



Thermal Lens Spectrometry and Microscopy

Analytical Chemist's Approach

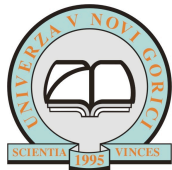
Mladen Franko

University of Nova Gorica

WINTER COLLEGE ON OPTICS:

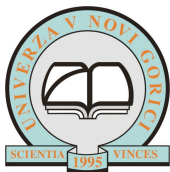
Advanced Optical Techniques for Bio-imaging

ICTP, Trieste: February 13th -24th, 2017



Requirements for analytical methods in bio-chemical analysis

- Sensitivity
- Selectivity
- Cost efficiency
- High sample throughput
 - Conventional (certified, rearguard) analytical methods are labour intensive, time consuming and costly
 - **quick** answers and analysis of **large numbers** of samples (and large number of compounds - screening) for **low cost – vanguard methods** (frequently semi-quantitative or just binary YES/NO response)

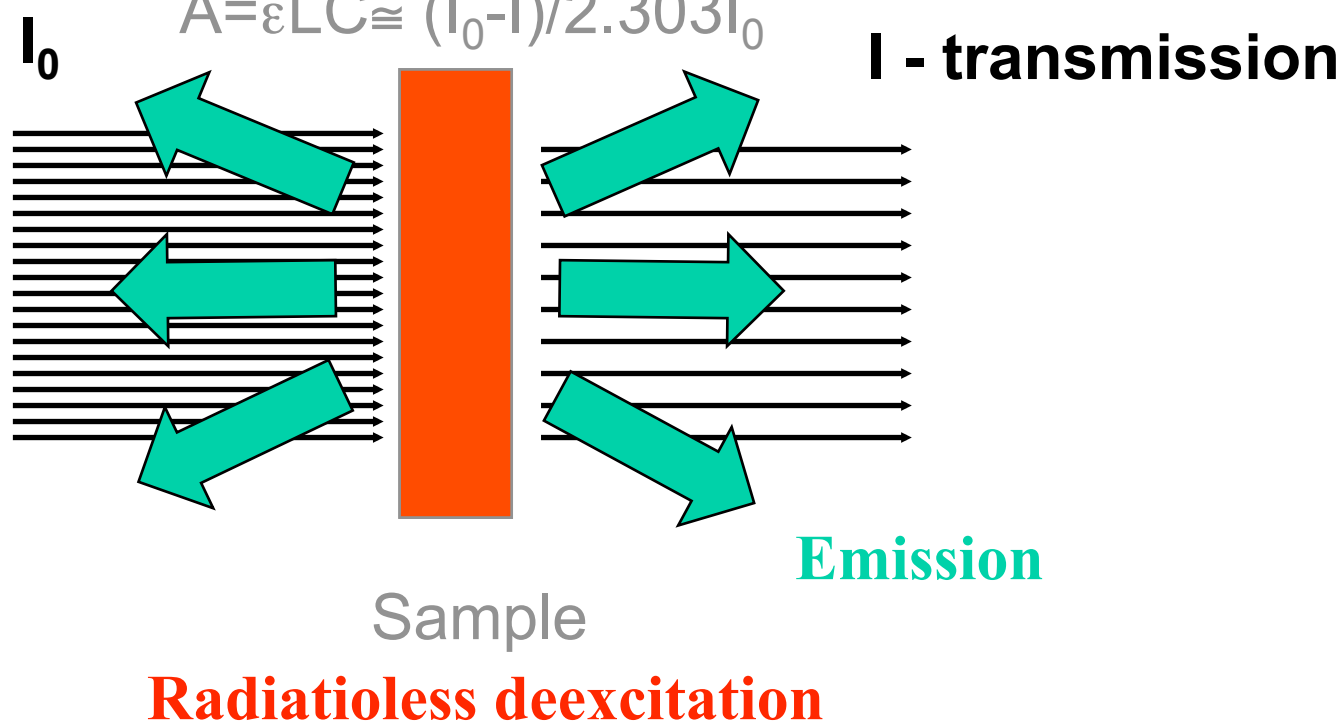


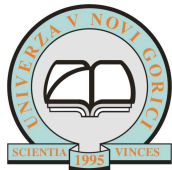
Transmission techniques - how to improve sensitivity?

$$A = -\log T = -\log(I/I_0)$$

for low absorbances:

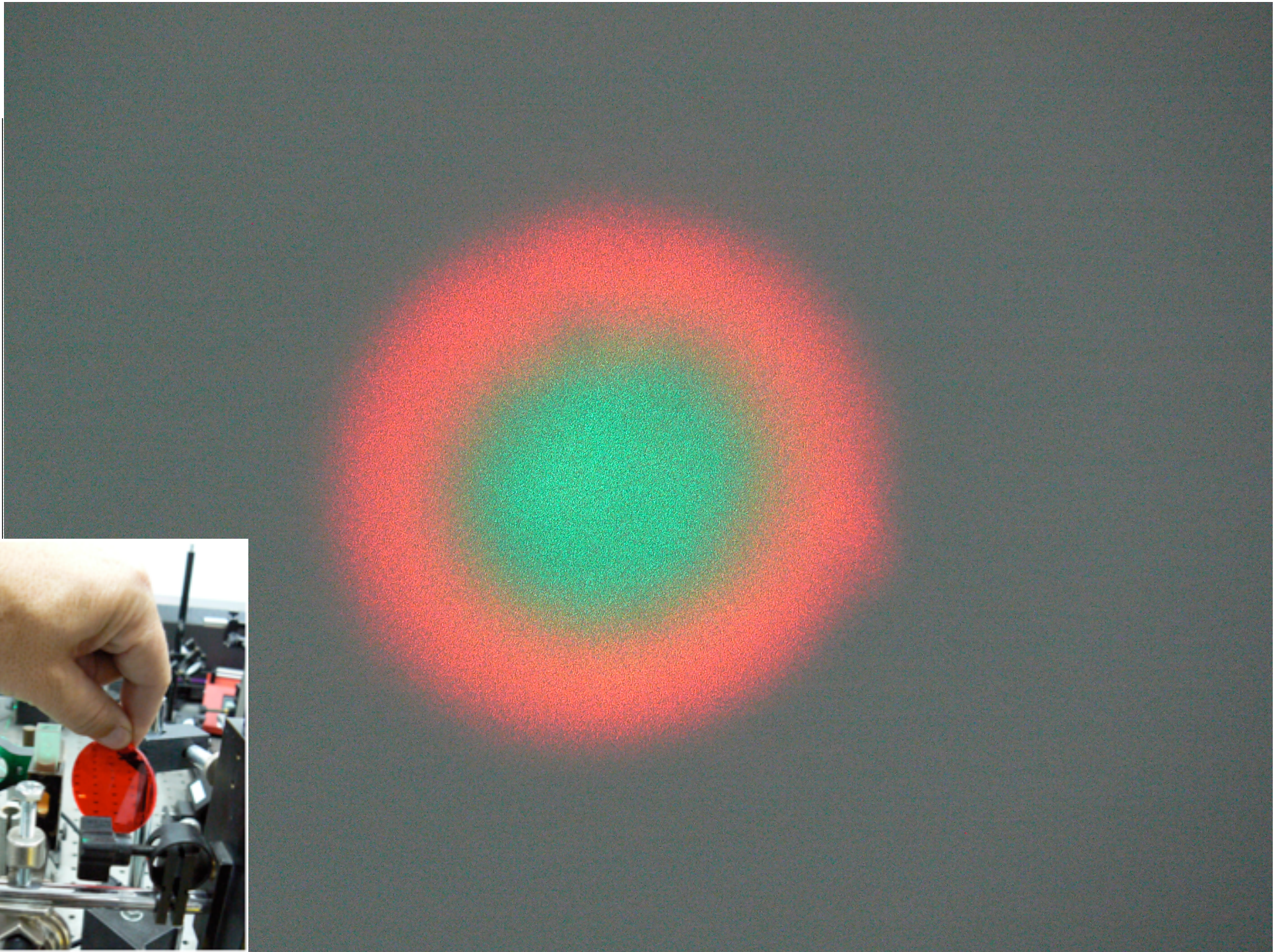
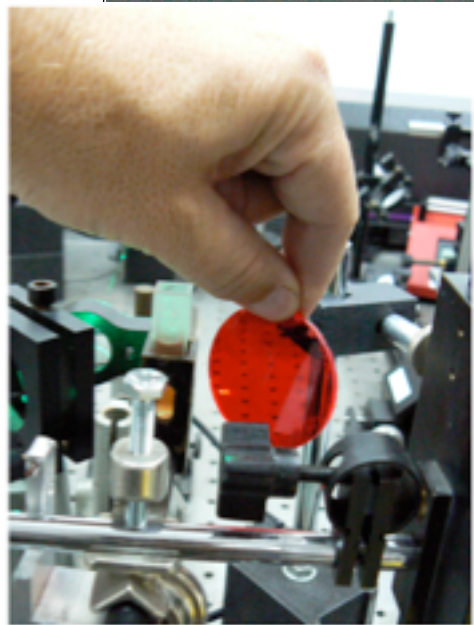
$$A = \varepsilon LC \approx (I_0 - I) / 2.303 I_0$$

