

# Engineered dissipative reservoir for microwave light using circuit optomechanics

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Workshop on Quantum Science and Quantum Technologies, Trieste, Italy

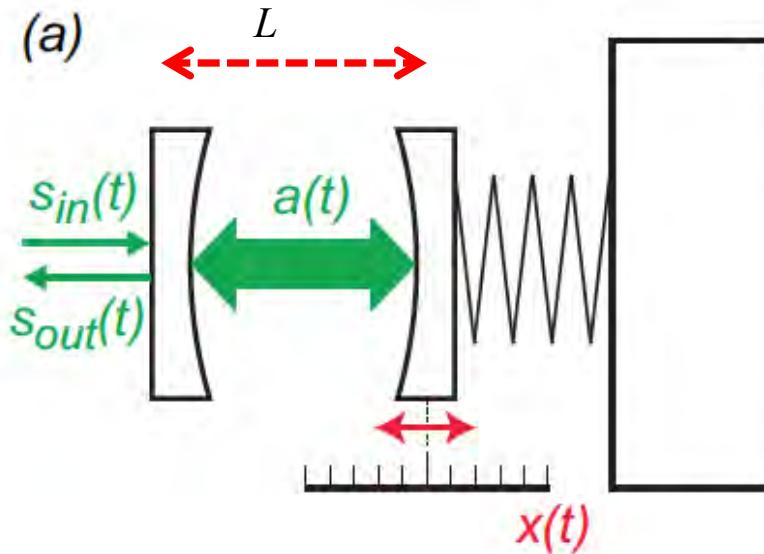
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European Research Council



# Canonical model for a cavity optomechanical system



$$\hat{H}_{\text{int}} = -\hbar G \hat{a}^\dagger \hat{a} \hat{x}$$

Optical frequency shift

$$\dot{\hat{a}} = i [\hat{H}, \hat{a}] / \hbar = i (\omega_c - G \hat{x}) \hat{a}$$

Radiation pressure force

$$\hat{F}_{\text{rp}} = - \frac{d \hat{H}_{\text{int}}}{d \hat{x}} = \hbar G \hat{a}^\dagger \hat{a}$$

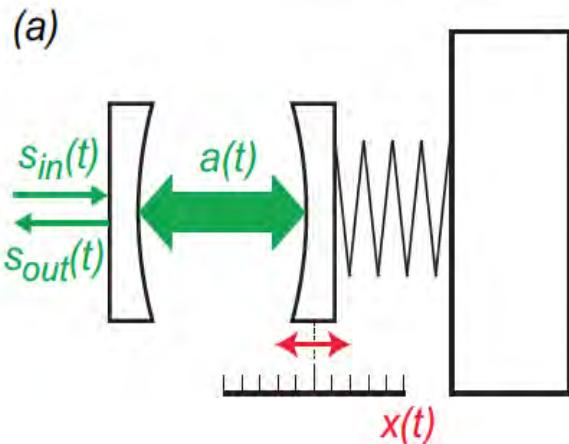
Vacuum optomechanical coupling rate

$$g_0 = G \sqrt{\frac{\hbar}{2m\Omega_m}}$$

measurement leads to  
a radiation pressure  
*'backaction'*

# Radiation pressure Dynamical backaction

Optical field responds on the mechanical motion with delay  $\tau \approx K^{-1}$



$$\frac{d^2x}{dt^2} + \Gamma_m \frac{dx}{dt} + \Omega_m^2 x = \frac{F_{rp}(x(t - \tau))}{m_{\text{eff}}}$$

Taylor expansion yields:

$$F_{rp}(x(t - \tau)) \approx \frac{dF}{dx} x - \tau \frac{dF}{dx} \frac{dx}{dt}$$

$$\Gamma_{\text{opt}} \approx \tau \frac{dF}{dx} \cdot \frac{1}{m_{\text{eff}}} \quad \Delta > 0$$

Amplification Blue detuning  
Dynamical backaction induced Parametric instability  
(JETP 1970, Braginsky)

$\Delta < 0$   
Cooling Red detuning  
(JETP 1970, Braginsky)

Braginsky, V. B. & Manukin A. B. *Measurement of Weak Forces in Physics Experiments.* (1977)

Braginsky, V. B. & Khalili, F. Y. *Quantum Measurement.* (1992)

Braginsky, V. B., Strigin, S. E. & Vyatchanin, S. P. Analysis of parametric oscillatory instability in power recycled LIGO interferometer. *Physics Letters A* 305, 111-124 (2002)

# Frequency domain picture

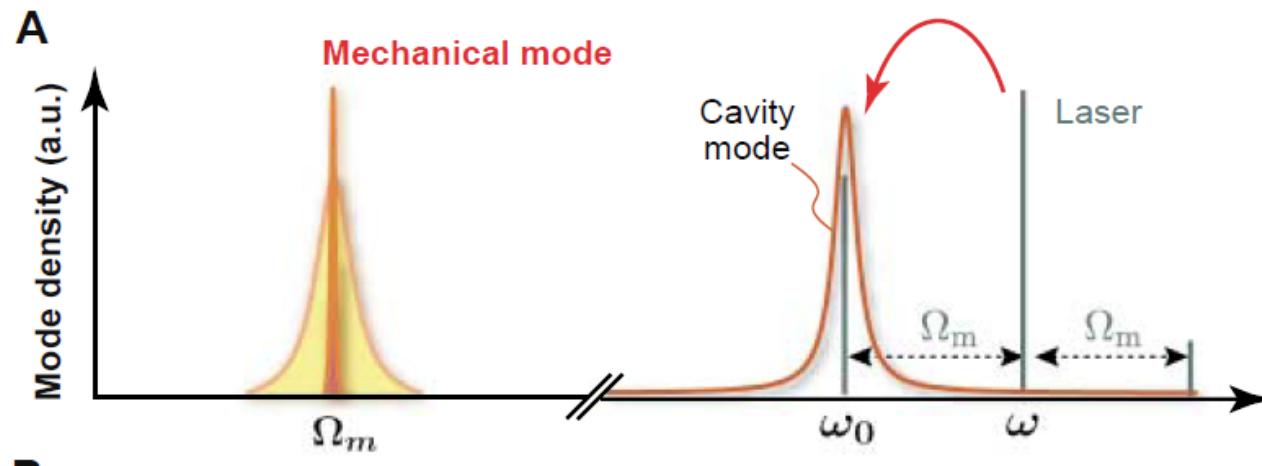
$$\Delta = -\Omega_m \quad H_{\text{int}} \approx -\hbar g_0 \sqrt{n_c} (\delta \hat{a}^\dagger \hat{b} + \delta \hat{a} \hat{b}^\dagger)$$

Coherent exchange of quanta, cooling

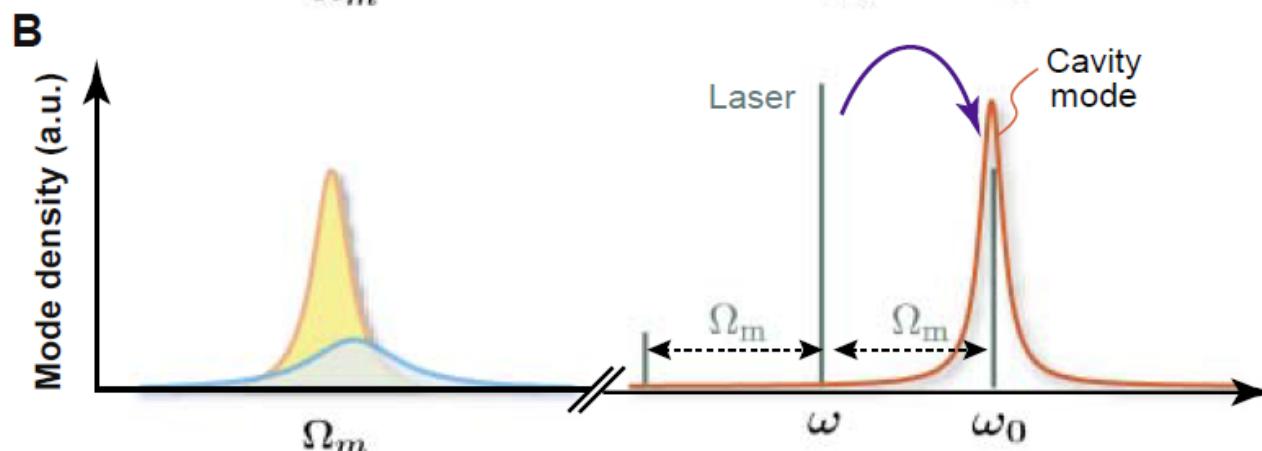
$$\Delta = +\Omega_m \quad H_{\text{int}} \approx -\hbar g_0 \sqrt{n_c} (\delta \hat{a}^\dagger \hat{b}^\dagger + \delta \hat{a} \hat{b})$$

Two-mode squeezing, amplification

Amplification



Resolved sideband  
Cooling



# Cavity optomechanics today

g



Suspended Macroscopic mirrors



Suspended micro-mirrors



Suspended micro-pillars



Trampoline resonators



Suspended membrane



Hybrid opto-mechanical systems



Microtoroid



Semiconductor microdisk resonator



Double-disk microresonator

fg



Near-field coupled nanomechanical oscillators



Free standing waveguides



Optical microsphere resonator



Micromechanical membrane in a superconducting microwave circuit



Photonic crystal defect cavity (2D)



Photonic crystal nano beam (1D)



Double string "zipper" cavity



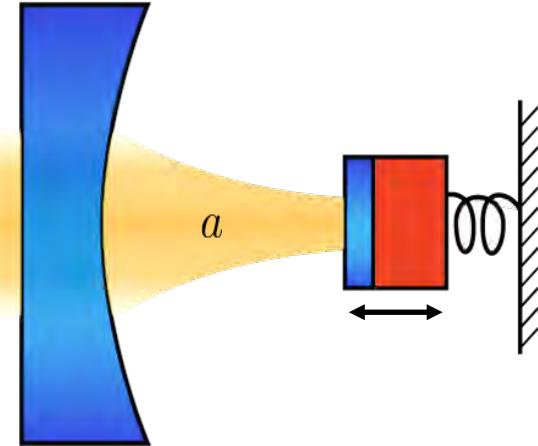
Nanorod inside a cavity



Cold Atoms coupled to an optical cavity

Mass

zg



M. Aspelmeyer, T. J. Kippenberg, F. Marquardt.  
*Rev. Mod. Phys.* **86**, 1391 (2014)

$$\dot{\delta\hat{a}} = +i\Delta\delta\hat{a} - \frac{\kappa}{2}\delta\hat{a} + ig_0\sqrt{n_c}(\hat{b} + \hat{b}^\dagger) + \sqrt{\kappa_{\text{ex}}}\delta\hat{a}_{\text{in,ex}} + \sqrt{\kappa_0}\delta\hat{a}_{\text{in,0}}$$

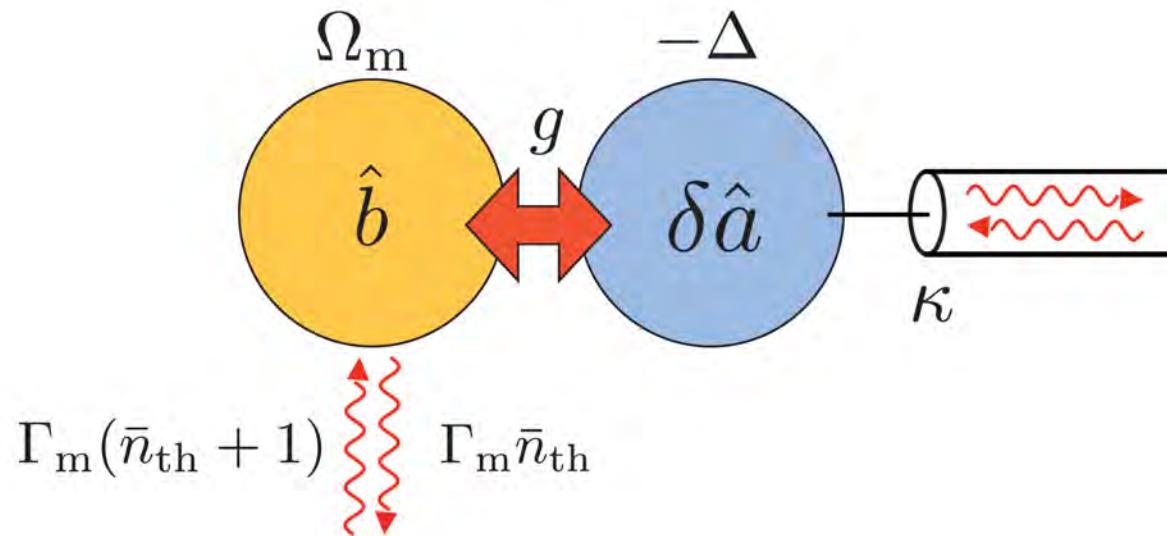
$$\dot{\hat{b}} = -i\Omega_m\hat{b} - \frac{\Gamma_m}{2}\hat{b} + ig_0\sqrt{n_c}(\delta\hat{a} + \delta\hat{a}^\dagger) + \sqrt{\Gamma_m}\hat{b}_{\text{in}}$$

# Cavity optomechanics and reservoir engineering

$$\kappa \gg \Gamma_m$$

$$k_B T \ll \hbar\omega$$

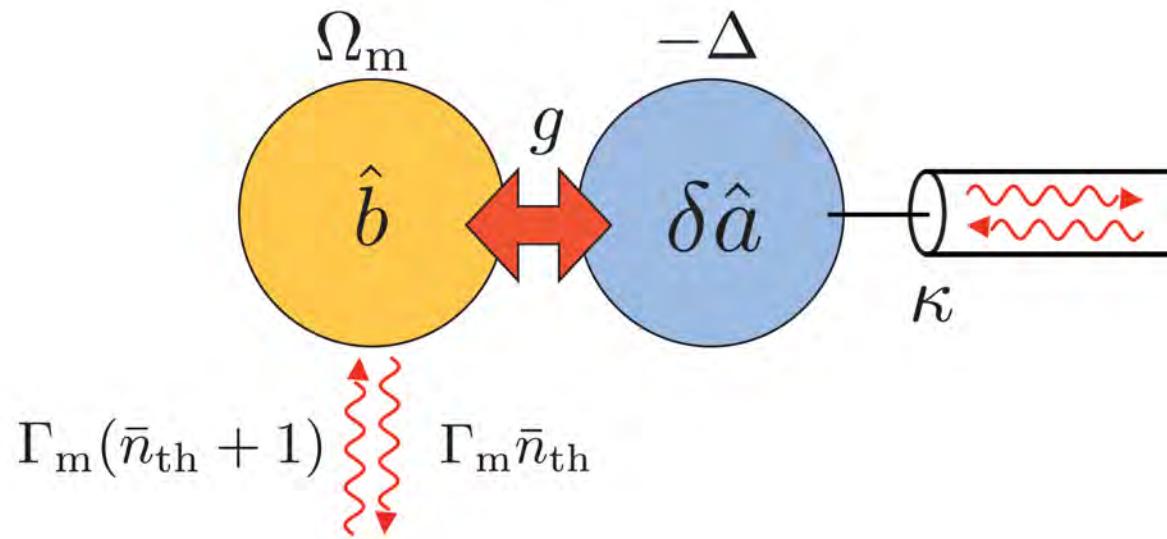
mechanical oscillator      Microwave cavity



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Electromagnetic mode constitutes a cold dissipative bath for the mechanical sub-system. We can *prepare* the state (e.g. ground state or squeezed state) of the *mechanical* oscillator by *controlling coupling* between the mechanical resonator and the electromagnetic mode.

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$$k_B T \ll \hbar\omega$$

- Resolved sideband cooling & amplification of mechanical motion
- Opto- and electromechanically induced transparency (OMIT/EMIT)
- Back-action evading measurements
- Mechanical squeezing via optomechanical reservoir engineering

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Can we turn the mechanical resonator into a reservoir for light?



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Can we turn the mechanical resonator into a reservoir for light?

Yes!

We need

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# The reversed dissipation regime

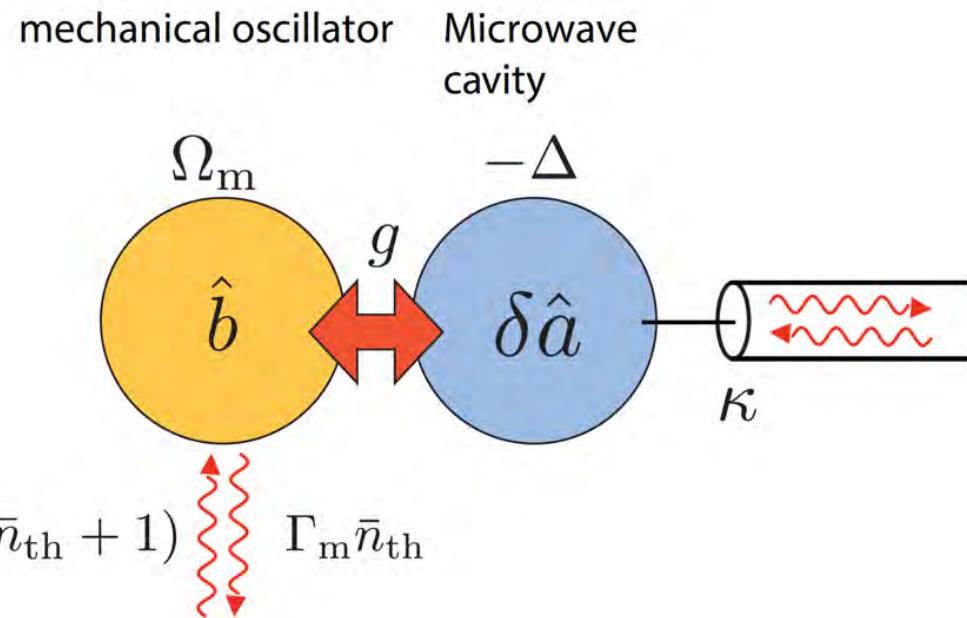
## Optomechanical interactions

$$\Delta = -\Omega_m$$

$$H_{\text{int}} \approx -\hbar g_0 \sqrt{n_c} (\delta \hat{a}^\dagger \hat{b} + \delta \hat{a} \hat{b}^\dagger)$$

Coherent exchange of quanta, cooling

Electromagnetic mode damps  
mechanical oscillator on **red sideband**



Conventional dissipation hierarchy:

$$\kappa \gg \Gamma_m$$

# The reversed dissipation regime

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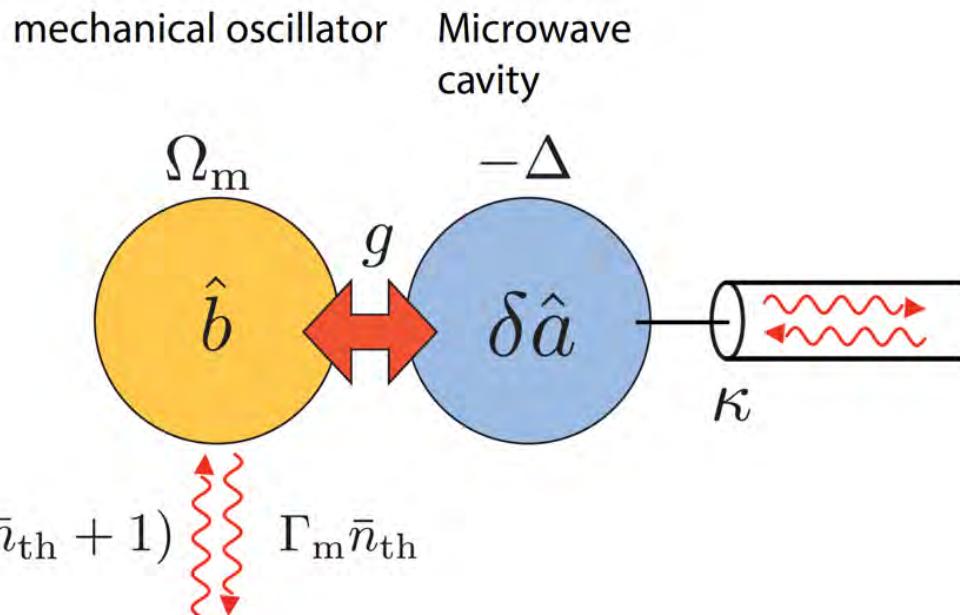
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Amplification and two mode squeezing  
Electromagnetic mode amplifies  
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$$\Gamma_{\text{eff}} \rightarrow \kappa_{\text{eff}}$$

**Reversed dissipation** hierarchy :

$$\kappa \ll \Gamma_m$$

Change in the *mechanical damping rate*,  
becomes change in the *optical decay rate*.

