

Joint ICTP-IAEA Workshop on Innovative Nuclear Energy Systems  
ICTP Leonardo da Vinci Building-Euler Lecture Hall, 20-24 August 2018

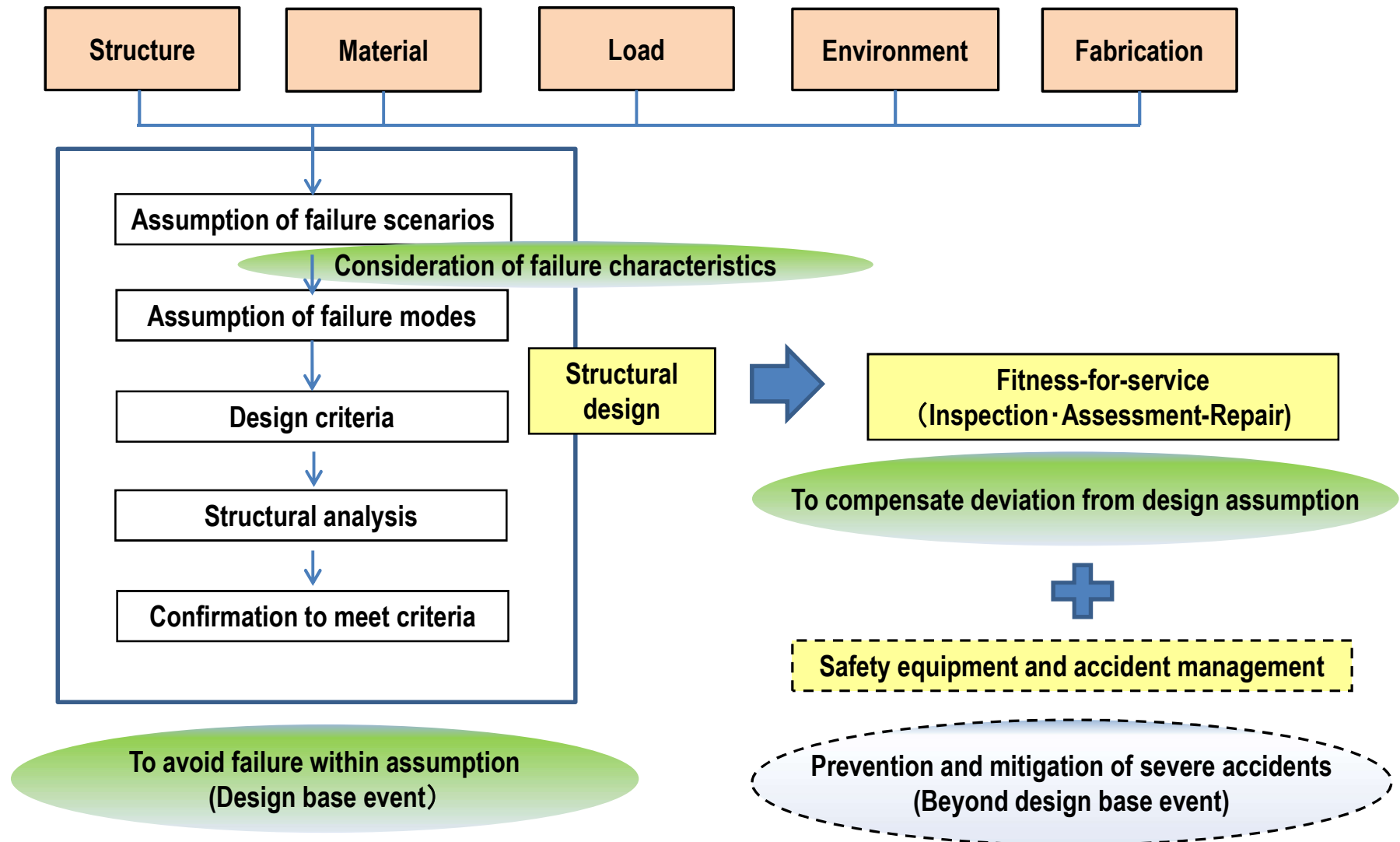
# **Innovative Nuclear Energy Systems: Reactor Design and Structural Designs**

**Masakazu ICHIMIYA**

# **Content**

- 1. Integrated Managements in Terms of Material, Design, Manufacturing, Inspection and Maintenance Features of Structural Conditions of FRs***
- 2. Component Design of FR***
- 3. Inspection and Maintenance***

***1. Integrated Managements in Terms of  
Material, Design, Manufacturing,  
Inspection and Maintenance***



## ***Approach to ensuring structural integrity of reactor facility***

## Relationship between failure modes and countermeasures

Failure modes	Material	Design	Fabrication	Inspection	Fitness-for-service
Brittle fractures	⊙	○ Requirement for ductility	△ Delayed fracture Heat treatment	○ Defect size	○ Defect assessment Monitoring of nil-ductility transition temperature (NDTT)
Ductile fractures	△	⊙		△ Plate thickness	△ Thinning assessment
Buckling		⊙	△ Tolerance		△
Excessive deformation		⊙			△
Fatigue		⊙	○ Finishing	○ Defect size	○ Defect assessment Monitoring of operating transients

## ***1.1 Structural Design Methods for Nuclear Components***

**rational design : keep the risk at an appropriate level.**

**→ imposing design margin according to *safety importance* and *loading frequency***

### ***Component Classification based on safety significance***

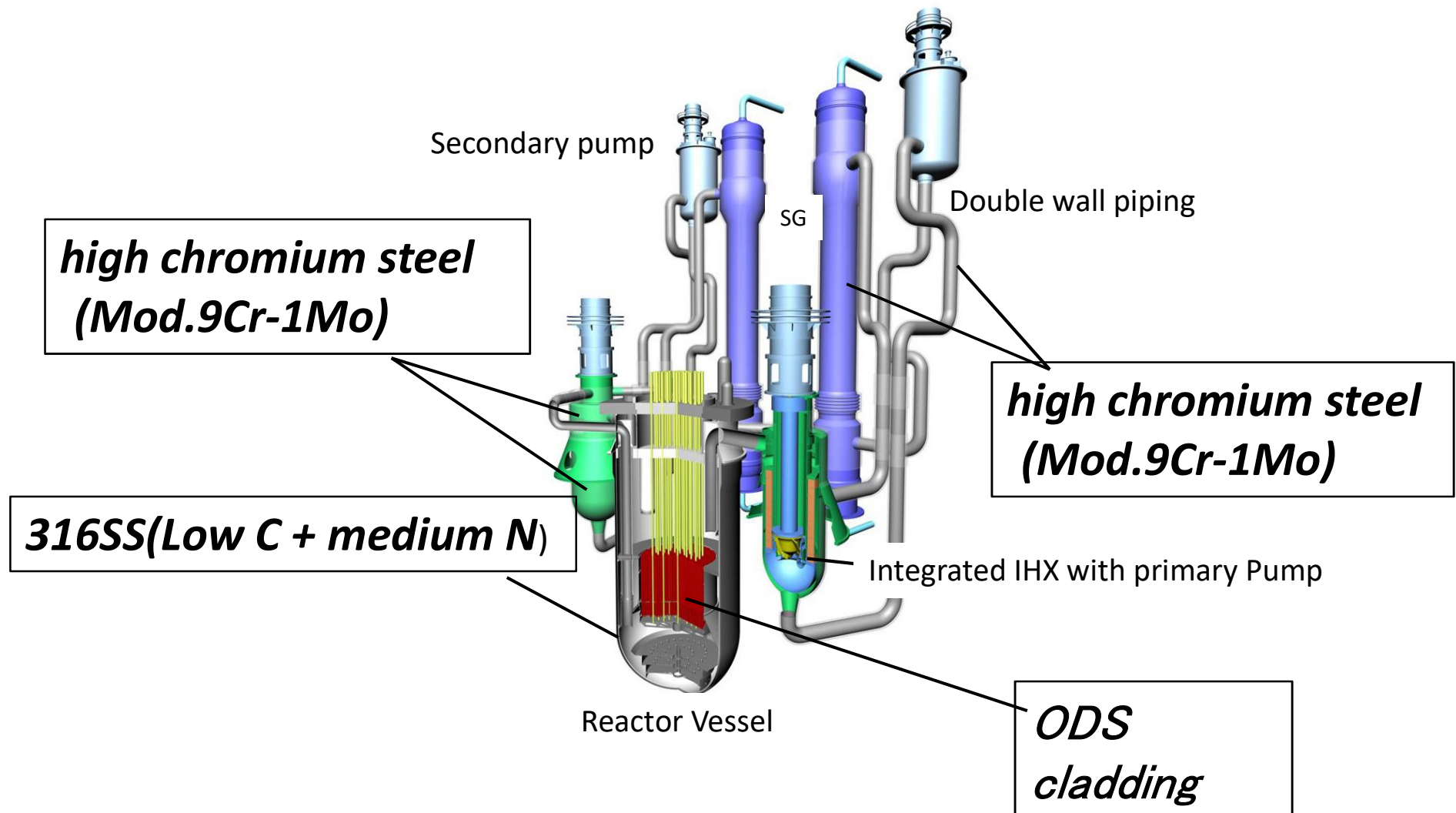
Class 1 Component	Components forming reactor coolant boundary (e.g., reactor vessel, IHX, primary pump)
Class 2 Component	Component forming reactor cover gas boundary, safety systems, etc. (e.g., secondary main pipe, guard vessel, primary cover gas system)
Components of less safety significance	Class 3 components etc. (e.g., steam generator, secondary cover gas system)
Class MC vessel	Metal containment vessel