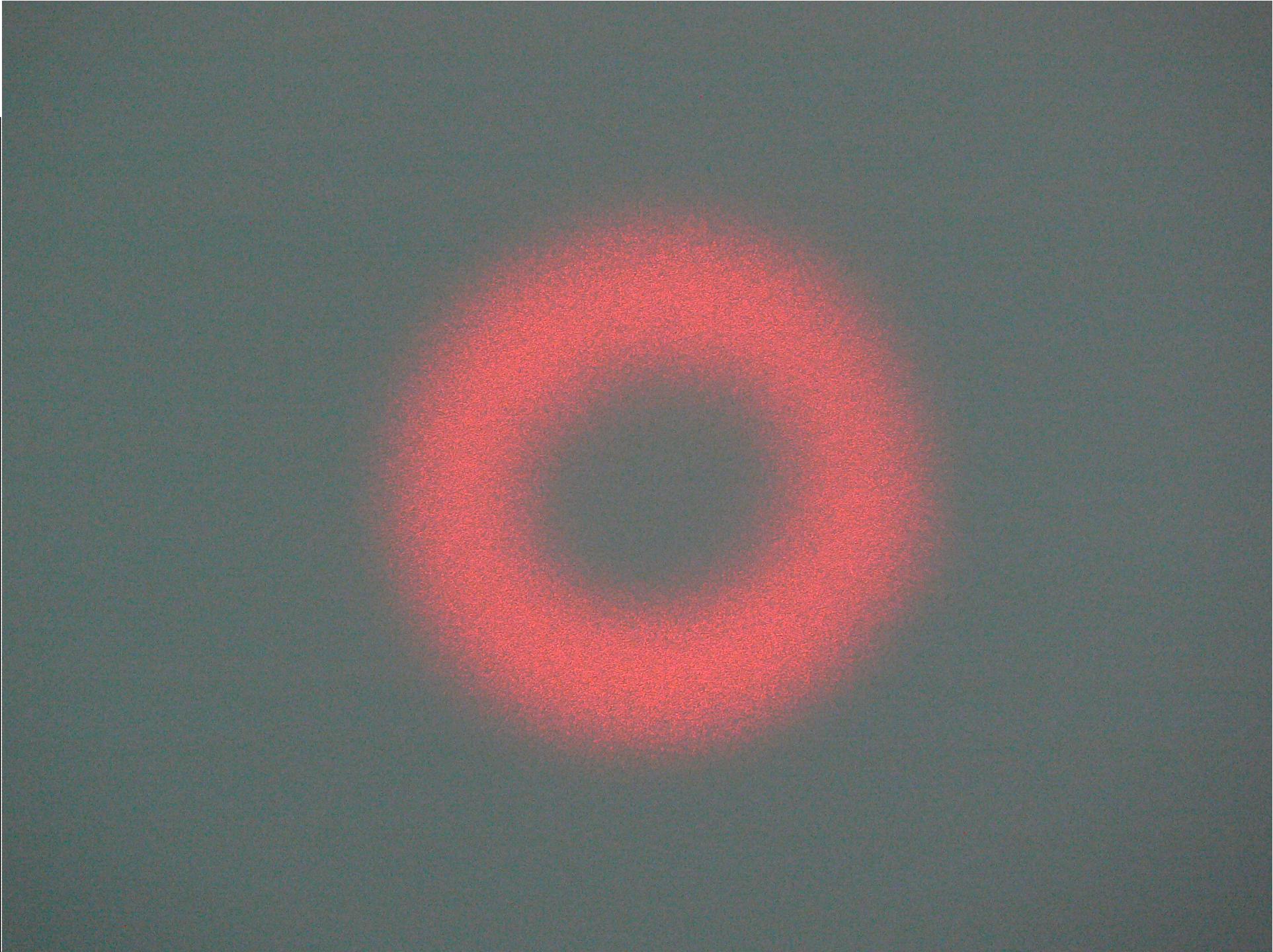


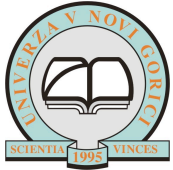


Basics of thermal lens effect

- During non-radiative relaxation of excited species temperature in the sample increases (10^{-4} - 10^{-3} K)
- a temperature gradient is generated with maximum temperature at the axis of the excitation beam
- the resulting refractive index gradient acts as a lens (mostly: $dn/dT < 0$, diverging lens)
- laser beam is defocused (single beam or pump/probe (collinear, crossed beam) configuration)
- beam radius and its intensity at the beam axis changes
- relative change in the beam intensity is proportional to the absorbance of the sample and to the power of the excitation beam.

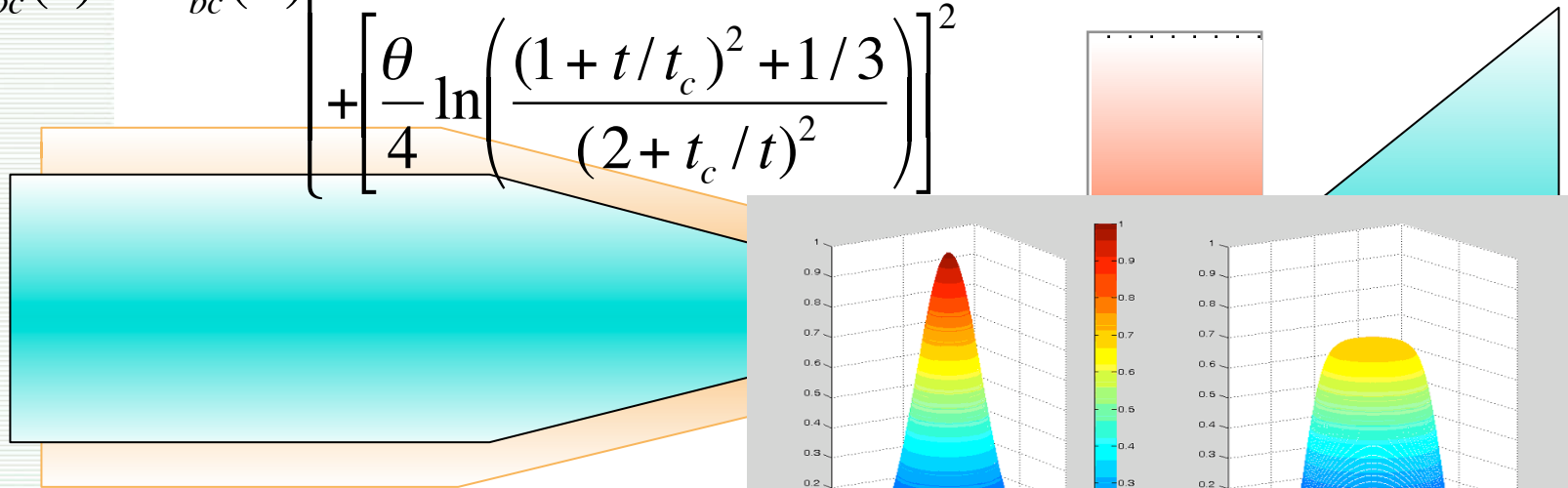






TLS – how to make good use of something not desired in laser technology?

$$I_{bc}(t) = I_{bc}(0) \left\{ 1 - \theta \tan^{-1} \left(\frac{1}{(1 + t_c/t)\sqrt{3}} \right) + \left[\frac{\theta}{2} \tan^{-1} \left(\frac{1}{(1 + t_c/t)\sqrt{3}} \right) \right]^2 + \left[\frac{\theta}{4} \ln \left(\frac{(1 + t/t_c)^2 + 1/3}{(2 + t_c/t)^2} \right) \right]^2 \right\}$$

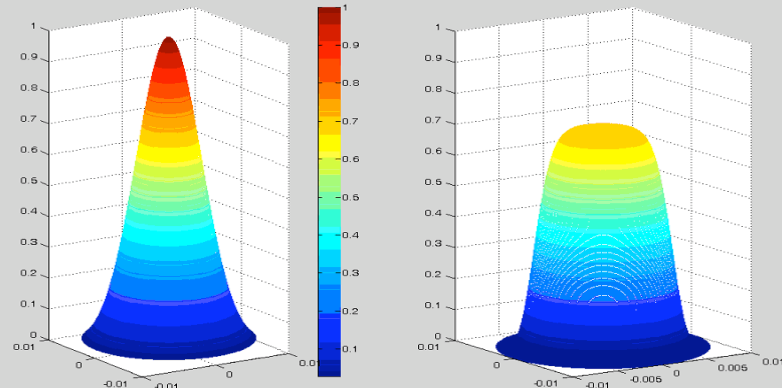


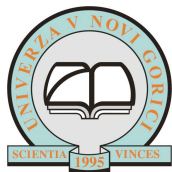
Signal = $\Delta I/I$

$$t_c = \frac{a^2 \rho C_P}{4k}$$

$$\theta = \frac{2.303AP(-dn/dT)}{\lambda k}$$

SAMPLE





TLS - advantages

- High sensitivity
 - signal proportional to excitation laser power
 - absorbances as low as 10^{-7} can be measured
- Enables On-line detection
 - fast response of TLS signal (on μs to ms time scale)
- Capability of measuring small samples
 - sub-pL volumes can be probed
 - detection in microfluidic systems



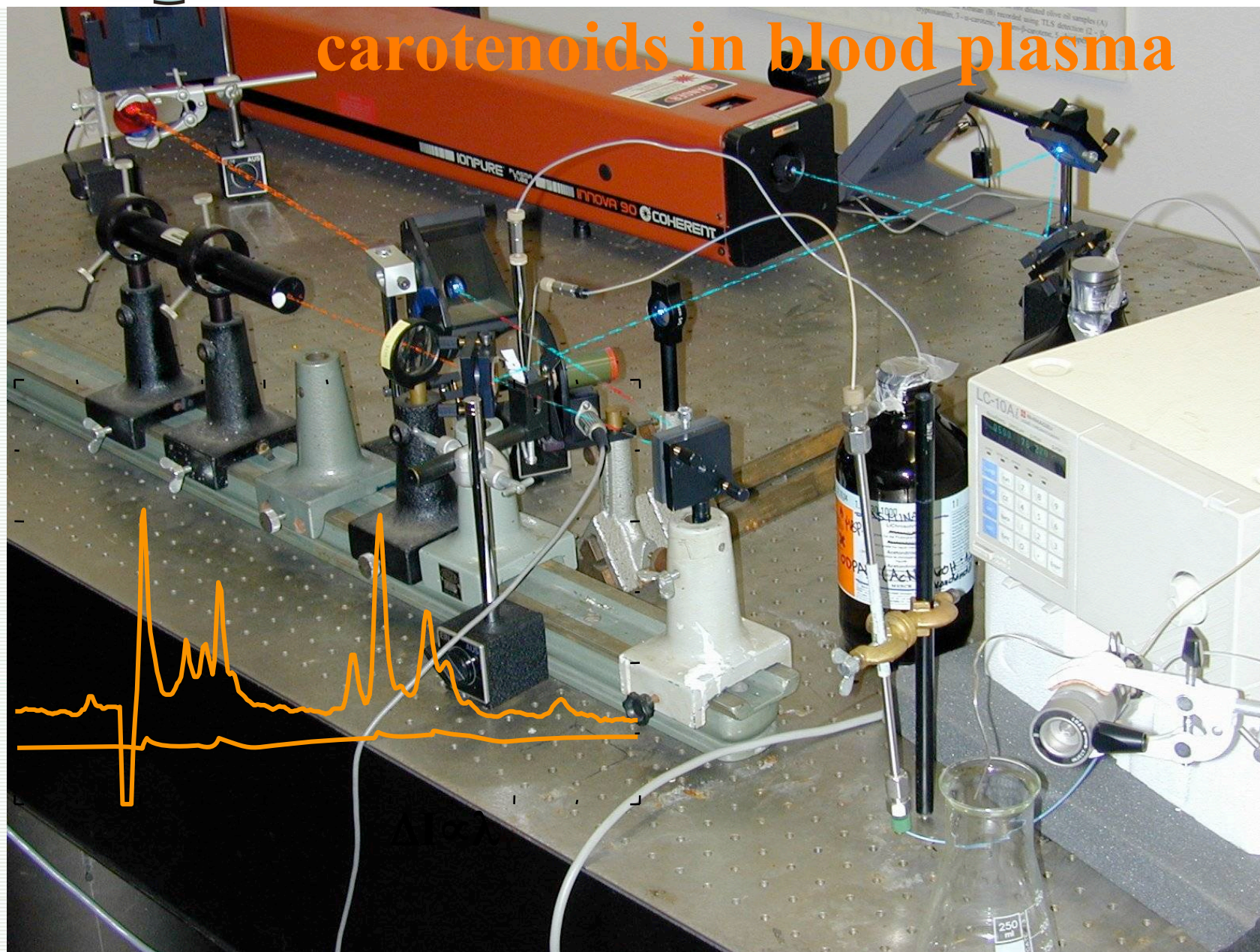
TLS – drawbacks and solutions

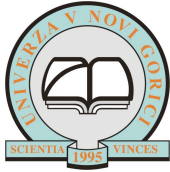
- Sensitivity still needs improvement
 - Higher laser power? (photo-labile compounds)
 - Modify solvents
- Limited availability of laser sources
 - Coloring reactions, indirect detection
- Poor selectivity
 - Single wavelength measurements
 - Coupling to separation techniques (HPLC, IC, CE)
- Photodegradation
 - Measure in flowing systems



HPLC-TLS degtermination of carotenoids in blood plasma

carotenoids in blood plasma



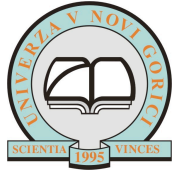


Nonsteady thermal diffusion

$$\frac{\partial T(r, t)}{\partial t} = D \nabla^2 T(r, t) - v_x \frac{\partial T(r, t)}{\partial x} + \frac{1}{\rho C_p} Q(r, t)$$

