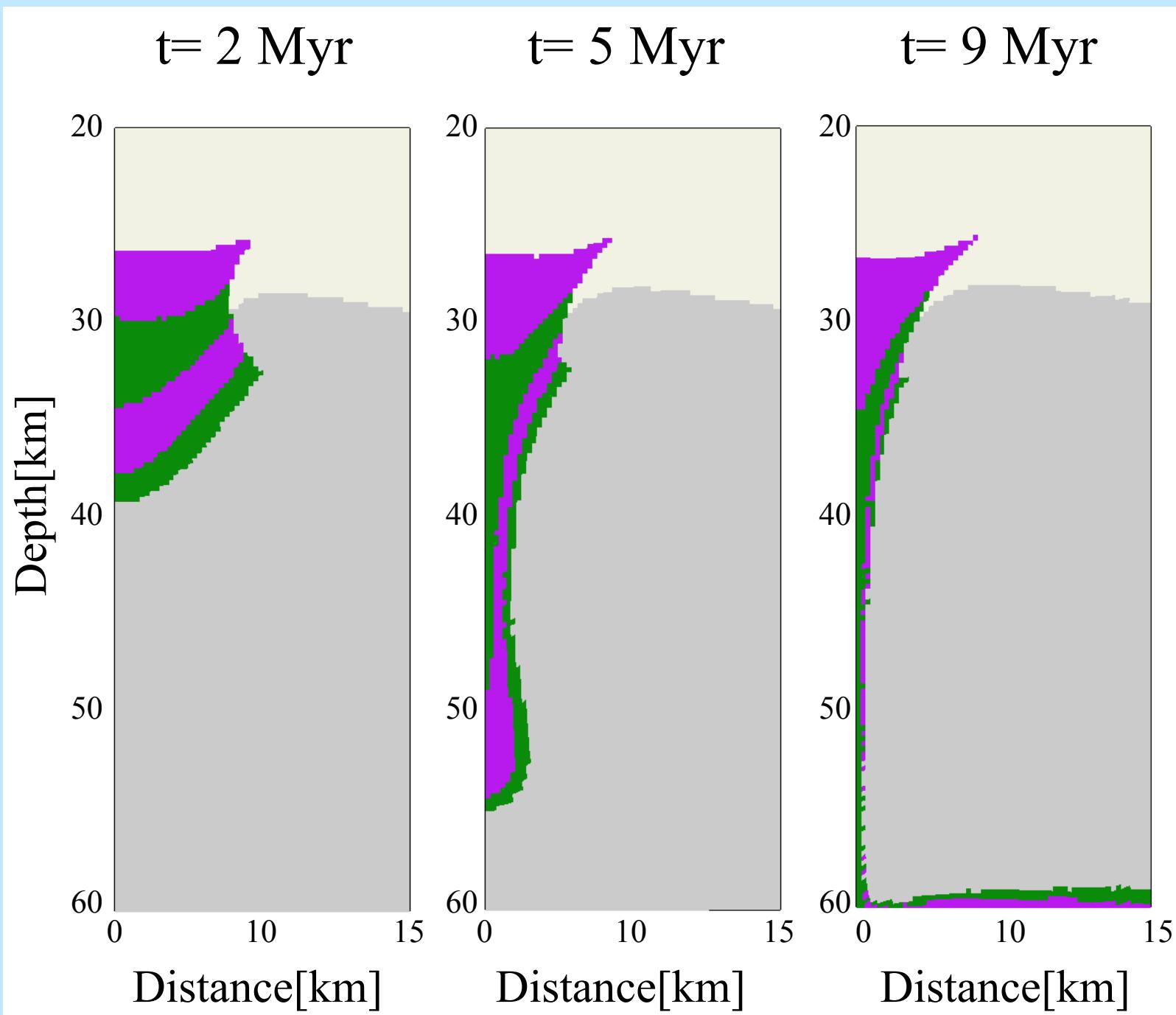


**Sinking  
regime:**  
very small  
