

ICTP (Trieste) 2016: Advanced School on Physics of Volcanoes

Fluid-filled fracture growth and related seismicity

Prof. Dr. Torsten Dahm

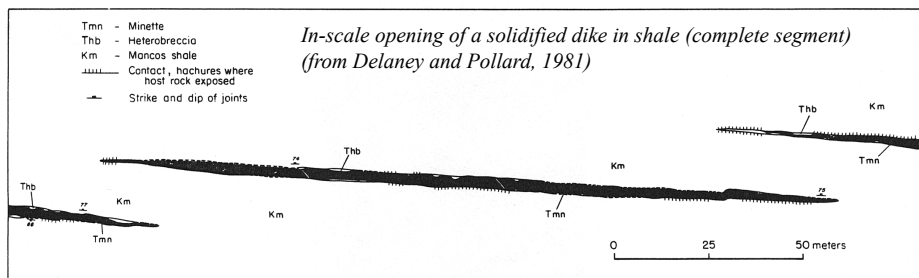
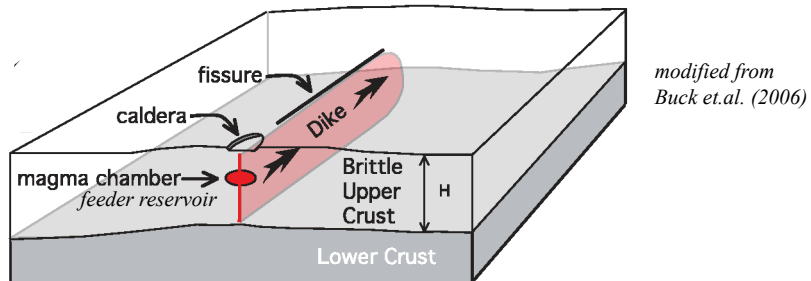
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University of Potsdam, Institute of Earth and Environmental Science, Germany*

Questions

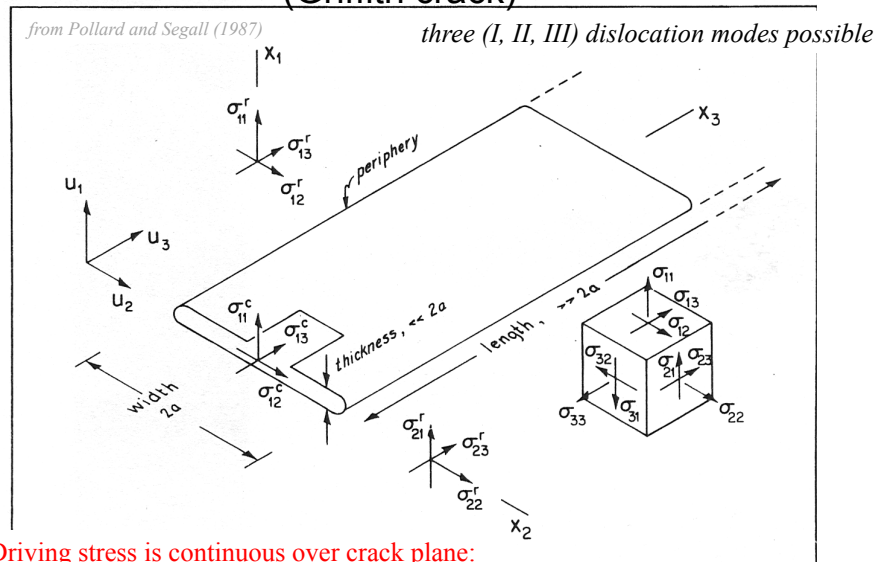
- ✓ *How do fluid-filled cracks grow ?*
- ✓ *What can we learn from shape and growth path ?*
- ✓ *What can we learn from induced seismicity?*

I) How do fluid filled fractures
form and grow ?

Schematic sketch on the generation of lateral dikes



Dislocation and stress of a planar 2D crack (Griffith crack)



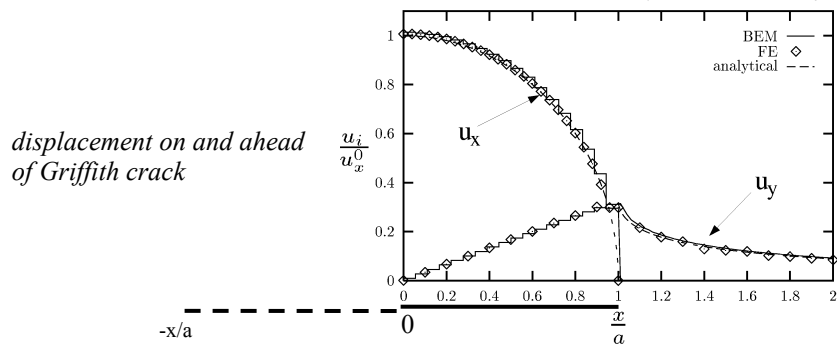
Driving stress is continuous over crack plane:

$$[\Delta\sigma^{(1)}, \Delta\sigma^{(2)}, \Delta\sigma^{(3)}] = [\Delta\sigma^I, \Delta\sigma^{II}, \Delta\sigma^{III}] = [(\sigma_{11}^r - \sigma_{11}^c), (\sigma_{12}^r - \sigma_{12}^c), (\sigma_{13}^r - \sigma_{13}^c)]$$

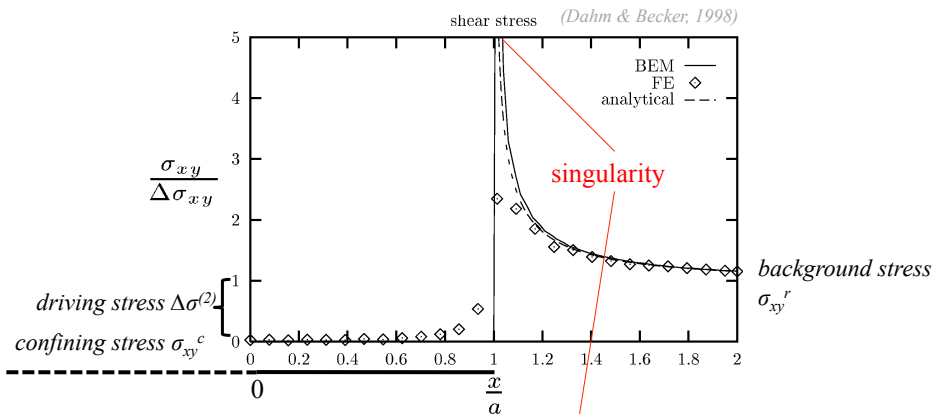
Crack opening Δu

$$\begin{Bmatrix} \Delta u_1 \\ \Delta u_2 \\ \Delta u_3 \end{Bmatrix} = \begin{Bmatrix} \sigma^I \\ \sigma^{II} \\ \frac{\sigma^{III}}{1-\nu} \end{Bmatrix} \frac{2(1-\nu)}{\mathcal{N}} \sqrt{a^2 - x_2^2} .$$

comparison of analytical and different numerical methods (Dahm & Becker, 1998)



Stress on and ahead of Griffith crack



stress in a small distance r_1 from crack tip

$$\sigma_{ij} = \underbrace{\Delta \sigma^{(m)} \sqrt{\pi a}}_K \frac{1}{\sqrt{2\pi r_1}} f_{ij}^{(m)}(\theta_1)$$

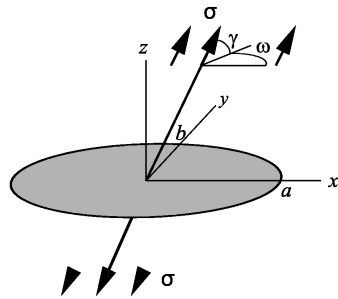
shape function (bounded)

with stress intensity factor

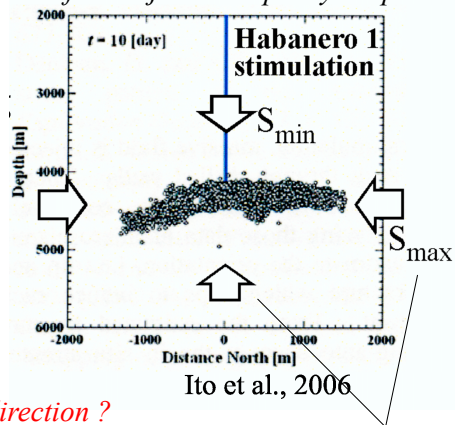
$$K = \Delta \sigma^{(m)} \sqrt{\pi a} .$$

More realistic: 3D cracks (circular or elliptical)

Penny shaped crack



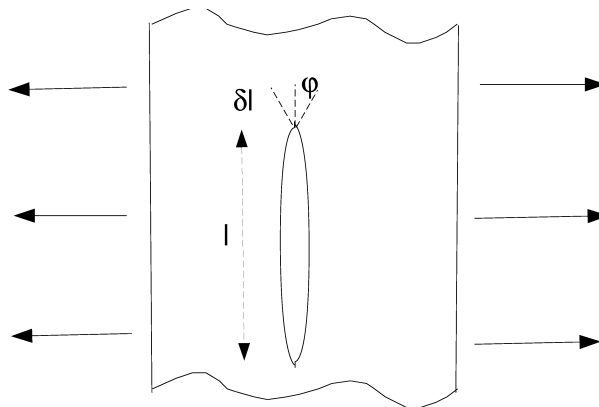
Induced seismicity from borehole fluid injection is penny shaped



- Do fluid-filled cracks open in S_{min} direction ?
- Do they grow in plane defined by $S_{max} - S_2$?

Principal stresses

In which direction do cracks grow ?