- $T(r, t)$ temperature
- Dthermal diffusivity
- ρ Density
- C_pheat capacity
- $Q(r, t)$source term (“heat”)
- v_xvelocity of the medium in x direction

By solving nonsteady the thermal diffusion equation, changes in refractive index and related TLS signal can be calculated for different beam geometries and excitation regimes (pulsed, cw)



Pulsed and cw excitation with a Gaussian beam

Assuming complete conversion of absorbed energy into heat, source terms are:

- Pulsed:

$$Q(r, t) = \frac{2\alpha E_0}{\pi a^2 t_0} \exp\left[-2(x^2 + y^2)/a^2\right]$$

- cw:

$$Q(r, t) = \frac{2\alpha P_{av}}{\pi a^2} \left\{ \exp\left[-2(x^2 + y^2)/a^2\right] \right\} \times (1 + \cos \omega t)$$

E_0 pulse energy

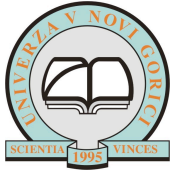
apump laser beam radius

t_0 pulse width

P_{av} ...cw laser average power

αabsorbance (cm^{-1})

ωmodulation frequency²

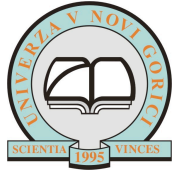


Thermal lens signal

$$s(t) = \frac{w_2^2(t) - w_2^2(0)}{w_2^2(0)}$$

- $w_2(0)$radius of an unperturbed probe beam at the detector site
- $w_2(t)$time dependent radius of a probe beam perturbed by the thermal lens
- w_0radius of the probe beam at its waist

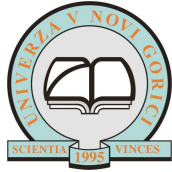
$$w_2^2(t) = w_0^2 \left[\left(1 - \frac{z_2}{f(t)} \right)^2 + \frac{1}{z_0^2} \left(z_1 + z_2 - \frac{z_1 z_2}{f(t)} \right)^2 \right]$$



Simplifications for usual far field experimental configuration

- $z_2 \gg z_1, z_2 \gg z_0 = \pi w_0^2 / \lambda$
- $f(t) \gg z_1, f(t) \gg z_0$
- @ $t = 0, f(0) = \infty$
 - λ, w_0 probe beam wavelength and waist
 - z_0confocal distance
 - z_1 probe beam waist to sample distance
 - z_2 sample-to-detector distance

$$s(t) = -\frac{2z_1}{f(t)}$$



Refractive index change and focal distance of thermal lens

$$n(x, y, t) = n_0 + \left(\frac{\partial n}{\partial T} \right)_{T_A} \times T(x, y, t)$$

- n_0 unperturbed refractive index at ambient temperature T_A

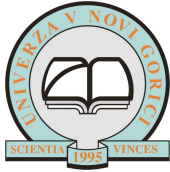
collinear:

$$\frac{1}{f} = -\frac{\partial n}{\partial T} \ell \left(\frac{\partial^2 T}{\partial r^2} \right)$$

transversal:

$$\frac{1}{f} = -\frac{\partial n}{\partial T} \int_{-\infty}^{\infty} \left(\frac{\partial^2 T}{\partial x^2} \right) dy$$

- fthermal lens focal length
- ℓinteraction length



TLS signal for collinear configuration

- Pulsed: ($t_0 \rightarrow 0$)

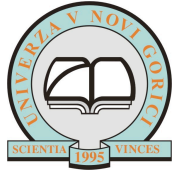
$$s(t) = - \frac{4AE_0 z_1 (\partial n / \partial T)}{\pi k a^2 t_c} \frac{1}{(1 + 2t / t_c)^2}$$

- CW:

$$s(t) = - \frac{2APz_1 (\partial n / \partial T)}{\pi k a^2} \frac{1}{(1 + t_c / 2t)}$$

$$A = \alpha \ell$$

- t_ctime constant = $a^2 \rho c_p / 4k = 4a^2 D$
- kthermal conductivity of the sample



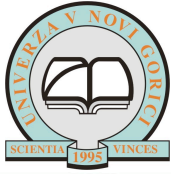
TLS signal for transversal configuration

- Pulsed: ($t_0 \rightarrow 0$)

$$s(t) = -\frac{2\alpha E_0 z_1 (\partial n / \partial T)}{\sqrt{2\pi k a t_c}} \frac{1}{(1 + 2t / t_c)^{3/2}}$$

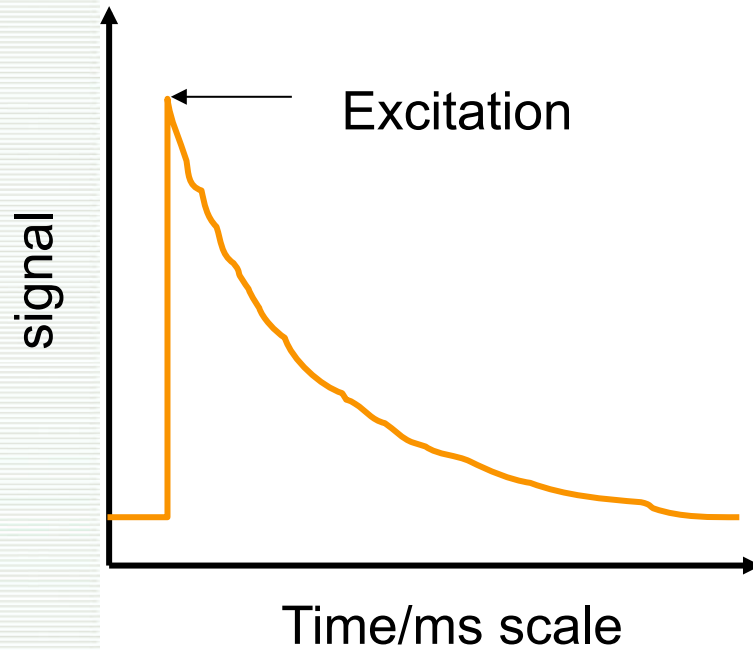
- CW:

$$s(t) = -\frac{2\alpha P z_1 (\partial n / \partial T)}{\sqrt{2\pi k a}} \frac{1}{(1 + t_c / 2t)^{1/2}}$$

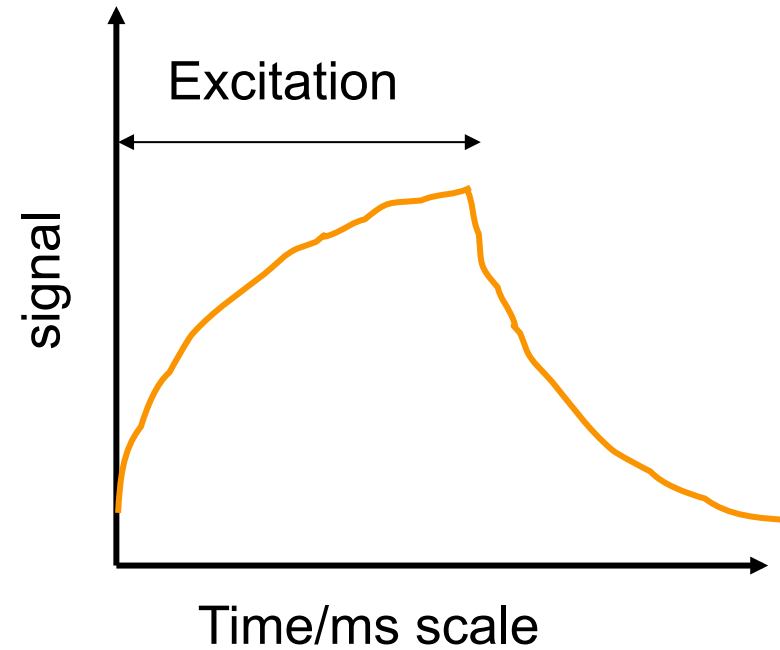


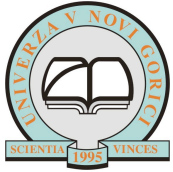
TLS signal form

Pulsed



CW



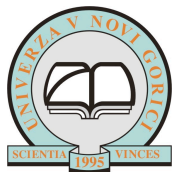


E - Enhancement factor in TLS

$$\frac{\Delta I}{I} = \frac{2.303P \left(-dn/dT \right) A}{\lambda k} \arctg\left(1/\sqrt{3}\right) = 2.303EA$$

Solvent	$-dn/dT$ (10^4 K^{-1})	k ($\text{W m}^{-1}\text{K}^{-1}$)	E (10^{-3} W^{-1})
H ₂ O	0.91	0.607	0.12
CCl ₄	5.9	0.103	4.74
acetone	5.42	0.190	2.36

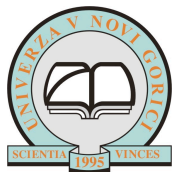
$E = (-dn/dT) / (1.91 \lambda k)$ is calculated for $\lambda = 632.8 \text{ nm}$



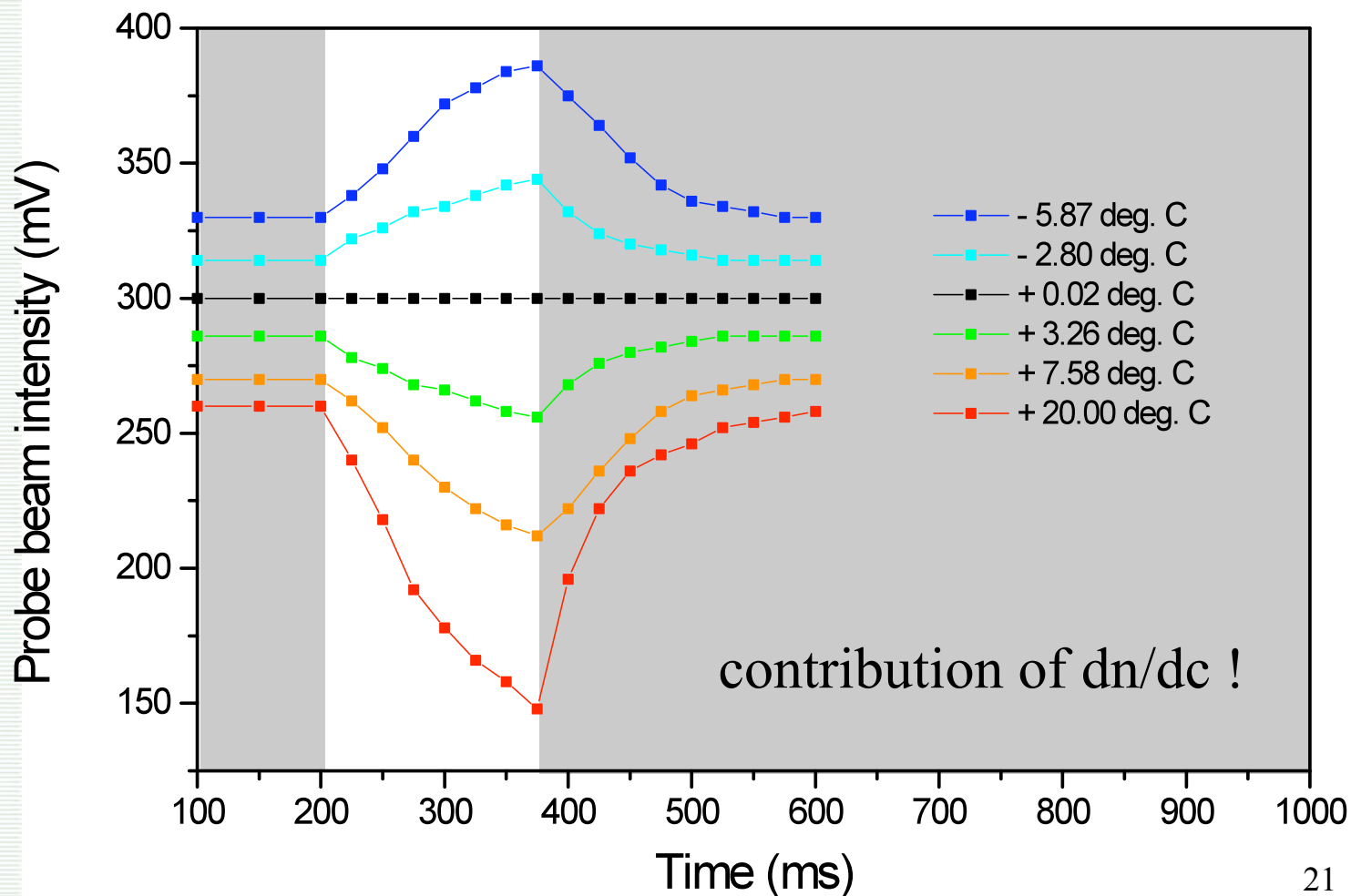
Thermo-optical properties of solvents for TLS measurements

