

L3, Wednesday

(1)

Ch. 7 Optimal Control

- If system is controllable, can put poles anywhere.
n-dim sys. \Rightarrow n poles \rightarrow where to put them?
- Rule of thumb: stabilize as needed; speed up slowest modes; leave rest untouched
- Here: define a "performance index" or "cost funct."
- choose controller to minimize the cost

1d example:

$$J(u_0^\infty, x(0)) \equiv \int_0^\infty dt L(x, u) \equiv \int_0^\infty dt \cdot \frac{1}{2} (Qx^2(t) + Ru^2(t))$$

$$\dot{x} = -ax + u(t), \quad x(0) = x_0, \quad a > 0$$

- J is a functional of $u_0^\infty \equiv u(t), t \in [0, \infty)$
and a function of $x(0) = x_0$ [but not of x_0^∞]
- need $J \geq 0$ (finite lower bound) $\Rightarrow Q \geq 0, R \geq 0$
 - $R=0 \Rightarrow$ want best performance (min $|x(t)|$)
regardless of control "effort"
 - $Q=0 \Rightarrow$ only care about cost (do nothing)

scale $Q \rightarrow 1$

Let $u = -Kx$ (will justify this form later)

$$\Rightarrow \dot{x} = -(a+K)x \Rightarrow x(t) = x_0 e^{-(a+K)t} \Rightarrow J = x_0^2 \frac{(1+RK^2)}{4(a+K)}$$

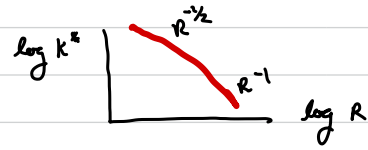
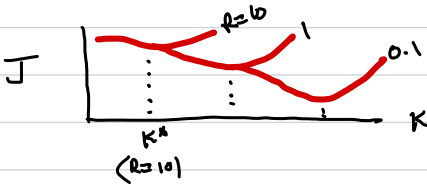
(2)

$$\frac{\partial J}{\partial K} = 0 \Rightarrow K^2 + 2aK - \frac{1}{R} = 0 \Rightarrow K^* = -a \pm \sqrt{a^2 + \frac{1}{R}}$$

choose $+$ as $K^* > 0$

$Ra^2 \ll 1$: cheap control, $J \approx \int_0^\infty dt \frac{1}{2} \dot{x}^2$, $K^* \sim R^{-1/2} \rightarrow \infty$

$Ra^2 \gg 1$: expensive control, $J \approx \int_0^\infty dt \frac{1}{2} u^2$, $K^* \sim \frac{1}{2Ra} \rightarrow 0$



- Rather than choose K, we choose R (or R/Q)
- We have more intuition about R than K (here, a bit artificial)
- **Optimal \neq good!** (poor R \Rightarrow poor control)

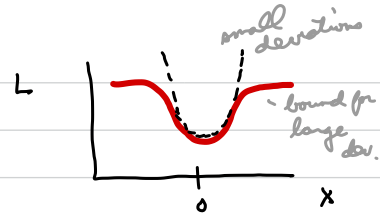
Q: unstable sys?

General setting $J = \underbrace{\varphi[x(\tau)]}_{\text{terminal cost}} + \underbrace{\int_0^\tau dt L(x, u)}_{\text{running cost}}$

- Dynamics $\dot{x} = f(x, u)$ as a constraint
- $J = J[u_0^T, x_0]$
- $\tau \rightarrow \infty \Rightarrow$ drop $\varphi(\cdot)$
- can replace **soft** constraint $\varphi(\cdot)$ with **hard** constraint $\rightarrow \text{BC: } x(\tau) = x_f$

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- Running cost $L(x, u)$
 - scalar
 - bounded from below
 - smooth (eg., twice differentiable)



- Large φ , small L : "ends justify the means".

