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international centre for theoretical physics

**ICTP/UCSB/TWAS
MINIWORKSHOP ON "FRONTIERS IN MATERIALS SCIENCE"
15 - 18 May 2001**

301/1311-4

"High-Temperature Thermally-Insulative Coatings"

**C.G. LEVI
Materials Department
UCSB
USA**

Please note: These are preliminary notes intended for internal distribution only.



High-Temperature Thermally-Insulative Coatings

C.G. Levi

Departments of Materials and Mechanical Engineering
Materials Research Laboratory
University of California, Santa Barbara

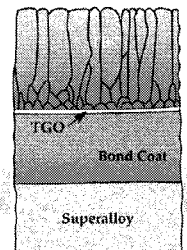
Presented at the

ICTP/UCSB/TWAS Workshop on
"Frontiers in Materials Science"

Trieste, Italy, May 15-18, 2001

Research supported by

The Office of Naval Research and the Department of Energy



Acknowledgments

UCSB

S.G. Terry, R.M.R. Leckie, N.R. Rebollo, J.R. Litty
J. Cho, D. Stave, J.P.A. Löfvander, V. Tolpygo
D.R. Clarke, T. Bennett

Princeton University

S. Chiras, A. Karlsson, D. Mumm, A.G. Evans

Max Planck Institut für Metallforschung

B. Raschkova, E. Sommer, M. Rühle

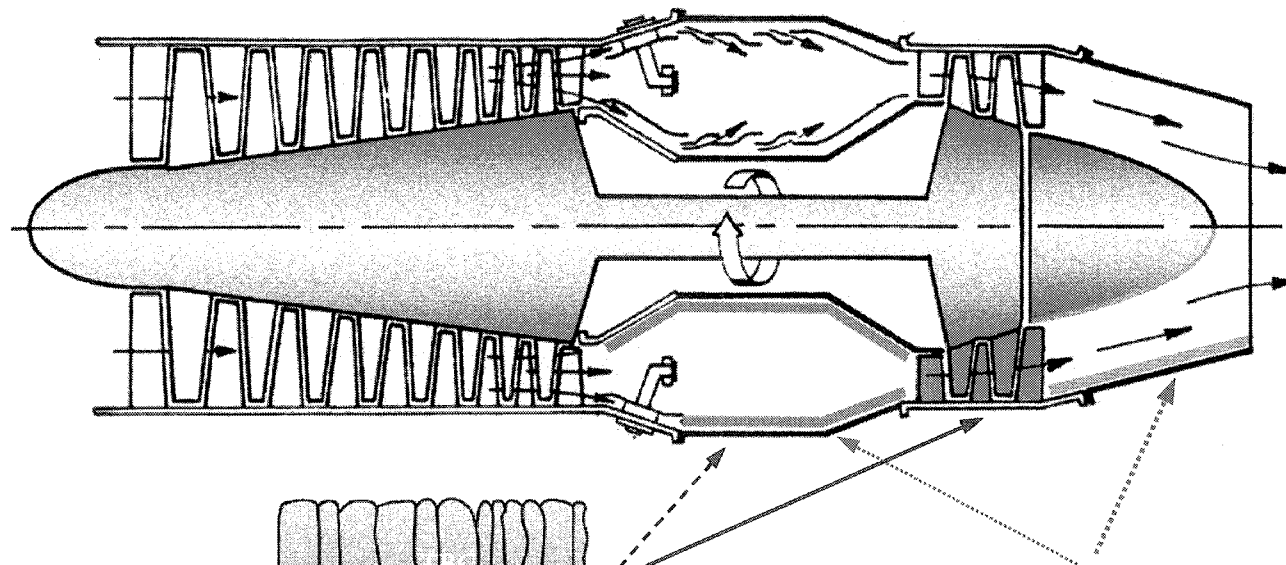
Laboratories

E. Fuller (NIST), O. Sudre (RSC), R. LeSar (LANL), U. Schulz (DLR)

Industry

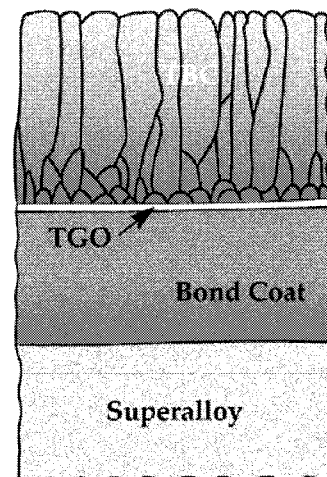
D. Wortman (GE-CRD), R. Darolia (GE-AE), M. Maloney (P&W)
J. Goedjen (SWPC), Z. Mutasim (Solar Turbines)
K. Murphy (Howmet), A. Feuerstein (Praxair)

Advanced Thermostructural Materials

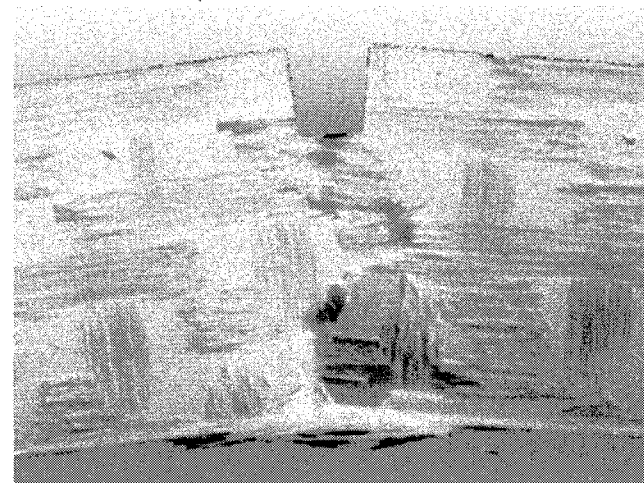


Research
at
UCSB

EB-PVD
Thermal
Barrier
Coatings

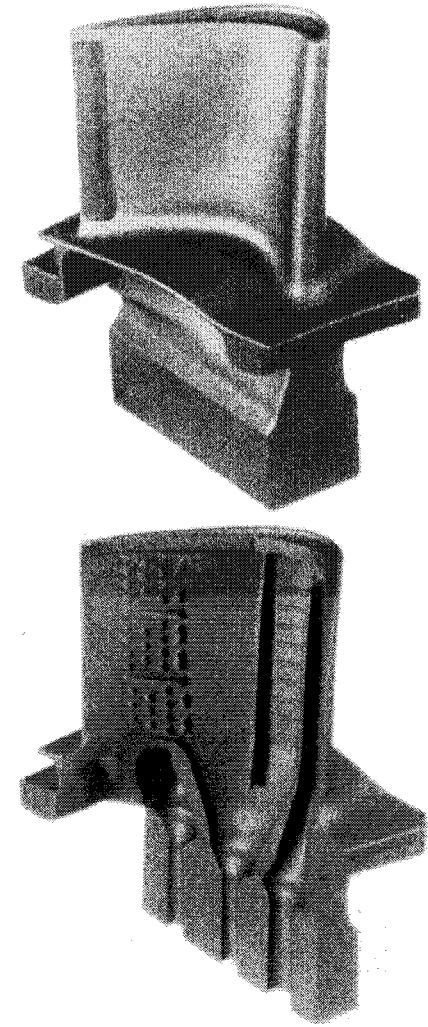
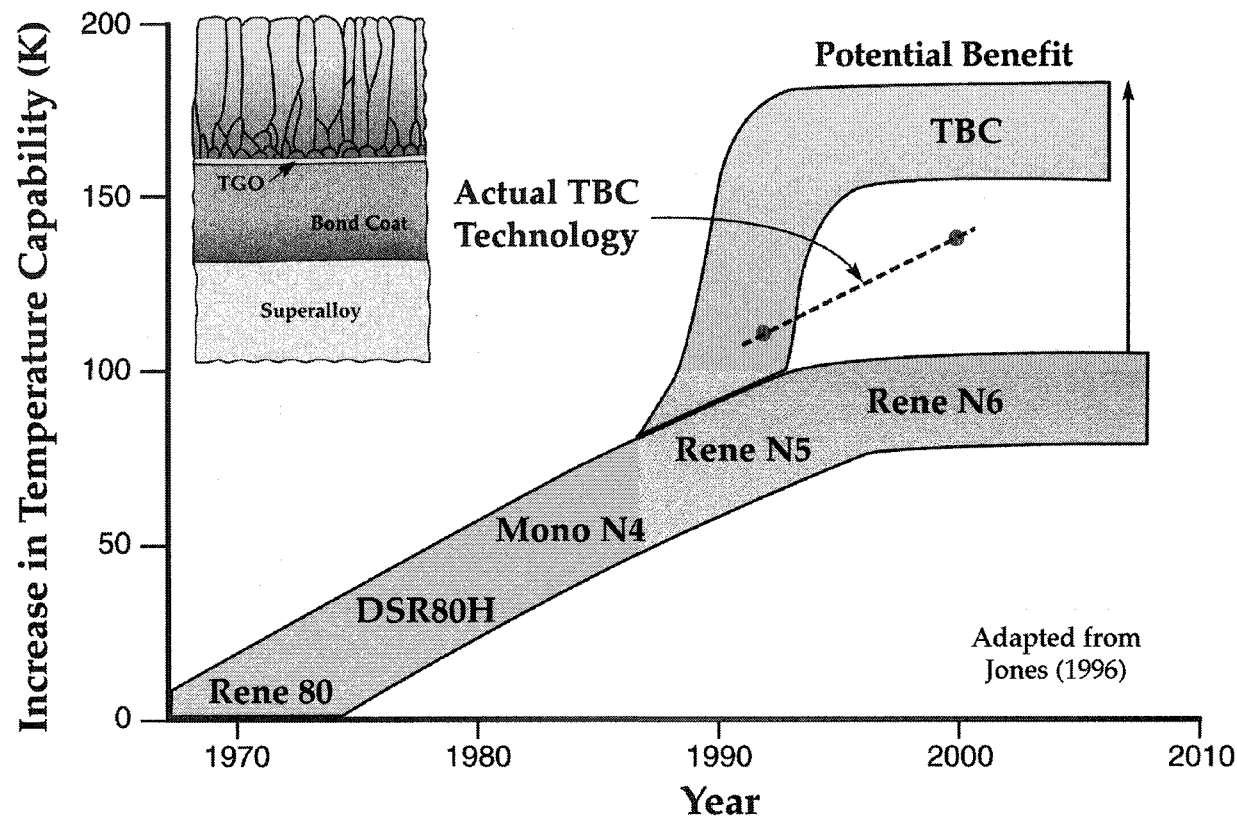


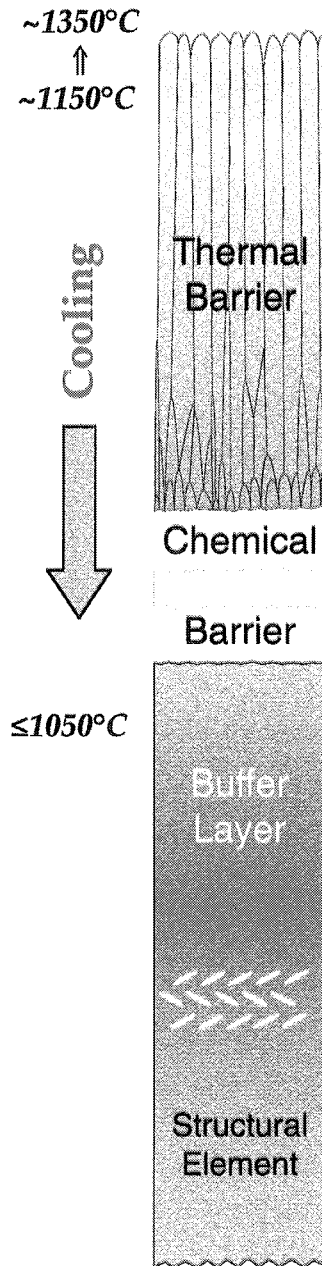
All-Oxide
Porous
Matrix
CFCCs



Benefits of Thermal Barrier Coatings

- Increase temperature capability of component
- Extend life and/or reduce cooling air





Anatomy of a TBC System

The Thermal Barrier: 7YSZ

- Low conductivity ($k \leq 1$ W/mK)
- Strain Tolerant
- Morphologically stable
- Erosion and Corrosion Resistant

The Chemical Barrier: Alumina (TGO)

- Low growth/diffusion kinetics
- Corrosion resistant
- Adherent over life of coating

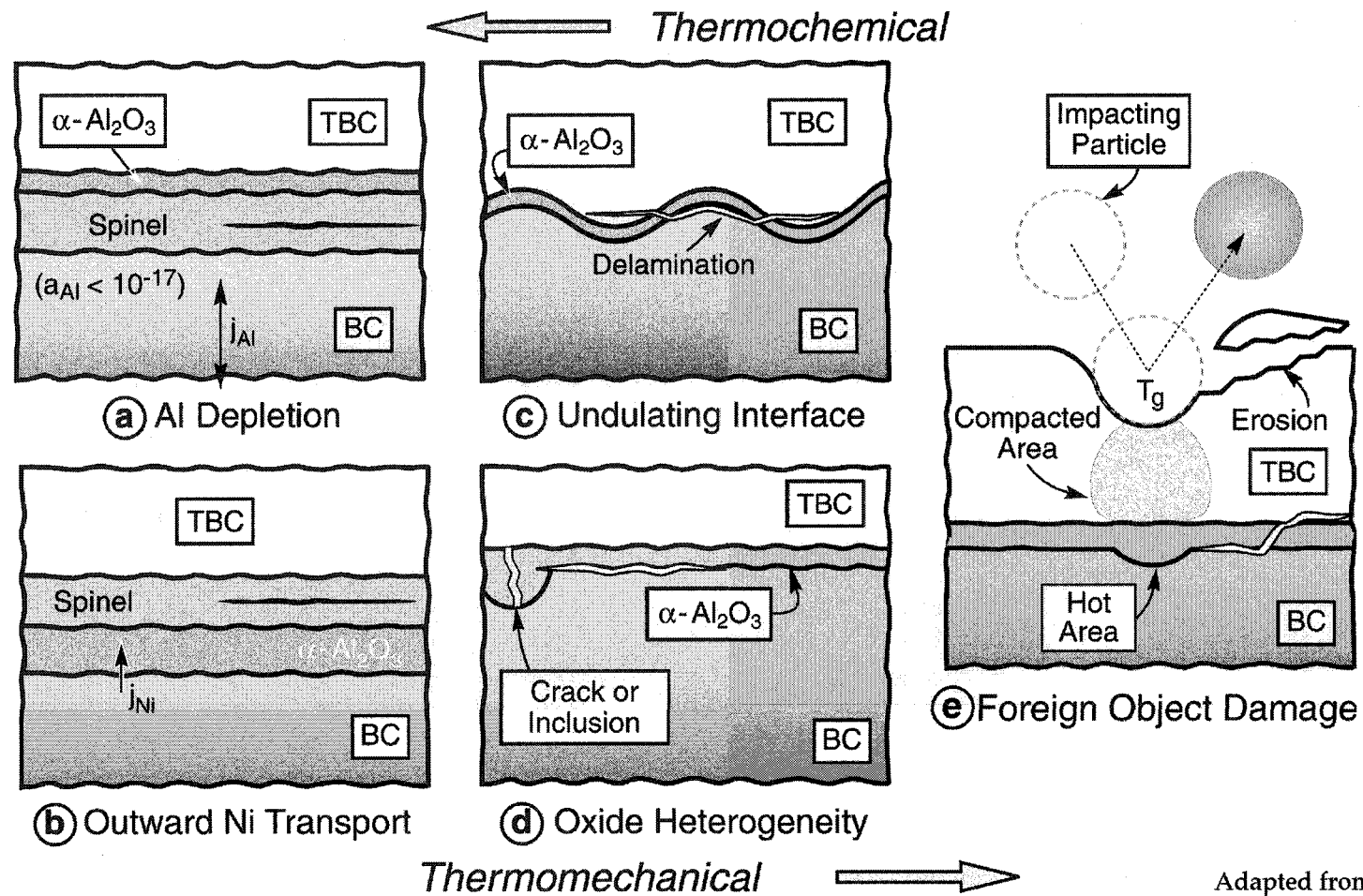
The Buffer Layer: Aluminide

- Sufficient Al to maintain stable TGO
- Microstructurally stable
- Adequate creep/yield strength
- Adequate toughness

The Structural Element: Superalloy

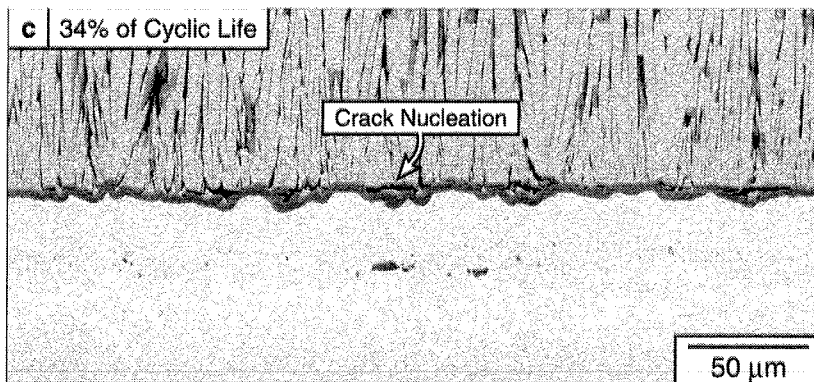
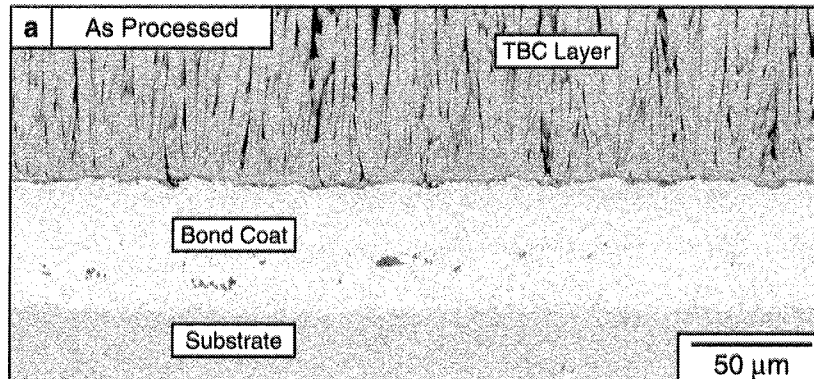
- Optimal mechanical properties
- Internally cooled

Partial Menu of Mechanisms leading to TBC Spallation

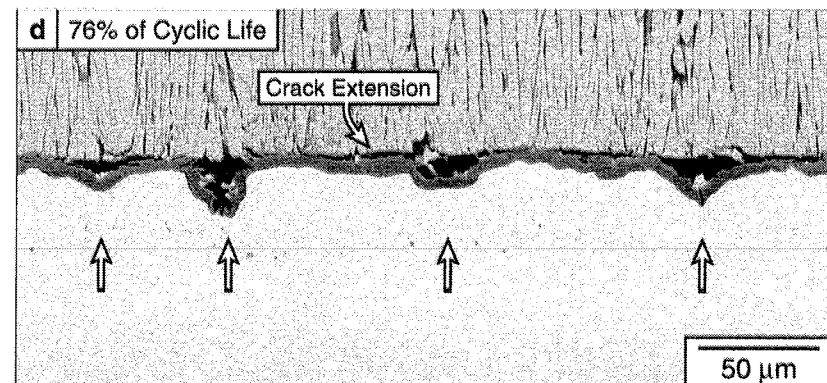
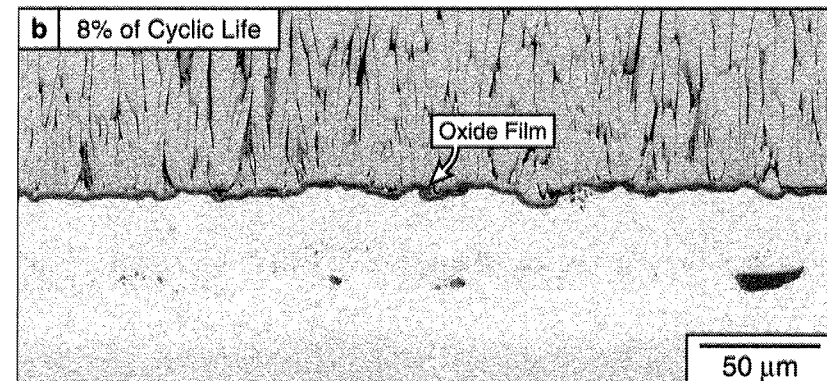


Adapted from A.G. Evans

Evolution of Interface Morphology under Cyclic Oxidation

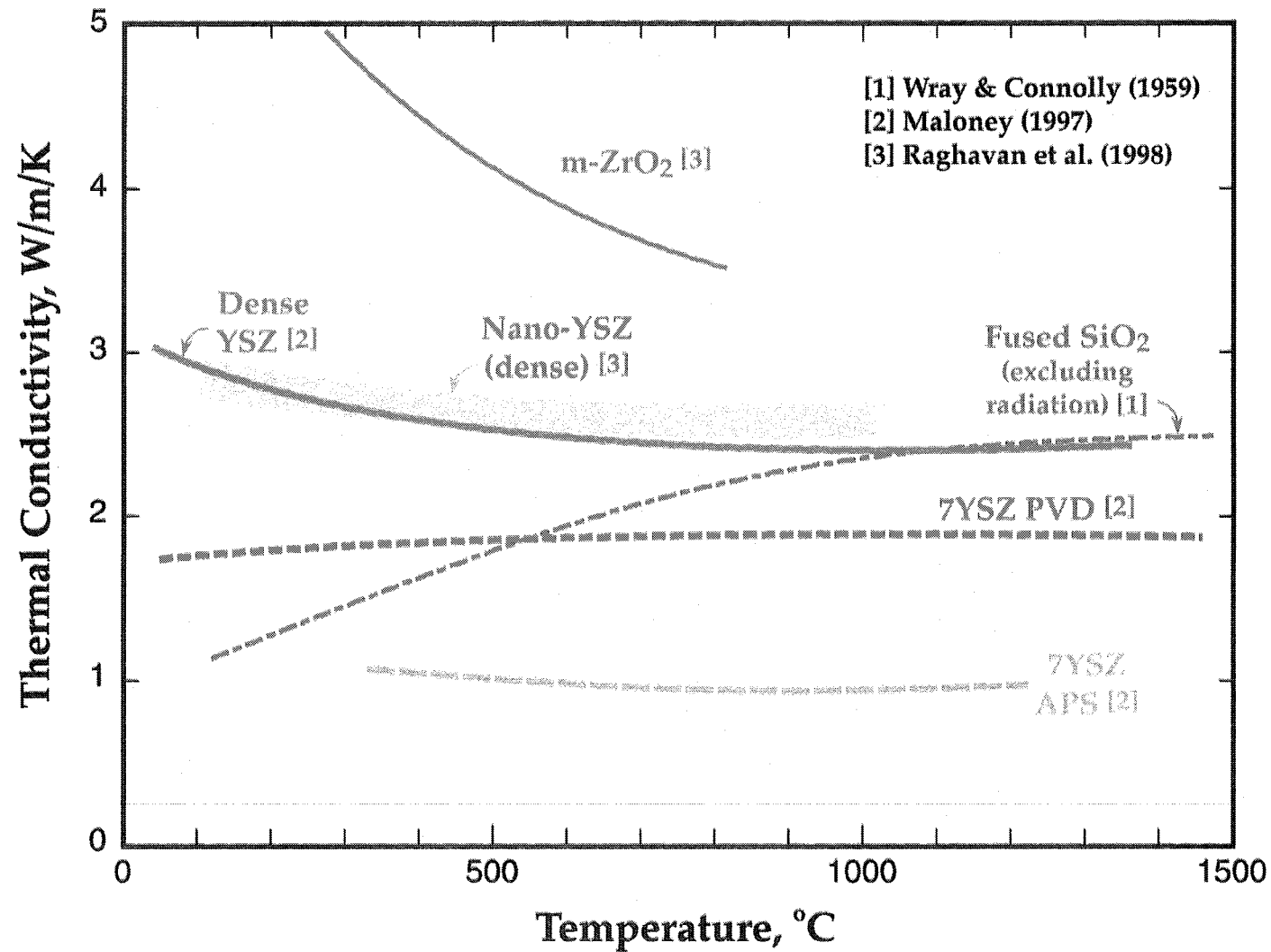


YSZ on (Ni,Pt) Al Bond Coat



Courtesy of D. Mumm
(Princeton University)