Solvent	Thermal conductivity, k $\text{mWcm}^{-1}\text{K}^{-1}$	$10^4(\text{dn}/\text{dT})$ K^{-1}	$-\frac{10^4(\text{dn}/\text{dT})}{k}$ cm mW^{-1}
CO ₂ (sc)	0.7	-100	143
CCl ₄	1.03	-5.9	5.73
Benzene	1.24	-6.4	5.16
C ₈ MImTf ₂ N	n.d.	n.d.	4.55
cyclohexane	1.24	-5.4	4.35
BMImBF ₄	1.78	-7.54	4.24
n-heptane	1.26	-5.0	3.97
BMImTf ₂ N	1.06	-4.0	3.78
dioxane	1.39	-4.6	3.31
EMImTf ₂ N	n.d.	n.d.	2.37
methanol	2.20	-4.7	2.14
water	6.11	-0.8	0.13

Calc. values (except CO₂) taken from Chieu D. Tran and T. A. Van Fleet, Anal. Chem. 60, (1988) 2478

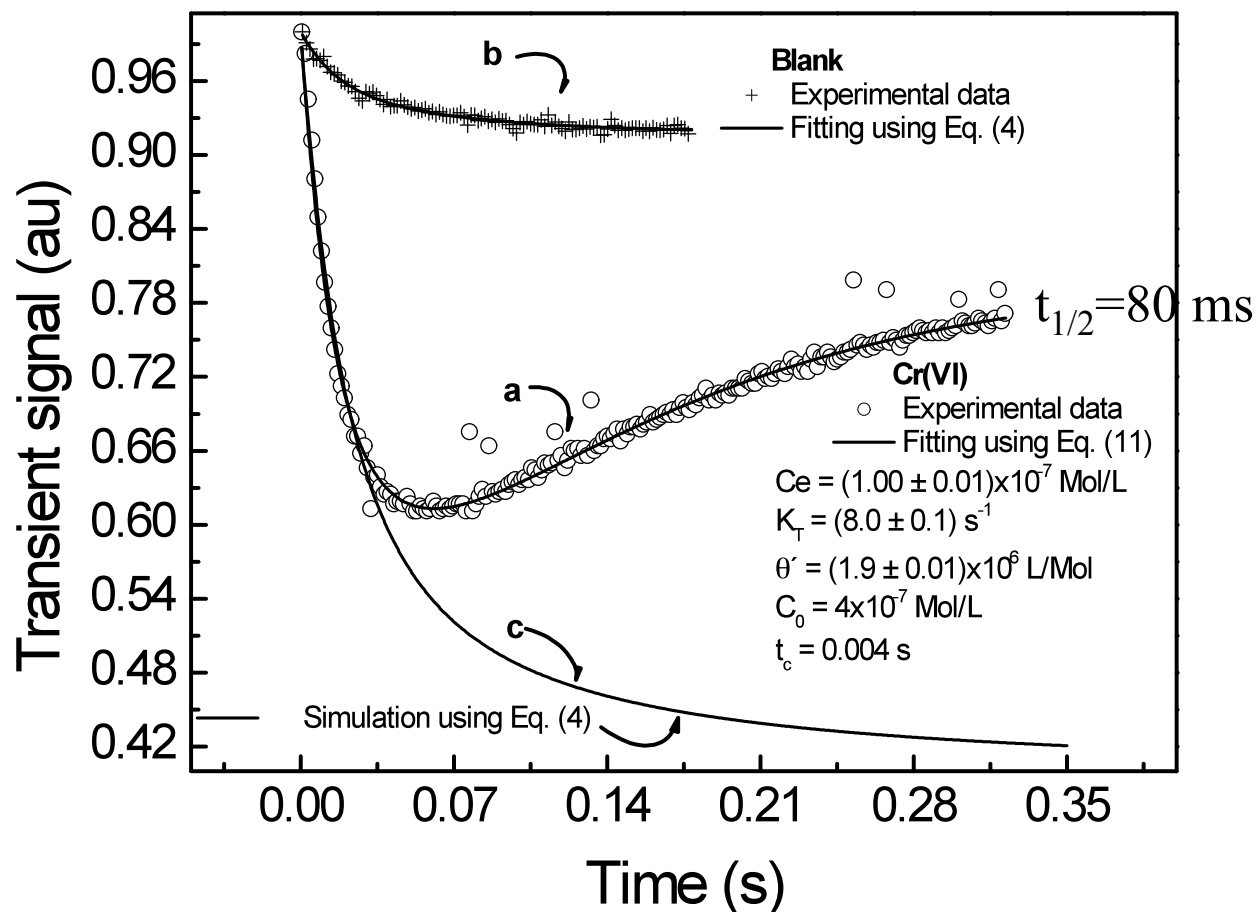


Temperature dependent TLS signal in water



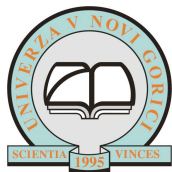


The effect of photosensitivity on TLS signal (case of Cr-DPC)

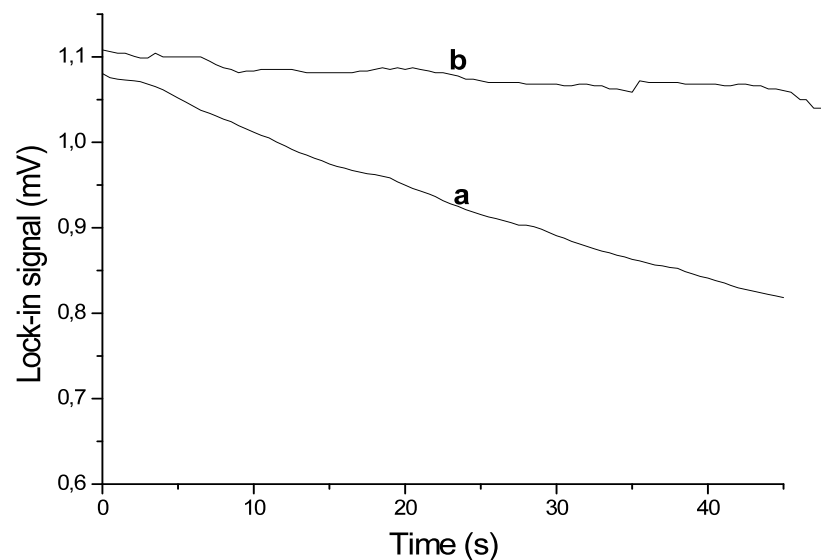
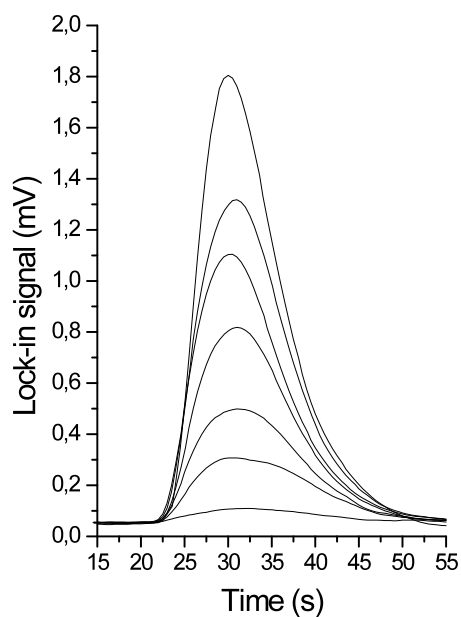


$$I_{bc}(t) = I_{bc}(0) \left[1 - \frac{\theta' [(C_0 - C_e) \exp(-(k_r + k_D)t) + C_e]}{2} \tan^{-1} \left(\frac{1}{(1 + t_c/t)\sqrt{3}} \right) \right]^2$$

Pedreira et al.: J. Appl. Phys., **100** (2006)
Chem. Phys. Lett. **396**(2004)221

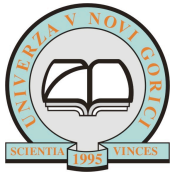


Degradation of photolabile analytes

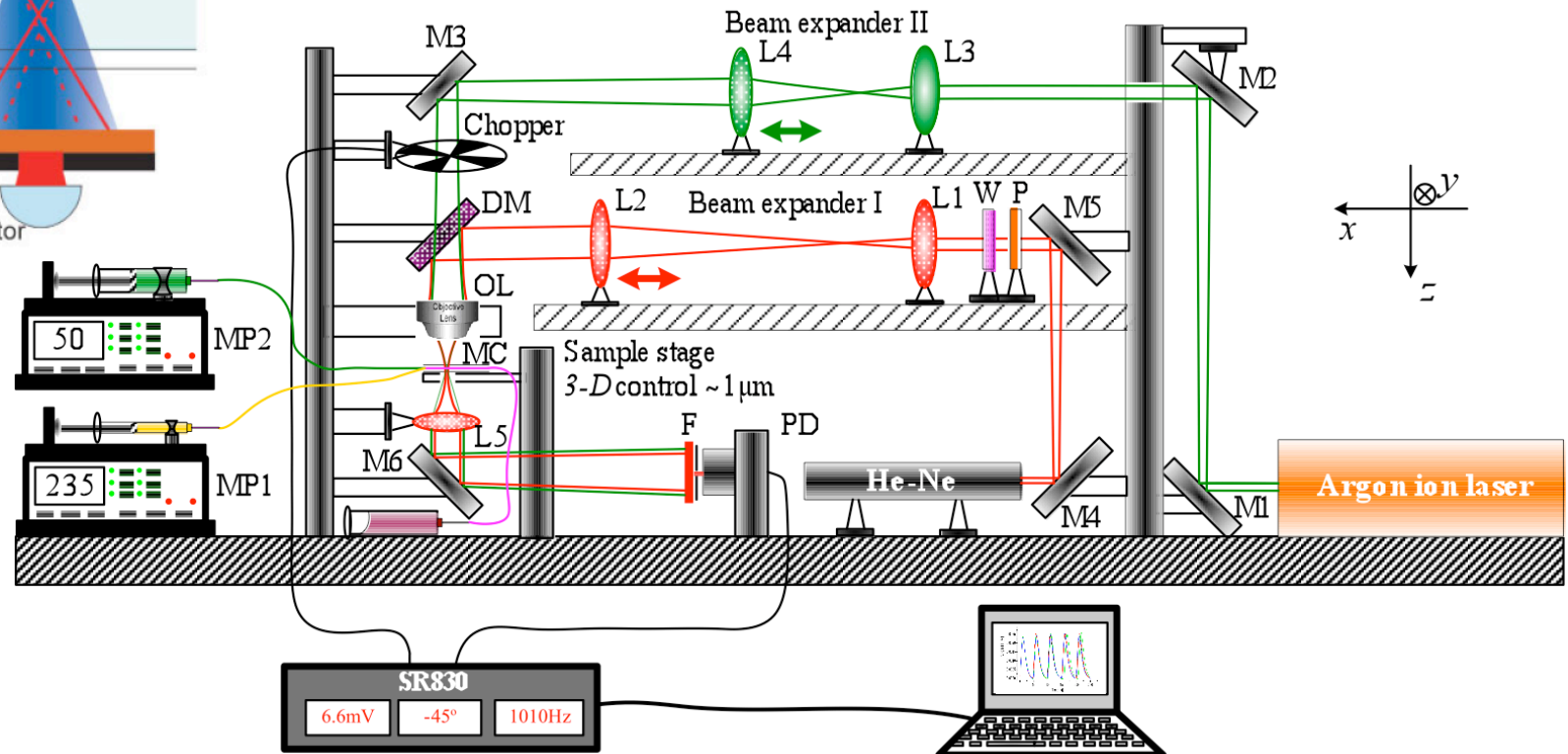
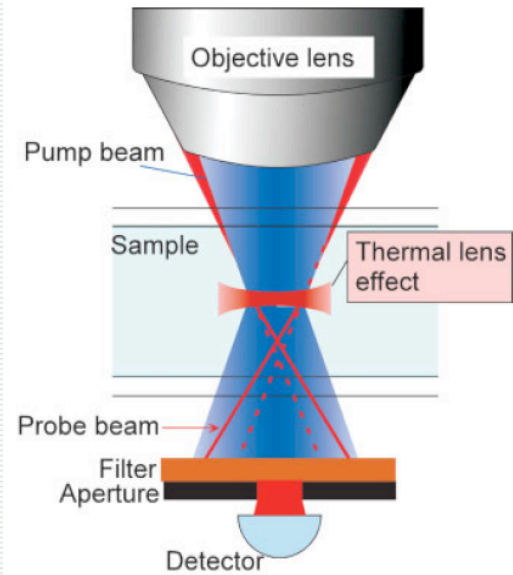