Impose constraints by Lagrange multipliers

— transpose of n -dim vector

$$J' \equiv \varphi[x(\tau)] + \int_0^\tau dt L(x, u) + \lambda^T(t) [f(x, u) - \dot{x}]$$

- Lagrange mult. $\lambda(t)$ is adjoint vector (costate)
- $\lambda(t)$ is a function of time because $\dot{x} = f$ must be imposed at every moment in time
- Solve unconstrained problem by allowing functional variations $\delta x(t)$, $\delta u(t)$, $\delta \lambda(t)$

$$\delta J' = (\partial_x \varphi) \delta x(\tau) + \int_0^\tau dt \left[(\partial_x L) \delta x + (\partial_u L) \delta u + \lambda^T \left((\partial_x f) \delta x + (\partial_u f) \delta u - \delta \dot{x} \right) + \delta \lambda^T (f - \dot{x}) \right]$$

$$= (\partial_x \varphi) \delta x(\tau) - \lambda^T(\tau) \delta x(\tau) + \lambda^T(0) \delta x(0) + \int_0^\tau dt \left[(\partial_x L) + \lambda^T (\partial_x f) + \dot{\lambda}^T \right] \delta x(t) + \int_0^\tau dt \left[(\partial_u L) + \lambda^T (\partial_u f) \right] \delta u(t) + \int_0^\tau dt (f - \dot{x})^T \delta \lambda(t)$$

use $a^T b = b^T a$

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- The extra boundary terms come from integrating $\lambda^T(t) \delta \dot{x}(t)$ by parts
- $x(0) = x_0$ is fixed $\Rightarrow \delta x(0) = 0$
- In classical mechanics (CM), $u(t)$ is fixed $\Rightarrow x(\tau)$ fixed $\Rightarrow \delta x(\tau) = 0$ **not here!**

$\delta J' = 0 \Rightarrow$ Euler-Lagrange eqs.

- Use Thm: $\int_0^\tau dt f(t) \delta \varphi(t) = 0 \quad \forall \delta \varphi(t) \Rightarrow f(t) = 0 \quad (0 < t < \tau)$

$$0 \rightarrow \tau: \quad \dot{x} = f(x, u) \quad x(0) = x_0$$

$$\tau \rightarrow 0: \quad \dot{\lambda} = -(\partial_x f)^T \lambda - (\partial_x L)^T, \quad \lambda(\tau) = (\partial_x \phi|_\tau)^T$$

$$t: \quad 0 = (\partial_u f)^T \lambda + (\partial_u L)^T$$

- These eqs. give only **necessary** conditions 

- Interpretation of adjoint $\lambda(t)$ (1d)
 - ignores λ -dependence in $(\partial_x f) \Rightarrow \dot{\lambda} = -(\partial_x f)\lambda - (\partial_x L)$
 - **Planning horizon** (timescale) $\sim -(\partial_x f)^T$
 - driven by $-\partial_x L$ term
 - **backwards in time**
- Together: **Boundary-value problem** (not init. val.)

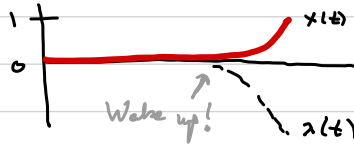
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1d ct. (again)

$$L = \frac{1}{2}(x^2 + u^2), \quad \dot{x} = -x + u$$

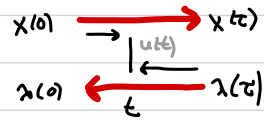
- but now let $x(0) = x_0$ and impose $x(\tau) = x_c$

Euler-Lagrange: $\dot{x} = -x + u, \quad \dot{\lambda} = +\lambda - x, \quad u = -\lambda$



• Nature of control signal $u(t)$

- depends on past states x_0^t
- depends on future plans λ_τ^t



Ex: Swing up a pendulum

$$\ddot{\theta} + \sin\theta = u(t) \quad \text{torque control}$$

	$(\theta, \dot{\theta})$
$t=0:$	$(0, 0)$
$t=\tau:$	$(\pi, 0)$

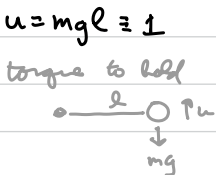
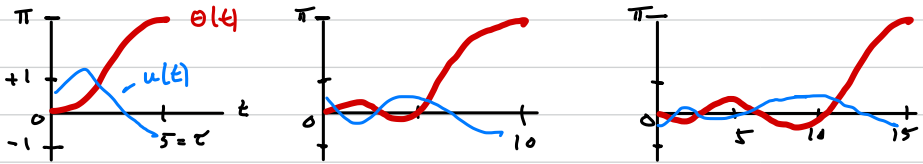
boundary conditions

$$J = \int_0^\tau dt \cdot \frac{1}{2} u^2(t) \quad \text{"control effort"}$$

hard constraint on $x = \{\theta, \dot{\theta}\}$ at $t=\tau \Rightarrow$ no λ cond.