### ***Condition classification based on the frequency of occurrence of loading***

Service condition I	Normal operating conditions of nuclear reactor facility
Service condition II	Conditions deviated from normal operating conditions due to single failure of component, misoperation or other causes
Service condition III	Conditions requiring emergency shutdown due to a failure or abnormality of reactor facility
Service condition IV	Conditions where an abnormal situation assumed in reactor safety design occurs
Testing Condition	Conditions where pressure exceeding the maximum service pressure is applied during a pressure test

# *1.2 Structural Material of FRs*

## Materials employed in GenIV SFR

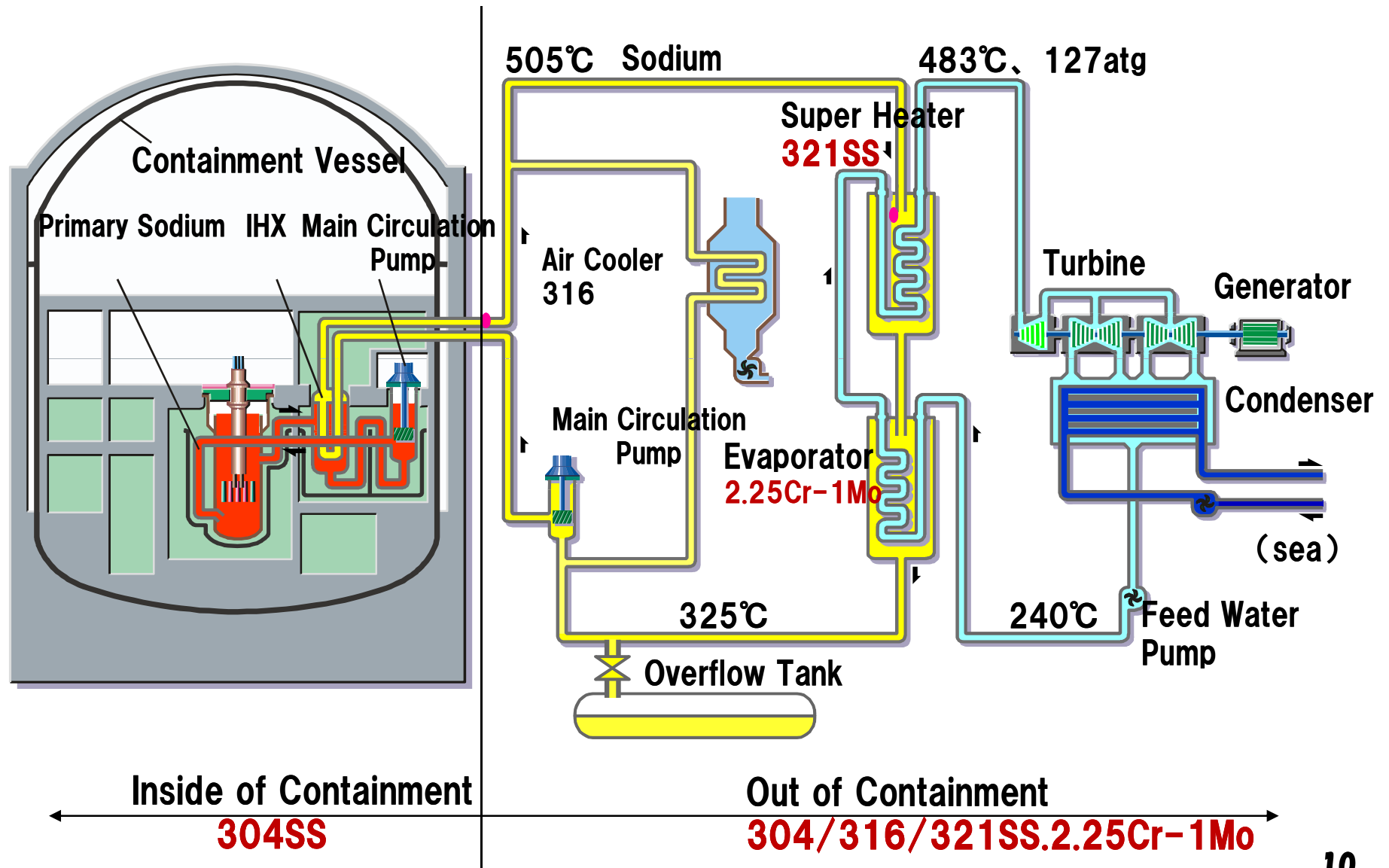




# Property of Materials Employed in GenIV SFR

<p><b>316SS</b> (Low C + Medium N)</p>	<p>It is excellent in high temperature strength and ductility, corrosion resistance, workability and has low degree of embrittlement and hardening due to neutron irradiation.</p> <p>2.5%Mo is added to improve corrosion resistance, high temperature strength etc.</p> <p>Restriction on Carbon content, and addition of Nitrogen with low to medium extent.</p>	<p>Reactor Vessel</p>
<p><b>Mod.9Cr– 1Mo</b></p>	<p>Developed in ORNL(US), followed by Japan etc.</p> <p><b>Mod.9Cr-1Mo steel has been used for boiler components in ultra-supercritical fossil power plants.</b></p>	<p>IHX–Pump Piping Integrated SG</p>

# materials employed in MONJU

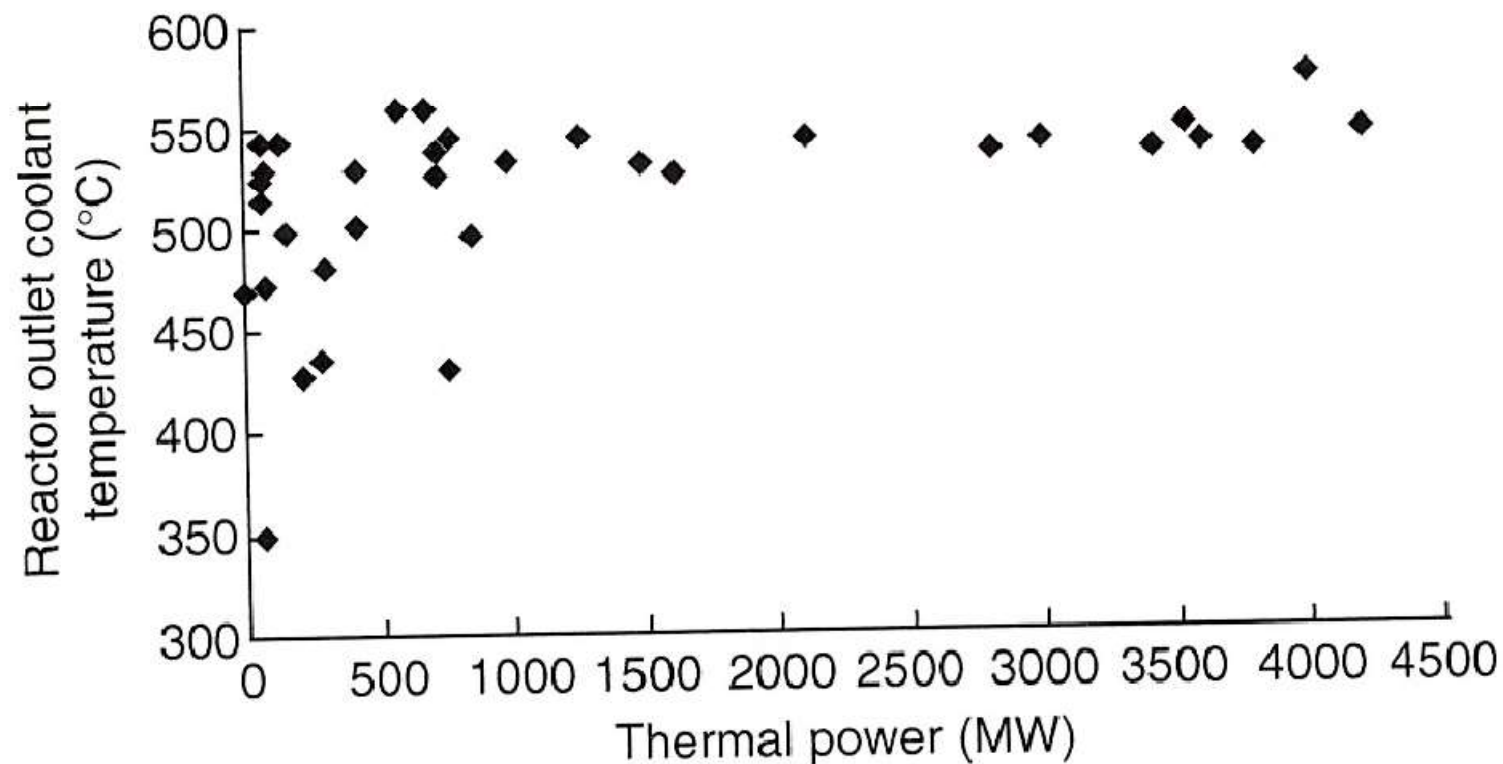


# Property of Materials Employed in MONJU

<b>304SS</b>	It is excellent in high temperature strength and ductility, corrosion resistance, workability, weldability, and has low degree of embrittlement and hardening due to neutron irradiation. Restrictions on C and Co.	Reactor Vessel, IHX, etc
<b>316SS</b>	2.5%Mo is added to improve corrosion resistance, high temperature strength etc.	Air Cooler
<b>321SS</b>	Improve inter-granular corrosion resistance by adding Ti.	Heat transfer Tube of Super Heater
<b>2.25Cr-1Mo</b>	Low alloy steel. Proven material in fossil power plant, in particular heat exchangers.	Evaporator

## ***1.3 Structural Design of FRs***

### ***(1) Loading Conditions Specific to the Use of Sodium***



Ref: Fast Reactor System Design, Naoto Kasahara Ed., Springer.