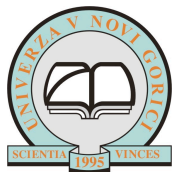
A. Madžgalj, M.L. Baesso, M. Franko, Eur. Phys. J. Special Topics **153** (2008) 503

Cr(VI) ($\mu\text{g/L}$)	1	3	9	15	20
Mean sig./mV (n = 5)	0.201	0.481	1.227	1.968	2.83
S.D.	0.005	0.005	0.015	0.010	0.014
R.S.D. (%)	2.52	0.95	1.23	0.49	0.48
LOD ($\mu\text{g/L}$)	0.065				23

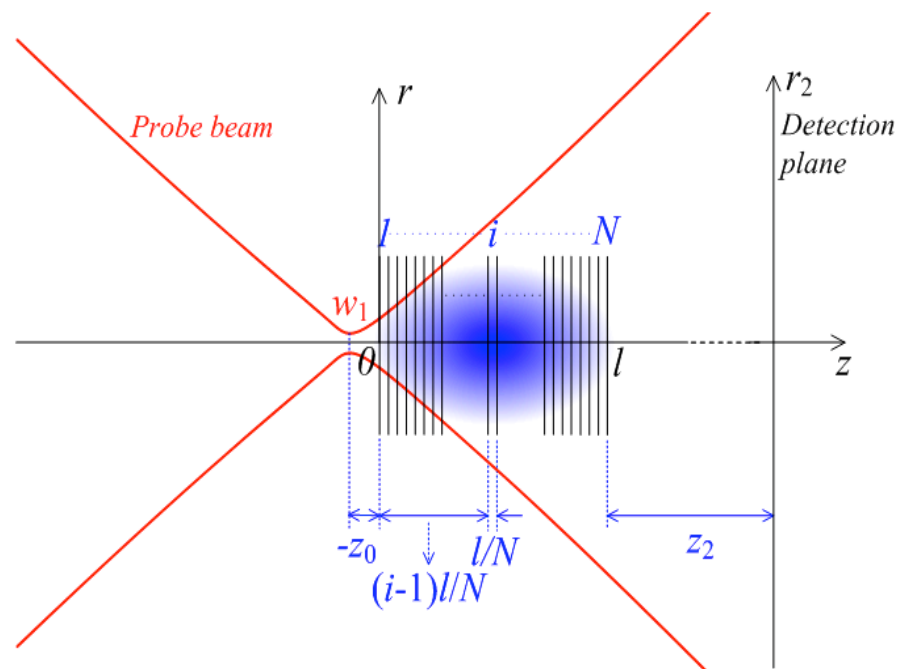


Adjustable beam size/position TLM



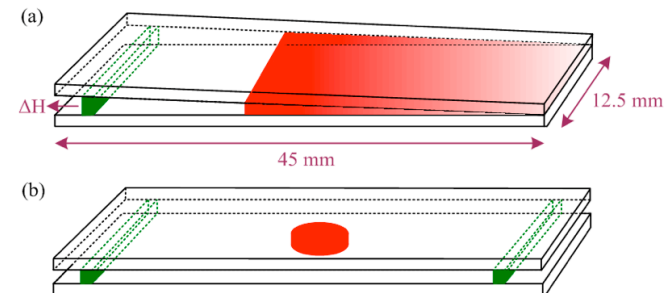
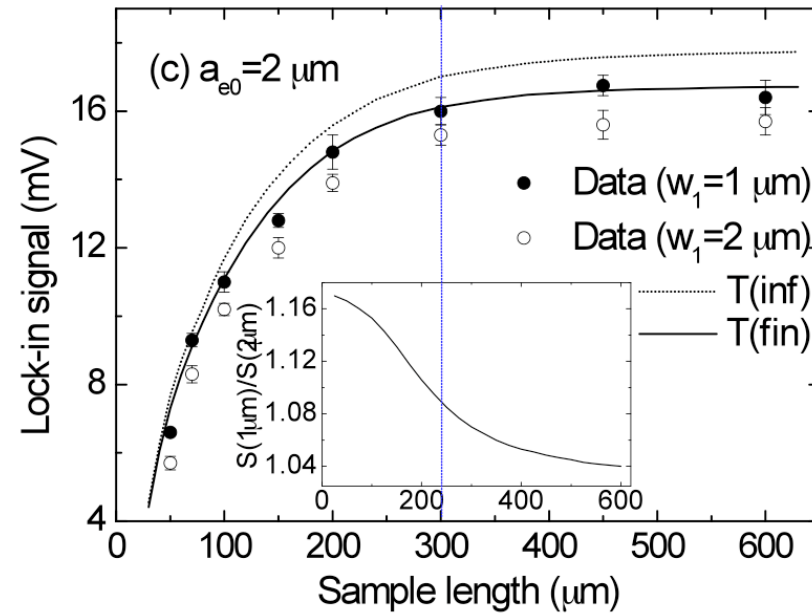
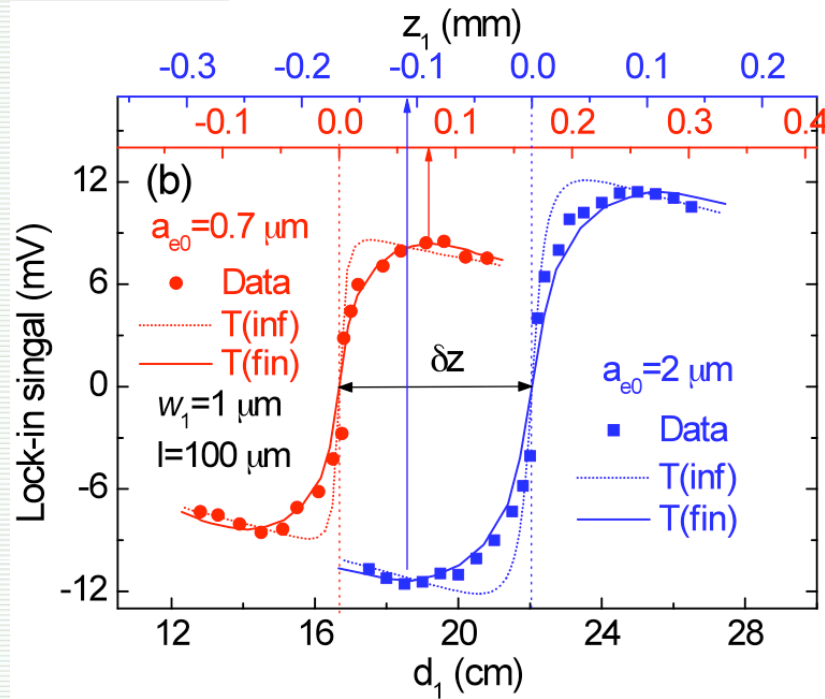


New theoretical model of thermal lens in TLM



$$S_{tl} = \sum_{i=1}^N \frac{|E_2(r_2, z_1(i) + z_2, t = n/f + 1/(2f))|^2 - |E_2(r_2, z_1(i) + z_2, t = n/f)|^2}{|E_2(r_2, z_1(i) + z_2, t = 0)|^2}$$

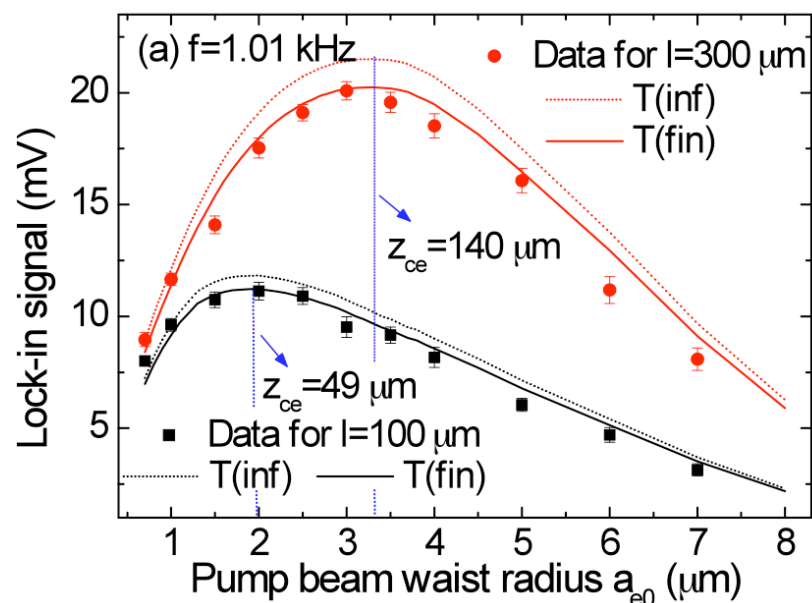
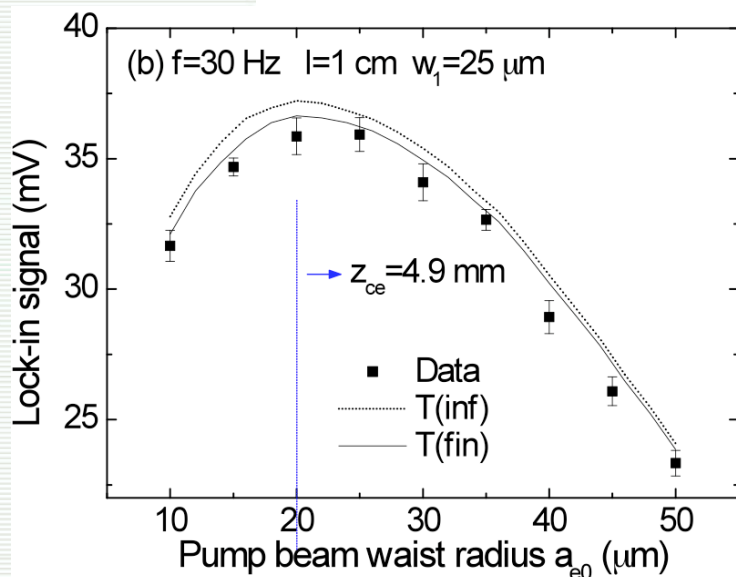
Effective sample length





