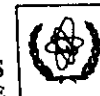




UNITED NATIONS EDUCATIONAL, SCIENTIFIC AND CULTURAL ORGANIZATION
INTERNATIONAL ATOMIC ENERGY AGENCY
INTERNATIONAL CENTRE FOR THEORETICAL PHYSICS
I.C.T.P., P.O. BOX 586, 34100 TRIESTE, ITALY, CABLE: CENTRATOM TRIESTE



SMR/1003 - 13

SUMMER COLLEGE IN CONDENSED MATTER ON
" STATISTICAL PHYSICS OF FRUSTRATED SYSTEMS "

(28 July - 15 August 1997)

"Theoretical description of the out of equilibrium "
"Dynamics of glassy systems"

presented by:

L.F. CUGLIANDOLO
Laboratoire de Physique Theorique
Ecole Normale Supérieure de Paris
24 Rue Lhomond
75005 Paris
France

These are preliminary lecture notes, intended only for distribution to participants.

THEORETICAL DESCRIPTION OF THE OUT OF EQUILIBRIUM

DYNAMICS OF GLASSY SYSTEMS.

L. F. CUGUARD.

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LETICIA@PHYSIQUE.ENS.FR.

CONTENTS:

LECTURE I: PHENOMENOLOGY.

EXPERIMENTAL OBSERVATIONS

NUMERICAL RESULTS

SOME ANALYTICAL RESULTS.

RELEVANT CORRELATIONS.

LECTURE II: (J. KURCHAN)

MICROSCOPIC DYNAMICS

EQUILIBRIUM THEOREMS (TIME TRANSLATION

INVARIANCE & FLUCTUATION-DISSIPATION)

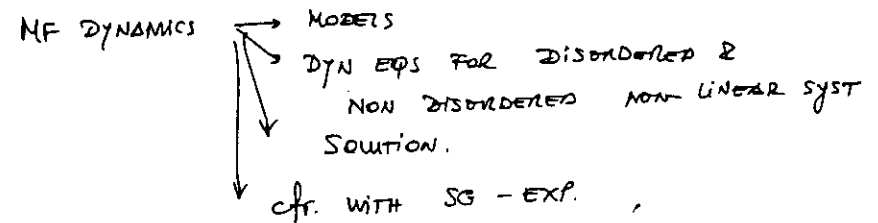
BOUNDS OUT OF EQUILIBRIUM.

LECTURE III

GENERAL PROPERTIES OF CORR & RESP FUNCTIONS.

CASE: SG, GLASSES, DOMAIN GROWTH.

LECTURE IV-V



SOME GRA REFS.

- E. VINCENT, J. HAMMERS, V. COIO, JP BOUCHAUD, LFC
TO APPEAR IN Springer Verlag, E. Riv. Ed
PRINC FROM SITE 96 COND-MAT/9604224.

EXPERIMENTS ↗

- JP BOUCHAUD, LFC, J. KURCHAN, H. MEZARD.
TO APPEAR IN 'ES & RANDOM FIELDS', P. Young Ed
COND-MAT/9702070

GENERAL ↗

GLASSY DYNAMICS

1. EXPERIMENTS & Motivations

SPIN-GLASSES, POLYMER GLASSES, GELS, ETC.
RESPONSES, CORRELATIONS

'UNIVERSALITY'

MODELLING → SPIN-GLASSES, GLASSES

'MAIN' OBSERVATIONS. (DATA)

2. EQUILIBRIUM vs. Nonequilibrium

INVARIANCE UNDER TIME TRANSLATIONS (TI)
FLUCTUATION-DISSIPATION THEOREM (FDT)

3. GENERAL PROPERTIES OF CORRELATION AND RESPONSE FUNCTIONS.

4-5. MF DYNAMICS FOR 'NON-TRIVIAL' MODELS

SOLUTION
GENERAL PREDICTIONS

'UNIVERSALITY' - SCALINGS - EXPERIMENTS.

GLASSES

- POLYMER GLASSES
- SPIN GLASSES
- STRUCTURAL GLASSES
- ORIENTATIONAL GLASSES
- VORTEX GLASSES

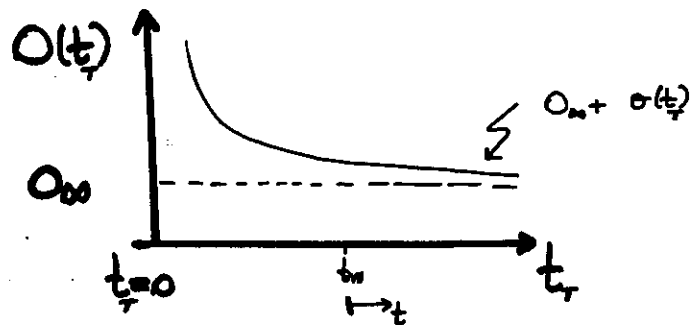
...

All rather different but

SIMILAR PHENOMENOLOGY

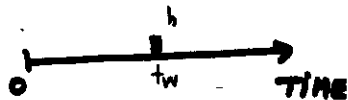
AT LOW TEMPERATURES

- ONE-TIME QUANTITIES eg. $E(t_f)$, $m(t_f)$



- APPEARS AS BEING EQUILIBRATED

for large times.



- TWO-TIME QUANTITIES eg.

$$\left\{ \begin{array}{l} \text{'LOCAL' CORRELATION} \\ \text{'LOCAL' RESPONSE} \end{array} \right. \quad C(t+tw, tw) = \frac{1}{N} \sum_{i=1}^N \langle s_i(t+tw) s_i(tw) \rangle$$

$$R(t+tw, tw) = \frac{1}{N} \sum_{i=1}^N \frac{\delta \langle s_i(t+tw) \rangle}{\delta h_i(tw)} \Big|_{h=0}$$

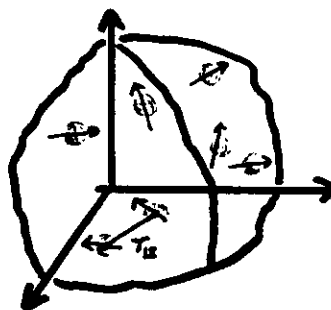
- DEPEND ON BOTH (tw, t)
- ARE NOT RELATED BY FDT

NO EQUILIBRIUM. [a moment I would talk about space for]

WHAT'S A SPIN GLASS ?

→ MODELS

MAGNETIC ALLOY, e.g. $\underline{\text{CuMn}}$, $\underline{\text{AgMn}}$



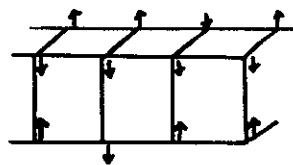
$\nearrow$ Mn MAGNETIC IMPURITIES
AT RANDOM FIXED
POSITIONS

QUENCHED RANDOMNESS

RKKY INTERACTIONS (BETWEEN Mn's)

$$J(\vec{r}_{12}) = J(|\vec{r}_{12}|) \simeq \frac{J_0 \cos(2k_F|\vec{r}_{12}| + \phi_0)}{(k_F|\vec{r}_{12}|)^3}$$

SYMMETRIC, RANDOM (THROUGH $|\vec{r}_{12}|$), $\sim |\vec{r}_{12}|^{-3}$ RAPID DECAY



$\nearrow$ Mn : ISING SPINS $s_i = \pm 1$
 $J(\vec{r}_{12})$: GAUSSIAN INTERACTIONS
 J_{ij} , $P[J]$ GAUSSIAN

DISORDER

$$H_J[\vec{s}] = \sum_{\langle ij \rangle} J_{ij} s_i s_j \longrightarrow \sum_{\langle ij \rangle} J_{ij} s_i s_j \quad \text{MF}$$

3D EDWARDS-ANDERSON $\rightarrow$ SHERRINGTON-KIRKPATRICK

MODELS : MORE SIMPLIFICATIONS

$$H_J[\vec{s}] = \sum_{\langle ij \rangle} J_{ij} s_i s_j$$

3DEA $s_i = \pm 1$



MF $H_J[\vec{s}] = \sum_{i \neq j} J_{ij} s_i s_j$

SK No GEOMETRY
 $s_i = \pm 1$



MF $H_J[\vec{s}] = \sum_{i_1 \neq i_2 \neq \dots \neq i_p} J_{i_1 \dots i_p} s_{i_1} \dots s_{i_p}$

p-spin MODEL
 $s_i = \pm 1$

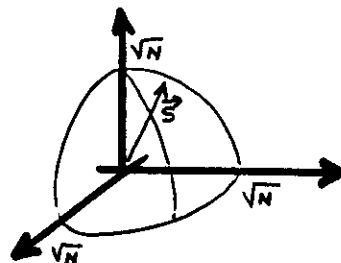
DISORDER

$P[J]: \begin{cases} \text{BIMODAL} \\ \text{GAUSSIAN (p \geq 2)} \end{cases} \left(\frac{N^{p-1}}{\pi p!} \right)^{1/2} \exp \left[-\frac{N^{p-1}}{p!} J_{i_1 \dots i_p}^2 \right]$

SPINS ISING : DIFFICULT!

: SPHERICAL

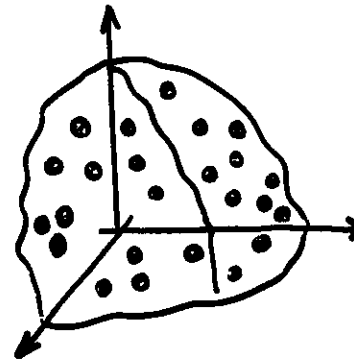
$\vec{s}$ ON A HYPERSPHERE
(N-DIMENSIONAL)



HOPE: $s_i = O(1), \forall i. \Rightarrow$ FINITE VALUE FOR s_i !

WHAT CAN FORM A 'STRUCTURAL' GLASS?

→ MODELS



● 'PARTICLES' THAT
'MOVE'
INSIDE THE SAMPLE

INTERACTIONS An example LÉNNARD-JONES

$$V(\vec{r}_1, \vec{r}_2) = V(|\vec{r}_1 - \vec{r}_2|) = -\frac{C_4}{|\vec{r}_1 - \vec{r}_2|^6} + \frac{C_2}{|\vec{r}_1 - \vec{r}_2|^{12}}$$

NO QUENCHED DISORDER

SIMPLIFIED MODELS

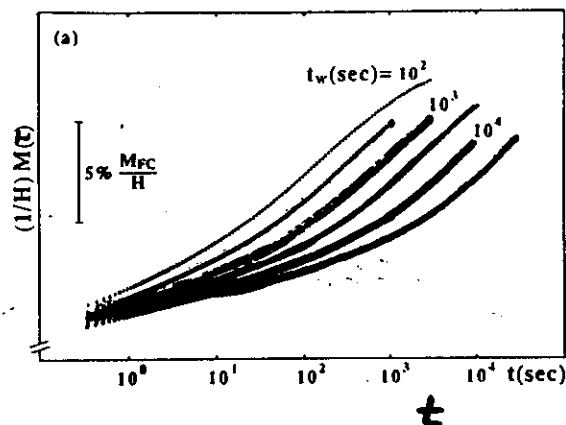
e.g. $H[\vec{r}_a] = \sum_{a \neq b}^{N_{\text{part}}} \sum_{i=1}^D (r_i^a \cdot r_i^b)^p$ or

$\sim$ p-spin model. Motivated by Spin-Glass Modelling.

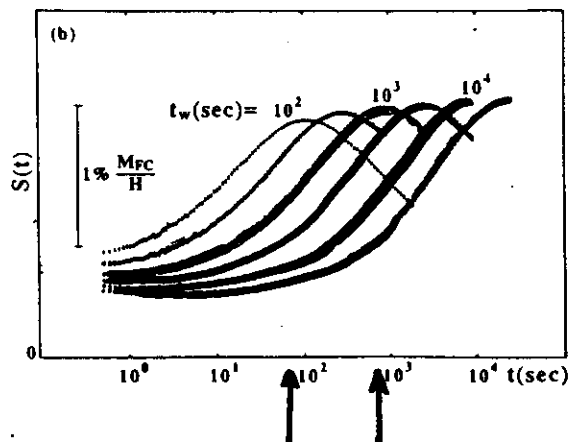
AGING IN SPIN-GLASSES

ZERO FIELD COOLING EXPERIMENT (ZFC)

$$\frac{m(t)}{h}$$



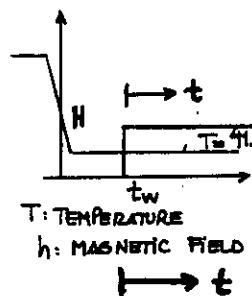
$$S(t) = \frac{1}{h} \frac{\partial m(t)}{\partial \ln t} \quad (t \sim \tau \text{ HERE})$$



max S(t) AT $t \sim t_w$

CuMn

($T_g = 45.3K$)
 $h = 0.8G$



$t_{w1} = 100s$

$t_{w2} = 300s$

$t_{w3} = 1000s$

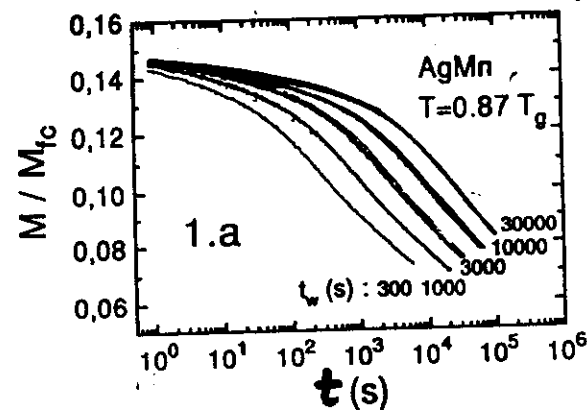
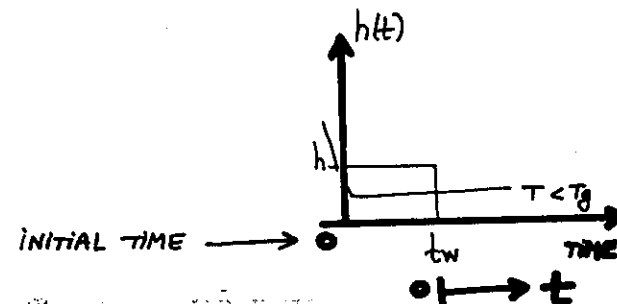
$t_{w4} = 3000s$

$t_{w5} = 10000s$

$t_{w6} = 30000s$

THERMO-REMANENT MAGNETIZATION

SACLAY-GROUP DATA



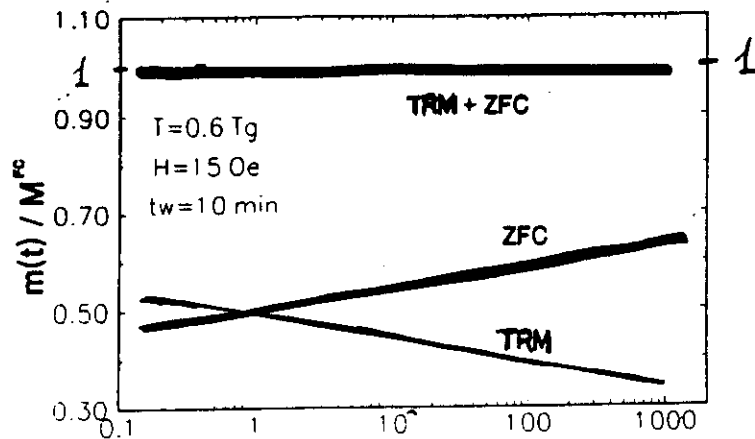
EXPLICIT t_w DEPENDENCE

AGING

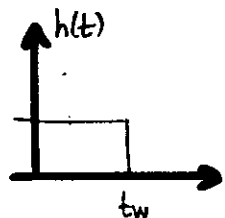
MECHANISM?
SCALING?

LINEAR RESPONSE THEORY

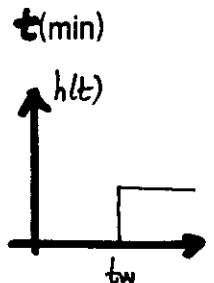
$$\frac{m^{TRM}}{m^{FC}} + \frac{m^{ZFC}}{m^{FC}} = 1$$



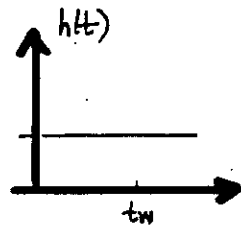
MAGNETIC FIELD



TRM



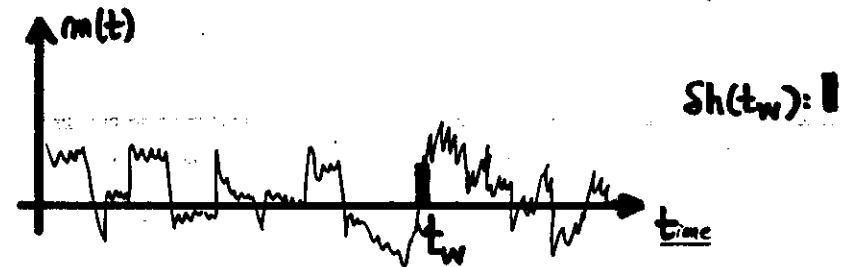
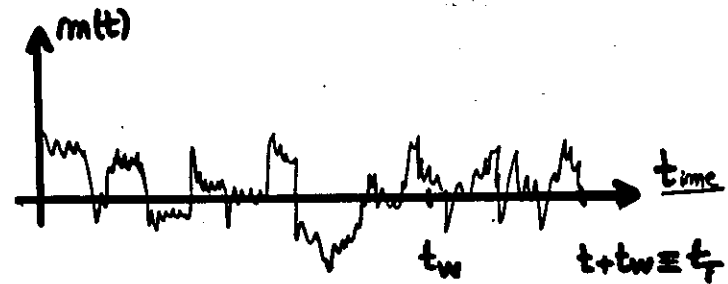
ZFC



FC

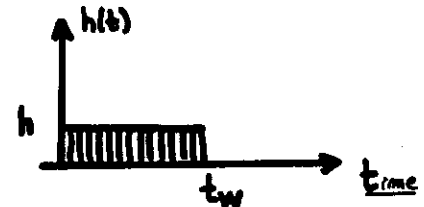
MOST PROBABLY $T_{\text{NON-LINEAR}}(h)$ FOR FINITE h

TRM - ZFC $\leftrightarrow$ RESPONSE



$$\left. \frac{\delta m(t)}{\delta h(t_w)} \right|_{h=0} \equiv R_m(t, t_w) \quad \text{RESPONSE}$$

IF WE NOW APPLY
TRM



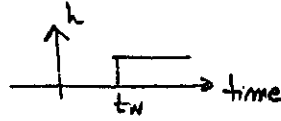
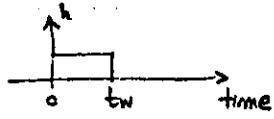
$$\frac{\Delta m(t, t_w)}{\Delta h} = \int_0^{t_w} ds \frac{\delta m(t)}{\delta h(s)} = \int_0^{t_w} ds R_m(t, s)$$

$$m(t, t_w)_{\text{TRM}} = h \cdot \int_0^{t_w} ds R_m(t, s)$$

LINEAR RESPONSE THEORY

$$m_{TRH}(t_T, t_W) \equiv h \int_0^{t_W} ds R(t_T, s)$$

$$m_{ZFC}(t_T, t_W) \equiv h \int_{t_W}^{t_T} ds R(t_T, s)$$



if $R(t_T, s) = R(t_T - s)$

$$m_{TRH}(t_T, t_W) = h \int_0^{t_T} ds R(t_T - s) - \underbrace{h \int_{t_W}^{t_T} ds R(t_T - s)}_{m_{ZFC}(t_T, t_W)}$$

$$m_{ZFC}(t_T, t_W) = h \int_{t_W}^{t_T} ds R(t_T - s)$$

$$m_{ZFC}(t_T, t_W) = h \int_0^t dt R(t) = m_{ZFC}(t \equiv t_T - t_W)$$

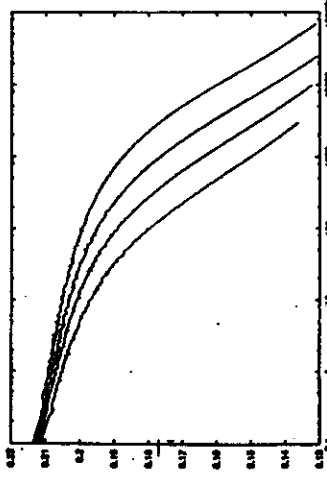
$$m_{TRH}(t_T, t_W) = \underbrace{h \int_0^{t_T} dt R(t)}_{\text{CONST}} - h \int_0^t dt R(t)$$

$$m_{TRH}(t_T - t_W) = \text{CONST} - h \int_0^t dt R(t) = m_{TRH}(t)$$

THIS PROOF CAN BE DONE BACKWARDS: $R(t_T - t_W) \Leftrightarrow m(t_T - t_W)$

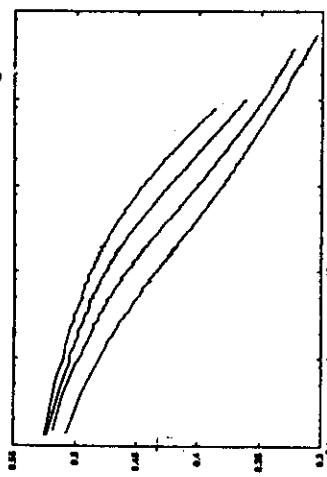
THERMO REMANENT MAGNETIZATION

(log-linear) Plots:



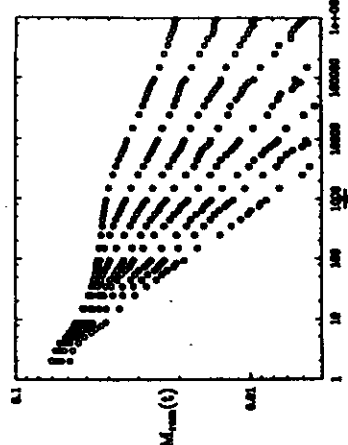
Ag:Mn (SACLA - DATA)

EXP



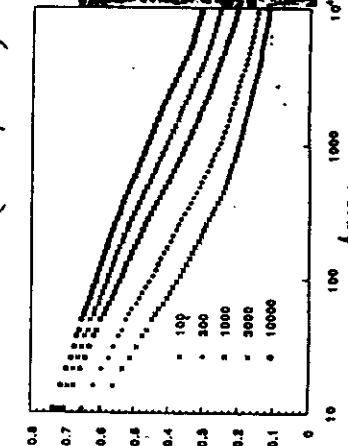
Thio spinel (SACLA - DATA)

EXP



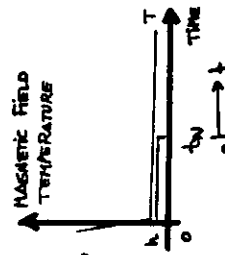
3D EA (H. RIEBER)

3D



Thio spinel (SACLA - DATA)

EXP



$$m_{TRH}(t_T, t_W) = h \int_0^{t_W} ds R(t_T, s)$$

LINEAR RESPONSE

MF D-HYPERCUBIC CELL (MF) ~ SK

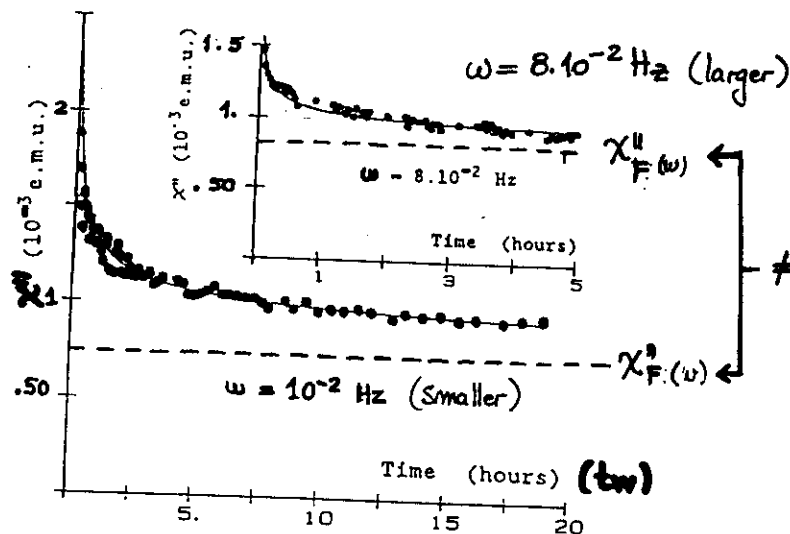
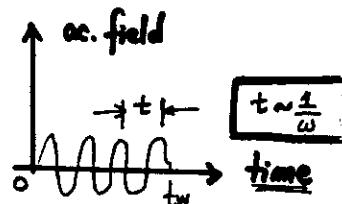
(L.F. CUSUMANO, J. KURCHAN, F. RYBART)

OUT OF PHASE SUSCEPTIBILITY

$T < T_g : \chi''(\omega, t_w)$

IN THESE PLOTS:

$\omega t_w \lesssim 0(10^3)$



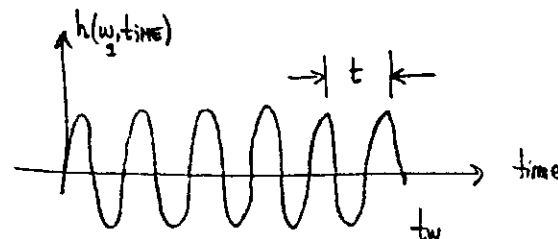
EXPERIMENTALLY OBSERVED $\left\{ 10^{-2} \text{ Hz} \sim 1 \text{ Hz} \right.$ FREQUENCIES.

