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WINTER COLLEGE ON LASERS, ATOMIC AND MOLECULAR PHYSICS

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Lecture 3
Single Longitudinal Mode Selection

D.C. HANNA
Department of Electronics
University of Southampton
Southampton SO9 5NH
U.K.

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Single Longitudinal Mode Selection

Why select a single mode?

- To obtain a long coherence length, useful for example in holography.

$$l_c \sim \frac{c}{\Delta\nu}, \text{ where } \Delta\nu \text{ is the bandwidth of the laser output.}$$

For a bandwidth limited pulse, duration Δt ,

$$\Delta\nu \sim \frac{1}{\Delta t}.$$

Hence 10nsec pulse $\rightarrow \Delta\nu \sim 100 \text{ MHz}$

$$\rightarrow \frac{\Delta\nu}{c} \sim 0.003 \text{ cm}^{-1}$$

$$\rightarrow l_c \sim 300 \text{ cm}$$

2. High resolution in spectroscopic applications.

3. To obtain clean temporal behaviour of the pulse. This is necessary for repeatability of results and is also necessary where a precise knowledge of laser intensity is required (e.g. in nonlinear optics)

See Koecher for a general discussion

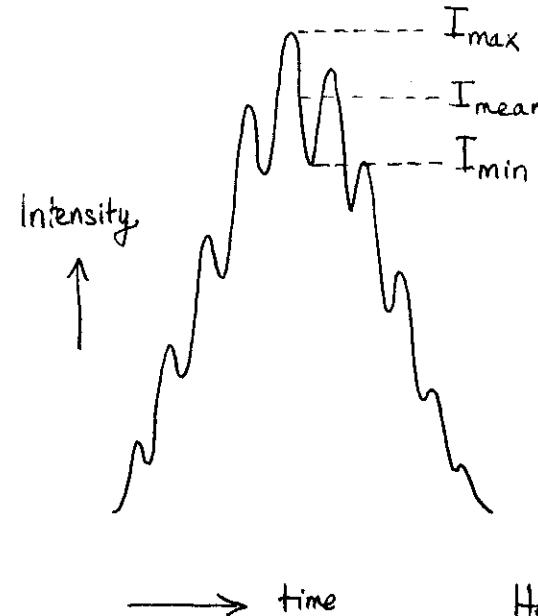
(1)

Criterion defining single-longitudinal mode operation.

(2)

The simultaneous presence of two modes in the laser output gives rise to a modulation of the pulse envelope at their frequency difference.

Even if one mode is much weaker than the other, the depth of modulation can be very large, hence this is a very sensitive test of SLM operation.



Specify depth of modulation by index k ,

$$k = \frac{I_{\max} - I_{\min}}{I_{\text{mean}}} \quad (1)$$

Two modes with intensities in the ratio $N:1$ give modulation

$$k = 4N^{-1/2} \quad (2)$$

Hence for $k < 0.01$, i.e. not quite observable on the oscilloscope trace, require $N > 10^5$

Frequency reflectivity of etalon used in reflection
(resonant reflector) and etalon used in transmission.

If mode m has frequency exactly at RR maximum and mode n is an adjacent mode (displaced by $c/2L$) then the ratio of the reflectivities is

$$\frac{R_m}{R_n} = 1 + \pi^2 \mu^2 t^2 \left(\frac{1-R}{L^2} \right)^2 \quad (3)$$

where μ, t are refractive index & thickness of etalon. (Hanna et al 1972)

After q round trips of the resonator the mode powers (assumed equal at first) will be in the ratio

$$\frac{P_m}{P_n} = \left(\frac{R_m}{R_n} \right)^q = \left[1 + \pi^2 \mu^2 t^2 \left(\frac{1-R}{L^2} \right)^2 \right]^q \quad (4)$$

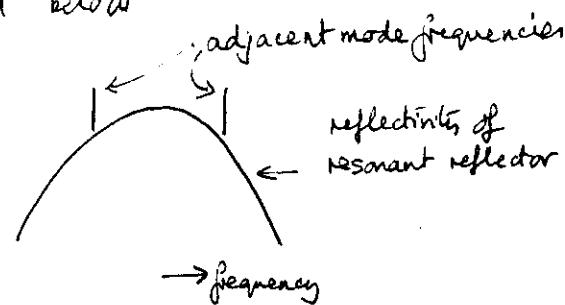
The corresponding expression for a transmission etalon (TE) is

$$\frac{P_m}{P_n} = \left[1 + \frac{8\pi^2 \mu^2 t^2 R}{L^2 (1-R)^2} \right]^q \quad (5)$$

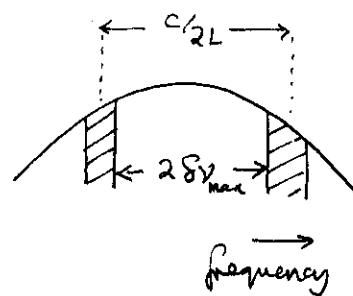
Aim to achieve $P_m/P_n \gtrsim 10^5$, so make μt large, L small, R large (for TE) and most usefully make q as large as possible. The latter can be achieved with a Saturable Absorber Q-switch (Sooy 1965) or its electronic analogue, 'prelase' Q-switching (Hanna et al 1972, 1981, 1982)