## Comparison of Operating Condition with LWR

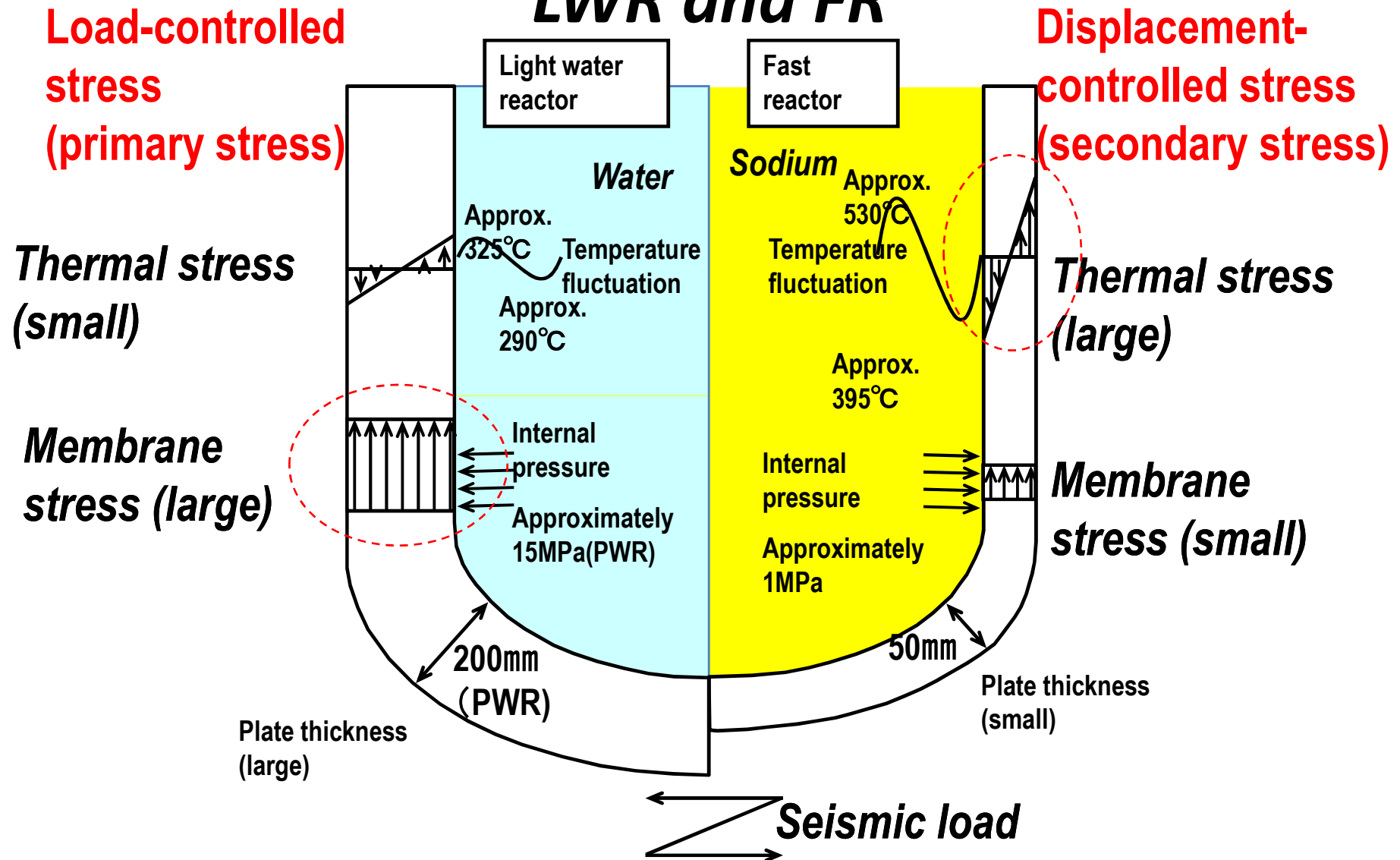
	LWR * 1	FBR * 2	Feature of FBR
Material	Ferrite Steel	Austenitic SS	Ductile Material
Coolant	Water	Sodium	High Boiling Point
Operating Temperature	320°C	529°C	High Temperature
Temperature difference	30°C	132°C	High Thermal Stress
Operation Pressure	≒ 16MPa	≒ 0.5MPa (Pump Outlet)	Low Pressure

\* 1: PWR

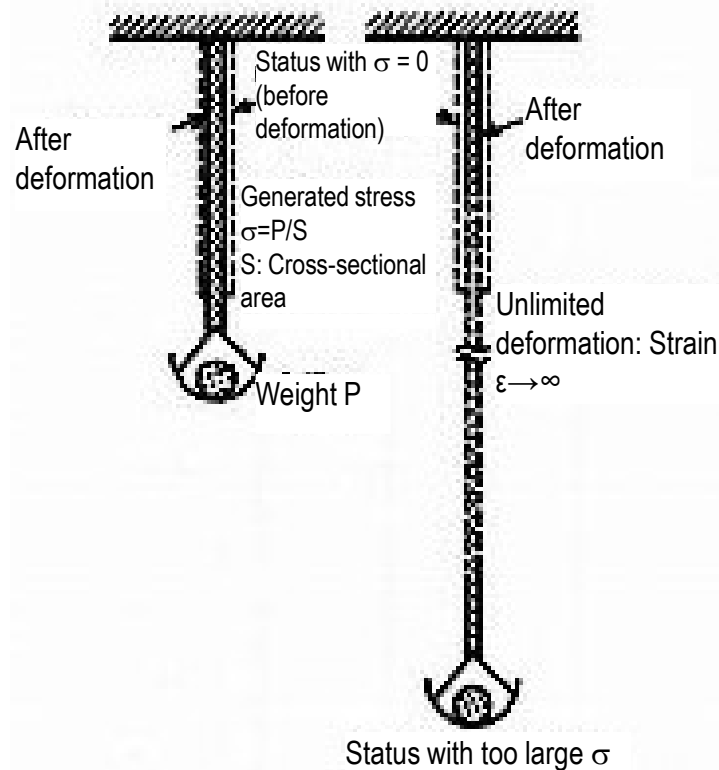
\* 2: Monju

# Comparison of loading conditions between

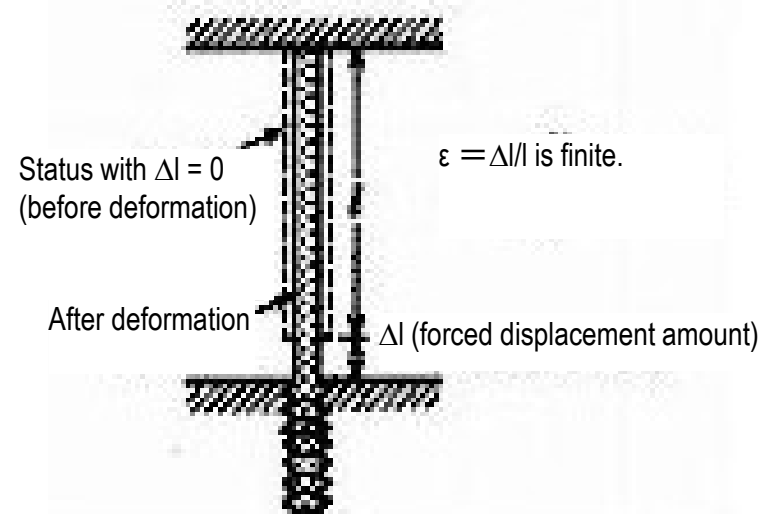
## LWR and FR



# Load-controlled stress versus Displacement-controlled stress



**Load-controlled stress  
(primary stress)**



**Displacement-controlled stress  
(secondary stress)**

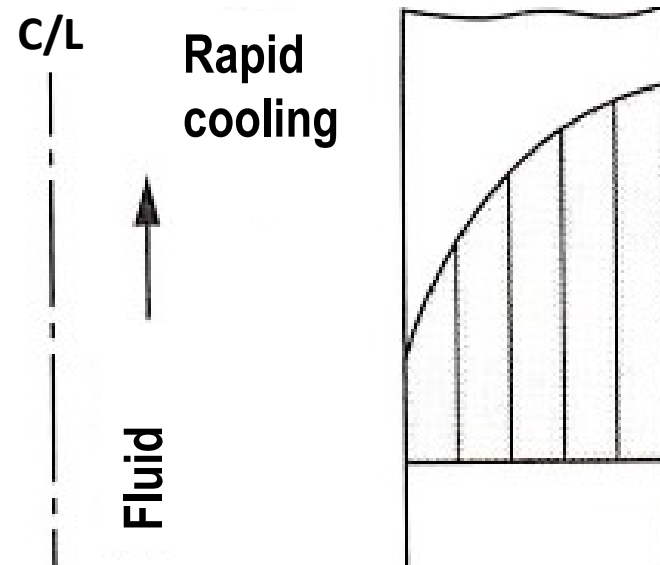
## ***(2) Types of Thermal Loads***

- Generally speaking, the effect of thermal transients on structural material in FRs are more severe than those in LWRs.
- Coolant; Heat transfer characteristic
- Structural material; Thermal conductivity, Thermal expansion rate