Optimization of pump beam radius and power density

With 1/10 or 1/20 power density of that at the diffraction limit, 1.36 times higher ($l=100\mu\text{m}$) or 2.3 times higher ($l=300\mu\text{m}$) TL signal is obtained at the optimum optical configuration – **important for photosensitive compounds!**

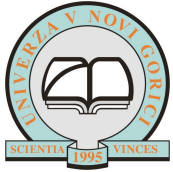


For
sample
length
 l

Optimal pump beam radius: $a_{e0} = \sqrt{\frac{\lambda_e l}{4\pi}}$

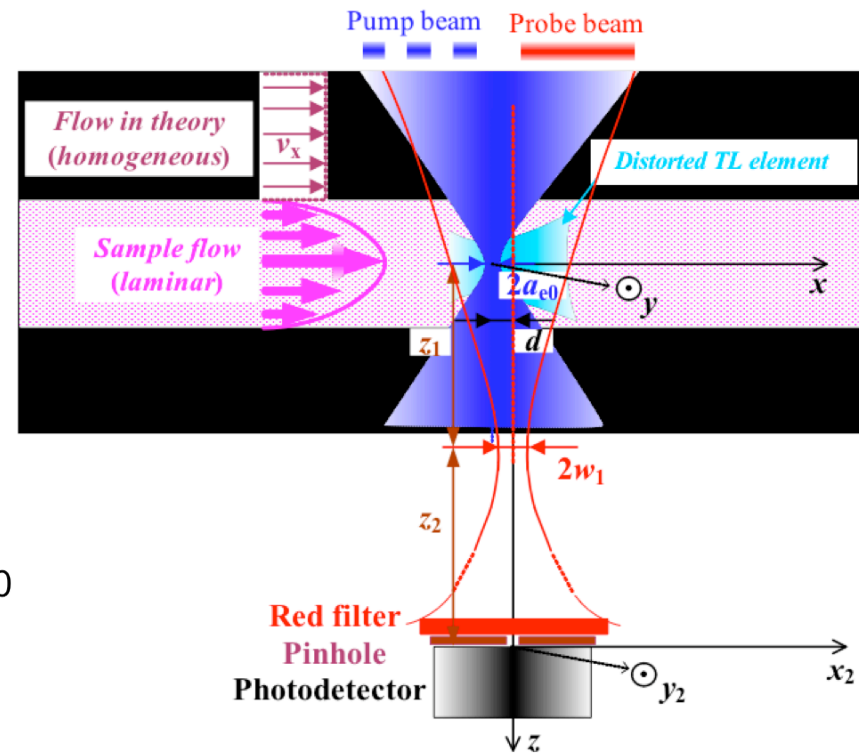
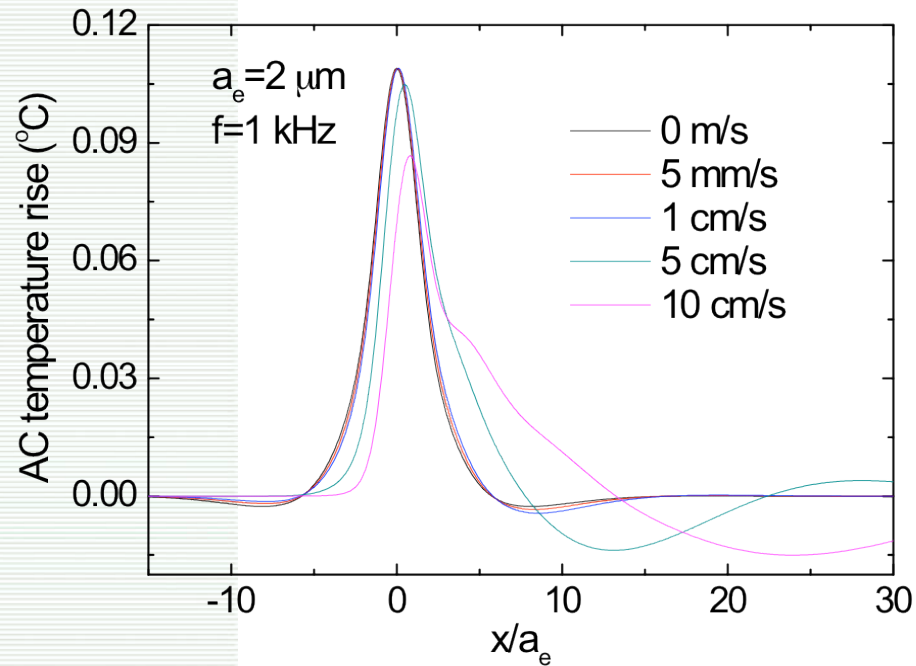
Optimal probe beam waist:

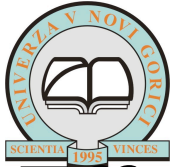
if $l < z_{ce}$, $w_1 = 0.5a_{e0} \sim a_{e0}$;
 otherwise $w_1 = 0.7a_{e0} \sim a_{e0}$



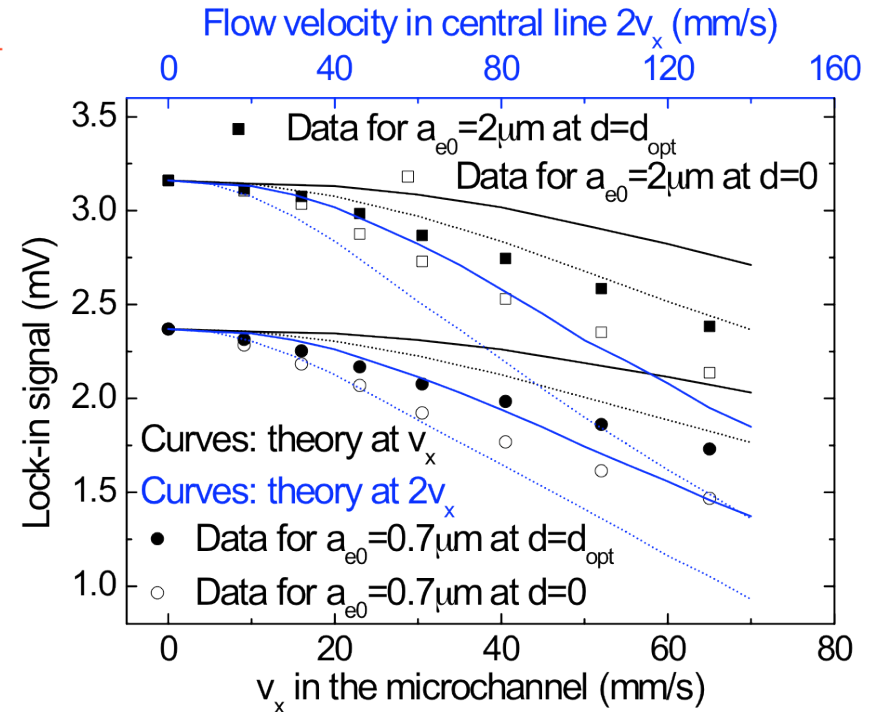
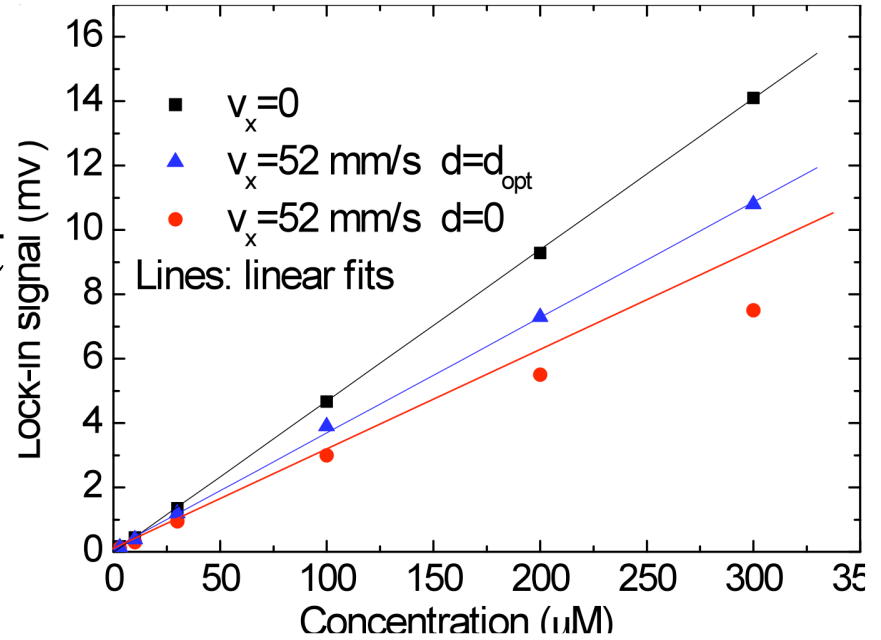
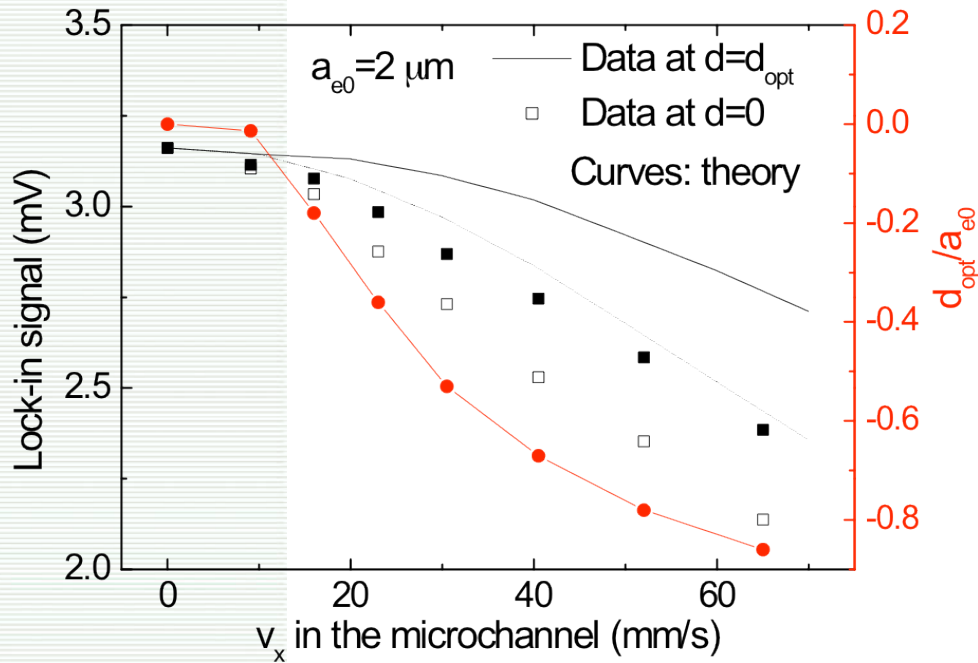
Effect of sample flow on TLM signal

$$\frac{\partial T(r,t)}{\partial t} = D\nabla^2 T(r,t) - v_x \frac{\partial T(r,t)}{\partial x} + \frac{1}{\rho C_p} Q(r,t)$$