residual volume  
at original  
emplACEMENT depth

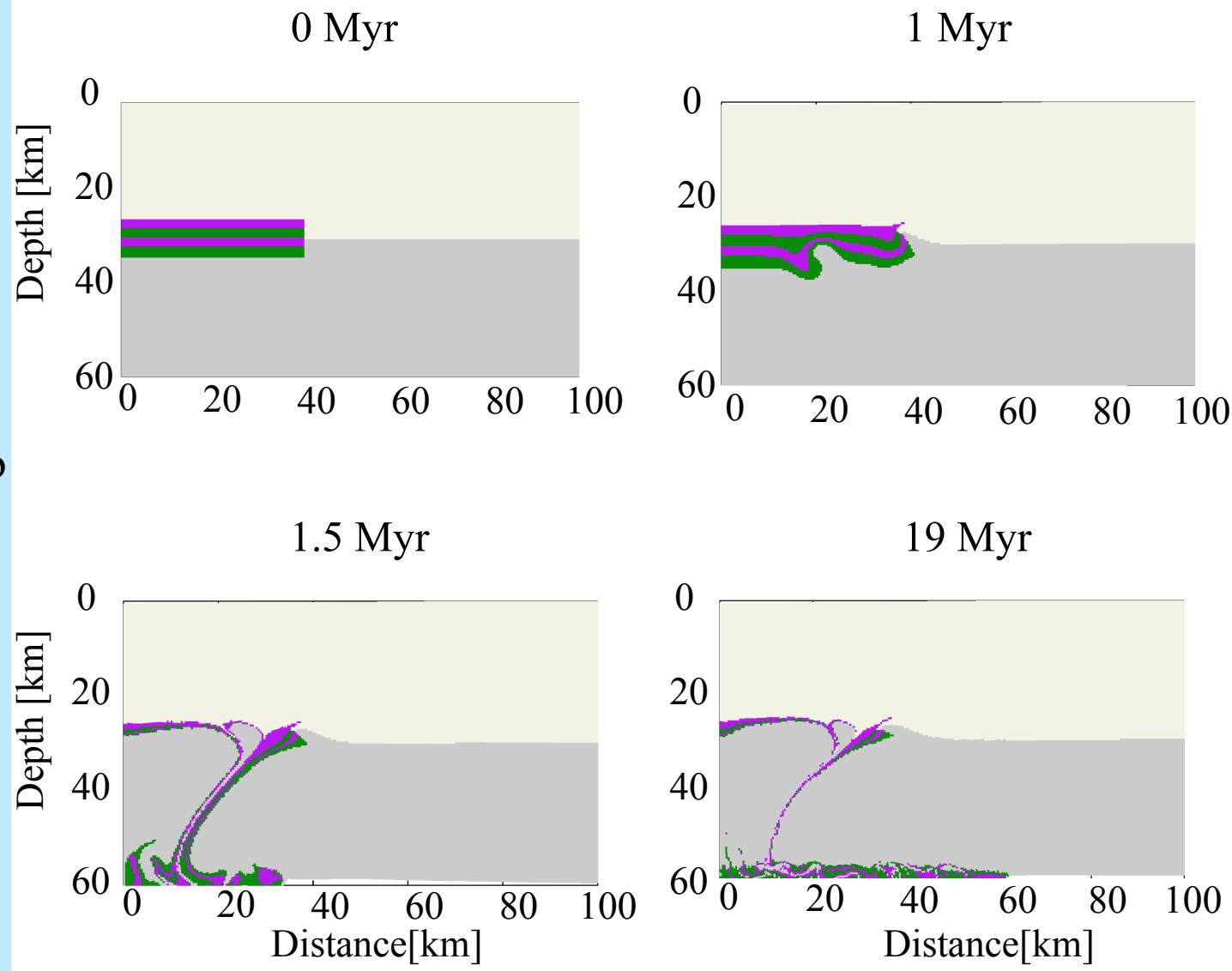