For DC motor, $u \sim$ torque $\sim I$
(ditto $I^*(t) \sim$ torque)

$$E-L: \quad \ddot{\lambda} + \lambda \cos\theta = 0 \quad u(t) = -\lambda(t)$$



- Increasing $\tau \Rightarrow$ reduce $|u|_{max}$
- # reversals increases w/ τ

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7.3 Linear Quadratic Regulator (LQR)

- small deviations, quadratic costs

$$J = \int_0^T dt \frac{1}{2} (x^T Q x + u^T R u) \quad \begin{array}{l} Q, R \text{ symmetric} \\ R > 0, \quad Q \geq 0 \\ \text{add final cost of } Qx \end{array}$$

E-L: $\dot{x} = f(x, u) \quad \text{w/ } f = Ax + Bu; \quad L = \frac{1}{2}(x^T Q x + u^T R u)$

$$\lambda = -(\partial_x f)^T \lambda - (\partial_x L)^T$$

$$0 = (\partial_u f)^T \lambda + (\partial_u L)^T$$

$$\dot{x} = Ax + Bu, \quad \dot{\lambda} = -A^T \lambda - Qx \quad u = -R^{-1} B^T \lambda$$

• Can try $\lambda(t) = S(t)x(t)$ n x n matrix
 this trick works only for linear dynamics!

$$u = -R^{-1} B^T S x \equiv -Kx \quad \text{m x n matrix}$$

$$\dot{\lambda} = -Qx - A^T (\underbrace{Sx}_\lambda) = \frac{d}{dt}(Sx) = \dot{S}x + S(Ax - BR^{-1}B^T Sx)$$

$$\dot{S} = -Q - A^T S - SA + SBR^{-1}B^T S \quad \begin{array}{l} \text{factor } x(t); \text{ holds } \forall t \\ \text{continuous time Ricatti Eq.} \end{array}$$

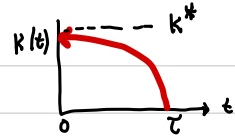
steady state

$$0 = -Q - A^T S - SA + SBR^{-1}B^T S \quad \text{algebraic Ricatti Eq.}$$

• quadratic eq \Rightarrow multiple solns; only 1 is physical

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$$k = R^{-1}(1)S = S/R$$



Ex: Id control yet again: $A = -a, B = Q = 1$

$$\Rightarrow \dot{s} = -1 + 2aS + S^2/R$$

$$\Rightarrow S = -aR \pm \sqrt{a^2 R^2 + R} \quad \text{steady state}$$

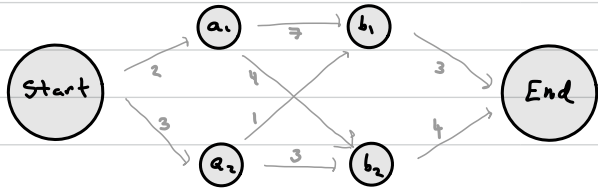
But fully optimal solution for finite τ has $K = K(t)$

$K \rightarrow 0$ as $t \rightarrow \tau$ (it costs for control, but no benefit if applied too close to end)

7.4 Dynamic Programming

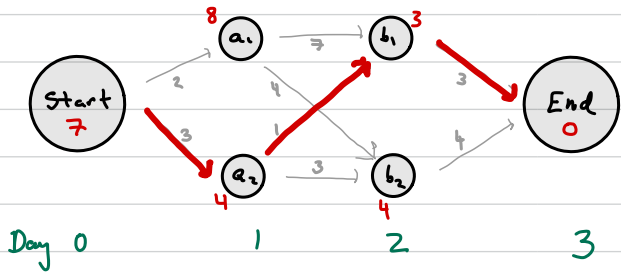
Richard Bellman, 1950s (RAND)

Shortest path between cities



$J(x) = \text{cost-to-go}$

$J^* = \text{optimal } J$



$$J^*(\text{End}) = 0$$

You are already there.

$$J^*(b_1) = 3, \quad J^*(b_2) = 4$$

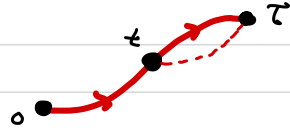
only one possibility in each case

$$J^*(a_1) = \min [7 + J^*(b_1), 4 + J^*(b_2)] = 8$$

$$J^*(a_2) = \min [1 + J^*(b_1), 3 + J^*(b_2)] = 4$$

$$J^*(\text{Start}) = \min [2 + J^*(a_1), 3 + J^*(a_2)] = 7$$

Principle of Optimality:



For any point on an optimal trajectory, the remaining trajectory is optimal, starting at that point.