AMPLITUDE OF

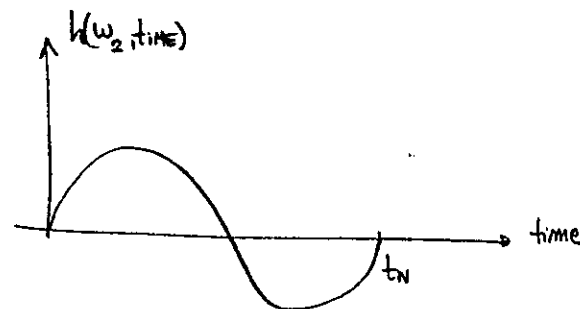
$\chi''(\omega, t_w) \equiv \text{Im} \int_0^{t_w} ds e^{i\omega s} \underbrace{R(t, s)}_{\text{RESPONSE FUNCTION}}$

$\chi''(\omega, t_w) \sim$ DEPENDS UPON ω VS. t_w .

OUT OF PHASE SUSCEPTIBILITY



'large' $\omega_1 = \frac{2\pi}{t}$



'smallest' $\omega_2 = \frac{2\pi}{t_w}$

EXPERIMENTAL
CONSTRAINT

$\omega = \frac{2\pi}{t} \geq \frac{2\pi}{t_w}$

(INDEED, THERE MUST BE A FEW CYCLES IN SUCH A WAY TO HAVE A 'GOOD' MEASUREMENT)

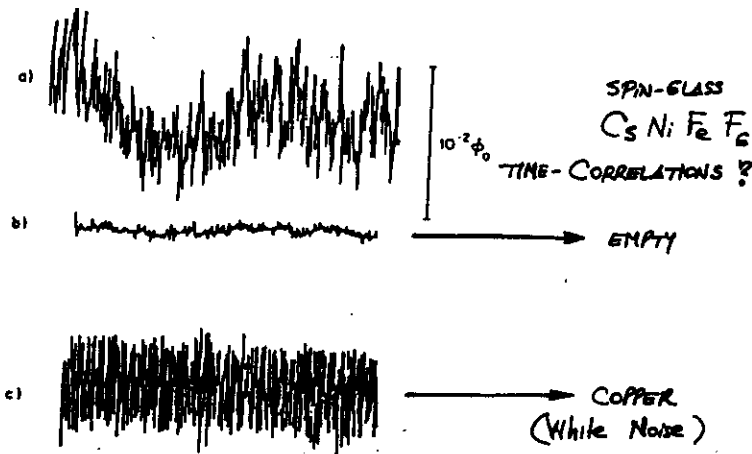
THUS

$t \leq t_w$

AND, IN SUSCEPTIBILITY MEASUREMENT ONE CANNOT REACH LARGER t 's !

* OUT OF PHASE SUSC. MEASUREMENTS ARE BETTER BECAUSE h IS SMALLER BUT ARE NOISIER BECAUSE ONE CANNOT REACH VERY LONG t 's.

MAGNETIC NOISE IN SPIN-GLASS

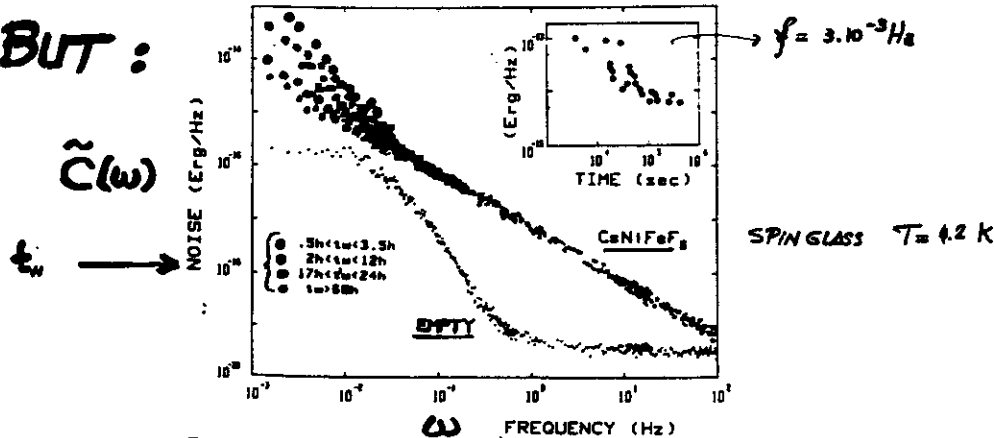


TI ASSUMPTION $\Rightarrow$
FOURIER TRANSFORM:

$$C(t) \rightarrow \tilde{C}(\omega)$$

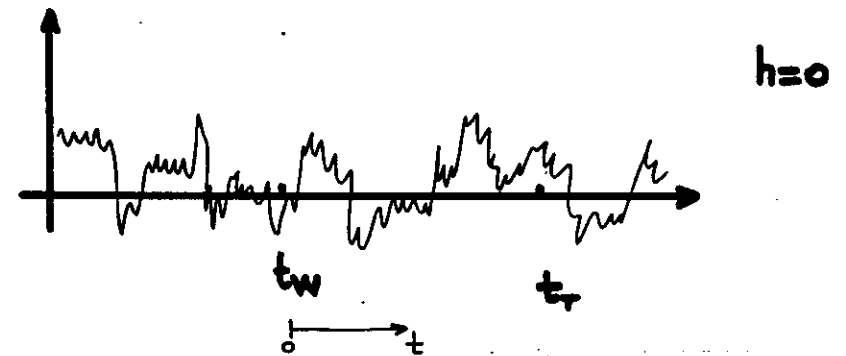
H. OCHO, H. BOUCHIAT AND P. MONOD, J. MAGN. MAGN. MAT 51 (1985) 11.

BUT:



NON STATIONARY CONTRIBUTION: t_w -DEPENDENCE

CORRELATION FUNCTIONS



NO FIELD (PERTURBATION) APPLIED

$$\frac{1}{N} m(t_r) m(t_w) \equiv C_m(t_r, t_w)$$

CORRELATION

NORMALIZATION

IN GLASSES: DENSITY - DENSITY CORRELATIONS

MEASUREMENT:

$\vec{r}$: Position in Space

$S(\vec{r}, t)$: Time Dependent Density at $\vec{r}$

$$S(\vec{q}, t) \equiv \int d^d r e^{i\vec{q} \cdot \vec{r}} S(\vec{r}, t)$$

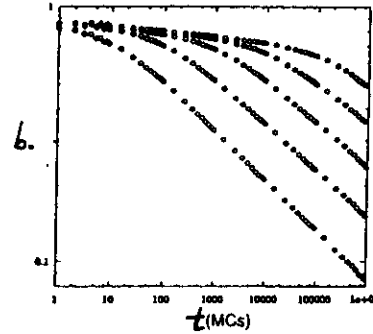
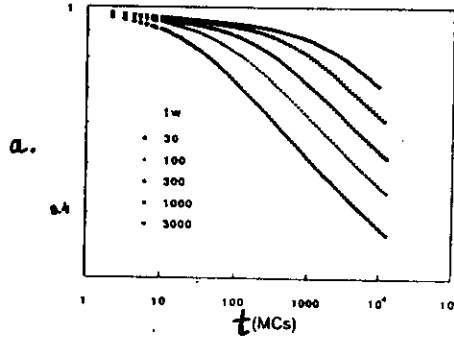
$$C_q(t_r, t_w) = \frac{\langle S^*(\vec{q}, t_r) S(\vec{q}, t_w) \rangle}{\langle |S(\vec{q}, t_w)|^2 \rangle} \leftarrow \text{Normalization.}$$

$\langle \cdot \rangle$ Average over dynamical histories (Numerics)

$C(t+t_w, t_w)$ vs. t

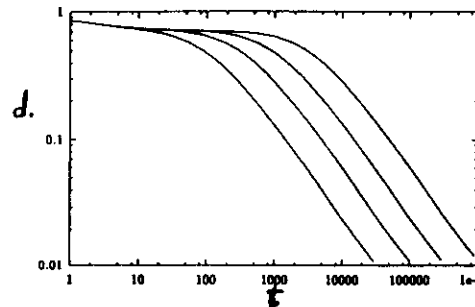
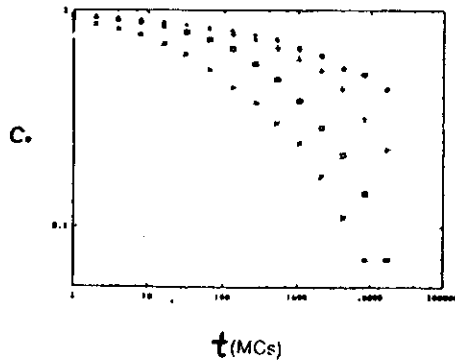
$$C(t+t_w, t_w) = \frac{1}{N} \sum_{i=1}^N \langle S_i(t+t_w) S_i(t_w) \rangle$$

log-log Plots:



(MF) D-HYPERCUBIC CELL (SK)
(D=17) $t_w = 30, 10^2, 300, 10^3, 3000$

3D EA
 $t_w = 10, 10^2, 10^3, 10^4, 10^5$



(MF) P-SPIN (SPHERICAL)
(P=3) $t_w = 4, 64, 1024, 16,000$

(MF) P=2 SPHERICAL
(ANALYTICAL)
 $t_w = 30, 100, 300, 1000$

a. L.F. CUGLIANDOLO, J. KURCHAN, F. RITORT; *PRB* **49**, 6331 (1994).

b. H. RIEGER; *J. PHYS A* **26**, L615 (1993).

c. D. STROCKA, H. RIEGER, H. SCHRECKENBERG; UNPUBLISHED.

d. L.F. CUGLIANDOLO, D.S. DEAN; *J. PHYS A* **28**, 4213 (1995).

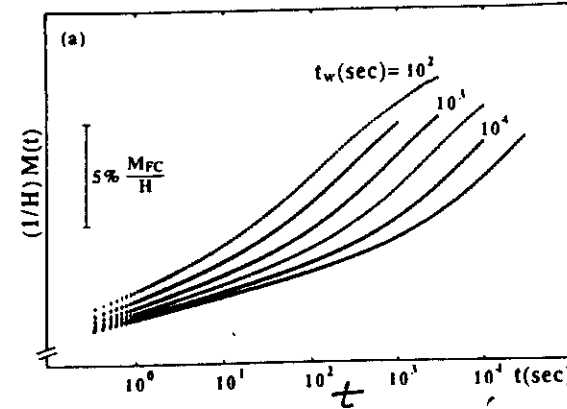
EXP ?

PHYSICAL AGING $T < T_g$

CuMn

SPIN-GLASS

ZFC EXPERIMENT

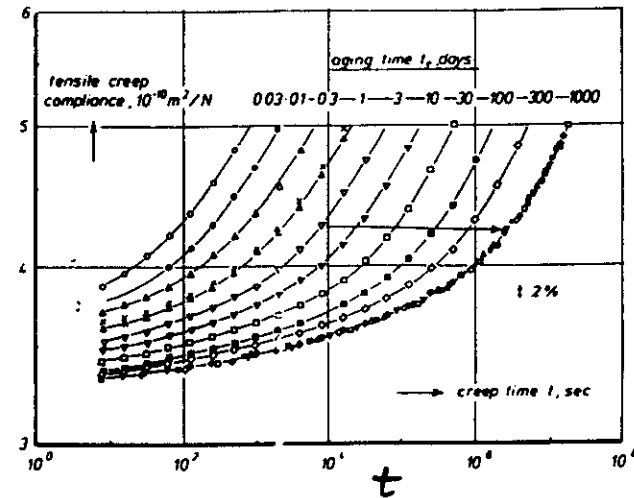


$T_g = 45.3 \text{ K}$
 $H = 0.8 \text{ G}$

L. SANDLUND, P. SVEDLINDH, P. NORBLAD, O. BECKMAN, *PHYS REV LETT* **51** (1983) 911.

PVC POLYMER GLASS

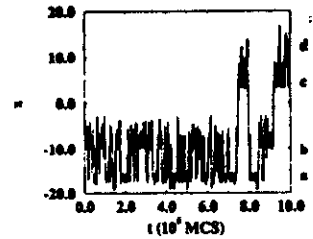
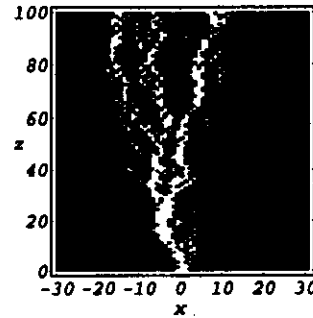
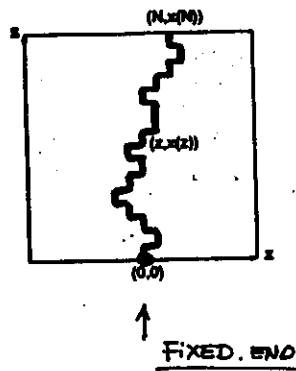
$\sigma-H$
 $t_0=0$ t_w t
 $T < T_g$
TIME
H: MAGNETIC FIELD
 σ : STRESS
 $f \rightarrow \infty$



L. STRUICK, 'PHYSICAL AGING IN AMORPHOUS POLYMERS' (1978)

1+1 DIRECTED POLYMER

RANDOM ENVIRONMENT

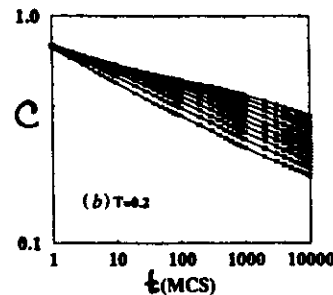
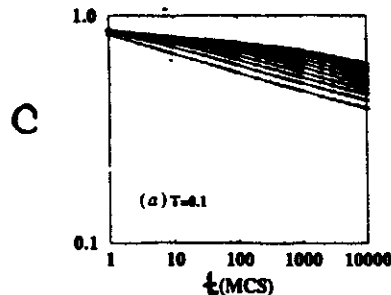


$$H = \sum_{k=1}^N V[z, x(z)]$$

WITH $V(z, x)$ TAKEN FROM
A UNIFORM DIST $[-1, 1]$.

Off-equilibrium dynamics of (1+1)-dimensional DPRM

H Yoshino J. PHYS. A29, 421 (1996).

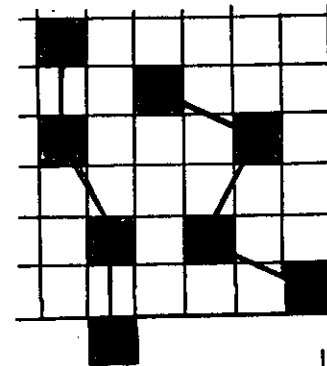


DIFFERENT
 t_W 'S

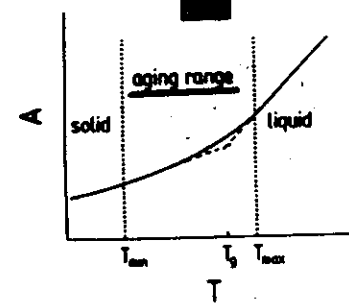
See Also A. BARRETT, J. PHYS. REV E (97) 9701021/COND-MAT.

POLYMER GLASSES

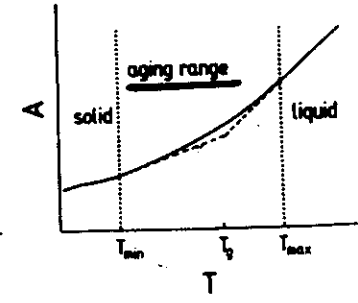
LATTICE MODEL



BINDER ET AL.



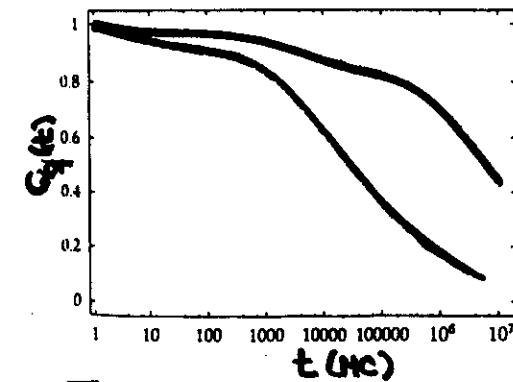
(a) experiment



(b) simulation

MC DYNAMICS

J. BASCHNAGEL, PHYS. REV. 69, 135 (96).



$$t_W = 4 \cdot 10^6 \text{ MC}$$

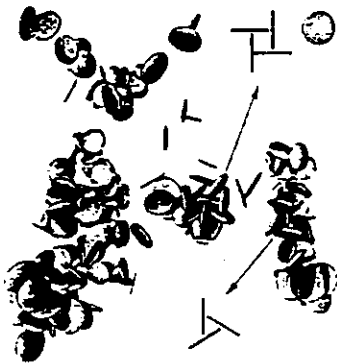
$$t_W = 6 \cdot 10^3 \text{ MC}$$

$$T_{min} < T = 0.16 < T_{max}$$

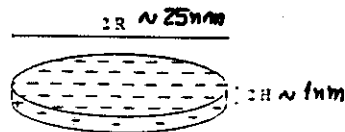
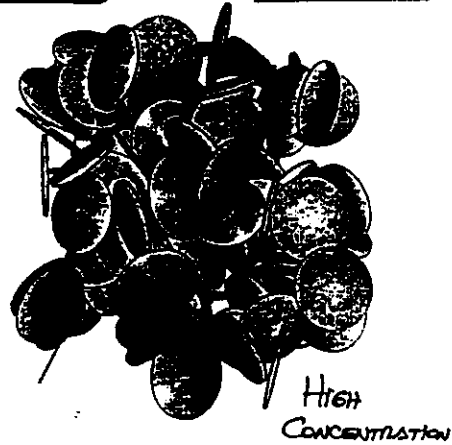
CLAY COLLOID SUSPENSIONS

LANGUIN DYNAMICS

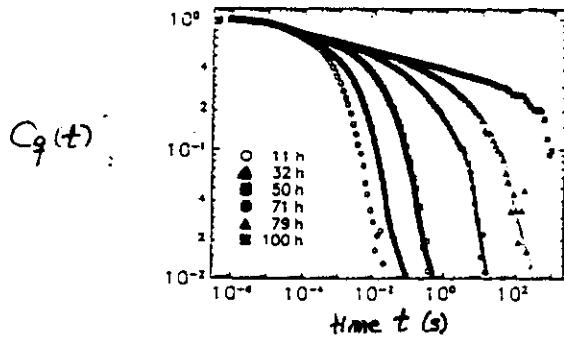
'HOUSE OF CARDS'



LOW CONCENTRATION



H. DIJKSTRA, J-P. HANSEN, P. A. MADDEN; *PHYS. REV. LETT.* **75**, 223 (95)
W. KROON, G. H. WEGDAM, R. SPRICK; *PHYS. REV. E* **54** (96).

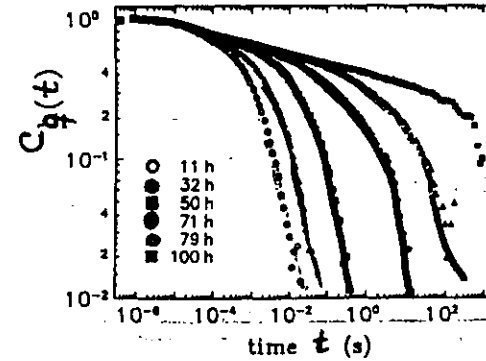


FOR A GIVEN q .

AGING AT LEAST UNTIL $\begin{cases} t_w \sim 100h \\ t \sim 1h \end{cases}$

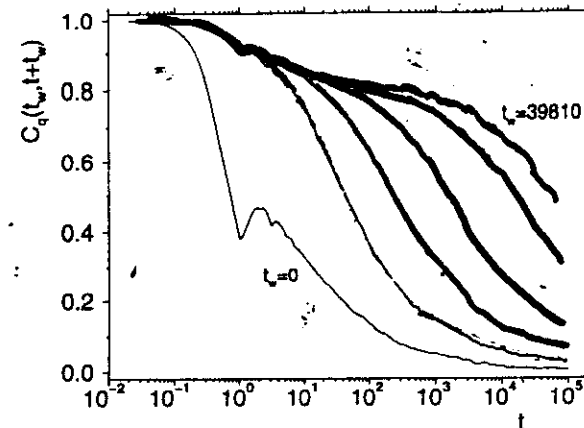
CORRELATION FUNCTIONS GLASSES

EXPERIMENT
(GEL)



M. KROON, G. H. WEGDAM, R. SPRICK; *PHYS. REV. E* **54**, 1 (1996).

(MOLECULAR DYNAMICS) SIMULATION



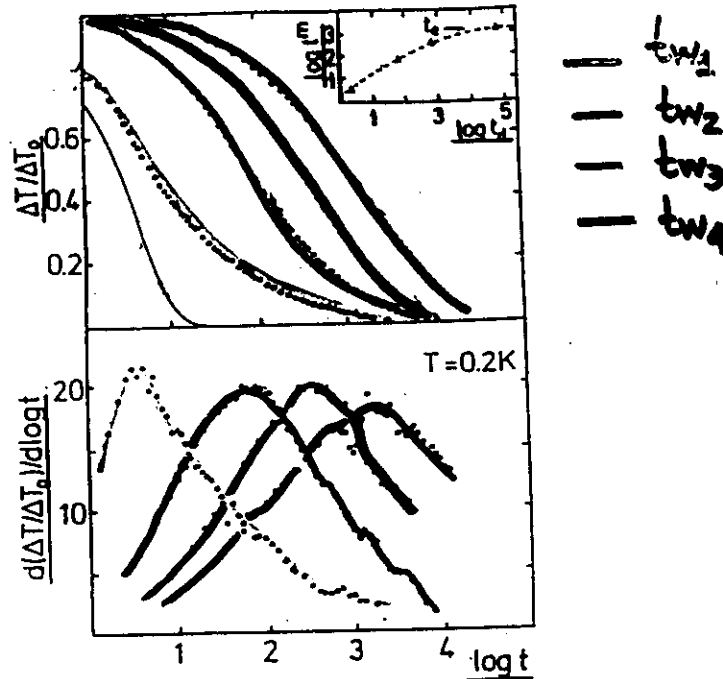
W. KOB, J. L. BARRAT *PHYS. REV. LETT.* (1997).