# The reversed dissipation regime

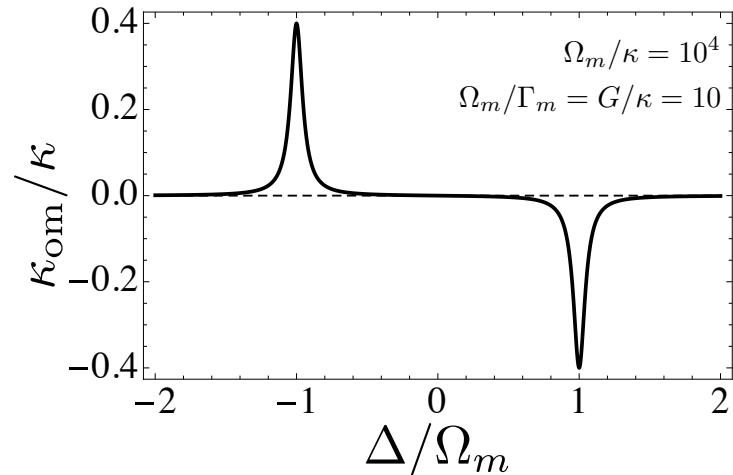
Reversed dissipation hierarchy :  $\kappa \ll \Gamma_m$

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Reversed dissipation hierarchy :  $\kappa \ll \Gamma_m$



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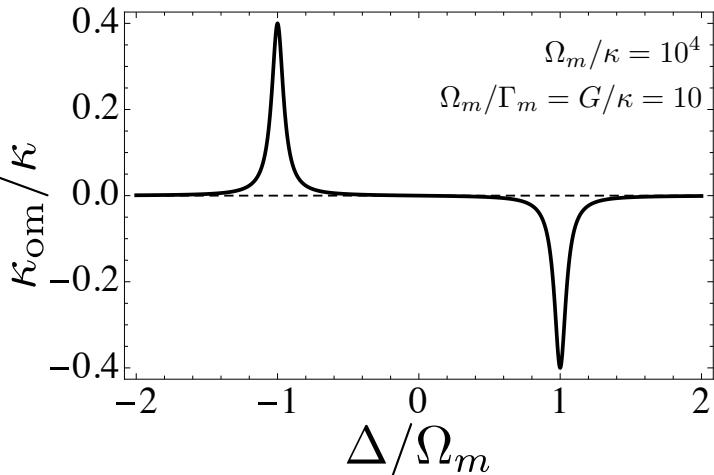
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**Change in the electromagnetic decay rate  
(mechanical damping)**

$$K_{\text{om}} = \frac{\Gamma_{\text{eff}} g_0^2 n_c}{(\Gamma_{\text{eff}}/2)^2 + (\Delta + \Omega_m)^2} - \frac{\Gamma_{\text{eff}} g_0^2 n_c}{(\Gamma_{\text{eff}}/2)^2 + (\Delta - \Omega_m)^2}$$

# The reversed dissipation regime

Reversed dissipation hierarchy :  $\kappa \ll \Gamma_m$



$$\Gamma_{\text{eff}} \rightarrow \kappa_{\text{eff}}$$

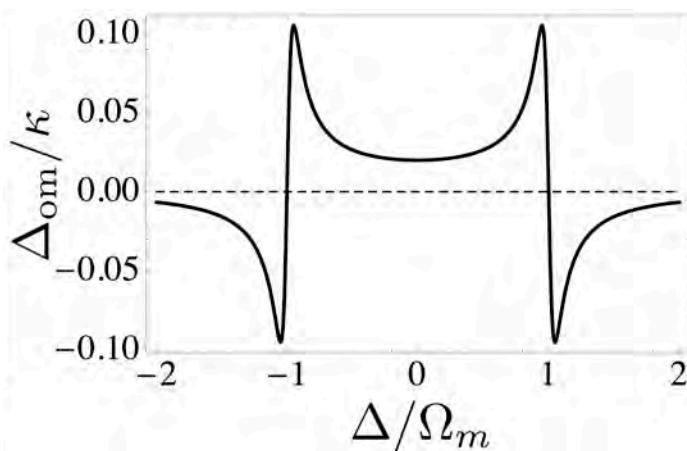
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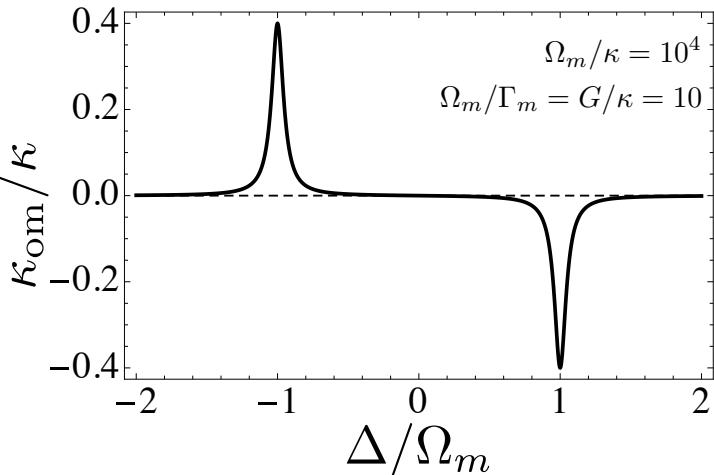
**Change in the electromagnetic resonance freq.**

$$\Delta\omega_{\text{om}} = \frac{\Gamma_{\text{eff}} g_0^2 n_c (\Delta - \Omega_m)}{(\Gamma_{\text{eff}}/2)^2 + (\Delta + \Omega_m)^2} - \frac{\Gamma_{\text{eff}} g_0^2 n_c (\Delta + \Omega_m)}{(\Gamma_{\text{eff}}/2)^2 + (\Delta - \Omega_m)^2}$$



# The reversed dissipation regime

Reversed dissipation hierarchy :  $\kappa \ll \Gamma_m$



$$\Gamma_{\text{eff}} \rightarrow \kappa_{\text{eff}}$$

Change in the *mechanical* damping rate,  
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Change in the electromagnetic decay rate  
(mechanical damping)

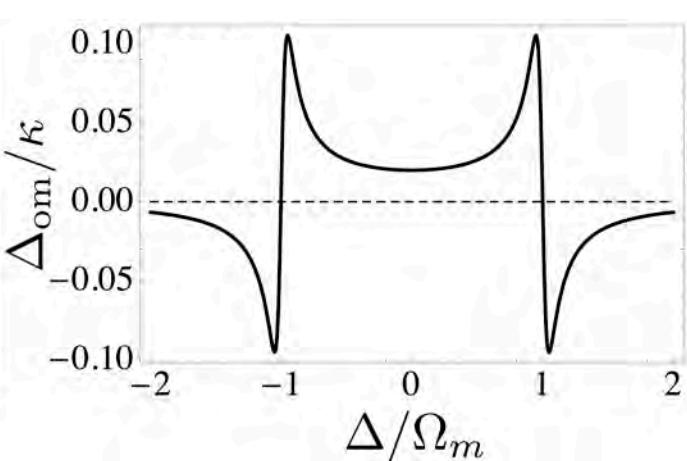
$$\kappa_{\text{om}} = \frac{\Gamma_{\text{eff}} g_0^2 n_c}{(\Gamma_{\text{eff}}/2)^2 + (\Delta + \Omega_m)^2} - \frac{\Gamma_{\text{eff}} g_0^2 n_c}{(\Gamma_{\text{eff}}/2)^2 + (\Delta - \Omega_m)^2}$$

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Modified cavity response

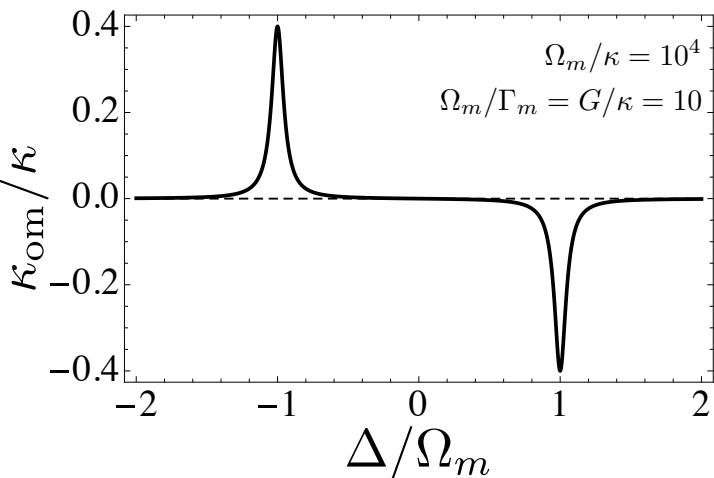
$$S_{11}(\omega) = 1 - \frac{\kappa_{\text{ex}}}{(\kappa_0 + \kappa_{\text{ex}} + \kappa_{\text{om}})/2 + i(\omega_c + \Delta\omega_{\text{om}} - \omega)}$$



# The reversed dissipation regime

Reversed dissipation hierarchy :  $\kappa \ll \Gamma_m$

Mechanics amplifies electromagnetic mode on blue sideband



$$\Gamma_{\text{eff}} \rightarrow \kappa_{\text{eff}}$$

Change in the *mechanical* damping rate, becomes change in the *optical* decay rate.

Change in the electromagnetic decay rate  
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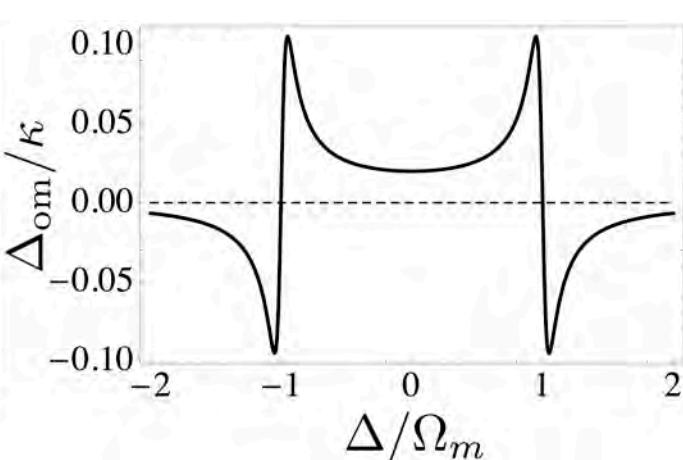
$$\kappa_{\text{om}} = \frac{\Gamma_{\text{eff}} g_0^2 n_c}{(\Gamma_{\text{eff}}/2)^2 + (\Delta + \Omega_m)^2} - \frac{\Gamma_{\text{eff}} g_0^2 n_c}{(\Gamma_{\text{eff}}/2)^2 + (\Delta - \Omega_m)^2}$$

Change in the electromagnetic resonance freq.

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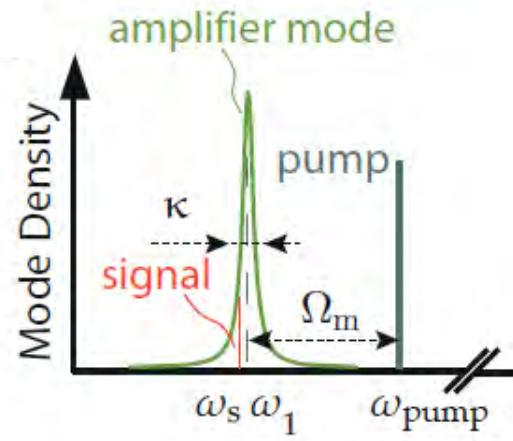
Modified cavity response

$$S_{11}(\omega) = 1 - \frac{\kappa_{\text{ex}}}{(\kappa_0 + \kappa_{\text{ex}} + \kappa_{\text{om}})/2 + i(\omega_c + \Delta\omega_{\text{om}} - \omega)}$$

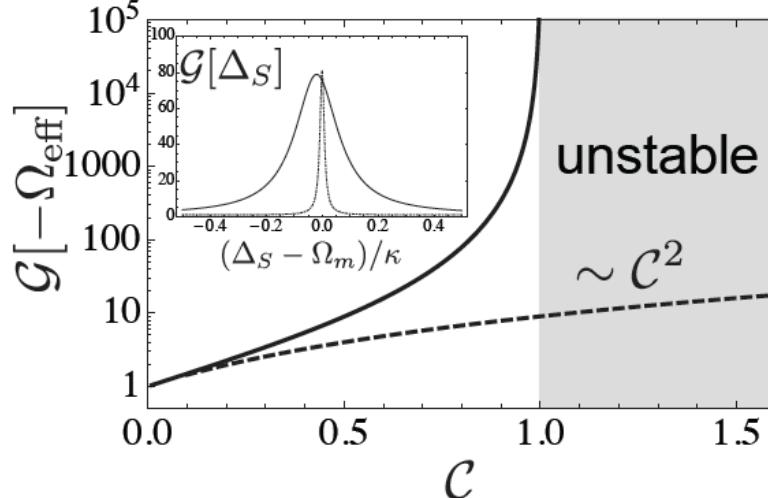


# Amplification in the reversed dissipation regime

Amplification scheme



$$\Gamma_m \gg \kappa$$



$$\hat{a}_{\text{out}} = A(\omega)\hat{a}_{\text{in}} + \underbrace{B(\omega)\hat{a}_{\text{in}}^\dagger}_{|B| \ll |A|} + C(\omega)\hat{b}_{\text{in}} + \underbrace{D(\omega)\hat{b}_{\text{in}}^\dagger}_{|C| \ll |D|}$$

The system operates as a **phase preserving parametric amplifier**

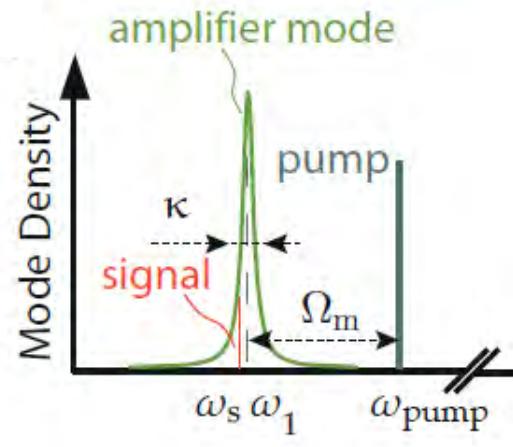
**Gain of the amplifier**

$$G(\Delta_s) = \left| 1 - \frac{\kappa}{\kappa_{\text{eff}} / 2 - i(\Delta_s + \Delta_{\text{eff}})} \right|^2$$

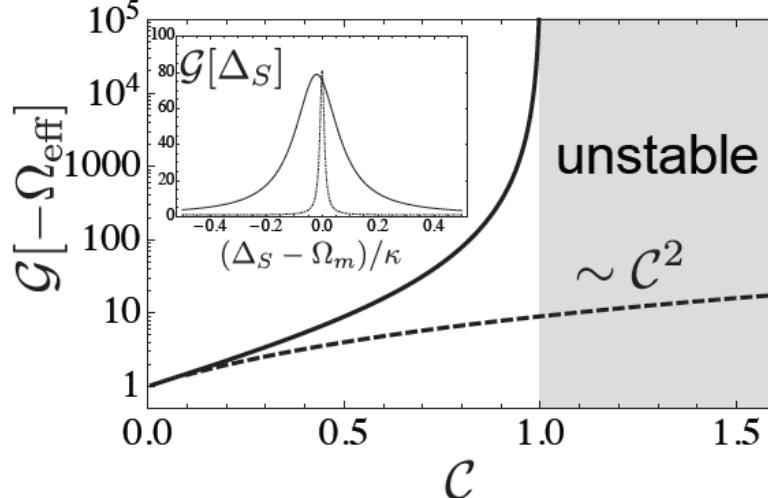
$$G(0) = \left| \frac{1+C}{1-C} \right|^2$$

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Amplification scheme



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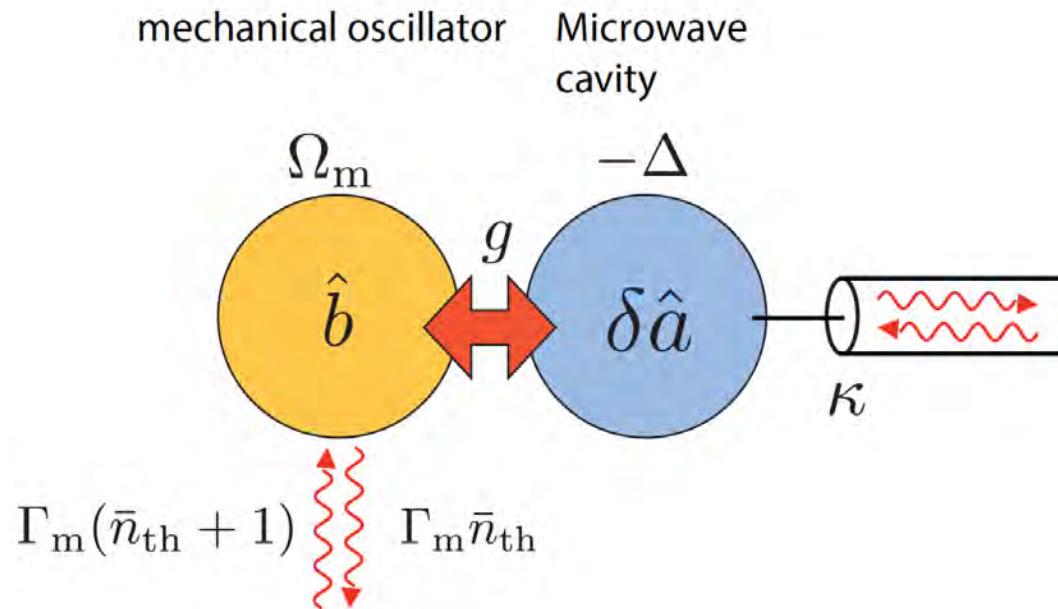
The system operates as a **phase preserving parametric amplifier**

## Noise added by the amplifier

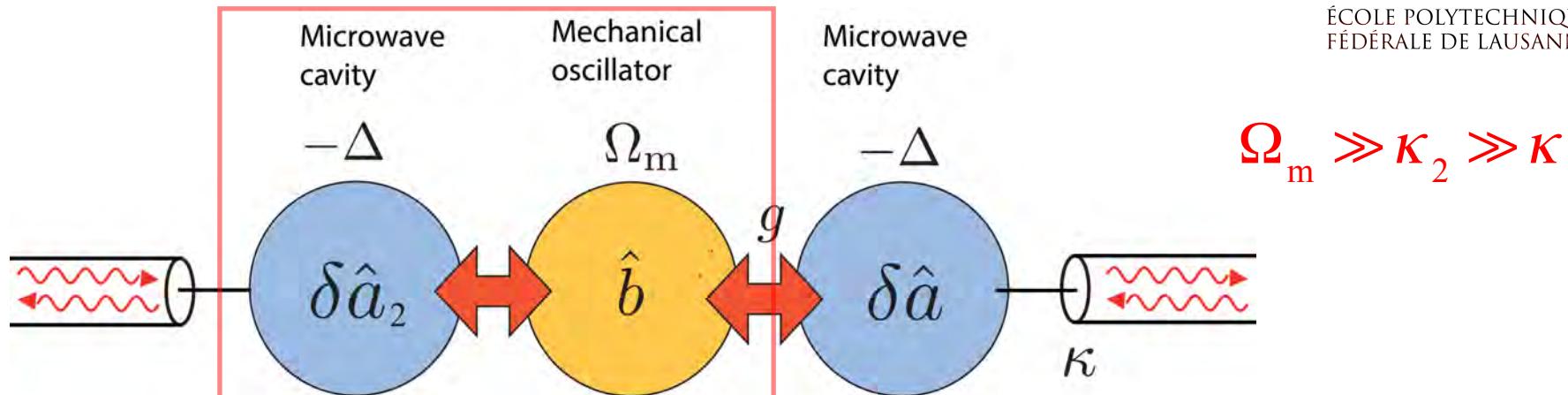
$$\mathcal{N} = (n_{\text{eff}} + \frac{1}{2}) \left| \frac{D(\omega)}{A(\omega)} \right|^2 = \frac{4C \left( n_{\text{eff}} + \frac{1}{2} \right)}{(C+1)^2} \rightarrow n_{\text{eff}} + \frac{1}{2}$$

Providing a dissipative but cold mechanical oscillator therefore realizes a **quantum limited phase preserving amplifier** based on a mechanical oscillator

# Two-mode implementation of the reversed dissipation regime



# Two-mode implementation of the reversed dissipation regime



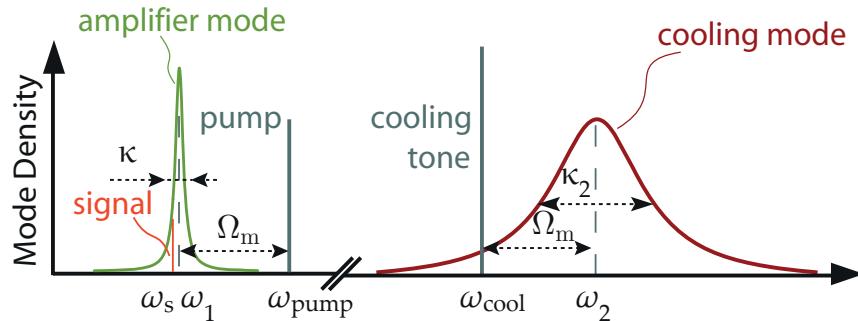
## Realization of RDR:

The second mode establishes the RDR with respect to the amplifier mode:

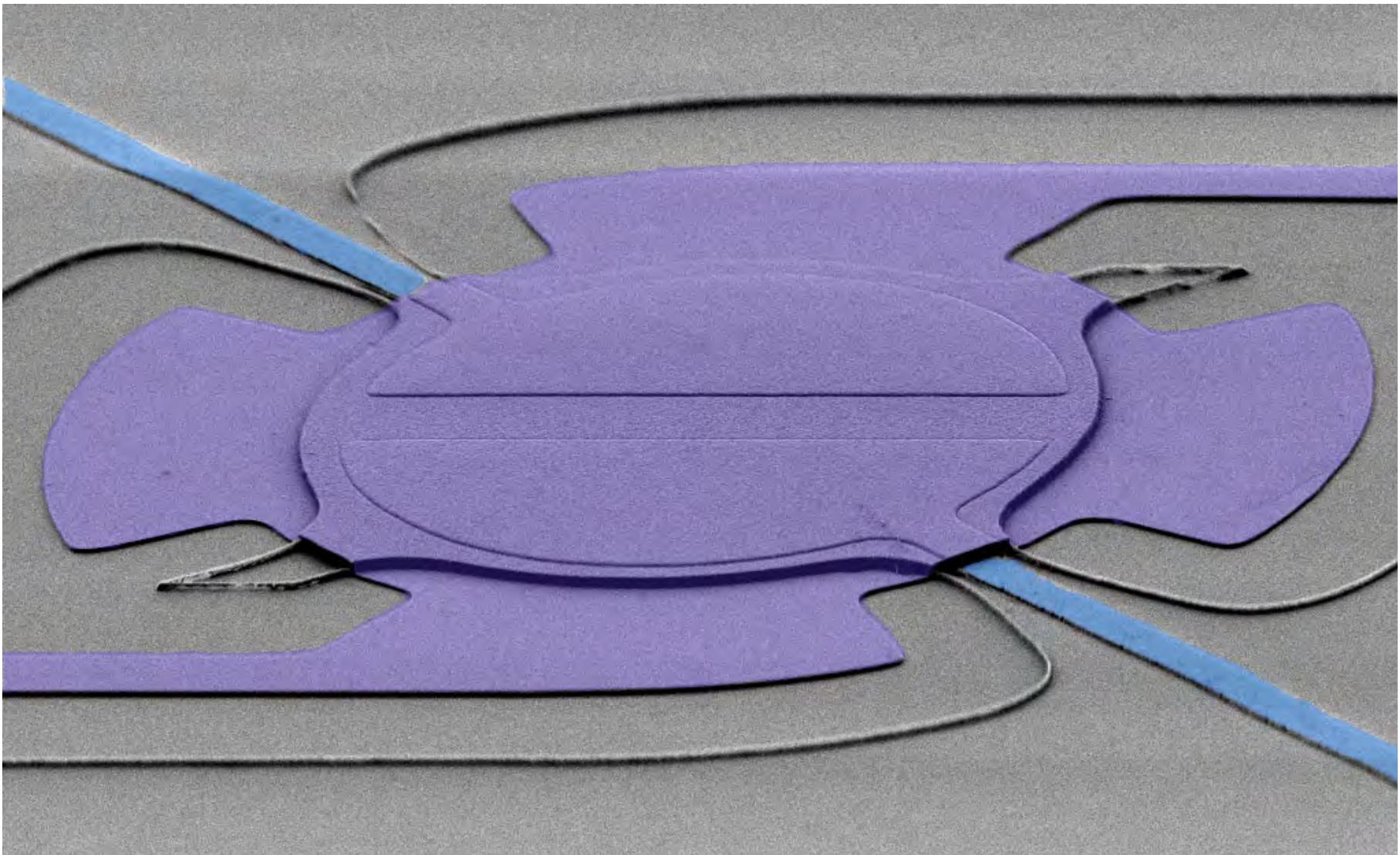
$$\Gamma_{\text{eff}} = \Gamma_m (\mathcal{C}_2 + 1)$$

$$\Gamma_{\text{eff}} \rightarrow \kappa_2 / 2 \gg \kappa$$

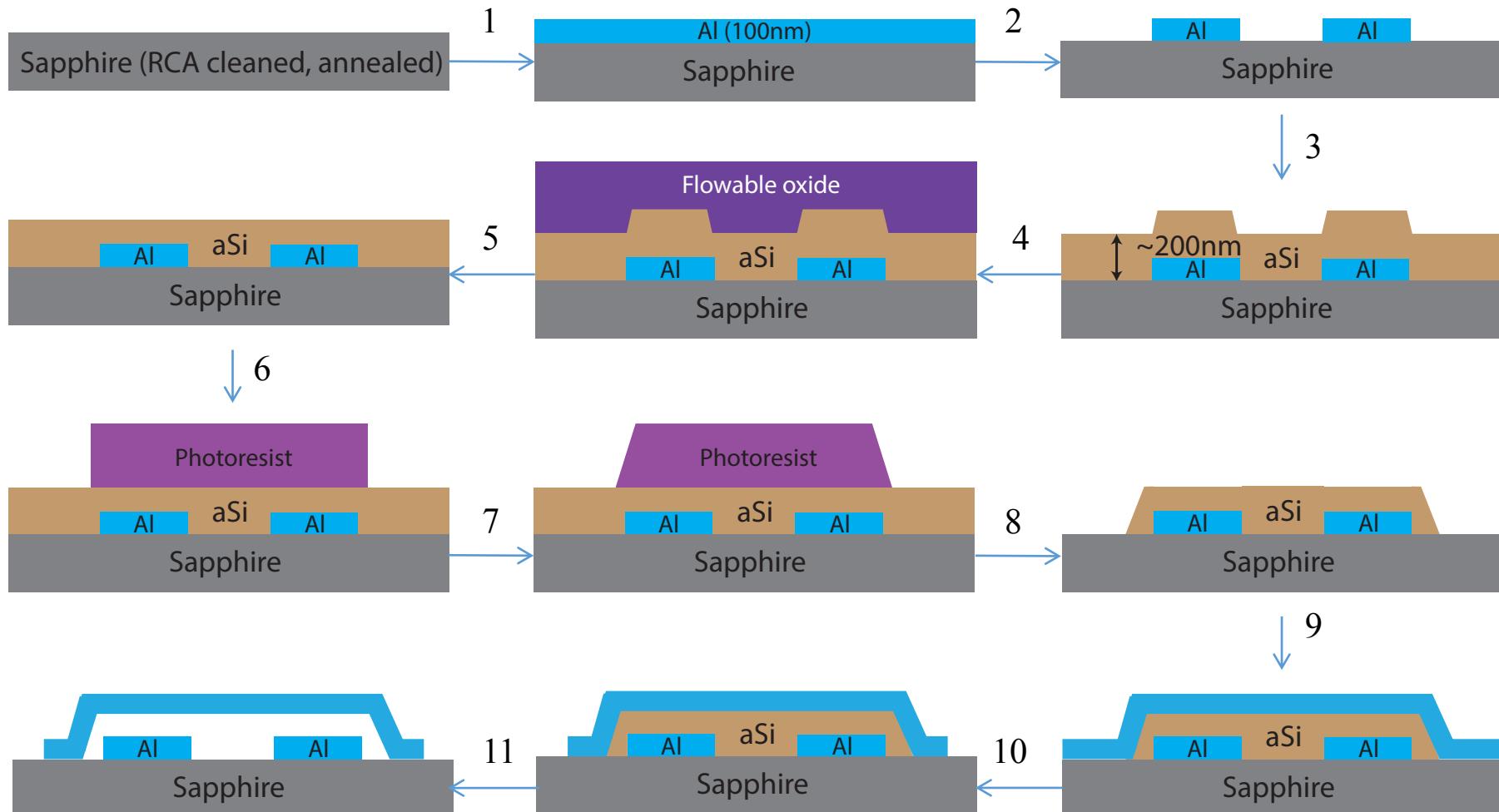
$$\text{for } \mathcal{C}_2 = \frac{4G_2^2}{\kappa_2 \Gamma_m} \gg 1$$