Bellman Eq. (discrete case)

$X_k =$ state

city at time k ; eg a_1, a_2

$u_k =$ action

road choice at time k

$L(X_k, u_k) \equiv L_k$

running cost of current step, given X_k, u_k

$J(X_k, u_k) \equiv J_k$

cost-to-go; start from X_k , choose u_k, \dots, u_{N-1}

$\varphi(X_N)$

terminal cost

[note: $u_N = 0$]

$$J = \sum_{n=0}^{N-1} L(X_n, u_n) + \varphi(X_N) \quad \text{total cost}$$

$$\begin{aligned} J_k &= \sum_{n=k}^{N-1} L(X_n, u_n) + \varphi(X_N) \\ &= \underbrace{L(X_k, u_k)}_{L_k} + \underbrace{\sum_{n=k+1}^{N-1} L(X_n, u_n) + \varphi(X_N)}_{J_{k+1}} \end{aligned}$$

So:

$$J_k = L_k + J_{k+1}$$

$$J_N = \varphi(X_N)$$

$$X_{k+1} = f(X_k, u_k)$$

X_0 given

← J_k obeys a backwards recursion relation

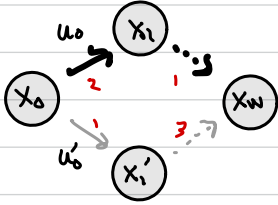
- solving it fixes u_k^* (optimal choice at time k)

- then solve forward recursion reln for X_k →

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Bellman eq.

$$J^*(x_k) = \min_{\{u_k\}} [L(x_k, u_k) + J^*(x_{k+1})]$$



We choose u_0 over u_0' even though it has a higher immediate cost.

Overall future costs are lower

Solve J_k backwards; get u_k^* ; iterate $x_{k+1} = f(x_k, u_k^*)$ forwards.

- Solution is possible because dynamics have a state structure \Rightarrow solution decomposes into stages

Numerical algorithm: $\left. \begin{array}{l} \underline{n \text{ nodes / step}} \\ \Rightarrow \text{each node has } n \text{ possibilities} \end{array} \right\} \mathcal{O}(n^2)$
 $\times \underline{N \text{ stages}} \Rightarrow \mathcal{O}(N \cdot n^2)$

vs. naive search $\mathcal{O}(n^N)$ huge difference for large N !

\Rightarrow Value of planning.

Bellman algorithm (re-) discovered many times

- Cell phones (Andrew Viterbi) Qualcomm.
- Sequence alignment (bioinf.) (Needleman - Wunsch, Smith-Waterman)

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"Livet skal forstås
baglæns, men leves
forlæns."



"Life must be understood backwards
but lived forwards."

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Bellman eq. (continuous case)

cost-to-go: $J(x, u) = \varphi[x(\tau)] + \int_t^\tau dt' L(x, u)$; $J^* = \inf_{u \in [t, \tau]} J(x, u)$

$$J^*(x) = \inf_u \left[\varphi[x(\tau)] + \int_t^\tau dt' L(x, u) \right]$$

$$= \inf_u \left[\int_t^{t+\Delta t} dt' L(x, u) + \varphi[x(\tau)] + \int_{t+\Delta t}^\tau dt' L(x, u) \right]$$

$$\approx \inf_{u \in [t, t+\Delta t]} \left[L(x, u) \Delta t + \inf_{u \in [t+\Delta t, \tau]} [J(x + \dot{x} \Delta t, u(t+\Delta t))] \right]$$

$$= \inf_{u \in [t, t+\Delta t]} \left[L(x, u) \Delta t + J^*(x + f \Delta t) \right]$$

$$\approx \inf_{u \in [t, t+\Delta t]} \left[L(x, u) \Delta t + J^*(x) + (\partial_t J^*) \Delta t + (\partial_x J^*) f \Delta t \right]$$

$$\partial_t J^* + \inf_{u(t)} \left[L(x, u) + (\partial_x J^*) f(x, u) \right] = 0$$

Hamilton - Jacobi - Bellman (HJB) eq.