The strain energy released with incremental length growth: $(\delta Q/\delta l)$

Fracture criterion: $\delta Q/\delta l > \text{threshold}$ and $\delta Q/\delta l$ is maximal

(alternativ: stress intensity factor $K > \text{fracture toughness } K_c$)

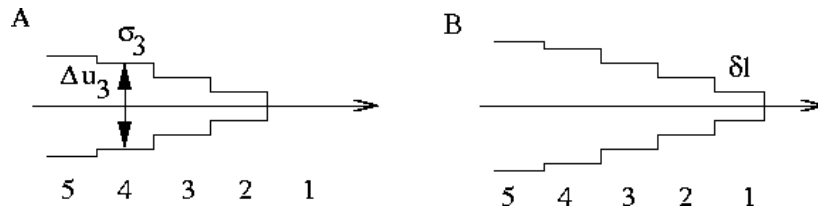
Analytical and numerical approach of Griffith growth

Analytical: e.g., find maximum of stress intensity K :

$$\text{strain energy } Q_u = \frac{1}{2} \int_{-a}^a (\bar{\sigma}_n \Delta u_n + \bar{\sigma}_s \Delta u_s) dx$$

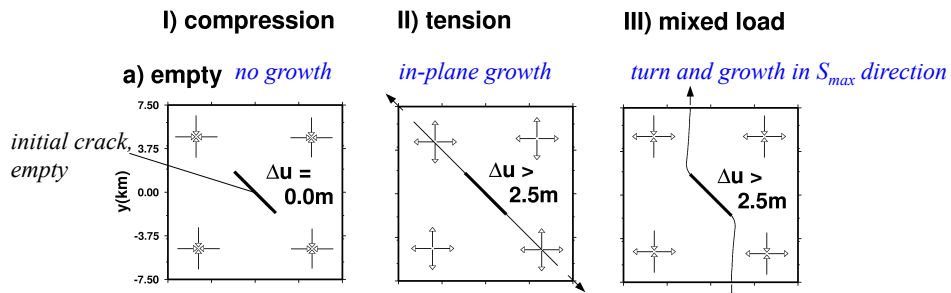
$$\frac{\delta Q}{\delta l} = \frac{(Q_U^B - Q_U^A)}{\delta l} = \mathcal{G} = \frac{(1-\nu)}{2\mathcal{N}} K_I^2$$

Numerical: estimate $Q_u(A)$ and $Q_u(B)$ and find maximum of $[Q_u(B) - Q_u(A)]/\delta l$:



Numerical simulation of crack growth and arrest

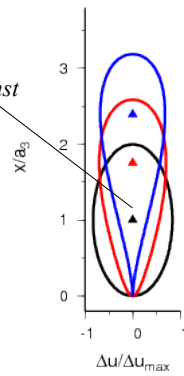
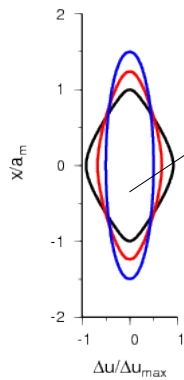
Dahm (2000)



Fluid-filled cracks of finite "volume"

overpressurized, symmetric crack expands (bilateral viscous flow)

unilateral expansion from quasi-static re-adjustment with apparent buoyancy

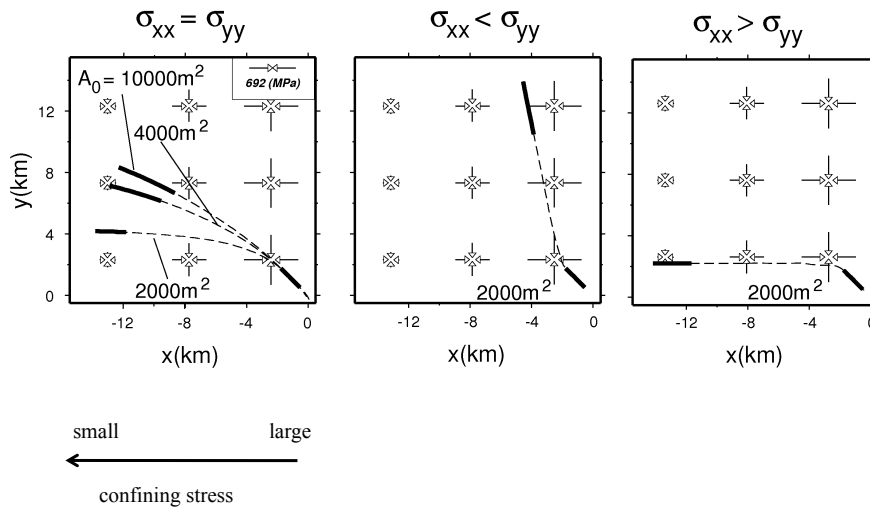


Ambient pressure changes as

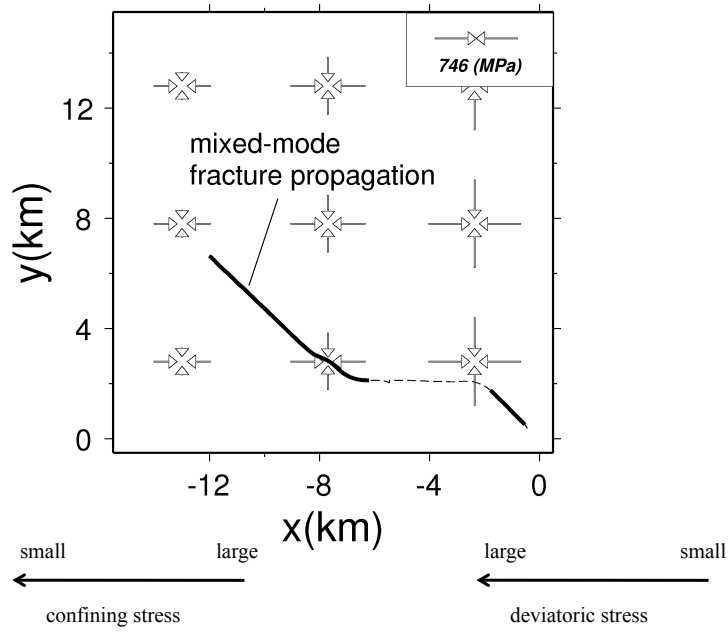
$$\Delta P = -K \Delta V / V_0$$

(decompression leads to small volume expansion)

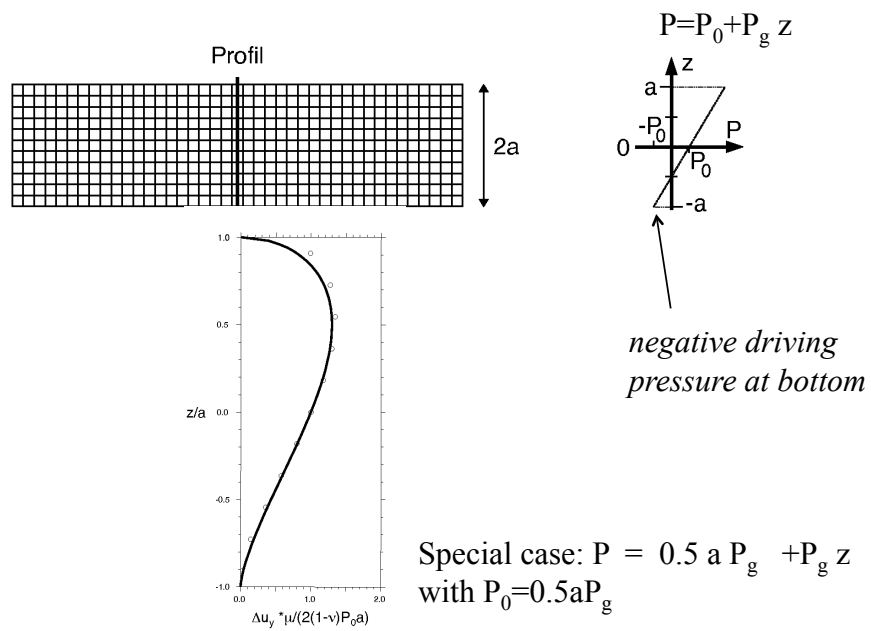
The influence of stress gradients



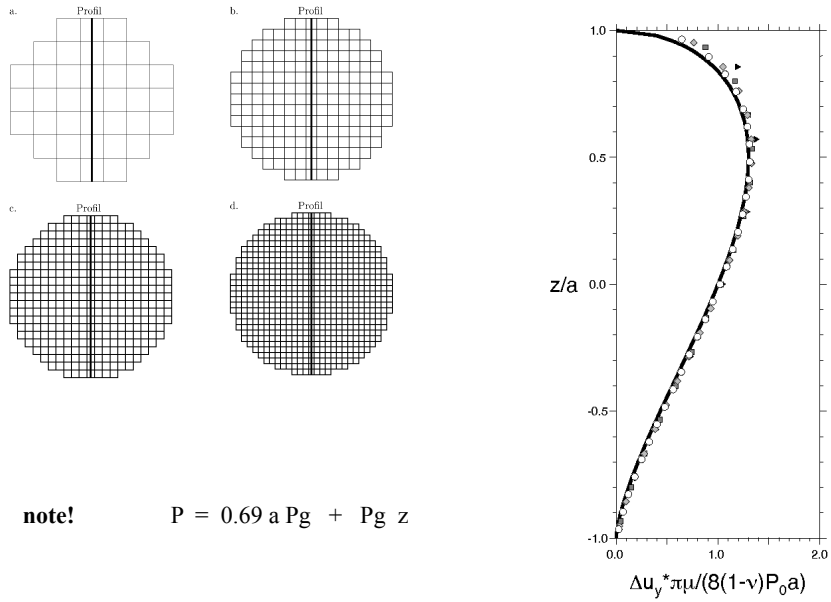
Is mixed-mode propagation possible ?