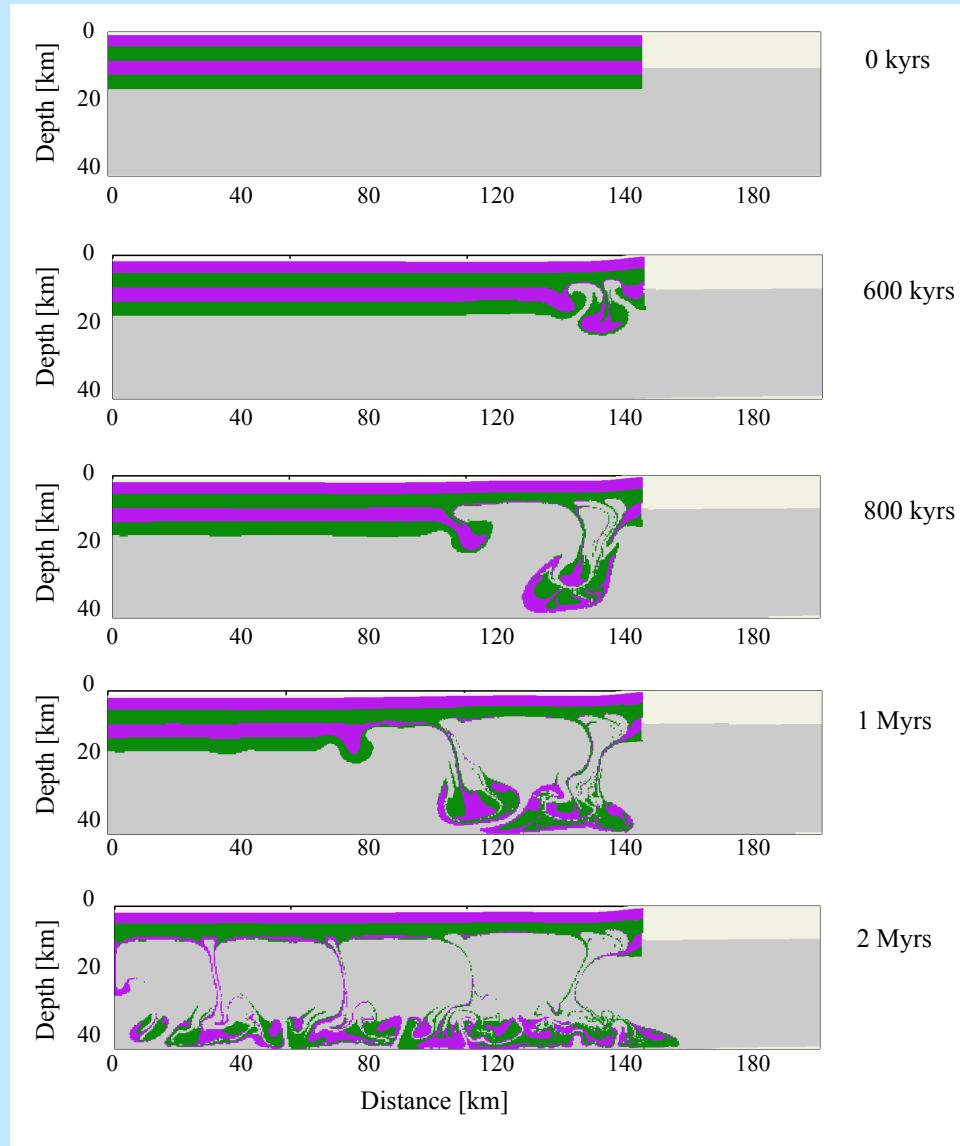
**Residual  
intrusion  
regime:**  
large volume  