LÉNNARD-JONES

Also: G. Parisi (1994)
MONTECARLO SIM

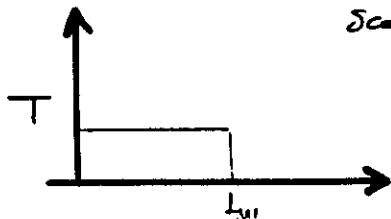
CHARGED DENSITY

WAVES



K. BILJAKOVIĆ, J.C. LASJAUMAS, P. MONCEAU, PRL (93).

K. BILJAKOVIĆ in 'Phase Transitions and Relaxation in Systems with Competing Energy Scales' Kluwer Ac. (1993).

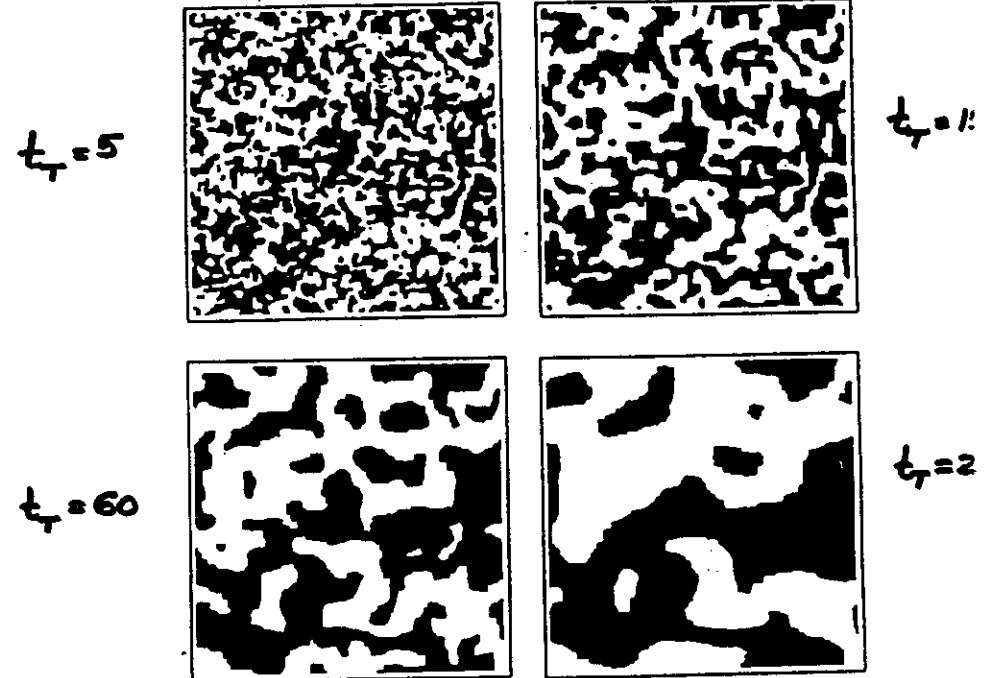


TEMPERATURE JUMP.

DOMAIN GROWTH

A.J. BRAY. (REVIEW). J. KISSNER

2D ISING MODEL (MC) $T=0$.



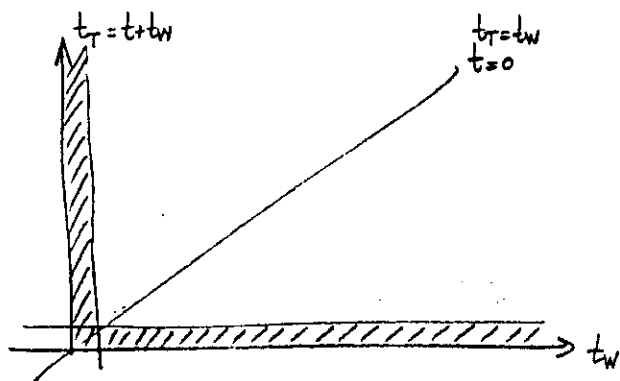
SCALING $\left\{ \begin{array}{l} \rightarrow \\ C(r, t, t') \end{array} \right.$

$$C(r/\ell(t), r/\ell(t'))$$

$$C(r=0, t, t') = f\left(\frac{\ell(t')}{\ell(t)}\right)$$

WHAT SORT OF FUNCTIONS DO WE HAVE?

TWO-TIME DEPENDENCES



SCHEMATICALLY: 'FINITE TIMES', i.e. $t_W \in [0, \delta]$
 $t_T \in [0, \delta]$

WITH δ 'FINITE'

WE'LL ASSUME THAT 'GLASSY' SYSTEMS WE DEAL WITH
 FORGET WHAT HAPPENED TO THEM IN FINITE TIME
 INTERVALS.

- PROP I OF 'WEAK-LONG-TERM MEMORY'.
 (SEE LATER.)

IF WE WANT TO STUDY THE ASYMPTOTIC BEHAVIOUR
 WE NEED TO TAKE THE LIMIT OF LARGE TIMES BUT WE
 HAVE TO EXPLICITATE HOW WE TAKE THIS LIMIT.

TIMES INVOLVED

MICROSCOPIC T_0 T_0 (1MC, 10^{-12} sec, T_0 IN LANGEVIN)
 TIME

WAITING
 TIME t_W

'MEASURING'
 TIME $t_T = t + t_W$

EQUILIBRATION
 TIME t_{eq}

- IN GLASSES t_{eq} IS EXTREMELY LARGE.
- IN EXPERIMENTS, IN SG PRESUMABLY NEVER REACHED.
- " MF SG t_{eq} IS BELIEVED TO BE $O(e^N)$

THUS

$$T_0 \ll (t_W, t_T) \ll t_{eq}$$

IN THE CALCULATIONS, THE ASYMPTOTIC LIMIT MEANS

$$\lim_{t_W, t_T \rightarrow \infty} \lim_{N \rightarrow \infty}$$

WE STILL HAVE TO SAY HOW DO (t_W, t_T) GO TO ∞ .

CORRELATIONS: DATA

$$C(t+tw, tw) = \frac{1}{N} \sum_{i=1}^N \overline{S_i(t+tw) S_i(tw)}$$

VARIATION WITH RESPECT TO t FOR tw FIXED.

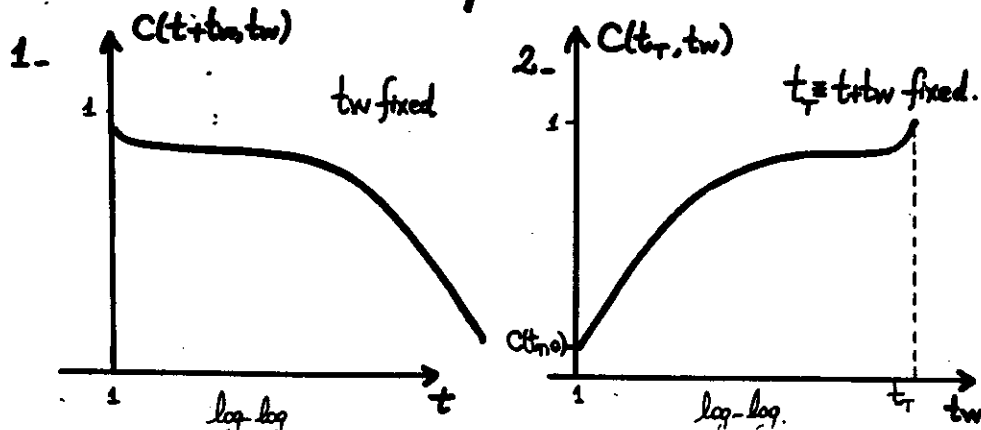
$$\bullet \quad \frac{\partial C(t+tw, tw)}{\partial t} \leq 0 \quad 1-$$

MONOTONOUSLY DECREASING

VARIATION WITH RESPECT TO tw FOR t FIXED.

$$\bullet \quad \frac{\partial C(t+tw, tw)}{\partial tw} \Big|_{t+tw \text{ fixed}} \geq 0 \quad 2-$$

MONOTONOUSLY INCREASING



CORRELATIONS DATA

$$C(t+tw, tw) = \langle \delta m(t+tw) \delta m(tw) \rangle$$

$$= \frac{1}{N} \sum_{i=1}^N \overline{S_i(t+tw) S_i(tw)}$$

OBSERVATION: C DEPENDS ON (t, tw) (BOTH!)

$$\bullet \quad C(t+tw, tw) \neq C(t) \quad \forall (t, tw)$$

NO INVARIANCE UNDER TIME-TRANSLATION

BUT

WHEN $tw \gg t$ $C(t+tw, tw) \sim C(t)$

$$\bullet \quad \lim_{tw \rightarrow \infty} C(t+tw, tw) = C_F(t)$$

$$\bullet \quad \lim_{t \rightarrow \infty} C(t) = \overline{f_{EA}}$$

(AGAIN: A 'TIMES-SECTOR' WHERE TH HOLDS!)

WHEN $t \gg tw$ $C(t+tw, tw) \sim 0$

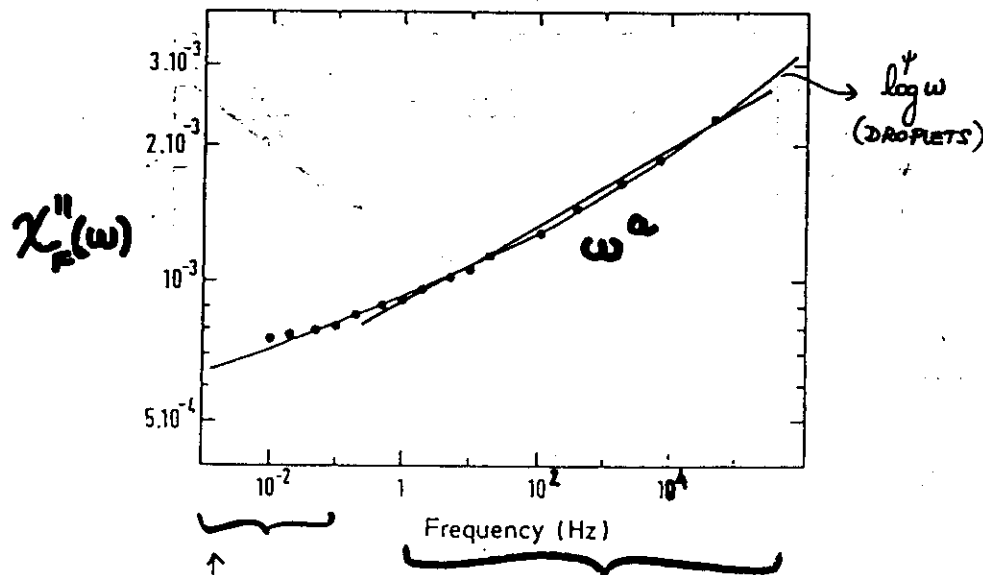
$$\bullet \quad \lim_{t \rightarrow \infty} C(t+tw, tw) = 0$$

OUT OF PHASE SUSCEPTIBILITY

$$T < T_g : \chi''(\omega, t\omega)$$

$$\omega t\omega \text{ LARGE} \Rightarrow \boxed{\chi''_F(\omega)}$$

'STATIONARY' PART : NO $t\omega$ -DEPENDENCE



HIGH FREQUENCIES

SMALLER FREQUENCIES

OUT OF EQUILIBRIUM $\Rightarrow t\omega$ -DEPENDENCE

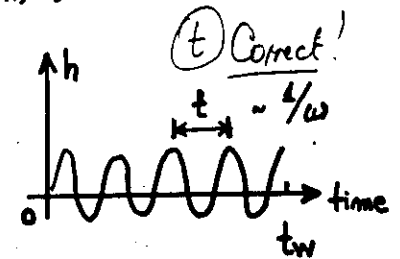
POWER LAW or LOGARITHMIC?

$$\boxed{\chi''_F(\omega) \sim \omega^a}$$

EXPONENT: $a(T) : 0.01 - 0.1$ ($T \uparrow$) (or $\log \omega$?)

OUT OF PHASE SUSCEPTIBILITY

$$\frac{\chi(\omega, t\omega)}{h} = \int_0^{t\omega} ds e^{i\omega s} R(t\omega, s)$$



$$\chi'(\omega, t\omega) = \text{Re } \chi(\omega, t\omega)$$

In phase Susceptibility

$$\chi''(\omega, t\omega) = \text{Im } \chi(\omega, t\omega)$$

Out of phase Susceptibility.

Observation: $\chi''(\omega, t\omega)$ Depends on both $(\omega, t\omega)$.

$$\bullet \chi''(\omega, t\omega) \neq \chi''(\omega)$$

$\forall (t, t\omega)$

NO INVARIANCE UNDER TIME-TRANSLATIONS

BUT IF $\omega t\omega \gg 1$ (large)

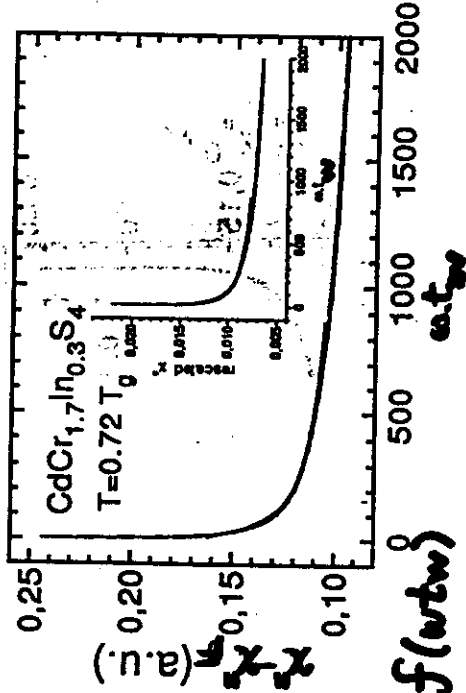
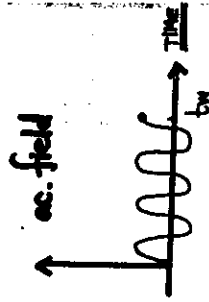
$$\bullet \lim_{\omega t\omega \rightarrow \infty} \chi''(\omega, t\omega) = \chi''_F(\omega) \sim \omega^{-a}$$

$$\bullet \chi''(\omega, t\omega) - \chi''_F(\omega) \sim (\omega t\omega)^b$$

$\hookrightarrow$ GENERAL $\forall (\omega, t\omega)$

OUT OF PHASE SUSCEPTIBILITY

LOW AND HIGH FREQUENCIES DYNAMICAL SCALING



SCALING

$$\chi''(\omega t_w) \sim \chi_F''(\omega) + f(\omega t_w)$$

$$(\omega) = 0.04, 0.03, 0.1, 1, H_z.$$

$$\chi''(\omega, t_w) \sim c t_w + \omega^a + c t_w \cdot (\omega t_w)^b$$

APPROX. FOR $\omega t_w > 1$

COND. MET / %
E. V. K. ... T. ... H. ... J. P. ... I. C. ...

SACLAY DATA

THERMO REMANENT MAGNETIZATION DATA

$$m^{TRM}(t+t_w, t_w) = h \cdot \int_0^{t_w} ds R(t+t_w, s)$$

OBSERVATION : m^{TRM} DEPENDS ON (t, t_w) BOTH!

$$\bullet R(t+t_w, t_w) \neq R(t)$$

NO INVARIANCE UNDER TIME-TRANSLATION.

BUT:

$$\text{WHEN } t_w \gg t, m^{TRM}(t+t_w, t_w) \sim m^{TRM}(t)$$

$$\bullet \lim_{t_w \rightarrow \infty} R(t+t_w, t_w) = R_F(t)$$

(DEFINES A 'TIMES-SECTOR' WHERE τ_1 HOLDS!)

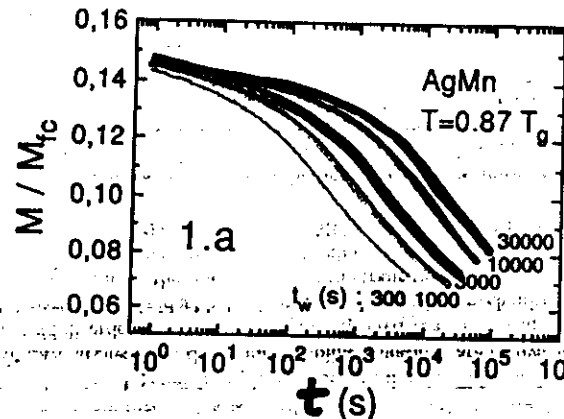
$$\text{WHEN } t \gg t_w, m^{TRM}(t+t_w, t_w) \sim 0$$

$$\bullet \lim_{t \rightarrow \infty} R(t+t_w, t_w) = 0$$

NO REMANENT MAGNETIZATION

$$m^{TRM}(t+t_w, t_w) \sim m_F(t) + m_A \left(\frac{h(t_w/\tau_0)}{h(t+t_w/\tau_0)} \right)$$

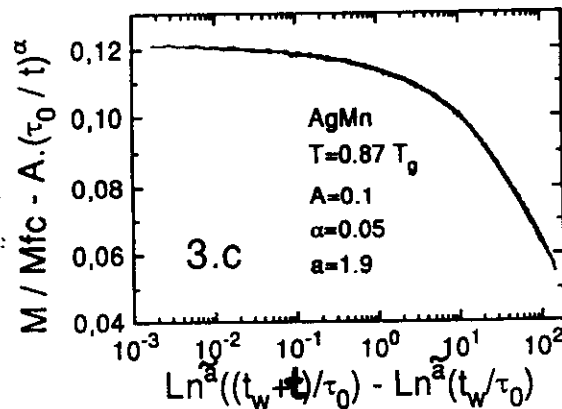
SLOW DYNAMICS



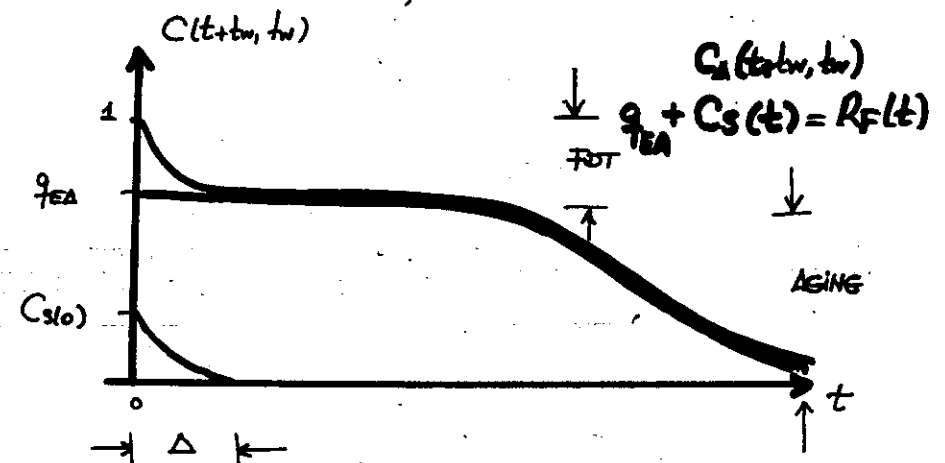
ENHANCED POWER LAW:

$$h(t_w/\tau_0) = \exp \ln^a(t_w/\tau_0)$$

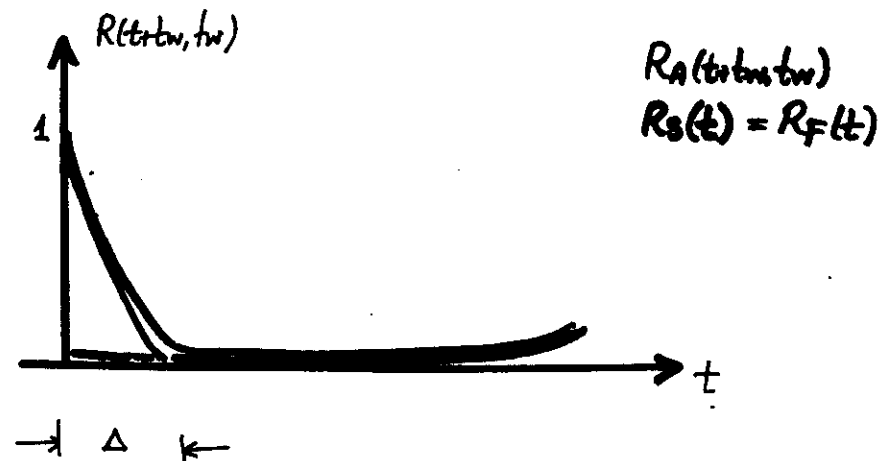
SCALING OF THE 5 CURVES



CORRELATION FUNCTION C(t+t_w, t_w)



RESPONSE FUNCTION R(t+t_w, t_w)



τ₀: MICROSCOPIC TIME SCALE.

SUMMARY

EXPERIMENTS

SPIN-GLASSES

MAGN RELAX $h \neq 0$
OUT OF PH. SUSC. $h \neq 0$
MAGN NOISE $h = 0$

COLLOIDS

DENS-DENS. CORR. $h =$

POLYMER GLASSES $\rightarrow$ MECH. PROP.

$f \neq 0$

CHARGED DENSITY WAVES $\rightarrow$ CALORIMETR

NUMERICS

SPIN-GLASSES

MAGN. RELAX $\left\{ \begin{array}{l} \text{FINITE D} \\ \text{HF-MODEL} \\ \text{MC-DYNAM} \end{array} \right.$
AUTO-CORR

'LENNARD-JONES' GLASSES

'MAGN' RELAX $\left\{ \begin{array}{l} \text{MC-MD} \\ \text{AUTO-CORR} \end{array} \right.$

SINGLE POLYMER

RESPONSE $\left\{ \begin{array}{l} \text{MC} \\ \text{AUTO-CORR} \end{array} \right.$

POLYMER GLASSES AUTO-CORR

LATTICE GASES, 'SELF-ORGANIZED CRITICALITY', ETC, ETC.

SCIENCE 267, 1924 (95).

FRONTIERS IN MATERIALS SCIENCE: ARTICLES

Physical Aging in Polymer Glasses

Ian M. Hodge

Physical aging refers to structural relaxation of the glassy state toward the metastable equilibrium amorphous state, and it is accompanied by changes in almost all physical properties. These changes, which must be taken into account in the design, manufacture, and use of glassy polymer materials and devices, present a daunting challenge.

— LET'S DEFINE THE MICROSCOPIC DYNAMICS OF THE SYSTEM:

To « T_{exp} : 'EXPERIMENTAL TIME SCALE' $\Rightarrow$ J, J_0 FIXED $\rightarrow$ QUENCHED.

$\rightarrow S_i(t)$ DYNAMICAL VARIABLES $i = 1, \dots, N$

WHAT IS THEIR TIME EVOLUTION?

WE WANT TO CHOOSE AN UPDATING RULE SUCH THAT THE SYSTEM COULD EVENTUALLY EQUILIBRATE, i.e. SUCH THAT, FOR N finite AND

$$P(\vec{s}, t \rightarrow \infty) = \exp[-\beta H_J[\vec{s}]] \quad (1)$$

BOLTZMANN'S DISTRIBUTION ($\beta = 1/k_B T$).