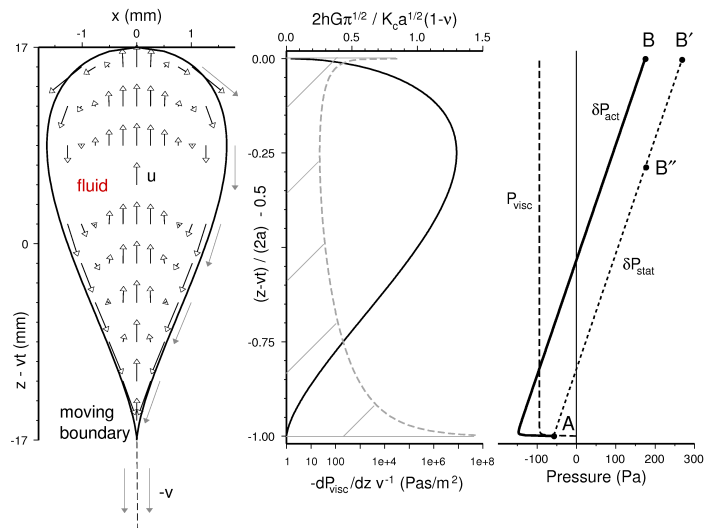
Fluid filled Griffith crack under linear increasing pressure



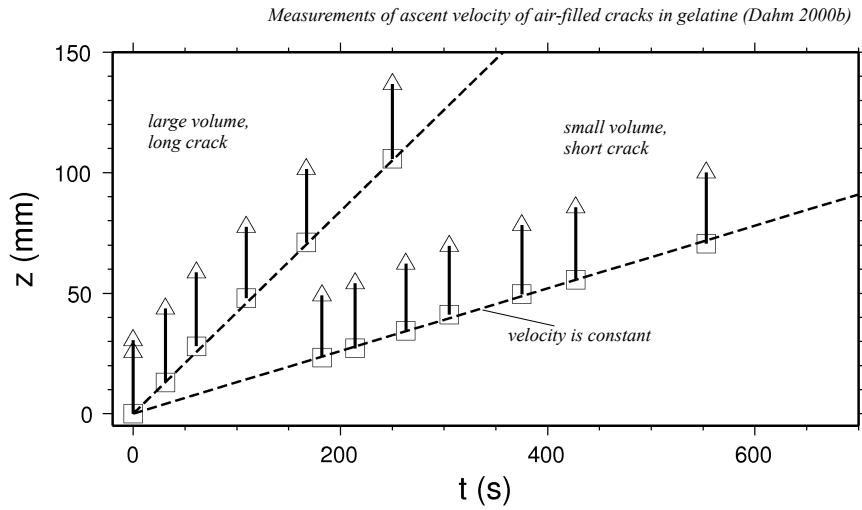
Fluid filled penny shaped crack under linear increasing P



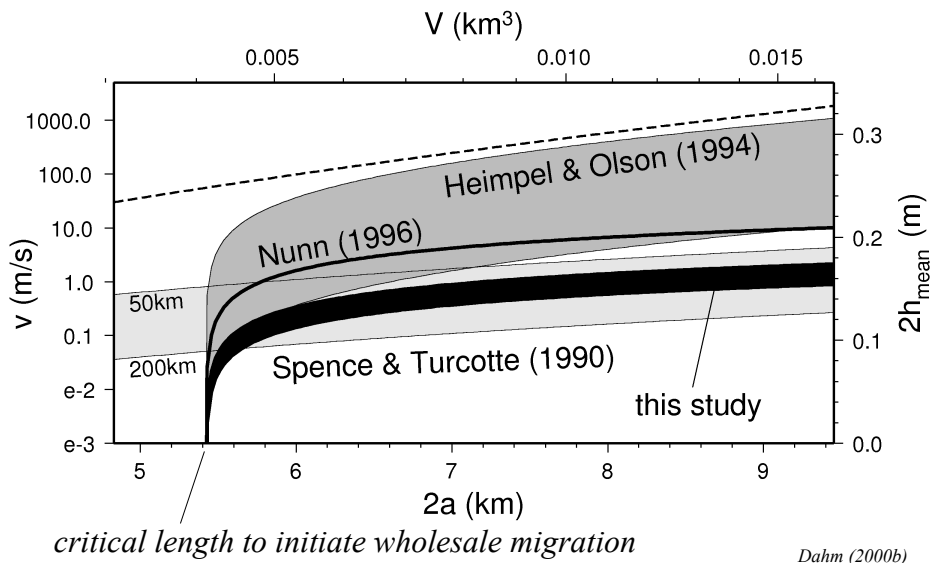
Weertmann crack: wholesale crack "ascent"



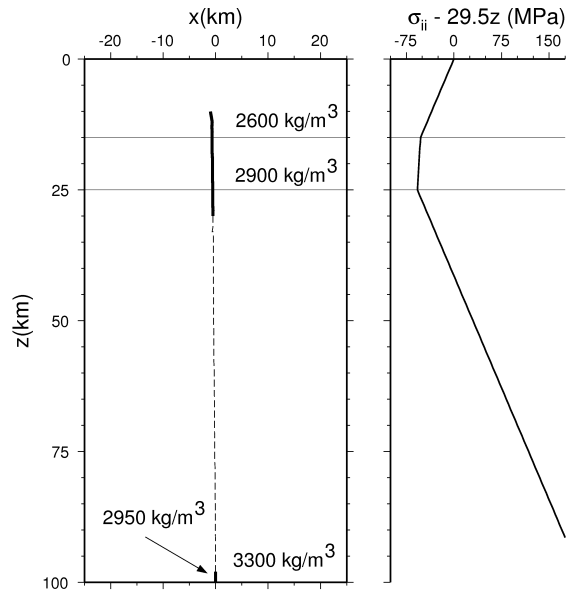
velocity of wholesale crack ascent



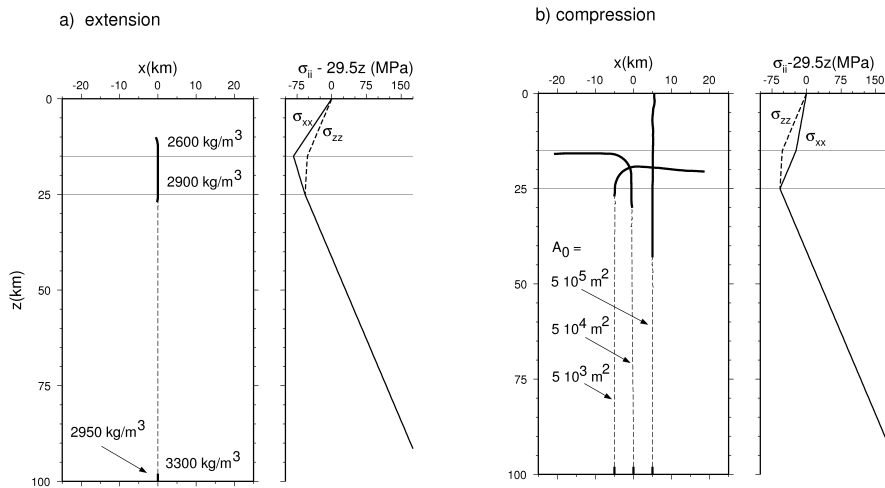
Ascent velocity of magma-filled dikes in mantle



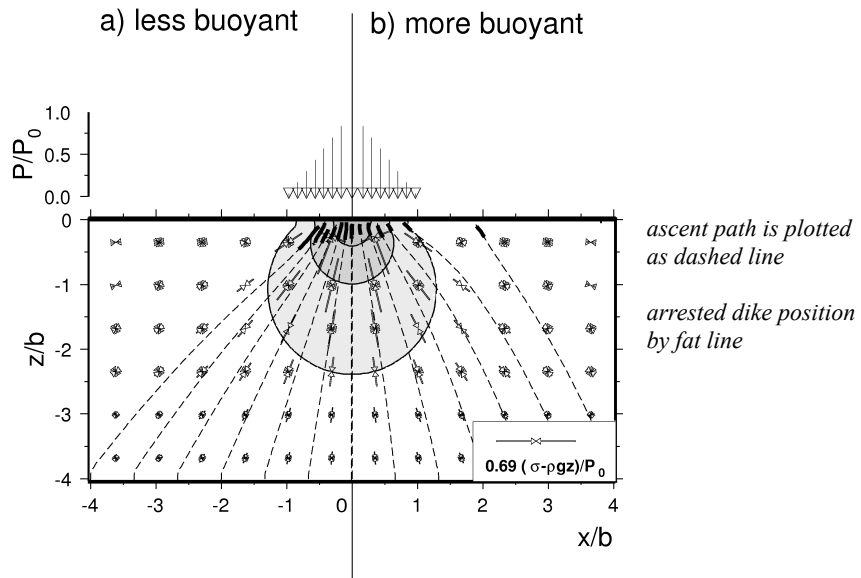
Simulation of dike ascent in crust and mantle



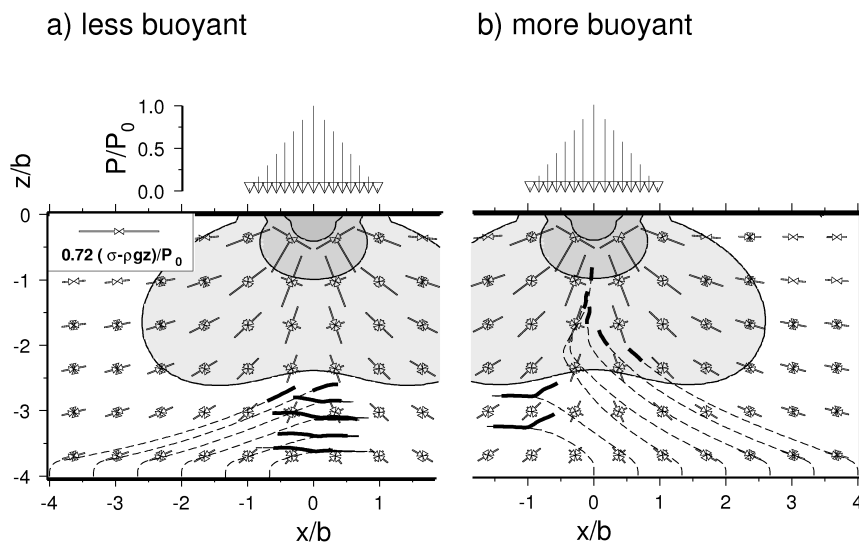
When do sills form and magmatic underplating occurs?