# Circuit design and fabrication



# Process flow – dual-mode circuits



**1, 3, 9:** metal and sacrificial layer (Si) deposition

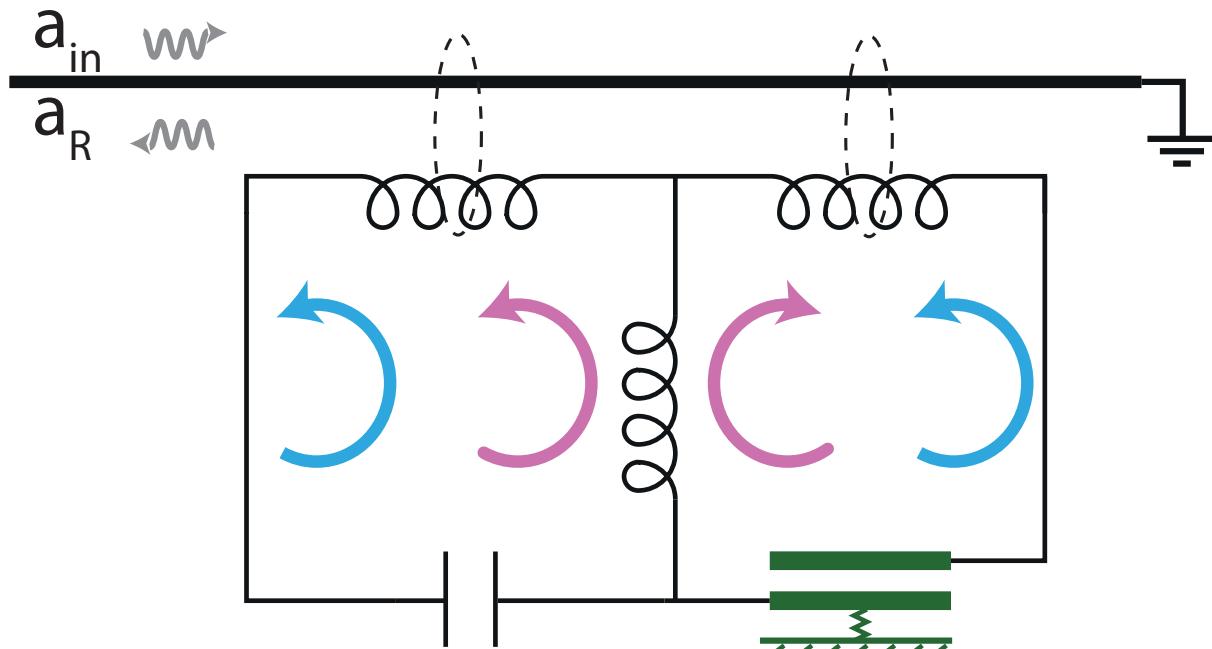
**2, 8, 10:** metal and Si etch

**4, 5:** planarization of Si layer (for split-plate drums)

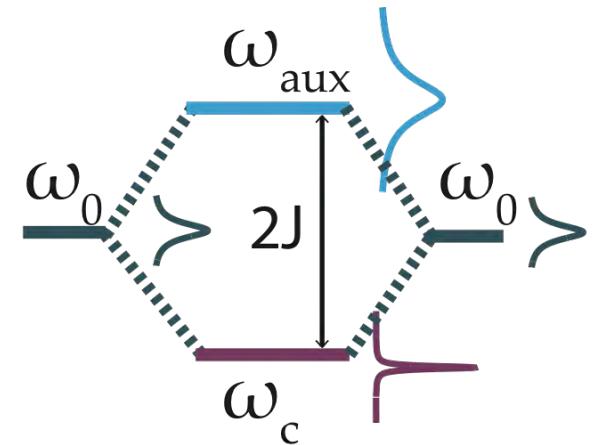
**6, 7:** lithography to open Si layer (with reflow)

**11:** releasing the drum capacitor ( $\text{XeF}_2$ )

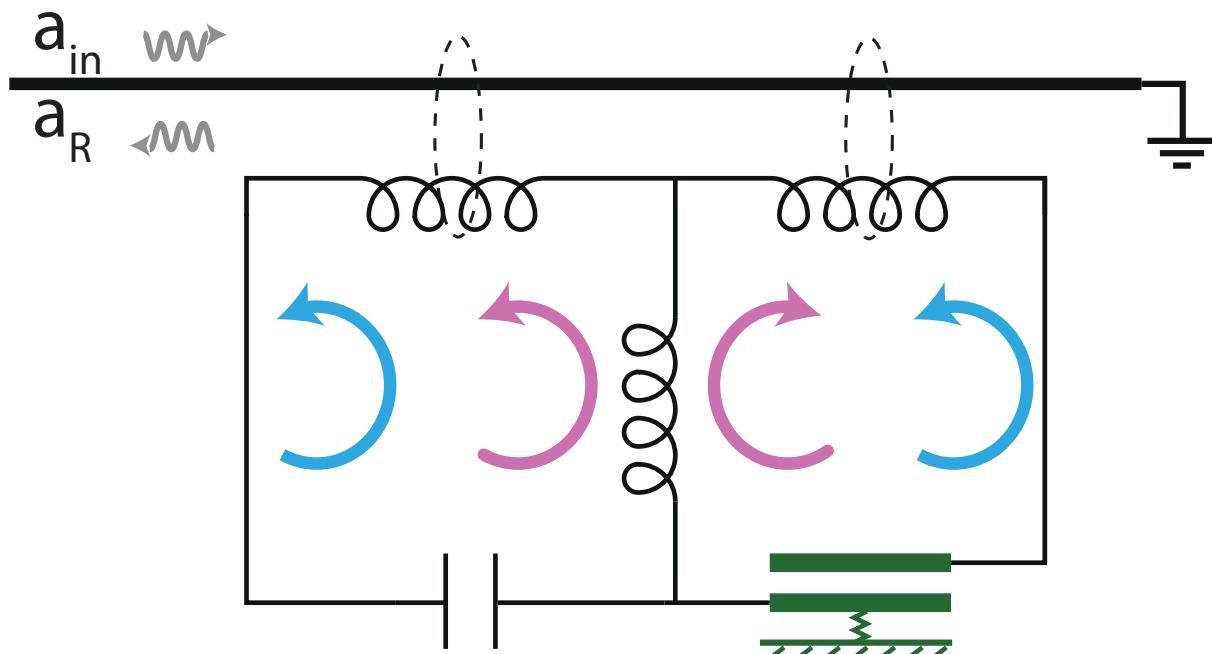
# New approach – hybrid modes



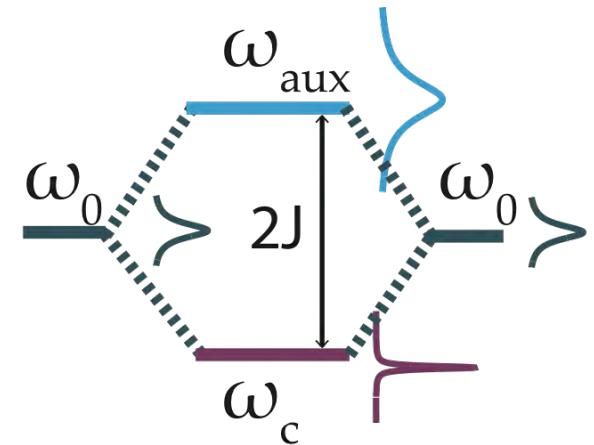
mechanical element



# New approach – hybrid modes

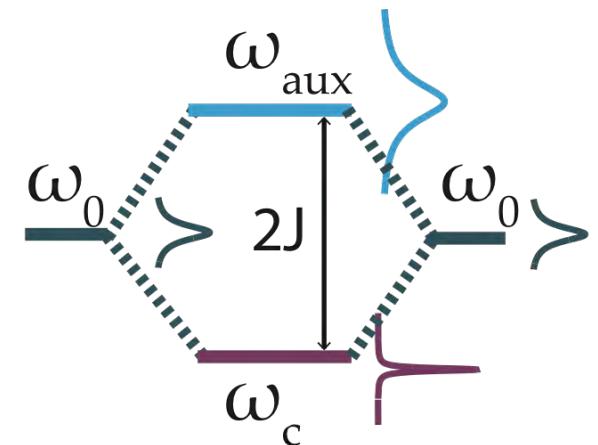
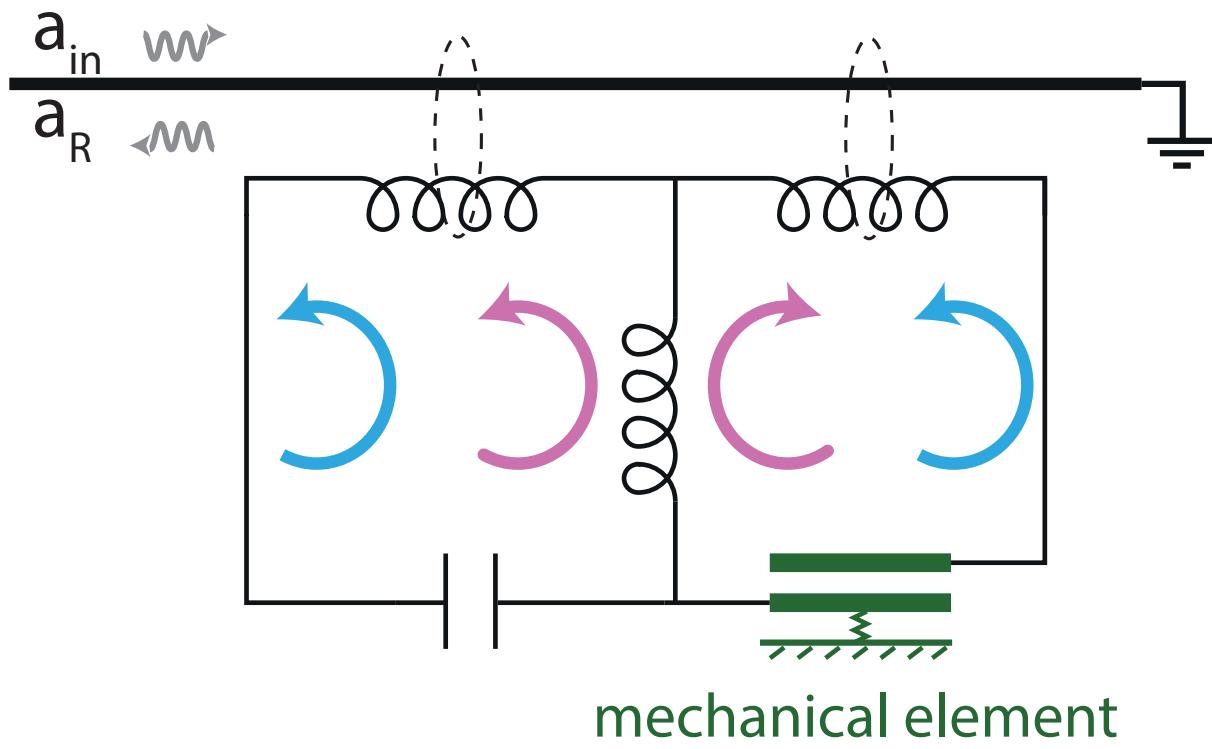


mechanical element



$$\hat{H}_{int} = \hbar J(\hat{a}_1^\dagger \hat{a}_2 + \hat{a}_2^\dagger \hat{a}_1) + \hbar g_0 \hat{a}_1^\dagger \hat{a}_1 (\hat{b} + \hat{b}^\dagger)$$

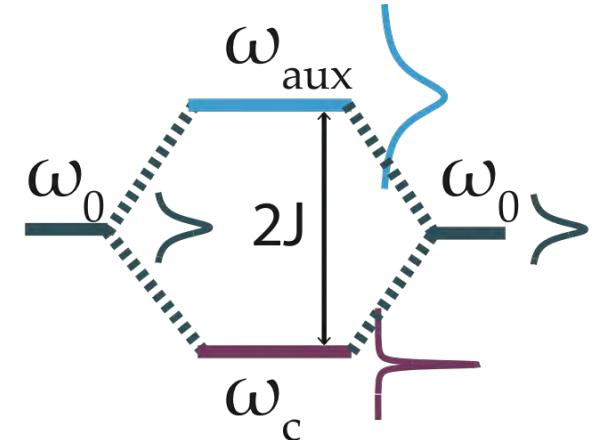
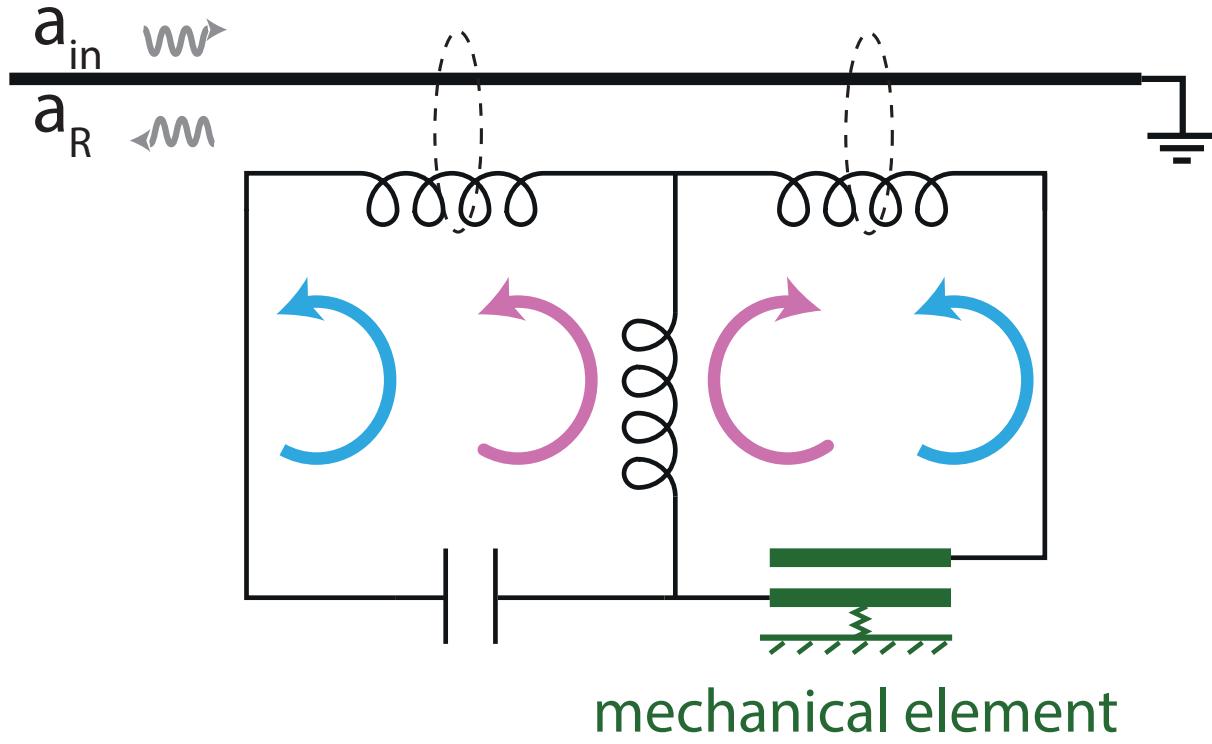
# New approach – hybrid modes



$$\hat{a}_{s,a} = \sqrt{2}^{-1} (\hat{a}_1 \pm \hat{a}_2)$$

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# New approach – hybrid modes

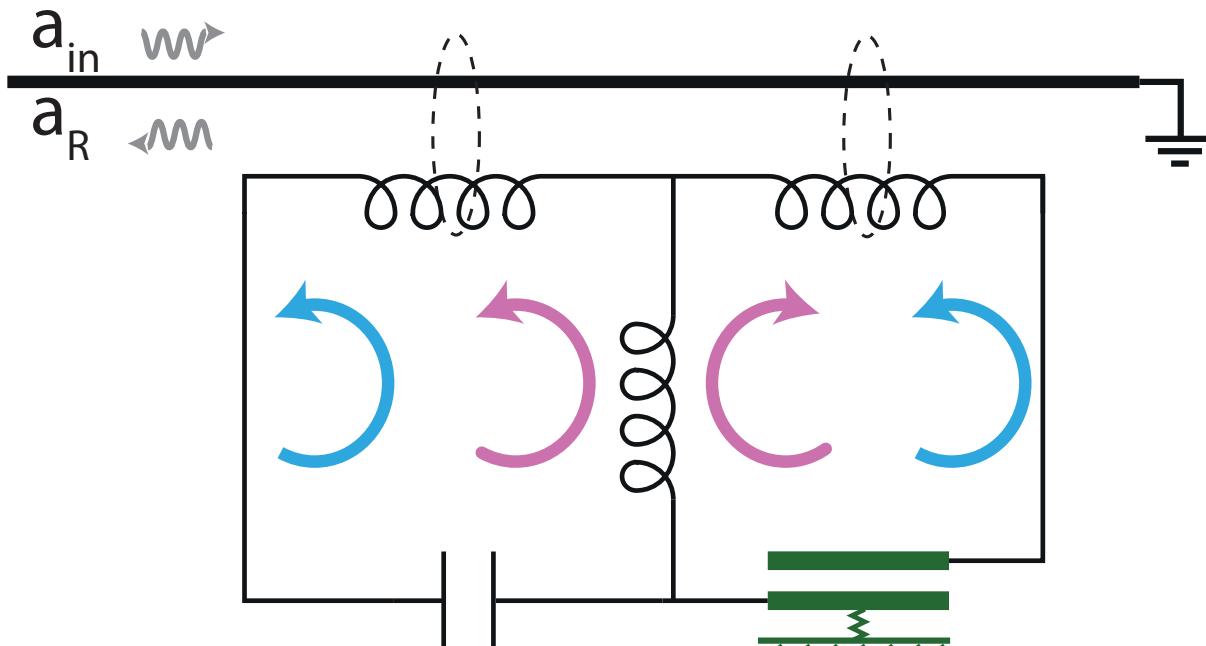


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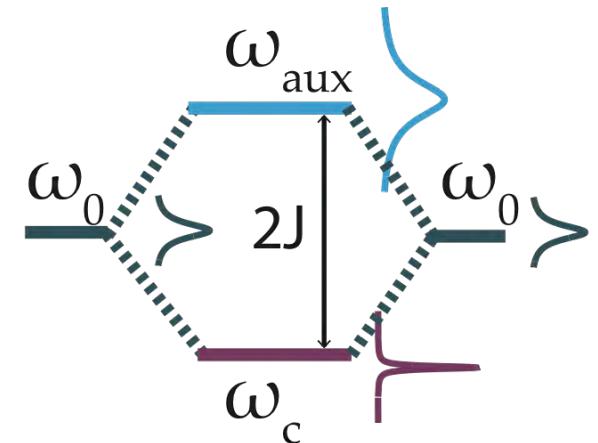
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$$\hat{H}_{\text{int}} = \hbar J(\hat{a}_s^\dagger \hat{a}_s - \hat{a}_a^\dagger \hat{a}_a) + \hbar \frac{g_0}{2} (\hat{a}_a^\dagger \hat{a}_a + \hat{a}_s^\dagger \hat{a}_s)(\hat{b} + \hat{b}^\dagger)$$