SINCE THE SYSTEM IS IN A THERMAL BATH, WE'LL MIMIC THE INTERACTION BETWEEN THE MAGN MOMENTS AND LATTICE VIBRATIONS (PHONONS) CONDUCTING ELECTRONS (IN METALLIC SS) BY A THERMAL NOISE $\xi_i(t)$ AND 'TRANSFORM' THEN THE SPINS INTO STOCHASTIC VARIABLES $\vec{S}_i, \vec{S}_j$. (2)

THUS, WE ARE LED TO CONSIDER A STOCHASTIC DYNAMICS THAT LEADS TO EQUILIBRIUM AT ∞ -TIMES. WHAT ∞ -TIMES MEAN IT'S A DIFFICULT QUESTION THAT WE'LL ANSWER LATER.

EQ. (1) MEANS THAT, IF THE SYSTEM IS IN A SITUATION SUCH THAT ITS CONF. IS WEIGHTED BY THE BOLTZMANN'S WEIGHT THEN

$$\overline{[f(\vec{s})]} = \lim_{T \rightarrow \infty} \frac{1}{T} \int_0^T dt f[\vec{s}(t)] = \langle f[\vec{s}] \rangle_{GB} \quad (2)$$

THAT EACH SPIN KNOWS THE CONF. OF ALL OTHER SPINS ONLY ONE TIME STEP BEFORE. THE SPINS DO NOT HAVE MEMORY.

* COMMENT $\rightarrow$ UNIVERSALITY $\rightarrow$ DON'T EXPECT THE MACROSCOPIC BEHAVIOUR TO DEPEND STRONGLY UPON THE DYNAMICS. GLAUBER DYNAMICS:

THE NATURAL CHOICE OF DYNAMICS FOR ISING SPINS IS THE ONE PROPOSED BY GLAUBER FOR THE ISING MODEL. BUT, IT IS DIFFICULT TO DEAL WITH IT ANALYTICALLY IN THESE PROBLEMS. MONTE CARLO: JUST A COMPUTATIONAL WAY OF IMITATING GLAUBER. SOFT SPINS $\rightarrow$ LANGEVIN DYNAMICS

ISING SPINS CAN BE MADE CONTINUOUS VARIABLES IF WE

ADD A SOFT SPIN CONSTRAINT

$$H_{soft} = \frac{A}{2} \sum_i [(S_i^2 - 1)^2] \quad -\infty \leq S_i \leq \infty \quad (3)$$

TO THE ENERGY, WITH A A PARAMETER THAT ONE TAKES TO ∞ AT THE END OF THE CALCULATIONS.

MANY OF THE COMMON MODELS DEAL DIRECTLY WITH CONTINUOUS SPINS, AS IS THE CASE OF THE SPHERICAL MODELS.

A WELL-KNOWN STOCHASTIC DYNAMICS OF CONTINUOUS VARIABLES IS PROVIDED BY THE LANGEVIN EQUATION

$$\dot{S}_i(t) = -\mu \frac{\delta H_J[\vec{S}]}{\delta S_i(t)} + \xi_i(t) \quad (4)$$

WITH

$$\langle \xi_i(t) \xi_j(t') \rangle = (2A)^{-1} \delta_{ij} \delta(t-t') \quad (5)$$

WHITE NOISE.

(IN THIS EXPRESSION ONE HAS NEGLECTED ANY 'INERTIA', ANY OTHER PARAMETER THAT COULD APPEAR IN FRONT OF THE $\dot{S}$ 'S CAN BE REABSORBED IN μ AND A .)

III (8)
 [ONE CAN OBTAIN SUCH AN EQ. BY CONSIDERING THE INTERACTION OF SYSTEM VARIABLES S_i WITH BATH VARIABLES X_i REPRESENTED, E.G. BY HARMONIC OSCILLATORS, & INTEGRATING OUT THE BATH VARIABLES IN SUCH A WAY TO REPRESENT THE EFFECT OF THE BATH BY A RANDOM FORCE $\xi_i(t)$. SEE EG. FORD, KAC, MAZUR. FEYNMAN - VERHOUWEN.]

• SOLUTION TO THE L-EQ

ONE HAS TO SOLVE EQ. (4) IN A PROBABILISTIC SENSE, SINCE WE ONLY KNOW $P[S_i(t)]$. THE SOLUTION TO EQ. (4) READS

$$\dot{x}_i^{\text{sol}}(t) = F[\vec{S}(t)] \quad \text{WITH } -t_0 \leq t \leq t \quad (6)$$

AND HENCE ANY FUNCTIONAL OF $S_i(t)$, E.G. $F[\vec{S}](t)$ MUST BE AVERAGED OVER VARIOUS THERMAL HISTORIES TO OBTAIN A 'DETERMINISTIC' RESULT:

$$\langle F[\vec{S}](t) \rangle_s = \int_{-\infty}^t d\vec{s}(t) e^{-\int_0^t \frac{\dot{S}_i^2}{2\lambda}} F[\vec{S}_i^{\text{sol}}(t)] \quad (7)$$

IN THE SG PROBLEM WE STILL HAVE A DEPENDENCE UPON THE QUENCHED DISORDER J_{ij} TO TAKE INTO ACCOUNT. WE SHOULD ALSO TAKE THE AVERAGE OVER IT +

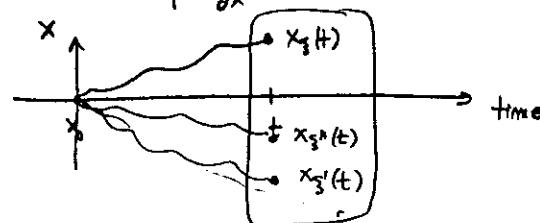
$$\langle F[\vec{S}](t) \rangle_s = \int_{\text{DIS}} d\vec{J} e^{-\int_0^t \frac{\dot{S}_i^2}{2\lambda}} F[\vec{S}_i^{\text{sol}}(t)] \quad (8)$$

THIS AVERAGE MEANS

WE SOLVE THE L-EQ FOR A $\{\vec{S}(t)\}$ & GET $\vec{S}_i^{\text{sol}}(t)$
 ANOTHER $\{\vec{S}(t)\}$ " $\vec{S}_i^{\text{sol}}(t)$
 ETC

EXAMPLE: JUST ONE VARIABLE

$$\dot{x} = -\lambda \frac{\partial V}{\partial x} + \xi \Rightarrow x_i^{\text{sol}}(t) = F[S](t)$$



AVERAGE OVER THESE VALUES.

CERTAINLY, ONE CAN FOLLOW THIS PROGRAM FOR THE SG-CASE & TRY TO FIND, E.G. DYN. EQS FOR $C_{ij} = \langle x_i x_j \rangle$ ETC. (SEE LECTURE IV).

OTHER WAY:

OBTAIN { DYNAMICAL EQS. FOR CORR. & RESPONSE FUNCTIONS

if $N \rightarrow \infty$: CLOSE THE HIERARCHY & ONLY THE CORR & RESPONSE* : $\{C(t), R(t)\}$ ENTER.

$\Rightarrow$ STUDY THE GENERAL PROPS OF $\{C, R\}$ TO USE THEM LATER

* TO BE DEF. LATER
 NOTATION
 HERE & IN THE REST OF LIT $\begin{cases} t' = t_w \\ t = t_f = (t_w + t) \end{cases}$
 0 $\xrightarrow{t'} t \xrightarrow{t}$ TIME

Fokker-Planck Eq

THE PROB. DIST OF $\vec{S}(t)$ INDUCES A TIME-DEP PROB. DIST OF $\vec{S}(t)$ THAT WE'LL CALL $P(\vec{s}, t)$. IF WE DEFINE *

$$P(\vec{s}, t) = \int dP[\vec{s}] \delta(\vec{s} - \vec{s}_s^{\text{sol}}(t)) \quad (9)$$

$$= \langle \delta(\vec{s} - \vec{s}_s^{\text{sol}}(t)) \rangle_s$$

THEN,

$$\langle F[\vec{s}](t) \rangle_s = \int d\vec{s} P(\vec{s}, t) F[\vec{s}] \quad (10)$$

ONE CAN SHOW, THAT $P(\vec{s}, t)$ SATISFIES THE FOKKER-PLANCK EQ:

$$\frac{\partial P(\vec{s}, t)}{\partial t} = - \vec{\nabla} \left[P(\vec{s}, t) \mu \frac{\partial H_J}{\partial \vec{s}} \right] + A \nabla^2 P(\vec{s}, t) \quad (11)$$

WITH $\vec{\nabla} = \frac{\partial}{\partial \vec{s}}$
 $\nabla^2 = \frac{\partial^2}{\partial s^2}$

*NB, $\int d\vec{s} P(\vec{s}, t) = \int d\vec{s} \int dP[\vec{s}] \delta(\vec{s} - \vec{s}_s^{\text{sol}}(t)) = \int dP[\vec{s}] = 1 \quad \forall t$

AND $P(\vec{s}, t) \geq 0 \quad \forall (\vec{s}, t)$

THE TIME-DEPENDENT PROB. DENSITY $P(\vec{s}, t)$ SHOULD APPROACH $P_{\text{GB}}(\vec{s})$ FOR LARGE TIMES, IF THE SYSTEM ARRIVES AT EQUILIBRIUM.

LET US CHECK WHEN

$\lim_{t \rightarrow \infty} P(\vec{s}, t) \stackrel{?}{=} P_{\text{GB}}(\vec{s})$ IS A LARGE-TIME SOL TO FPEQ.

(DEM)

$$0 \stackrel{?}{=} \vec{\nabla} \left[e^{-\beta H_J[\vec{s}]} \mu \frac{\partial H_J}{\partial \vec{s}} \right] + A \nabla^2 (e^{-\beta H_J[\vec{s}]})$$

$$- \beta \frac{\partial H_J[\vec{s}]}{\partial \vec{s}} \mu \frac{\partial H_J[\vec{s}]}{\partial \vec{s}} + \mu \frac{\partial^2 H_J[\vec{s}]}{\partial s^2} +$$

$$+ A \left[- \beta \frac{\partial^2 H_J[\vec{s}]}{\partial s^2} + \beta^2 \frac{\partial H_J[\vec{s}]}{\partial \vec{s}} \frac{\partial H_J[\vec{s}]}{\partial \vec{s}} \right] \stackrel{?}{=} 0$$

$$\beta (A\beta - \mu) \left(\frac{\partial H_J[\vec{s}]}{\partial \vec{s}} \right)^2 + (\mu - A\beta) \left(\frac{\partial^2 H_J[\vec{s}]}{\partial s^2} \right) \stackrel{?}{=} 0$$

$$(\mu - A\beta) \left\{ \frac{\partial^2 H_J[\vec{s}]}{\partial s^2} - \beta \left(\frac{\partial H_J[\vec{s}]}{\partial \vec{s}} \right)^2 \right\} \stackrel{?}{=} 0$$

$\forall \text{ AND } \forall \vec{s} \Rightarrow \mu = A\beta \Rightarrow A = \frac{\mu}{\beta} = \mu k_B T$

$A = \mu k_B T$ (12)

EINSTEIN'S RELATION OR 2ND FDT (KUBO)

Thus,

$$\text{L-EP} \quad \begin{cases} \dot{S}_i(t) = -\mu \frac{\delta H}{\delta S_i(t)} + S_i(t) \\ \langle S_i(t) S_j(t') \rangle = 2\mu k_B T \delta(t-t') \end{cases}$$

F-P EQ

$$\frac{\partial P(\vec{s}, t)}{\partial t} = -\vec{\nabla} \left[P(\vec{s}, t) \mu \frac{\partial H_I}{\partial \vec{s}} \right] + \mu k_B T \nabla^2 P(\vec{s}, t)$$

USING THE RELATION BETWEEN FP & THE SCHRÖDINGER EQ THAT WE'LL EXPLAIN BELOW ONE CAN SHOW THAT $P_{eq}(\vec{s})$

IS THE UNIQUE SOL TO $\frac{\partial P(\vec{s}, t)}{\partial t} = 0$.

THE FO-RELATION ($A = \mu k_B T$) EXPRESSES THE FACT THAT THE BATH IS AT EQUILIBRIUM AT $t=0$ AND STAYS AT EQUILIBRIUM AT ALL SUBSEQUENT TIMES.

Analogy WITH THE SCHRÖDINGER EQ = [Laid G]

$$\frac{\partial P(\vec{s}, t)}{\partial t} = -\vec{\nabla} \left[P(\vec{s}, t) \mu \left(\frac{\partial H_I}{\partial \vec{s}} \right) \right] + \mu k_B T \nabla^2 P(\vec{s}, t)$$

Let's identify $-i \frac{\partial}{\partial \vec{s}} = \hat{\vec{p}}$ $\leftrightarrow$ $\frac{\partial}{\partial \vec{s}} = i \hat{\vec{p}}$ $[\hat{\vec{p}}, \hat{\vec{s}}] = -i$

$P(\vec{s}, t) = |\phi(t)\rangle$

THIS IS IN THE SCHRÖDINGER'S REPRESENTATION WHERE STATES DEPEND UPON TIME BUT OPERATORS DON'T.

LET'S CALL $\frac{\partial H_I}{\partial \vec{s}} = -\vec{F}_I[\vec{s}]$ ($= -\frac{\partial V[\vec{s}]}{\partial \vec{s}}$) DETERMINISTIC VELOCITY

$$\frac{\partial P(\vec{s}, t)}{\partial t} = -\vec{\nabla} \left[P(\vec{s}, t) \mu \vec{F}_I[\vec{s}] \right] + \mu k_B T \nabla^2 P(\vec{s}, t)$$

$$\begin{aligned} \frac{\partial}{\partial t} |\phi(t)\rangle &= -i \hat{\vec{p}} \left[\mu \vec{F}_I[\vec{s}] |\phi(t)\rangle \right] + \mu k_B T (i \hat{\vec{p}})^2 |\phi(t)\rangle \\ &= -i \hat{\vec{p}} \left[\mu \vec{F}_I[\vec{s}] + \mu k_B T (-i \hat{\vec{p}}) \right] |\phi(t)\rangle \end{aligned}$$

$$\frac{\partial}{\partial t} |\phi(t)\rangle = -H_{FP}[\hat{\vec{p}}, \hat{\vec{s}}] |\phi(t)\rangle \quad (13)$$

$$H_{FP}[\hat{\vec{p}}, \hat{\vec{s}}] = -\hat{\vec{p}} \left[-i \mu \vec{F}_I[\vec{s}] - \mu k_B T \hat{\vec{p}} \right] \quad (14)$$

(IF THERE'S A FIELD, COUPLED TO $\vec{s}$)

$$H_{FP}[\hat{\vec{p}}, \hat{\vec{s}}] = -\hat{\vec{p}} \left[-i \mu \vec{F}_I[\vec{s}] - i \mu \hbar - \mu k_B T \hat{\vec{p}} \right]$$

$$\begin{aligned}
 [\hat{p}, B(\vec{s})] \phi &= -i \frac{\partial}{\partial \vec{s}} (B(\vec{s}) \phi) - B(\vec{s}) \left(-i \frac{\partial}{\partial \vec{s}} \phi \right) \\
 &= -i \left(\frac{\partial B}{\partial \vec{s}} \right) \phi - \cancel{i B(\vec{s}) \frac{\partial \phi}{\partial \vec{s}}} + \cancel{i B(\vec{s}) \frac{\partial \phi}{\partial \vec{s}}} \\
 &= -i \left(\frac{\partial B}{\partial \vec{s}} \right) \phi
 \end{aligned}$$

$$[\hat{p}, B(\vec{s})] = -i \frac{\partial B}{\partial \vec{s}}$$

$$[\hat{p}, B(\vec{s})] = \frac{\partial B}{\partial \vec{s}} \Rightarrow [B(\vec{s}), \hat{p}] = -\frac{\partial B}{\partial \vec{s}}$$

MEAN VALUES IN THIS NOTATION

$$\begin{aligned}
 \langle F(\vec{s})(t) \rangle &= \int \pi d\vec{s}(t) \cdot \underbrace{F(\vec{s})}_{\downarrow} \underbrace{P(\vec{s}, t)}_{\downarrow} \\
 &= \langle - | F(\hat{s}) | \phi(t) \rangle
 \end{aligned}$$

$$\langle F(\vec{s})(t) \rangle = \langle - | F(\hat{s}) | \phi(t) \rangle \quad (15)$$

Solution to eq FP-SCHROD:

$$|\phi(t)\rangle = e^{-H_{FP} \cdot t} |I_{wt}\rangle \quad (16)$$

(if H_{FP} is indep of t , ie if $H_F[\vec{s}]$ is indep of t ,
OTHERWISE, ONE HAS TO INCLUDE A TIME ORDER.)

$$\langle F(\vec{s})(t) \rangle = \langle - | F(\hat{s}) e^{-H_{FP} t} | I_{wt} \rangle$$

Taking $F(\vec{s}) = 1 \Rightarrow$ Eq. (15) implies

$$\begin{aligned}
 \langle 1 \rangle &= 1 = \langle - | \phi(t) \rangle \quad (\text{NORMALIZATION}) \quad (17) \\
 &= \int \pi d\vec{s}(t) P(\vec{s}, t) = 1
 \end{aligned}$$

CORRELATION FUNCTIONS

$$\langle A(t) B(t') \rangle$$

$$t > t' \geq t_0$$

$$= \langle - | A e^{-H_{FP}(t-t')} B e^{-H_{FP}t'} | I_{int} \rangle$$

IN PARTICULAR $A \Rightarrow S_i(t)$
 $B \Rightarrow S_i(t')$

$$\langle S_i(t) S_i(t') \rangle = \langle - | S_i e^{-H_{FP}(t-t')} S_i e^{-H_{FP}t'} | I_{int} \rangle$$

• IF $|I_{int}\rangle = |E_\phi\rangle \Rightarrow H_{FP}|I_{int}\rangle = H_{FP}|E_\phi\rangle = 0$
 $\Rightarrow e^{-H_{FP}t'}|E_\phi\rangle = |E_\phi\rangle$

$$\langle A(t) B(t') \rangle = \langle - | A e^{-H_{FP}(t-t')} B | E_\phi \rangle = f(t-t') \quad (18)$$

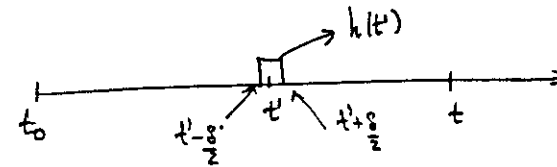
AND π HOLDS

• IF AT $t' > t'' \geq t_0$: $|\phi(t'')\rangle = |E_\phi\rangle$ (ie EVEN STARTING FROM Δ $|I_{int}\rangle \neq |E_\phi\rangle$ IF WE CAN ASSUME THAT AT t'' EQ IS ESTABLISHED) THEN,

$$\langle A(t) B(t') \rangle = f(t-t') \quad (19)$$

THUS, TIME-TRANSLATION INVARIANCE (π) IS A DIRECT CONSEQUENCE OF $|\phi(t'')\rangle = |E_\phi\rangle \quad \forall$ OPERATORS A, B.

RESPONSE FUNCTION



TIME

$$R(t, t') = \left. \frac{\delta \langle A(t) \rangle}{\delta h(t')} \right|_{h=0}$$

ASSUMING $t > t'$

$$\langle A(t) \rangle = \langle - | A e^{-H_{FP}t} | I_{int} \rangle$$

$$\langle A(t) \rangle_{h(t')} = \langle - | A e^{-H_{FP}(t-(t'+\frac{\delta}{2}))} e^{-H_{FP}[(t'+\frac{\delta}{2})-(t'-\frac{\delta}{2})]} e^{-H_{FP}(t'-\frac{\delta}{2})} | I_{int} \rangle$$

$$= \langle - | A e^{-H_{FP}[t-t'-\frac{\delta}{2}]} e^{-H_{FP}\delta} e^{-H_{FP}(t'-\frac{\delta}{2})} | I_{int} \rangle$$

$$\left. \frac{\delta \langle A(t) \rangle}{\delta h(t')} \right|_{h=0} = \langle - | A e^{-H_{FP}[t-t'-\frac{\delta}{2}]} \left(-\frac{\delta H_{FP}}{\delta h} \right) e^{-H_{FP}\delta} e^{-H_{FP}(t'-\frac{\delta}{2})} | I_{int} \rangle$$

WHAT'S $\left. \frac{\delta H_{FP}}{\delta h} \right|_{h=0}$?

USING

$$+\frac{\delta H_{FP}}{\delta h} = i\mu \hat{p} \quad \text{AND TAKING } \delta \rightarrow 0.$$

$$\left. \frac{\delta \langle A(t) \rangle}{\delta h(t')} \right|_{h=0, \delta=0} = \langle - | A e^{-H_{FP}(t-t')} (i\mu \hat{p}) e^{-H_{FP}t'} | I_{int} \rangle \quad (20)$$

$$R(t, t') = \left. \frac{\delta \langle A(t) \rangle}{\delta h(t')} \right|_{h=0} = \langle - | A e^{-H_{FP}(t-t')} (i\mu \hat{p}) e^{-H_{FP}t'} | \text{Init} \rangle$$

Causality

$$\boxed{\text{IF } t < t'}$$

$$R(t, t') = \langle - | i\mu \hat{p} e^{-H_{FP}(t-t')} A e^{-H_{FP}t'} | \text{Init} \rangle$$

But $\langle - | \hat{p} = 0$ (it's a total derivative in the integral version)

$$\boxed{R(t, t') = 0 \text{ if } t < t'}$$

RESPONSE OF A(t) TO A KICK AT (t')

$$H_J[\vec{s}] \rightarrow H_J[\vec{s}] + h \cdot B[\vec{s}]$$

$$H_{FP}[\hat{p}, \hat{s}] \rightarrow H_{FP}[\hat{p}, \hat{s}] + i\mu \hat{p} \frac{\partial B[\vec{s}]}{\partial \vec{s}} \cdot h$$

$$\frac{\delta H_{FP}}{\delta h} \rightarrow i\mu \hat{p} \frac{\partial B[\vec{s}]}{\partial \vec{s}}$$

Thus,

$$R_{AB}(t, t') = \left. \frac{\delta \langle A(t) \rangle}{\delta h(t')} \right|_{h=0}$$

$$R_{AB}(t, t') = \langle - | A e^{-H_{FP}(t-t')} \left(i\mu \hat{p} \frac{\partial B[\vec{s}]}{\partial \vec{s}} \right) e^{-H_{FP}t'} | \text{Init} \rangle \quad (21)$$

EQUILIBRIUM:

IF $| \text{Init} \rangle = | E_0 \rangle \rightarrow$

$$R_{AB}(t, t') = \chi(t-t')$$

RESPONSE AT = TIMES

$$R_{AB}(t, t^-) = \langle - | A i\mu \hat{p} \frac{\partial B[\vec{s}]}{\partial \vec{s}} e^{-H_{FP}t'} | \text{Init} \rangle$$

$$= -\mu \langle - | [A, i\hat{p}] \frac{\partial B[\vec{s}]}{\partial \vec{s}} | \phi(t') \rangle$$

$$= +\mu \langle - | \frac{\partial A}{\partial \vec{s}} \frac{\partial B}{\partial \vec{s}} | \phi(t') \rangle$$

$$[A, i\hat{p}] = -i[\vec{p}, A] = -i(-i) \frac{\partial A}{\partial \vec{s}} = -\frac{\partial A}{\partial \vec{s}}$$

if $\begin{cases} A = s_i \\ B = s_i \end{cases} \Rightarrow \begin{aligned} \frac{\partial A}{\partial s_k} &= \delta_{ik} \\ \frac{\partial B}{\partial s_k} &= \delta_{ik} \end{aligned}$

$$\boxed{R_{ii}(t, t^-) = +\mu \langle - | \phi(t') \rangle = +\mu}$$

FOR OF THE 1st kind

R vs. C

$t > t'$

$$\begin{aligned} \frac{\partial C_{AB}(t, t')}{\partial t'} &= \frac{\partial}{\partial t'} \langle -1 A e^{-H_{FP}(t-t')} B e^{-H_{FP}t'} | \text{In} \rangle \\ &= \langle -1 A e^{-H_{FP}(t-t')} [H_{FP}, B] e^{-H_{FP}t'} | \text{In} \rangle \end{aligned}$$