The apparent “attraction” depends on magma density



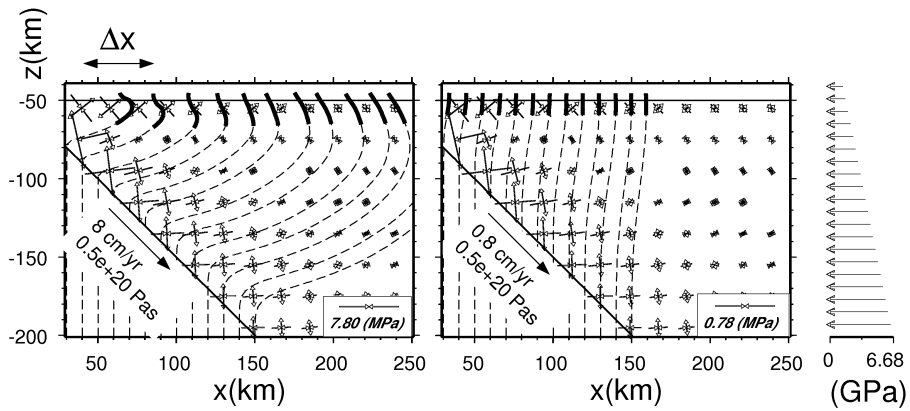
Dike ascent under tectonic compression



Mantle corner flow above a subducting slab

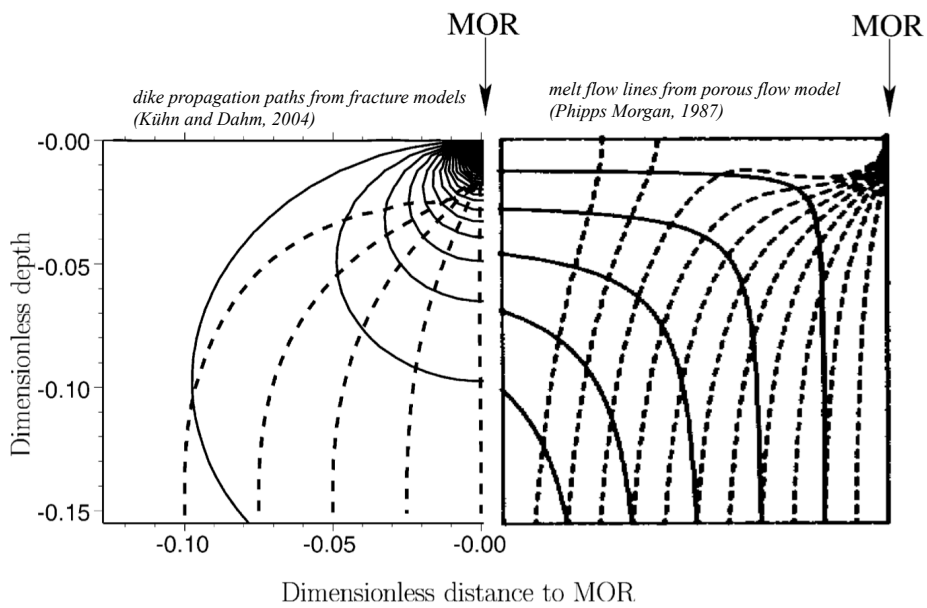
a) faster subduction

b) slower subduction



Dahm (2000a)

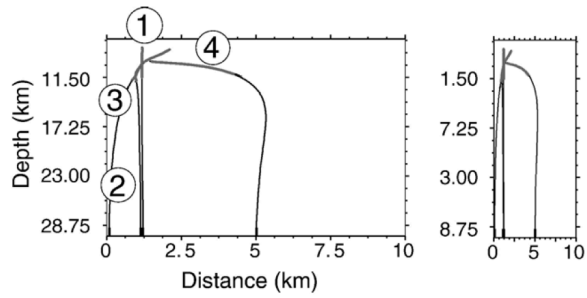
Dike ascent in mantle beneath mid-oceanic ridges



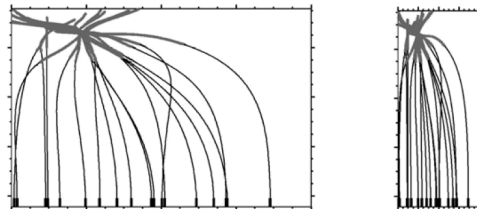
Crack-crack interaction in mud (influence of self stress)



Interaction of sequentially intruding dikes



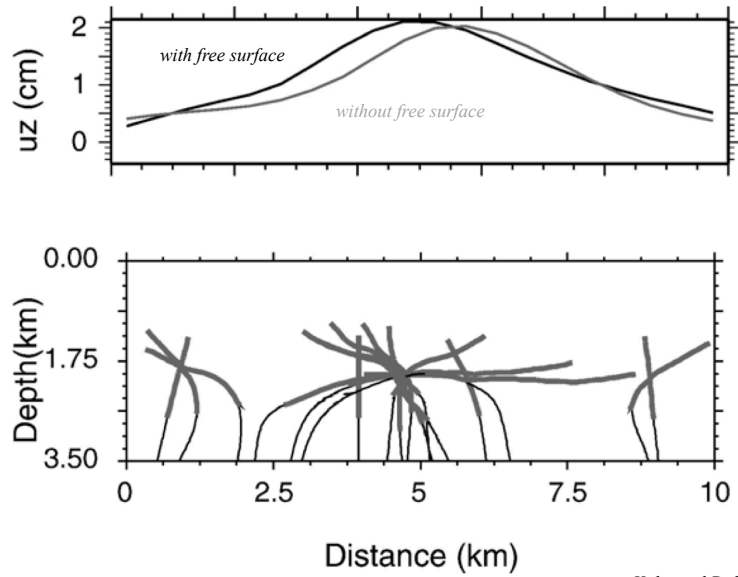
(a)



(b)

Kühn and Dahm (2008)

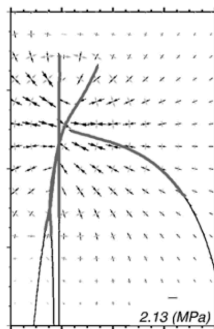
Simulation of oceanic crust along axis magma ascent



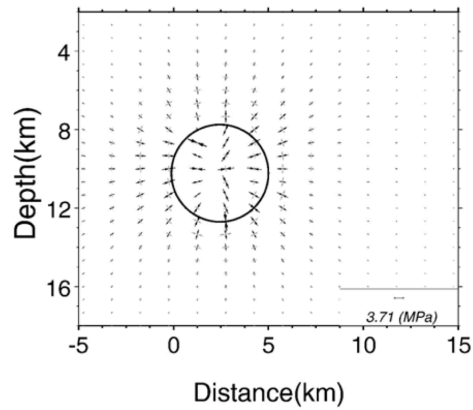
Kühn and Dahm (2008)

Interaction of dikes explains how magma chambers form

first 3 interacting dikes



stress field after 18 dikes



Kühn and Dahm (2008)

Ib) Growth controlled by injection of fluids

examples:

- lateral intrusions fed by central magma reservoir (rifting)
- mid-crustal earthquake swarms (from fluid intrusions)
- hydraulic fracturing (e.g. in tight gas sandstone)

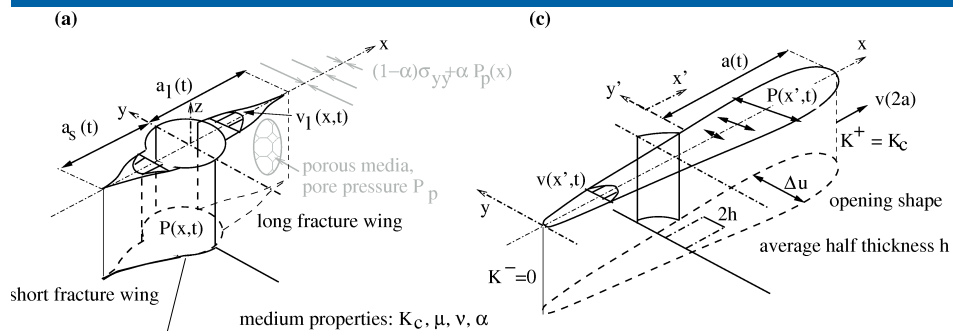
Ib) Growth controlled by injection of fluids

Fracture model for asymmetric and uni-directional growth

Injection, bilateral growth

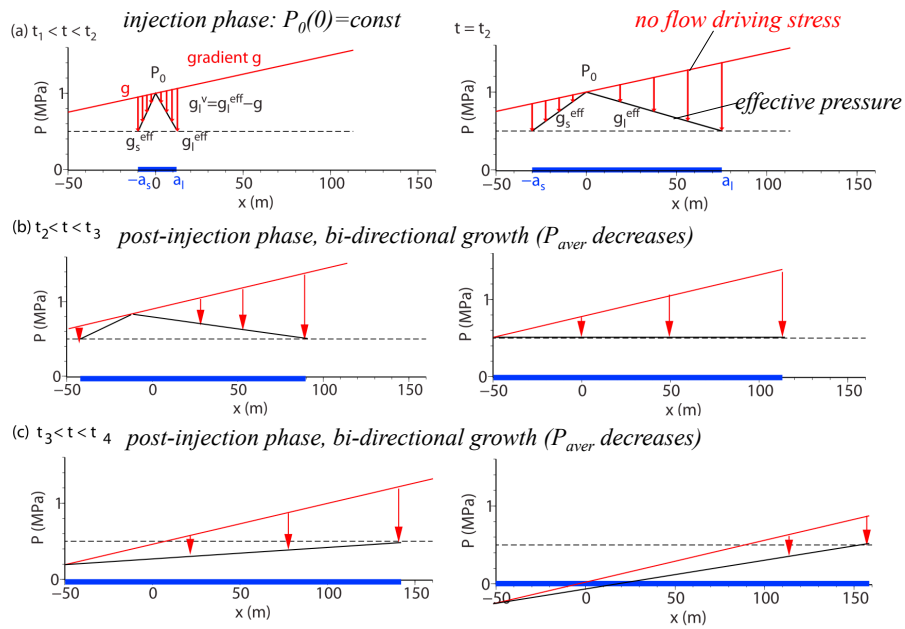
Post-injection, unilateral growth

growing style is controlled by stress gradient $g!$



borehole

Concept



fracture model

Injection phase ($P(x_0) \approx \text{const}$): asymmetric growth

short wing

long wing

fracture fronts

a_m

$g a_m / P_0 = 0.50$

a (m)

t (min)

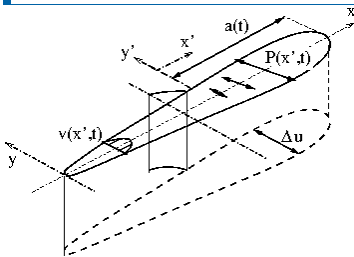
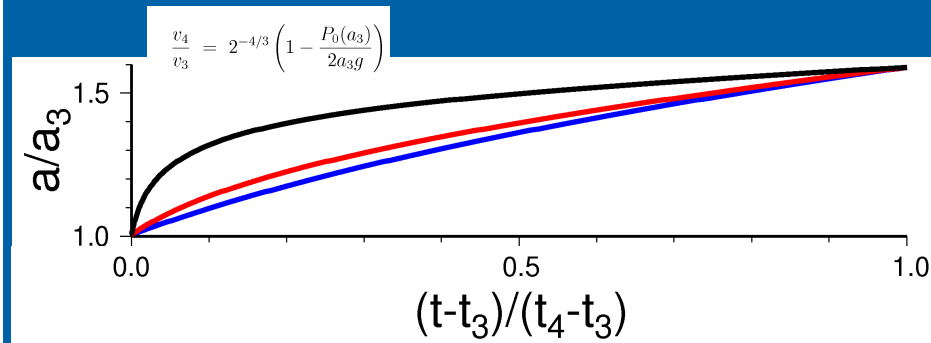
gradient / overpressure

$$\pi \left(\frac{a_l(t) - a_s(t)}{a_s^2(t) + a_l^2(t)} \right) \approx \frac{g}{P_0}$$