left at  
original  
emplacement  
level  
**BUT**  
intrusion  
strongly deformed

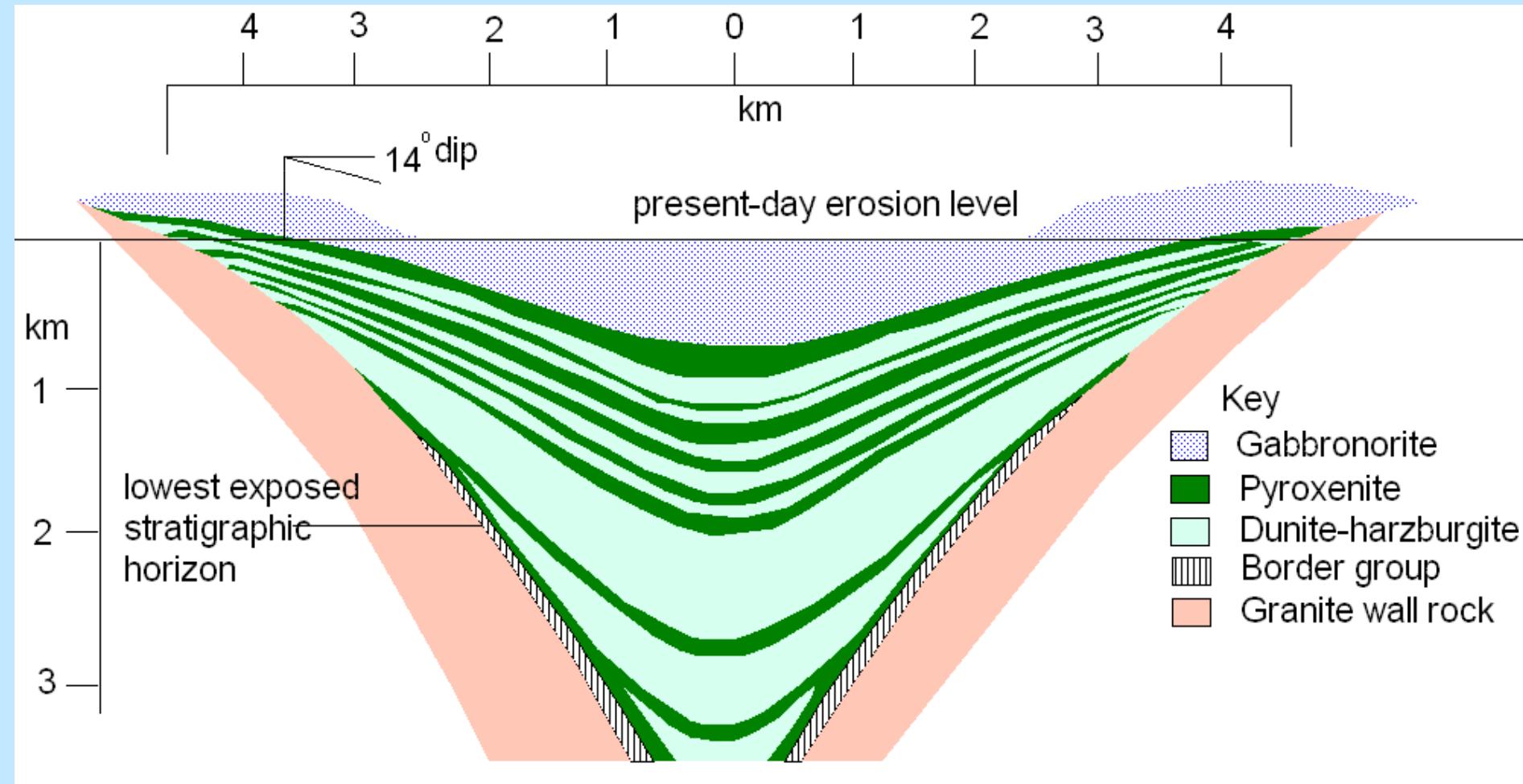


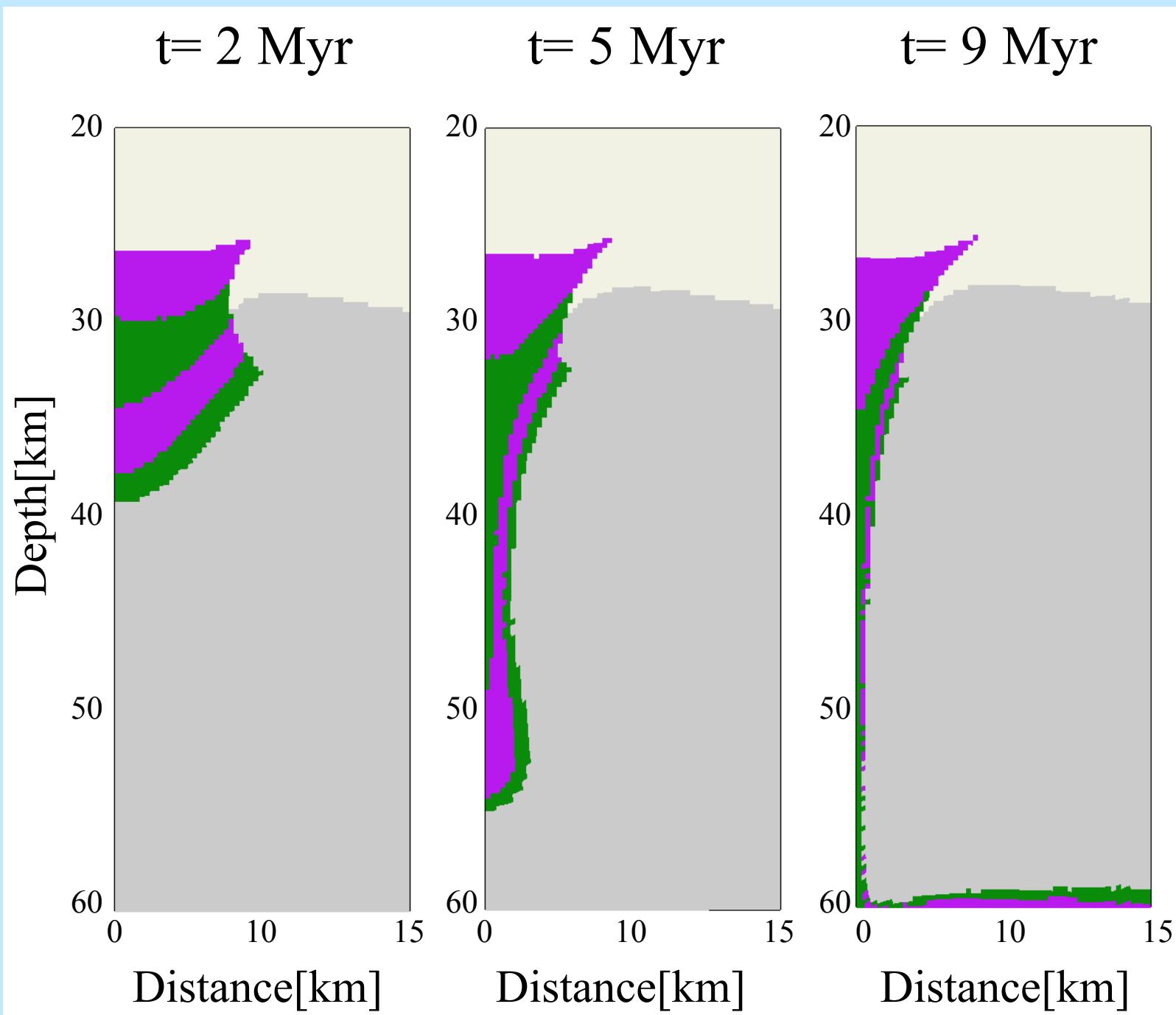