# New approach – hybrid modes



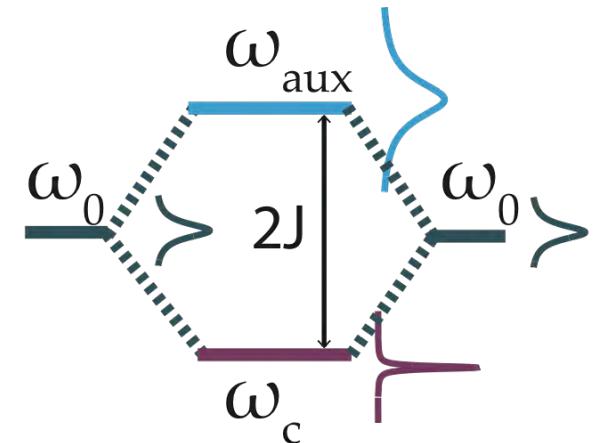
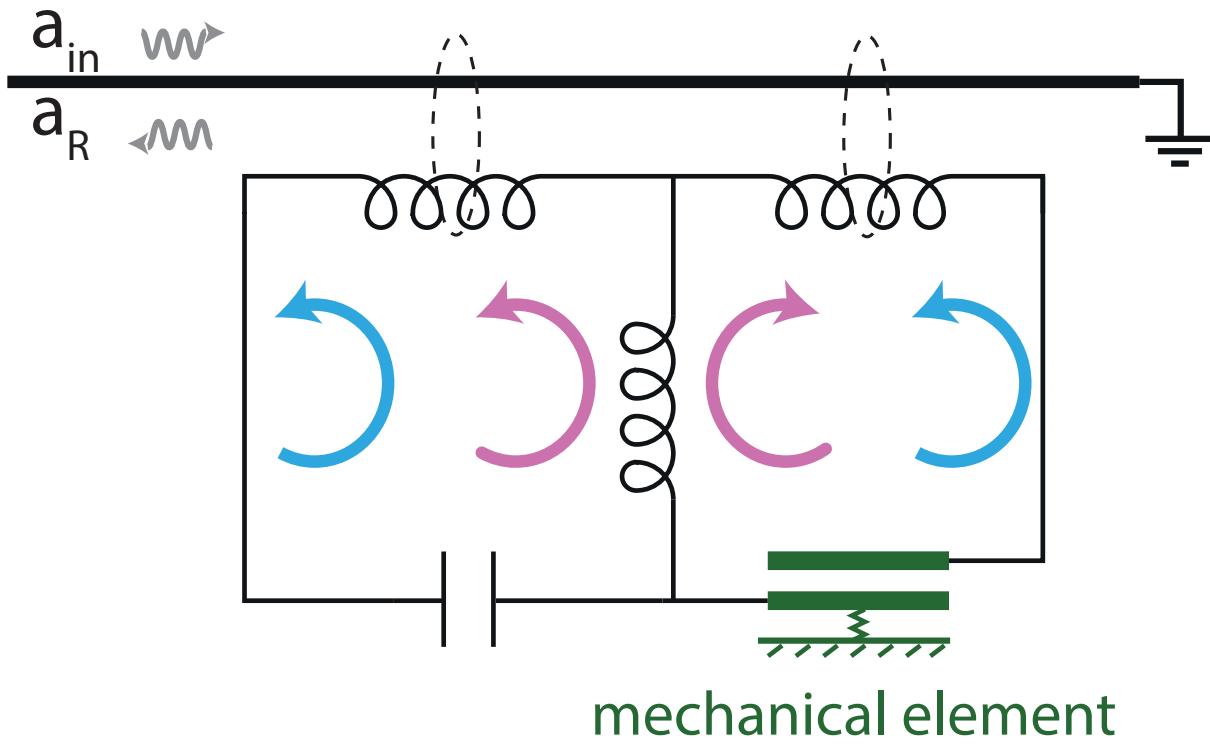
mechanical element



$$\hat{a}_{s,a} = \sqrt{2}^{-1} (\hat{a}_1 \pm \hat{a}_2)$$

$$\begin{aligned} \hat{\mathcal{H}} &= \hbar\omega_0(\hat{a}_1^\dagger\hat{a}_1 + \hat{a}_2^\dagger\hat{a}_2) + \sum_k \hbar\omega_k \hat{c}_k^\dagger\hat{c}_k + \hbar J(\hat{a}_1^\dagger\hat{a}_2 + \text{H.c.}) \\ &+ \hbar \sum_k (g_k^{(1)} \hat{a}_1 \hat{c}_k^\dagger + \text{H.c.}) + \hbar \sum_k (g_k^{(2)} \hat{a}_2 \hat{c}_k^\dagger + \text{H.c.}) \end{aligned}$$

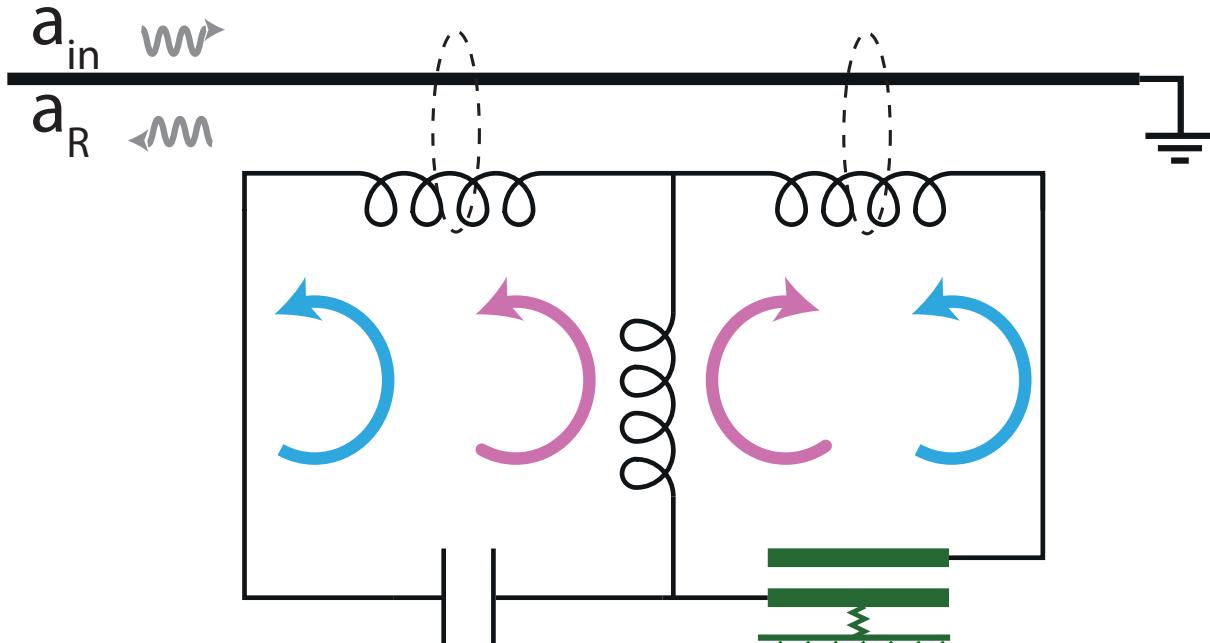
# New approach – hybrid modes



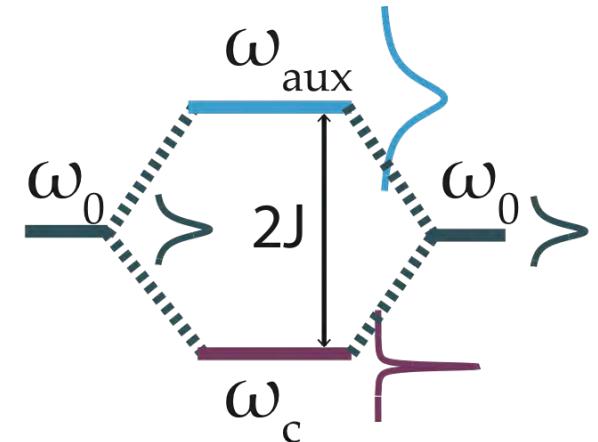
$$\hat{a}_{s,a} = \sqrt{2}^{-1} (\hat{a}_1 \pm \hat{a}_2)$$

$$\begin{aligned} \hat{\mathcal{H}} = & \hbar(\omega_0 + J)\hat{a}_s^\dagger \hat{a}_s + \hbar(\omega_0 - J)\hat{a}_a^\dagger \hat{a}_a + \sum_k \hbar\omega_k \hat{c}_k^\dagger \hat{c}_k \\ & + \hbar \sum_k \left( \frac{g_k^{(1)} + g_k^{(2)}}{\sqrt{2}} \hat{a}_s \hat{c}_k^\dagger + \text{H.c.} \right) + \hbar \sum_k \left( \frac{g_k^{(1)} - g_k^{(2)}}{\sqrt{2}} \hat{a}_a \hat{c}_k^\dagger + \text{H.c.} \right) \end{aligned}$$

# New approach – hybrid modes



mechanical element

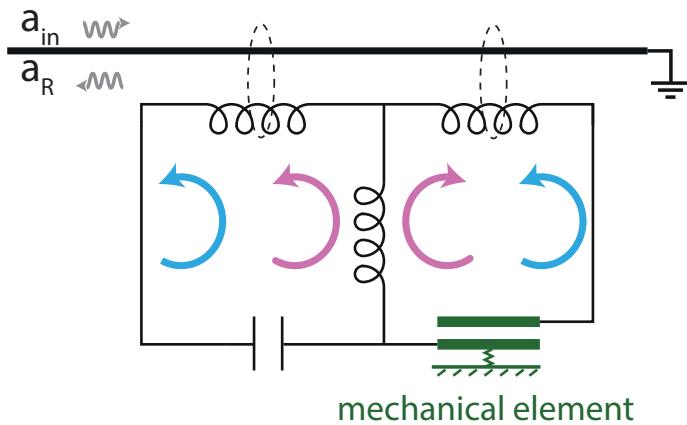


$$\hat{a}_{s,a} = \sqrt{2}^{-1} (\hat{a}_1 \pm \hat{a}_2)$$

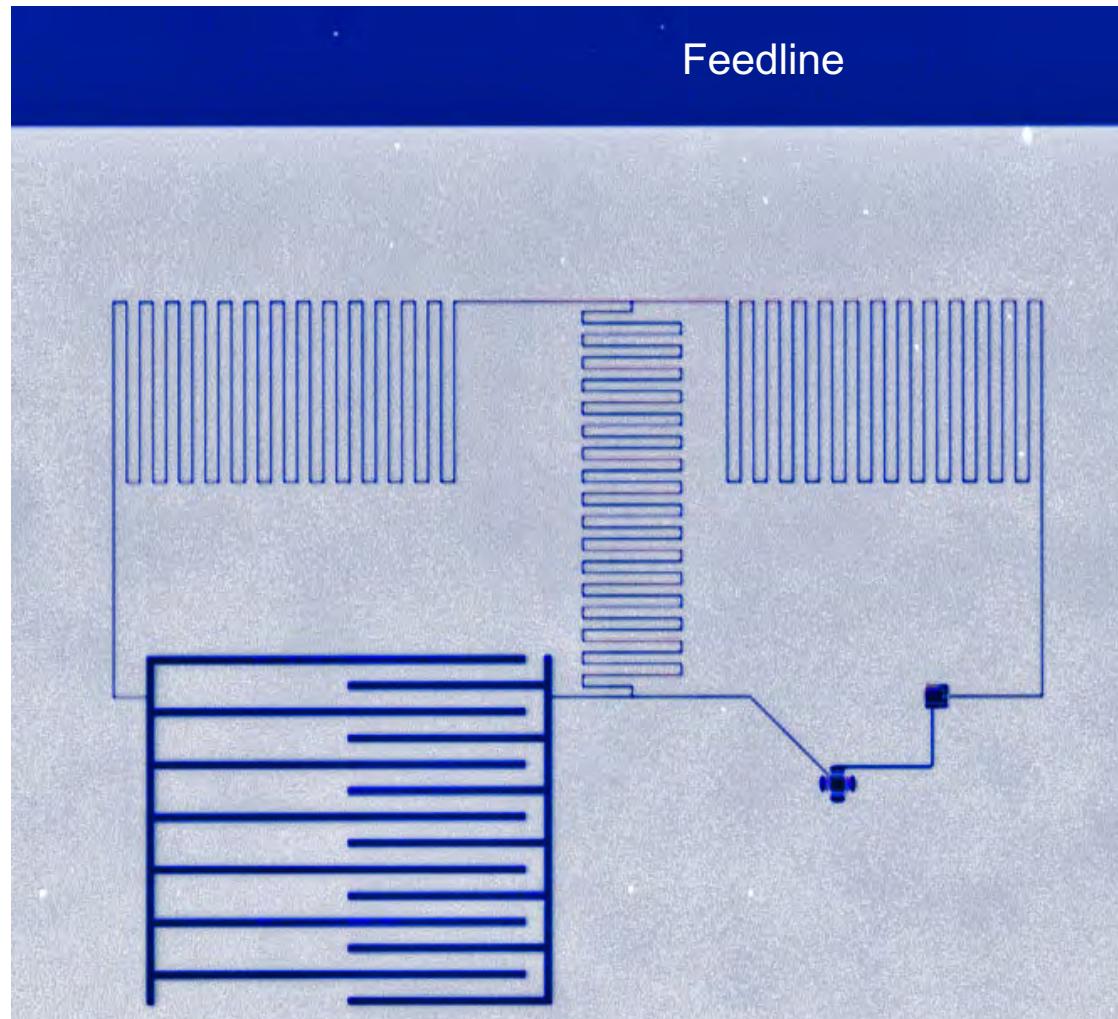
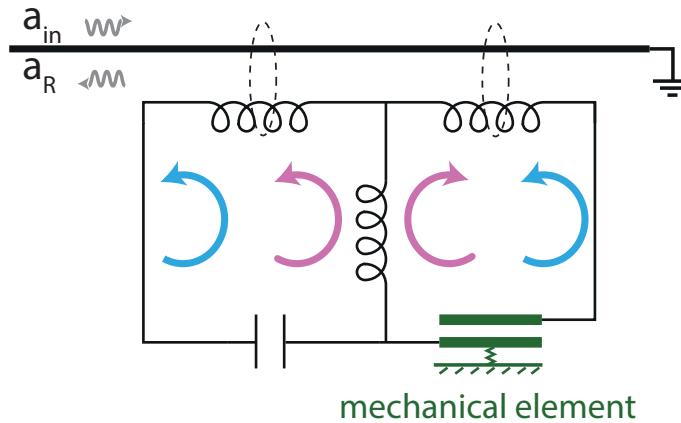
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Bright and dark modes  
due to interference

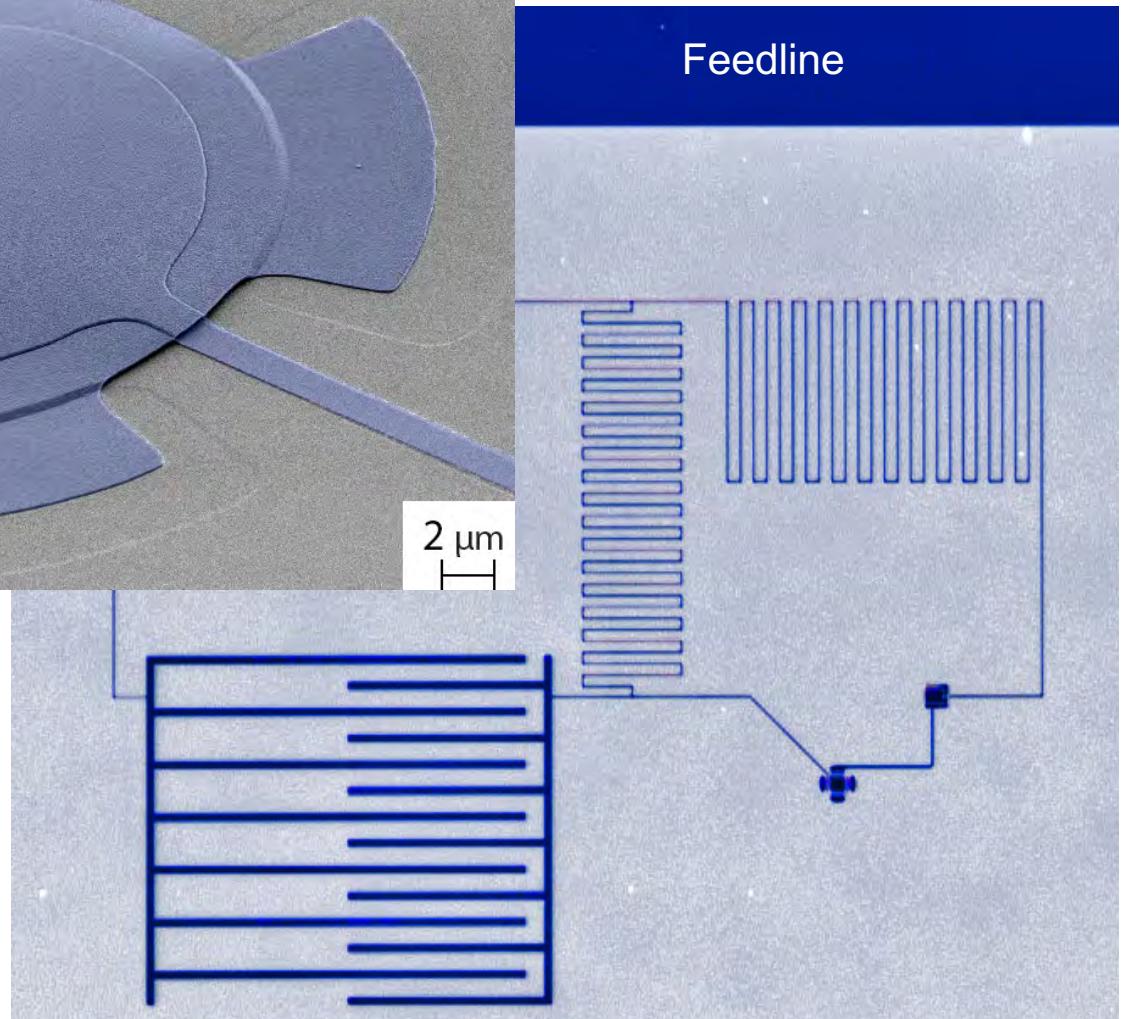
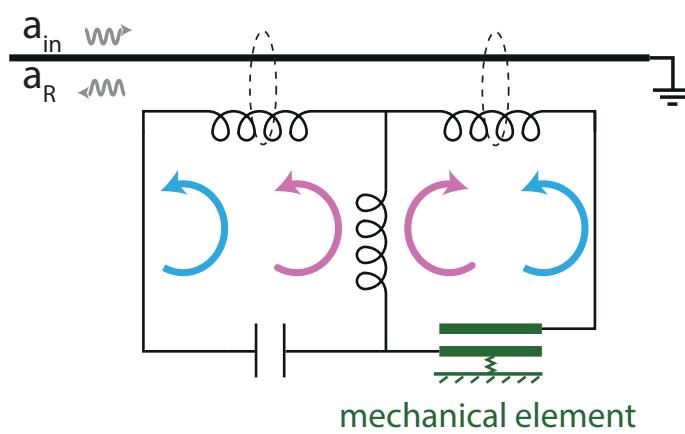
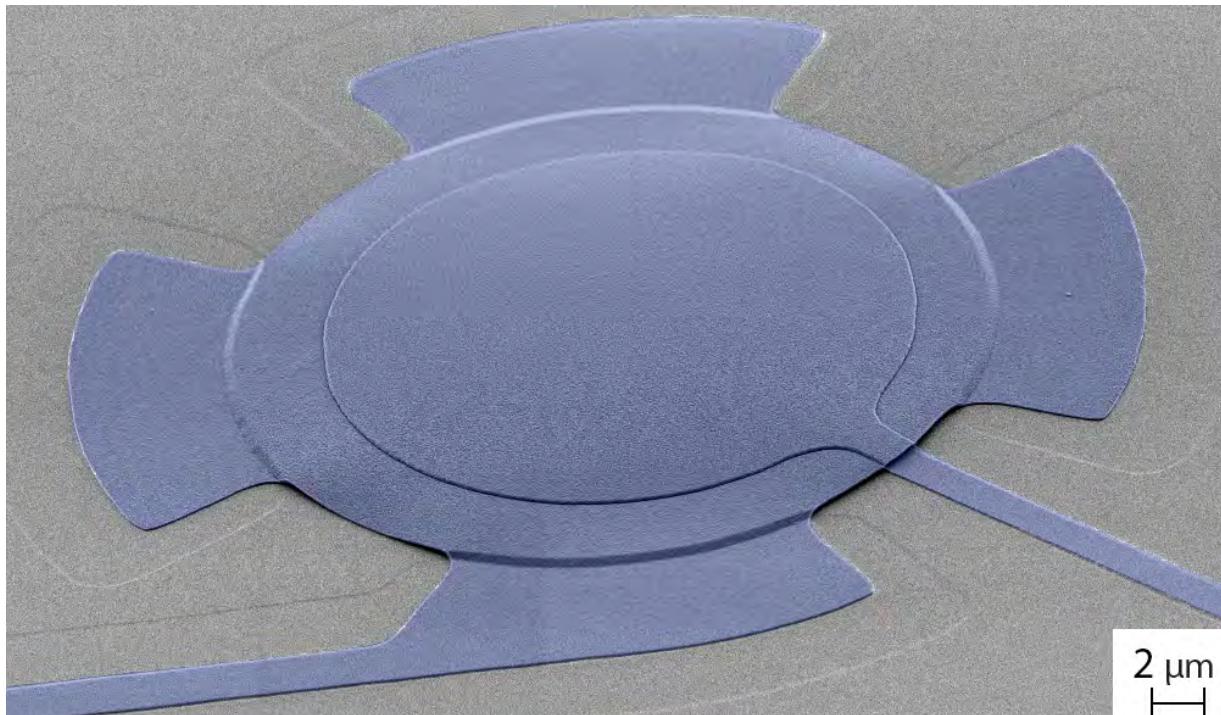
# Circuit layout