(3)

Even if $P_m/P_n \gg 10^5$ with mode m situated at the peak of the etalon maximum, the situation can arise where the resonator modes drift to the situation depicted below



Then the output will appear as two-mode beating. In fact there will be some maximum allowable displacement $\delta\nu_{max}$ of the dominant mode from the reflectivity maximum, before the criterion of single mode operation is violated (Hanna & Koo 1982). Thus if one mode falls in one hatched region, the adjacent mode falls in the other symmetrically placed hatched region and



the single-mode criterion is no longer met. Over a long period the fractional shifts which are single mode will be

$$\left(\frac{4L}{c} \right) \delta\nu_{max} = 1 - \frac{\ln N}{q} \cdot \frac{L^2}{\pi^2 \mu^2 t^2} \left(\frac{1+R}{1-R} \right)^2 \quad (\text{for RR}) \quad (6)$$

$$\text{or } = 1 - \frac{\ln N}{q} \cdot \frac{L^2 (1-R)^2}{8R \pi^2 \mu^2 t^2} \quad (\text{for TE})$$

(4)

Thus one can actually predict, using ⑥ the fraction of laser shots which can be expected to be single-mode (according to the criterion that the dominant mode is at least N times more intense than its weaker neighbour).

On the other hand if the hatched regions are narrow enough one can apply a technique in which the laser frequencies are allowed to sweep themselves out of the hatched region during a pumping pulse and thus ensure that every laser shot gives SLM output (Hanna & Koo 1982)

⑤

References on Single Longitudinal Mode Selection

⑥

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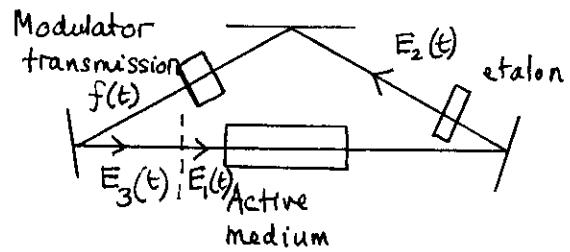
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Analysis of Active Mode-Locking.

Kuizenga and Siegman (1970) first analysed the steady-state mode-locked pulse.



Assume Gaussian time-dependence of pulse $E_1(t)$. Transform to frequency domain and then transmit through the active medium and etalon (if any). Transform back to time domain ($E_2(t)$). Effect of modulator in the time domain (e.g. acousto-optic modulator) is to provide a transmission

$$f(t) = \cos(\Omega_m \sin \omega_m t), \quad \omega_m = 2\pi f_m \quad (1)$$

Hence find $E_3(t)$.

Now require self-consistency,

$$E_3(t) = E_1(t - \text{round trip time})$$

Result (Kuizenga (1981)) is that the steady-state pulse width τ_{po} is given by

$$\tau_{po} = \left(\frac{2 \ln 2}{\pi} \right)^{1/2} \frac{1}{\Omega_m^{1/2}} \cdot \frac{1}{f_m^{1/2}} \left(\frac{g}{(\Delta f)^2} + \frac{1}{(\Delta f_e)^2} \right)^{1/4} \quad (2)$$

where g is the saturated amplitude gain for one round trip, at line centre.

Δf is the gain linewidth (6 cm^{-1} for NdYAG)

Δf_e is an effective bandwidth for the etalon,

$$\Delta f_e = \frac{2c}{\pi h} \frac{1}{n^2 - 1} \quad \text{for an}$$

uncoated solid etalon of thickness h and refractive index n .

Typically pulse durations down to $\sim 50 \text{ ps}$ can be obtained (without the etalon) and these can be increased to $\sim 1 \text{ nsec}$ with appropriate etalons.

To analyse the development of the mode-locked pulse as it evolves towards the steady state,

Kuizenga et al (1973) generalised the self-consistency requirement. They still assumed a Gaussian pulse $e^{-\alpha t^2}$ but α was allowed

to change by a variable amount Δx per round trip. This led to a differential equation for Δx which could be solved, thus giving a pulse duration τ_p , after M round trips,

$$\tau_p = \tau_{p0} / [\tanh(M/M_0)]^{1/2} \quad (3)$$

$$\text{where } M_0 = \frac{1}{4\sqrt{g}} \cdot \frac{\Delta f}{f_m} \quad (4)$$

Thus τ_p is within 5% of the steady state value τ_{p0} when $M > 1.52 M_0$, i.e.

$$M > \frac{0.38}{\sqrt{g}} \cdot \frac{\Delta f}{f_m} \quad (5)$$

Since $\Delta f/f_m$ is large ($\approx 10^3$) this implies a large number of round trips, and hence tens of usecs build up.

With an etalon, $\frac{\Delta f}{\sqrt{g}}$ is replaced by Δf_e ,

which can be much smaller, hence steady state is reached much more quickly for longer pulses.

(3)

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