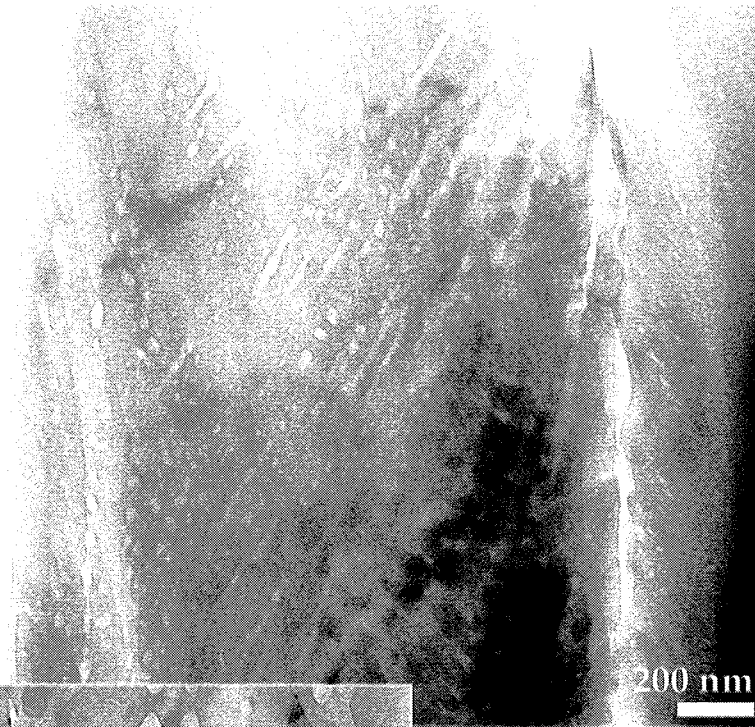
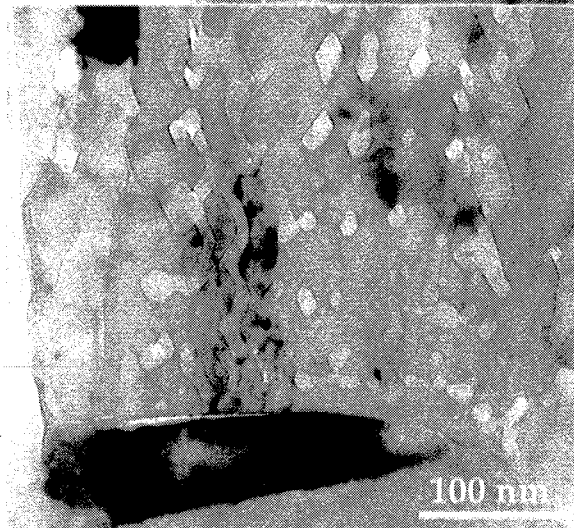
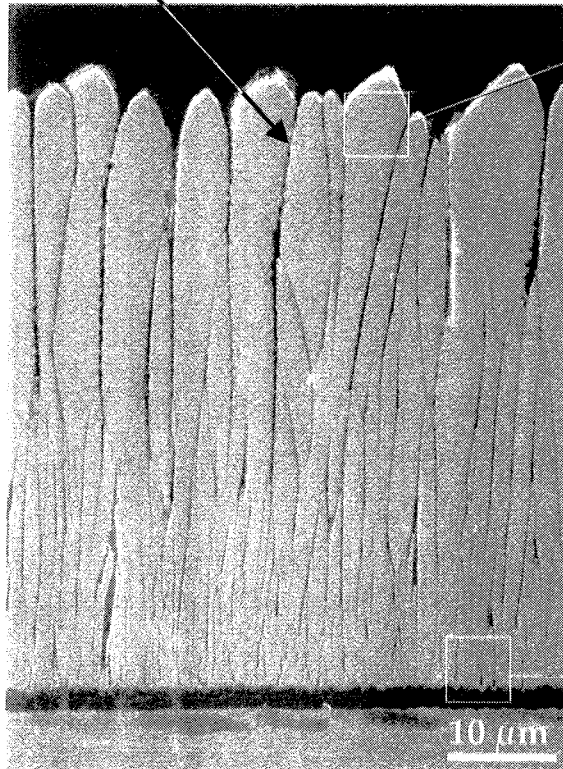
Thermal Conductivity of ZrO₂ and YSZ



Porosity: key to TBC Performance

Intercolumnar
⇒ Compliance

Intracolumnar
⇒ Insulation

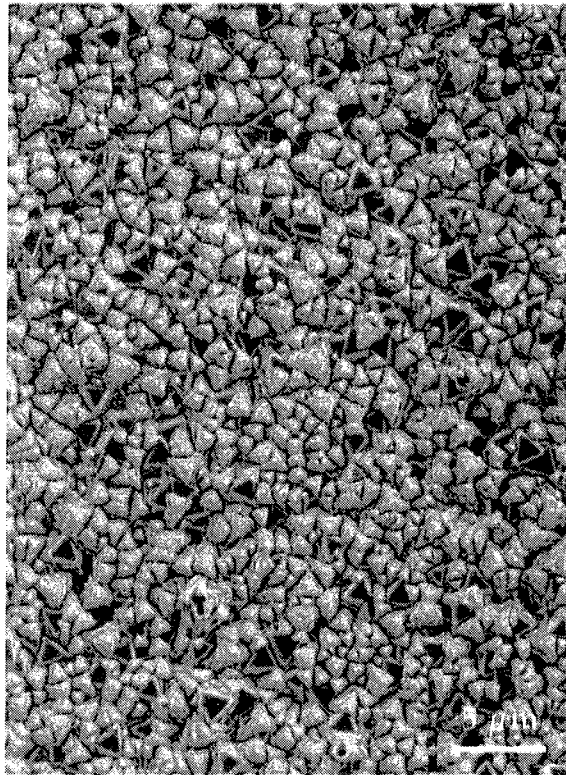


*Different
scales of
shadowing*

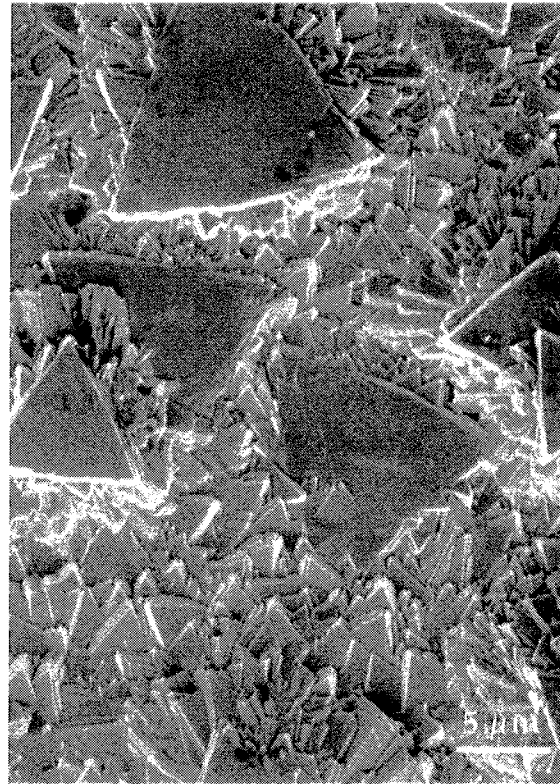
TEM on NiCrAlY
courtesy of E. Sommer
and M. Rühle
MPI-Stuttgart

Effect of Temperature on Surface Morphology and Texture

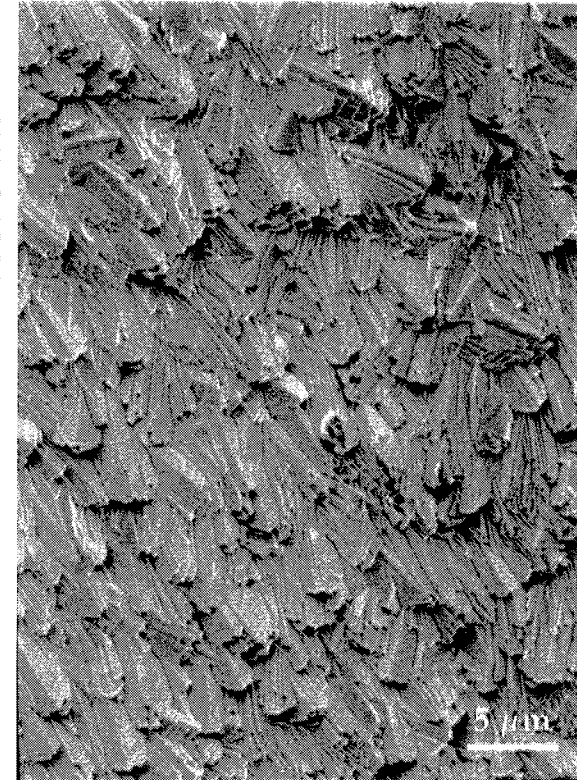
↓ Stationary Substrates



900°C: Dominant $\langle 111 \rangle$

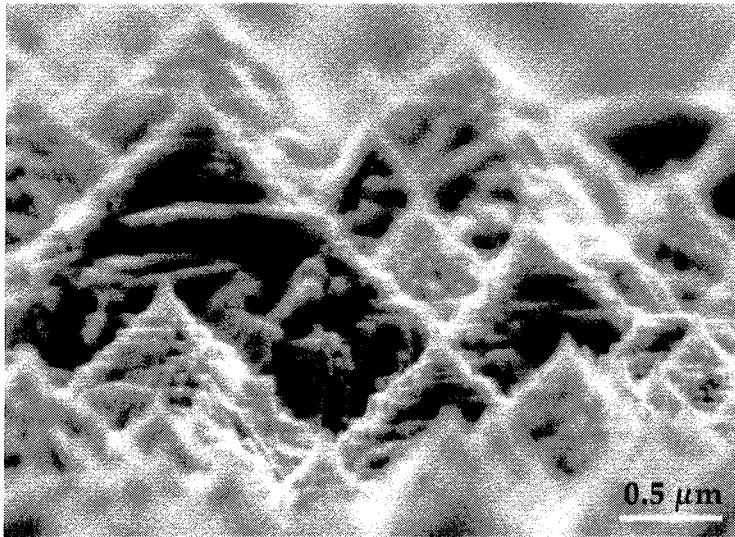
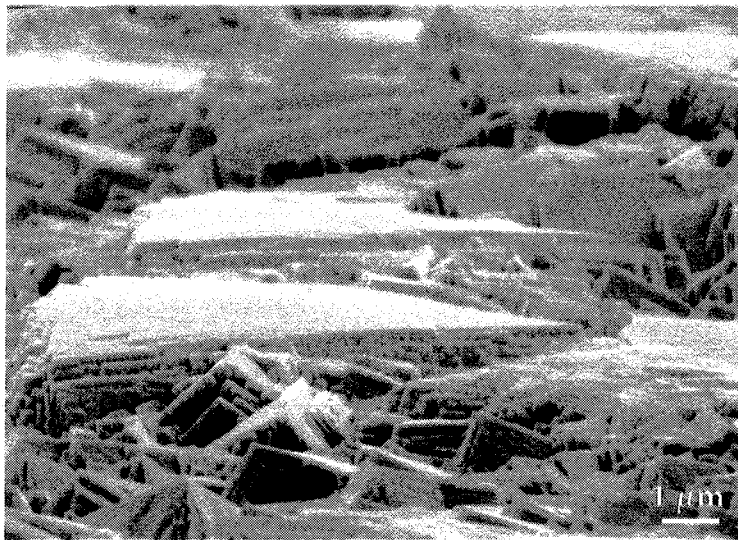


1000°C: $\langle 111 \rangle > \langle 220 \rangle$



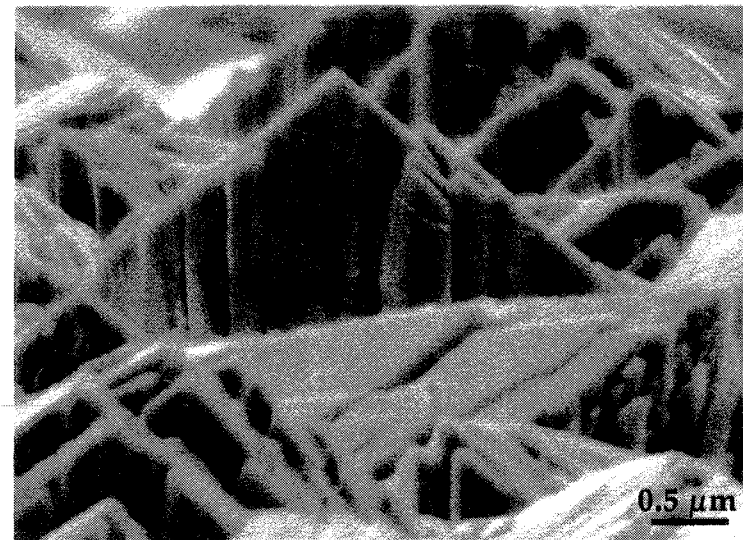
1100°C: $\langle 220 \rangle > \langle 311 \rangle > \langle 111 \rangle$

Normal Vapor Incidence
Pre-oxidized FeCrAlY Substrates

900°C: Dominant $\langle 111 \rangle$ 1000°C: $\langle 111 \rangle > \langle 220 \rangle$

Effect of Temperature on Tip Morphology

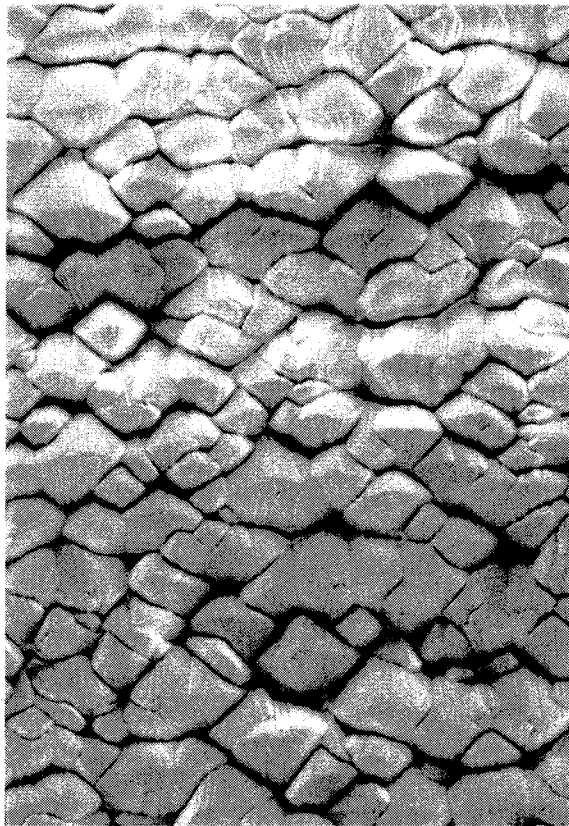
- Growth facets always $\{111\}$
- “111” columns grow with (111) facet normal to axis in two distinct morphologies
- Other column orientations grow with facets oblique to axis.

1100°C: $\langle 220 \rangle > \langle 311 \rangle > \langle 111 \rangle$

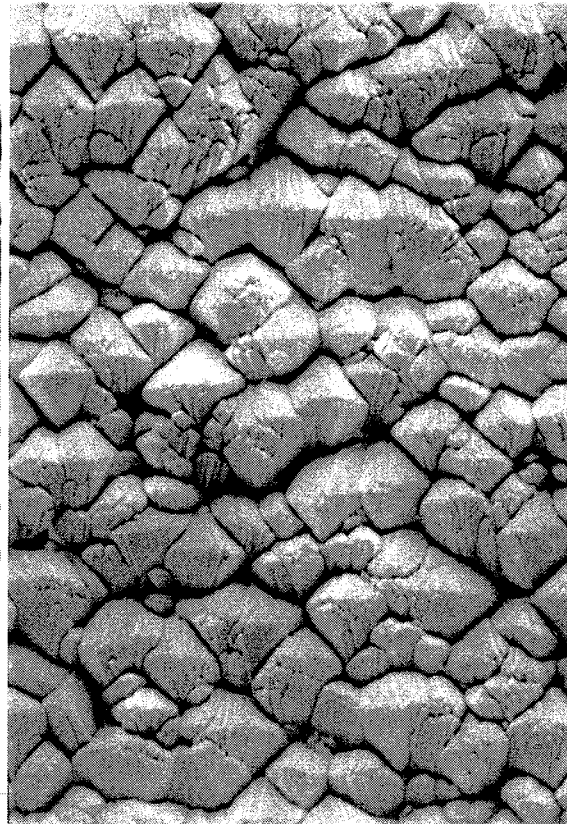
Effect of Temperature on Surface Morphology and Texture



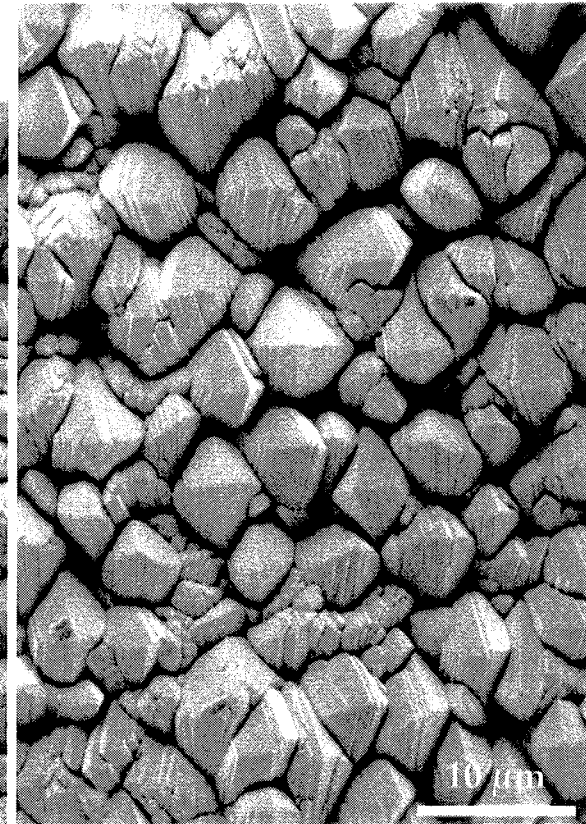
Rotating Substrates



900°C: $\langle 200 \rangle$

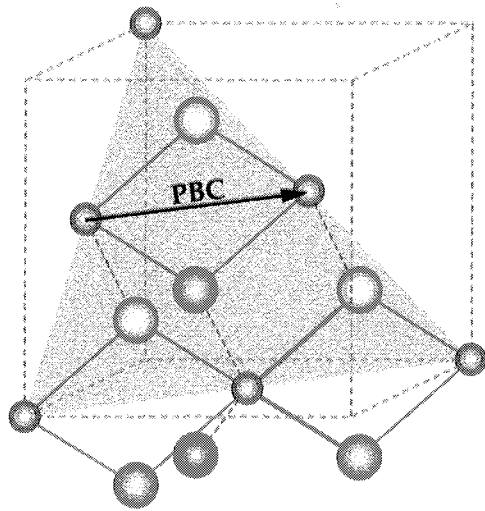


1000°C: $\langle 200 \rangle$



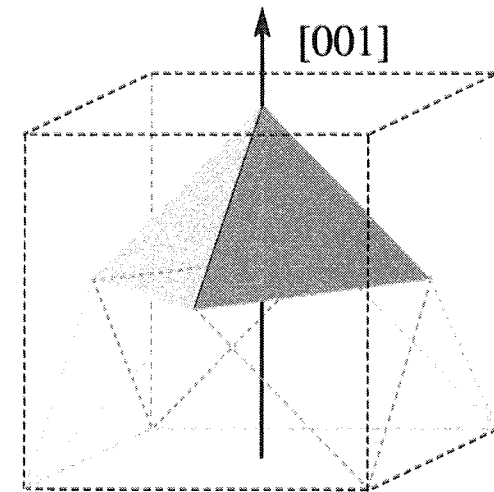
1100°C: $[002] + \langle 200 \rangle$

8 RPM, $\sim 0.9 \mu\text{m}/\text{min}$
(Flux $\sim 3.2 \mu\text{m}/\text{min}$)

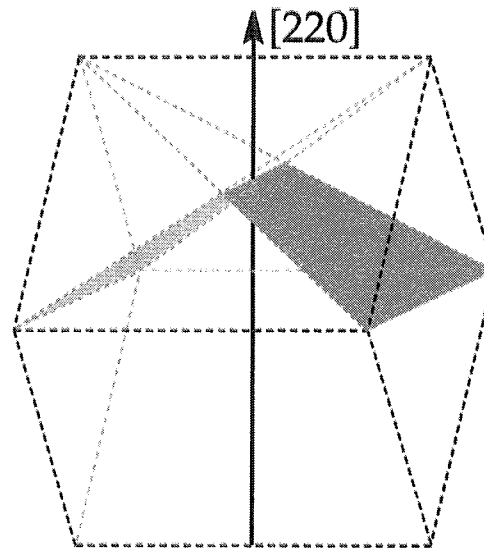
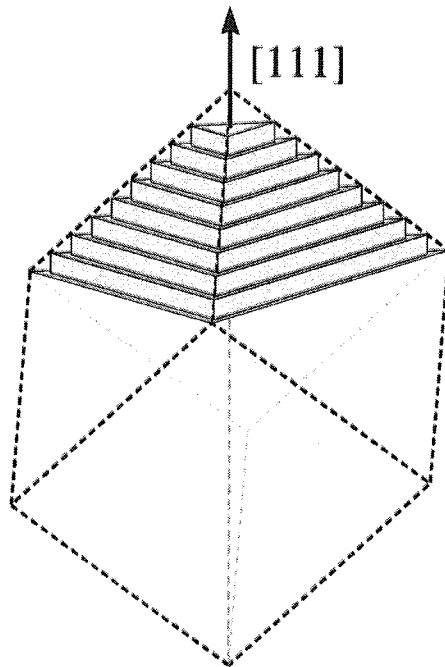