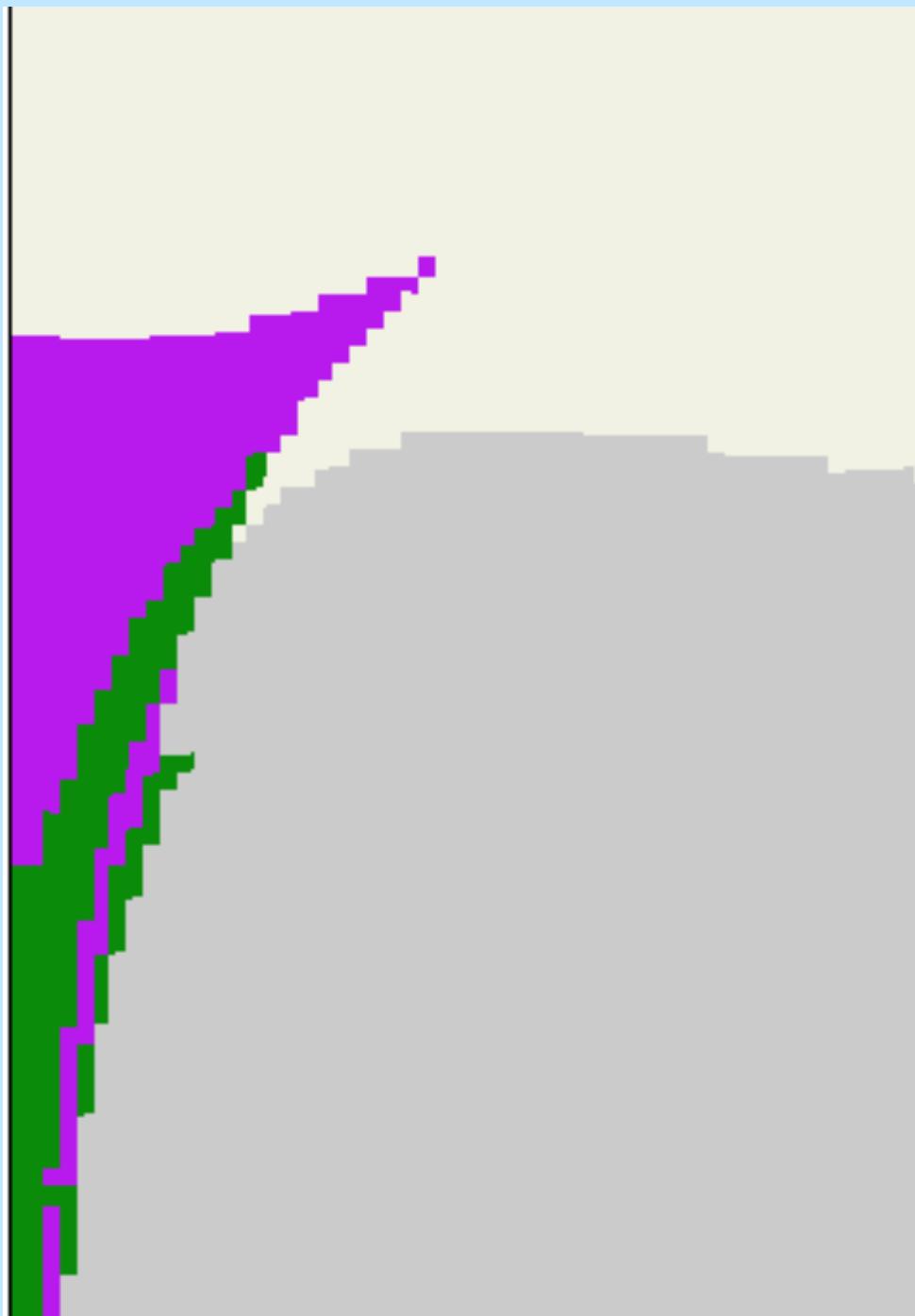
Foundering  
proceeds  
differently  