# Typical Thermal Stresses in Fast Reactor

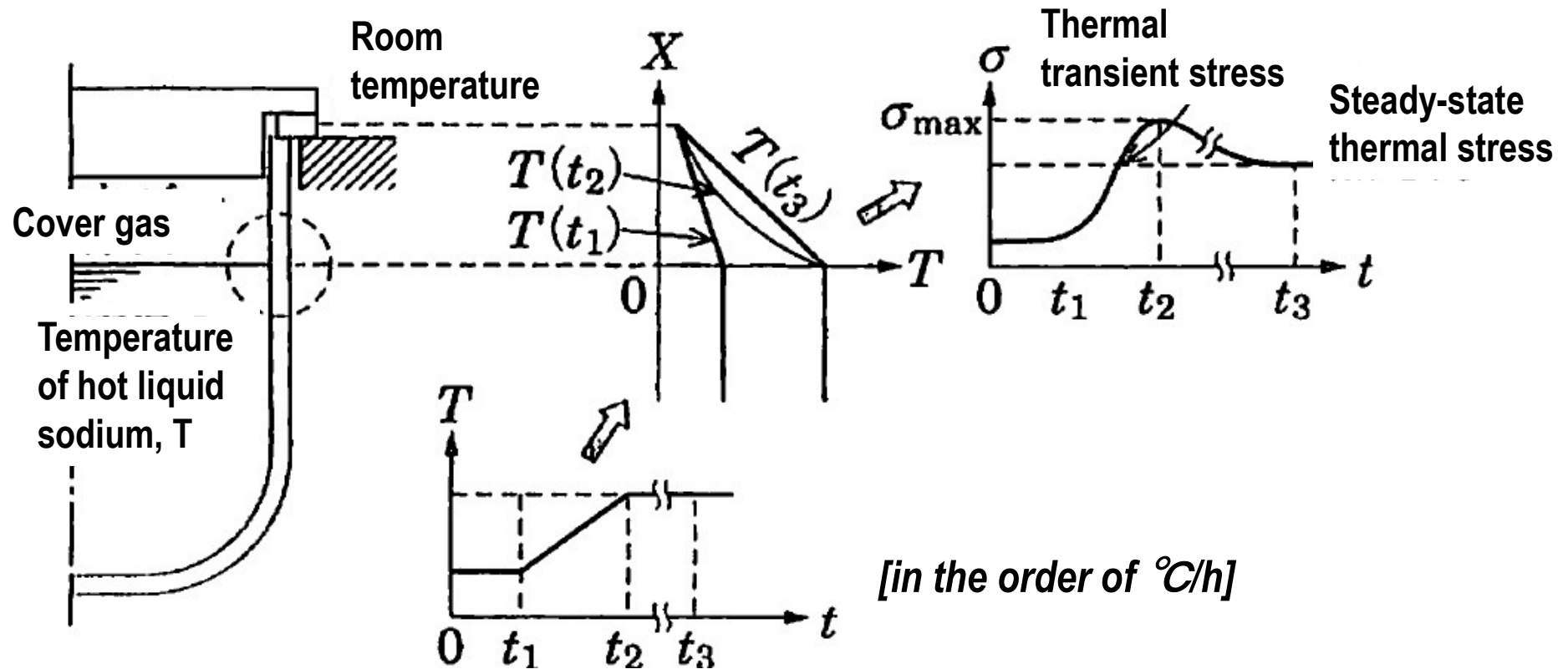
## (a) Through-thickness temperature gradient



Temperature gradient may occur during steady-state conditions.