What's $[H_{FP}, B]$?

$$\begin{aligned} [H_{FP}, B] &= -\left[\hat{p} \left(-i\mu \vec{F}_j[\vec{x}] - \mu h_0 T \hat{p} \right), B(\vec{x}) \right] \\ &= -[\hat{p}, B] \left(-i\mu \vec{F}_j[\vec{x}] - \mu h_0 T \hat{p} \right) \\ &\quad + (-\hat{p}) \left[-i\mu \vec{F}_j[\vec{x}] - \mu h_0 T \hat{p}, B(\vec{x}) \right] \end{aligned}$$

(SINCE $B = B[\vec{x}]$).

$$\begin{aligned} &= +i \frac{\partial B}{\partial \vec{x}} \left(-i\mu \vec{F}_j[\vec{x}] - \mu h_0 T \hat{p} \right) \\ &\quad + \hat{p} (+\mu h_0 T) \left(-i \frac{\partial B}{\partial \vec{x}} \right) \end{aligned}$$

$$= +i \frac{\partial B}{\partial \vec{x}} \left(-i\mu \vec{F}_j[\vec{x}] - \mu h_0 T \hat{p} \right) + \mu h_0 T \hat{p} \left(-i \frac{\partial B}{\partial \vec{x}} \right)$$

(22)

Thus,

$$\begin{aligned} \frac{\partial C_{AB}(t, t')}{\partial t'} &= \langle -1 A e^{-H_{FP}(t-t')} \left\{ +i \frac{\partial B}{\partial \vec{x}} \left(-i\mu \vec{F}_j[\vec{x}] - \mu h_0 T \hat{p} \right) \right. \right. \\ &\quad \left. \left. + \mu h_0 T \hat{p} \left(-i \frac{\partial B}{\partial \vec{x}} \right) \right\} e^{-H_{FP}t'} | \text{In} \right\rangle \end{aligned} \quad (23)$$

if $| \text{In} \rangle = | E_q \rangle \rightarrow e^{-H_{FP}t'} | E_q \rangle = | E_q \rangle$

AND $(-i\mu \vec{F}_j[\vec{x}] - \mu h_0 T \hat{p}) | E_q \rangle = 0$. AND THE 1st TERM

Vanishes.

$$\begin{aligned} \frac{\partial C_{AB}(t, t')}{\partial t'} &= -\langle -1 A e^{-H_{FP}(t-t')} \mu h_0 T \hat{p} \left(\frac{\partial B}{\partial \vec{x}} \right) | E_q \rangle \\ &= f(t, t') \end{aligned}$$

THE RESPONSE IS (FROM EQ. (21))

$$R_{AB}(t, t') = \langle -1 A e^{-H_{FP}(t-t')} i\mu \hat{p} \frac{\partial B}{\partial \vec{x}} | E_q \rangle$$

COMPARING WE HAVE

$$\begin{aligned} R_{AB}(t, t') &= \frac{1}{h_0 T} \frac{\partial C_{AB}(t, t')}{\partial t'} \quad \text{or,} \\ R_{AB}(t, t') &= \frac{1}{h_0 T} \frac{\partial C_{AB}(t, t')}{\partial t'} \end{aligned} \quad (24)$$

FOR OF THE 1st kind

Thus, if $| \text{In} \rangle = | E_q \rangle$, OR EVEN IF $| \phi(t') \rangle = | E_q \rangle$ FOR $t' < t$, THEN FDT FOR THE SYSTEM HOLDS.

WHAT HAPPENS OUT OF EQUILIBRIUM?

A SIMPLER WAY OF GETTING THE LAST RESULT IS THE FOLLOWING:

THAT ALLOWS US TO OBTAIN GENERALIZATIONS.

LET US COMPUTE:

$$V_{AB}(t, t') \equiv k_B T R_{AB}(t, t') - \frac{\partial C_{AB}(t, t')}{\partial t'}$$

$$= \langle - | A e^{-H_F(t-t')} \left[k_B T i \hat{p} \frac{\partial B}{\partial \vec{s}} + i \frac{\partial B}{\partial \vec{s}} (-\mu \vec{F}_S[\vec{s}] - \mu k_B T \hat{p}) - k_B T i \hat{p} \frac{\partial B}{\partial \vec{s}} \right] e^{-H_F t'} | \text{init} \rangle$$

$$= \langle - | A e^{-H_F(t-t')} \frac{\partial B}{\partial \vec{s}} \left(\mu \vec{F}_S[\vec{s}] - \mu k_B T \hat{p} \right) | \phi(t') \rangle \quad (25)$$

• If $|\phi(t')\rangle = |E_F\rangle \Rightarrow V_{AB}(t, t') = 0$ SINCE $(\quad) |E_F\rangle = 0$.

• If $|\phi(t')\rangle \neq |E_F\rangle$?

WE'LL TRY TO FIND A BOUND TO THE

FDT VIOLATION.

CDK COND-MAT / 9705002

DISCUSSION ON (N vs. t) LIMITS

— IF N is finite AND $t \rightarrow \infty \Rightarrow$ EQUIL WILL BE EVENTUALLY ACHIEVED.

— IF N IS VERY LARGE ($\approx 10^{23}$) AND t' IS LARGE BUT SMALL WRT $t_{eq} = f(N)$

$$t' < t_{eq}$$

THUS, THE RELEVANT ORDER OF LIMITS, TO OBTAIN ASYMPTOTIC RESULTS IS

$$\lim_{t' \rightarrow \infty} \lim_{N \rightarrow \infty}$$

[TYPICALLY, FOR HFSG ONE EXPECTS $t_{eq} \sim O(e^N)$.]

IN THIS SITUATION THE SYSTEM IS OUT OF EQ AT $\frac{t'}{t} < \frac{t}{t_{eq}}$ AND FDT CAN BE VIOLATED.

NB. THE THERMODYN. LIMIT IS DETERMINANT TO HAVE SUCH A SITUATION!

WE'LL STUDY WHEN WE CAN HAVE FDT-VIOLATIONS

OUR AIM IS TO BOUND $|V_{AB}(t)|$

LET US FIRST CHOOSE A AND B, FOR THE SAKE OF CLARITY, TO BE

$$\begin{cases} A(t) = s_i(t) \\ B(t) = s_i(t) \end{cases} \Rightarrow |V(t)| = \left| \frac{1}{N} \sum_i V_{ii}(t) \right|$$

IT IS GOING TO BE IMPORTANT, AT LEAST UP TO WHERE WE CAN SHOW THINGS - THAT $A(t)$ DEPENDS ON A FINITE # OF DYN. VARIABLES TO GET A SHARP BOUND.

LET'S NOW GO BACK TO THE FUNCTION NOTATION:

$$\begin{aligned} |V(t,t)| &\leq \frac{1}{N} \sum_i |V_{ii}(t,t)| \\ &= \frac{1}{N} \sum_i \left| \int d\vec{s} \int d\vec{s}' s_i P(\vec{s}, \vec{s}'; t-t') \left[-\mu \frac{\partial H}{\partial s_i} - \mu k_B T \frac{\partial}{\partial s_i} \right] \right. \\ &\quad \left. P(\vec{s}', t') \right| \\ &= \frac{1}{N} \sum_i \left| \int d\vec{s} \int d\vec{s}' s_i P^{\frac{1}{2}}(\vec{s}, \vec{s}'; t-t') P^{\frac{1}{2}}(\vec{s}', t') \right. \\ &\quad \left. \frac{\left[-\frac{\partial H}{\partial s_i} - k_B T \frac{\partial}{\partial s_i} \right] P(\vec{s}', t')}{P^{\frac{1}{2}}(\vec{s}', t')} \right| \end{aligned}$$

or (18)

$$\leq \frac{1}{N} \sum_i \left[\int d\vec{s} \int d\vec{s}' s_i^2 P(\vec{s}, \vec{s}'; t-t') P(\vec{s}', t') \right]^{\frac{1}{2}} \quad \text{or (19)}$$

$$\left[\int d\vec{s} \int d\vec{s}' P(\vec{s}, \vec{s}'; t-t') \left(\left[-\frac{\partial H}{\partial s_i} - k_B T \frac{\partial}{\partial s_i} \right] \frac{P(\vec{s}', t')}{P(\vec{s}', t')} \right)^2 \right]^{\frac{1}{2}}$$

$$= \frac{1}{N} \sum_i \langle s_i^2(t) \rangle^{\frac{1}{2}} \left[\int d\vec{s}' \frac{\left(\left[-\frac{\partial H}{\partial s_i} - k_B T \frac{\partial}{\partial s_i} \right] P(\vec{s}', t') \right)^2}{P(\vec{s}', t')} \right]^{\frac{1}{2}}$$

$$\leq \left(\frac{1}{N} \sum_i \langle s_i^2(t) \rangle \right)^{\frac{1}{2}} \left[\frac{1}{N} \sum_i \int d\vec{s}' \frac{\left(\left[-\frac{\partial H}{\partial s_i} - k_B T \frac{\partial}{\partial s_i} \right] P(\vec{s}', t') \right)^2}{P(\vec{s}', t')} \right]^{\frac{1}{2}}$$

$$= \sqrt{C(t,t)} \cdot \sqrt{-\frac{d\mathcal{H}(t')}{dt'}}$$

$$\boxed{|V(t,t)| \leq \sqrt{C(t,t)} \sqrt{-\frac{d\mathcal{H}(t')}{dt'}}$$

ENTROPY PRODUCTION PER SPIN

$$O(1) \leq O(1) \cdot O(1) \quad \underline{O(1)}$$

THE THERMODYN. LIMIT YIELDS A NON-TRIVIAL BOUND.

How do I know that

$$\frac{1}{N} \sum_i \int d\vec{s}' \frac{\left[\left(-\mu \frac{\partial H}{\partial s'_i} - \mu k_B T \frac{\partial}{\partial s'_i} \right) P(\vec{s}', t') \right]^2}{P(\vec{s}', t')}$$

is the entropy production?

Let's define:

$$\dot{H}_b(t) = \mu \int d\vec{s} \quad P(\vec{s}, t) \left[k_B T \ln P(\vec{s}, t) + H_J[\vec{s}] \right]$$

$$\dot{H}_b(t) = \mu \int d\vec{s} \left\{ \dot{P}(\vec{s}, t) \left[k_B T \ln P(\vec{s}, t) + H_J[\vec{s}] \right] + \mu k_B T \cancel{P(\vec{s}, t)} \frac{1}{\cancel{P(\vec{s}, t)}} \dot{P}(\vec{s}, t) \right\}$$

$$= \mu \int d\vec{s} \nabla \left\{ \left[P(\vec{s}, t) \mu \frac{\partial H_J}{\partial \vec{s}} \right] + \mu k_B T \nabla P(\vec{s}, t) \right\} \left(k_B T \ln P(\vec{s}, t) + H_J[\vec{s}] \right)$$

$$= -\mu \int d\vec{s} \left\{ P(\vec{s}, t) \frac{\partial H_J}{\partial \vec{s}} + k_B T \nabla P(\vec{s}, t) \right\} \left(\frac{k_B T \nabla P(\vec{s}, t) + \frac{\partial H_J[\vec{s}]}{\partial \vec{s}}}{P(\vec{s}, t)} \right)$$

$$\dot{H}_b(t) = - \int d\vec{s} \frac{\left(\mu k_B T \nabla P(\vec{s}, t) + \mu P(\vec{s}, t) \frac{\partial H_J}{\partial \vec{s}} \right)^2}{P(\vec{s}, t)} \leq 0$$

Thus, the rhs in the inequality is

$$|V(t, t')| \leq \sqrt{C(t, t')} \sqrt{-\mu \frac{dH_b(t')}{dt'}}$$

(μ -factor)

$$\leq K \cdot \sqrt{-\mu \frac{dH_b(t')}{dt'}}$$

• If the system is at equilibrium $\Rightarrow$

$$\frac{dH_b(t')}{dt'} = 0$$

And rhs = 0 $\Rightarrow$

$$\boxed{|V(t, t')| \leq 0} \Rightarrow \left| \underbrace{k_B T R(t, t')}_{\text{Positive}} - \underbrace{\frac{\partial C(t, t')}{\partial t'}}_{\text{Positive}} \right| = 0 \Rightarrow$$

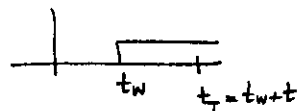
If the diff. doesn't change signs $\Rightarrow$

FDT holds

• If $\frac{d^2\phi(t')}{dt'^2} \sim$ is a DECREASING FUNCTION OF t'

WHAT HAPPENS?

REM THE EXPERIMENTS



$$h \cdot \int_{t_w}^{t_r} dt R(t, \tau) \equiv m(t, t_w) : \text{FINITE}$$

AND $C(t+t_w, t_w)$ FROM NUMERICS.

$$\frac{\partial C(t_r, t_w)}{\partial t_w} \geq 0, \quad \frac{\partial C(t_r, t_w)}{\partial t_r} \leq 0 \quad (\text{SLOWER AND SLOWER})$$

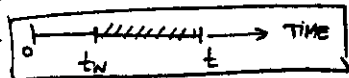
Thus,

$$|V(t, t')| = \left| k_B T R(t, t') - \frac{\partial C(t, t')}{\partial t'} \right| \leq K \sqrt{-\frac{d^2\phi(t')}{dt'^2}}$$

BUT $\frac{\partial C(t, t')}{\partial t'} \rightarrow 0$ AND $R(t, t') \rightarrow 0$ TOO!

Thus, it's NOT TELLING US MUCH...

BOTH SIDES ARE POSITIVE DEFINITE $\Rightarrow$ INTEGRATE THEM OVER AN INTERVAL



$$\int_{t_w}^t dt' |V(t, t')| = \int_{t_w}^t dt' \left| k_B T R(t, t') - \frac{\partial C(t, t')}{\partial t'} \right| \leq K \cdot \int_{t_w}^t dt' \sqrt{-\frac{d^2\phi(t')}{dt'^2}}$$

LI (2)

$$\left| \int_{t_w}^t dt' \left(k_B T R(t, t') - \frac{\partial C(t, t')}{\partial t'} \right) \right| \leq \int_{t_w}^t dt' \left| \dots \right| \leq K \cdot \int_{t_w}^t dt' \sqrt{-\frac{d^2\phi(t')}{dt'^2}} \quad \text{LI (23)}$$

$$|I| \equiv \left| k_B T m(t, t_w) - C(t, t) + C(t, t_w) \right| \leq K \int_{t_w}^t dt' \sqrt{-\frac{d^2\phi(t')}{dt'^2}}$$

STRONGER (INTEGRAL) BOUND

LET'S CHECK SOME EXAMPLES:

⊕ IF $\phi(t') = \phi_{\infty} + c t'^{-1}$ (or Slower)

$$\ddot{\phi}(t') = -c t'^{-2}$$

$$K \int_{t_w}^t dt' \sqrt{-c t'^{-2}} = K \sqrt{c} \cdot \ln(t/t_w) \rightarrow$$

rhs is finite and

$$\lim_{\substack{t \rightarrow \infty \\ t_w \text{ fixed}}} \text{rhs}(t, t_w) = \infty$$

FDT VIOL. ALLOWED

lhs Can be finite and there can be FDT Violations

⊕ IF $\phi(t) = \phi_{\infty} + c t^{1-\alpha}$ $\alpha > 1$

$$\text{rhs} = \frac{K \sqrt{\mu c}}{1-\alpha/2} \left(t^{1-\alpha/2} - t_w^{1-\alpha/2} \right) \rightarrow 0.$$

NO FDT VIOLATION ALLOWED

$\rightarrow$ **FDT VIOLATIONS ARE ALLOWED $\forall$ SLOWER THAN t^{-1} DECAY OF $\phi(t)$**

REMINDER OF TIME-SCALES & FDT VIOLATIONS

LI (2)

Entropy - arguments. WE'VE SHOWN BEFORE (IN COMPLETE GENERALITY)

$$\left| k_B T R_H(t) - \frac{\partial}{\partial t} C_H(t) \right| \leq K \sqrt{-\dot{H}(t)} \rightarrow$$

$$\left| k_B T \int_{t_W}^t ds R_H(s) - \frac{C(t)}{1} + C(t_W) \right| \leq K \int_{t_W}^t ds \sqrt{-\dot{H}(s)}$$

$$\left| k_B T M(t, t_W) - 1 + C(t, t_W) \right| \leq K \int_{t_W}^t ds \sqrt{-\dot{H}(s)}$$

Example

if $H(s) = H_\infty + c s^{-\alpha}$

$\dot{H}(s) = -\alpha c s^{-(\alpha+1)}$

$$\left| k_B T M(t, t_W) - (1 - C(t, t_W)) \right| \leq K \sqrt{\alpha c} \int_{t_W}^t ds s^{-\frac{\alpha+1}{2}}$$

$$\leq \frac{K \sqrt{\alpha c}}{\frac{1-\alpha}{2}} \left(t^{\frac{1-\alpha}{2}} - t_W^{\frac{1-\alpha}{2}} \right)$$

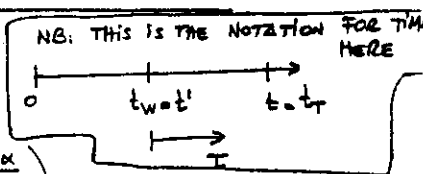
if $\alpha < 1$

FDT VIOLATION IS ALLOWED!

But if $t = t_W + \tau$

$$r_{HS} = K' \left((t_W + \tau)^{\frac{1-\alpha}{2}} - t_W^{\frac{1-\alpha}{2}} \right)$$

$$= K' t_W^{\frac{1-\alpha}{2}} \left[\left(1 + \frac{\tau}{t_W} \right)^{\frac{1-\alpha}{2}} - 1 \right]$$



$$\sim K' t_W^{\frac{1-\alpha}{2}} \left[1 + \left(\frac{\tau}{t_W} \right)^{\frac{1-\alpha}{2}} - 1 \right] \quad \text{if } \tau \ll t_W$$

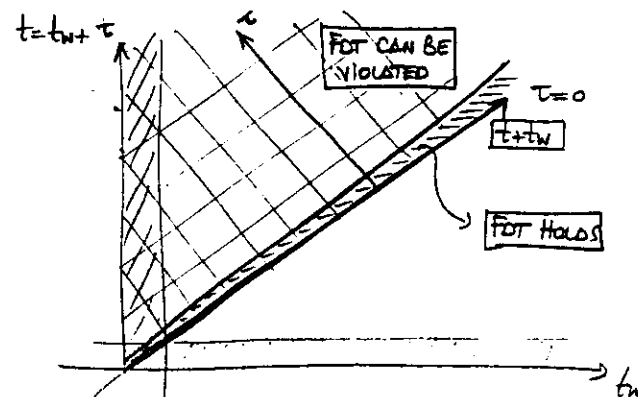
$$= K' \left(\frac{\tau}{t_W^{\frac{\alpha+1}{2}}} \right)$$

NOW, $\alpha < 1$ IN ORDER TO HAVE THE POSSIBILITY OF FDT VIOLATIONS.

IF $\tau \sim t_W^a \rightarrow r_{HS} \sim t_W^{a - \frac{\alpha+1}{2}}$

$$\begin{cases} a < \frac{\alpha+1}{2} \Rightarrow r_{HS} \rightarrow 0 & \text{FDT HOLDS} \\ a = \frac{\alpha+1}{2} \Rightarrow r_{HS} = \text{FINITE} & \text{FDT CAN BE VIOL.} \\ a > \frac{\alpha+1}{2} \Rightarrow r_{HS} \rightarrow \infty & \text{"} \end{cases}$$

THIS BOUND DETERMINES WHERE IN THE TWO TIMES SECTOR FDT MUST HOLD.



IF $\tau \sim t_W^a$
WITH $a = \frac{\alpha+1}{2}$
 $\Rightarrow$ 1st TIME
FDT IS VIOL

ANOTHER WAY TO WRITE IT:

$$C_T = t^{\frac{1-\alpha}{2}} - t^{\frac{1-\alpha}{2}} = -\ln \exp t^{\frac{1-\alpha}{2}} + \ln \exp t^{\frac{1-\alpha}{2}}$$

$$C_T = -\ln \left[\frac{\exp t^{\frac{1-\alpha}{2}}}{\exp t^{\frac{1-\alpha}{2}}} \right]$$

IN (L.III) WE SHOW WHY IT IS RELEVANT TO WRITE IT
IN THIS WAY.

THE FDT - VIOLATION

PHENOMENOLOGY.

INTERPRETATION

THE CORR FUNCTIONS $\rightarrow$ CORR SCALES.

J. Phys. A27, 5749 (94) - PRE (MANS 97) 55, 3898 (97)

- SYSTEMS WITH τ_{eq} finite
- SYSTEMS WITH $\tau_{eq} \rightarrow \infty$

- DOMAIN GROWTH $\tau_{eq}(L) \xrightarrow{L \rightarrow \infty} \infty$

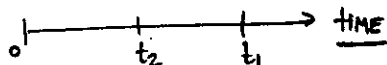
- MF SG $\tau_{eq}(N) \xrightarrow{N \rightarrow \infty} \infty$

- FINITE D SG $\rightarrow ?$

$$X(t_1, t_2)$$

$$t_2 \leq t_1$$

III (2)



IF THERE CAN BE FDT VIOLATIONS, HOW ARE THEY?

$$R(t_1, t_2) = \frac{\tilde{X}(t_1, t_2)}{T} \frac{\partial C(t_1, t_2)}{\partial t_2} \quad \text{GRAL. (DEFINED } \tilde{X}(t_1, t_2) \text{)}$$

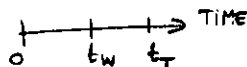
$C(t_1, t_2)$ IS MONOTONOUS WRT t_2 AND $t_1 \Rightarrow$

FROM $C = C(t_1, t_2)$ WE CAN OBTAIN:

$$t_2 = f[C, t_1] \quad (\text{WITHOUT ANY ASSUMPTION})$$

$$TR(t_1, t_2) = \tilde{X}[C(t_1, t_2), t_1] \cdot \frac{\partial C(t_1, t_2)}{\partial t_2}$$

$$m^{TRM}(t_f, t_w) = h \cdot \int_{t_w}^{t_f=t_r} dt' R(t_f, t')$$



$$= \frac{h}{T} \int_{t_w}^{t_r} dt' \tilde{X}[C(t_f, t'), t_r] \frac{\partial C(t_f, t')}{\partial t'}$$

SUGGESTS TO TAKE $C(t_f, t')$ AS AN INTEGRATION VARIABLE.

$$\lim_{t_w \rightarrow \infty} m^{TRM}(t_f, t_w) = \frac{h}{T} \lim_{t_w \rightarrow \infty} \int_{t_w}^{t_f} dt' \tilde{X}[C(t_f, t'), t_f] \frac{\partial C(t_f, t')}{\partial t'} = \int_0^1 dc' \tilde{X}[c', t_f] = 1$$

$\lim_{t_f \rightarrow \infty} C(t_f, t_w) = C$ $\lim_{t_f \rightarrow \infty} C(t_f, t_f) = C$ $C(t_f, t_w) = C$

$$m(C) = \frac{h}{T} \int_C^1 dc' \left(\lim_{t_f \rightarrow \infty} \tilde{X}[c', t_f] \right) \Rightarrow$$

IF THIS LIMIT $\exists \Rightarrow$

$$X[C] \equiv \lim_{t_f \rightarrow \infty} \tilde{X}[c', t_f]$$

EQUIVALENT TO SAYING

$$\lim_{t_2 \rightarrow \infty} \tilde{X}[C(t_1, t_2), t_2] = X[C] \quad (2)$$

$t_f / C(t_f, t_2) = C$

$\frac{X[C]}{T}$ IS GOING TO BE $\neq \frac{1}{k_B T}$ IN GLASSY SYSTEMS.