- Integrate backwards in time from final condition

$$J^*[x(t), \tau] = \varphi[x(\tau)]$$

$$\Rightarrow u^*(t)$$

- Then integrate $\dot{x} = f(x, u^*)$ forward from $x(0) = x_0$

- $\partial_x J^* = n$ -dim row vector $\Rightarrow (\partial_x J^*) f$ is a scalar

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One-dim control, yet again!

$$J = \int_t^{\tau} dt' \frac{1}{2}(x^2 + u^2), \quad \dot{x} = -x + u$$

$$\text{HJB:} \quad \partial_t J^* = - \inf_u \left[\underbrace{\frac{1}{2}(x^2 + u^2)}_{L(x,u)} + (\partial_x J^*) \underbrace{(-x + u)}_{f(x,u)} \right]$$

Since there are no restrictions on $u(t)$, we can do the minimization by taking ∂_u of right-hand side.

$$\begin{aligned} \partial_u \left[\frac{1}{2}(x^2 + u^2) + (\partial_x J^*)(-x + u) \right] &= u + (\partial_x J^*) = 0 \\ \Rightarrow u^* &= -\partial_x J^* \end{aligned}$$

$$\Rightarrow \partial_t J^* = -\frac{1}{2}x^2 + \frac{1}{2}(\partial_x J^*)^2 + x(\partial_x J^*)$$

Looks intimidating! But try $J^*(x, t) = \frac{1}{2}x^2 S(t)$

$$\Rightarrow \dot{S} = -1 + S^2 + 2S, \quad S(\tau) = 0$$

$$\Rightarrow u^* = -\partial_x J^* = -Sx \equiv -Kx$$

Now we can find $\dot{x} = -x - Kx = -(1+K)x$, $x(0) = x_0$, etc.

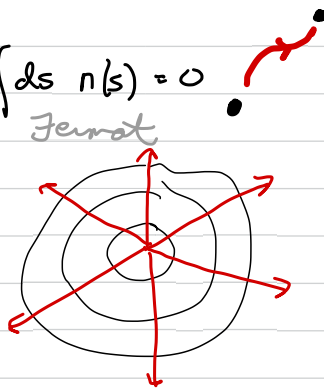
HJB vs. Euler-Lagrange

- Why do we have two apparently different ways to solve the optimal control problem?
- Same story in classical mechanics, optics, ...

Eg. , Optics

① **Calculus of variations**: $\delta \int ds n(s) = 0$ Fermat

② **Eikonal** (Huygen's wavefronts)
PDE for wavefronts.



So we can solve for rays (trajectories)
or wavefronts (cost functions)

Since rays are \perp wavefronts, methods are equiv.

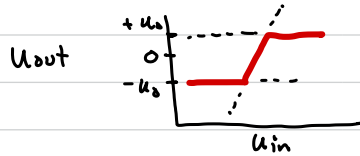
- **HJB** usually much harder to solve, but you get sol'n for all x_0 at once.
- **Euler-Lagrange** is simpler but has to be redone for each x_0 .

7.5 Hard constraints

soft: $J = \varphi[x(\tau)] + \dots$
 $\alpha = \dots \int \frac{1}{2} dt R u^2(t)$

hard: $x(\tau) = x_\tau$
 $|u(t)| \leq u_0$

Notice that the hard constraint $|u| \leq u_0$ is a nonlinearity.

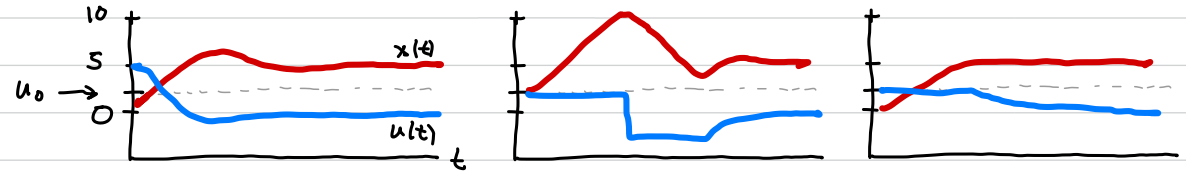


Strategies

- 0) Method 0: Buy a bigger actuator "increase control authority"
 - ie, increase u_0
- 1) Anti-windup - simple extension of PID
- 2) Minimum principle of Pontryagin (bang-bang control)

1) Anti-windup

Ex: $G = 1/s$, $\dot{x} = u$ (overdamped part.)
 PI control $K(s) = (1 + 1/s)$



No sat.