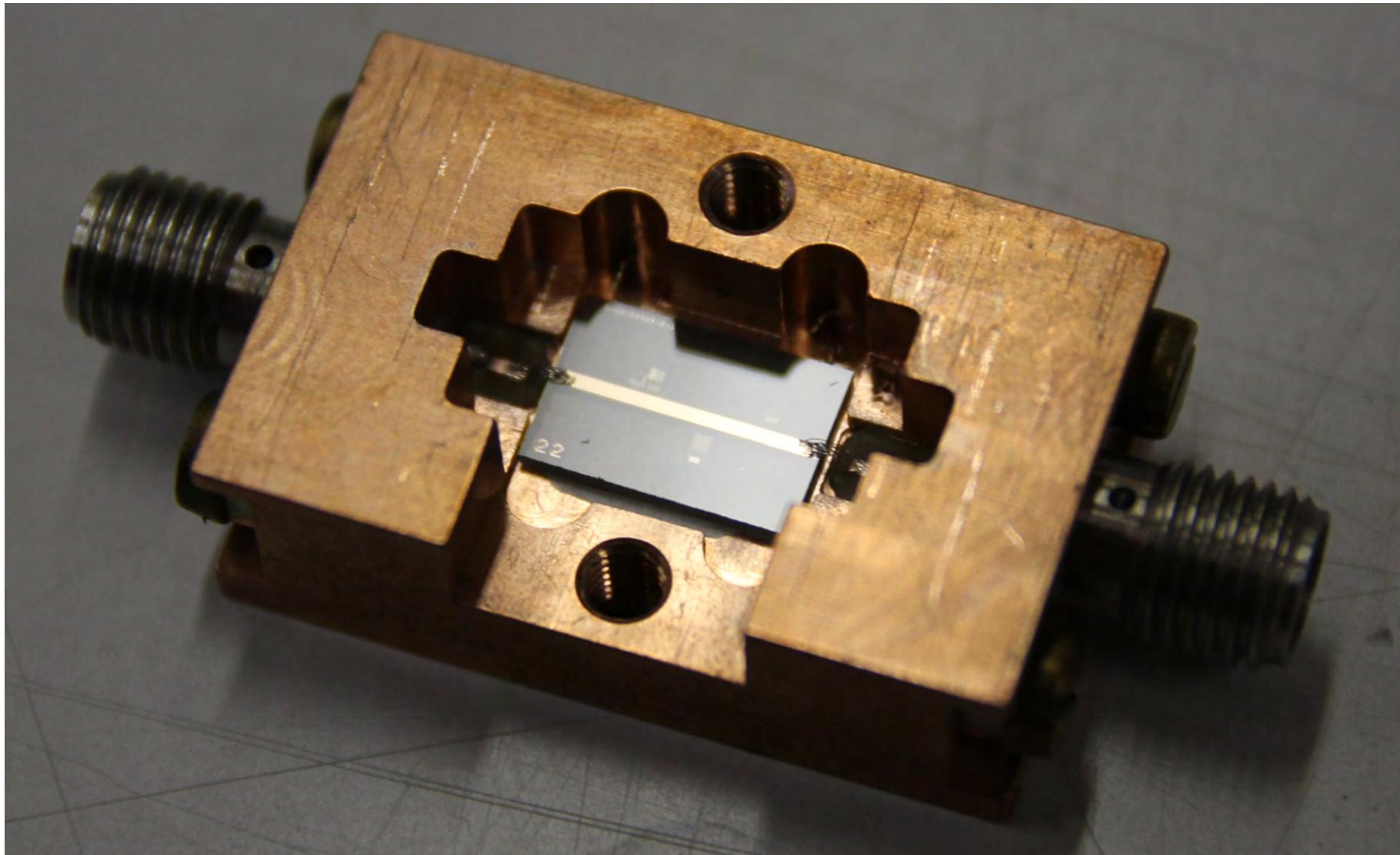
# Circuit layout



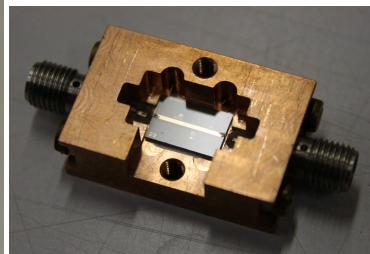
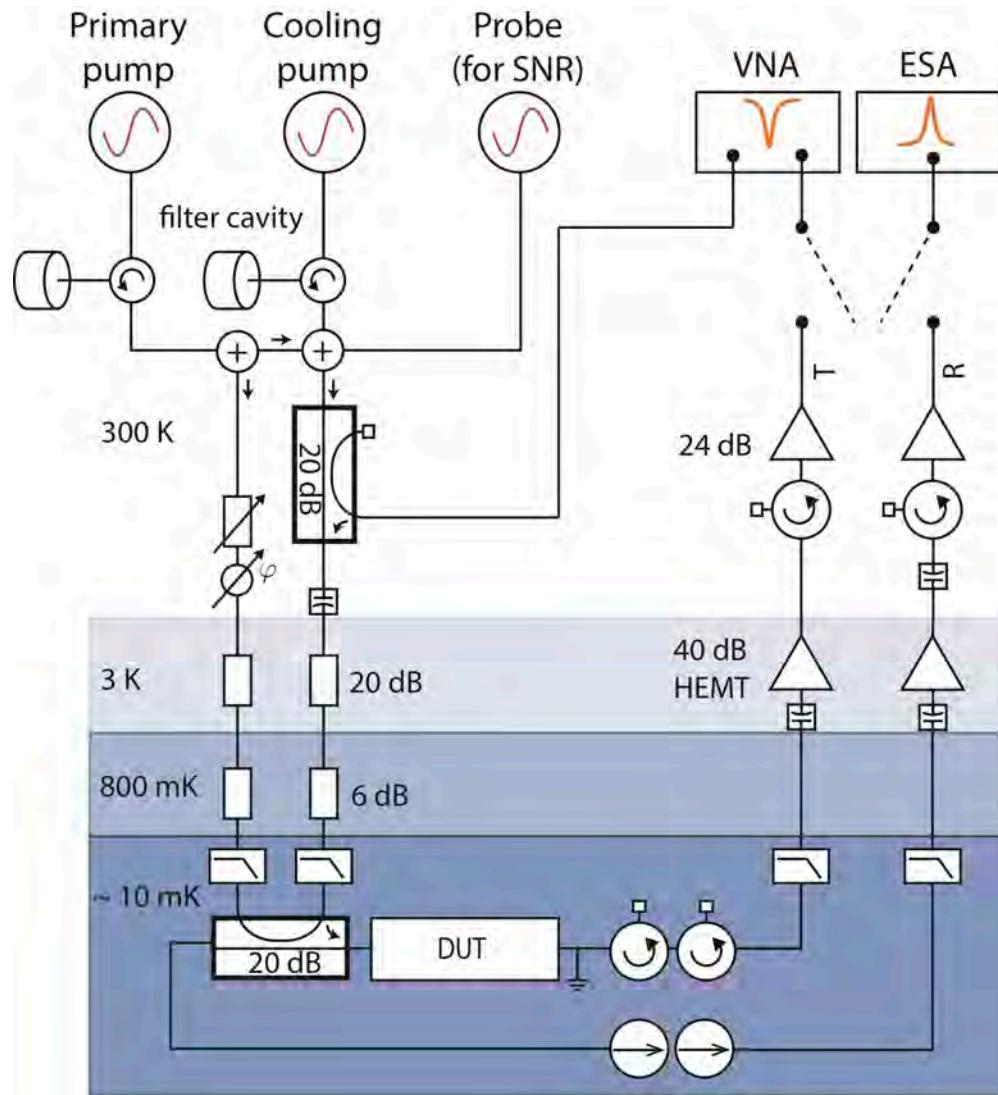
# Circuit layout



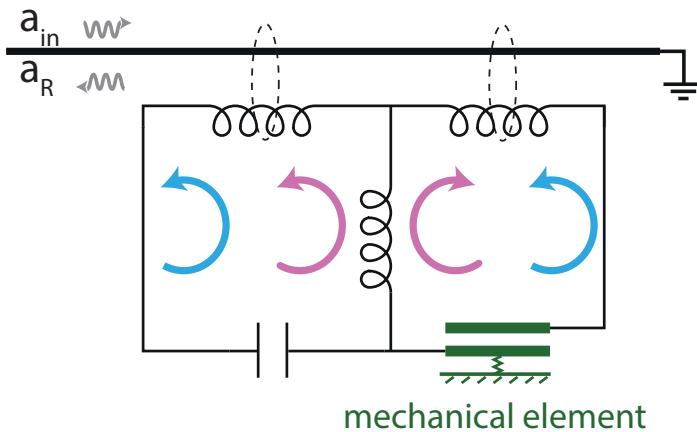
# Measurement setup



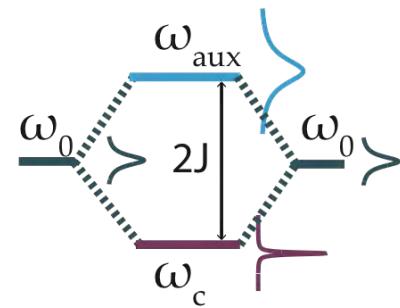
# Measurement setup



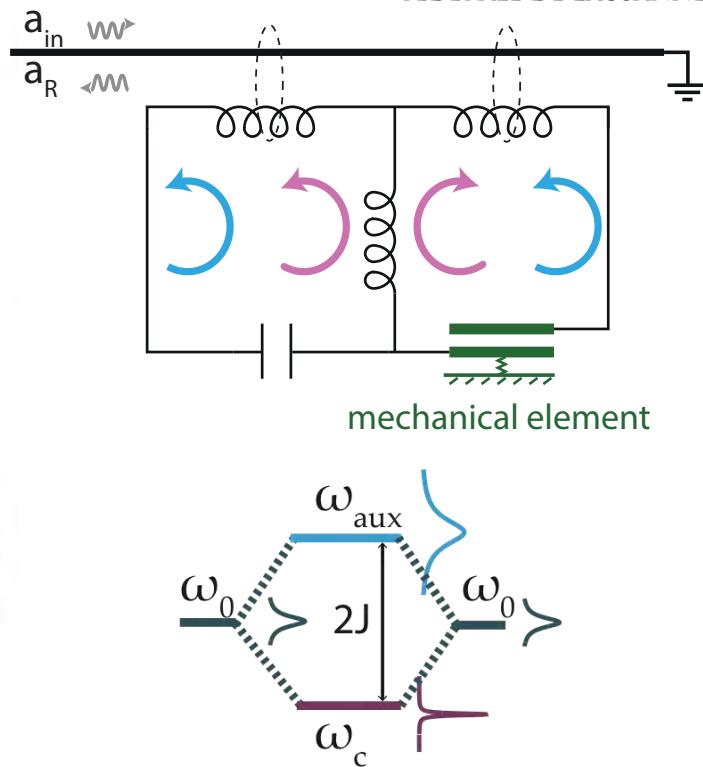
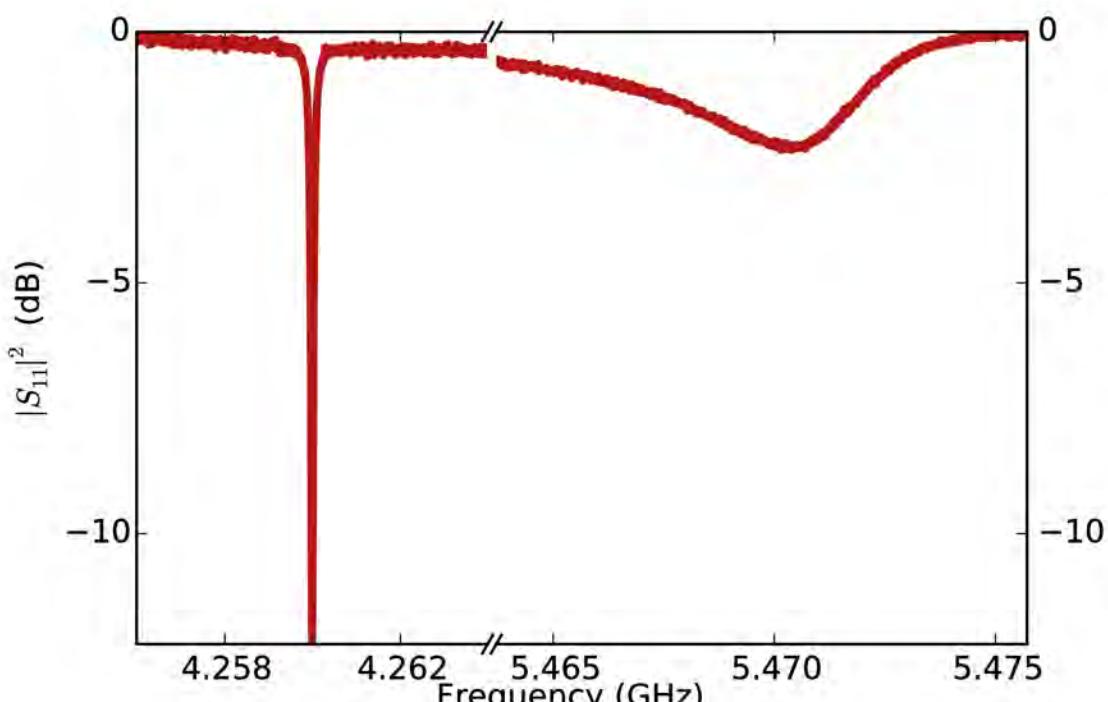
# Device characterization



mechanical element

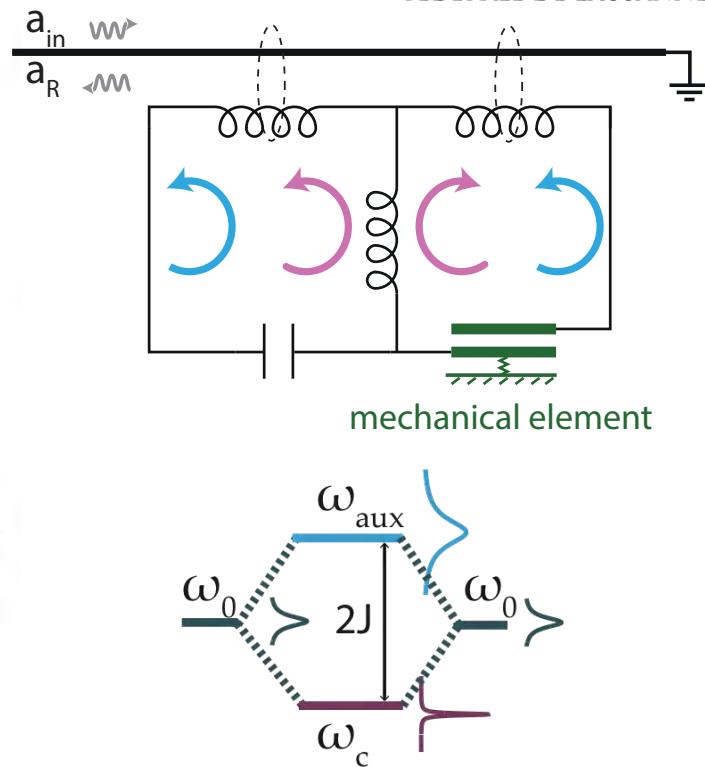
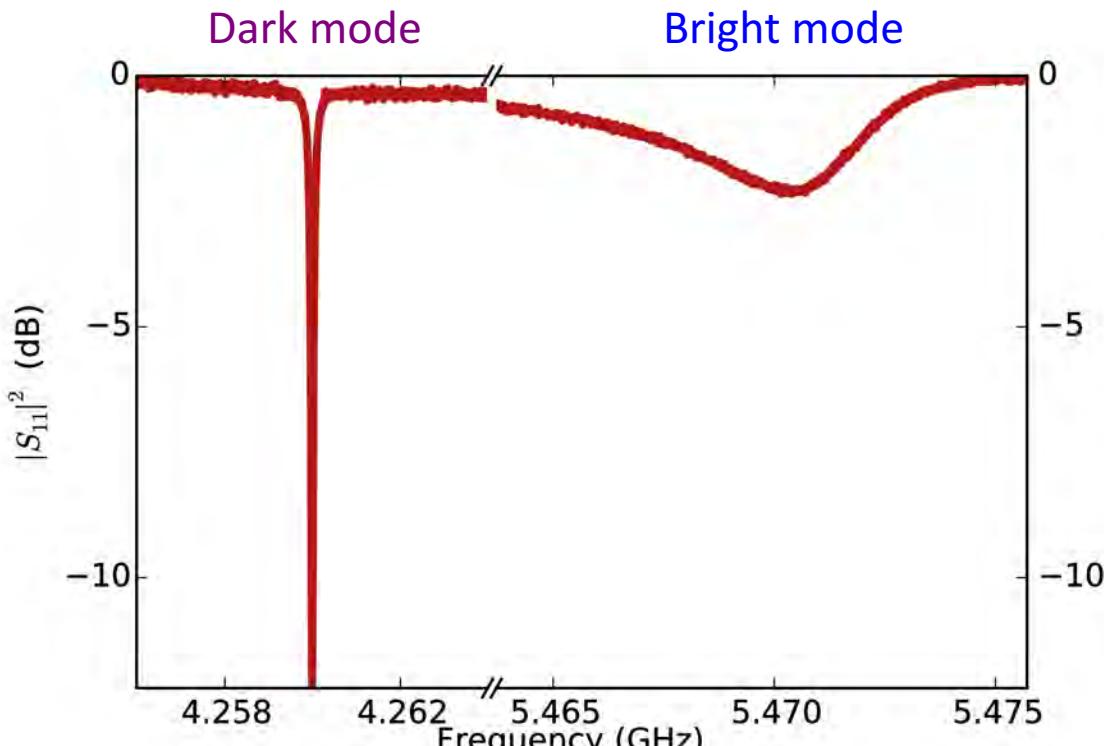


# Device characterization



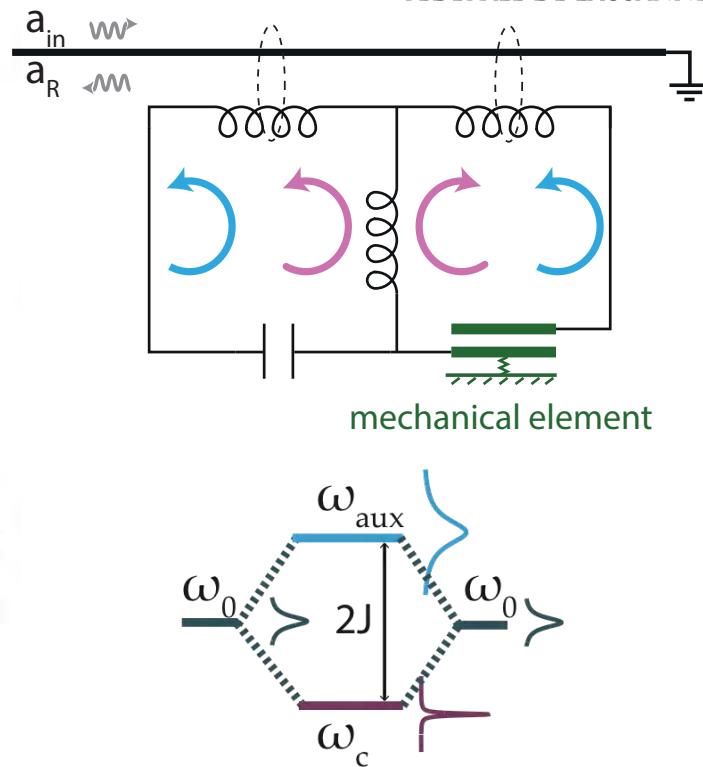
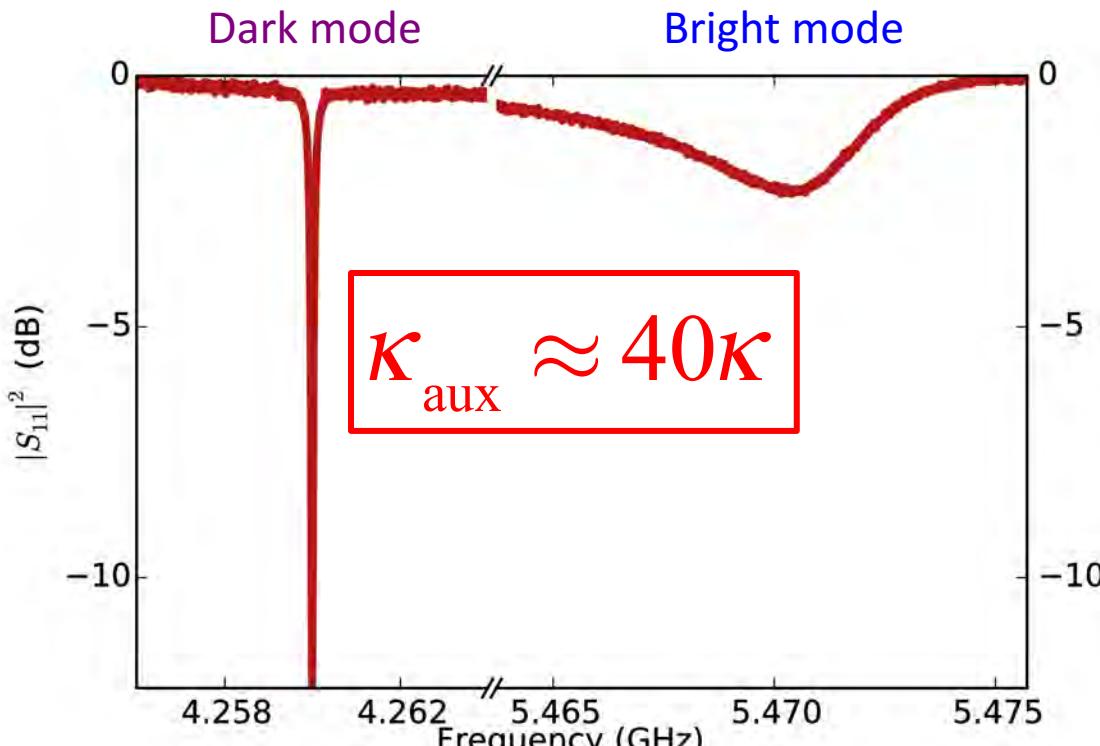
$\omega_c / 2\pi$	$\kappa / 2\pi$	$\omega_{aux} / 2\pi$	$\kappa_{aux} / 2\pi$	$\Omega_m / 2\pi$	$\Gamma_m / 2\pi$	$g_0 / 2\pi$
4.3 GHz	118 kHz	5.4 GHz	4.4 MHz	5 MHz	$\sim 30$ Hz	$\sim 120$ Hz

# Device characterization



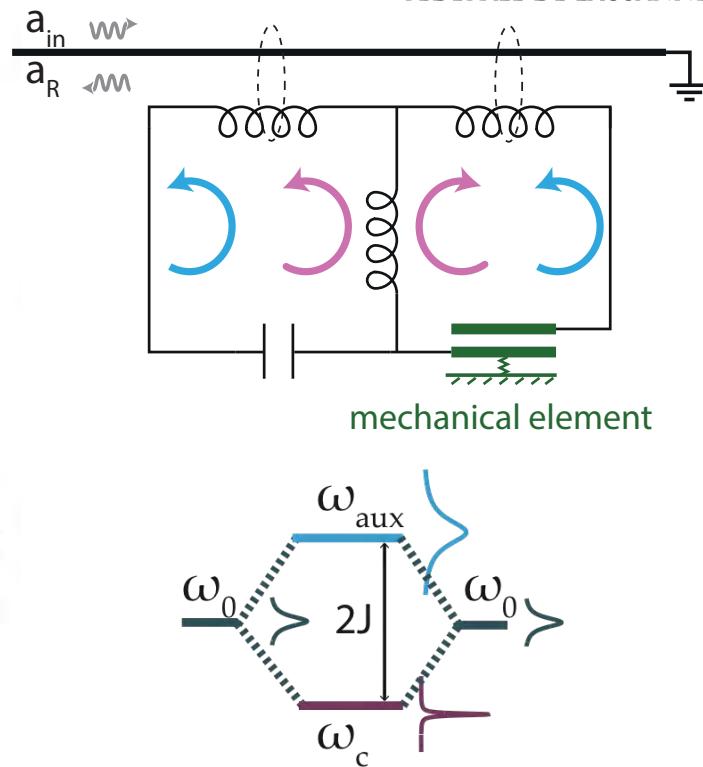
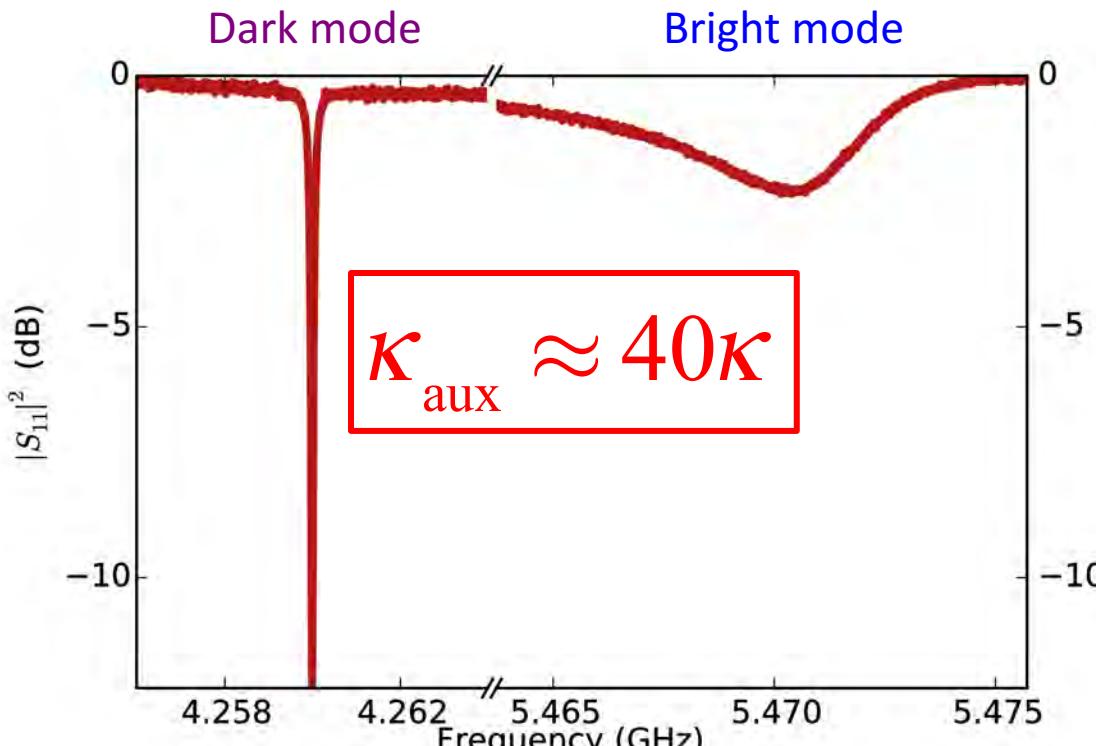
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# Device characterization