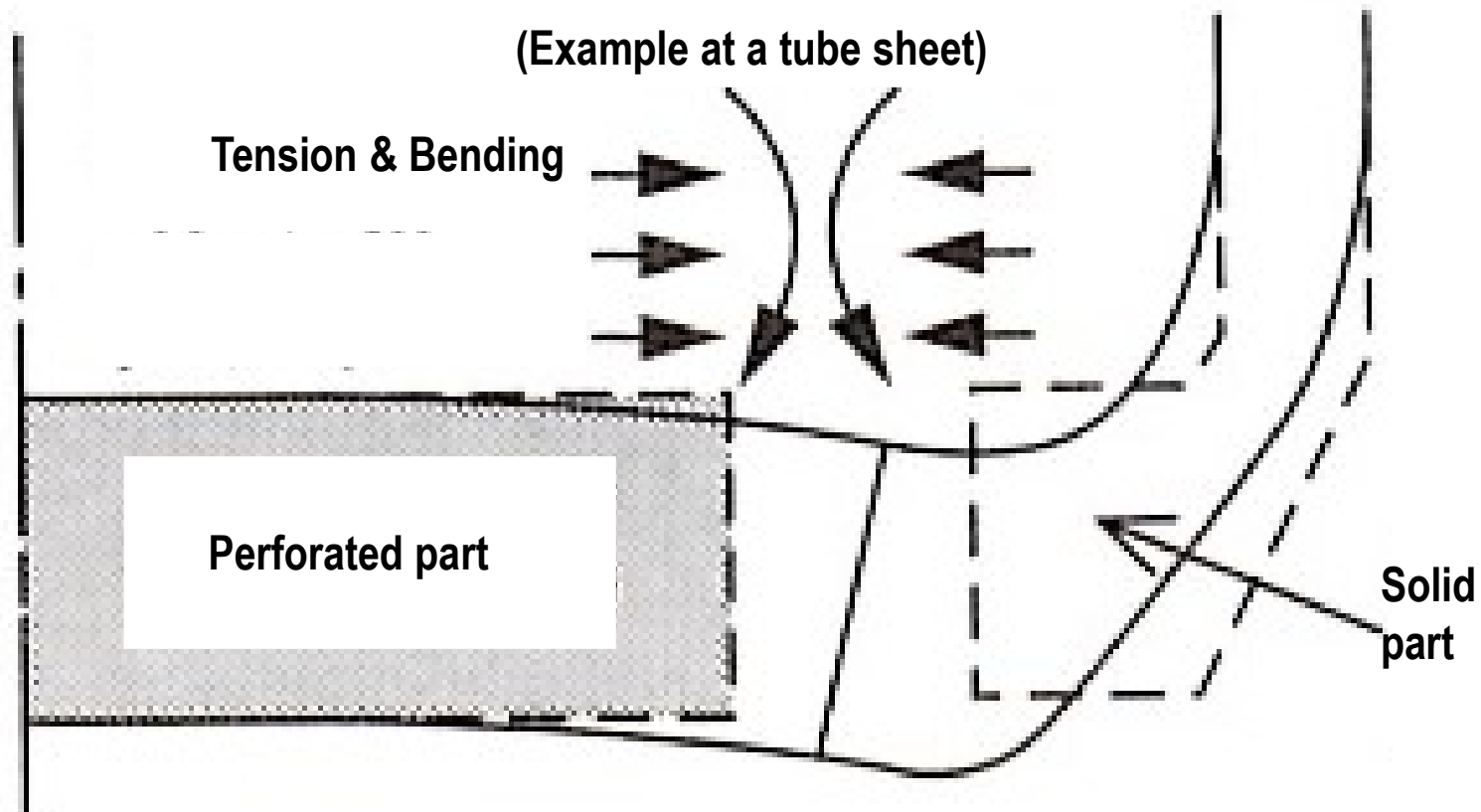
*[in the order of °C/s]*

## (b) Axial temperature gradient near sodium surface

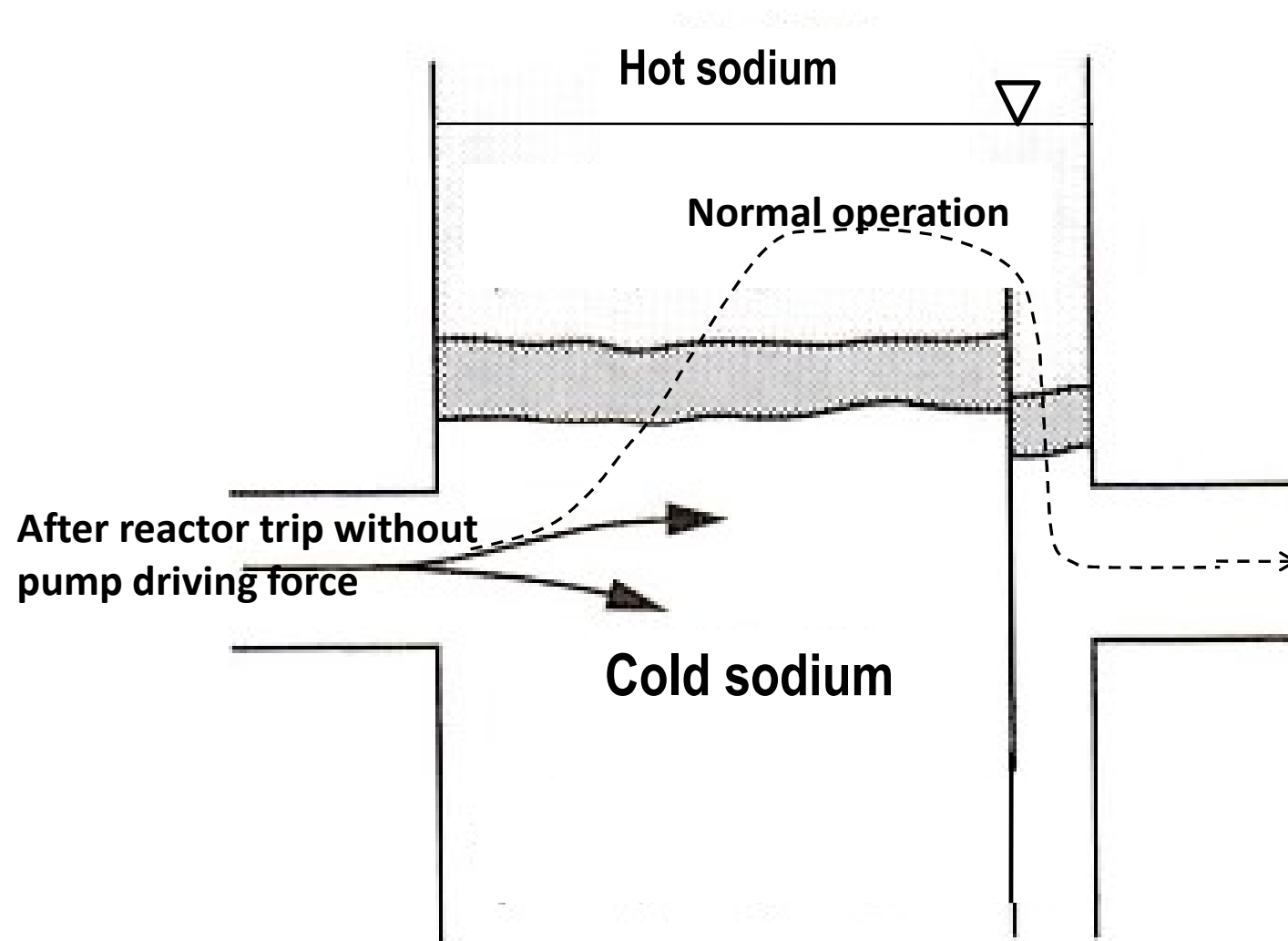


## (c) Hoop force

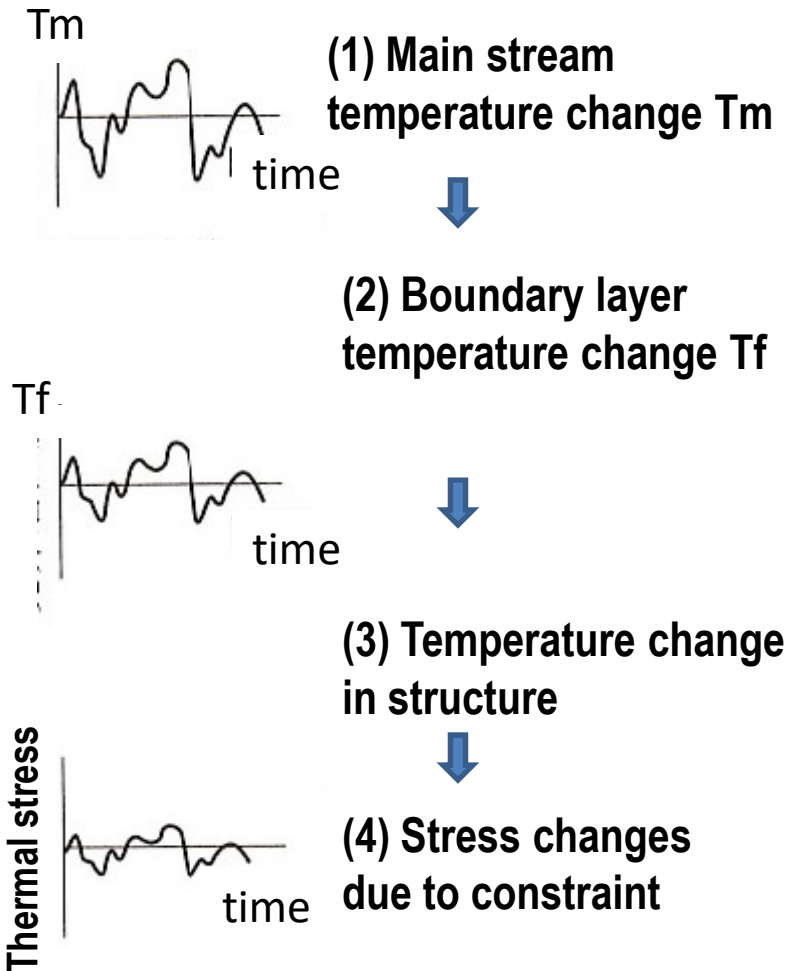
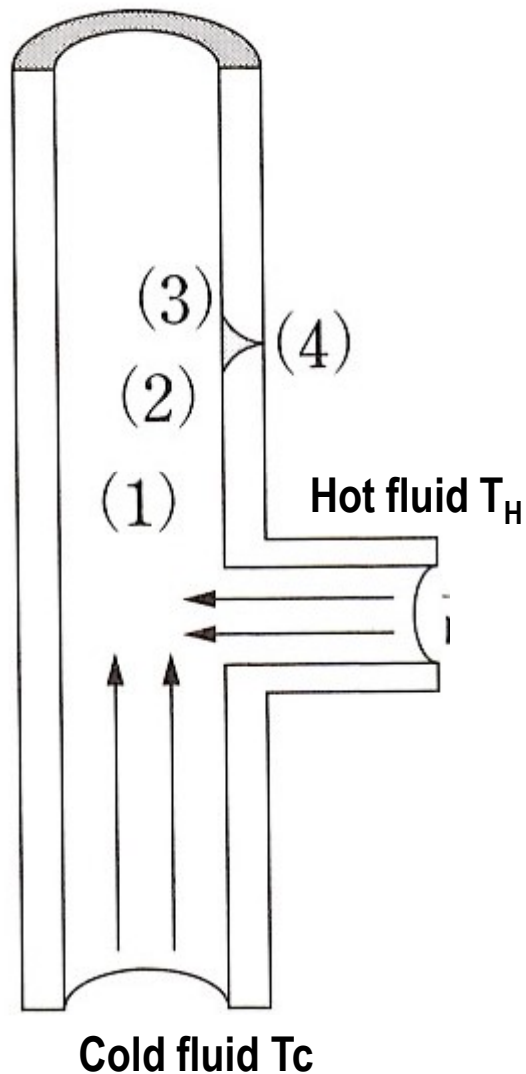
Binding force is exerted between perforated part that rapidly follows thermal transient and solid part that slowly follows.