Texture and Tip Configurations

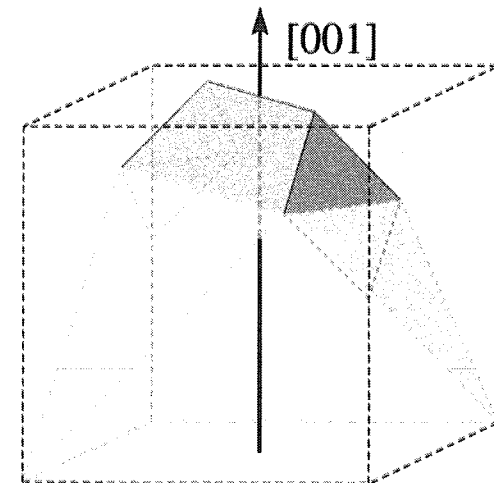
*{111} active growth facets,
independent of texture.
(Consistent with PBC analysis of
fluorite, Hartman, 1972)*



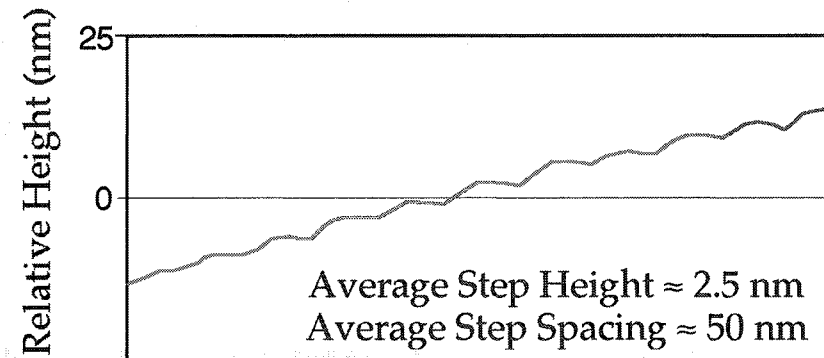
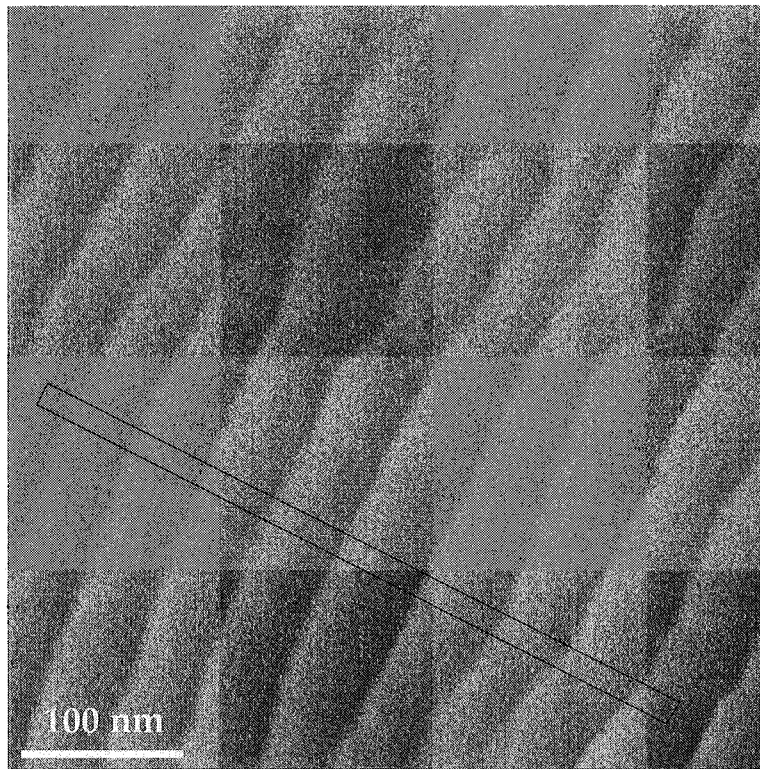
Rotating Substrates



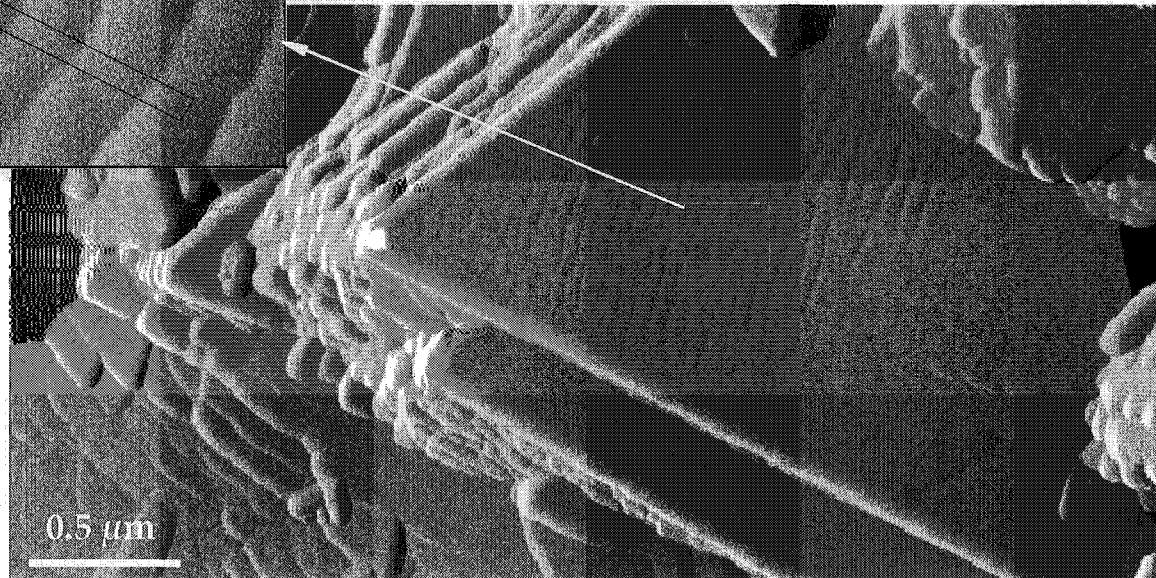
← *Stationary Substrates* →



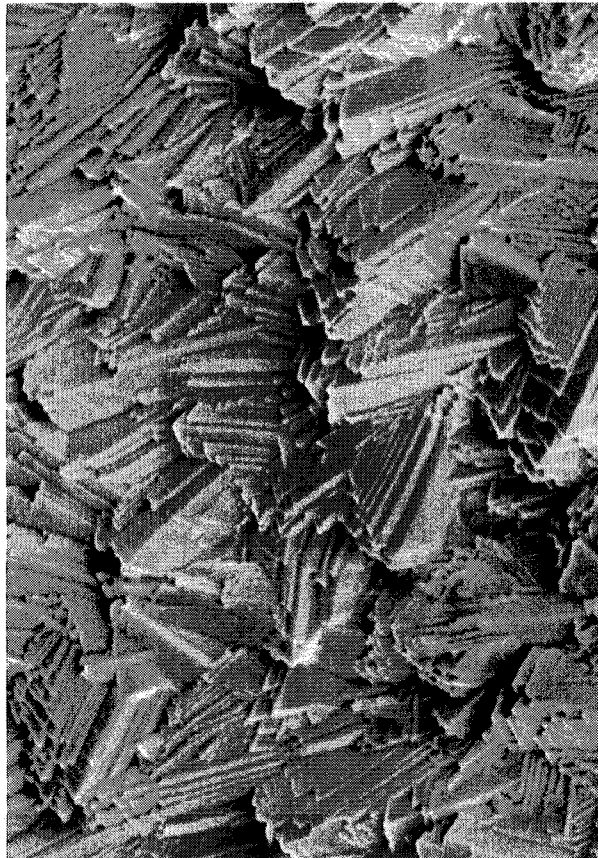
Step Propagation on "Flat" (111) Facet



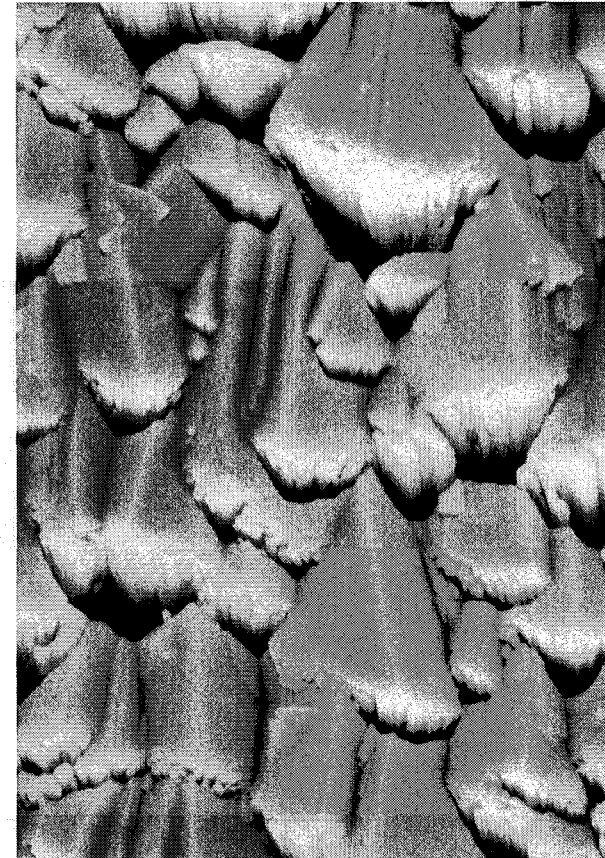
Stationary Deposition
Normal VIA
 1000°C , $1.1 \mu\text{m}/\text{min}$



In-Plane Texture Development Under Oblique Vapor Incidence

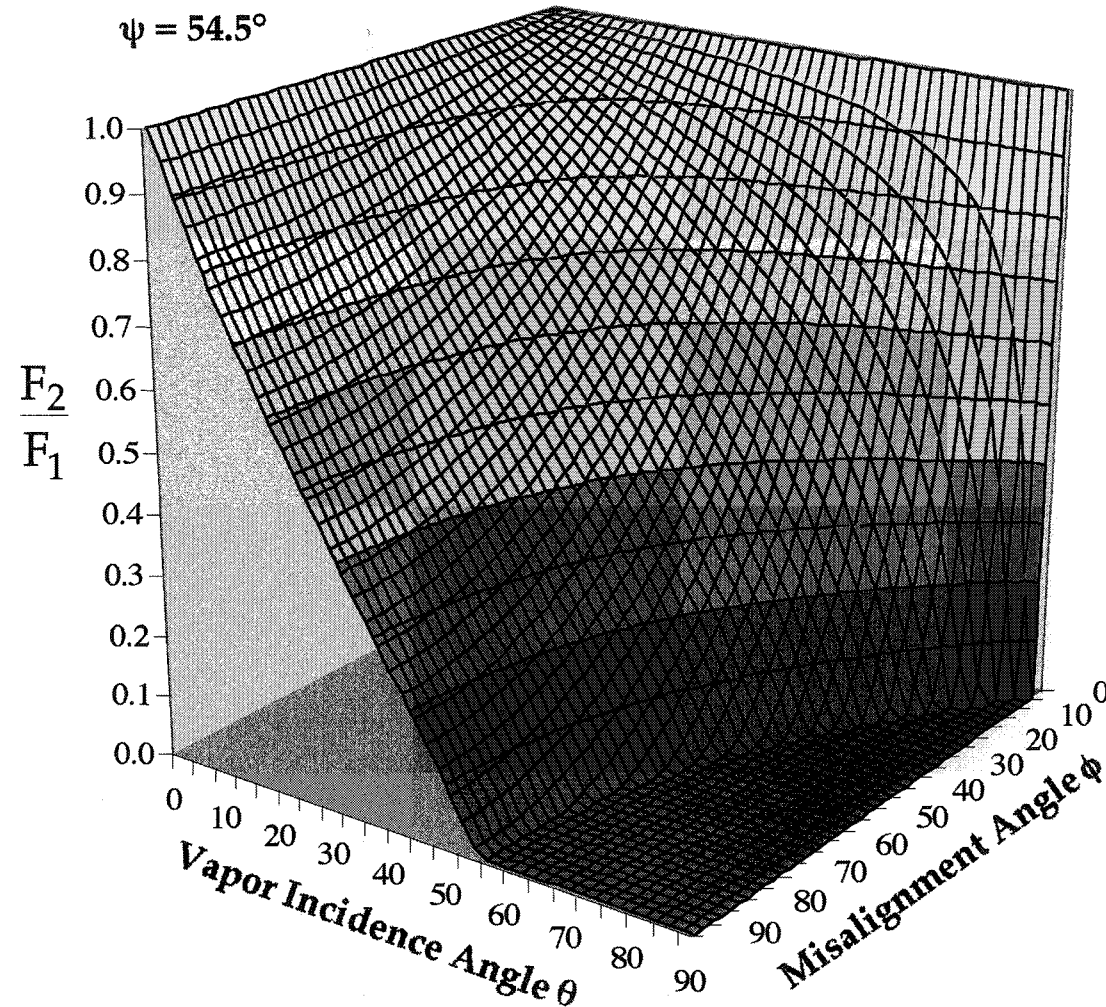


Normal VIA (0°)



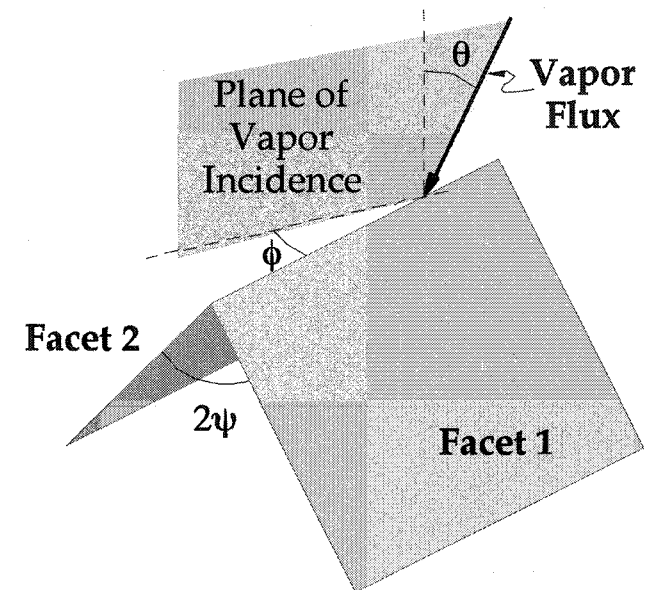
Oblique VIA (45°)

Stationary Deposition, 1100°C, ~1 $\mu\text{m}/\text{min}$



Geometric Argument for Evolution of In-Plane Texture

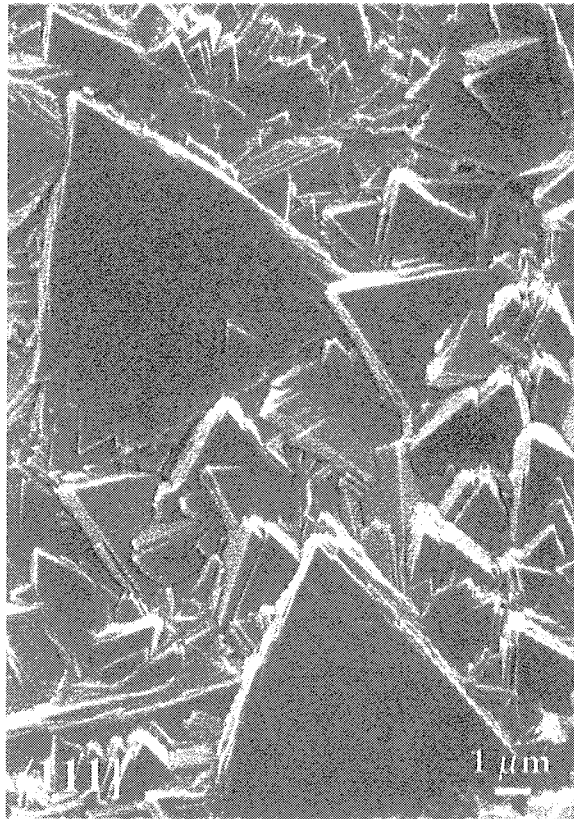
- Ridge misalignment under oblique vapor incidence results in asymmetric growth of rooftop column tip and eventual elimination.



Facet Flux Ratio

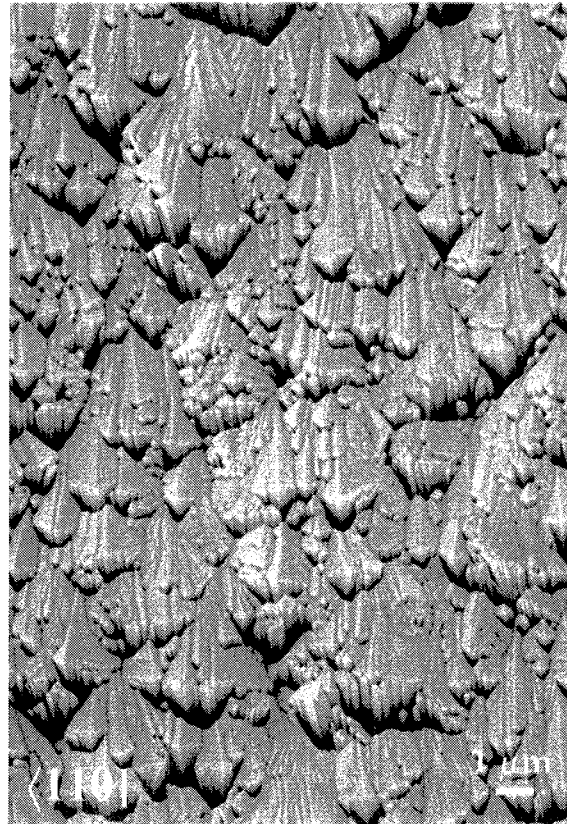
$$\frac{F_2}{F_1} = \frac{\cos\theta \sin\psi - \sin\theta \sin\phi \cos\psi}{\cos\theta \sin\psi + \sin\theta \sin\phi \cos\psi}$$

Effect of Vapor Incidence Pattern on Column Tip Morphology

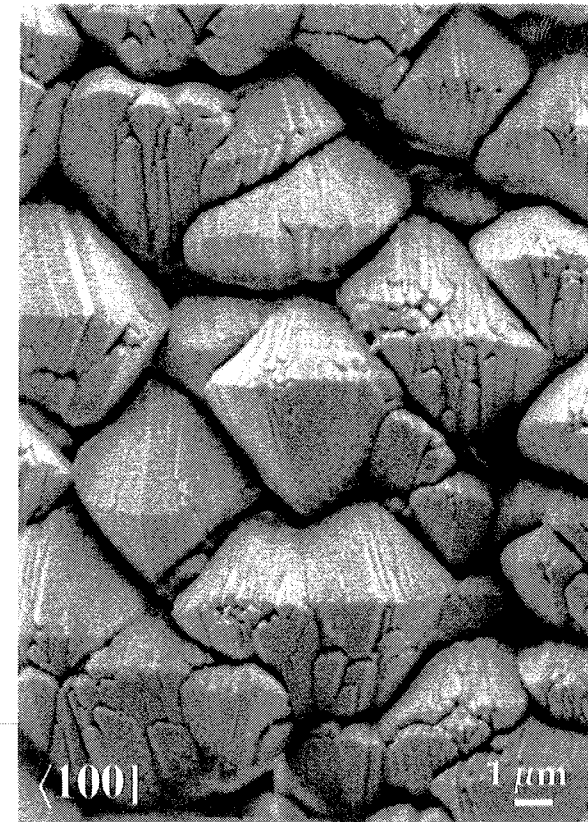


Stationary, Normal VIA

Deposition Temperature = 1000°C
Net Deposition Rate $\approx 1 \mu\text{m}/\text{min}$