$a(t)$ is the time dependent wing length of the fracture

see Fischer, Hainzl and Dahm (2009): GJI

Post-injection phase ($m_{\text{fluid}} \approx \text{const}$): unidirectional growth



Summary “fluid-filled crack growth”

- ✓ Fluid-filled crack growth is controlled by 3 factors:
 - orientation of σ_{least} (least compressive stress)
 - gradients of effective driving stress (buoyancy + stress)
 - self stress generated by the crack (i.e. length and shape of dike)

→ no sharp turns, whole-sale and post-injection movement, path depends also on volume/length of dikes
- ✓ Growth is influenced by crack-crack interaction
 - localized volcanic centers may result from diffuse dike ascent
 - sills can stop “buoyant” dikes / fluid-cracks
- ✓ Deviation from penny shaped cracks arise from:
 - $\sigma_1 \neq \sigma_2$ (elliptical growth)
 - wholesale movement if overcritical length (Weertman shape)
 - confining layers and free surface

→ vertical (dikes) and horizontal (sills) length of lateral intrusion depend (also) on effective “overpressure”

Summary “injection-related” fractures

- ✓ Asymmetric bi-lateral growth during injection is possible
 - the time function depends on K_c and fluid viscosity
 - ratio between long and short wing depends only on gradient

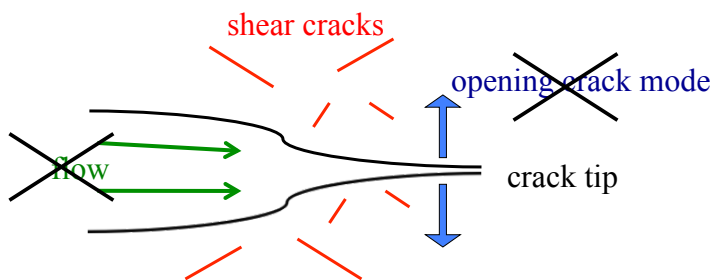
- ✓ After injection, self similar, bi- and unilateral expansion
 - length increase is always 1.5 of length at end of transition (injection)
 - time dependency of expansion depends on driving stress gradient

- ✓ Crack opening and stress buildup in rock explains
 - bilateral front of seismicity during injection
 - shape of unilateral front and backfront of seismicity in post-injection

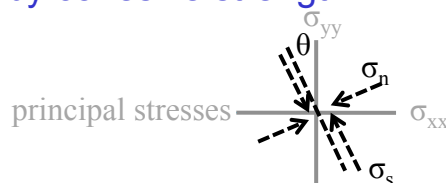
II) How are earthquakes triggered (seismicity models)

Key message

Seismicity accompanying fluid-filled fracture growth is (usually) not associated with the crack tip opening itself, but represents triggered shear cracks in the rock which experiences stress increase



Shear rupture is driven by “shear stress” and hindered by cohesive strength



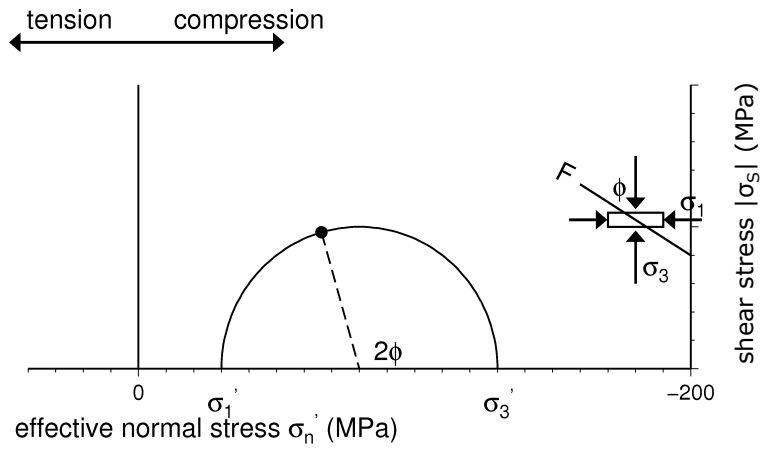
Normal and shear stress on dipping fault (Mohr circle)

$$\sigma_n = \frac{\sigma_{xx} + \sigma_{yy}}{2} + \frac{\sigma_{xx} - \sigma_{yy}}{2} \cos 2\Theta$$

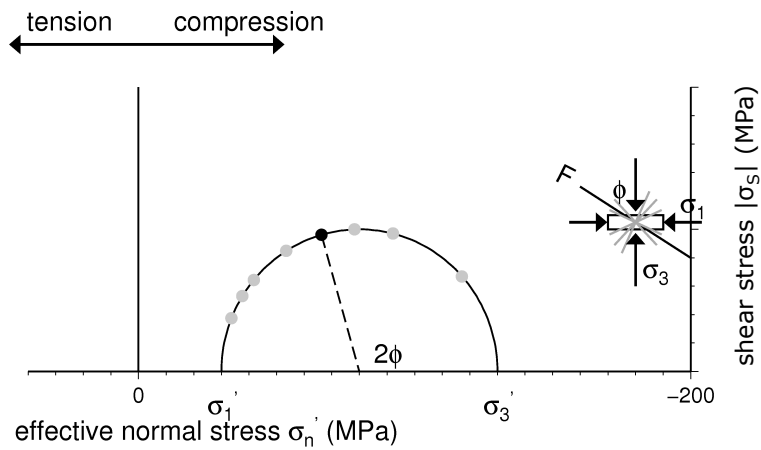
$$\sigma_s = -\frac{(\sigma_{xx} - \sigma_{yy})}{2} \sin 2\Theta .$$

Here: tensional stress is **positive**

(3) from failure criteria to seismicity models

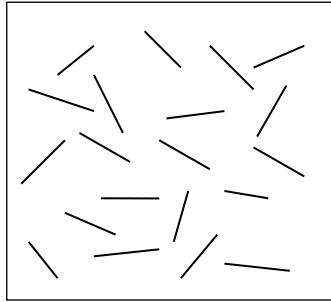


distribution of faults in arbitrary orientations

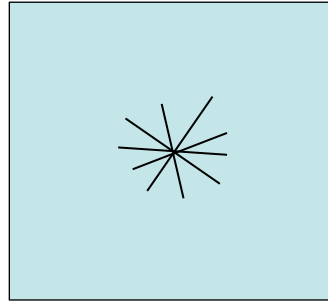


effective media model

real rock with with distribution of cracks / flaws with random orientation effective media model with single crack of random orientation

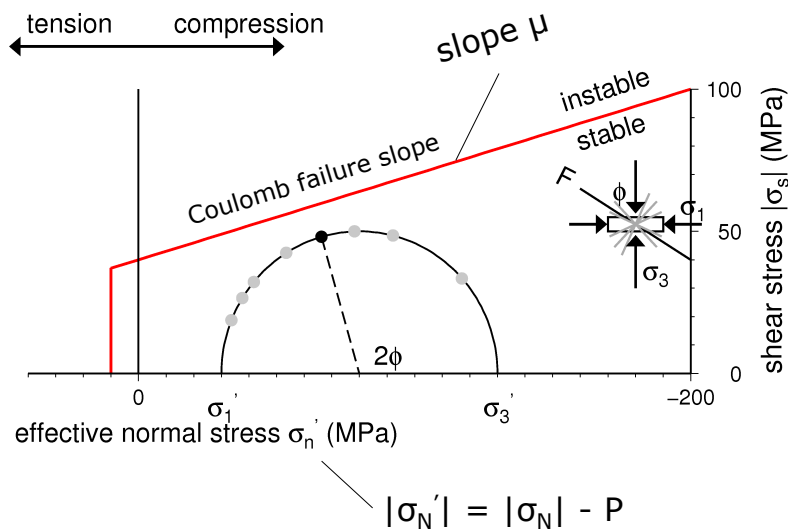


heterogeneous stress on micro-scale

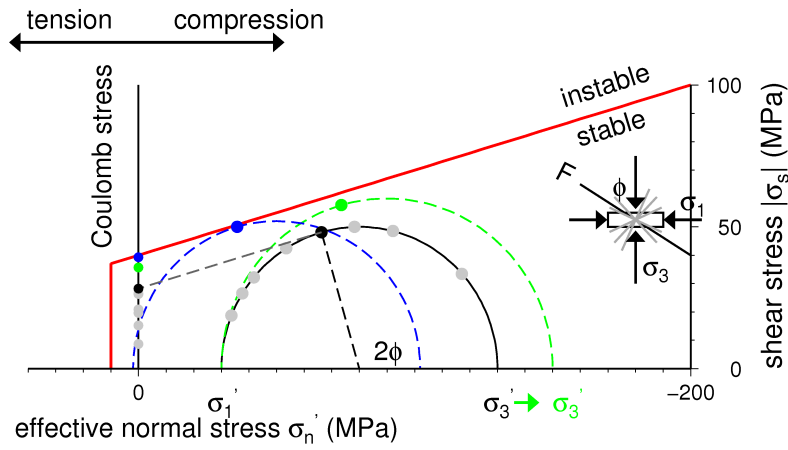


homogeneous effective media, homogeneous stress

(3) seismicity models

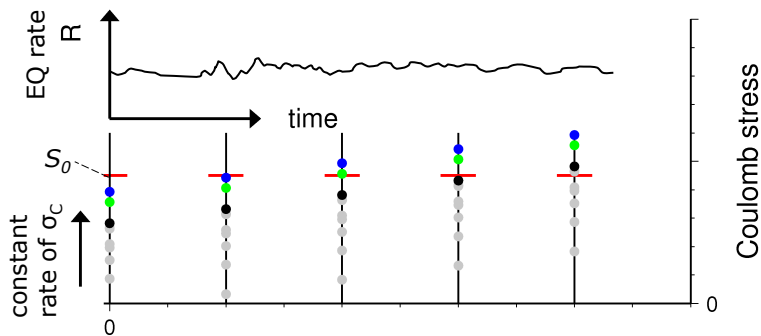


(3) seismicity models



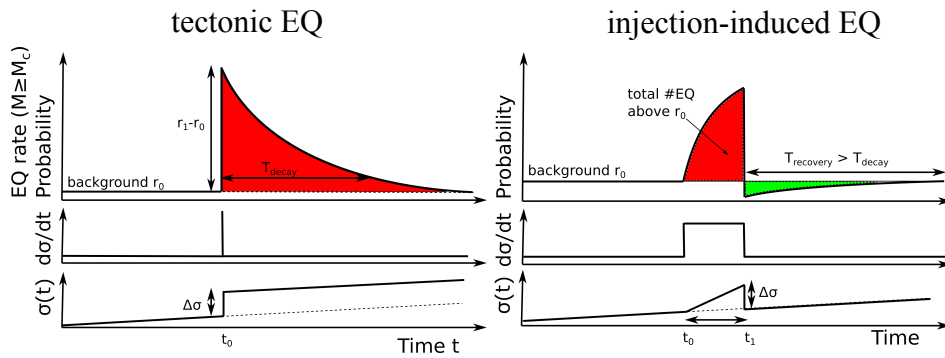
Earthquake rate R from constant stress loading rate