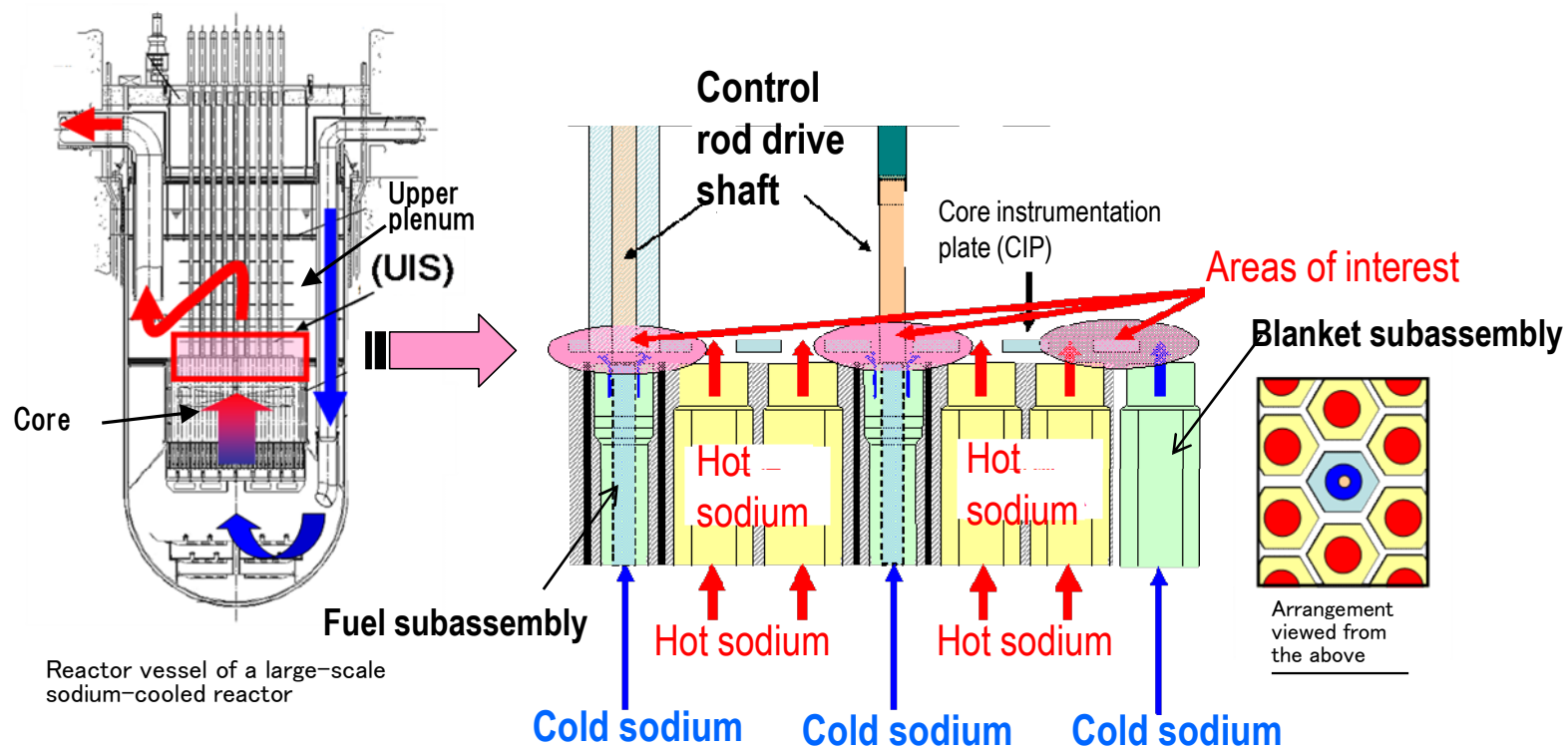
## (d) Thermal stratification



## (e) Thermal striping-1



## (e) Thermal striping-2



**Schematic Diagram of Thermal Striping Phenomenon in the Lower Part of Core Internals**

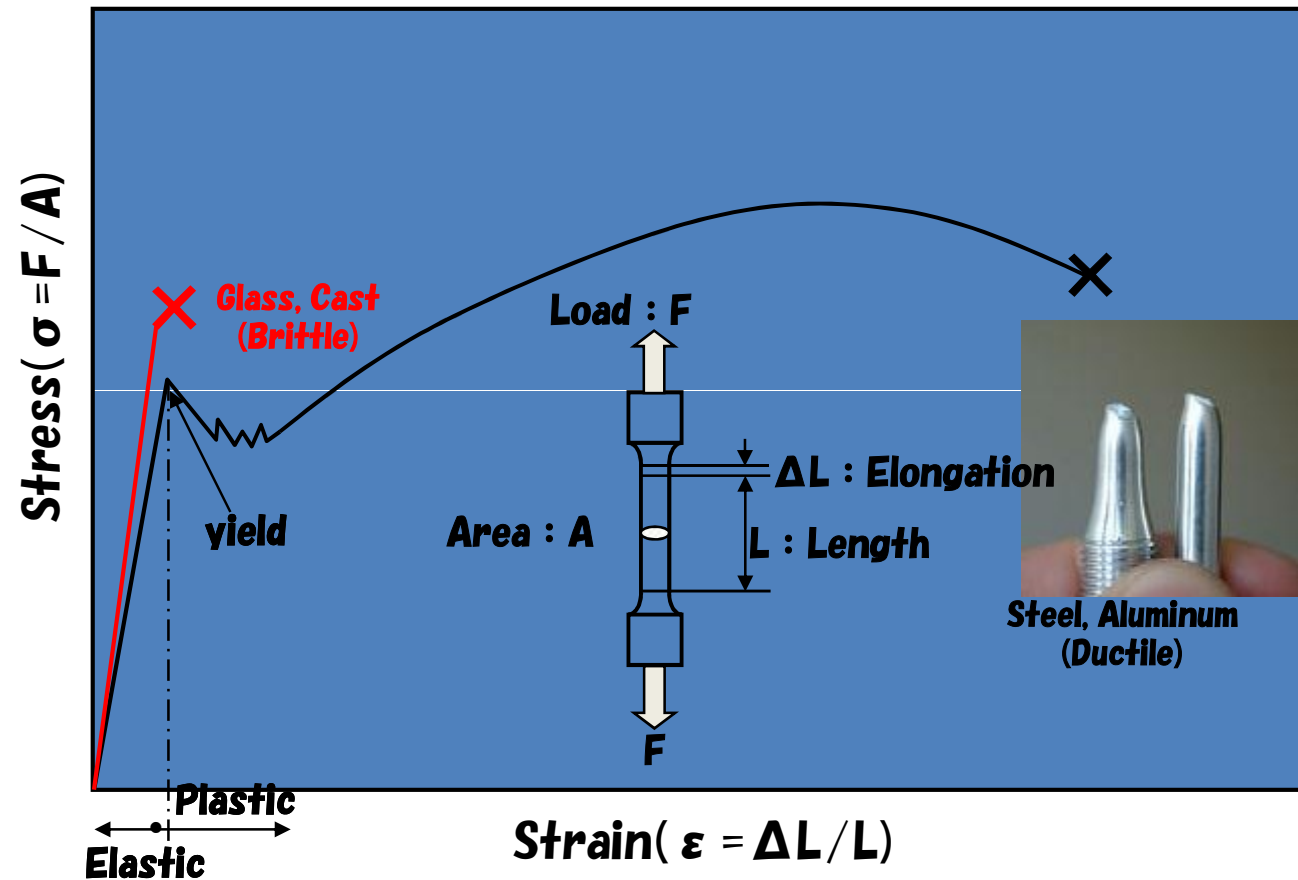
### ***(3) Failure Modes Assumed in FRs***

Failure modes	Material	Design	Fabrication	Inspection	Fitness-for-service
Brittle fractures	⊙	○ Requirement for ductility	△ Delayed fracture Heat treatment	○ Defect size	○ Defect assessment Monitoring of nil-ductility transition temperature (NDTT)
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# Ductile Fracture and Brittle Fracture