FOR DEFINITE MODELS ONE CAN MAKE DEFINITE PREDICTIONS FOR $\frac{X[C]}{T}$

ONE CAN ALSO WRITE (2) ABOVE AS

$$\lim_{t_2 \rightarrow \infty} \tilde{X}[C(t_1, t_2), t_2] = X[C] = \lim_{t_2 \rightarrow \infty} \left(\frac{R(t_1, t_2)}{\partial_{t_2} C(t_1, t_2)} \right) \quad (3)$$

$t_f / C(t_f, t_2) = C$

AND (1) TOGETHER WITH (1) $\Rightarrow$

$$\frac{m(C)}{h} = \frac{1}{T} \int_C^1 dc' X[c'] \quad \forall C, 0 \leq C \leq 1$$

BACK TO:

$$R(t_1, t_2) = \frac{\tilde{X}(t_1, t_2)}{T} \frac{\partial C(t_1, t_2)}{\partial t_2} \quad \text{DEFINES } \tilde{X}(t_1, t_2)$$

CASES:

* NOTE THAT, FOR ANY SYSTEM, IF t_2 IS SMALL

$$\tilde{X}(t_1, t_2) \neq \frac{1}{T}$$

EVEN FOR THE HARMONIC OSCILLATOR, IF WE LOOK AT FINITE TIMES (IE t_2 FINITE $< T_{eq}$) $\Rightarrow$ THERE WILL BE A FDT VIOLATION.

* FOR A SYSTEM SUCH THAT T_{eq} IS FINITE, IF $t_2 \gg T_{eq}$, $t_1 = t_2 + \tau$ WITH τ ANYTHING

$$\frac{\tilde{X}(t_1, t_2)}{T} = \frac{1}{T}$$

WE WANT TO STUDY THE BEHAVIOUR OF $\frac{\tilde{X}(t_1, t_2)}{T}$ WHEN $t_2 \rightarrow \infty$ AND $t_1 = t_2 + \tau$ MOVES $-(t_2 \leq t_1 < T_{eq})$. IN THIS

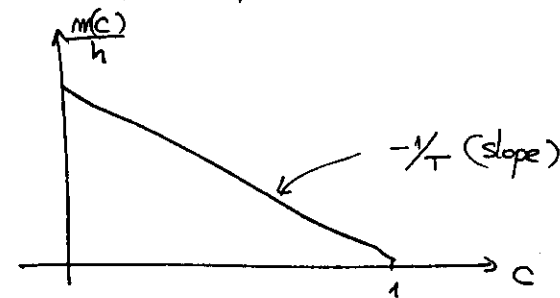
LIMIT, IF THE LIMITS ABOVE $\exists$ THIS IS EQUIV. TO STUDYING

$$\frac{m(c)}{h} = \frac{1}{T} \int_c^1 dc' \times [c']$$

AS A FUNCTION OF C (FOR LARGE TIMES, ONCE THE SYST. IS IN THE ASYMPTOTIC REGIME).

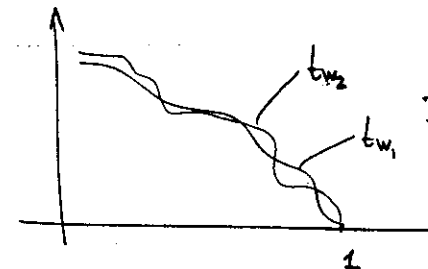
* IF

$$t_w \gg T_{eq}$$



* IF

$$t_w \text{ finite} \ll T_{eq}$$

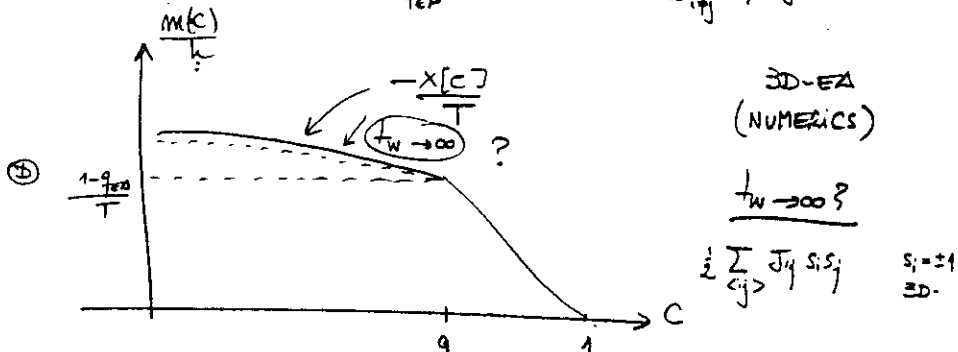
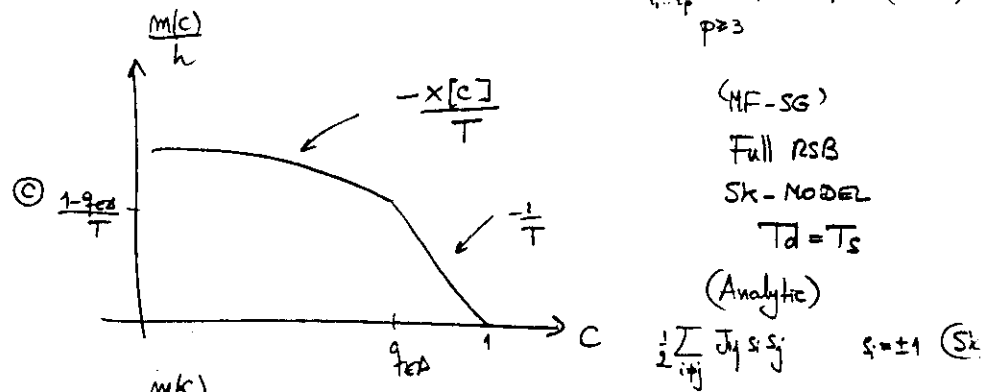
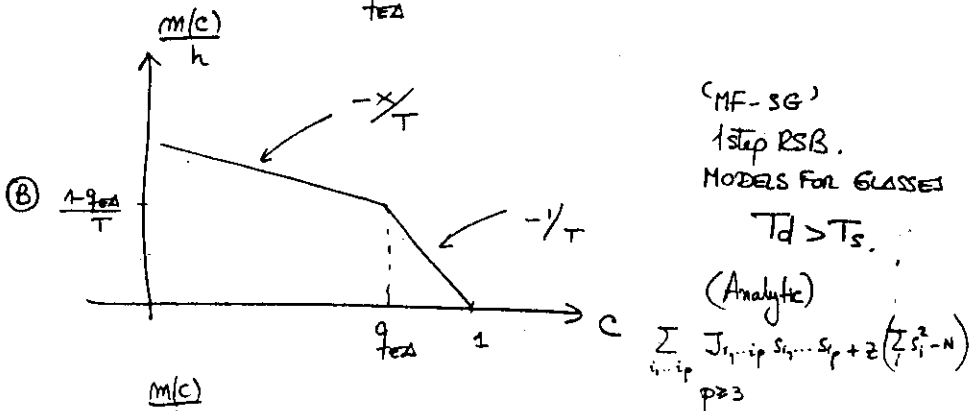
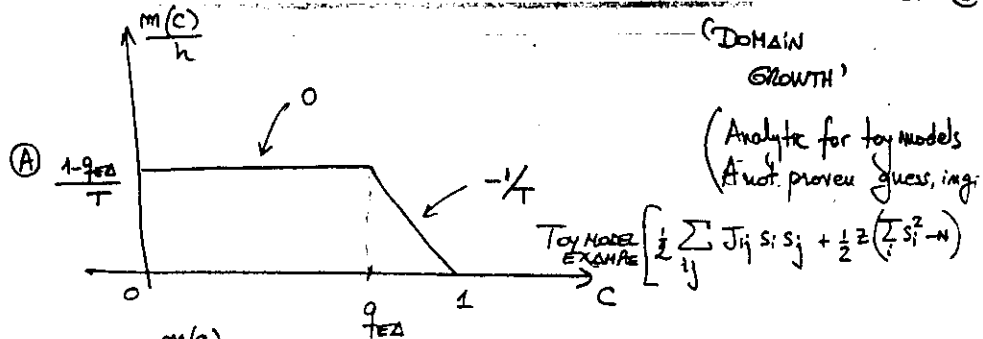


I DON'T KNOW. (PRE-ASYMPTOTIC REGIME)

* IF

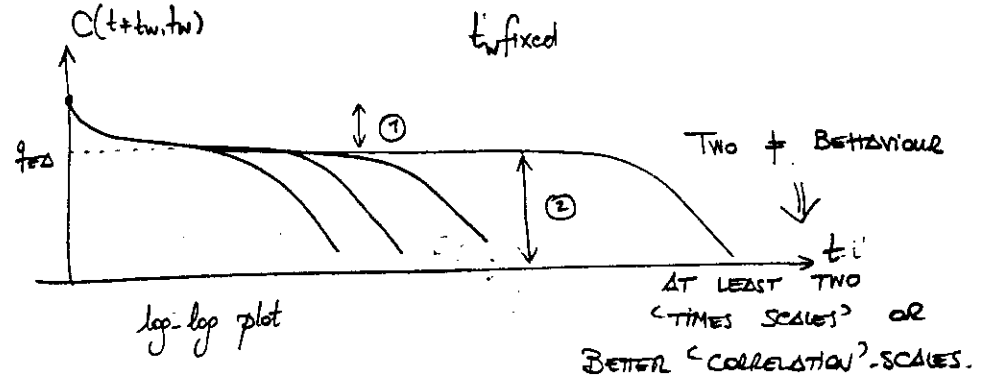
$$t_w \rightarrow \infty \ll T_{eq}$$

WE HAVE OBSERVED THREE POSSIBILITIES. (FOR SYSTEMS WITH $0 \leq c \leq 1$):



IN ALL THESE CASES THERE'S A RANGE OF VALUES OF THE CORRELATIONS SUCH THAT FDT HOLDS $C \in [q_{EA}(T), 1]$ AND A RANGE WHERE IT DOESN'T. $C \in [0, q_{EA}]$.

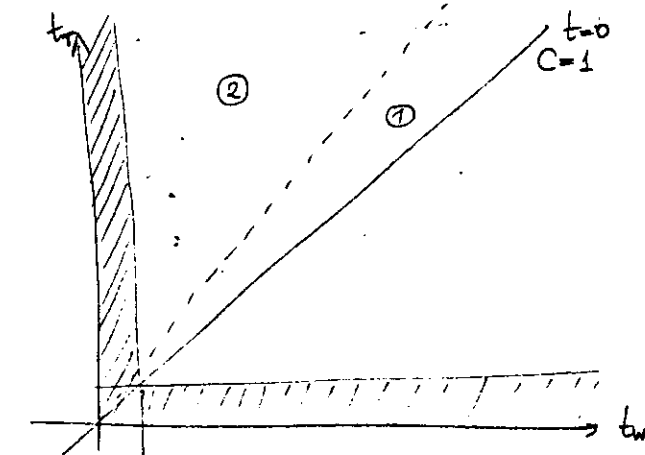
LET'S REMEMBER THE BEHAVIOUR OF $C(t+t_w, t_w)$ WITH TIMES.



①: FDT - STATIONARY TIMES SECTION $\rightarrow$ Like Equilibrium!

②: AGING - NON-STATIONARY " " $\rightarrow$ Non equilibrium.

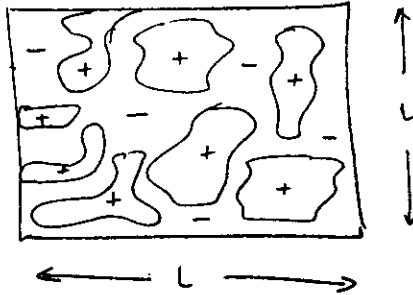
$t \geq 0$



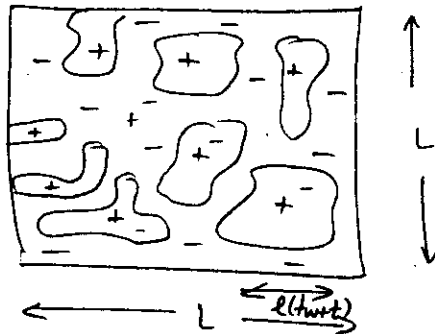
$t_w \text{ finite or } t_f \text{ finite} \Rightarrow$ PRE-ASYMPTOTIC

* HOW DO WE UNDERSTAND THE FDT-STATIONARY REGIME?

④ DOMAIN GROWTH - 'HAND WAVING ARGUMENT'



t_w (large)



t_w+t t (small)

$$\lim_{t_w \rightarrow \infty} C(t_w+t, t_w) = g_{\text{eq}}(t) = m^2(t)$$

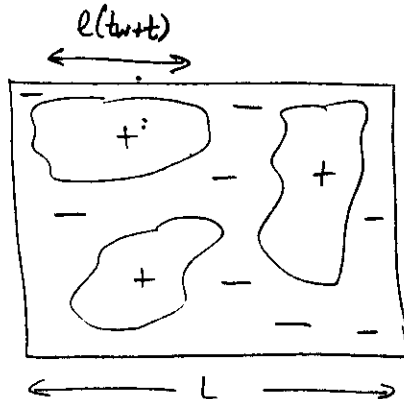
THE CONF IS ALMOST THE SAME (DOMAIN WALLS HAVE NOT MOVED). THERE ARE ONLY THERMAL FLUCT. INSIDE THE DOMAINS $\Rightarrow$

$\sim$ EQUIL. DYNAMICS

NB: $T=0 \Rightarrow g_{\text{eq}}=1$

t_w+t t (large)

NON EQUILIBRIUM



WHAT WE MEAN BY 'LARGE' DEPENDS ON THE PART. PROBLEM

$$\begin{cases} T_{\text{eq}}(L) \rightarrow \infty \\ L \rightarrow \infty \\ \text{RANDOM IC} \end{cases}$$

SCALING

WHEN t_w AND t_w+t ARE LARGE AND IN THE TIME REGION SUCH THAT THE WALLS MOVE; THE AUTO-CORR. FUNCTION SCALES AS:

$$C(t_w+t, t_w) \sim e^{-\left(\frac{l(t_w)}{l(t_w+t)}\right)}$$

WITH $l(t)$ THE TYPICAL LENGTH OF A DOMAIN AT TIME t . (WE'LL SEE LATER HOW THIS SCALING FOLLOWS FROM GENERAL - 'FORMAL' ARGUMENTS.)

WE ALREADY SEE:

- π IS VIOLATED $\rightarrow$ AGING IN C . (SCALING)
- FDT . . .

GUESS

$$\tilde{X}(t_1, t_2) = \tilde{X}[c(t_1, t_2); t_1] \sim$$

$$(*) \quad \tilde{X}(t_1, t_2) \sim f[c] \frac{1}{l(t_1)} \xrightarrow{t \rightarrow \infty} 0$$

GUESS, OBTAINED IN SIMPLE EXAMPLES

SCALING ARGUMENT?

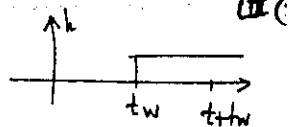
IF THIS IS TRUE

$$\tilde{X}(t_1, t_2) \sim f[c] \frac{1}{l(t_1)}$$

cfr Alan Bray's argument:

(*) NB THE FIELD WE APPLY IN THIS CASE DOES NOT FAVOUR ANY OF THE 2 (OR MORE) DOMAINS. IT'S A RANDOM FIELD. WE DO IT THIS WAY SINCE WE WANT TO COMPARE WITH SG WHEN WE DON'T KNOW HOW ARE (IF THERE ARE) DOMAINS & HENCE WHICH FIELD APP.

$$\frac{m_{tw}(t+tw)}{h} = \int_{tw}^{t+tw} ds R(t+tw, s) =$$



III(

$$= \int_{tw}^{t+tw} ds f[c(t+tw, s)] \frac{1}{l(s)} \frac{\partial c(t+tw, s)}{\partial s} +$$

$$+ \int_{\Delta(t+tw)}^{t+tw} ds \frac{1}{T} \frac{\partial c(t+tw, s)}{\partial s}$$

$$= \int_{c(t+tw, \Delta(t+tw))}^{c(t+tw, t+tw)} dc' f[c'] \frac{1}{e^{-1}(c') l(t+tw)} +$$

AGING

$$+ \int_{c(t+tw, \Delta(t+tw))}^1 dc' \frac{1}{T}$$

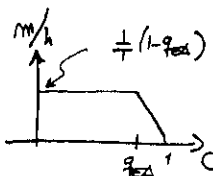
FDT

$$= \frac{1}{T} (1 - q_{EA}) + \frac{1}{l(t+tw)} \cdot \underbrace{f[q_{EA}, c]}_{\text{finite}}$$

→ 0

$$\rightarrow \frac{1}{T} (1 - q_{EA})$$

THE m VS c CURVE SHOULD LOOK LIKE FOR 'ALL' DOMAIN-GROWTH PROBLEMS



$$c' = c(t+tw, s) = l\left(\frac{l(s)}{l(t+tw)}\right) \rightarrow e^{-1}[c'] l(t+tw) = l(s)$$

THE FACT THAT $m(c)$ GOES ABOVE $\frac{1-q_{EA}}{T}$ FOR SG-MODE REFLECTS A PROP OF THE 'WEAK LONG-TERM MEMORY' SCENARIO FOR GLASSES THAT WE EXPLAIN IN LIX - LIX IN THE CONTEXT OF THE ϕ -SPIN MODEL (SEE BELOW)

③ - ④ - ⑤

WE DON'T HAVE AN OBVIOUS REAL-SPACE INTERPRETATION OF $X(C)$. BUT WE HAVE AN INTERP IN TERMS OF:

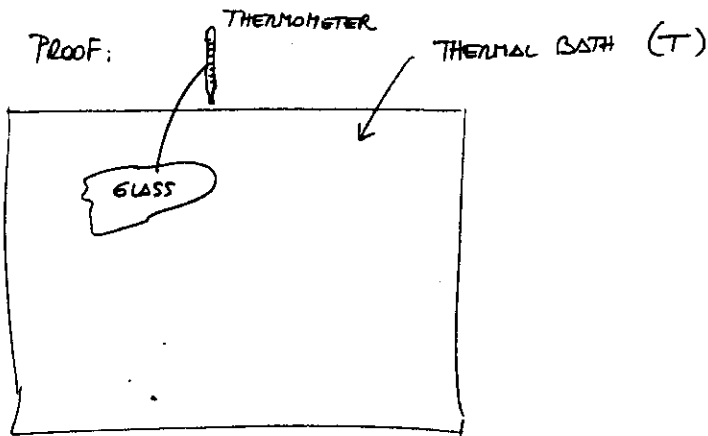
EFFECTIVE TEMPERATURES

(J. KURCHAN'S LECTURE)

WHEN COMPARING $\frac{X(C)}{T}$ WITH $\frac{1}{T}$

ONE CAN THINK ABOUT

$$\frac{X(C)}{T} = \frac{1}{T_{eff}(C)}$$



LET THE GLASS BE OF AGE t_w WHEN THE THERMOMETER IS CONNECTED TO IT.

$$E_{TOTAL} = E_{SYST} + E_{THERMOMETER} + E_{INT}$$

EXAMPLE OF THERMOMETER: HARMONIC OSCILLATOR.

$$E_{THERM} = \frac{1}{2} \dot{x}^2 + \frac{1}{2} \omega_0^2 x^2$$

$$E_{INT} = -a \underbrace{O(\vec{s})}_{\text{OBSERVABLE OF THE SYST.}} \cdot x$$

ACTS AS AN EXTERNAL (DYN) FIELD ON THE SYSTEM.

$$\begin{cases} C_0(t_f, t_w) = \langle O_b(t_f) O_b(t_w) \rangle & \text{BARE-CORR.} \\ R_0(t_f, t_w) = \left. \frac{\delta \langle O(t_f) \rangle}{\delta a x(t_w)} \right|_{a=0} & \text{RESPONSE (OF THE SYSTEM)} \end{cases}$$

$\vec{z}(t) \rightarrow$ follow Lange Dynamics THAT IMPLIES $\{C_0, R_0\}$

THE EQ FOR $\vec{x}$ IS

$$\ddot{x}_t = -\omega_0^2 x_t - \frac{\delta E_{INT}}{\delta x_t} = -\omega_0^2 x_t + a O(t)$$

$$\ddot{x}_t = -\omega_0^2 x_t + a O(t)$$

$$O(t) = O_b(t) + a \int_0^t ds R_0(t, s) x(s)$$

(ASSUMING LINEAR RESPONSE)

III (13)

$$\ddot{x}_{t_T} = -\omega_0^2 x_{t_T} + a O_b(t_T) + a^2 \int_0^{t_T} ds R_0(t_T, s) x(s) \quad (*)$$

Eq FOR THE OSCILLATOR. (DAMPED)

LINEAR IN $x(t_T)$, WITH AN INHOMOG.
GIVEN BY $O_b(t_T)$

THE IDEA IS:

MEASURE $E_{osc}(t_w, \omega_0)$ AND RELATED,

THROUGH EQUIPARTITION (APPLIED UPON THE THERMION)

TO

$$k_B T_{eff}(t_w, \omega_0) = E_{osc}(t_w, \omega_0)$$

WITHOUT ENTERING INTO ALL THE DETAILS OF THE CALCULATIONS, LET ME DEFINE THE QUANTITIES THAT ENTER THE SOL TO EQ (*) AND GIVE THE SOLUTION

$$\begin{cases} X(\omega, t_T) e^{i\omega t_T} = \int_0^{t_T} ds e^{i\omega s} R(t_T, s) \\ \tilde{C}(\omega, t_T) e^{i\omega t_T} = \int_0^{t_T} ds e^{i\omega s} C(t_T, s) \end{cases}$$

NB: THEY ARE 'EXTENDED' FOURIER TRANSFORMS IN THE SENSE THAT THEY ACT UPON THE 2nd (SMALLEST) TIME ONLY.

$$X(\omega, t_T) = \underbrace{X'(\omega, t_T)}_{\text{IN PHASE}} + i \underbrace{X''(\omega, t_T)}_{\text{OUT OF PHASE}}$$

III (14)

THE GREEN FUNCTION IS

$$G(t, t') = \exp\left(-\frac{t-t'}{t_c(t)}\right) \sin(\omega_0(t-t')) \theta(t-t')$$

FOR SMALL COUPLING / $a^2 \ll 1$

$$\text{WITH } t_c(t) = \frac{2\omega_0}{a^2 X''(\omega_0, t)}$$

$$\text{AND } \langle x^2(t) \rangle = a^2 \int_0^{t_T} ds \int_0^{t_T} ds' G(t_T, s) G(t_T, s') C(s, s')$$

AFTER SEVERAL (BORING) MANIPULATIONS

$$\frac{\omega_0^2}{2} \langle x^2(t) \rangle = \frac{\omega_0 \tilde{C}(\omega_0, t_T)}{2 X''(\omega_0, t_T)}$$

CHECK: I NEED

$$t_T \gg t_c(t_T)$$

{ CHARACTER TIME FOR THE EQUIL. OF THE OSCILLATOR

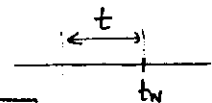
AT THE SAME TIME $a^2 X''(\omega_0, t_T)$ SMALL TO DEAL WITH THE INT. ON THE RHS OF $\langle x^2(t) \rangle$.