depending on  
intrusion aspect ratio

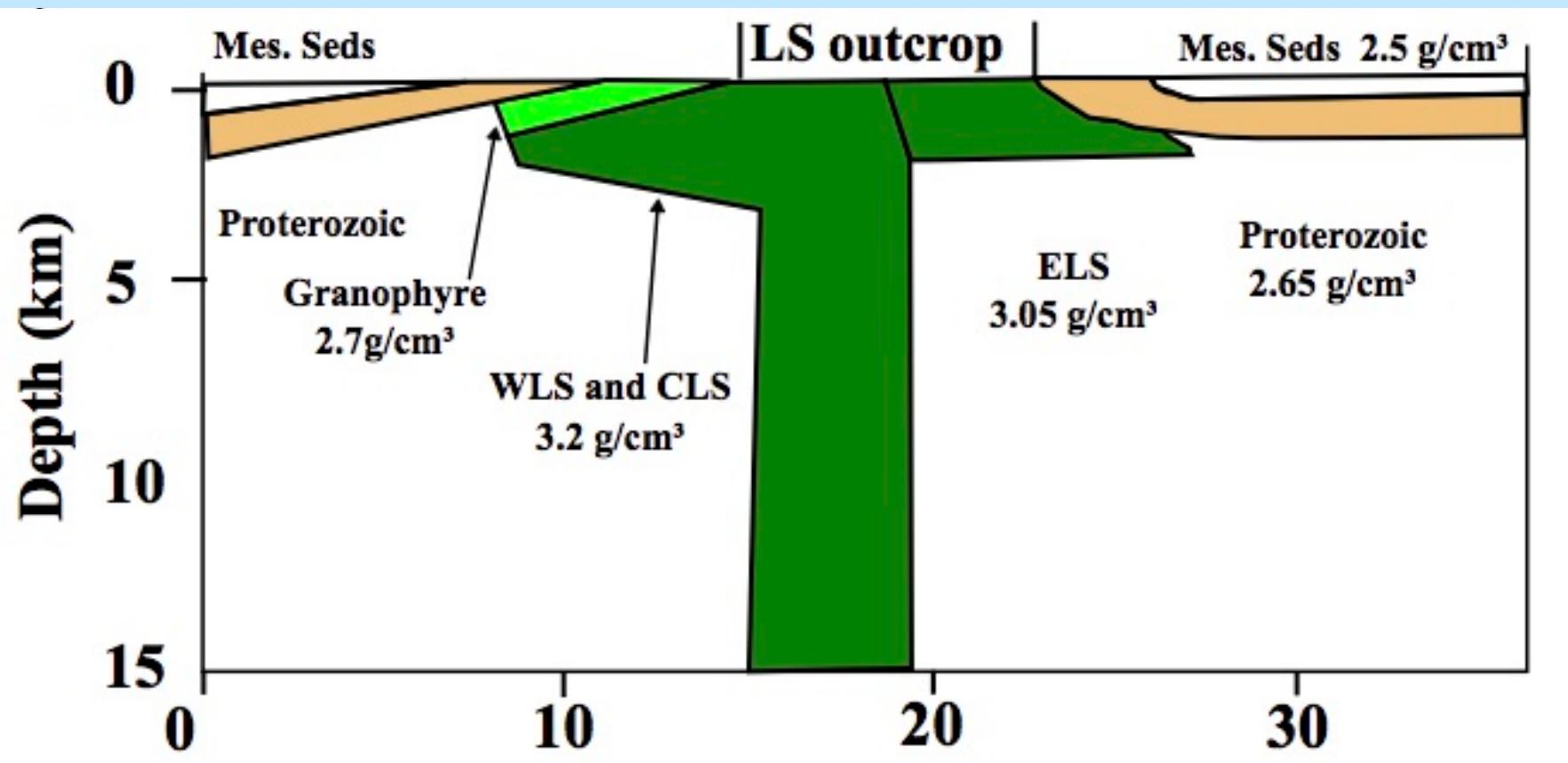