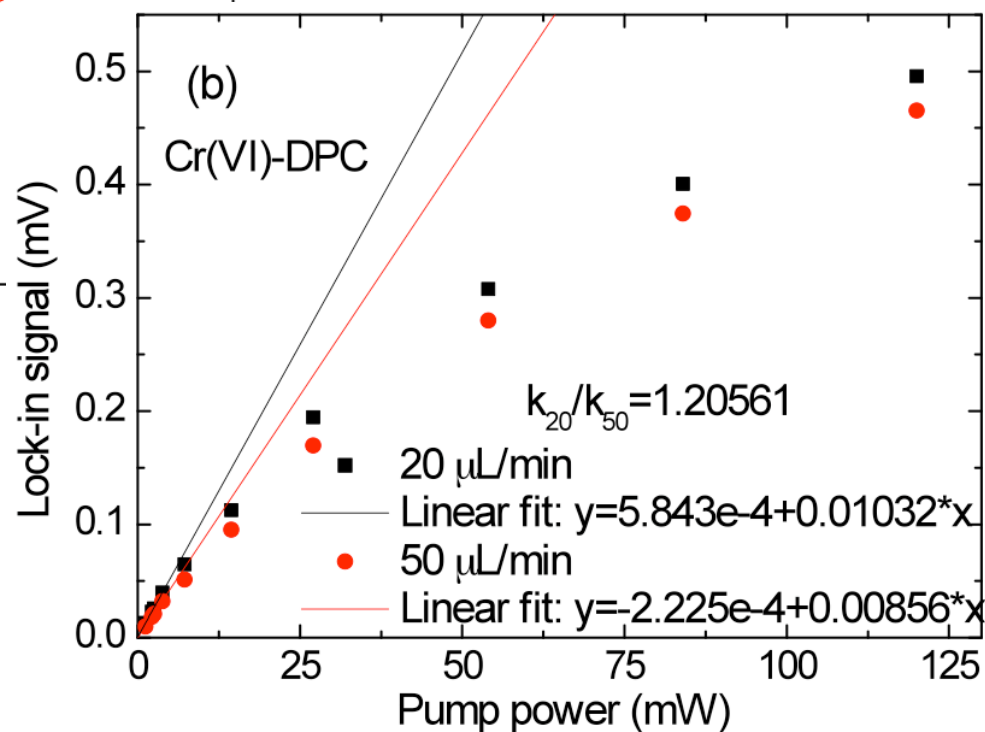
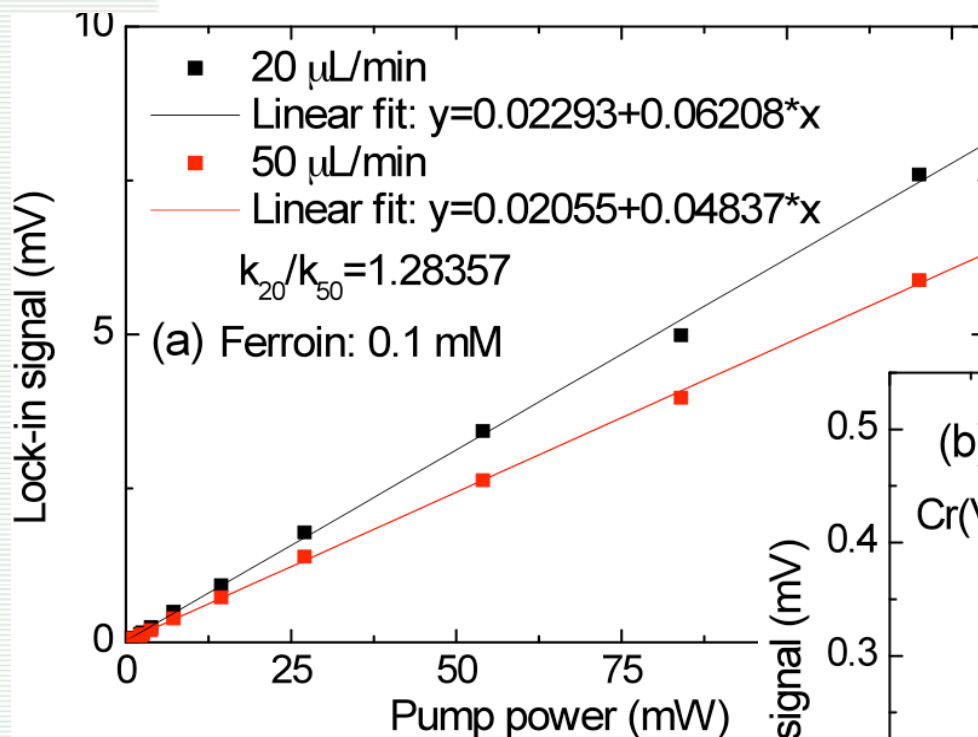


Effects of flow velocity and beam displacement on TLS signal



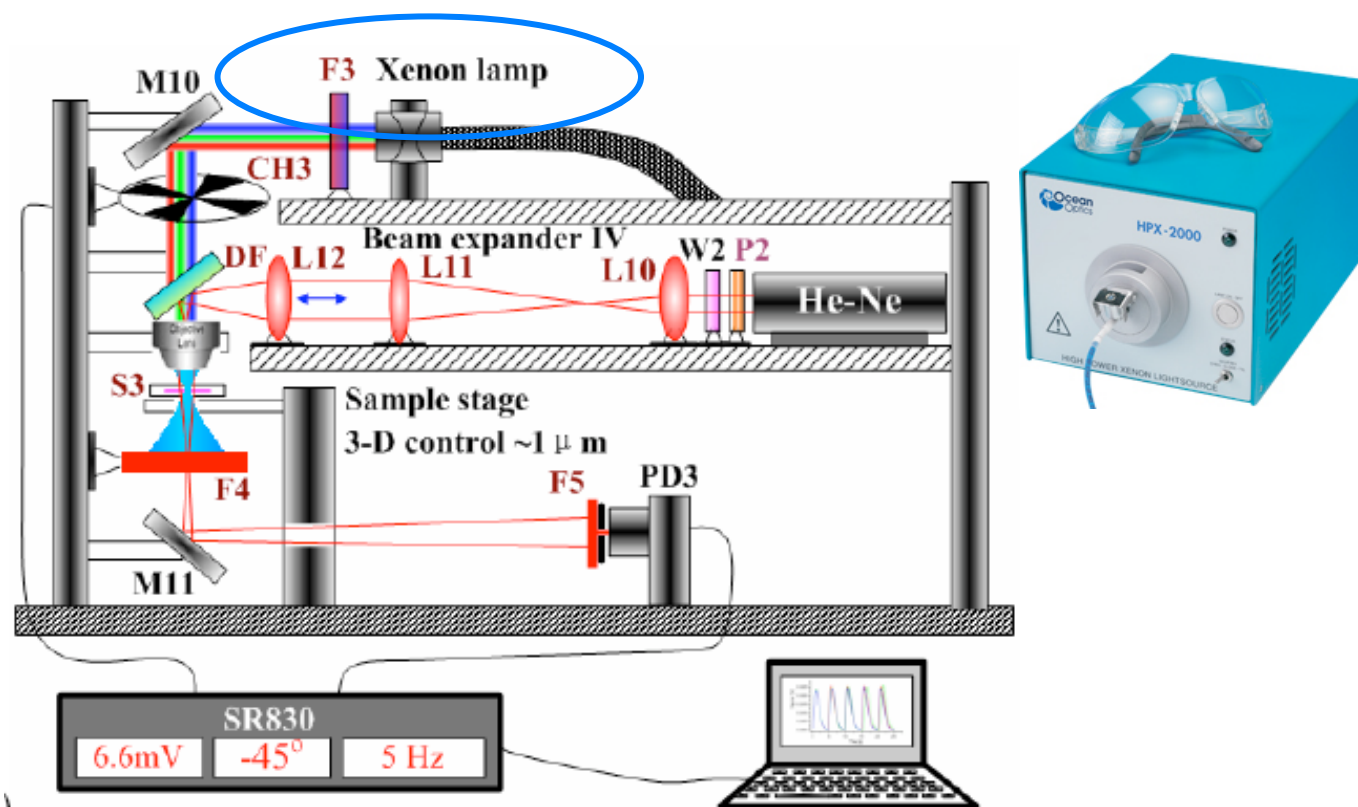


Effect of photodegradation in a microfluidic system



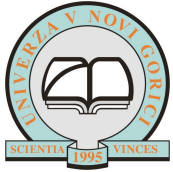


Incoherent light source (ILS)-excited TLM



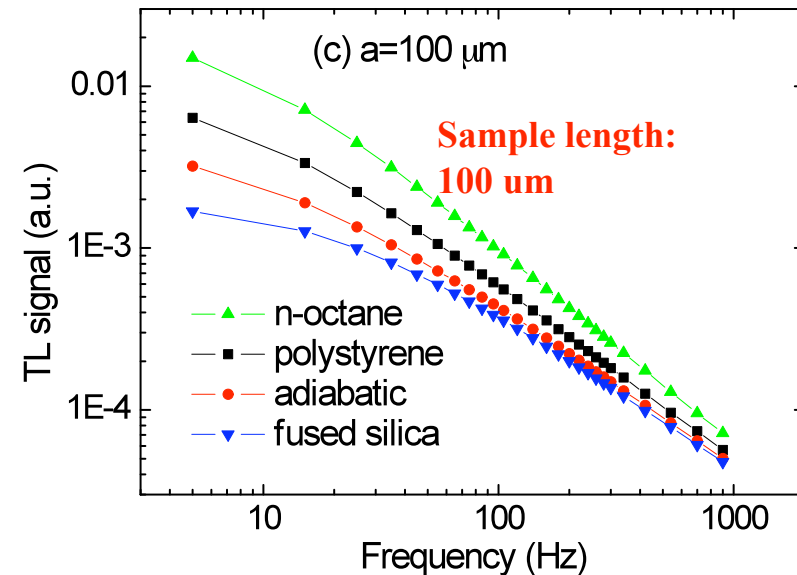
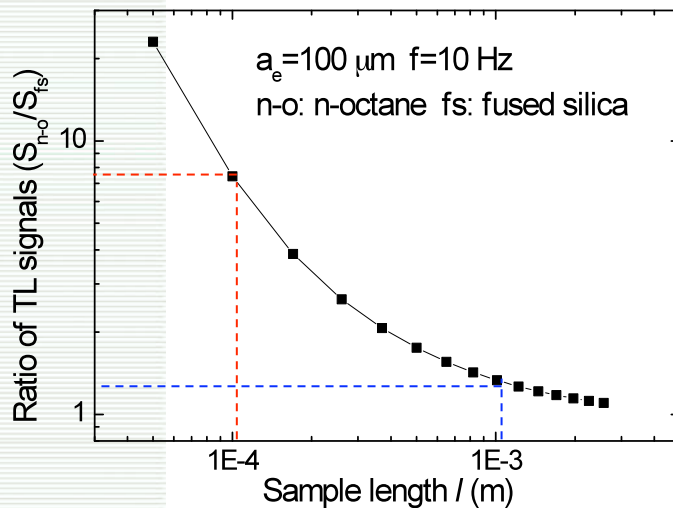
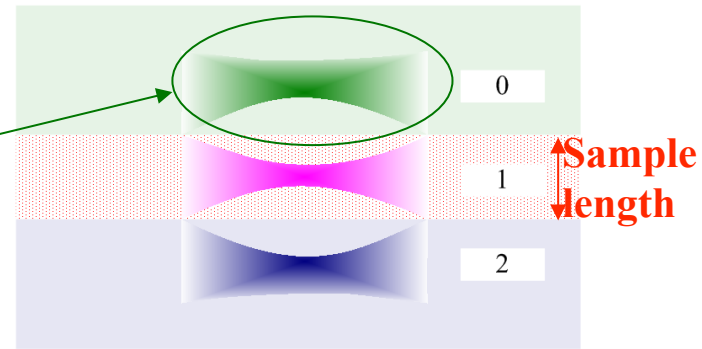
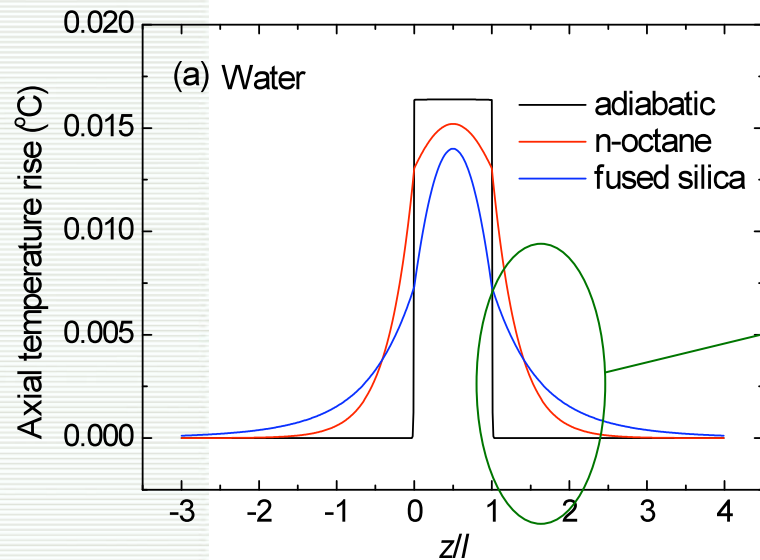
$$P_{eq}(514.5 \text{ nm})=1.05 \text{ mW}$$