$\omega_c / 2\pi$	$\kappa / 2\pi$	$\omega_{\text{aux}} / 2\pi$	$\kappa_{\text{aux}} / 2\pi$	$\Omega_m / 2\pi$	$\Gamma_m / 2\pi$	$g_0 / 2\pi$
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# Device characterization

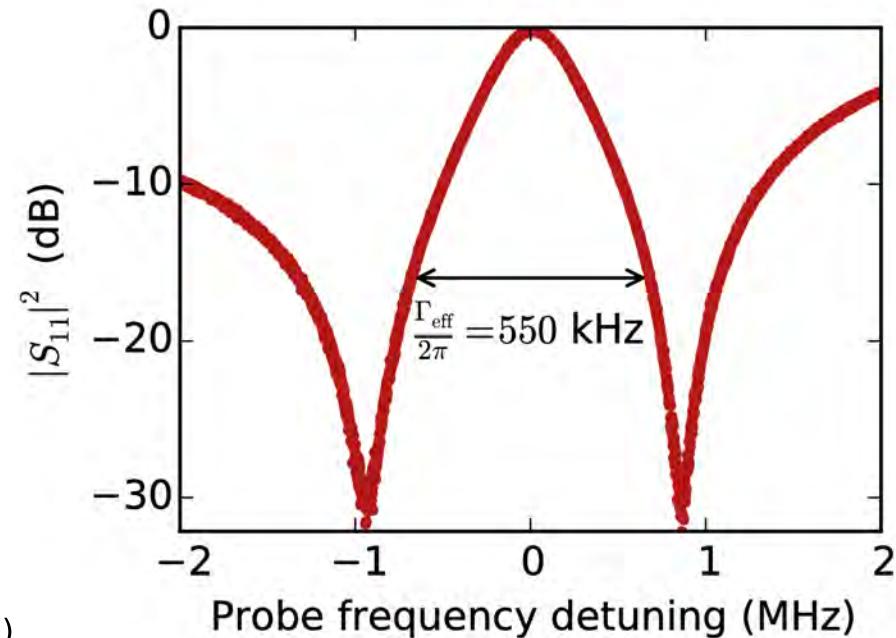
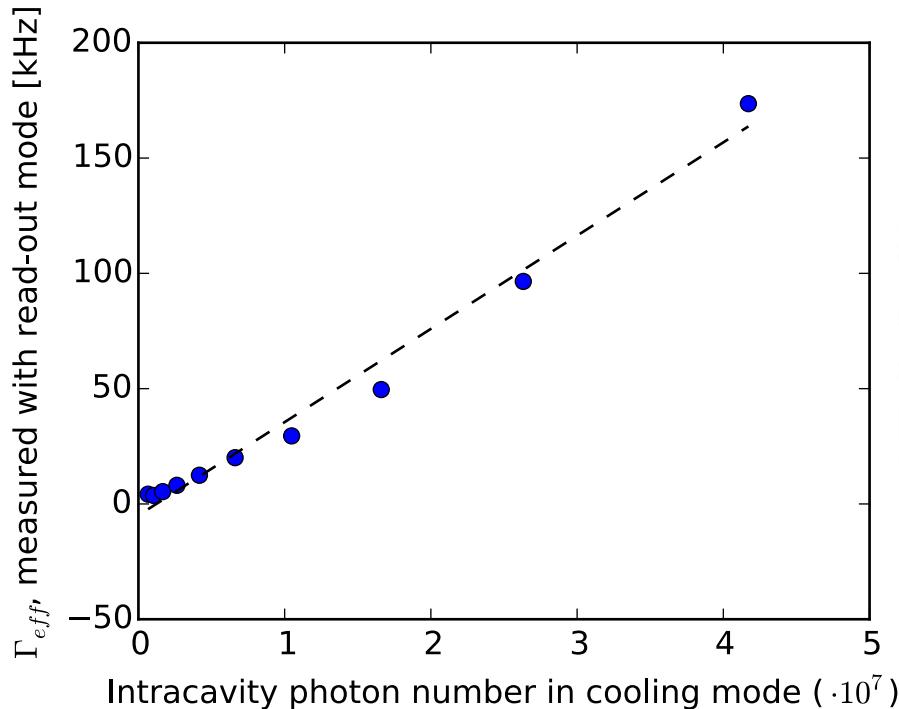


$\omega_c / 2\pi$	$\kappa / 2\pi$	$\omega_{\text{aux}} / 2\pi$	$\kappa_{\text{aux}} / 2\pi$	$\Omega_m / 2\pi$	$\Gamma_m / 2\pi$	$g_0 / 2\pi$
4.3 GHz	118 kHz	5.4 GHz	4.4 MHz	5 MHz	$\sim 30$ Hz	$\sim 120$ Hz

With these parameters we can easily damp the mechanics to  $\Gamma_{\text{eff}} \sim 2\pi \times 550$  kHz  $\approx 5\kappa$

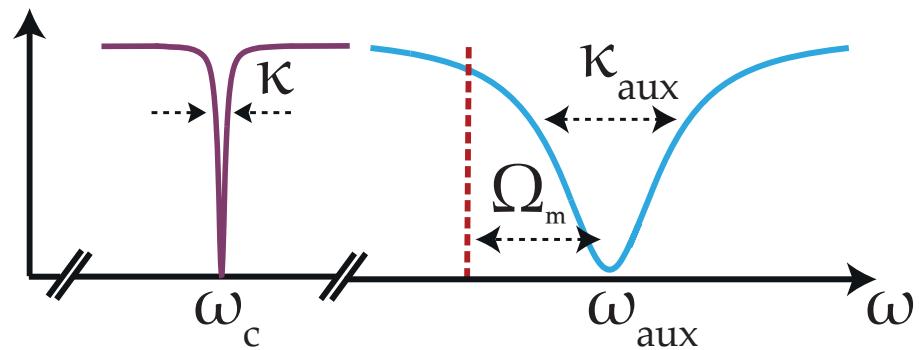
$$\Omega_m \gg \Gamma_{\text{eff}} \gg \kappa$$

# Preparation of a dissipative reservoir



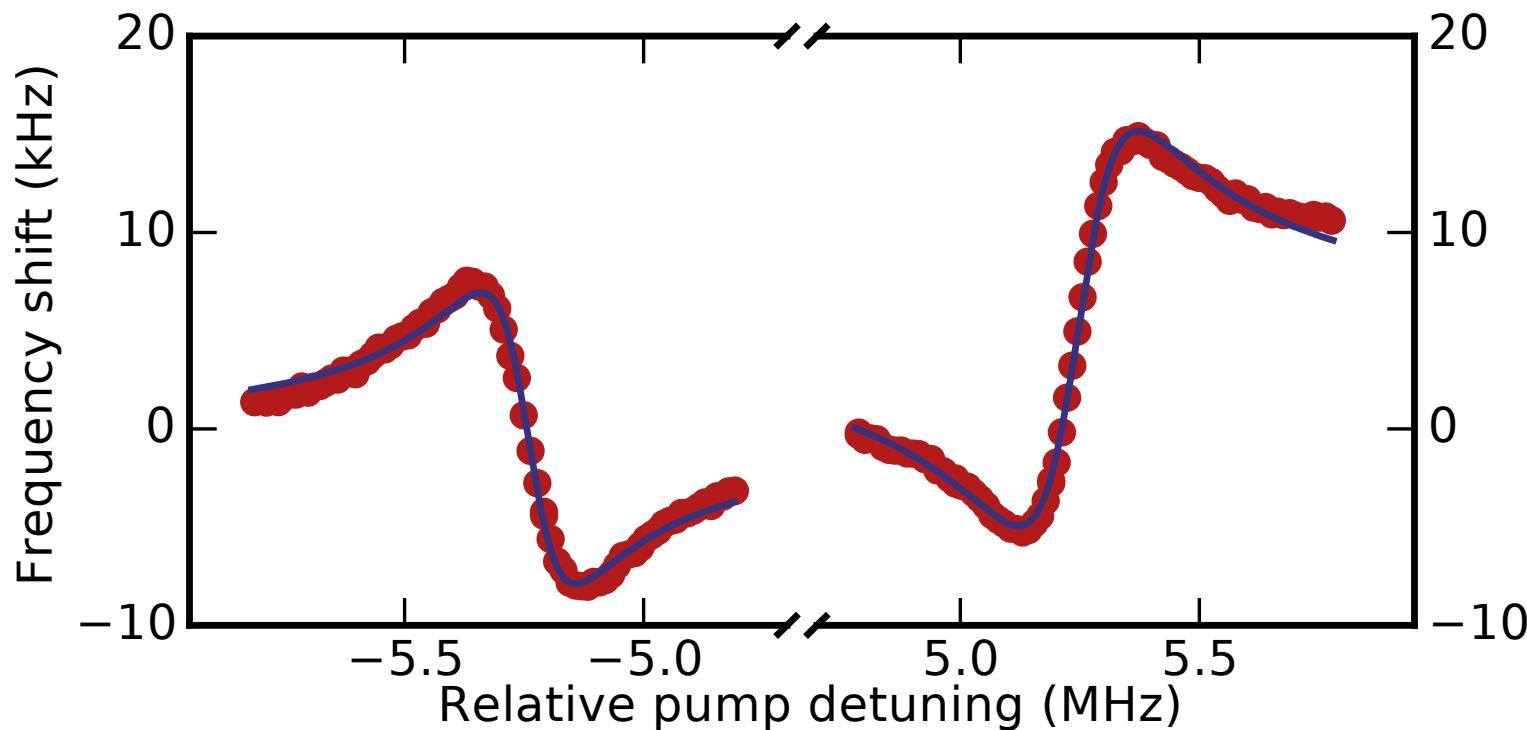
- Prepare of a dissipative reservoir by increasing  $\Gamma_{\text{eff}} / 2\pi$  to 550 kHz
- Create close to Markovian dissipative bath for electromagnetic mode

$$\Omega_m \gg \Gamma_{\text{eff}} \gg \kappa$$

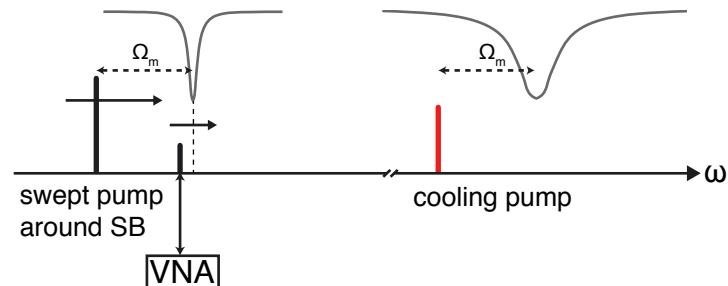


# “Mechanical” spring effect

Fix pump power (5 dBm) and sweep detuning

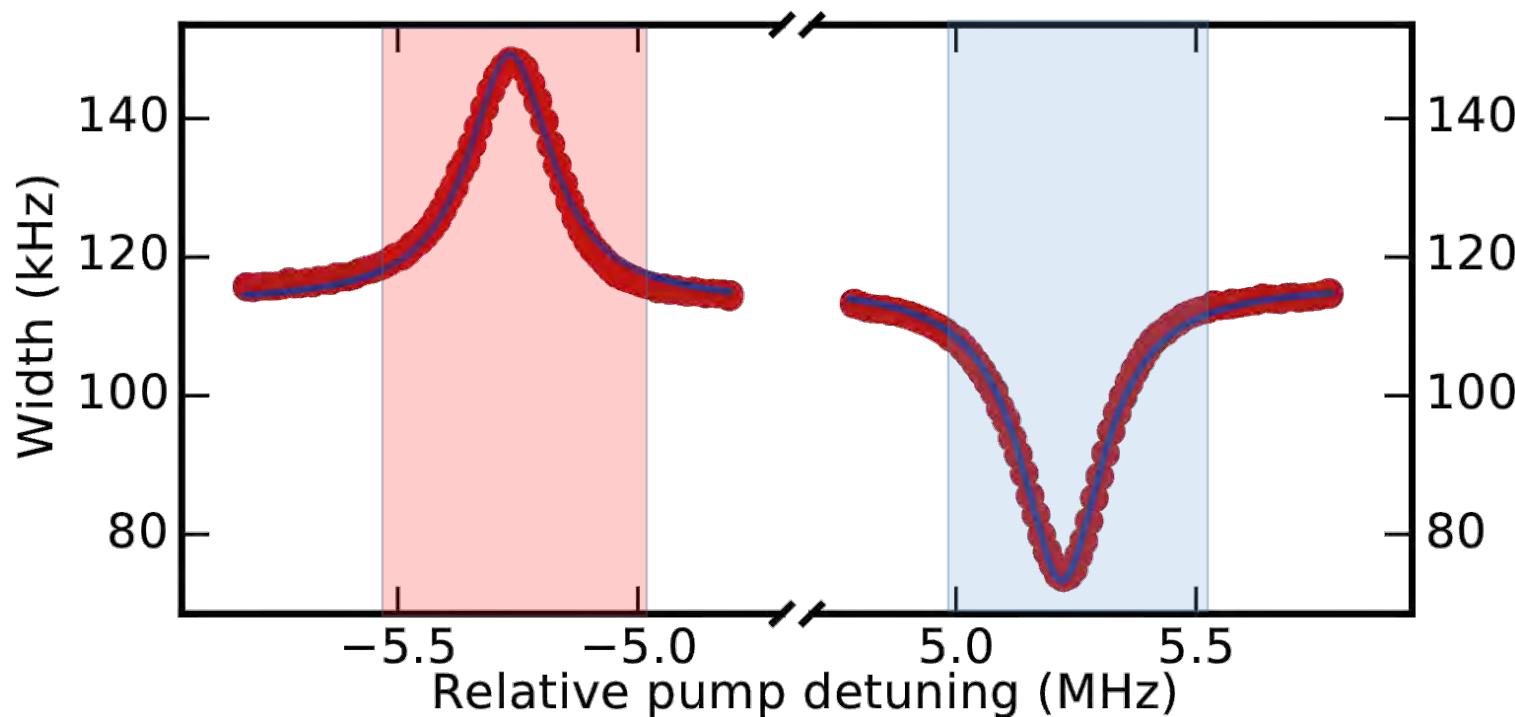


$$\Delta\omega_{OM} = \frac{\Gamma_{\text{eff}} g_0^2 n_p (\Delta - \Omega_m)}{(\Gamma_{\text{eff}} / 2)^2 + (\Delta + \Omega_m)^2} - \frac{\Gamma_{\text{eff}} g_0^2 n_p (\Delta + \Omega_m)}{(\Gamma_{\text{eff}} / 2)^2 + (\Delta - \Omega_m)^2}$$

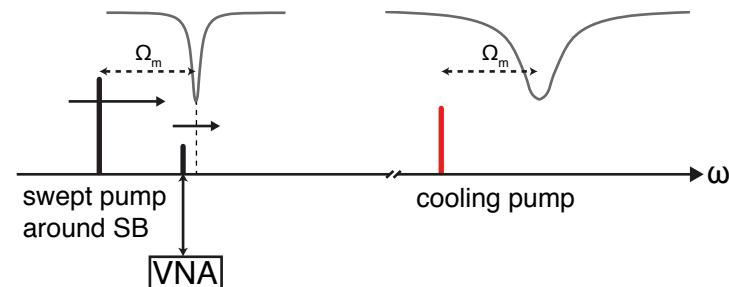


# Electromagnetic dynamical backaction

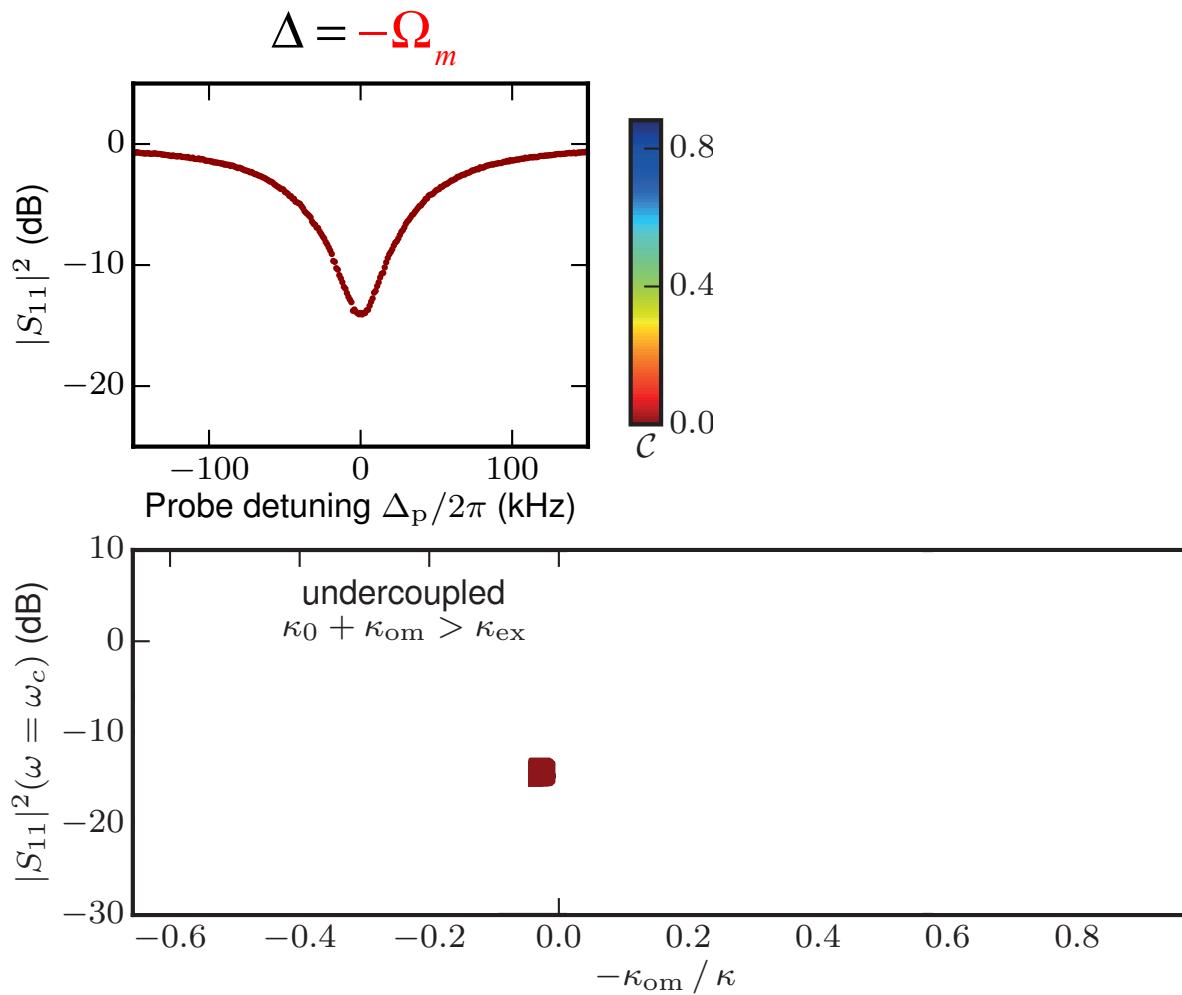
Fix pump power (5 dBm) and sweep detuning



$$\kappa_{om} = \frac{\Gamma_{\text{eff}} g_0^2 n_p}{(\Gamma_{\text{eff}} / 2)^2 + (\Delta + \Omega_m)^2} - \frac{\Gamma_{\text{eff}} g_0^2 n_p}{(\Gamma_{\text{eff}} / 2)^2 + (\Delta - \Omega_m)^2}$$



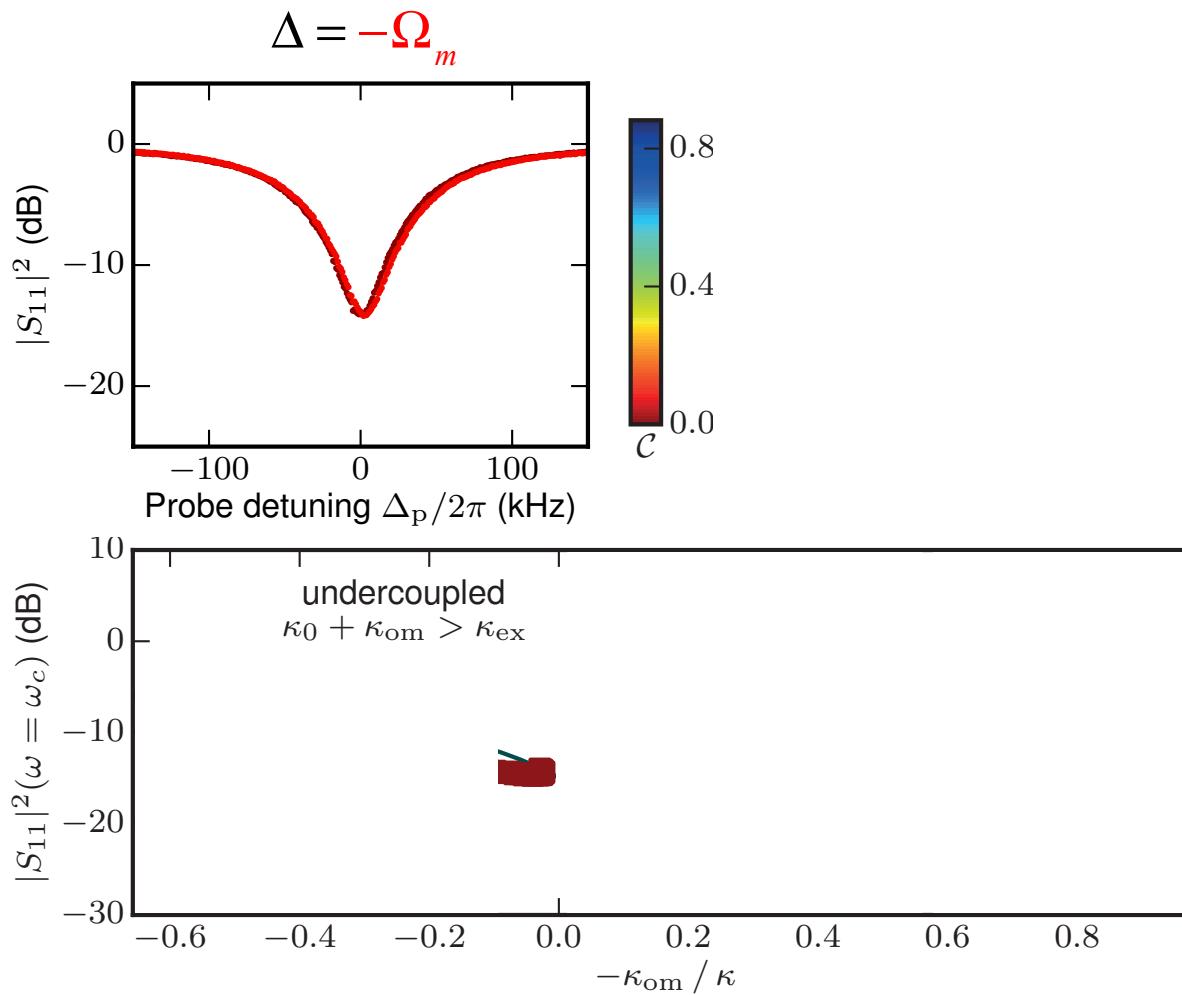
# (De)amplification by mechanical reservoir engineering



$$\kappa_{\text{om}} = \pm \mathcal{C} \kappa$$

$$S_{11}(\omega = \omega_0) = \frac{\kappa_0 - \kappa_{\text{ex}} + \kappa_{\text{om}}}{\kappa_0 + \kappa_{\text{ex}} + \kappa_{\text{om}}}$$