Saturation

Anti-windup

What happened in middle case?

$$u \sim \int_0^t dt' e(t') \quad e(t) = x_r - x(t)$$

When you exceed u -limit ($|u_0|$) integral keeps accum. to switch sign of $u(t)$, $x(t)$ must be below the setpoint long enough to "erase" the accumulated input.

Anti-windup: Stop integrating when u would exceed sat.

2) Minimum Principle + Bang-Bang control

- Assume $u(t)$ normalized so $|u(t)| \leq 1$
 - n -components \Rightarrow m -dim. hypercube

Ex: 1d dynamics, w/ constraints

$$J = \int_0^{\infty} dt \frac{1}{2} (x^2 + u^2), \quad \dot{x} = -x + u, \quad x(0) = x_0$$

$$\Rightarrow u = -kx \quad k^* = \sqrt{2} - 1 \quad \Rightarrow \begin{aligned} x(t) &= x_0 e^{-\sqrt{2}t} \\ u(t) &= -k^* x_0 e^{-\sqrt{2}t} \end{aligned} \quad |u(t)| < 1$$

When $x_0 > (k^*)^{-1} = \sqrt{2} + 1$, $u(0) < -1 \Rightarrow$ sat.

Intuitive resolution: $u(t) = -1 \quad t < \tau_0$
 $= -kx \quad t \geq \tau_0$

where $x(\tau_0) = x_0 e^{-\tau_0} = 1$ fixes τ_0

Hamiltonian formalism

Classical Mech: Lagrangian $L(q, \dot{q}) = T - U$

Generalized momenta $p = \frac{\partial L}{\partial \dot{q}}$

Legendre transf: $H = p\dot{q} - L$

Hamilton's eqs: $\dot{q} = (\partial_p H)^T \quad \dot{p} = -(\partial_q H)^T$

kinetic en. / potential en.

If $H = H(p, q)$ does not have an explicit t -depend.

$$\frac{dH}{dt} = \frac{\partial H}{\partial p} \dot{p} + \frac{\partial H}{\partial q} \dot{q} = 0 \quad (\text{via Ham. eqs.})$$

- note change of sign!

Control-theory version: $H = L + \lambda^T \dot{x} = L + \lambda^T f$

$$\dot{x} = (\partial_{\lambda} H)^T = f \quad \dot{\lambda} = -(\partial_x H)^T \quad (\partial_u H)^T = 0$$

Much simpler than Euler-Lagrange (p. 4)

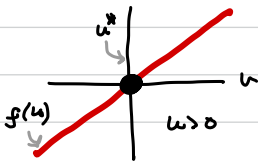
Pontryagin: $\mathcal{H}(x, \lambda) = \inf_{u \in U} H(x, \lambda, u)$

$$\dot{x} = (\partial_x \mathcal{H})^T, \quad \dot{\lambda} = -(\partial_x \mathcal{H})^T$$

$$x(0) = x_0, \quad \lambda(\tau) = (\partial_x \varphi)^T|_{t=\tau}$$

If $u(t)$ is not constrained $\inf_u \Rightarrow \partial_u = 0$

With constraint, $u(t)$ might get stuck at boundary



$$\inf_{u > 0} f(u) = f(0)$$

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$$\frac{d}{dt} \begin{pmatrix} x_1 \\ x_2 \end{pmatrix} = \begin{pmatrix} 0 & 1 \\ 0 & 0 \end{pmatrix} \begin{pmatrix} x_1 \\ x_2 \end{pmatrix} + \begin{pmatrix} 0 \\ 1 \end{pmatrix} u = \begin{pmatrix} \dot{x}_2 \\ u \end{pmatrix}$$

Ex. Moving in minimal time

- free particle in space: $\dot{x}_1 = x_2, \dot{x}_2 = u \quad (u = F/m)$

Goal: go from $\begin{pmatrix} x_1 \\ x_2 \end{pmatrix}_0 \rightarrow \begin{pmatrix} 0 \\ 0 \end{pmatrix}$ as fast as possible