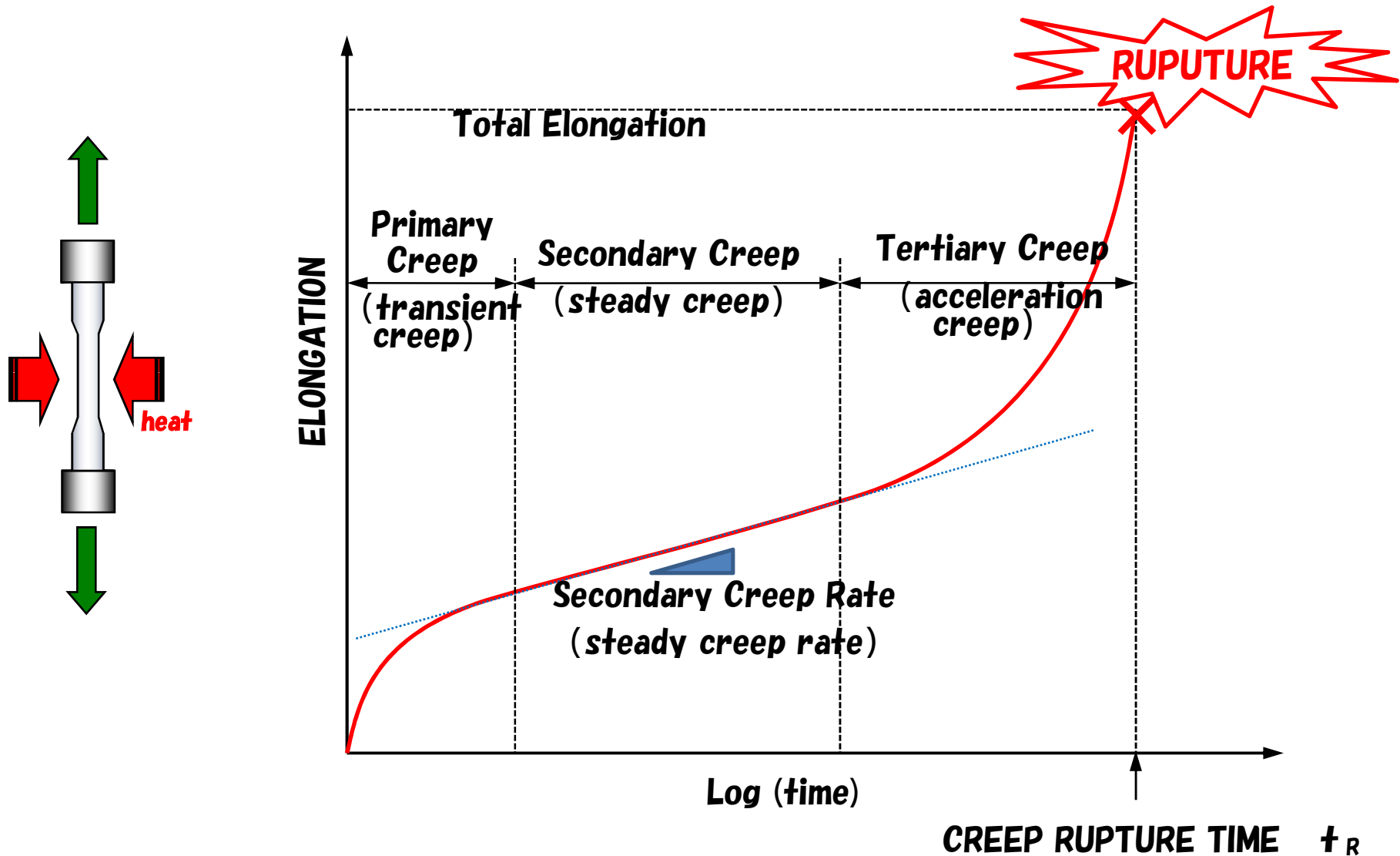


**Tensile Test Machine**

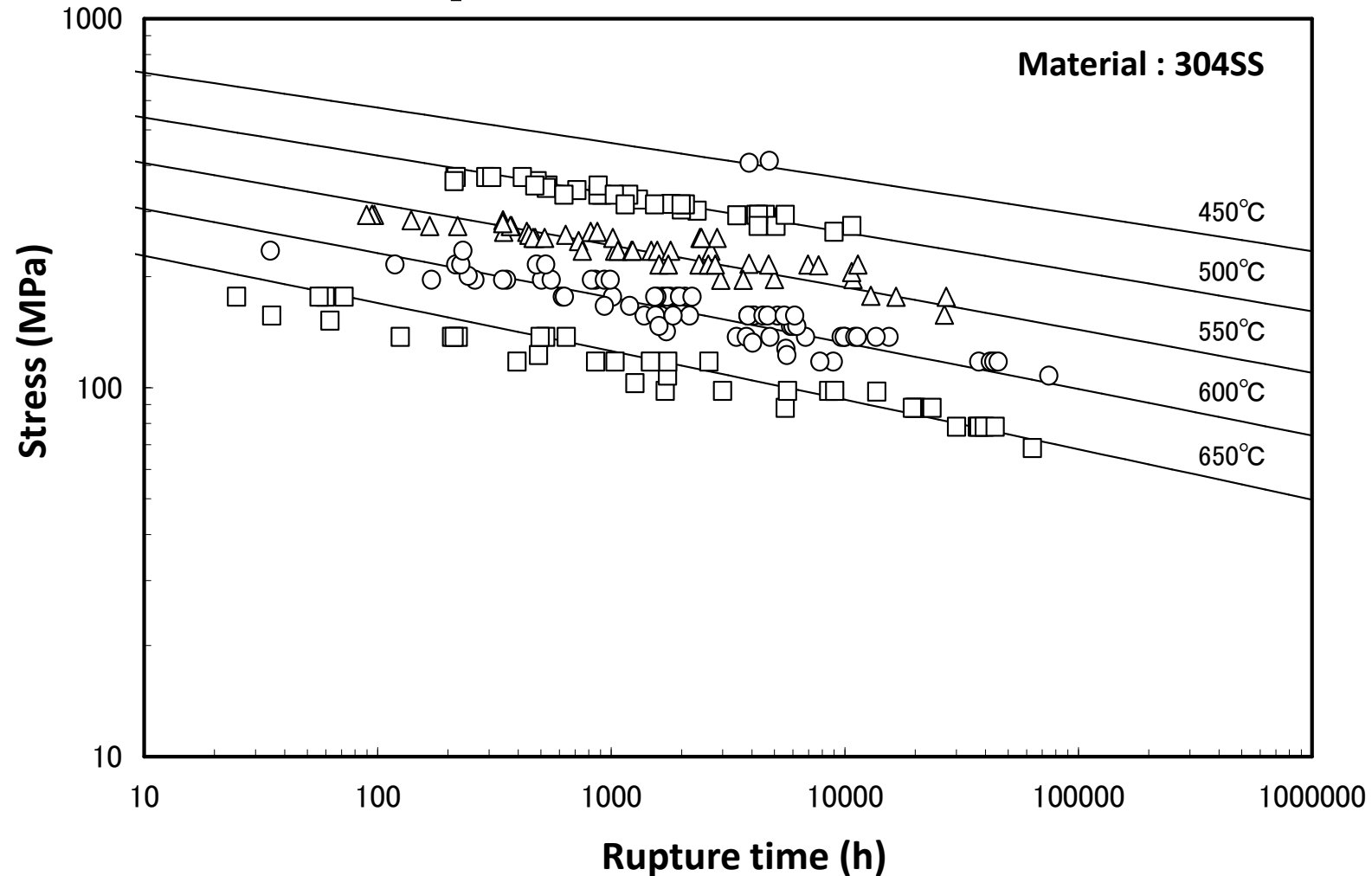




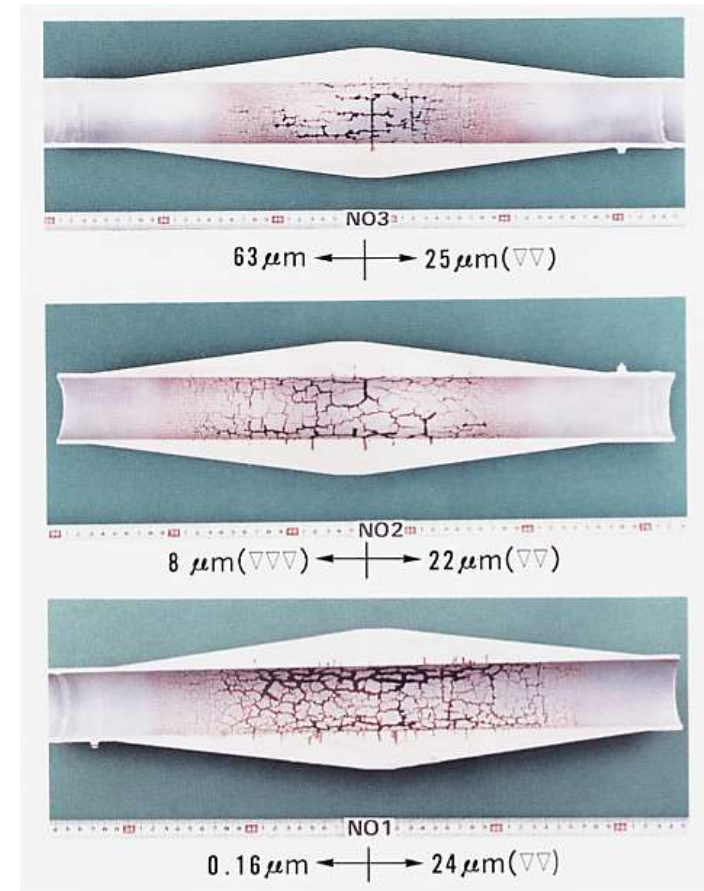
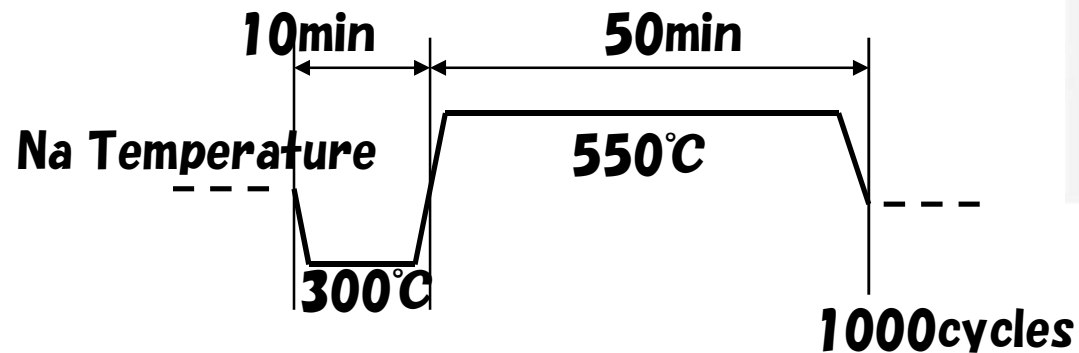
# CREEP



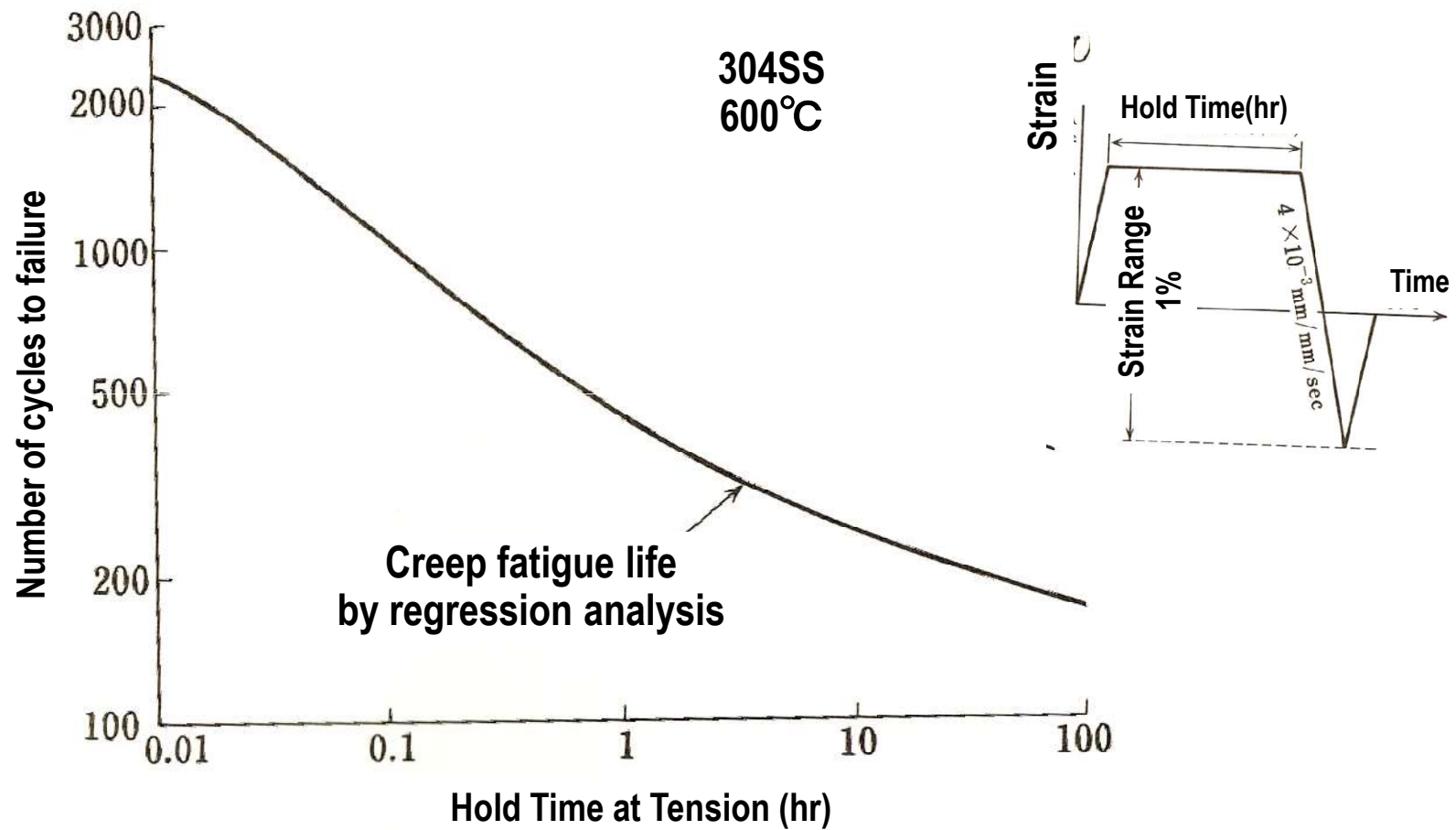
# Relationship between creep rupture time and temperature/stress