Note: R is the same as the a-value in GR relation (if $M=0$) or seismogenic index



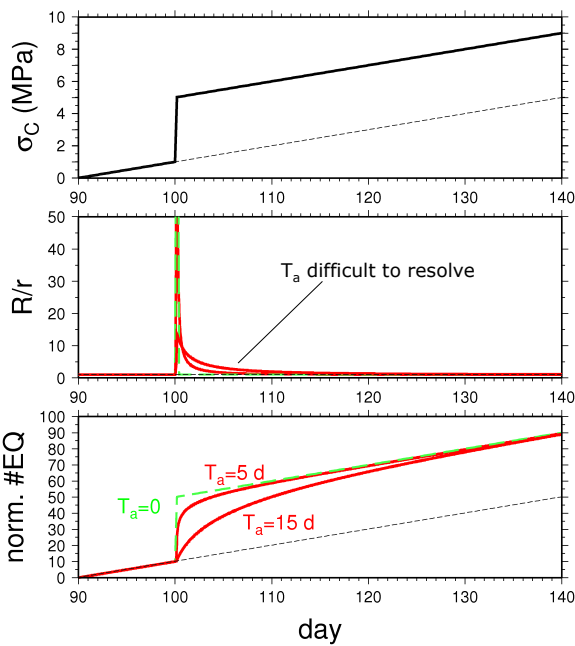
1. threshold model (Coulomb failure model, CFM, or Brownian Passage Time)
2. frictional nucleation phase model (e.g. rate and state, RSM)

EQ rate r in given rock volume experiences different stressing



- ✓ Both, stressing rate and steps (increase) lead to higher EQ rate
- ✓ Stress shadow from decreasing stress can have long memory
- ✓ Growing and propagating dikes involve positive and negative stress changes

Sudden pressure step loading (e.g. EQ aftershocks)



✓ positive ΔP

2nd parameter:
decay time T_a

transition depends T_a :

Rate & state model (RSM)

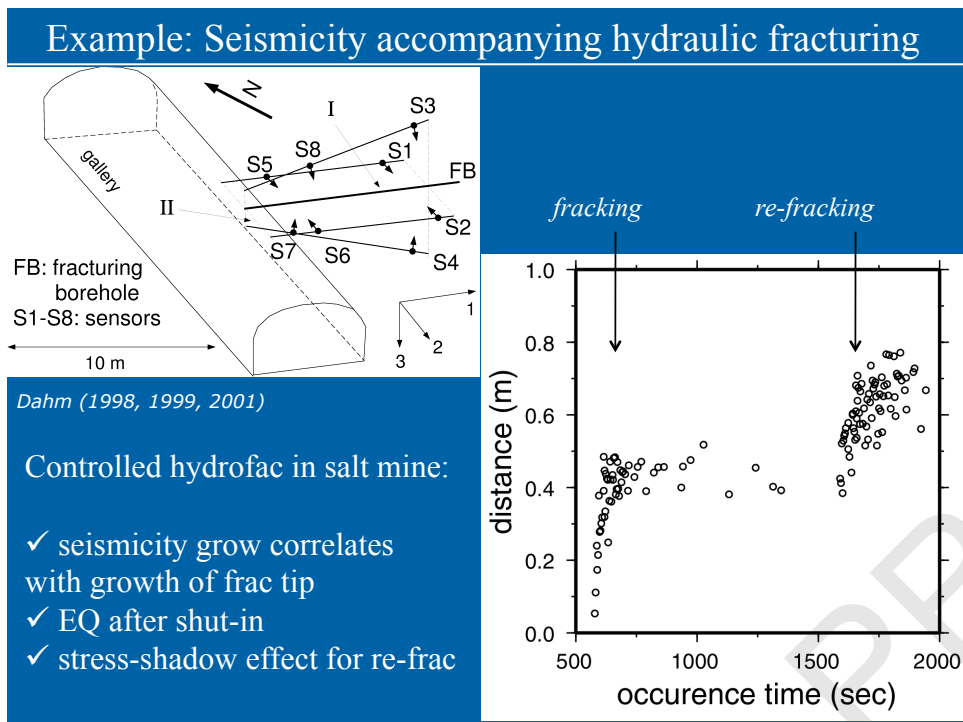
limiting case for $T_a=0$:

Coulomb failure model (CFM)

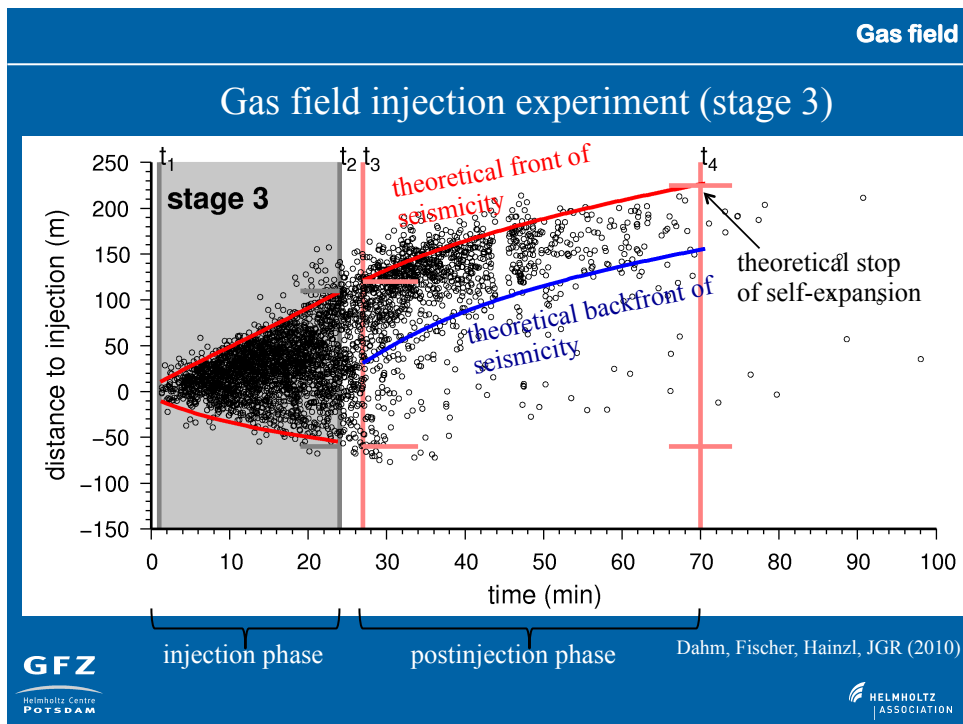
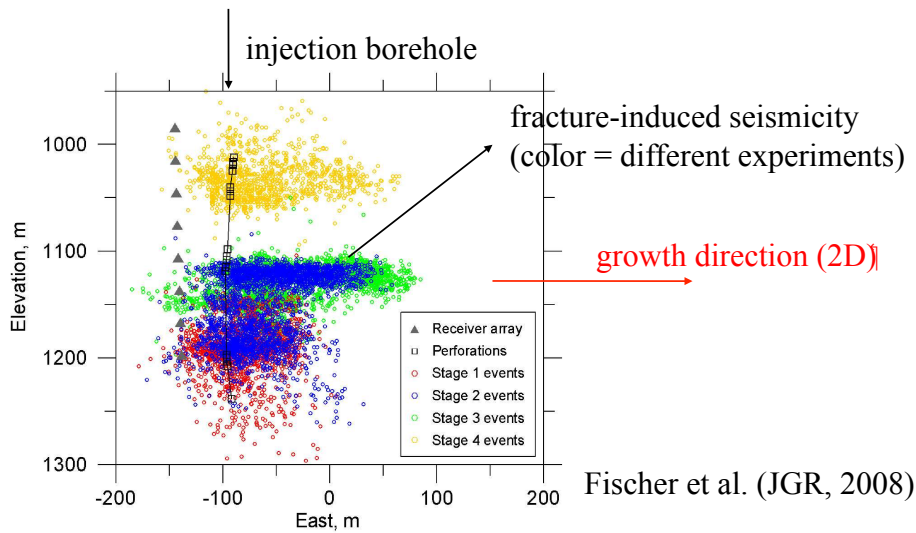
Total number constant:
short $T_a \rightarrow$ high peak
long $T_a \rightarrow$ small peak