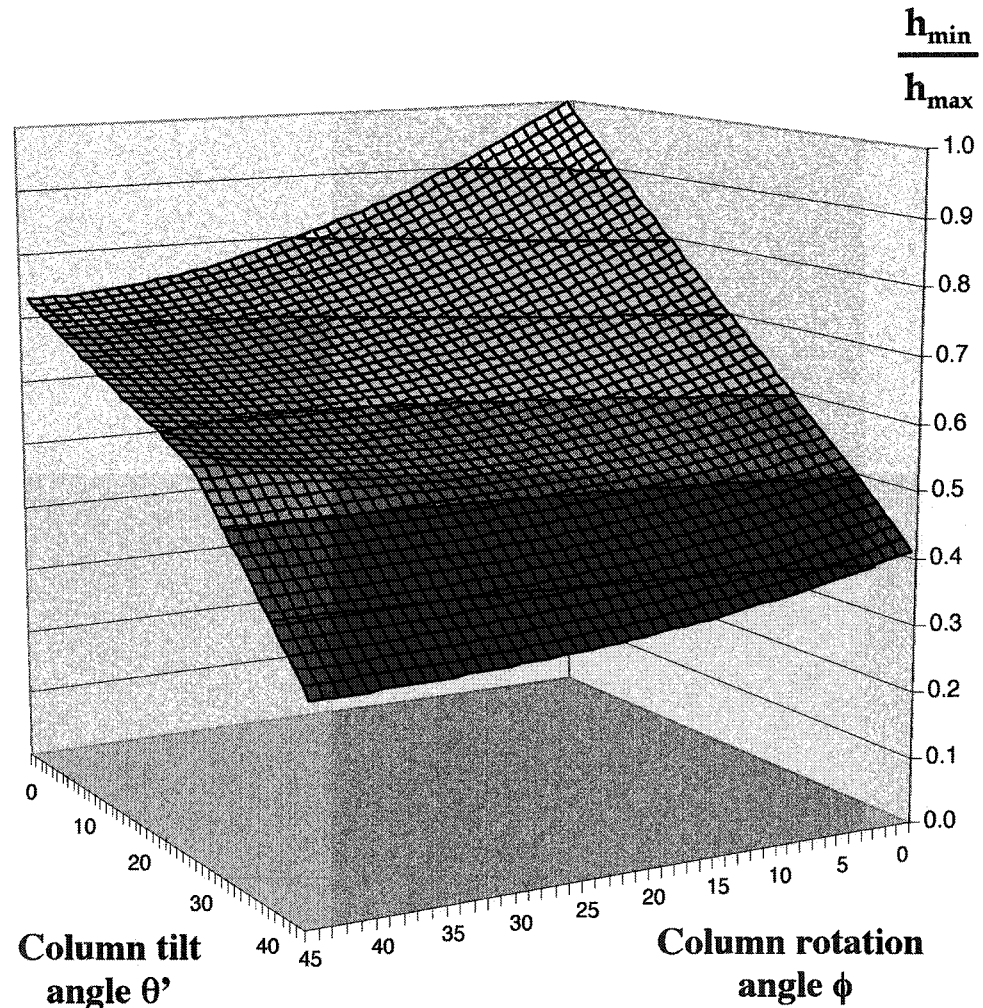
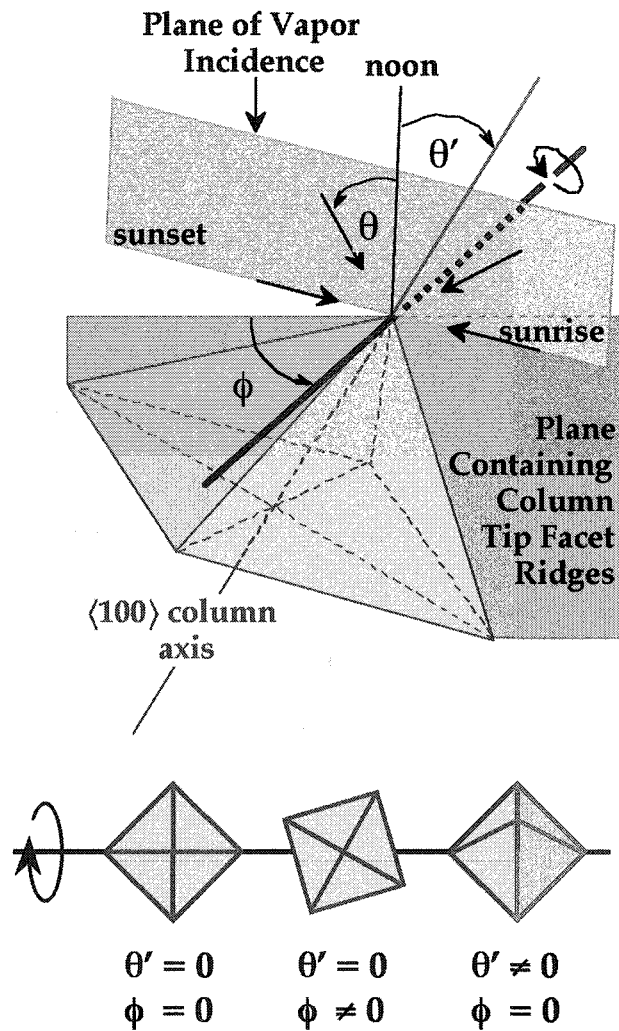
Stationary, 45° VIA



Rotating, 8 RPM

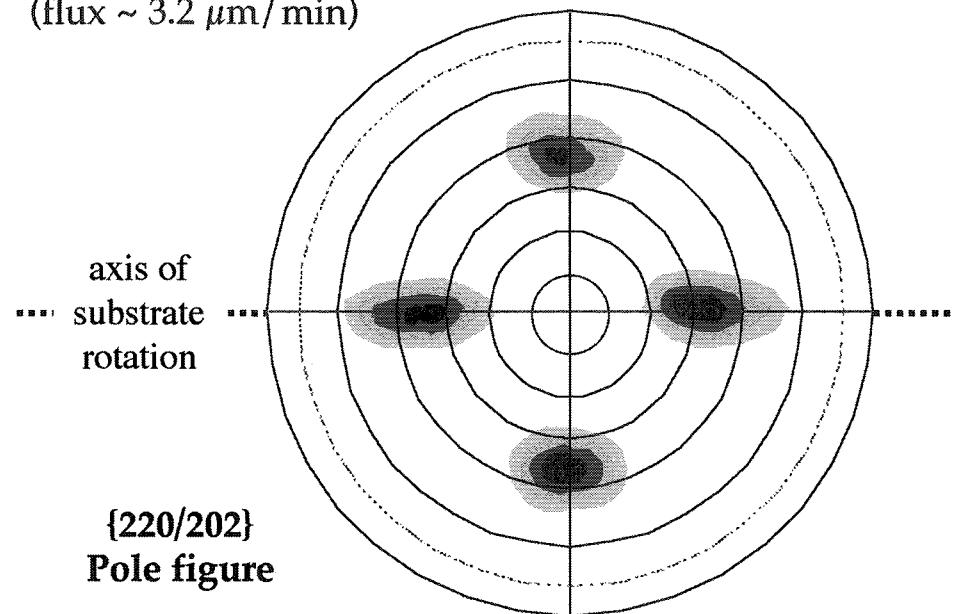


Selection of In-Plane Orientation upon Rotation

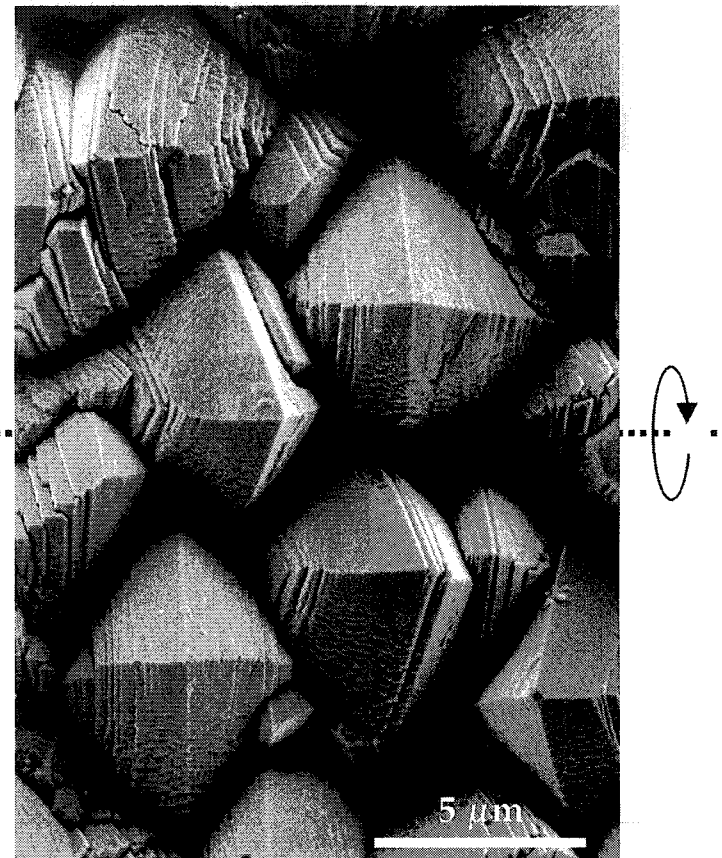


Deviations from Dominant Texture

1100°C, 8 RPM
 $\sim 0.9 \mu\text{m}/\text{min}$
(flux $\sim 3.2 \mu\text{m}/\text{min}$)



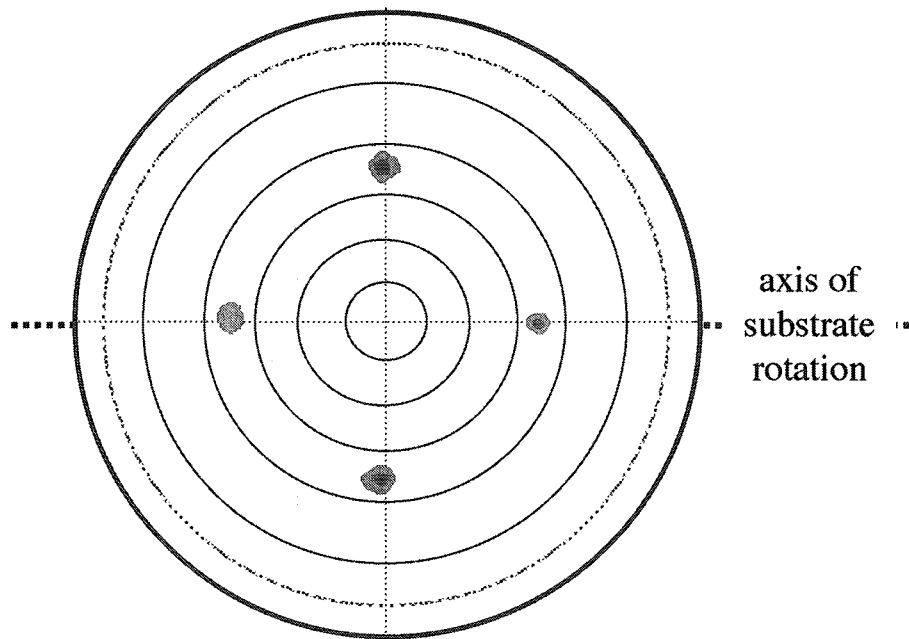
*Larger column orientation scatter
along plane parallel to the rotation axis*



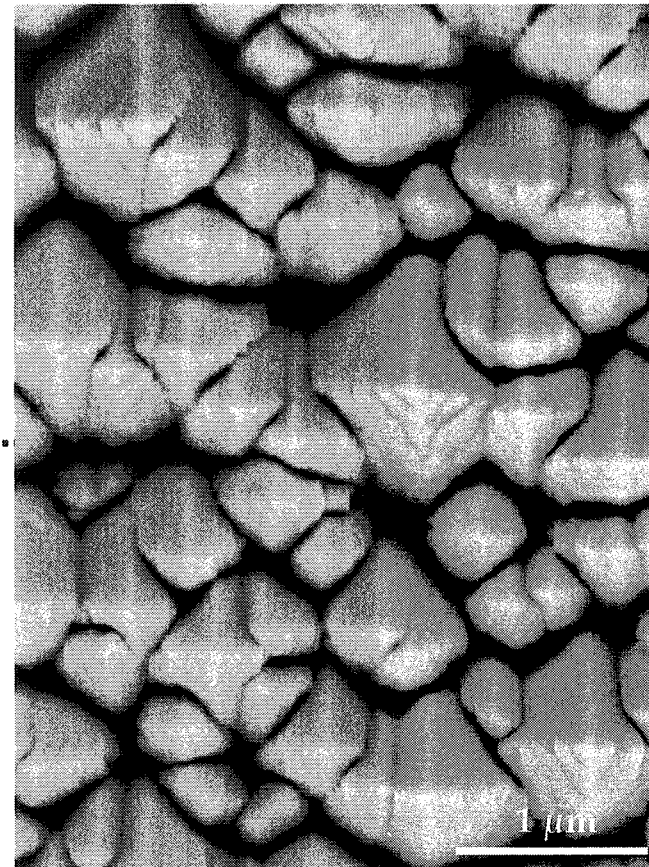
[002] + •200 Texture

Texture Dispersion on Flat Sapphire Substrate

1000°C, 8 RPM, $\sim 0.3 \mu\text{m}/\text{min}$
{220/202} Pole figure

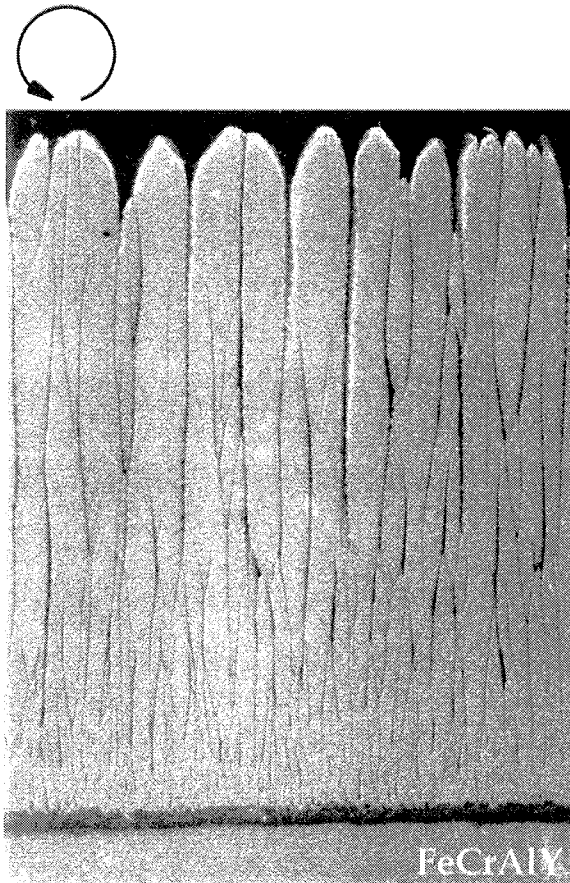


*Reduced scatter in column tip
orientation and texture anisotropy*

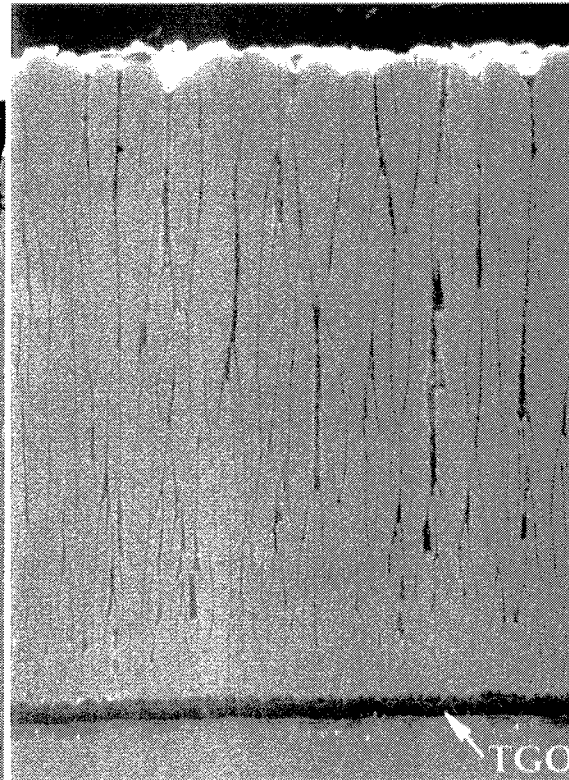


$\langle 200 \rangle$ Texture

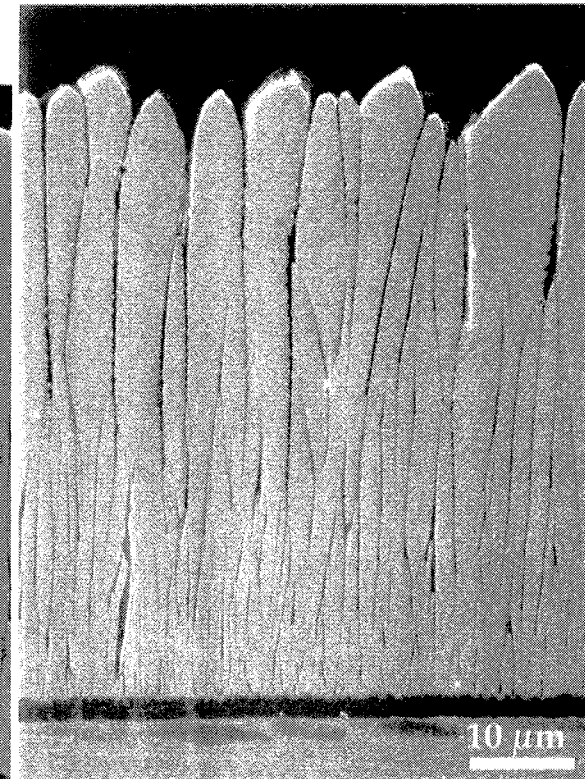
Columnar Microstructures for Deposition under Rotation



900°C: Dominant $\langle 200 \rangle$



1000°C: Dominant $\langle 200 \rangle$



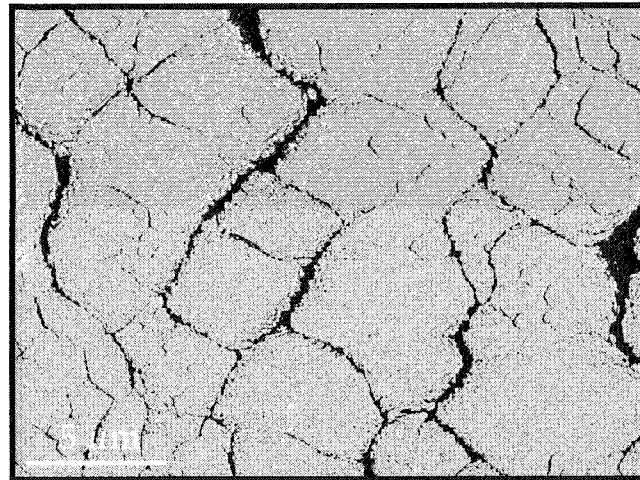
1100°C: $[002] + \langle 200 \rangle$

8 RPM, $\sim 0.9 \mu\text{m}/\text{min}$
(Flux $\sim 3.2 \mu\text{m}/\text{min}$)

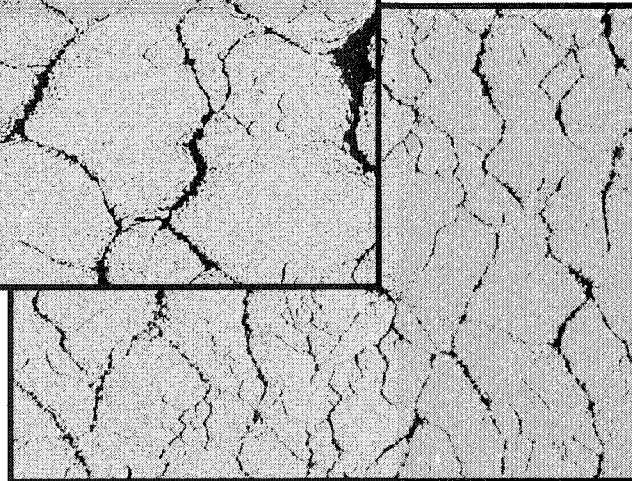
Intercolumnar Gap Porosity

$T_s = 1100^\circ\text{C}$, 8 RPM, $0.9 \mu\text{m}/\text{min}$.

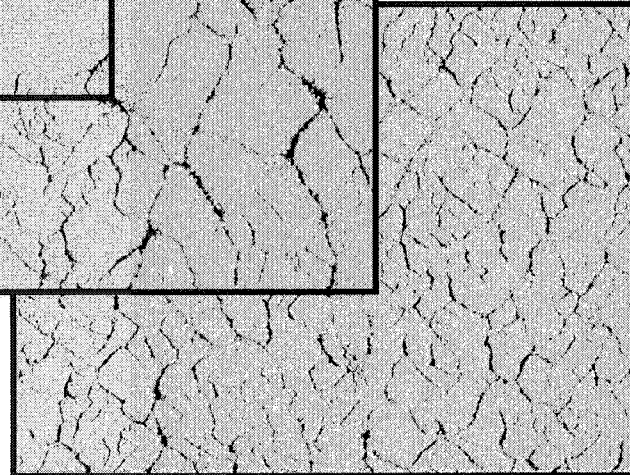
Area Fraction Measurements:
Intercolumnar porosity
content remains
essentially constant
through thickness
of film.