***Creep-Fatigue Crack observed in the structure  
subject to repeated temperature change***



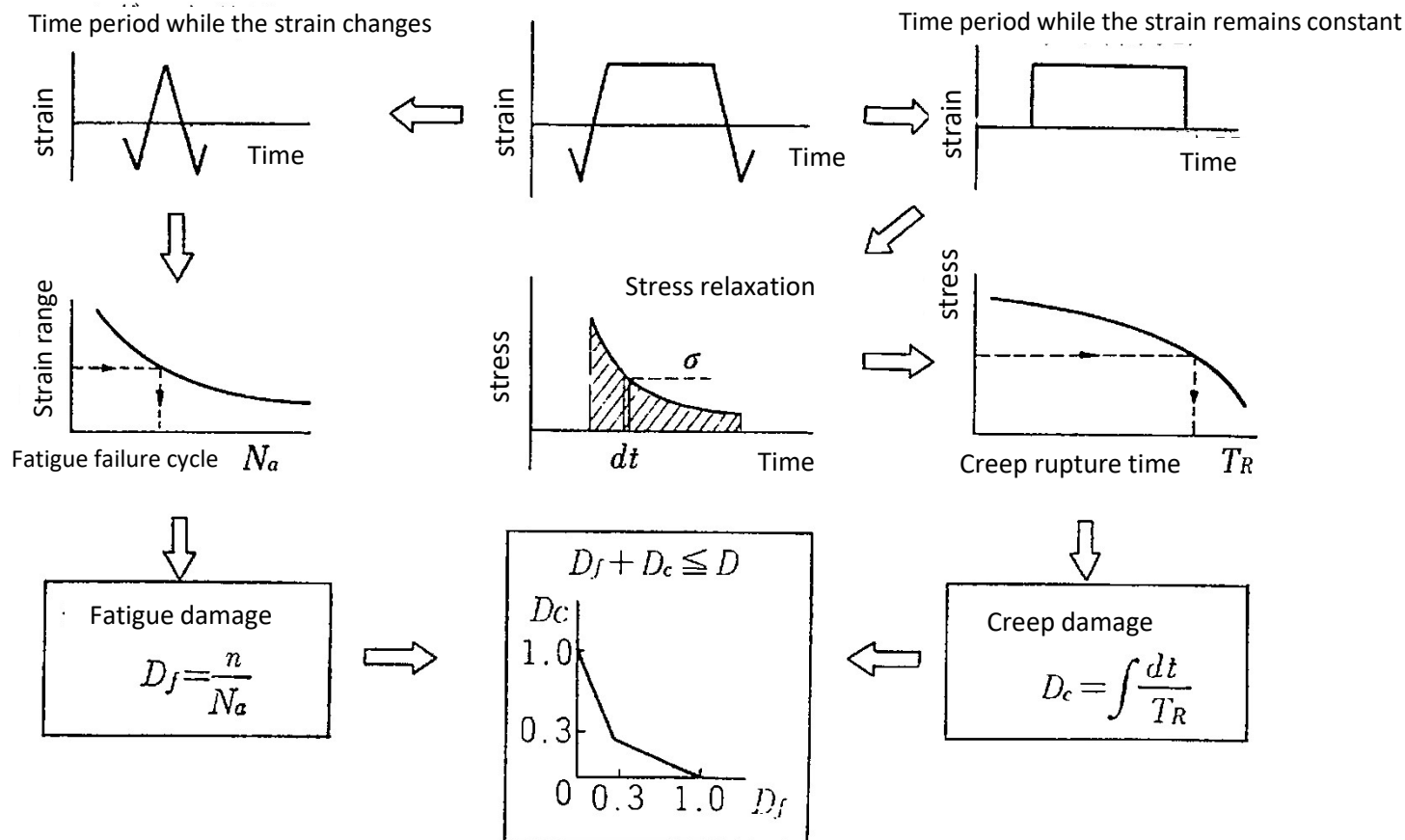
# Creep-Fatigue Life



# Limits for creep fatigue damage

The prevention of the creep fatigue failure is achieved according to the linear cumulative damage rule that limits the sum of the following calculated values :

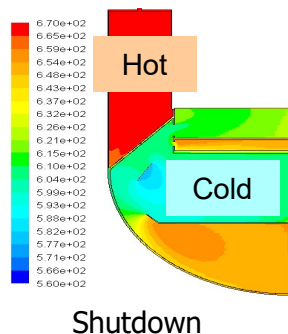
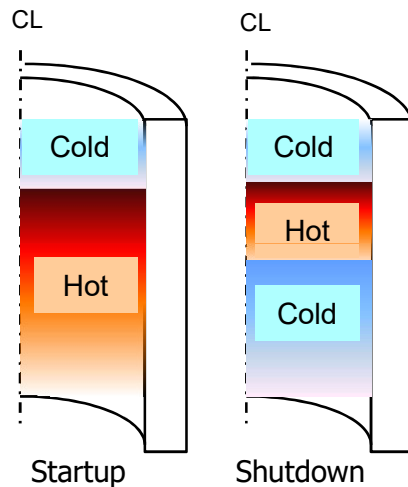
i) usage factor  $D_f$ , and ii) creep damage factor  $D_c$ .



# Expected failure modes of Reactor Vessels

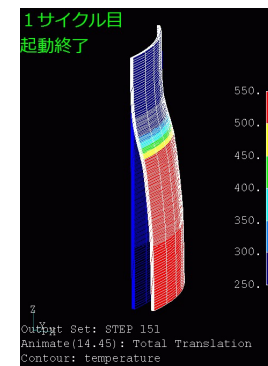
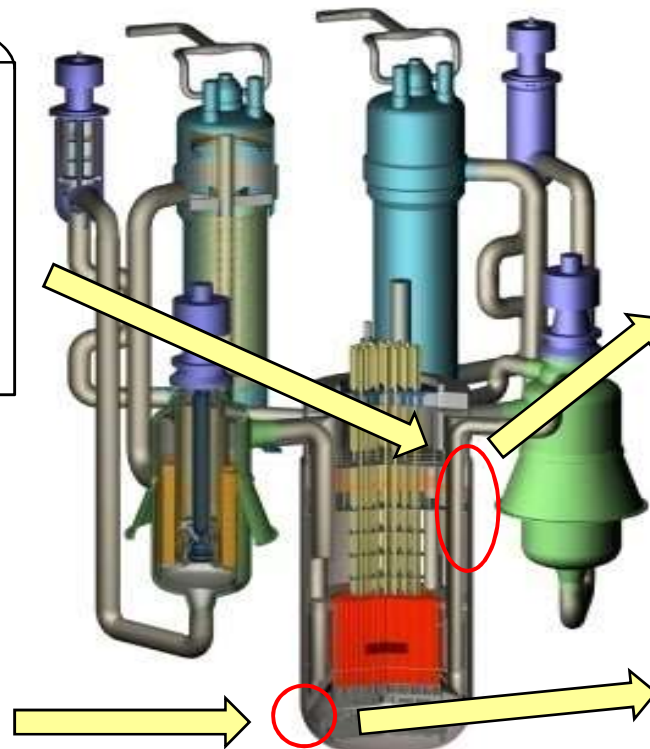
## Thermal load

The dominant load is thermal stress caused by the change in fluid temperature during plant startup/shutdown

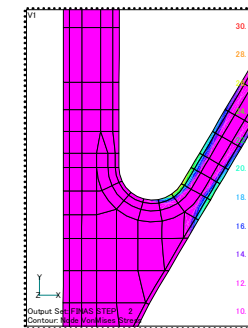


## Structural response

Elastic plastic creep response of structure due to operation at high temperatures



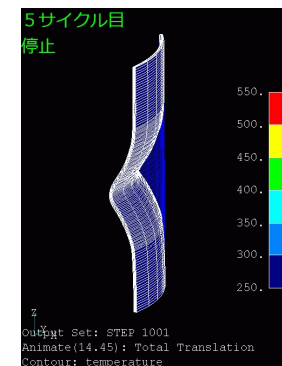
Residual strain



Strain concentration

## Failure

Failure mode due to cyclic loading during lifetime



Excessive deformation due to ratcheting strain



Creep fatigue crack

Ref: Fast Reactor System Design, Naoto Kasahara Ed., Springer.

# Neutron Irradiation Effect

- ① **Atoms on the metal crystal lattice are knocked out by collision with neutron to produce a disturbance of the crystal lattice(i.e., lattice defect)**

⇒ **Fast neutron ( $E > 0.1\text{MeV}$ )**

⇒ **These defect hinder the distortion movement and lead to a reduction in ductility due to hardening.**

- ② **Thermal neutrons convert minute impurities in steel into He.**

⇒ **Thermal neutron ( $E < 0.4\text{eV}$ )**

⇒ **The generated He atoms enhance the aggregation of vacancy to the grain boundary, etc., a reduction in ductility and creep strength results.**