Limits $|u(t)| \leq 1 \quad J = \int_0^\tau dt (1) \quad \tau$ not fixed

Running cost $L=1 \Rightarrow H = 1 + \lambda_1 x_2 + \lambda_2 u \rightarrow (\lambda_1, \lambda_2) \begin{pmatrix} x_2 \\ u \end{pmatrix}$

$$\Rightarrow \dot{\lambda}_1 = -\frac{\partial H}{\partial x_1} = 0, \quad \dot{\lambda}_2 = -\frac{\partial H}{\partial x_2} = -\lambda_1$$

$$\Rightarrow \lambda_1 = \text{const}, \quad \lambda_2 = -c_1 t + c_2$$

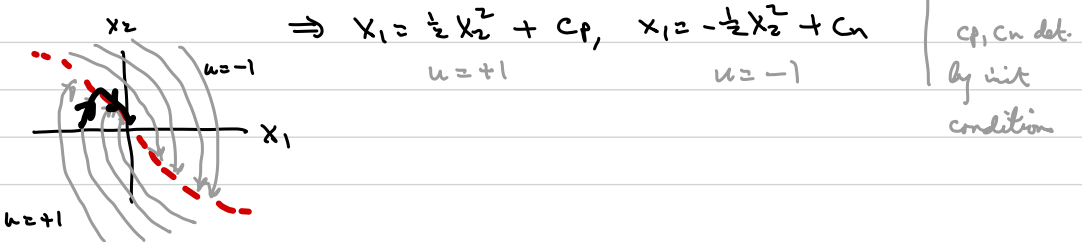
Can't min. H by $\frac{\partial H}{\partial u} = 0$, but can min. at boundary.

$\min_u H \Rightarrow u = -\text{sign}(\lambda_2)$ at all times

$$\Rightarrow u(t) \text{ always } = \pm 1$$

Since $\lambda(t)$ varies linearly, $u(t)$ switches once.

Solve eqs. of motion separately for $u = \pm 1$



Bang-bang control

In the previous problem, the control "lived" at $u = \pm u_0$

This behavior, "bang-bang control," results when $H(x, \lambda, u)$ is linear in u (or has no min. in range)

7.6 Feedback

The calc. of variations approach (or Hamiltonian) lead to a control $u^*(t)$ to take sys from $x_0 \rightarrow x_T$.
This is open loop, feedforward control. via optimal $x(t)$

If there are disturbances or modeling inaccuracies, then trajectory will deviate from optimal.
 \Rightarrow need some kind of feedback

- 1) Local linear feedback
- 2) Model Predictive Control

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① Local linear feedback

$$J = \varphi[x(\tau)] + \int_0^{\tau} dt L(x, u), \quad \dot{x} = f(x, u), \quad x(0) = x_0$$

$$E-L \Rightarrow \dot{\lambda} = -(\partial_x f)^T \lambda - (\partial_x L)^T, \quad 0 = (\partial_u f)^T \lambda + (\partial_u L)^T$$

- Assume we have solved the "nominal feedforward" problem:
 $\Rightarrow x_{ff}(t), u_{ff}(t), \lambda_{ff}(t)$
- Perturb about nominal solution:

$$x(t) = x_{ff}(t) + \delta x(t), \quad u(t) = u_{ff}(t) + \delta u(t), \quad \lambda(t) = \lambda_{ff}(t) + \delta \lambda(t)$$

- Because the nominal "ff" solution is optimal, $\delta J = 0$

$$\Rightarrow \delta^2 J = \frac{1}{2} \delta x^T (\partial_{xx} \varphi) \delta x \Big|_{t=\tau} + \int_0^{\tau} dt (\delta x^T \quad \delta u^T) \begin{pmatrix} Q & M \\ M & R \end{pmatrix} \begin{pmatrix} \delta x \\ \delta u \end{pmatrix}$$

with $Q(t) = \partial_{xx} L$, $M(t) = \partial_{xu} L$, $R(t) = \partial_{uu} L$
 - evaluated along $x_{ff}(t)$ and $u_{ff}(t)$

Augment the cost pert. w/ perturbed dynamics. $\text{i.e. } Q = \frac{\partial^2 L(x, u)}{\partial x^2} \Big|_{x_{ff}, u_{ff}}$

$$\delta^2 J' = \delta^2 J + \delta \lambda^T [A \delta x + B \delta u - \delta \dot{x}] \quad A(t) = \partial_x f, \quad B(t) = \partial_u f$$

$$E-L: \quad \delta \dot{\lambda} = -Q \delta x - M \delta u - A^T \delta \lambda, \quad \delta u = -R^{-1} (M \delta x + B^T \delta \lambda)$$

This is just a slightly more complicated LQR problem!