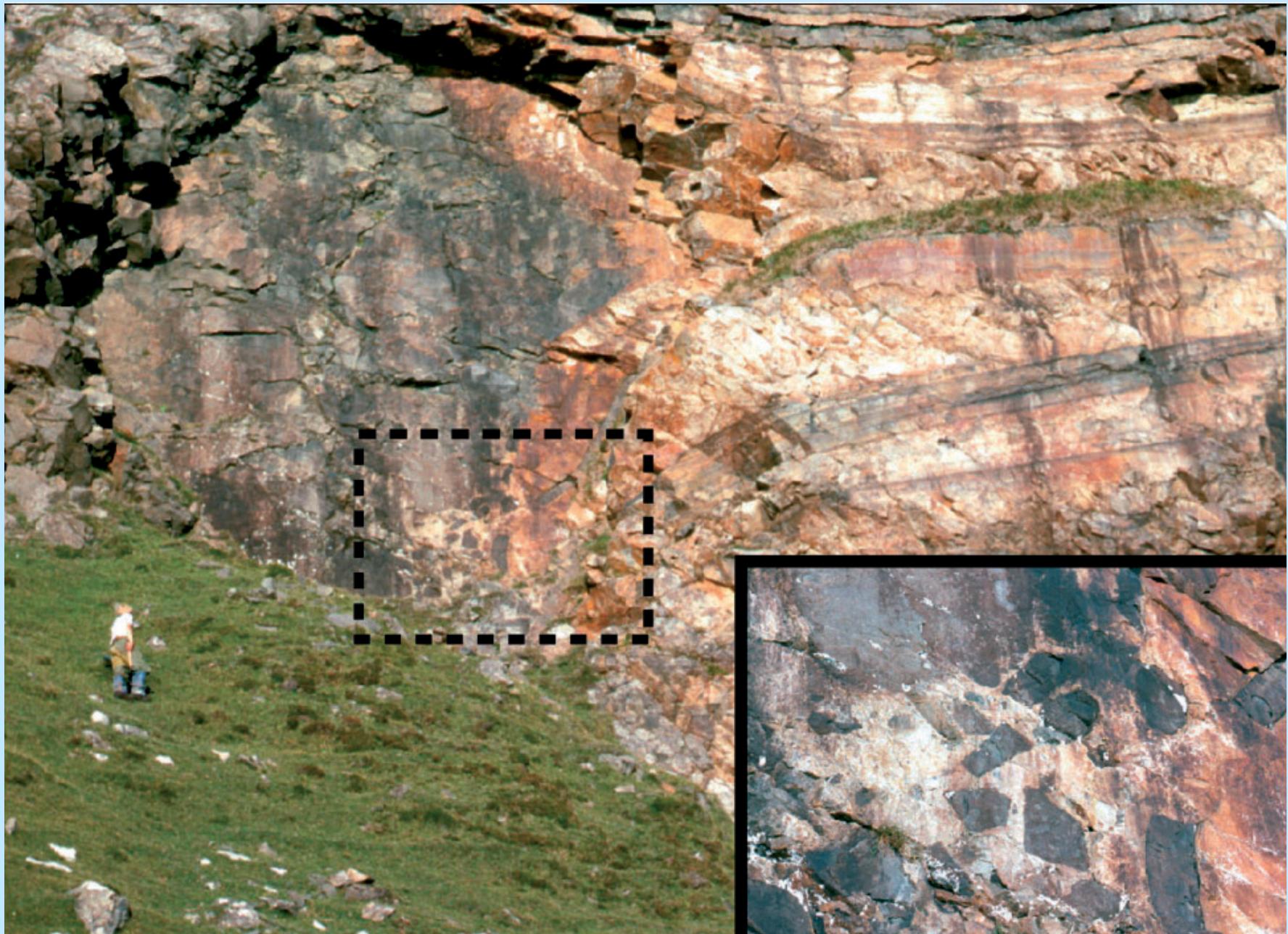


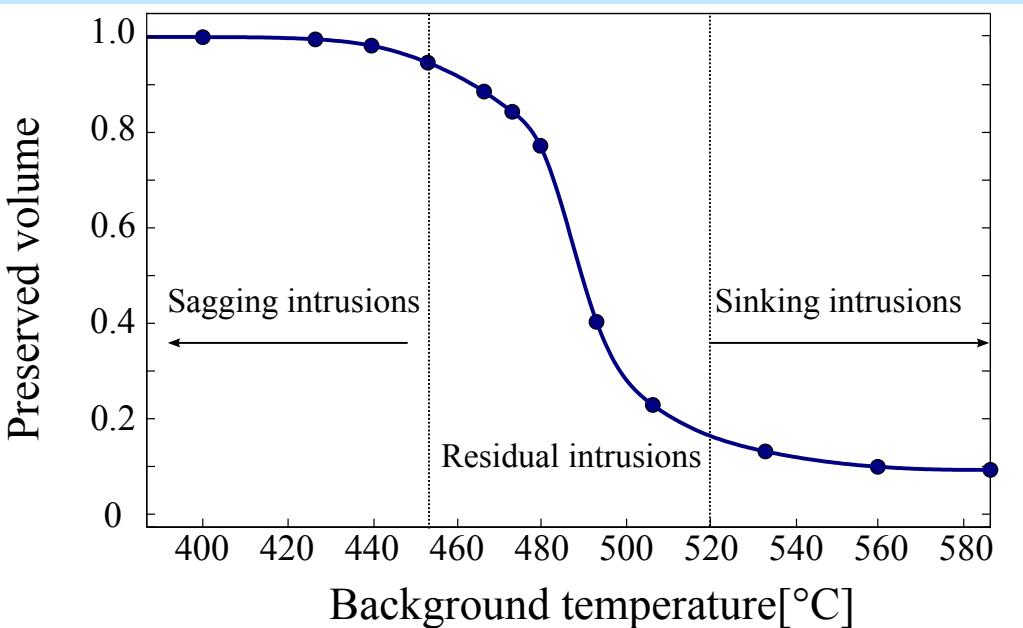












b)