Liu M., Franko M.: *Appl.Phys.Lett.*, **100**, 2012, 121110.



Thermal lens extends beyond the boundaries of microchannel

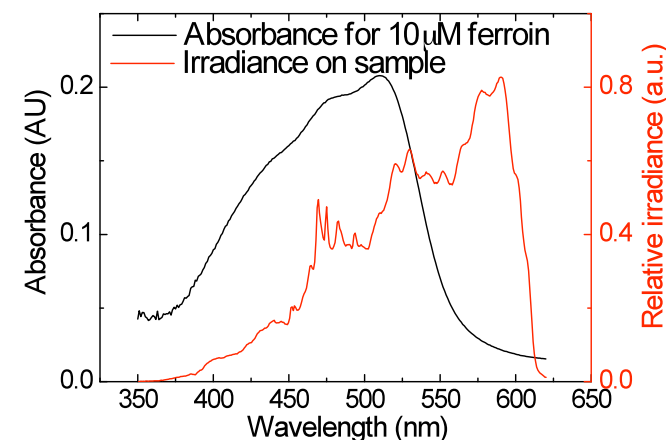
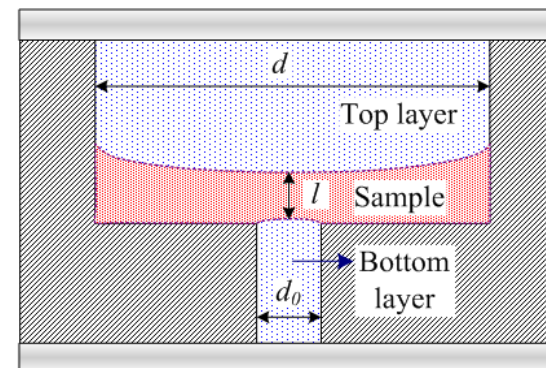
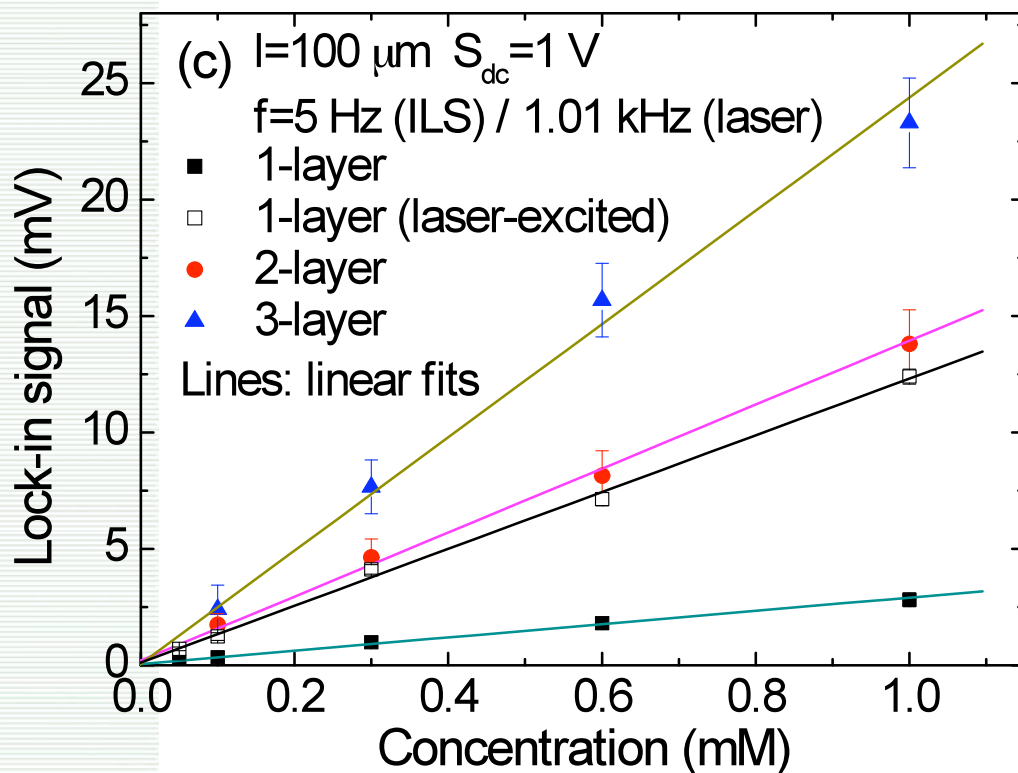
Sensitivity enhancement in ILS-TLM





Sensitivity enhancement in ILS-TLM in layered samples

LOD: 5×10^{-7} M at $P=1.05$ mW and $l=100$ μm for ferriin $\sim 2.2 \times 10^{-5}$ AU



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Thermal Lens Spectrometry

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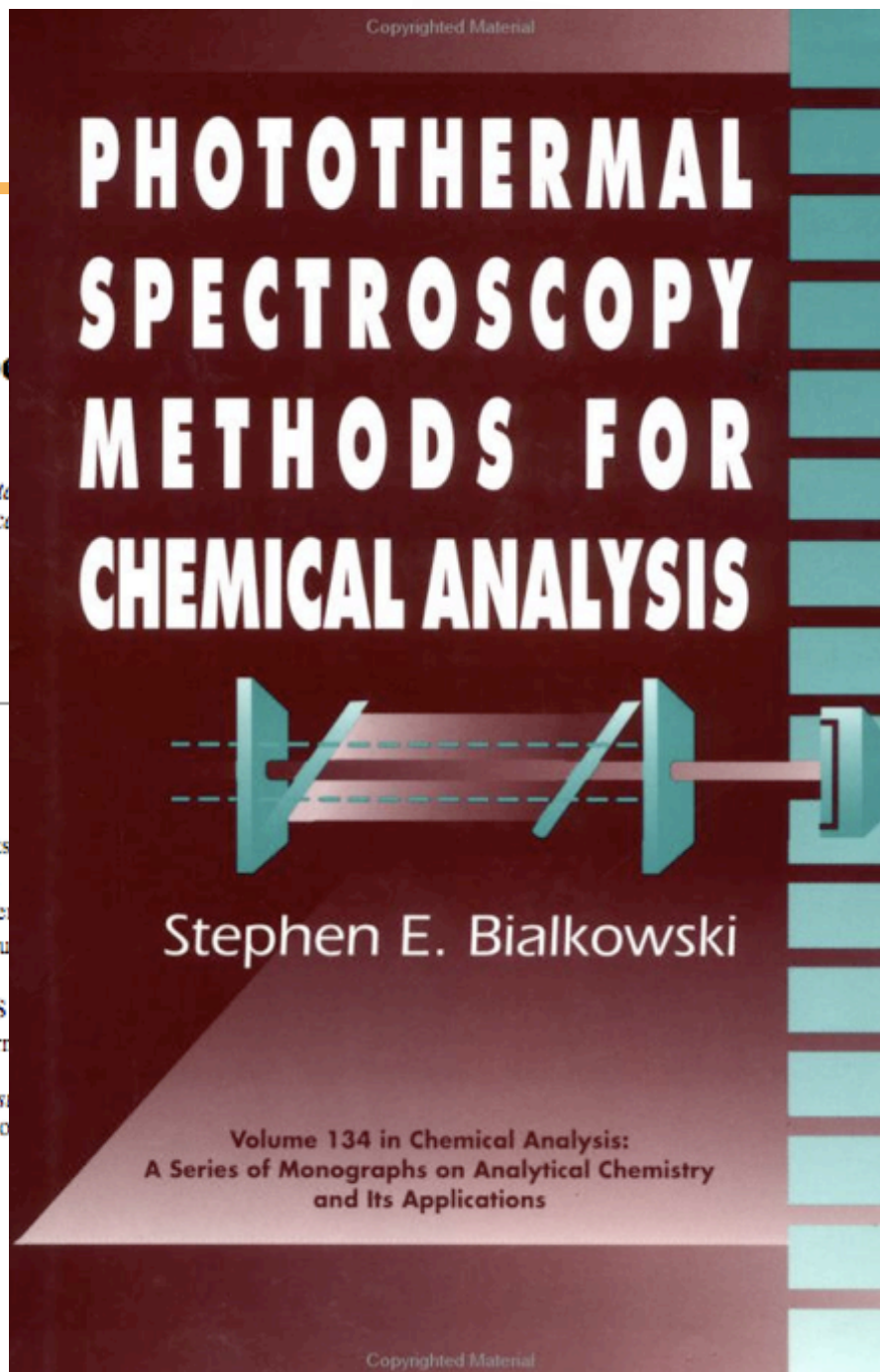
1 Introduction

2 Theory

3 Instrumentation

- 3.1 Single-beam Instruments
- 3.2 Dual-beam Instruments
- 3.3 Differential Thermal Lens Spectrometers
- 3.4 Multiwavelength and Tunable Laser Thermal Lens Spectrometers
- 3.5 Circular Dichroism TLS
- 3.6 Miniaturization of Thermal Lens Spectrometers

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Electric Detection in Flow Injection Separation Techniques

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University of Nova Gorica, Slovenia*

Flow injection analysis, liquid chromatography,

Thermal lens spectrometry in liquid chromatography), secondary electrophoresis and flow effects in TLS measurements in flow injection analysis is given to

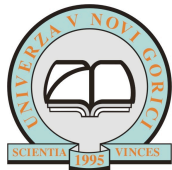
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