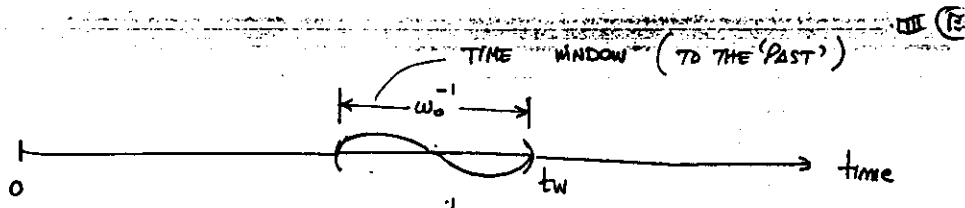
THUS,

$$k_B T_{eff}(t_w, \omega_0) = \frac{\omega_0 \tilde{C}(\omega_0, t_w)}{X''(\omega_0, t_w)}$$

THIS LOOKS VERY MUCH LIKE IMAGINING

$$k_B T_{eff}(t_w, t_w - t) = \frac{\partial_T C(t_w, t_w - t)}{R(t_w, t_w - t)}$$





'LOCAL' MEASURE IN TIME.

$t_c(t_w) \ll t_w$ CONDITION ON THE COUPLED THERMOM.

Now, WE COMPARE ω_0 WITH t_w

WE WANT TO GO BACK TO TIMES. SUPPOSE THAT FOR A CERTAIN RELATION BETWEEN

$$k_B T_{eff}(t_w, \omega_0) \chi''(\omega_0, t_w) = \omega_0 \tilde{C}(\omega_0, t_w)$$

IF ω_0 VS t_w IS SUCH THAT

$$T_{eff}(t_w, \omega_0) \sim T_{eff}$$

$\Rightarrow$

$$k_B T_{eff} R(t_w, t_w) = \frac{\partial C(t_w, t_w)}{\partial (t_w - t)}$$

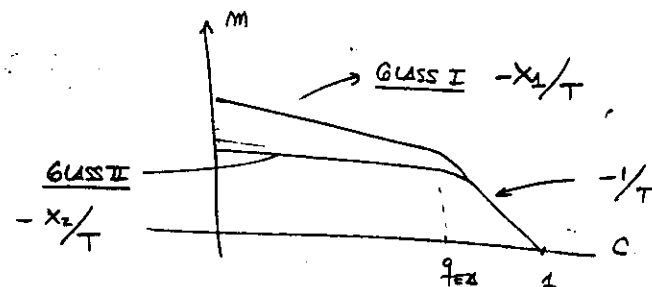
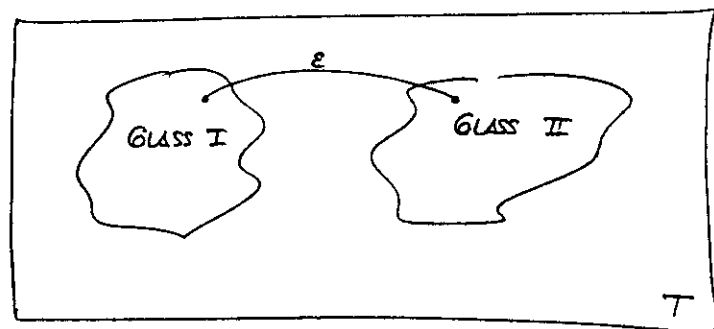
$$k_B T_{eff} R(t_w, t_w) = \frac{\partial C(t_w, t_w)}{\partial t'} \Big|_{t'=t_w}$$

BUT!

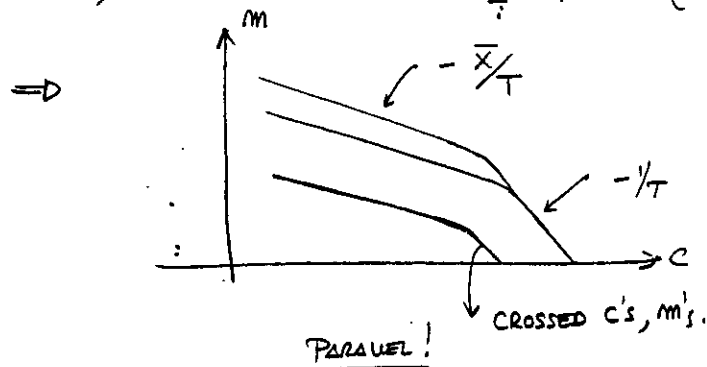
I CAN CHOOSE ω_0 VS. t_w IN SUCH A WAY TO GET $\neq T_{eff}$'s!

A CHECK: DOB T_{eff} BEHAVE AS A 'TEMPERATURE'?

PARTIAL EQUILIBRATION



NOW, CONNECT THEM WITH $E \neq 0$; σ_i (EXAMPLE)



WE COMPUTE

$$\begin{aligned}
 m^{11}(t_f, t_w) &= h \int_{t_w}^{t_f+t_w} ds R_{11}(t_f, s) & \text{vs} & & C_{11}(t_f, t_w) \\
 m^{22}(t_f, t_w) &= h \int_{t_w}^{t_f+t_w} ds R_{22}(t_f, s) & \text{vs} & & C_{22}(t_f, t_w) \\
 m^{12}(t_f, t_w) &= h \int_{t_w}^{t_f+t_w} ds R_{12}(t_f, s) & \text{vs} & & C_{12}(t_f, t_w) \\
 m^{21}(t_f, t_w) &= h \int_{t_w}^{t_f+t_w} ds R_{21}(t_f, s) & \text{vs} & & C_{21}(t_f, t_w)
 \end{aligned}$$

FOR

$$H_J[\vec{s}, \vec{\sigma}] = - \sum_{i \dots p} J_{i \dots p} s_i \dots s_p - \sum_{i \dots p} J_{i \dots p} \sigma_i \dots \sigma_p + E \sum_i s_i \sigma_i$$

THIS IS IMPORTANT SINCE (SYST 1) & (SYST 2) CAN BE JUST 'PARTS' OR 'OPERATORS' OF A SAME SYSTEM. IF THEY ALWAYS 'EQUILIBRATE' INSIDE A CORR SCALE THEN WE CAN UNDERSTAND WHY $X=CT$ INSIDE A CORR SCALE (MEANING THE TIME VECTOR WHERE C VARIES AS $C(h(t_2)/h(t_1))$, SEE BELOW FOR AN EXPLANATION)

BUT, NOTE THAT NEITHER SYST 1 NOR SYST 2 ARE EQUILIBRATED WITH THE BATH SINCE $X < 1$!

WHAT DOES THIS MEAN FOR $\neq$ OPERATOR OF THE SAME SYSTEM LIKE $E(t)$, $M(t)$?

IT MEANS THAT INITIALLY - SHORT TIMES, PRE-ASYMPTOTIC - THEY MAYBE DIFFERENT BUT FOR LARGE TIMES THEY 'MUST' BECOME THE SAME.

LAST SURPRISE

ONSAGER RELATIONS:

$$\langle A(t+t_w) B(t_w) \rangle = \langle A(t_w) B(t+t_w) \rangle$$

OR { NUMERICALLY (3D-3D-ISING)
MF

NB ONSAGER RELATIONS LIKE THE ONE ABOVE ARE

PROVEN TO HOLD ONLY IN EQUILIBRIUM.

ONE OBSERVES THEY EVEN HOLD ($\forall (t_w, t) / t_w$ IS LARGE)

FOR GLASSY SYSTEMS THAT ARE WELL OUT OF EQUILIBRIUM. IS THIS RELATED TO THE 'SMALL ENTROPY PRODUCTION'?

OUT OF EQ (THERMODYNAMICS)

$\dot{H}(t)$ SMALL $\Rightarrow$ $\left\{ \begin{array}{l} T_{eff} \\ \text{ONSAGER} \\ \text{SLOW DYN. - AGING.} \end{array} \right.$

How STRONGLY ARE THESE PROPERTIES RELATED?

STILL AT A GENERAL LEVEL

WHAT CAN WE SAY ABOUT THE BEHAVIOUR OF THE CORR FUNCTIONS?

J. PHYS. A27, 5749 (94).

IMAGINE THAT YOU HAVE 3 TIMES:

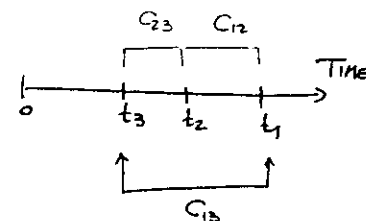
$t_1 \geq t_2 \geq t_3 \Rightarrow$ you can construct 3 corr

$$C(t_1, t_2) \Rightarrow t_1 = g(C(t_1, t_2), t_2)$$

$$C(t_2, t_3) \Rightarrow t_2 = g(C(t_2, t_3), t_3)$$

$$C(t_1, t_3)$$

$$C_{13} \leq \min(C_{12}, C_{23})$$



$$C(t_2, t_3) = C \left[g \left(C(t_1, t_2), t_2 \right); t_3 \right]$$

$$= C \left[g \left(C(t_1, t_2), g \left(C(t_1, t_3), t_3 \right) \right); t_3 \right]$$

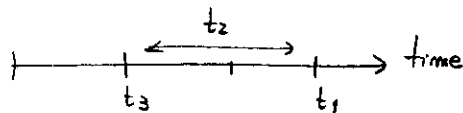
$$\lim_{t_3 \rightarrow \infty} C(t_2, t_3) = \bar{f} \left(C(t_1, t_2), C(t_1, t_3) \right)$$

$$C(t_1, t_3) = C_{13}$$

$$C(t_1, t_2) = C_{12}$$

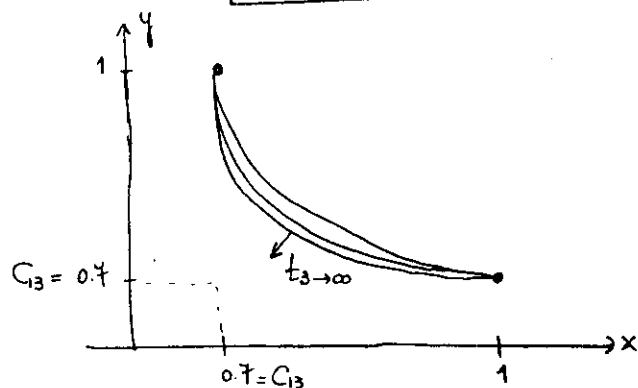
CONSTRUCTION

TAKE $C_{13} = 0.7$



if $\begin{cases} t_2 = t_3 \Rightarrow C(t_2, t_3) = 1 \\ t_2 = t_1 \Rightarrow C(t_1, t_2) = 1 \end{cases}$

$$y = \bar{f} \left(x, C_{13} \right)$$



$y = C(t_2, t_3)$
 $x = C(t_1, t_2)$

CHOOSE t_3

MOVE t_2 UNTIL
 $C(t_2, t_3) = 0.7$
 THAT SETS $t_4 = t_2$

RE-DO THE WHOLE
 COMPUTING
 $C(t_2, t_3) \neq C(t_1, t_2)$

IF THE LIMIT $\exists \Rightarrow$ THIS CONSTRUCTION HAS AN
 ASYMPTOTIC FORM (DOESN'T OSCILLATE)

NOW, LET ME INTRODUCE

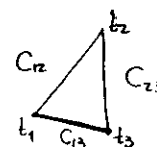
THE 'INVERSE' OF THIS FUNCTION $\bar{f} = \bar{f}(x, y)$

AND WRITE

$$C_{13} = f(C_{12}, C_{23})$$

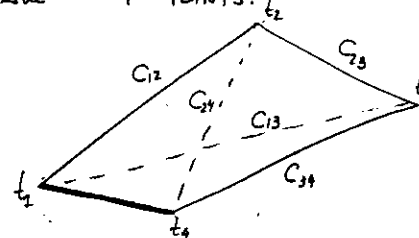
Smallest

DEFINES A 'TRIANGLE'

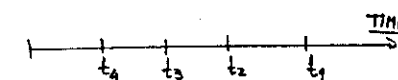


I'll WORK WITH f INSTEAD OF $\bar{f}$ EVEN IF
 IT'S TRICKY TO TAKE THIS INVERSE.

TAKE 4 POINTS:



$$t_1 \geq t_2 \geq t_3 \geq t_4$$



$$C_{14} = f(C_{12}, C_{24})$$

$$C_{14} = f(C_{13}, C_{34})$$

= THEY MUST BE EQUAL!

$$t_1 < t_2 < t_3 < t_4 \quad \text{III (2)}$$

$$f(c_{12}, c_{24}) = f(c_{13}, c_{34})$$

BUT $c_{13} = f(c_{12}, c_{23})$

$$c_{24} = f(c_{23}, c_{34})$$

$$f(c_{12}, f(c_{23}, c_{34})) = f(f(c_{12}, c_{23}), c_{34})$$

$$f(x, f(y, z)) = f(f(x, y), z)$$

⇓

$$\underline{f \text{ IS ASSOCIATIVE}}$$

$$\underline{f: \mathbb{R}^2 \rightarrow \mathbb{R}}$$

PROPERTIES:

$$c_{13} = f(c_{12}, c_{23})$$

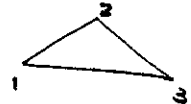
if $t_2 = t_1 \Rightarrow c_{23} = f(1, c_{23}) \Rightarrow x = f(1, x)$

if $t_2 = t_3 \Rightarrow c_{12} = f(c_{12}, 1) \Rightarrow x = f(x, 1)$

IT HAS AN IDENTITY

SINCE $c_{13} \leq \min(c_{12}, c_{23})$

$$f(c_{12}, c_{23}) \leq \min(c_{12}, c_{23})$$



EXAMPLES:

→ $f(x, y) = \min(x, y) \rightarrow$ Ultrametricity.

→ $f(x, y) = xy$

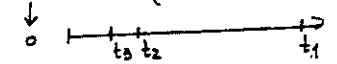
NO DETAILS SINCE LONG BUT

ONE CAN SHOW WITHOUT ANY ASSUMPTION AND
QUITE FORMALLY THAT:

IT HAS AT LEAST 1 ZERO.

IF $t_3 = 0^+ \ll t_1 \Rightarrow c_{13} = 0 = f(c_{12}, c_{23}) = f(c_{12}, 0)$

$t_3 = t_2 = 0^+ \ll t_1 \Rightarrow c_{13} = 0 = f(0, c_{23})$



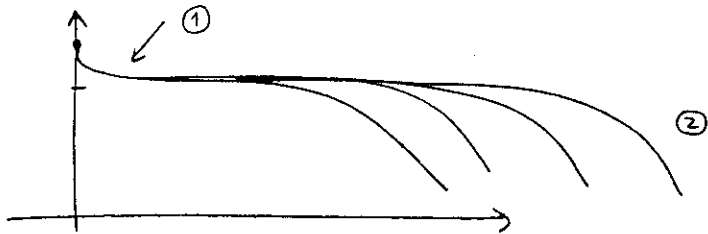
COMBINATIONS OF THESE TWO EXAMPLES ARE THE UNIQUE POSSIBILITIES FOR f !

TAKE $t_2 / C_{12} = C_{23} = a \Rightarrow$

$$f(a, a) \leq \min(a, a) = a$$

WE CAN HAVE 'FIXED POINTS' $a^* / f(a^*, a^*) = a^*$
OR VALUES $a \neq a^* / f(a, a) < a$.

a^* SEPARATE $\neq$ CORR SCALES. LIVE IN THE CORR. $a^* = q_{FEA}$



WHEN $C \geq q_{FEA} \Rightarrow C_{①}(t, t') = j_{①}^{-1} \left(\frac{h_{①}(t')}{h_{①}(t)} \right)$
WHEN $C \leq q_{FEA} \Rightarrow C_{②}(t, t') = j_{②}^{-1} \left(\frac{h_{②}(t')}{h_{②}(t)} \right)$

THIS SCALING IS PROVEN!

INSIDE A SCALE, IE BETWEEN TWO FIXED POINTS:

$$f(a, b) = a \cdot b \Leftrightarrow a = j^{-1} \left(\frac{h(t')}{h(t)} \right)$$

JUST A COUPLE OF EXAMPLES:

$$(*) C_{①}(t, t') = C_F(t - t') = j_F^{-1} \left(\frac{h_F(t')}{h_F(t)} \right)$$

FDT - STATIONARY
SECTOR

CHOOSING $h_F(t') = \exp(\alpha t')$

$$\frac{h_F(t')}{h_F(t)} = \exp[\alpha(t - t')]$$

$$C_F(t - t') = j_F^{-1} \left[\exp(-\alpha(t - t')) \right]$$

$$C_F = j_F^{-1} \circ \exp - \alpha$$

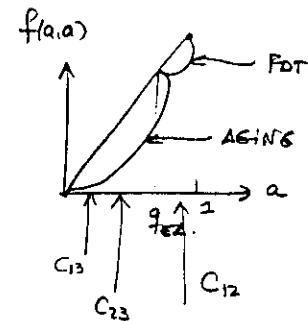
$$(*) C_{②}(t, t') = j^{-1} \left(\frac{h(t')}{h(t)} \right)$$

e.g. Domain Growth $\ell \left(\frac{\ell(t')}{\ell(t)} \right)$

(*) f BETWEEN $\neq$ CORR SCALES:

I WANT TO COMPUTE

$$C_{13} = f(C_{12}, C_{23})$$



$$\begin{cases} C_{12} = j_F^{-1} [\exp(-\alpha(t_1 - t_2))] \\ C_{23} = j_A^{-1} \left[\frac{h(t_3)}{h(t_2)} \right] \end{cases}$$

$$C(t_1, t_3) \leq \min(C_{12}, C_{23})$$

I NEED TO WRITE $C(t_1, t_3)$

I'U ASSUME $C_{13} \in \text{AGING} \Rightarrow$

$$\begin{aligned} C_{13} &= j_A^{-1} \left(\frac{h(t_3)}{h(t_1)} \right) \\ &= j_A^{-1} \left(\frac{h(t_3)}{h(t_2)} \cdot \frac{h(t_2)}{h(t_1)} \right) \\ &= j_A^{-1} \left[j_A(C_{23}) \cdot \frac{h(t_2)}{h(t_1)} \right] \end{aligned}$$

$$\frac{h(t_2)}{h(t_1)} = ?$$

$$\begin{aligned} \ln[j_F(C_{12})] &= -\alpha(t_1 - t_2) \\ \frac{1}{\alpha} \left[\alpha t_1 + \ln j_F(C_{12}) \right] &= t_2 \\ \frac{h \left[t_1 + \frac{1}{\alpha} \ln j_F(C_{12}) \right]}{h(t_1)} &= \frac{h(t_2)}{h(t_1)} \\ &\downarrow 1 \end{aligned}$$

LIII (27)

Thus,

$$C_{13} = C_{23} = \min(C_{12}, C_{23})$$

THIS HAS BEEN PROVEN IN FULL GENERALITY.

LIII (28)

THIS WILL HELP US SOLVING THE EQUATIONS,
IN PARTICULAR

$$C(h(t)) = j^{-1} \left(\frac{h(t')}{h(t)} \right).$$

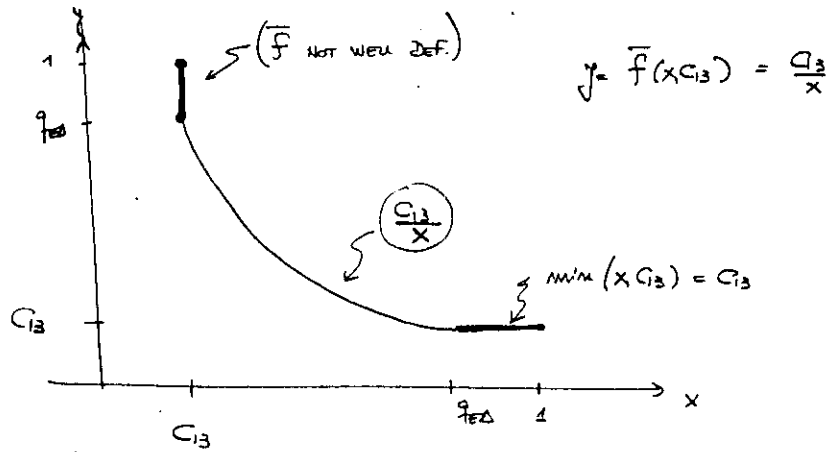
HOW MANY FIXED POINTS ARE, WHAT'S THE FORM OF j^{-1} ,
 h WILL BE DETERMINED BY THE MODEL.

ACTUALLY, FOR THE MOMENT WE HAVE:

$$\begin{cases} 2 \text{ SCALES.} & \rightarrow \text{ALL } p\text{-SPINS, DOMAIN GROWTH} \\ \text{DO NOT SCALES} & \rightarrow \text{SK} \end{cases}$$

THIS IS REMINISCENT OF THE STRUCTURE OF REPLICAS
SYMMETRY BREAKING AT THE STATIC LEVEL.
FORMAL CONNECTION? SUSY.

THUS, STANDARD CASE (FDT + SOMETHING, E.G. DOMAIN GROWTH, IS



$$xy = f(x, y) = C_{13}$$

$$C_{13} = f(x, y) = \min(x, y) = \min(C_{13}, y) = C_{13} \quad (\text{indep of } y) \quad \bar{f} = \frac{C_{13}}{x}$$

NO INVERSE WELL DEFINED. BUT I CAN PUT IT AS ABOVE

LECTURES IV & V

- DYN. EPS. FOR DISORDERED & NON-DISORDERED MODELS
- SOLUTION TO A PARTICULAR CASE: THE p -SPIN SPHERICAL MODEL OR A SIMPLE MODE-COUPLING APPROACH TO GLASSES.

AN EXAMPLE p -SPIN MODEL

$$H_J[s] = - \sum_{i_1, \dots, i_p} J_{i_1, \dots, i_p} s_{i_1} \dots s_{i_p}$$

$$\dot{s}_i(t) = - \frac{\delta H_J[s]}{\delta s_i(t)} - z(t) s_i(t) + \xi_i(t)$$

HOW DO WE OBTAIN DYN EPS FOR MACROSCOPIC QUANTITIES LIKE $\{CR\}$? THROUGH THE MARTIN-SIEGEL-ROSE (MSR) FORMALISM.

MSR (REM: H. KANDAS LECTURE)

$$\left\{ \begin{aligned} Z_{dyn} &= 1 = \int \mathcal{D}\vec{s} \exp \left[-\frac{1}{4\pi} \int d\tau \vec{s}^2(\tau) \right] \\ \mathcal{D}\vec{s} &= \prod_i \frac{d\vec{s}_i(\tau)}{\sqrt{4\pi\pi}} \end{aligned} \right. \quad (1)$$

$$P[J_{i_1, \dots, i_p}] = \sqrt{\frac{N^{p-1}}{\pi p!}} \exp \left[-\frac{N^{p-1} J_{i_1, \dots, i_p}^2}{p!} \right]$$

CIRANO
LIST OF STEPS

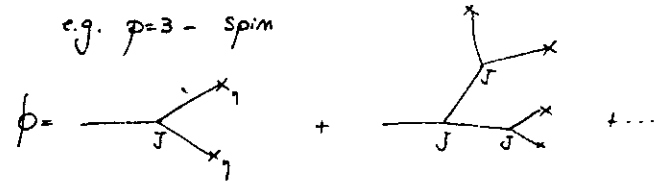
- Start from (1)
- Fix the gauge à la Fadeev-Popov inserting

$$\int \mathcal{D}\vec{s} \delta(\vec{s} - E_q[\vec{s}]) \left| \det \left(\frac{\delta E_q(\vec{s})}{\delta \vec{s}} \right) \right| = 1$$
- Write $Z_{dyn} = 1 = \int \mathcal{D}\vec{s} \mathcal{D}\hat{s} \mathcal{D}\hat{i} \hat{s} \exp - S_J^{(1)}[\vec{s}, \hat{i}, \hat{s}]$
- Int over $\hat{s} \Rightarrow Z_{dyn} = 1 = \int \mathcal{D}\vec{s} \mathcal{D}\hat{i} \exp - S_J^{(2)}[\vec{s}, \hat{i}]$
- Take $\int dJ P[J] Z_{dyn} = 1 = \int \mathcal{D}\vec{s} \mathcal{D}\hat{i} \exp - N S^{(3)}[\vec{s}, \hat{i}]$
- Now, Large N approx $\Rightarrow$ SEVERAL WAYS OF OBTAINING EPS FOR C&R (2 m if $h \neq 0$).