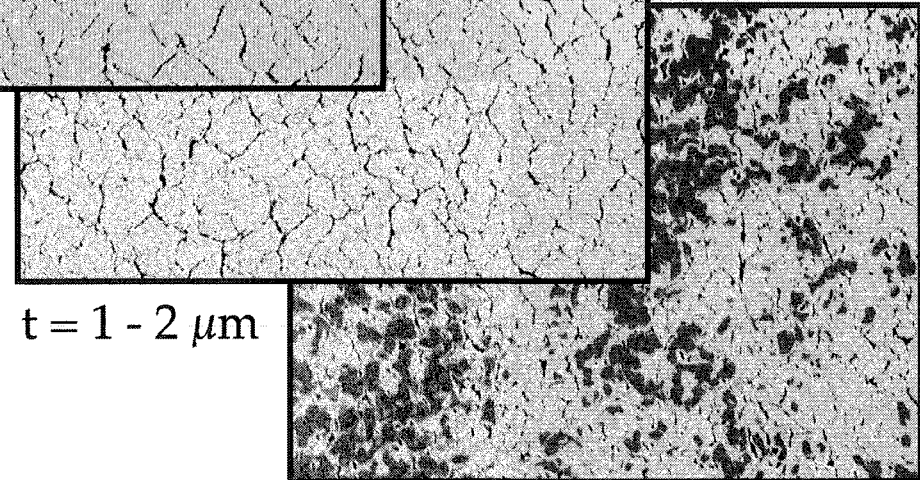
$t = 60 \mu\text{m}$



$t = 40 \mu\text{m}$

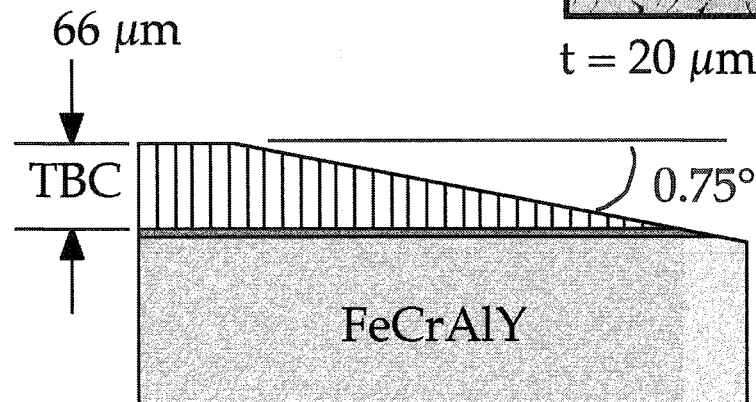


$t = 20 \mu\text{m}$



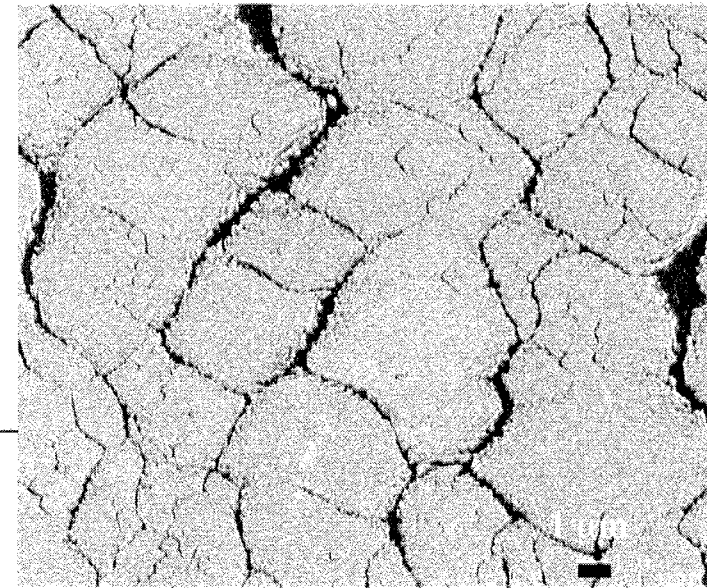
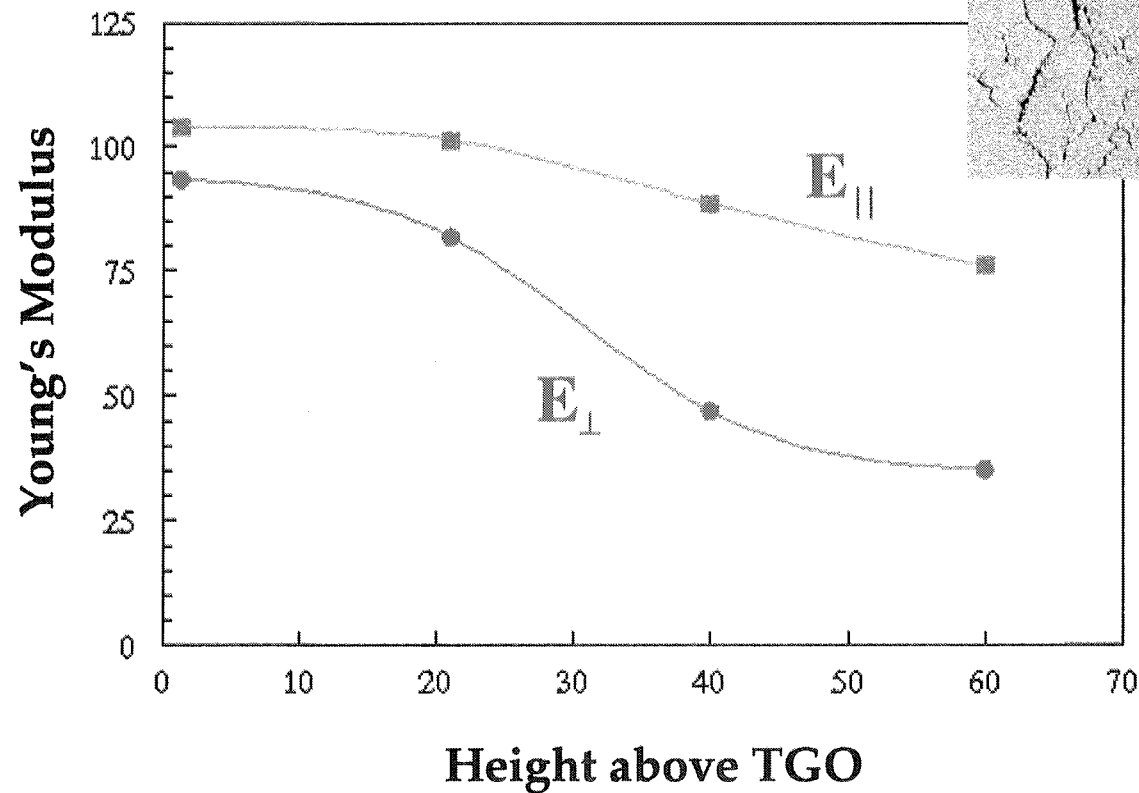
$t = 1 - 2 \mu\text{m}$

$t = 0 \mu\text{m}$

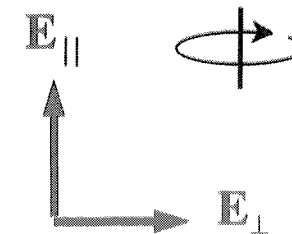


Calculated In-Plane Modulus Anisotropy

(Courtesy of Ed Fuller, NIST)



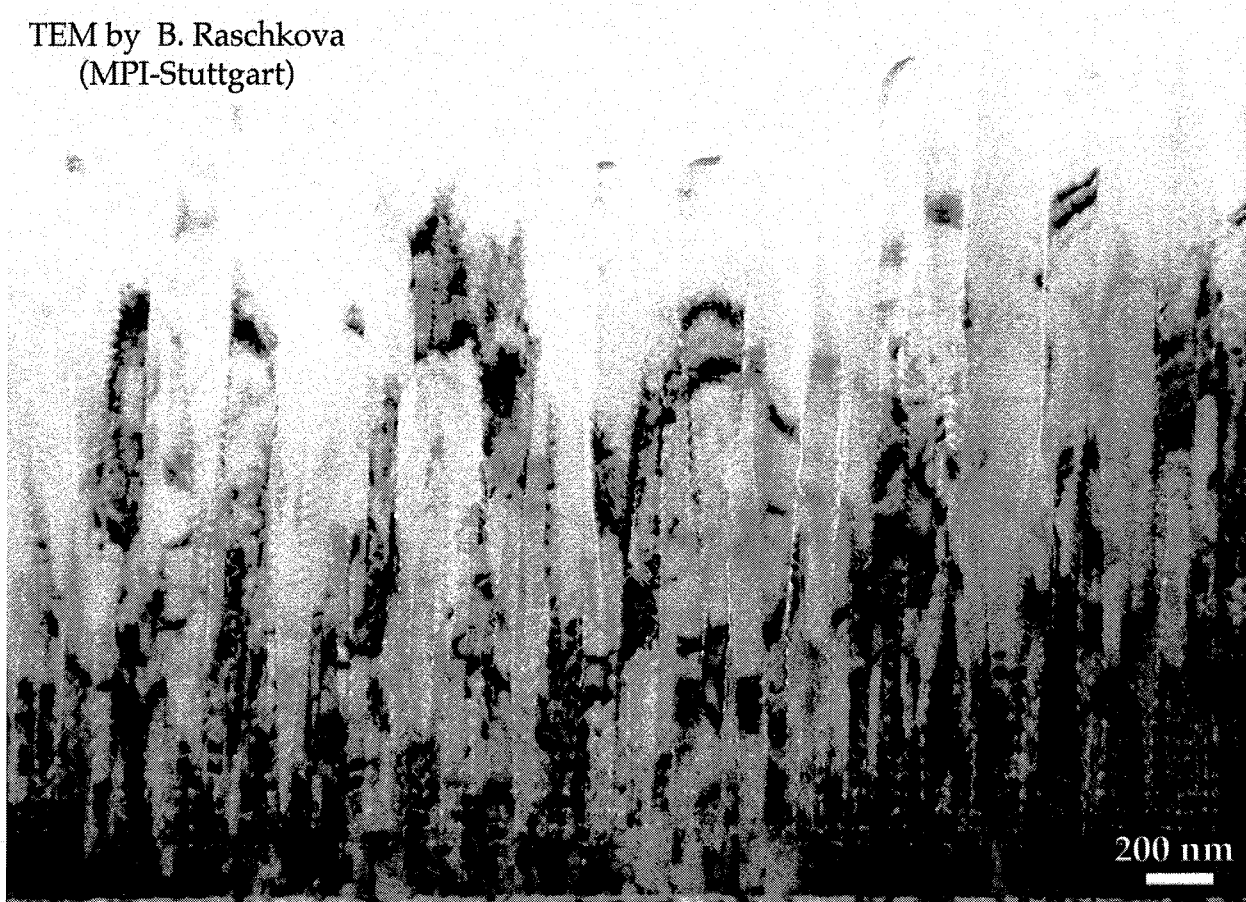
60 μm above TGO



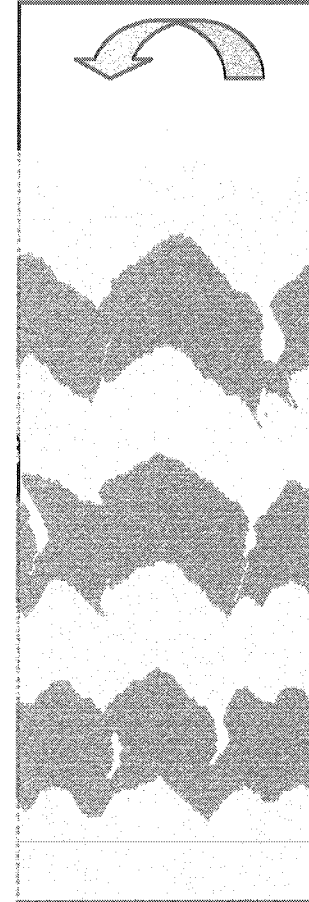
Graph assumes 60% reduction due to intra-columnar porosity

Near-Substrate Pore Structure

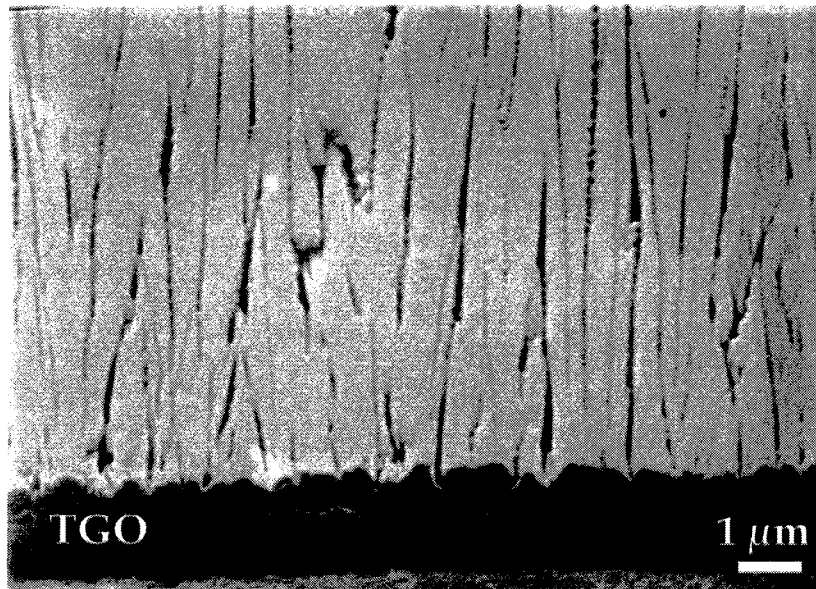
TEM by B. Raschkova
(MPI-Stuttgart)



*YSZ Grown on Sapphire. Pore Spacing Equivalent to
Thickness Deposited per Revolution (~35 nm)*



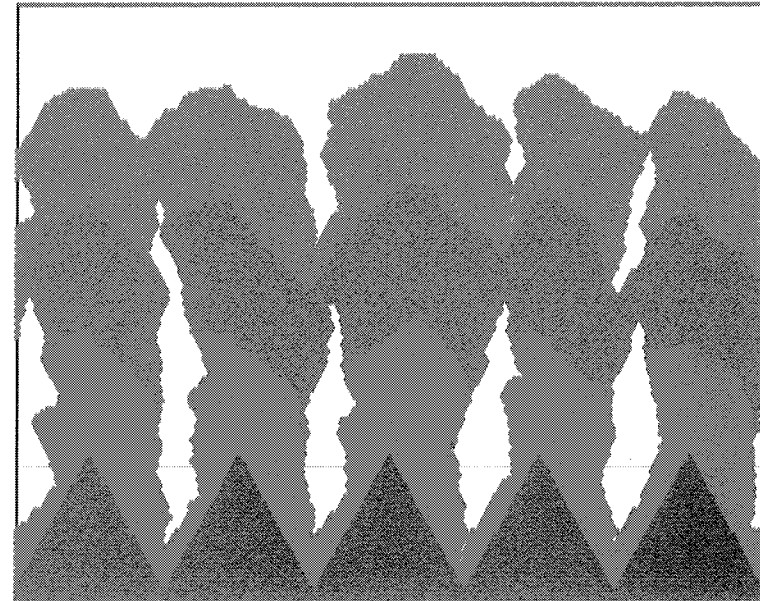
2D Kinetic MC
(~40000 atoms)



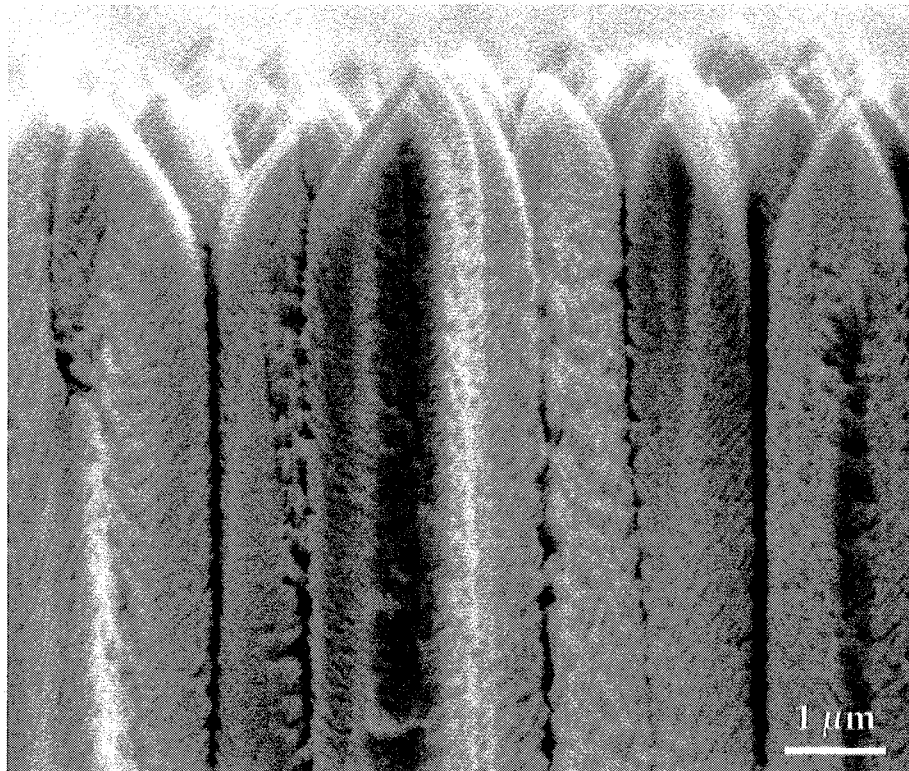
Intercolumnar Gap Initiation by Shadowing from TGO Roughness

Root of Columns in TBC
Deposited on Pre-Oxidized
FeCrAlY Substrate
(1100°C, 8 RPM, ~0.9 μm/min)

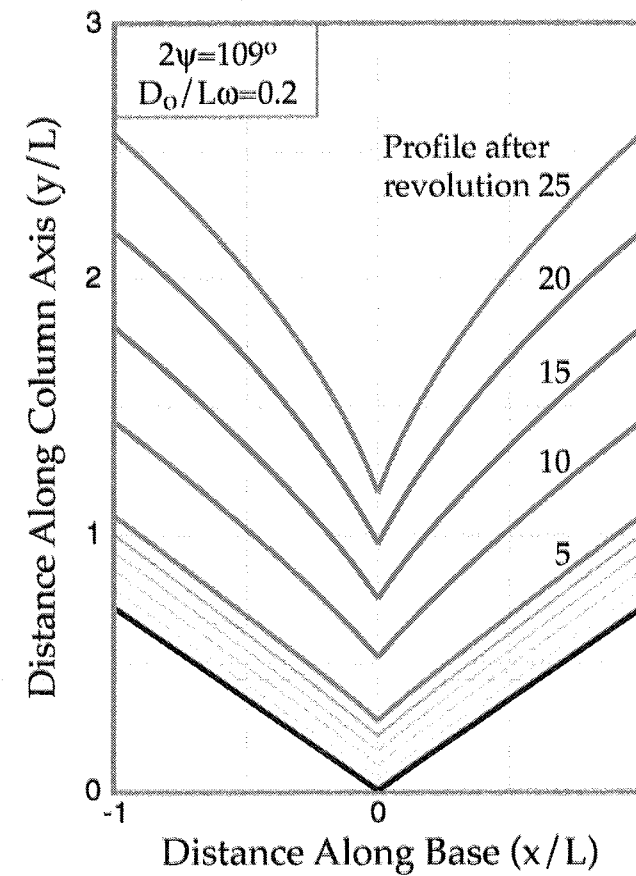
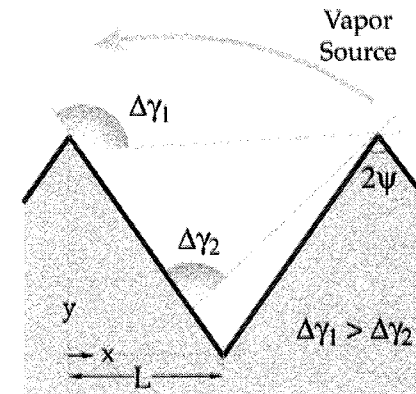
ABD Simulation
on Substrate with
Periodic Roughness



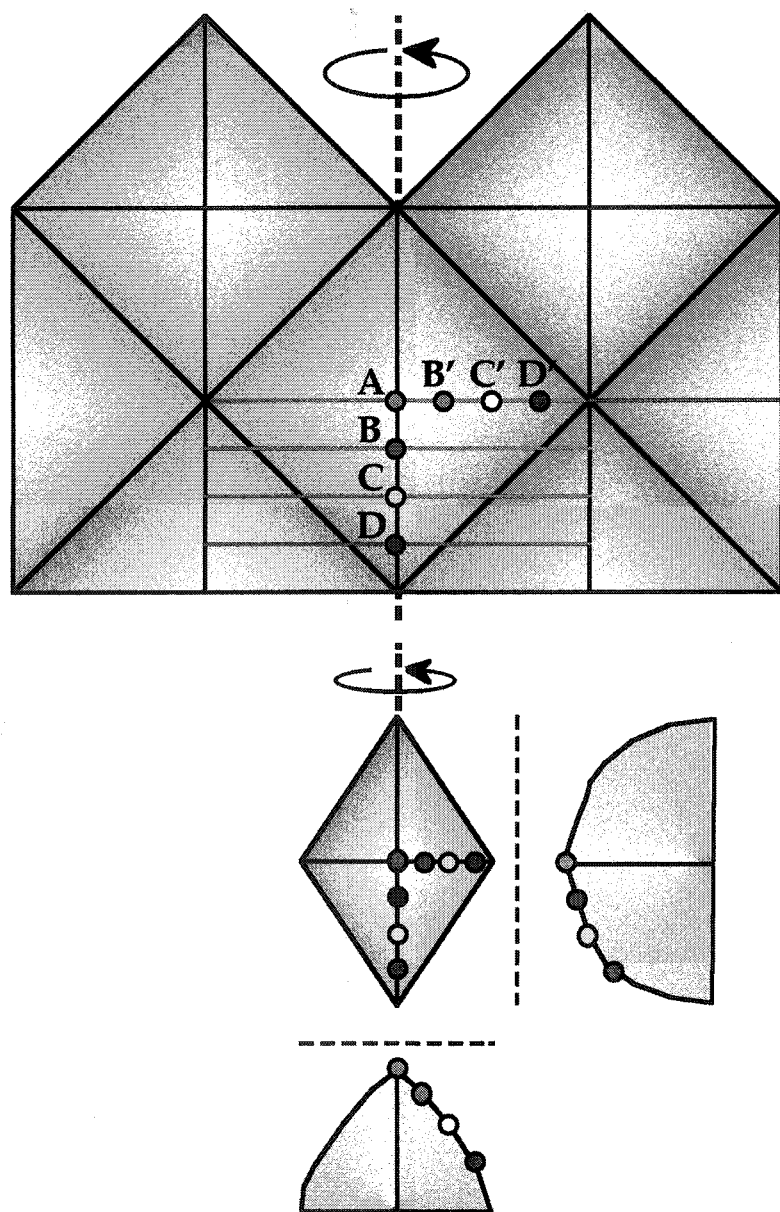
Evolution of Intercolumnar Gap



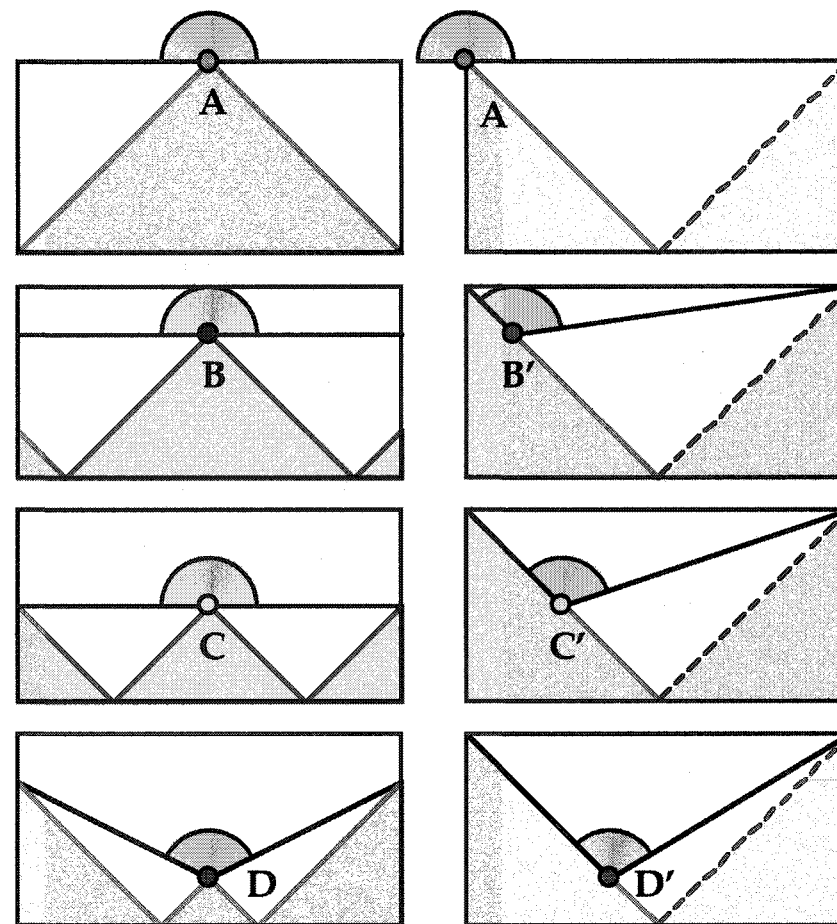
TBC Grown on FeCrAlY Substrate, 950°C, 8RPM