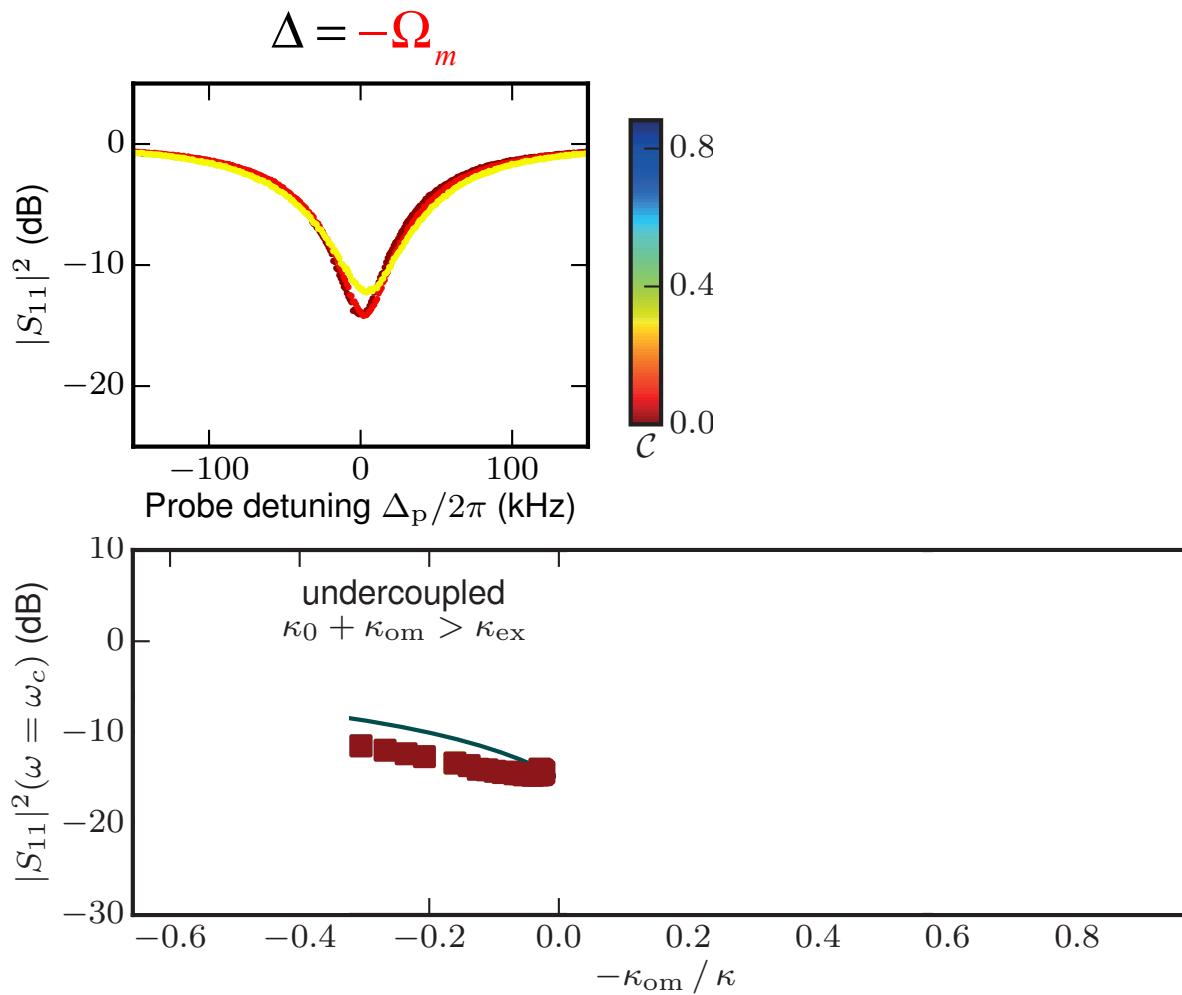
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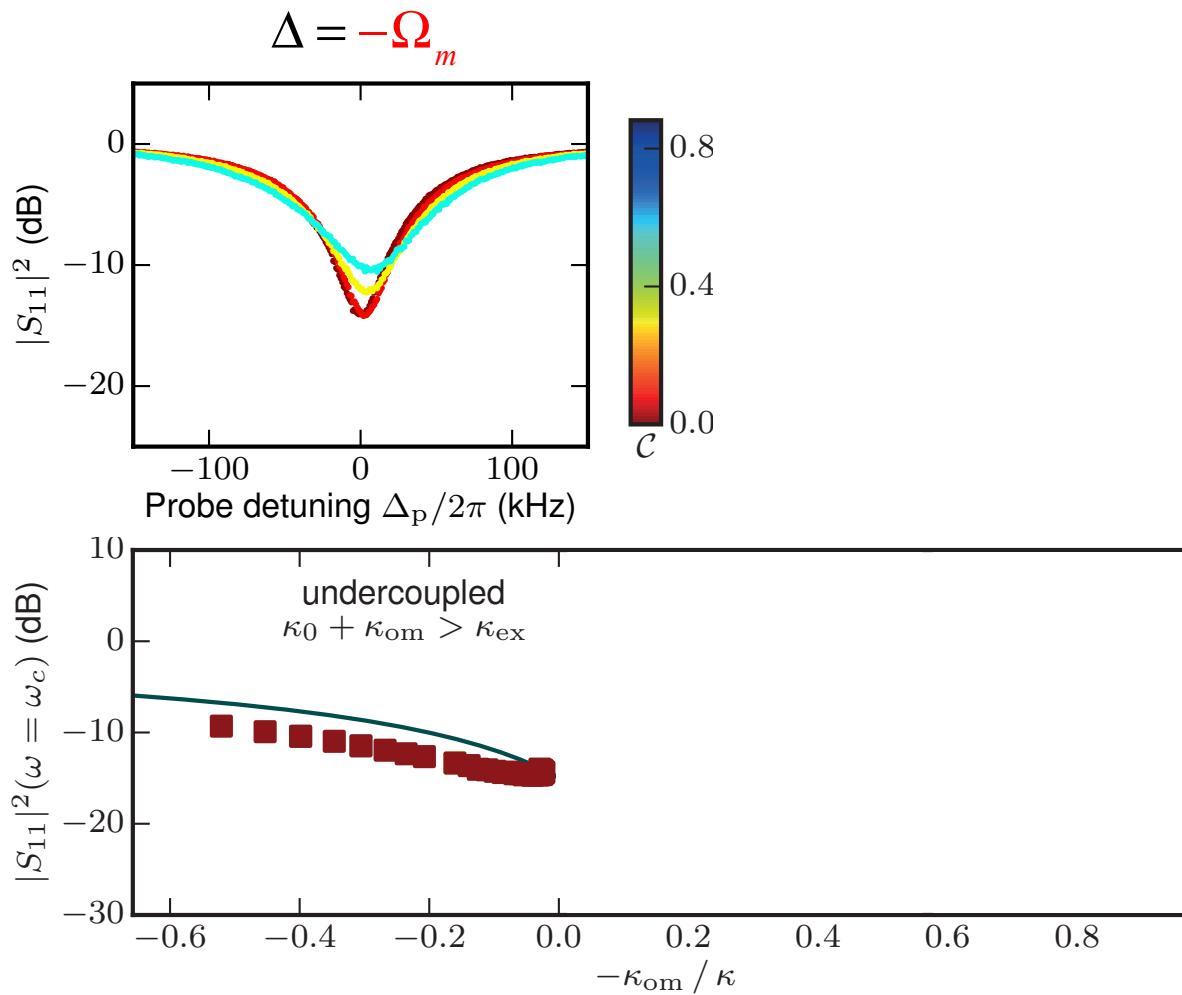
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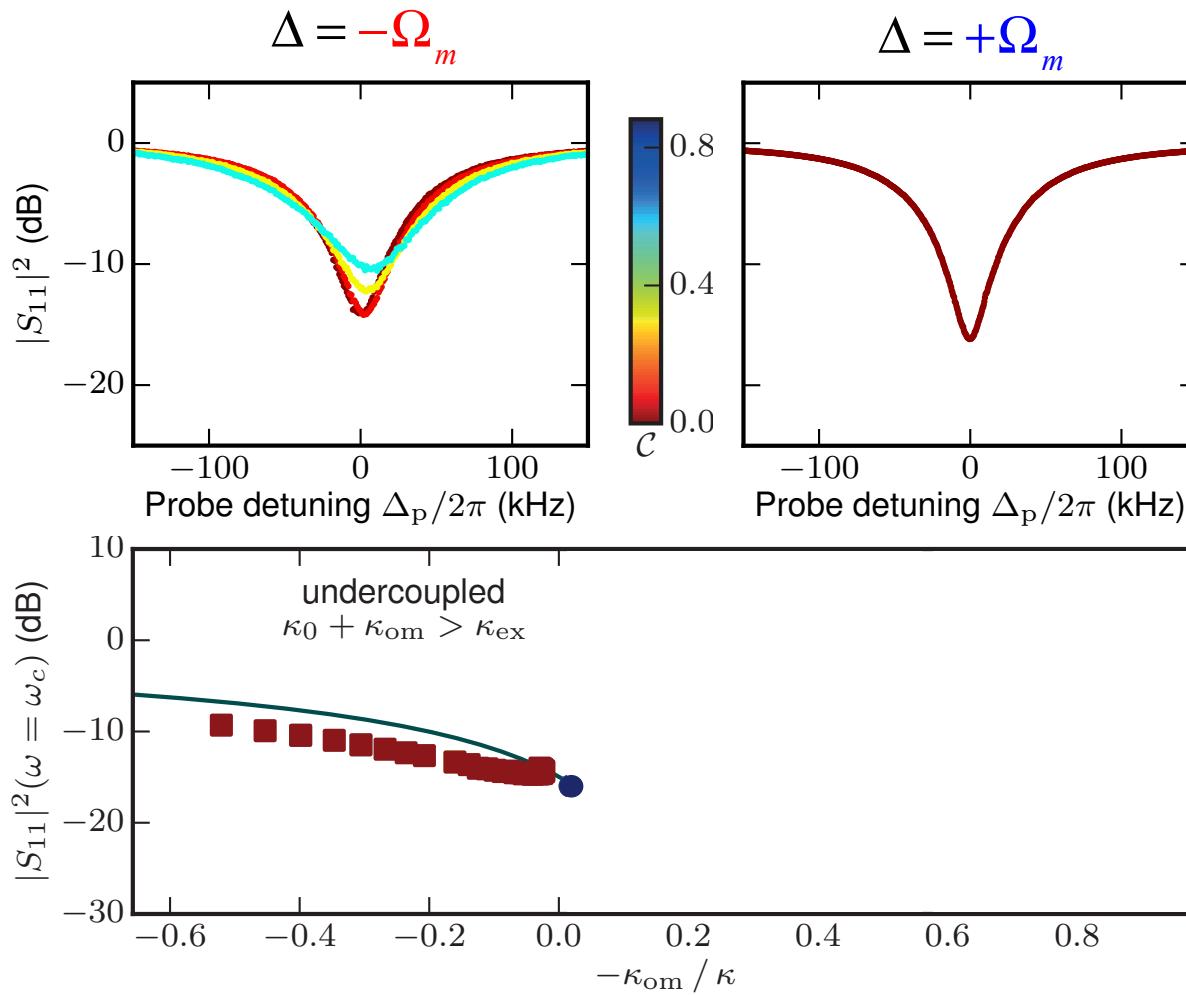
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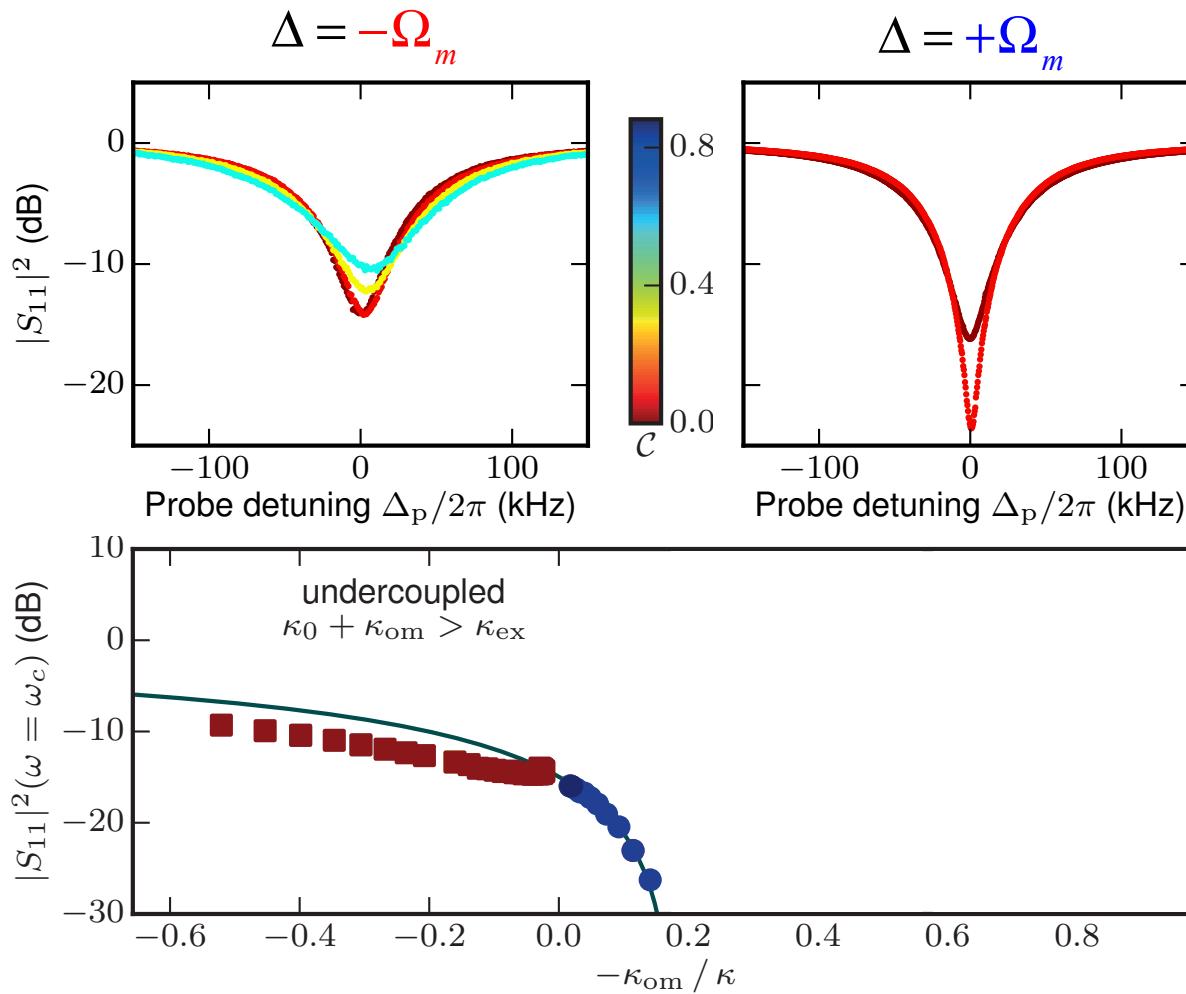
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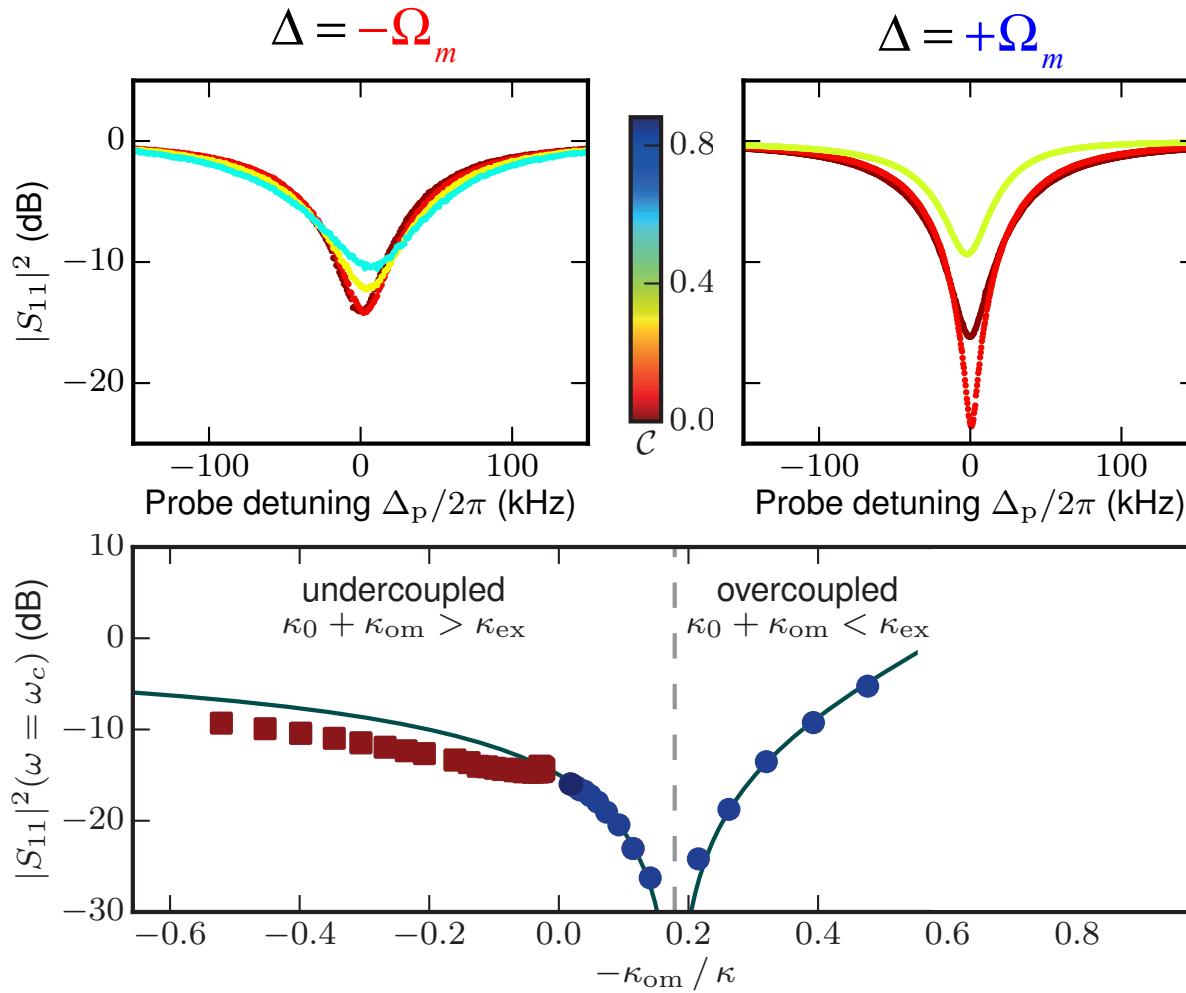
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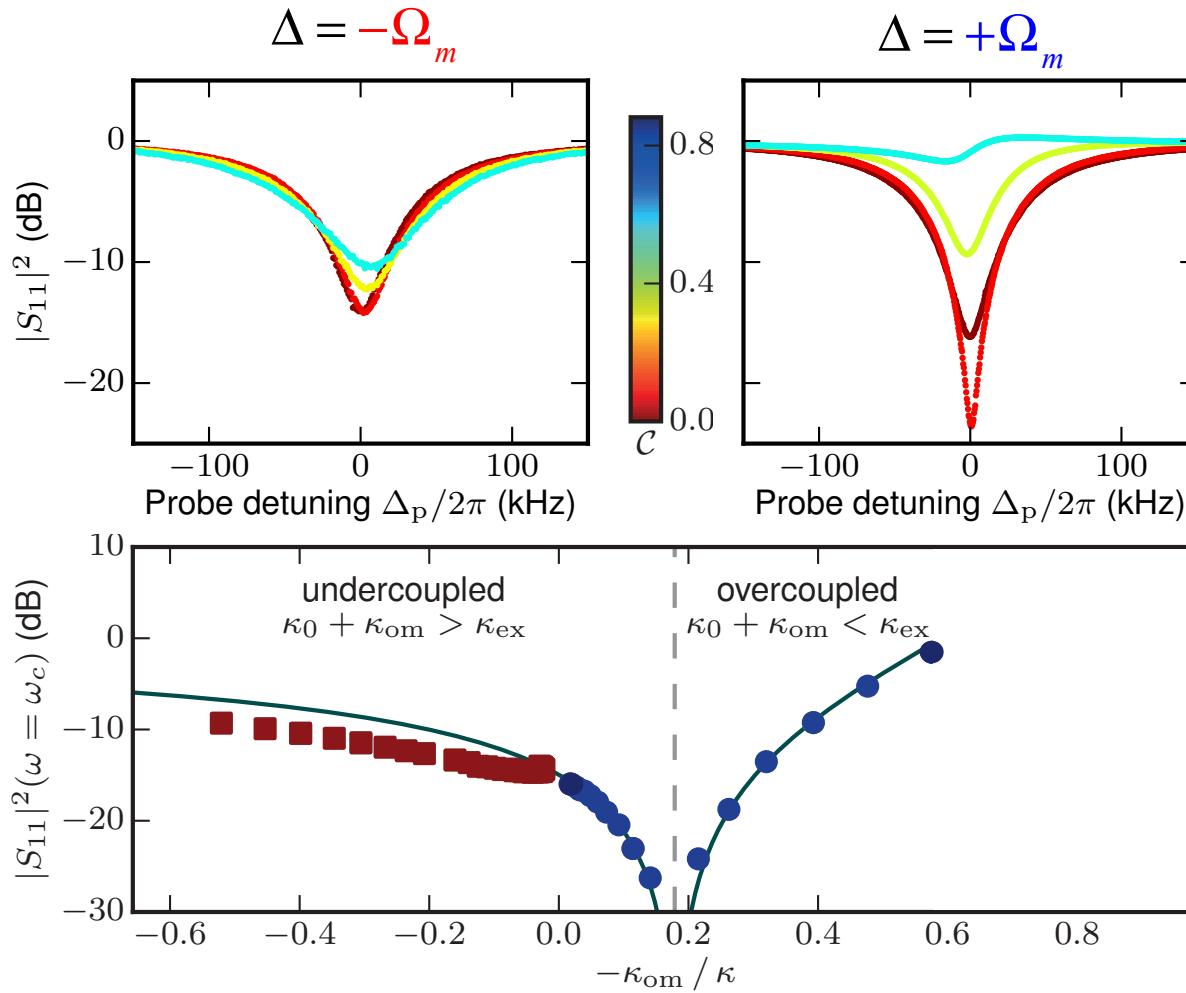
# (De)amplification by mechanical reservoir engineering