III) Examples

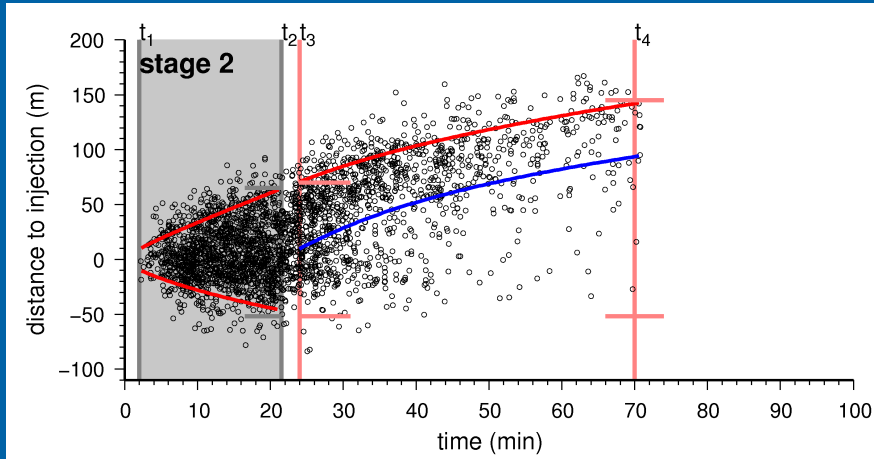
“Hydrofracture” induced seismicity



Hydrofrac stimulations in Canyonsand gas field, W. Texas

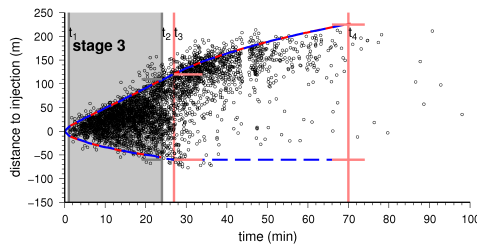


Gas field injection experiment (stage 2)



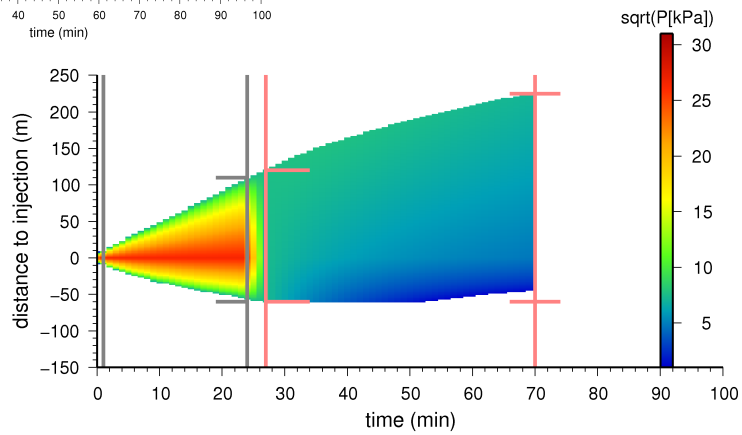
Dahm, Fischer, Hainzl, JGR (2010)

Modeling stress changes



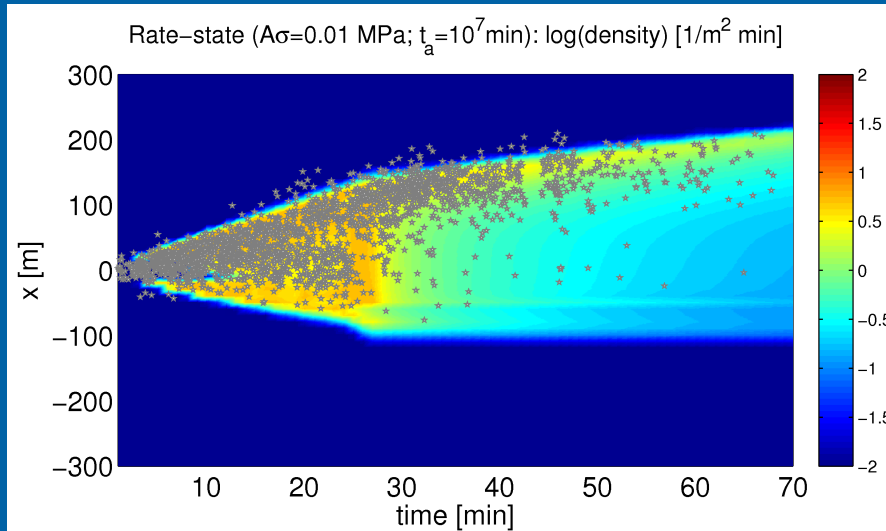
hydrofrac length

internal
effective
pressure



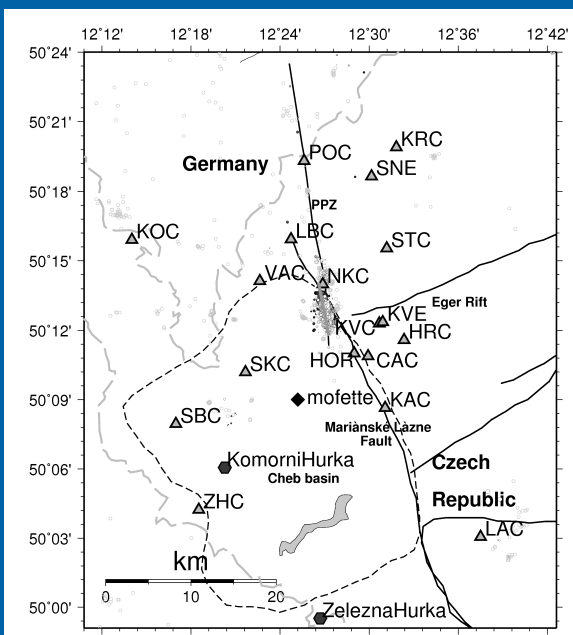
stage 3 : rate and state, low $A\sigma$, long decay

stress model



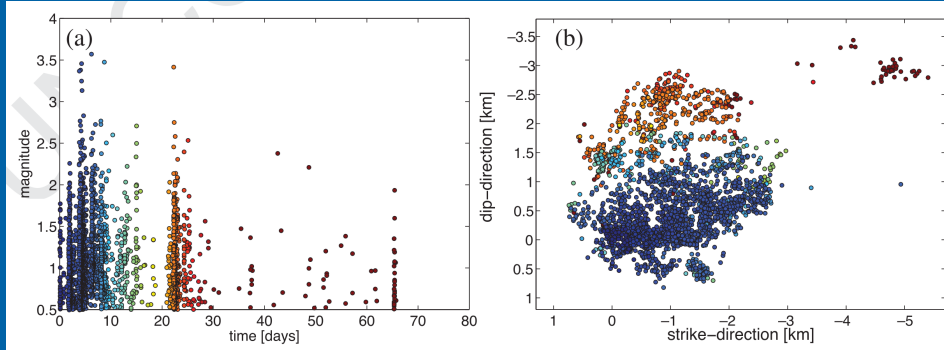
$P_0 \approx 0.7$ MPa
 $dP/dx \approx 14 P_0/\text{km}$, $K_c \approx 1$ MPa $\sqrt{\text{km}}$
 $T_{\text{inject}} \approx 0.4$ h, $l_{\text{inject}} \approx 0.18$ km

Mid-crustal earthquake swarms (NW Bohemia)

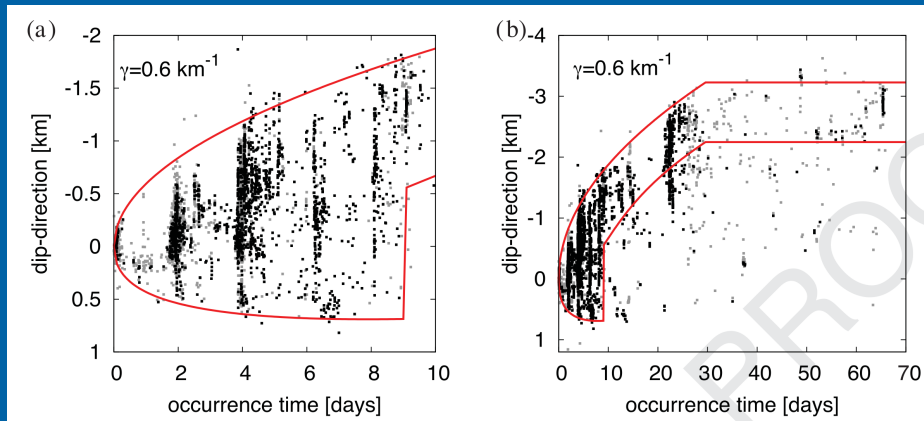


Hainzl et al., GJI, 2012

NW Bohemia 2008 swarm



NW Bohemia 2008 swarm

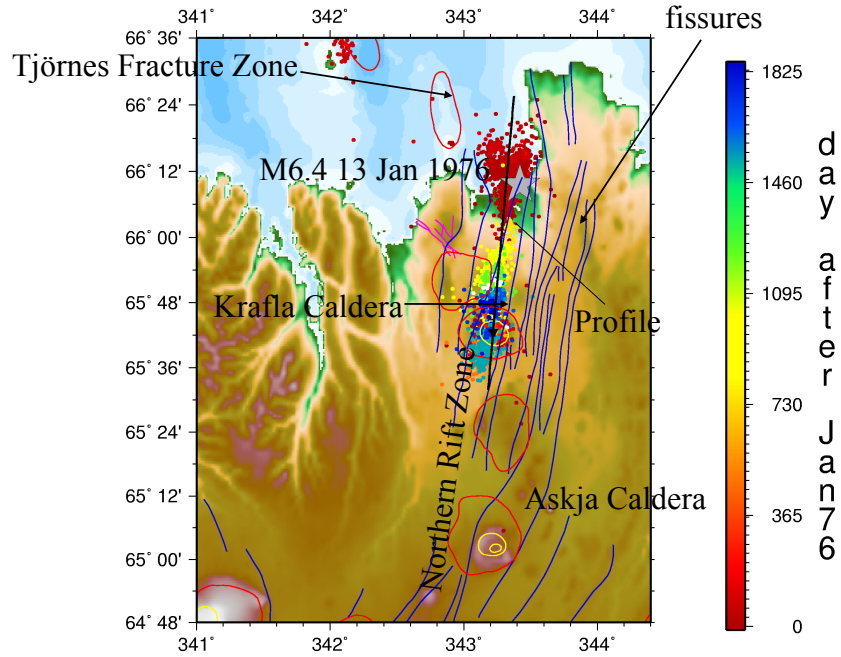


$\Delta P \approx 15 \text{ MPa}$ (water) or 25 MPa (gas)