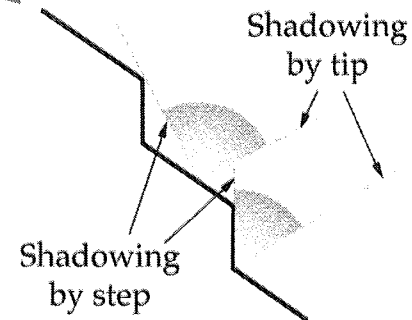
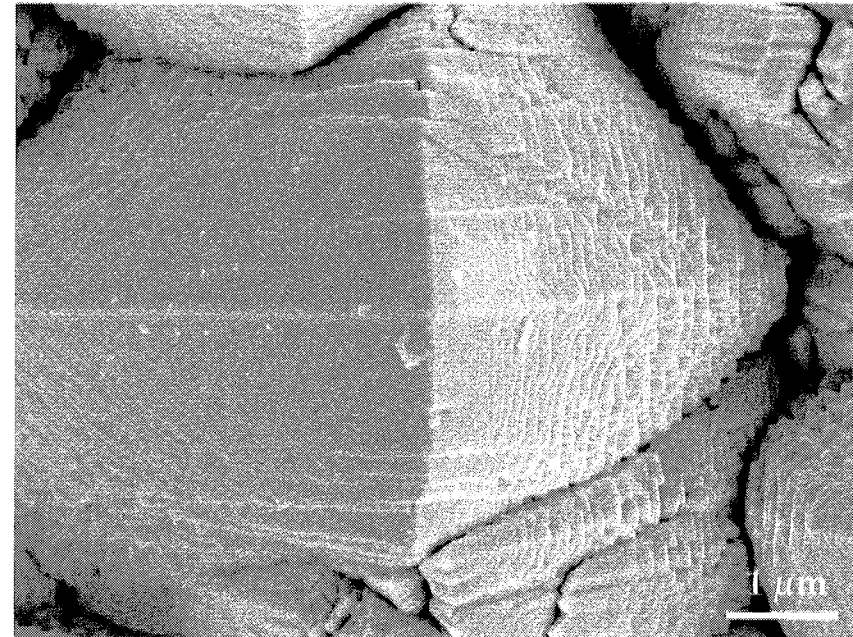
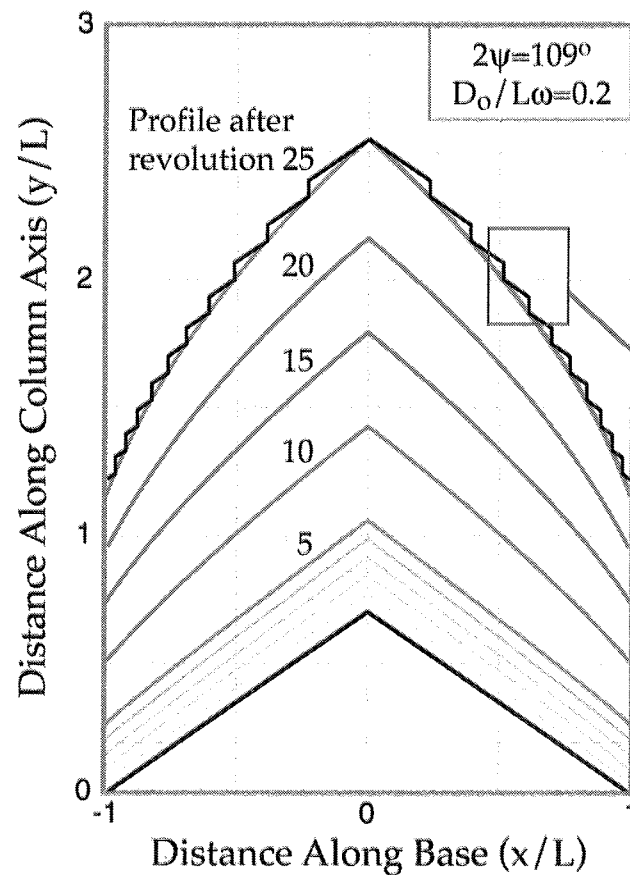
Levi-01/01



Column Anisotropy from Tip Shadowing



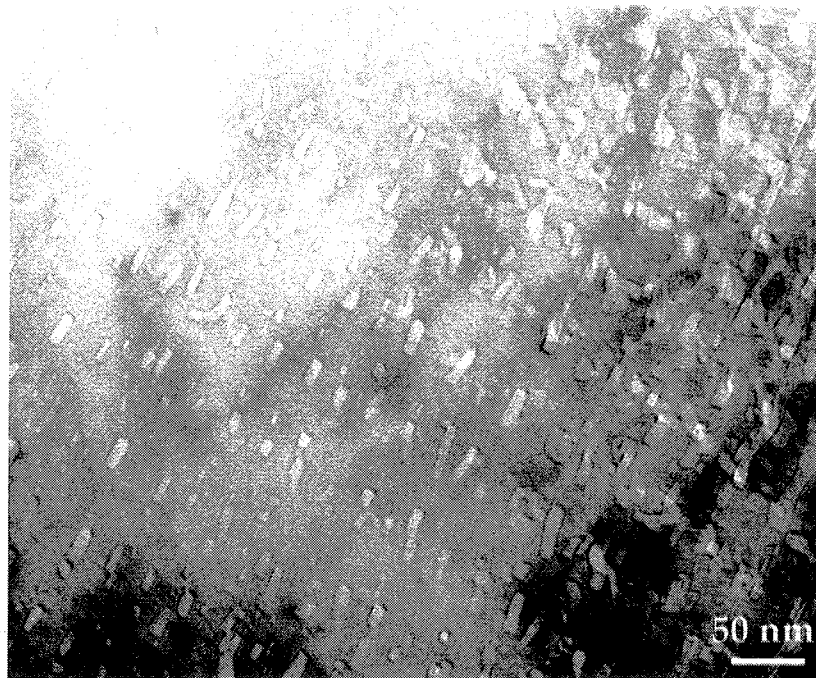
Shadowing by Tip Roughness



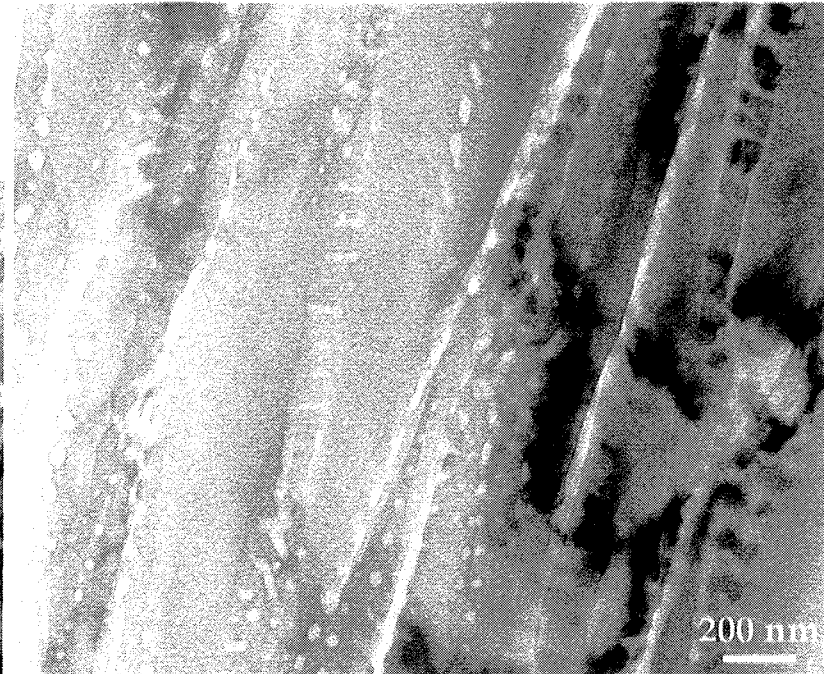
Shadowing enhanced by crystallographic "steps" which become accentuated toward the "valley".

Intra-columnar Porosity in Rotated Specimens

Cross Sections Parallel
to Column Axis

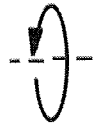


900°C $k = 1.1 \text{ W/mK}$

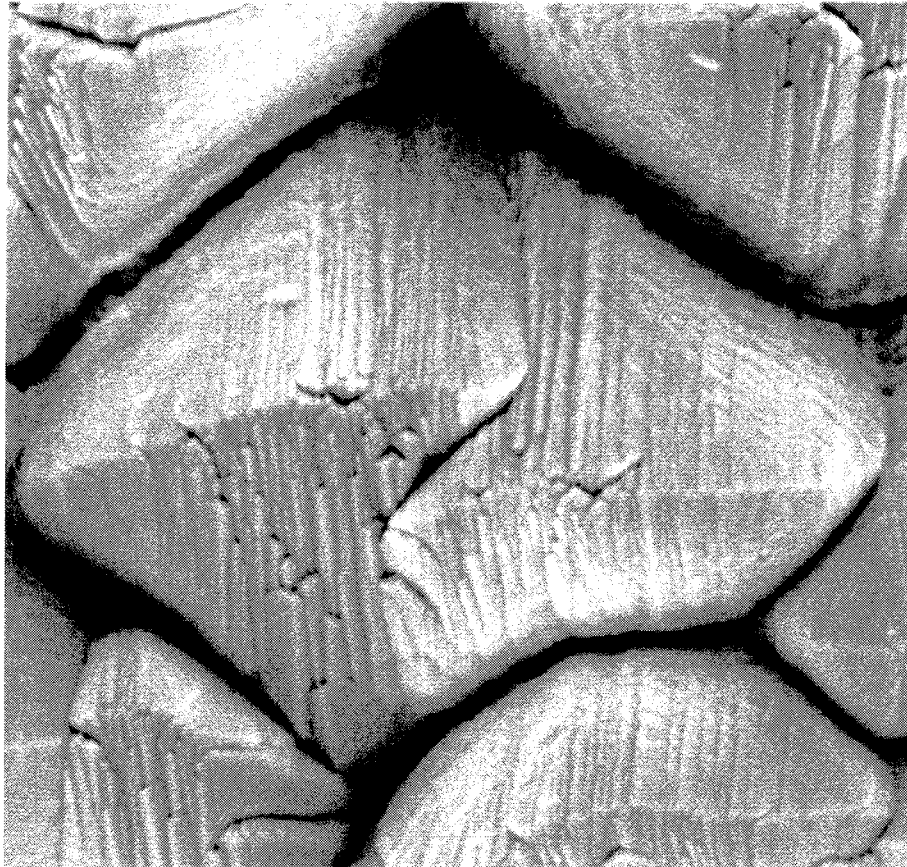


1100°C $k = 1.5 \text{ W/mK}$

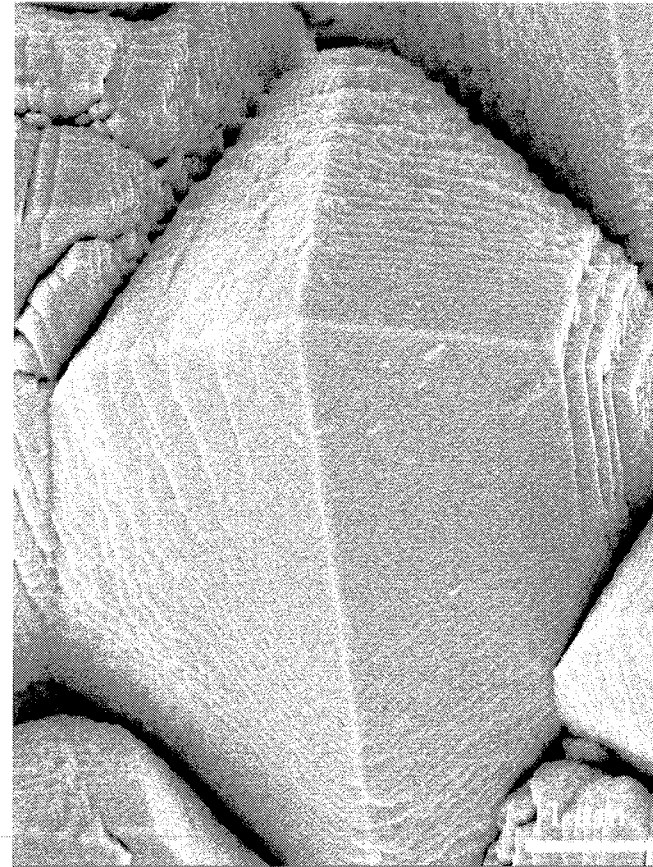
Rotation rate = 8 RPM
Deposition rate $\sim 0.9 \mu\text{m/min}$
Flux $\sim 3.2 \mu\text{m/min}$



Facet Configurations on Column Tips



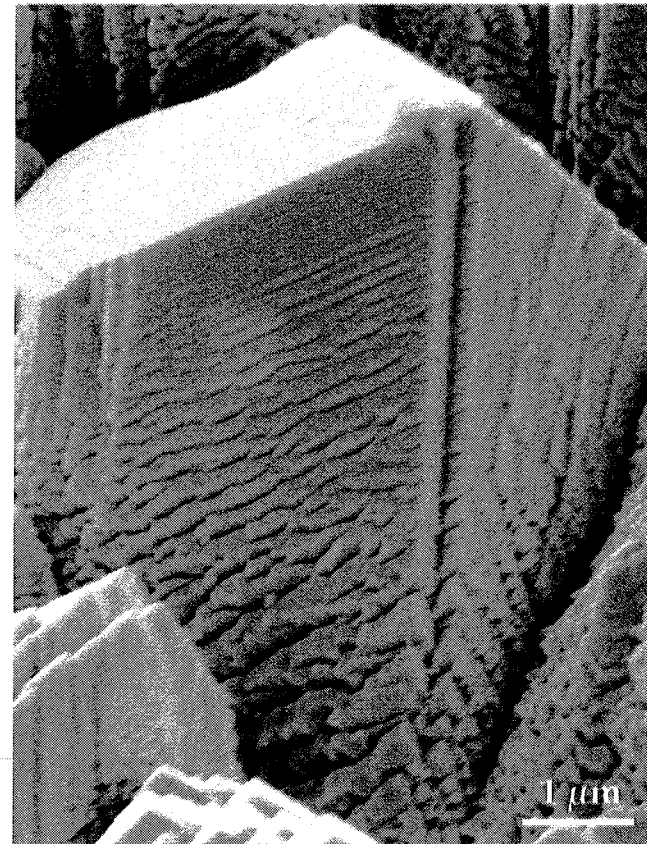
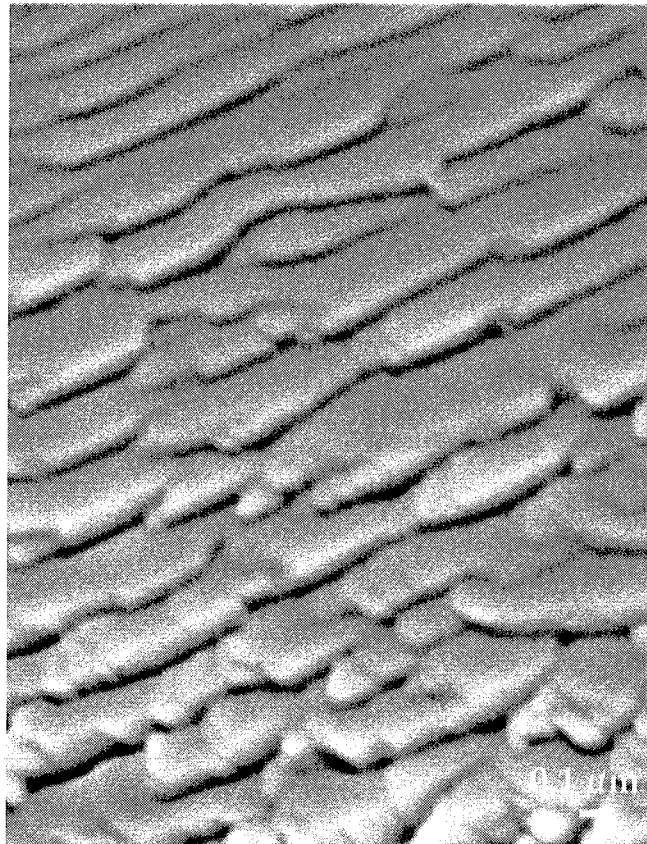
900°C



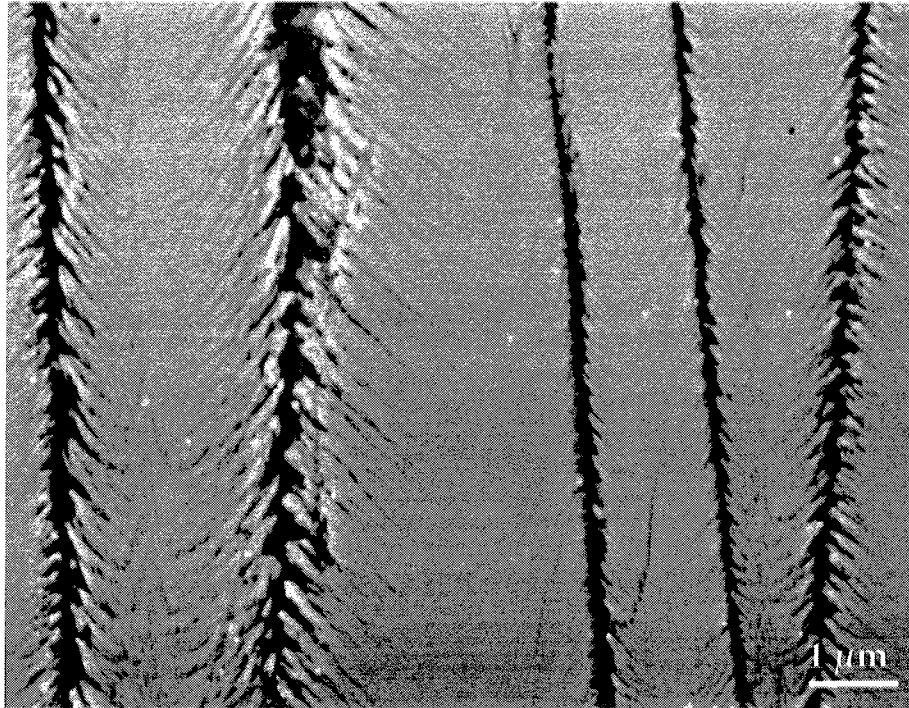
1100°C

Rotation rate = 8 RPM
Deposition rate $\sim 0.9 \mu\text{m}/\text{min}$
Flux $\sim 3.2 \mu\text{m}/\text{min}$

Evolution of Porosity at Steps on the Growth Surface

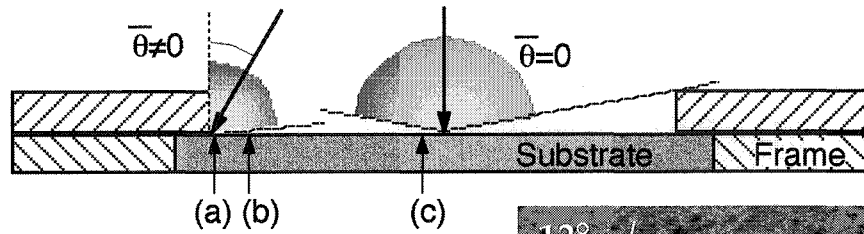


Origin of Feathery Structure

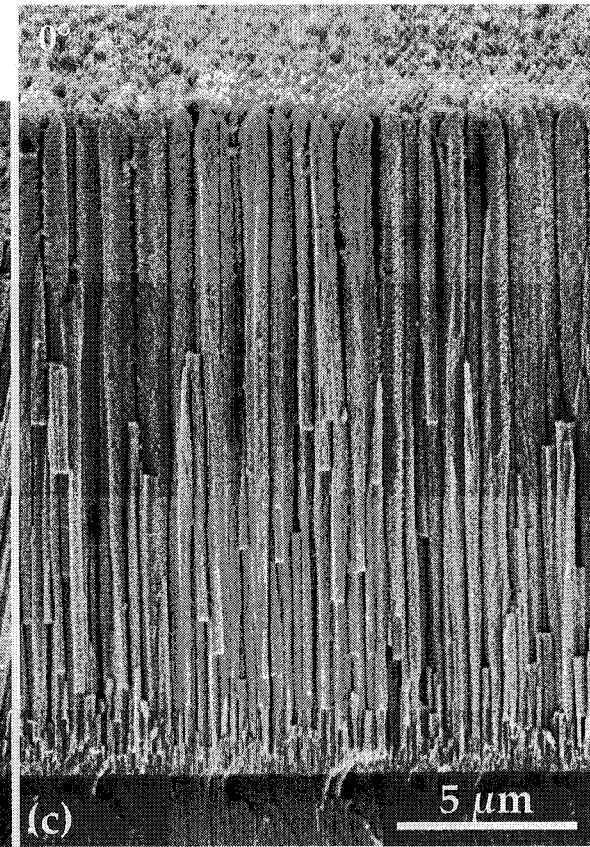
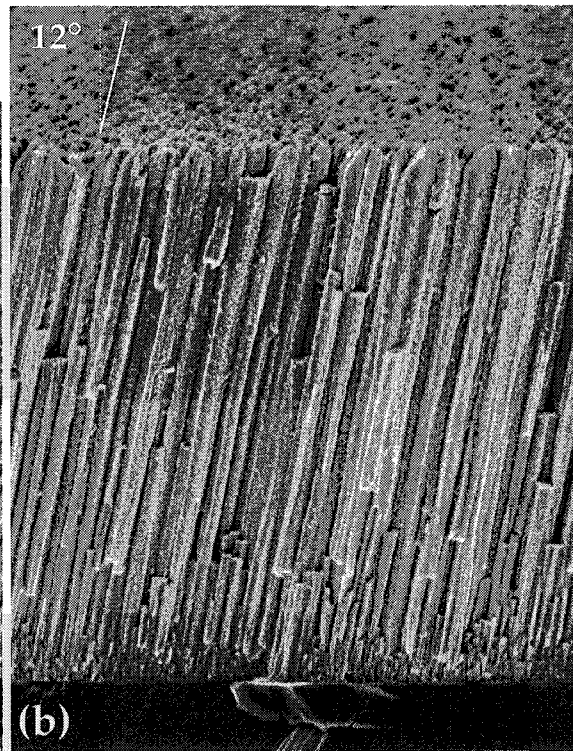
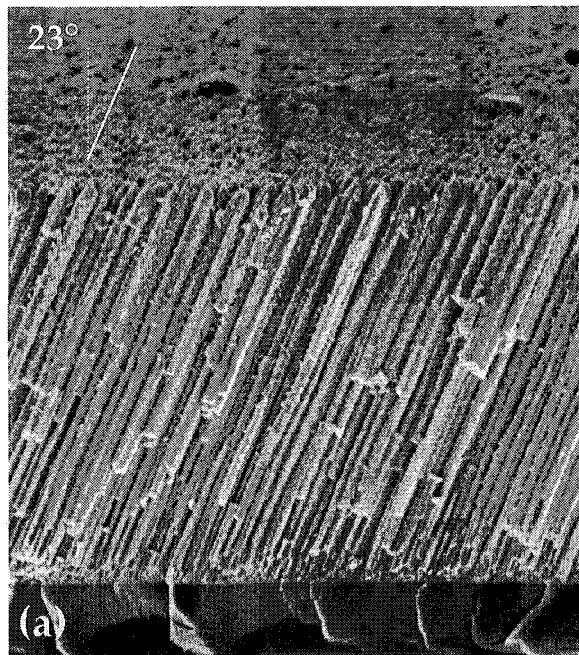


- Shadowing pattern gives rise to pores at steps in the growth front.
- Features propagate outward from column axis. Net rate and direction depend on interplay of local flux with crystallography / surface diffusion.
- Subsequent morphological reconfiguration leads to discrete pores.