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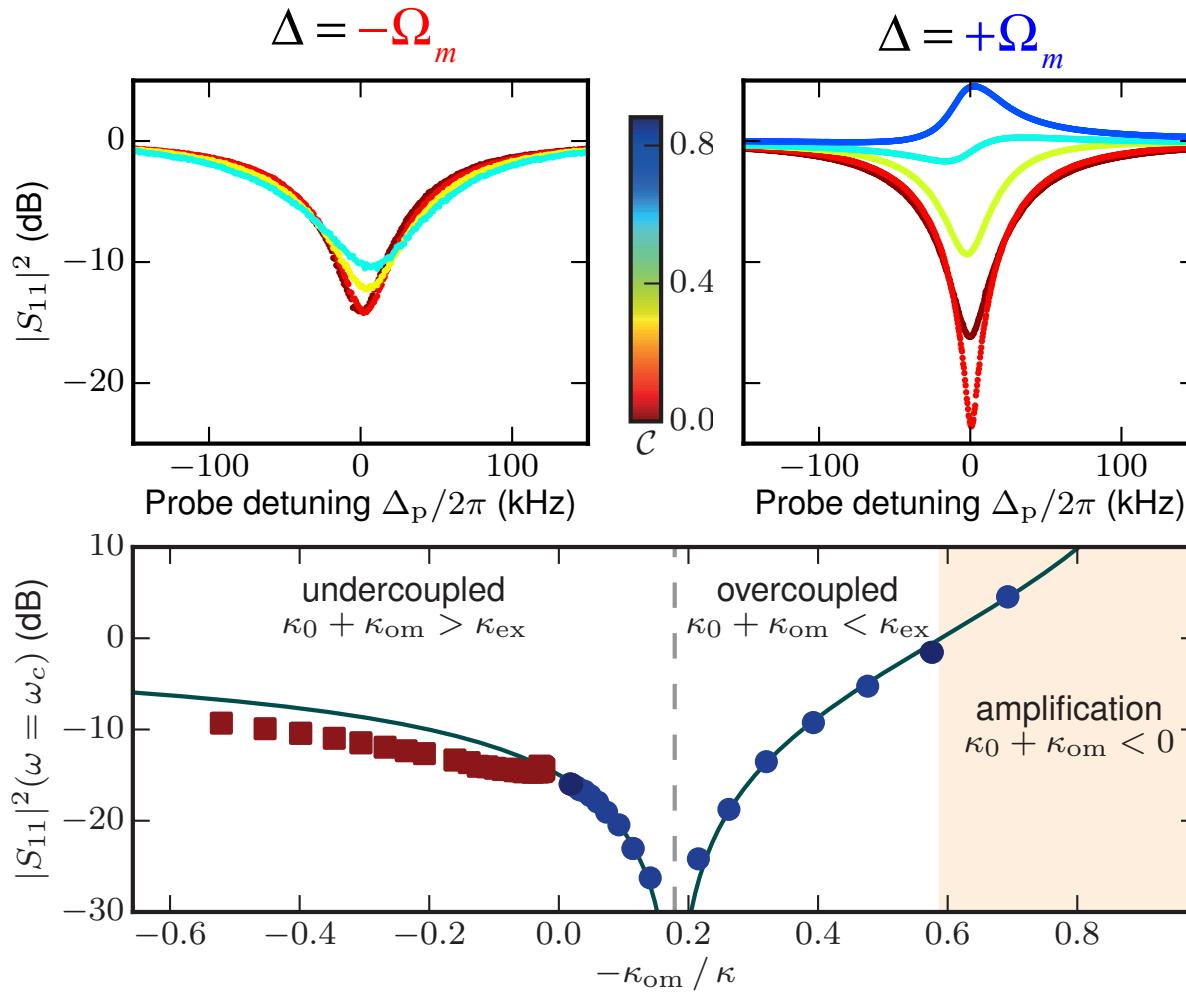
# (De)amplification by mechanical reservoir engineering



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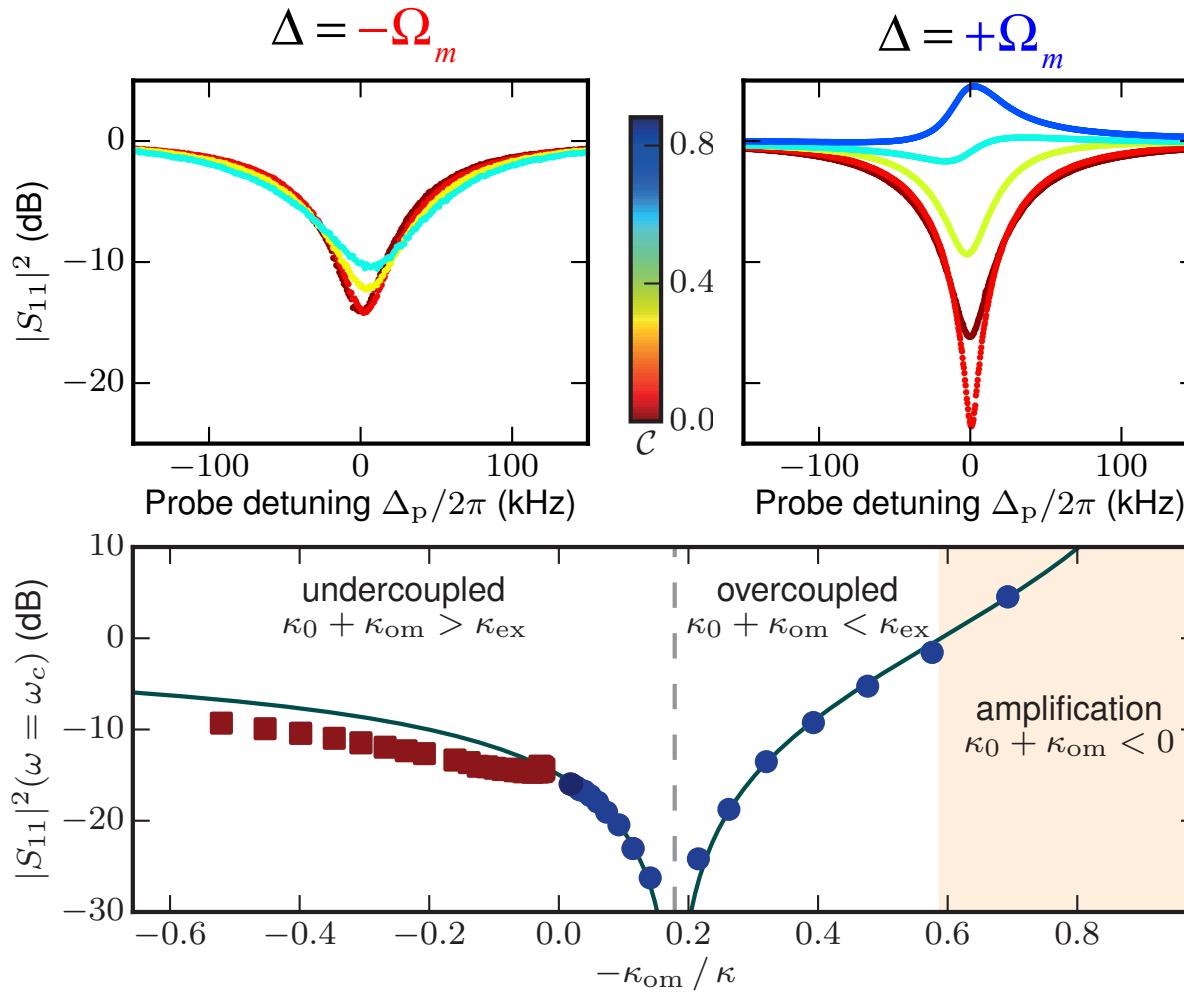
# (De)amplification by mechanical reservoir engineering



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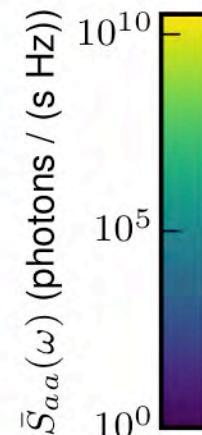
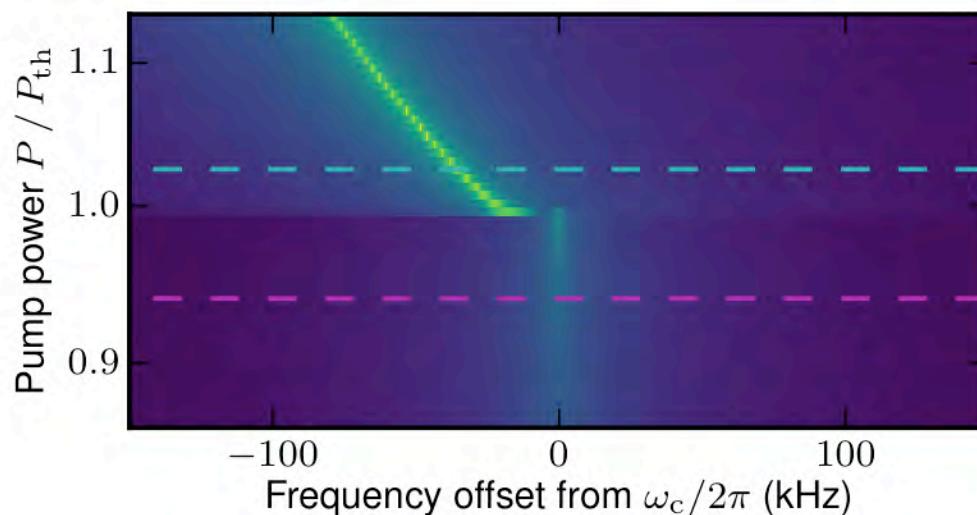
# (De)amplification by mechanical reservoir engineering



$$\kappa_{\text{om}} = \pm C \kappa$$

Demonstrates electromagnetic control over the *cavity damping rate*, via mechanical dissipative reservoir

# Maser using a mechanical dissipative reservoir



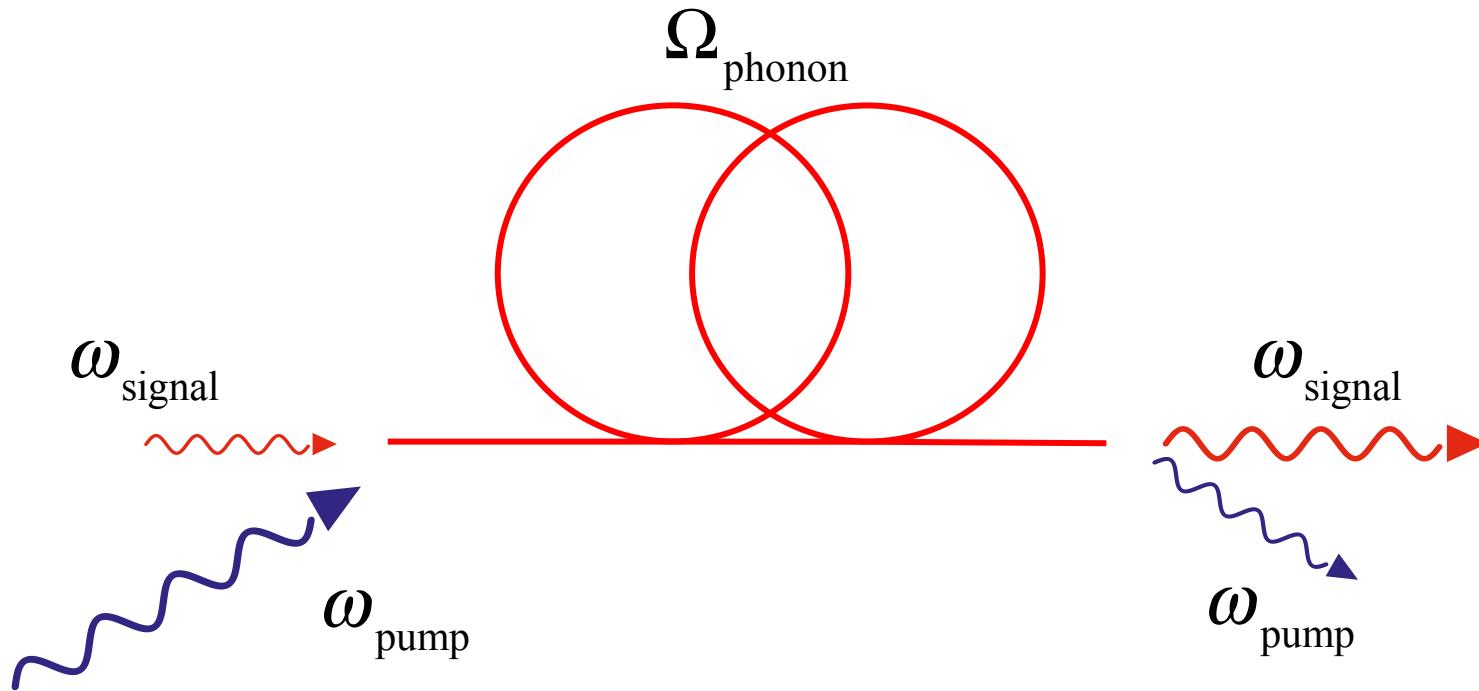
- Linewidth narrows as we increase pump power.
- Above threshold, the noise turns into self-sustained oscillations in the cavity.

$$\begin{aligned} \bar{S}_{aa}(\omega) = & \left[ 1 + \frac{\kappa_{\text{ex}} (\kappa_{\text{ex}} - \kappa_{\text{eff}})}{\left(\frac{\kappa_{\text{eff}}}{2}\right)^2 + (\omega - \omega_c)^2} \right] (n_{\text{in}} + \tfrac{1}{2}) \\ & + \frac{\mathcal{C} \kappa_{\text{ex}} \kappa}{\left(\frac{\kappa_{\text{eff}}}{2}\right)^2 + (\omega - \omega_c)^2} (n_{\text{eff}} + \tfrac{1}{2}). \end{aligned}$$

$$\kappa_{\text{eff}} = (1 - \mathcal{C}) \kappa$$

**First observation of dynamical backaction on an *electromagnetic mode***

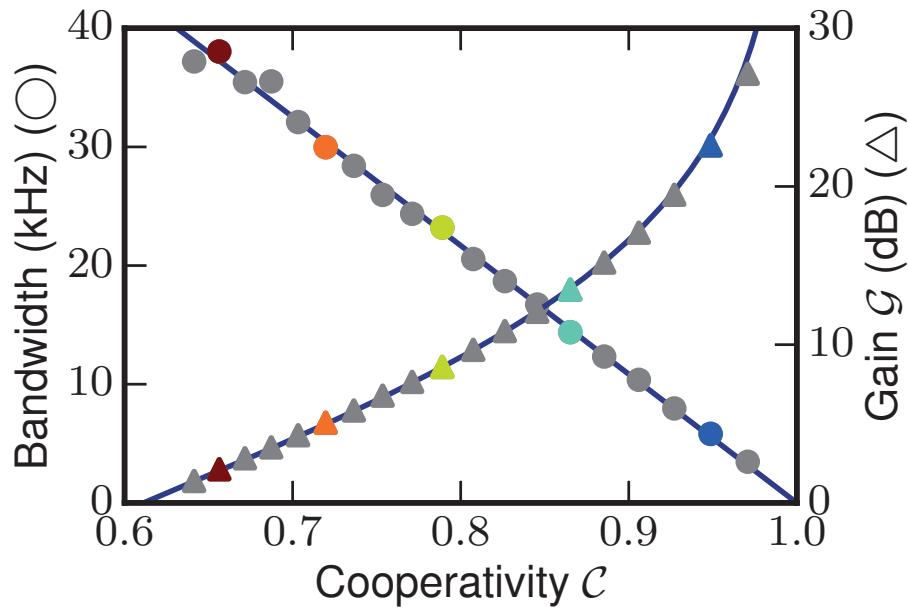
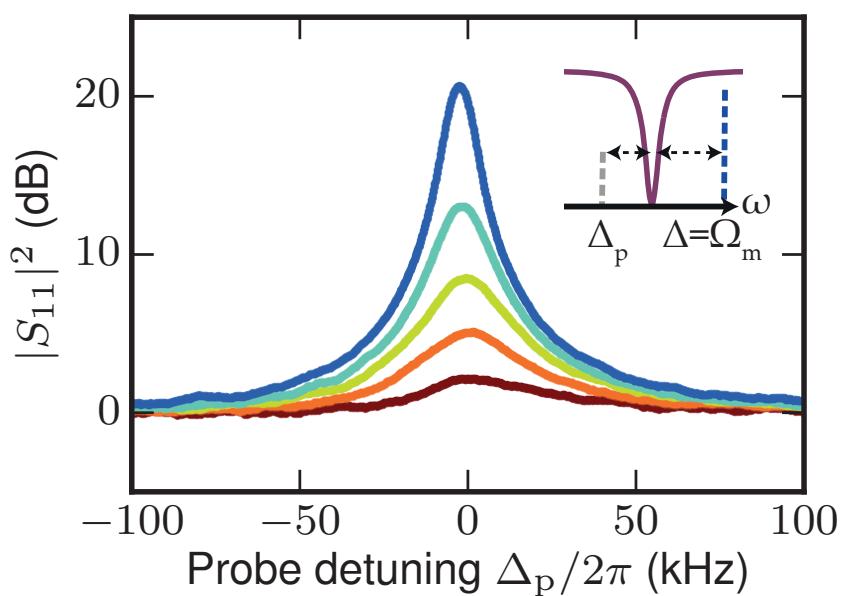
## Stimulated Raman Scattering (SRS)



$$\omega_{\text{pump}} = \omega_{\text{signal}} + \Omega_{\text{phonon}}$$

Phonons (*idler mode* population) decay quickly

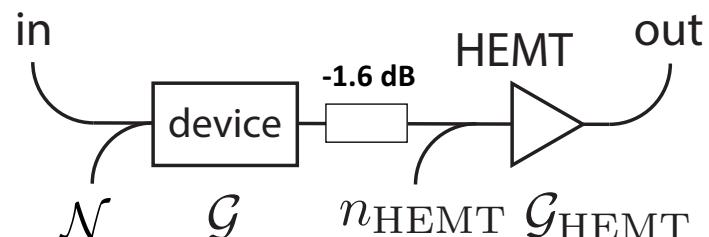
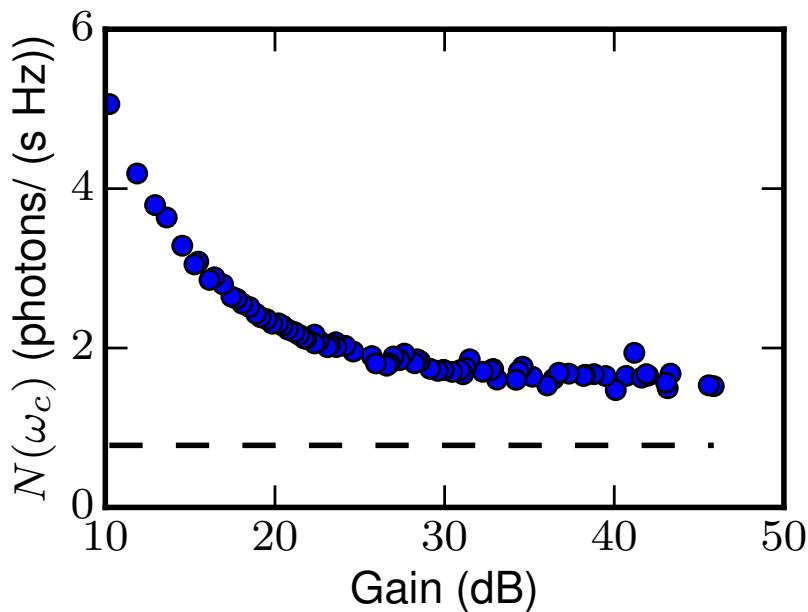
# Amplification by mechanical reservoir engineering



$$\mathcal{G} = |S_{11}(\omega_c)|^2 = \left| \frac{\left(2\kappa_{\text{ex}}/\kappa - 1\right) + \mathcal{C}}{1 - \mathcal{C}} \right|^2$$

$$\kappa_{\text{eff}} = (1 - \mathcal{C})\kappa$$

# Noise added by the electromechanical amplifier (chip B)



$$N = \mathcal{N} + n_{\text{HEMT}} / (\alpha \cdot \mathcal{G})$$

$$\mathcal{N}_{\text{QL}} = \frac{1}{2} + \frac{\kappa_0}{\kappa_{\text{ex}}} \approx 0.78$$

$$\mathcal{N} = \frac{4C \frac{\kappa_{\text{ex}}}{\kappa} \left( n_{\text{eff}} + \frac{1}{2} \right) + 4 \frac{\kappa_{\text{ex}} \kappa_0}{\kappa^2} \cdot \frac{1}{2}}{\left( C - 1 + \frac{2\kappa_{\text{ex}}}{\kappa} \right)^2}$$

The system noise is  $(2.09 \pm 0.13) \times \text{QL}$

$n_{\text{HEMT}} = 22.5 \pm 0.25$  quanta

$n_{\text{eff}} = 0.65 \pm 0.08$  quanta

## Realized electromechanics in the reversed dissipation regime

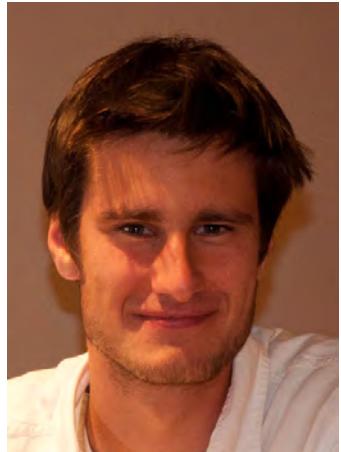
- Control over electromagnetic cavity properties  
*via cold dissipative mechanical reservoir*
- Near-quantum-limited amplification of microwave field
- Maser action

More generally, realized a **dissipative mechanical reservoir for microwaves**:  
a prerequisite for a **new class of dissipative optomechanical interaction**

*Nature Physics 13, 787-793 (2017)*

# Thank you

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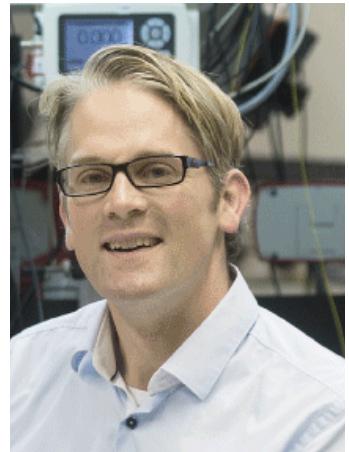
L. D. Tóth



N. R. Bernier



A. Nunnenkamp



T. J. Kippenberg