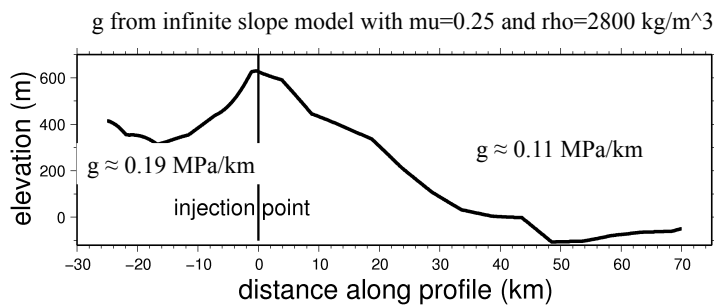
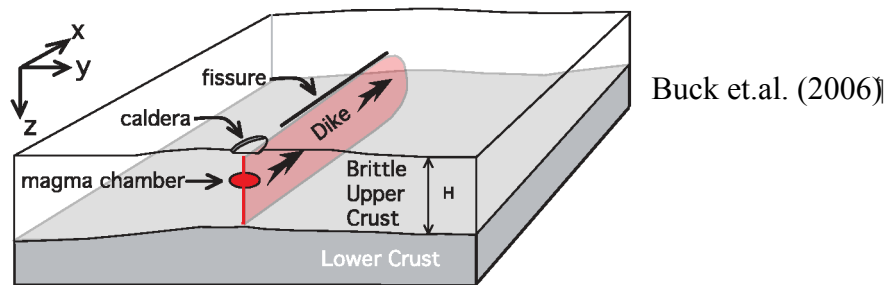
$dP/dx \approx 0.6 P_0/\text{km}$

$T_{\text{inject}} \approx 9\text{h}$, $l_{\text{inject}} \approx 2.4 \text{ km}$

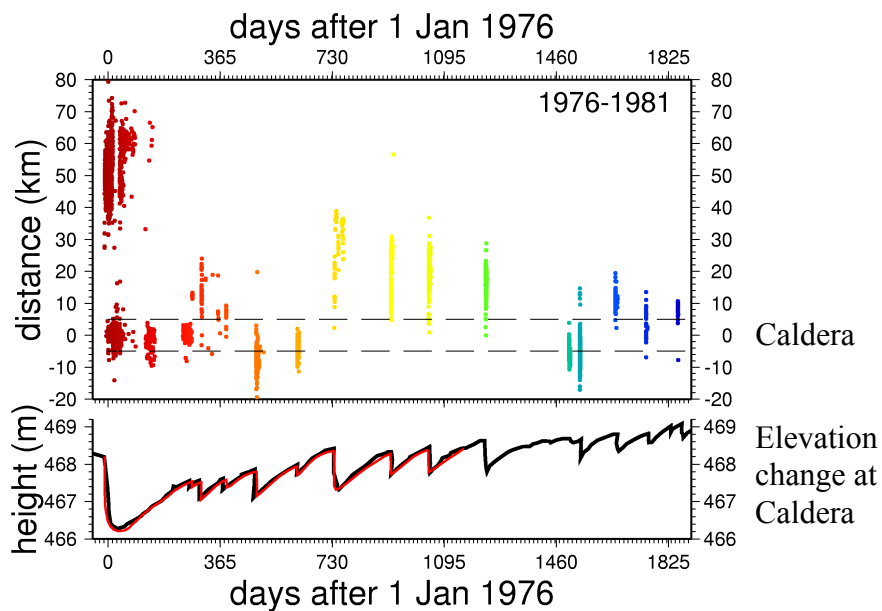
Seismicity during the Krafla rifting events Dec75 - Jan81



Rifting at Krafla: topography may control stress gradients

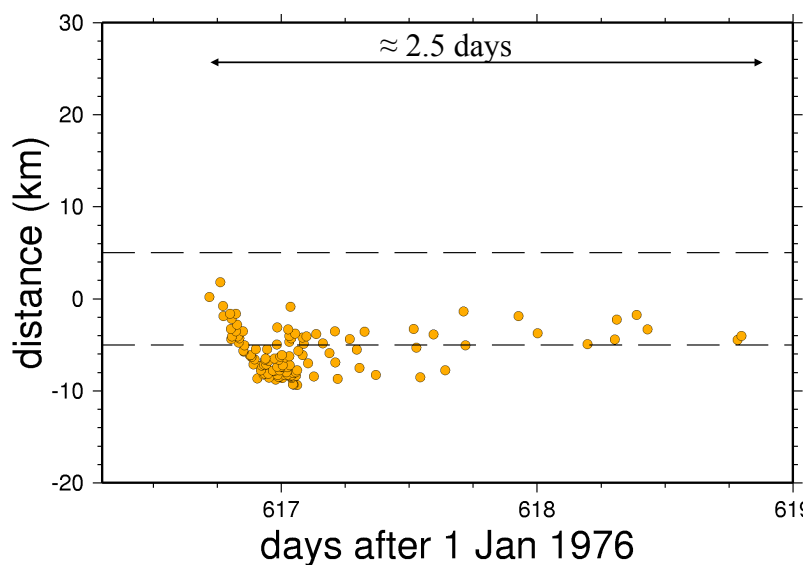


Along strike seismicity and caldera deflation

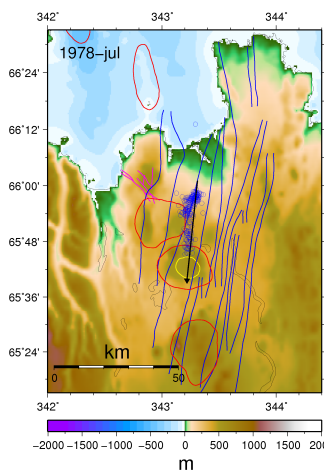
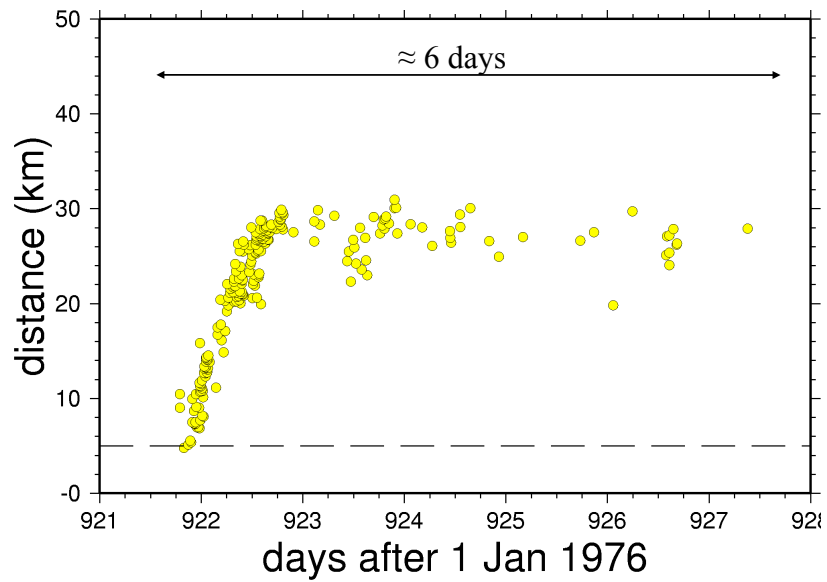


see Einarsson, 1991, Buck et al., 2006 and references therein

induced seismicity: Sep 77 intrusion



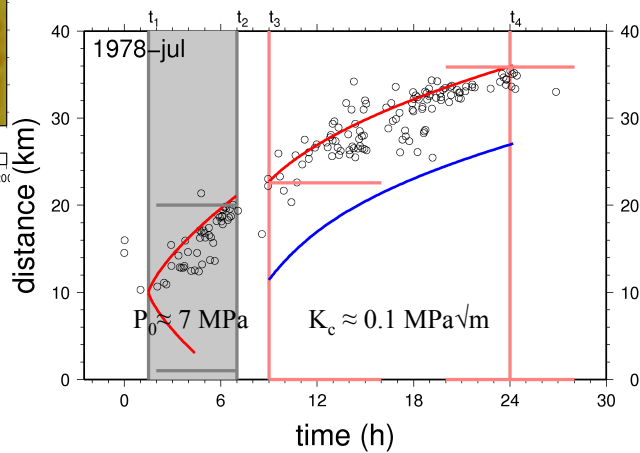
induced seismicity: Jul 78 intrusion



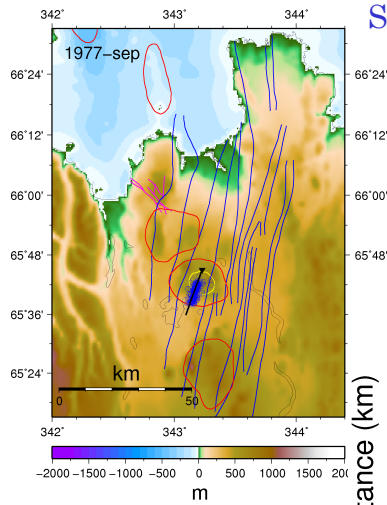
July 1978 intrusion northward

- self-expansion starts after 9 h
- injection controlled length is 19-22 km
- final length is 34 km
- gap after 7 h: re-organisation of flow

assuming $g \approx 0.11$ MPa/km
 $\eta \approx 20$ Pa s

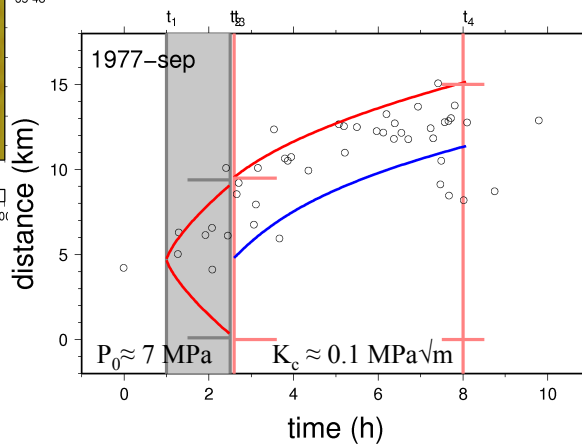


Sep 1977 intrusion southward



- self-expansion starts after 2.5 h
- injection controlled length ≈ 10 km
- final length is ≈ 15 km

assuming $g \approx 0.19$ MPa/km
 $\eta \approx 20$ Pa s



What can be learned from intrusion-induced seismicity?

- Retrieve the geometry and dynamics of the intrusion (duration of injection, overpressure, viscosity?, ...)
- Estimate the fracture properties of the medium (e.g. K_c)
- Estimate the stress direction and state of stress
- Estimate the permeability of the medium