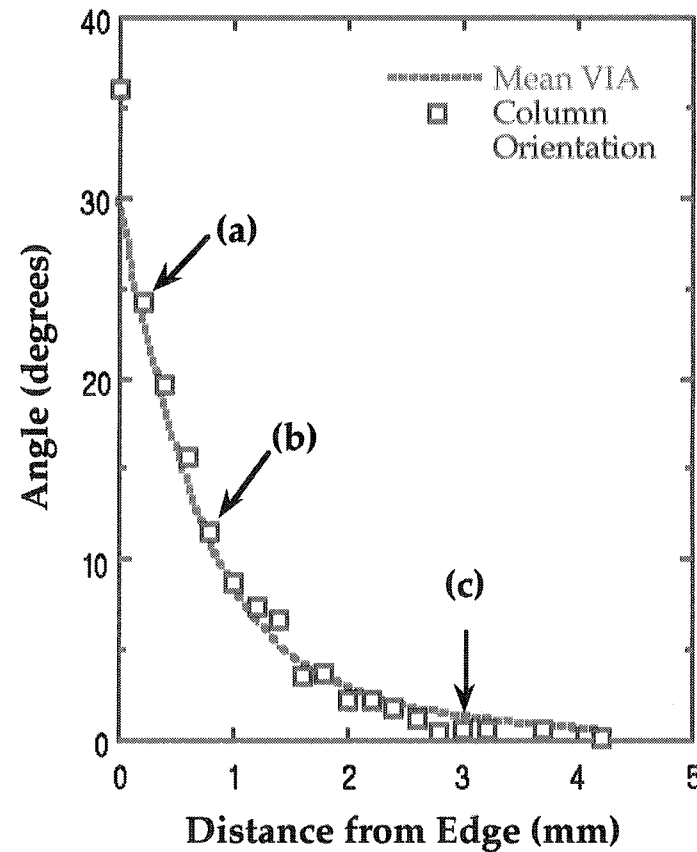
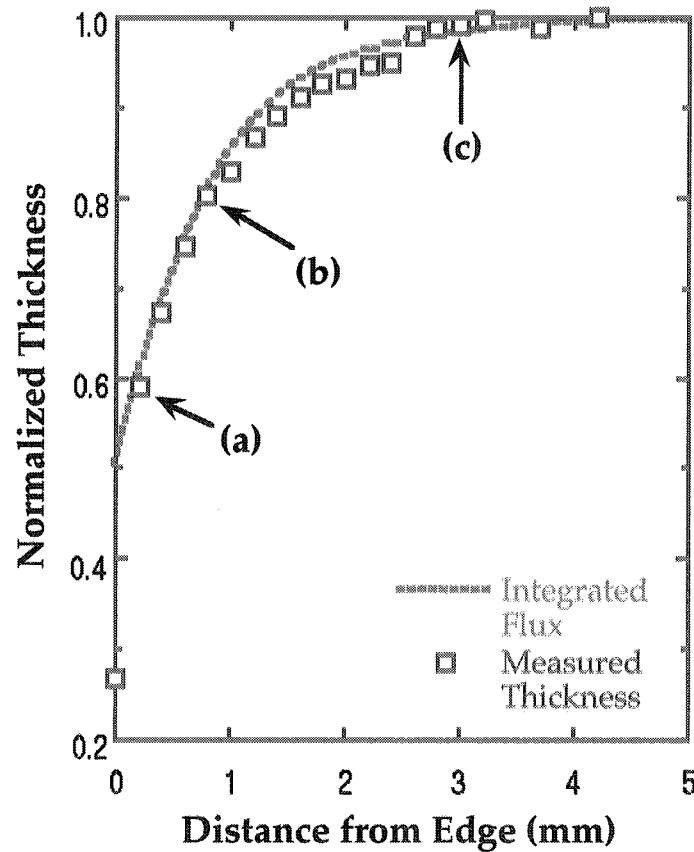
Effect of Macroscopic Shadowing on Structure



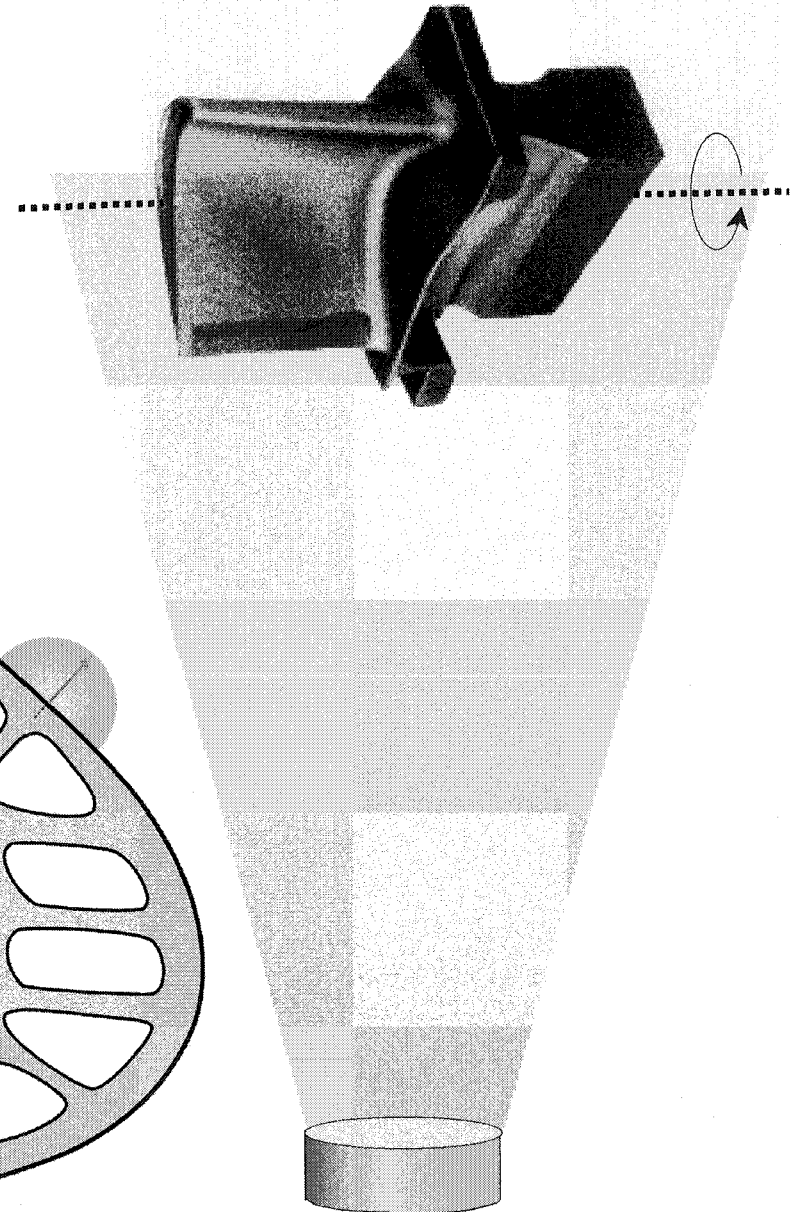
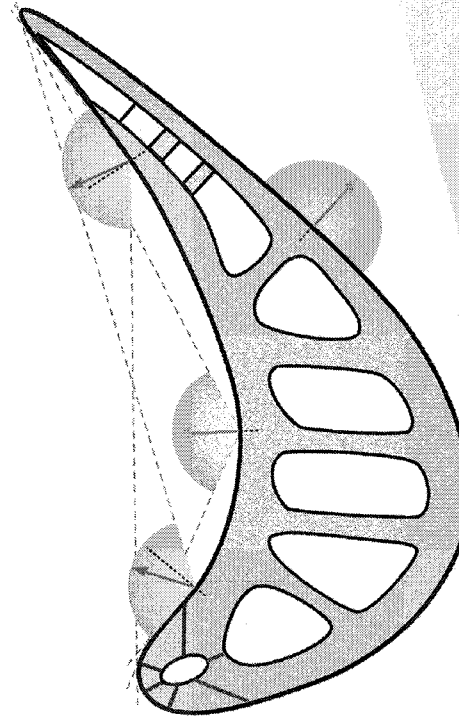
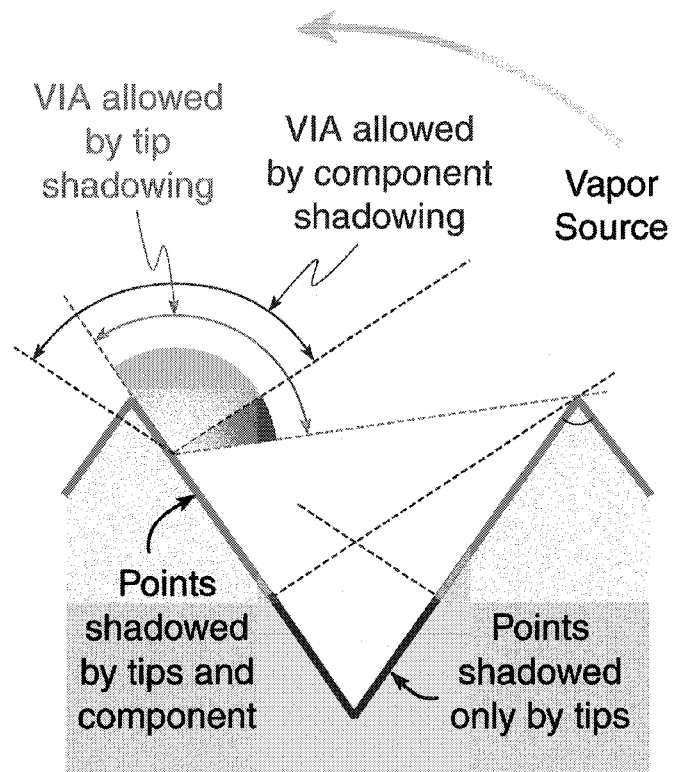
Sapphire Substrate
1000°C/~1 μ m/min/8 RPM



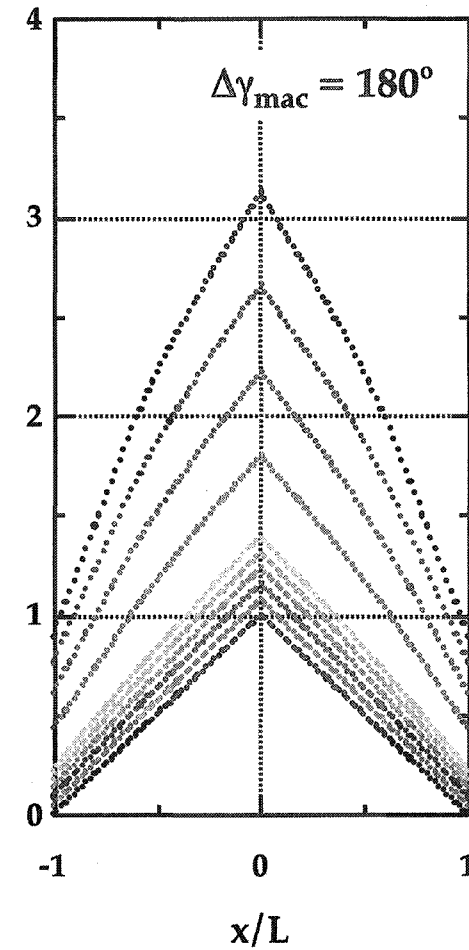
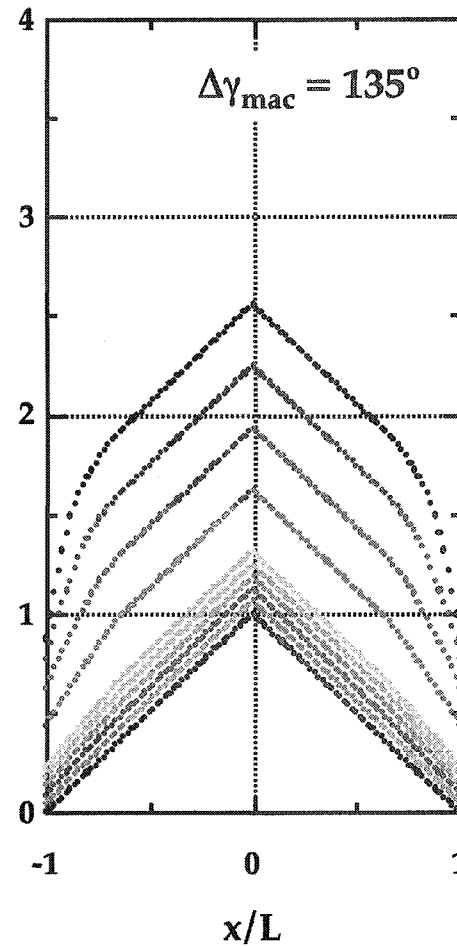
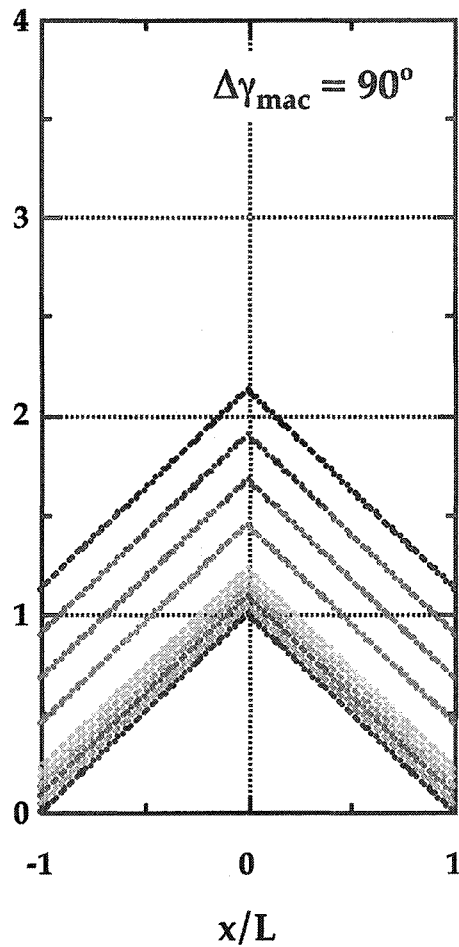
Macroscopic Shadowing Effects on Thickness and Column Orientation



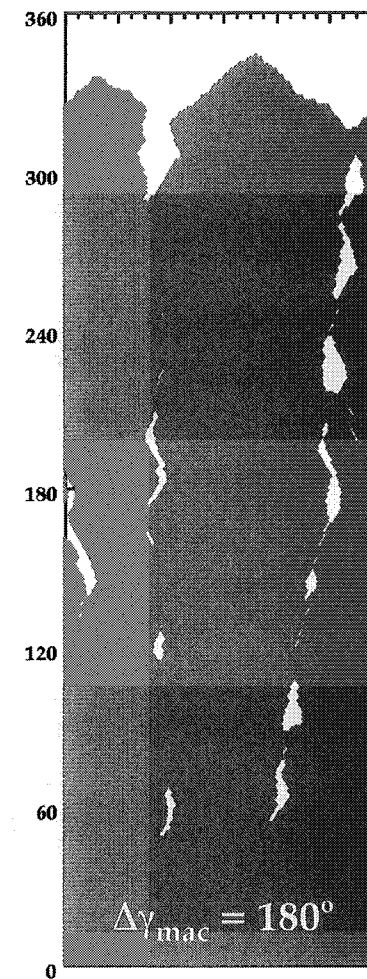
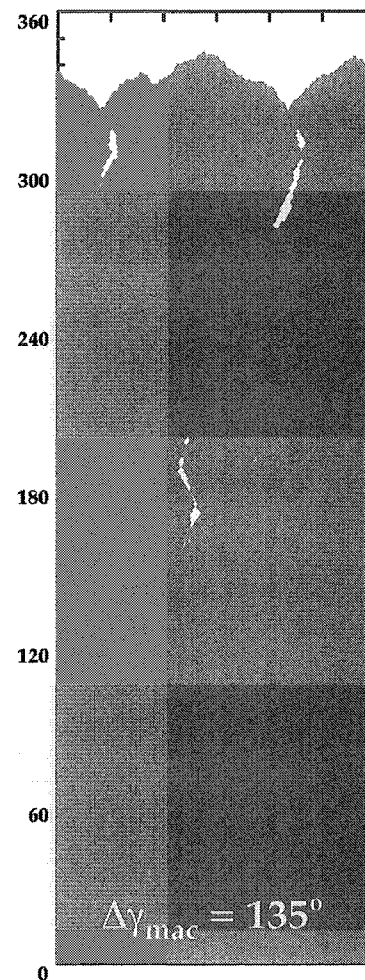
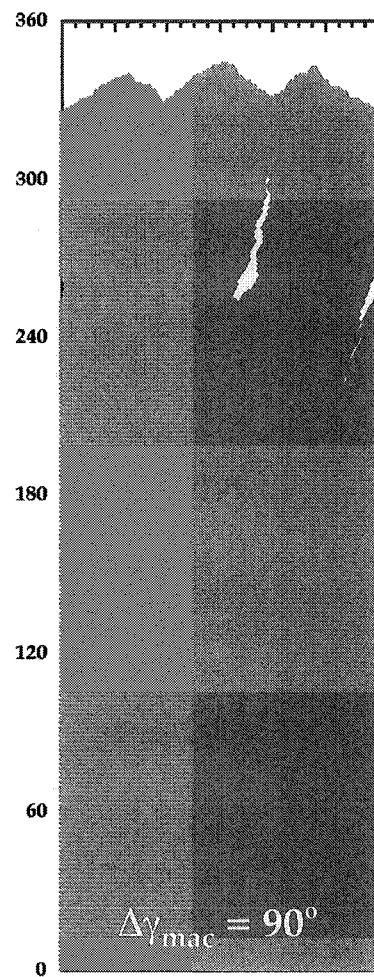
Shadowing by Vapor Interplay with Component Shape



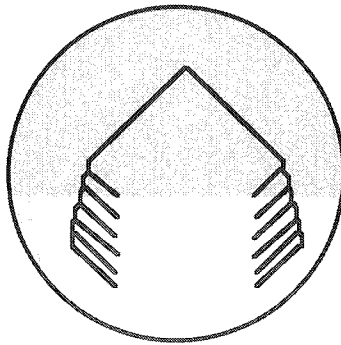
Influence of Macroscopic Shadowing on Tip Evolution



Influence of Macroscopic Shadowing on Intracolumnar Porosity



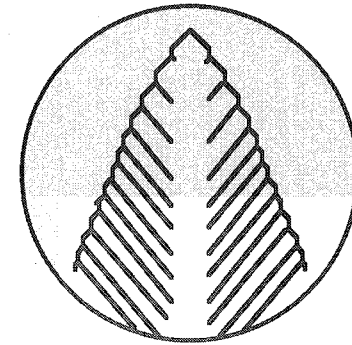
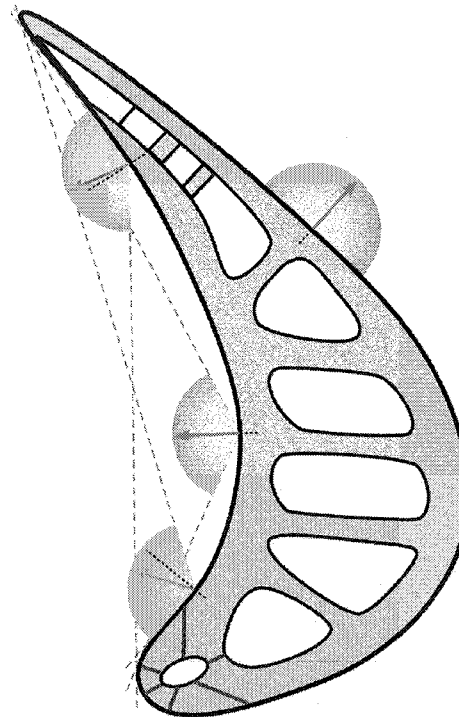
Expected Coating Variability from Macroscopic Shadowing Phenomena