- all matrices time dependent $A \rightarrow A(t)$, etc.
- quadratic costs have cross-term $M(t)$

Fortunately, all steps of LQR carry through analogously.

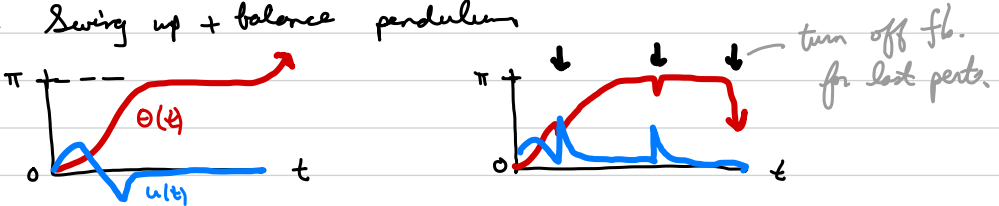
Let $\delta \lambda = S \cdot \delta x \Rightarrow \dot{S} = -Q + MR^{-1}M^T - A^T S - SA' + SBR^{-1}$
 where $A' = A - BR^{-1}M^T$

Optimal feedback gains: $K(t) = R^{-1} [B^T S + M^T]$, $\delta u_{fb} = -K \delta x$

The full control signal is then

$u(t) = u_{ff}(t) + u_{fb}(t) = u_{ff}(t) + K(t) [x_{ff}(t) - x(t)]$

Ex: Swing up + balance pendulum



Can choose different feedback laws

1. Time-dep. LQR *what we should do...*
2. Quasistationary LQR
3. Basic LQR *fixed gains for "typical" x_0*
4. Heuristic control: *pick gains by heuristic method*

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Nonlinear Observers

(set $u=0$ for simplicity)

$$\dot{x} = f(x), \quad y = h(x) \quad (p \text{ outputs})$$

$$\text{Obs: } \dot{\hat{x}} = f(\hat{x}) + L(y - \hat{y}), \quad \hat{y} = h(\hat{x})$$

$$\begin{aligned} \text{notice that } e = x - \hat{x} &\Rightarrow \dot{e} = f(x) - f(\hat{x}) - L[h(x) - h(\hat{x})] \\ &\approx (\partial_x f) e - L(\partial_x h) e \\ &= (A - Lc) e \quad \text{as before} \end{aligned}$$

Because we approx $f(x) - f(\hat{x}) \approx Ae$, this scheme works if systems begin (and stay) "close enough".

Model Predictive Control (MPC)

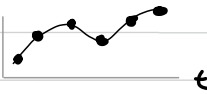
- Compute ff from $x(t)$ to $x(t+\tau) \Rightarrow u_{ff}(t)$
- Apply $u_{ff}(t)$ for short time ("one step")

"Feedback by repeated ff"

- good for problems w/ constraints
- costly to compute \Rightarrow good for "slow" problems
- widely used in "slow" industries (eg chemical plants)

Numerical Methods

Direct: $\min_{u(t) \in U} J[u(t); x_0]$

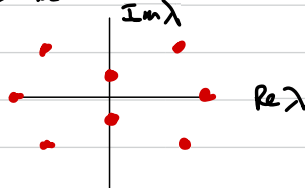
Project $u(t)$ on finite set $u(t)$ 

$$u: u(t) = \sum_n a_n \varphi_n(t) \quad \text{basis funct.}$$

Then solve directly (often non-convex )

Indirect: solve rec. eqs. (Euler-Lagrange, PMP)

• $n \rightarrow 2n + N$ constraints dim

Hamiltonian H real \Rightarrow 

\Rightarrow stiff eqs.

(beard for shooting methods)

\rightarrow solve by **Newton's method**

\rightarrow can write **Jacobian** as band diag $\Rightarrow \mathcal{O}(N)$
can even solve each stage in \parallel !