Thinner

Less Insulating

Less Compliant



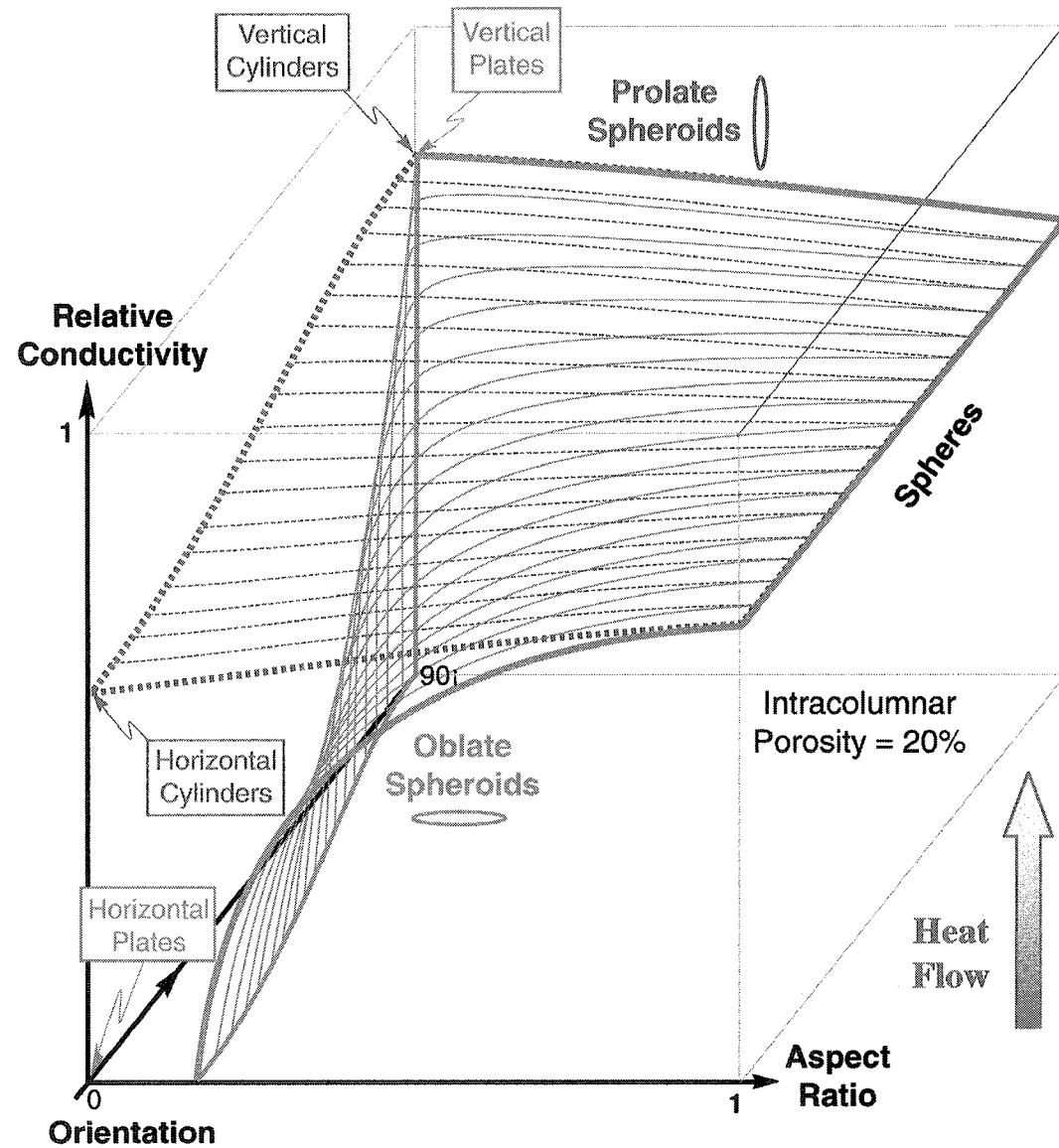
Thicker

More Insulating

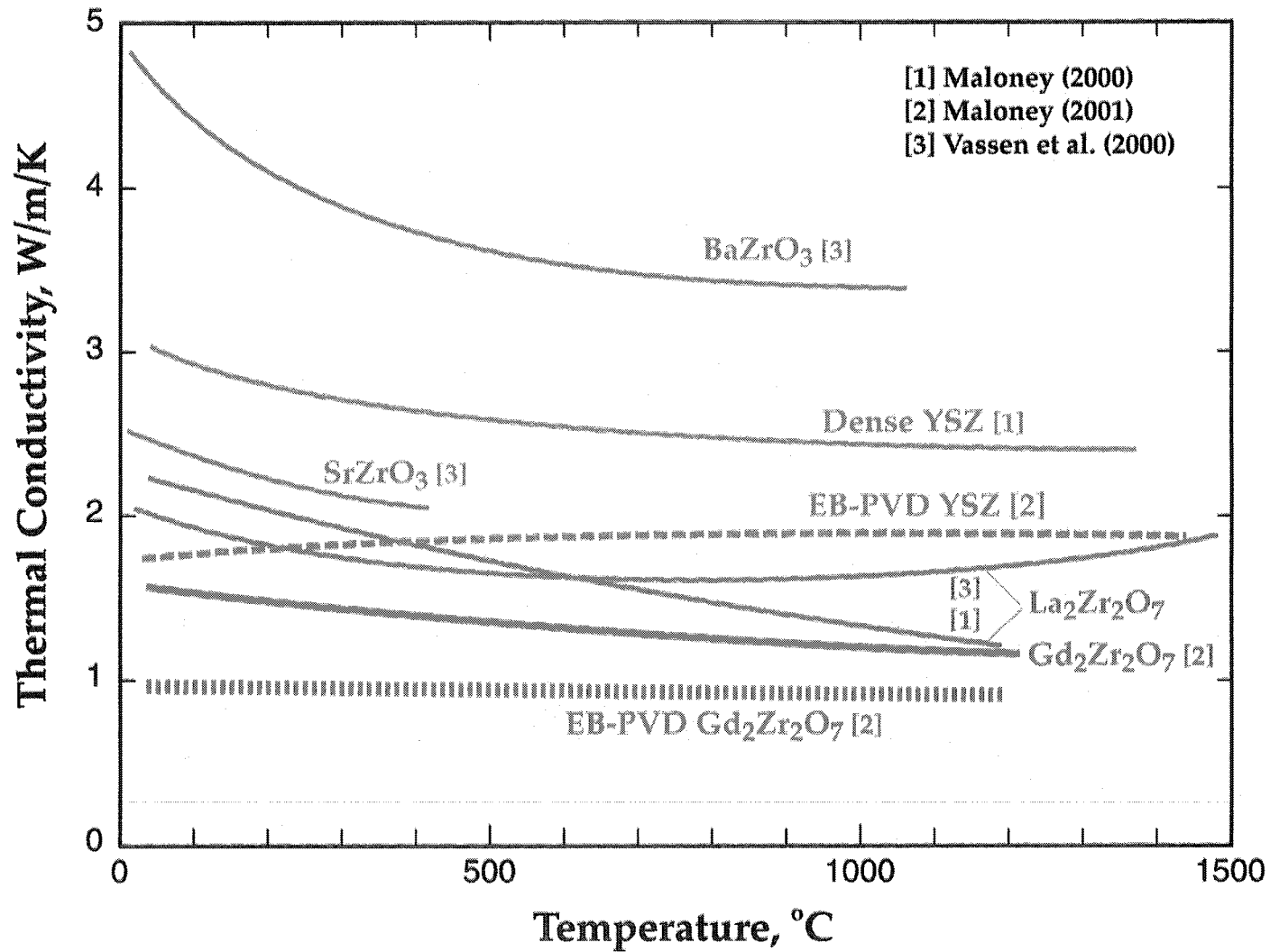
More Compliant

Effect of pore morphology on the thermal conductivity

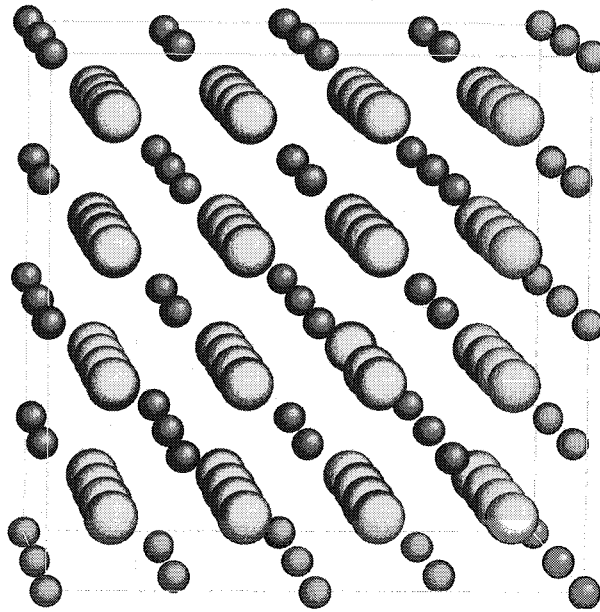
Evolutionary breakdown and spheroidization of lamellar pores rapidly degrades insulating efficiency



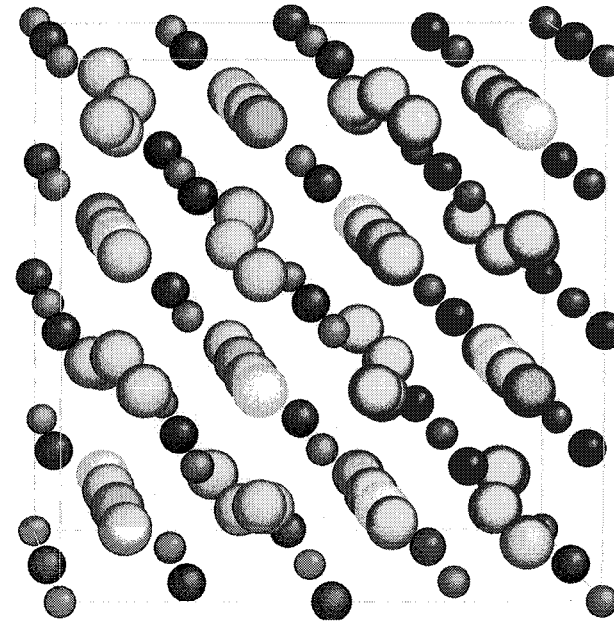
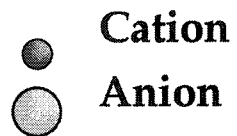
Thermal Conductivity of Zirconates



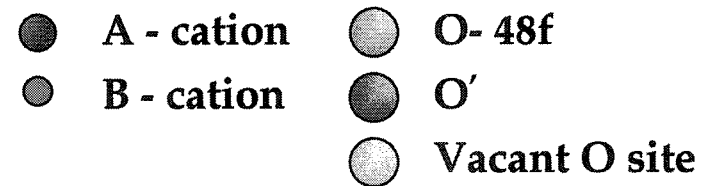
Fluorite and Pyrochlore Structures



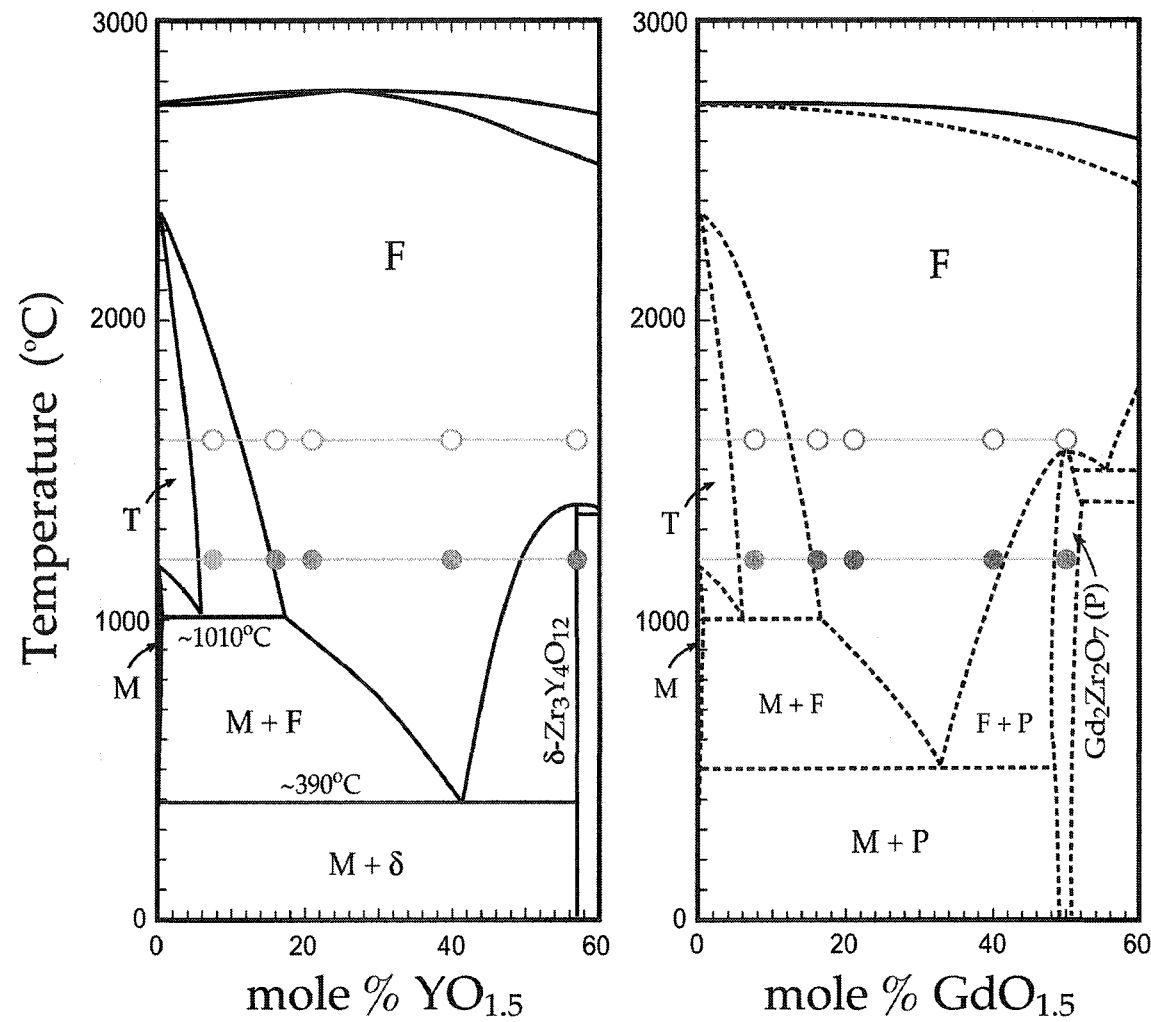
Fluorite: MX_2



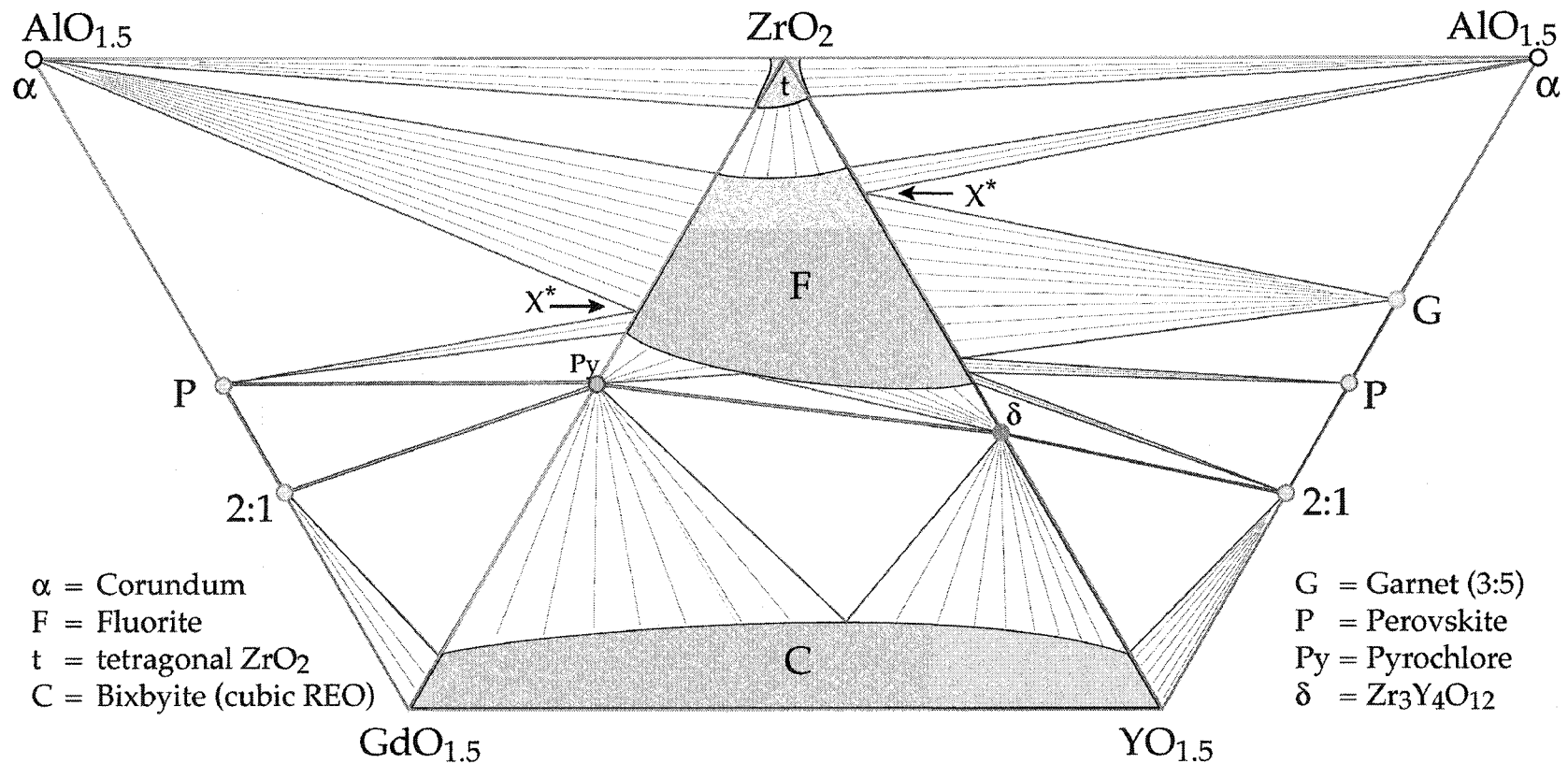
Pyrochlore: $A_2B_2O_7$



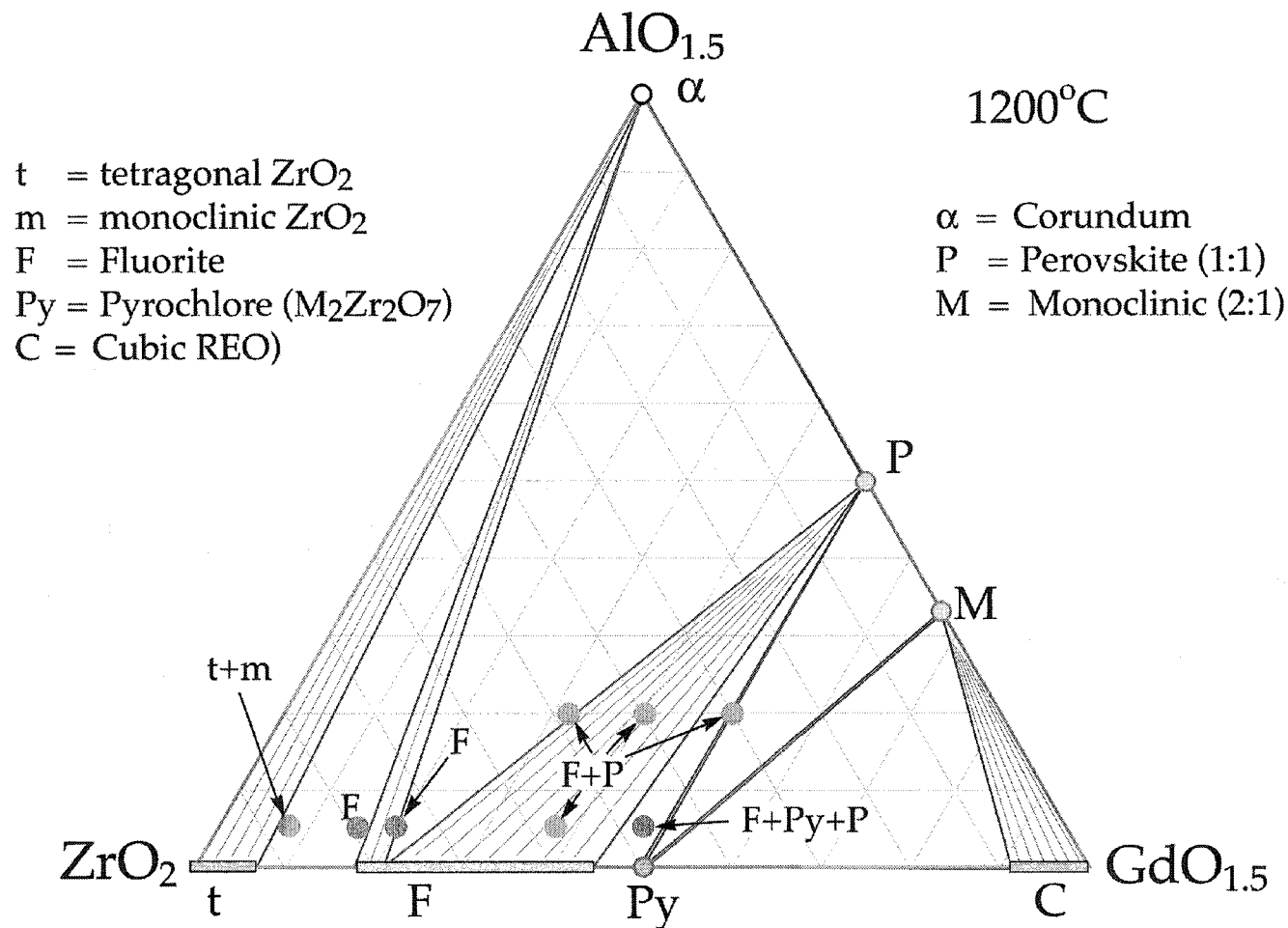
$\text{ZrO}_2\text{-(Y/Gd)O}_{1.5}$ Phase Diagrams



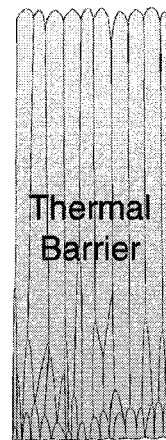
Schematic Ternary Sections at 1200 °C ZrO_2 - $\text{YO}_{1.5}$ - $\text{GdO}_{1.5}$ - $\text{AlO}_{1.5}$ Systems



Thermochemical Compatibility of ZrO_2 - $\text{GdO}_{1.5}$ with Alumina



Increasing Temperature Capability →



Chemical
Barrier



Buffer
Layer

Structural
Element

7% Yttria
Partially
Stabilized
Zirconia
(7YSZ)

Alumina

(Ni,Pt) Al
MCrAlY

Ni-Base
Superalloy

Rare Earth
Zirconate
+
Compatible
layer

Alumina

(Ni,Pt) Al
MCrAlY

Ni-Base
Superalloy

?

Silica

Refractory
Silicide

Refractory
Metal Alloy

?

BSAS
+
Mullite
+
Silica

Silicon
Alloy

Si-based
Ceramic