ANOTHER WAY

PERTURBATIVELY

e.g. $p=3$ -spin



$$\left. \begin{aligned} C(t,t') &= \overline{\langle \phi \phi \rangle} \\ R(t,t') &= \overline{\langle \phi \eta \rangle} \end{aligned} \right\} \Rightarrow \text{BUT } \overline{\cdot} \text{ -D ONLY CERTAIN TERMS SURVIVE (SYMM. PROD. OF } P[J], S. \Rightarrow \text{SCHWINGER-DYSON EPS AND } \left(\frac{\Sigma}{D} \right)$$

REMARK:

ONE NOTICES THAT

DISORDERED SYSTEM $\equiv$ NON-DISORDERED APPROXIMATED. !
(SAME GRAPHS SURVIVE)



SAME PHENOMENOLOGY

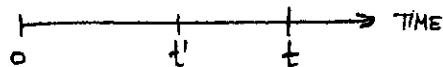
(AND A POSSIBLE WAY OF SEEING THE 'UNIVERSALITY' APPEAR)

(KRAICHNAN; KIRKPATRICK & THIRUMALAI, FRANZ & HEUTE, JPB, LFC, JK, MM)

DYNAMICAL EQS. FOR THE p-SPIN SPH MODEL

LFC - JK PRL 71, 173 (93).

NOTATION



$\forall(t, t')$

$$\partial_t R(t, t') = -z(t) R(t, t') + \frac{p(p-1)}{2} \int_{t'}^t ds R(t, s) C^{p-2}(t, s) R(t, s) + \delta(t-t') \quad (\text{Eq-R})$$

$$\partial_t C(t, t') = -z(t) C(t, t') + \frac{p}{2} \int_0^{t'} ds C^{p-1}(t, s) R(t, s) + \frac{p(p-1)}{2} \int_0^t ds R(t, s) C^{p-2}(t, s) C(s, t') + 2T R(t, t') \quad (\text{Eq-C})$$

THE EQ FOR THE LAGRANGE MULTIPLIER $z(t)$ FOLLOWS FROM IMPOSING THE SPH CONSTRAINT $C(t, t) = 1$.
IF $C(t, t) = 1 \Rightarrow$

$$\lim_{t' \rightarrow t^-} \left(\partial_t C(t, t') + \partial_{t'} C(t, t') \right) = 0$$

$$\lim_{t' \rightarrow t^-} \left[\text{Eq-C}(t, t') + \text{Eq-C}(t', t) \right] = 0.$$



IV.6

$$0 = -2z(t) + p^2 \int_0^t ds R(t, s) C^{p-1}(t, s) + 2T \lim_{t' \rightarrow t^-} \left(R(t, t') + R(t', t) \right) \quad (\text{IV.4})$$



$$z(t) = \frac{p^2}{2} \int_0^t ds R(t, s) C^{p-1}(t, s) + T \quad (\text{Eq-z})$$

$$\text{SINCE } \lim_{t' \rightarrow t^-} R(t, t') = 0, \quad \lim_{t' \rightarrow t^-} R(t', t) = 1. \quad (1)$$

PROPS. OF THE DERIV. OF C AROUND $t \approx t'$

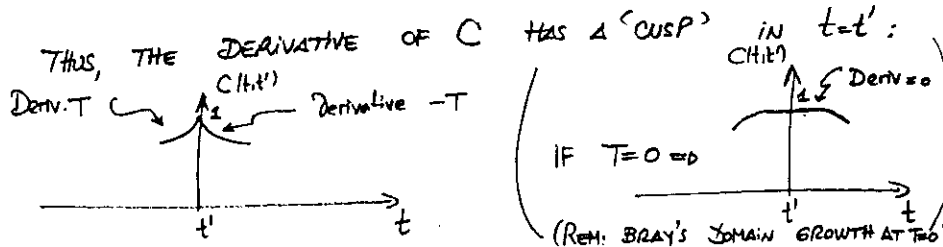
$$\text{PROPS OF } \lim_{t' \rightarrow t^-} \partial_t C(t, t') \quad \neq \quad \lim_{t' \rightarrow t^+} \partial_t C(t, t')$$

LET'S CONSIDER $t > t'$ IN (Eq-C) AND TAKE $\lim_{t' \rightarrow t^-}$:

$$\lim_{t' \rightarrow t^-} \partial_t C(t, t') = -z(t) + \frac{p^2}{2} \int_0^t ds R(t, s) C^{p-1}(t, s) = -T \quad (\text{USING Eq-z})$$

NOW, CONSIDER $t < t'$ IN (Eq-C) AND TAKE $\lim_{t' \rightarrow t^+}$:

$$\lim_{t' \rightarrow t^+} \partial_t C(t, t') = -z(t) + \frac{p^2}{2} \int_0^t ds R(t, s) C^{p-1}(t, s) + 2T = T \quad (3)$$



CONFRONT R WITH $\partial_t C$ AT $t' \rightarrow t^-$:

$$-\frac{1}{T} \lim_{t' \rightarrow t^-} \partial_t C(t, t') = \lim_{t' \rightarrow t^-} R(t, t')$$

FROM (2)-(3), AROUND $t' \simeq t$ ONE CAN WRITE:

$$C(t, t') \simeq 1 - T |t - t'|$$

AND THEN

$$\lim_{t' \rightarrow t^-} R(t, t') = + \frac{1}{T} \lim_{t' \rightarrow t^-} \partial_{t'} C(t - t')$$

IE FDT HOLDS AROUND THE DIAGONAL. (1st ORDER IN $(t - t')$)

$\forall t' \geq 0. \quad \forall T!$

(NB) THIS IS NOT TRUE IF THERE'S INERTIA ($m \partial_t^2$). IN THIS CASE ONE NEEDS t' LARGE TO HAVE FDT AROUND $t' \simeq t$.

REM FORMAL BOUNDS & TIME-SECTORS $\Rightarrow$ OK.

SOLUTION ABOVE T_d

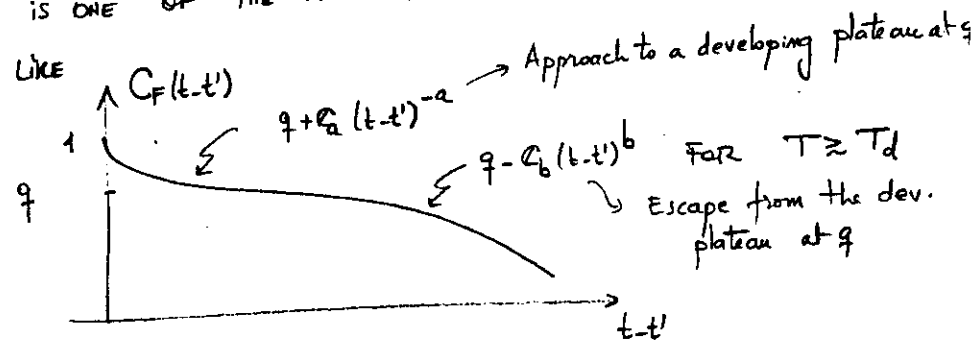
ONE CAN CHECK (EXERCISE!) THAT (EQ-C)-(EQ-R)-(EQ-Z)
ADMIT, FOR $T > T_d$ A SOLUTION

$$\left\{ \begin{array}{l} Z(t) \rightarrow Z_\infty \\ R(t, t') \rightarrow R_F(t - t') \\ C(t, t') \rightarrow C_F(t - t') \end{array} \right\} R_F(t - t') = \frac{1}{T} \frac{dC_F(t - t')}{dt'}$$

FOR LARGE t' AND $\forall (t - t')$.

IN OTHER WORDS, ABOVE T_d THE SYSTEM EQUILIBRATES
AFTER A NONEQUILIBRIUM TRANSIENT — EVEN IF $N \rightarrow \infty$ FIRST.

THE RESULTING EQ FOR $C_F(t - t')$ (ONCE THE R-EQ & C-EQ HAVE BEEN COLLAPSED TO A SINGLE ONE USING FDT) IS ONE OF THE MC-EQS FOR GLASSES. THE SOL. LOOKS



$\rightarrow$ THIS SOL BREAKS DOWN BELOW T_d !

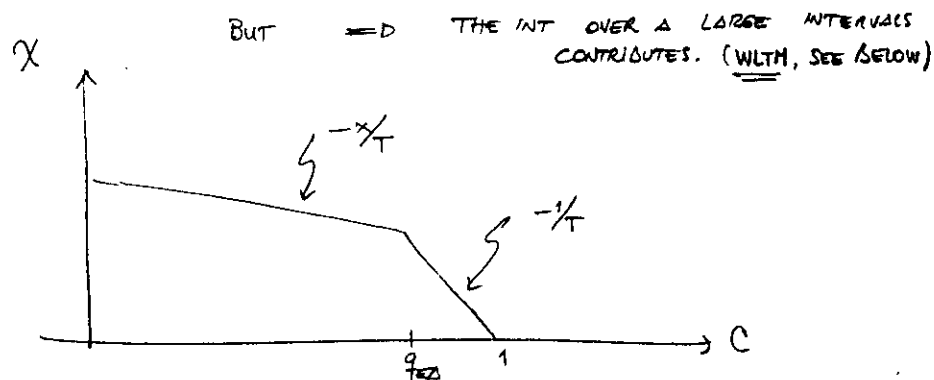
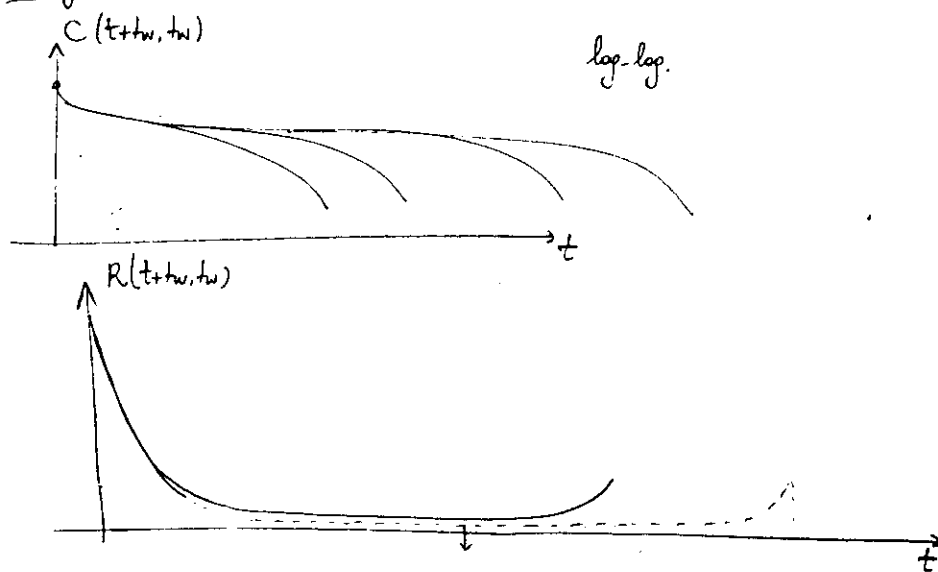
$T < T_d \rightarrow$ NUMERICAL SOLUTION

LIV (7)

NUMERICAL SOLUTION OF THE DYN EQS (CAUSAL) HELP US
DEVELOPING AN ANSATZ TO SOLVE THEM. THE MAIN POINTS ARE:

NUMERICAL SOLUTION:

$T < T_d$



$T < T_d \rightarrow$ THE CORRELATION
LET'S DEF

LIV (8)

$$C(t+tw, tw) = C_S(t) + C_A(t+tw, tw)$$

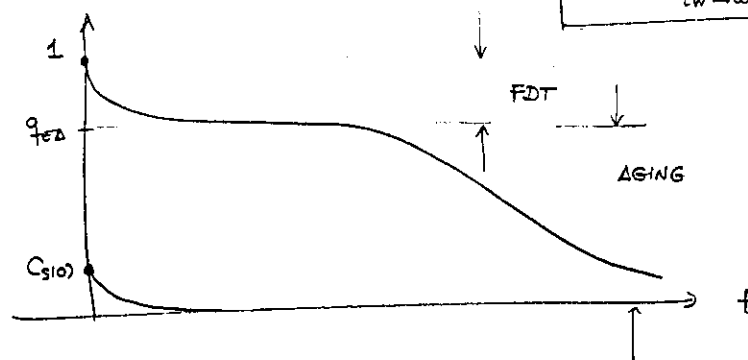
• $t=0$ $C(tw, tw) = 1 = C_S(0) + C_A(tw, tw)$

Let's choose $C_S(0) = 1 - q_{EZ}$
 $C_A(tw, tw) = q_{EZ} \quad \forall tw.$

• $\lim_{tw \rightarrow \infty} \lim_{t \rightarrow \infty} C = C_F(t) = C_S(t) + \lim_{tw \rightarrow \infty} C_A(t+tw, tw)$

$C(t+tw, tw)$

$q_{EZ} = \lim_{tw \rightarrow \infty} C_A(t+tw, tw)$



$$\lim_{t \rightarrow \infty} \lim_{tw \rightarrow \infty} C = q_{EZ} = \lim_{t \rightarrow \infty} C_S(t) + q_{EZ}$$

$\lim_{t \rightarrow \infty} C_S(t) = 0$

$\lim_{t \rightarrow \infty} C_F(t) = q_{EZ}$

$$\lim_{t \rightarrow \infty}$$

$$\lim_{t \rightarrow \infty} C = 0 = \lim_{t \rightarrow \infty} \cancel{C_s(t)} + \lim_{t \rightarrow \infty} C_d \quad \text{LII (9)}$$

$$\lim_{t \rightarrow \infty} C_d(t+tw, tw) = 0$$

$$C_{su} \quad C_F(t) = C_s(t) + q_{\text{EZ}} \quad (\text{LIVES IN AN INTERVAL})$$

THE RESPONSE

$$I \text{ EXPECT} \quad R = X(c) \frac{\partial C}{\partial t} \quad X(c) = \begin{cases} 1/T & C > q_{\text{EZ}} \\ \infty/T & C < q_{\text{EZ}} \end{cases}$$

$$R(t+tw, tw) = \underbrace{R_s(t)}_{\text{SAME INT AS } C_s} + \underbrace{R_d(t+tw, tw)}_{\text{SAME INT AS } C_d}$$

$$\cdot \boxed{t=0^+} \quad R(tw, tw) = 1 = R_s(0) + R_d(tw, tw)$$

$$\boxed{\begin{aligned} R_s(0) &= 1 \\ R_d(tw, tw) &= 0 \end{aligned}}$$

$$\lim_{t \rightarrow \infty} R(t+tw, tw) \equiv R_F(t) = R_s(t) + \lim_{tw \rightarrow \infty} \underbrace{R_d(t+tw, tw)}_0 \quad (\text{WLTM})$$

$$R_F(t) = R_s(t) = -\frac{1}{T} \frac{dC_s(t)}{dt} = -\frac{1}{T} \frac{dC_F(t)}{dt}$$

$$\lim_{t \rightarrow \infty} R_s(t) = 0$$

NO FDT

$$\lim_{\substack{t, tw \rightarrow \infty \\ C < q_{\text{EZ}}}} R = \lim_{\substack{t, tw \rightarrow \infty \\ C < q_{\text{EZ}}}} R_d = \frac{\infty}{T} \left. \frac{\partial C_d(t+tw, t')}{\partial t'} \right|_{t'=tw}$$

SLOW DYNAMICS & WLTM

$$\text{BOTH } R_d \text{ AND } \frac{\partial C_d}{\partial t'} \rightarrow 0$$

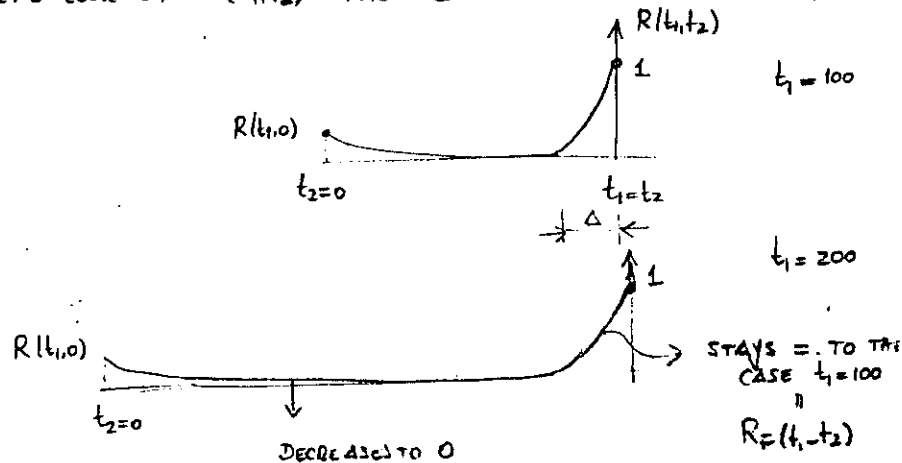
$$\text{BUT } R_d / \frac{\partial C_d}{\partial t'} \rightarrow \infty \neq 0$$

→ REM FORMAL DEMONSTRATION & INEQUALITIES IN LII & LIII!

WEAK LONG-TERM MEMORY

EVEN IF $R(t, t_2) \rightarrow 0$ as $t_2 \rightarrow \infty$, ITS INTEGRAL OVER A LONG INTERVAL IS FINITE!

LET'S LOOK AT $R(t_1, t_2)$ FOR t_2 FIXED, AS A FUNCTION OF $t_1 - t_2$.



BUT, WHEN WE LOOKED AT $m(c)$ VS c :

- $\lim_{t_w \rightarrow 0} \int_0^{t^*} ds R(t + t_w, s) = 0 \quad \forall t^* \text{ fixed (ie finite wrt } t_w)$
- $\lim_{t, t_w \rightarrow \infty} \int_{t_w}^{t+t_w} ds R(t + t_w, s) > \frac{1 - q_{\text{ED}}}{T}$
 $C(t, t_w) = C q_{\text{ED}}$

THIS IS IMPORTANT! EVEN IF THE SYSTEM HAS MEMORY OF

THE PAST, IT KEEPS IT ONLY IN AN INTEGRATED WAY.

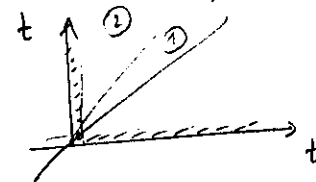
IT MAKES THE PROBLEM DIFFICULT BUT SOLVABLE.

BELOW T_d TACTICS:

ASSUME THERE ARE $\begin{cases} \text{FDT-REGION} \\ \text{AGING II} \end{cases}$, WRITE THE EQS FOR EACH OF THEM & TRY TO SOLVE THEM (GUIDED BY THE NUMERICAL SOL)

EXERCISEFDT-REGION

CHOOSE (t, t') IN ④, ie $C(t, t') = C_F(t - t') > q_{\text{ED}}$.



$$\tau = t - t'$$

 R_F -EQ

$$\frac{d}{dt} R_F(t) = -z_{\infty} R_F(t) + \frac{p(p-1)}{2} \int_0^t dt' R_F(t-t') C_F^{p-2}(t-t') R_F(t')$$

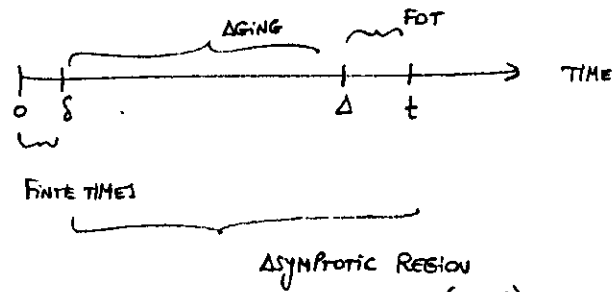
 R_F -EQ

Easy: all times fall between (t', t) that are assumed to fall in ①.

NB: z_{∞} DISCUSSED JUST BELOW

Z-EQ IT'S A ONE-TIME QUANTITY: WE ASSUME IT GOES TO A CT. LIV ⑩

$$Z(t) = T + \frac{P^2}{2} \int_0^t ds C^{P1}(t,s) R(t,s)$$



$$\lim_{t \rightarrow \infty} Z(t) = T + \frac{P^2}{2} \left(\int_0^\delta + \int_\delta^\Delta + \int_\Delta^t \right)$$

$$\approx T + \frac{P^2}{2} \lim_{t \rightarrow \infty} \left[\int_0^\Delta ds \underbrace{R_A(t,s)}_{\frac{X}{T} \frac{\partial C_A(t,s)}{\partial s}} C_A^{P1}(t,s) + \int_\Delta^t ds \underbrace{R_F(t,s)}_{\frac{1}{T} \frac{dC_F(t-s)}{ds}} C_F^{P1}(t,s) \right]$$

$$= T + \frac{P^2}{2} \left[\frac{X}{T} \lim_{t \rightarrow \infty} \int_{C_A(t,0^+) \rightarrow 0}^{C_A(t,\Delta) \rightarrow q_{\text{ss}}} dC_A^{P1} + \frac{1}{T} \lim_{t \rightarrow \infty} \int_{C_F(t-\Delta) = q_{\text{ss}}}^{C_F(0) = 1} dC_F^{P1} \right]$$

$$= T + \frac{P^2}{2} \left[\frac{X}{T} q_{\text{ss}}^P + \frac{1}{T} (1 - q_{\text{ss}}^P) \right]$$

$$\boxed{Z_{\infty} = T + \frac{P^2}{2} \left[\left(\frac{X-1}{T} \right) q_{\text{ss}}^P + \frac{1}{T} \right]} \quad \text{Z-EQ}$$

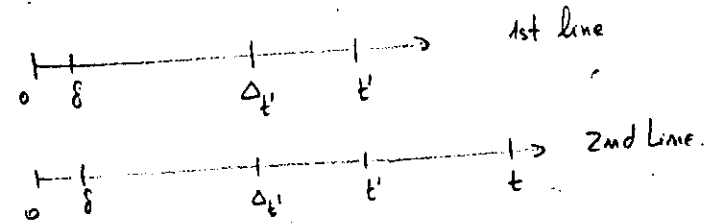
C_F-EQ

MORE DIFFICULT.

$$\frac{d}{dt} C_F(t) = -Z_{\infty} C_F(t) + \underbrace{\frac{P}{2} \text{Int} \textcircled{1} + \frac{P(P-1)}{2} \text{Int} \textcircled{2}}_{\downarrow}$$

$$\frac{P}{2} \left[\left(\int_0^\delta + \int_\delta^{\Delta'} + \int_{\Delta'}^{t'} \right) C^{P1}(t,s) R(t,s) \right] +$$

$$+ \frac{P(P-1)}{2} \left[\left(\int_0^\delta + \int_\delta^\Delta + \int_\Delta^{t'} + \int_{t'}^t \right) R(t,s) C^{P2}(t,s) C(s,t') \right]$$



$$= \frac{P}{2} \left[\int_0^{\Delta'} ds C_A^{P1}(t,s) R_A(t,s) + \int_{\Delta'}^{t'} ds C_F^{P1}(t-s) R_F(t,s) \right]$$

$$+ \frac{P(P-1)}{2} \left[\int_0^{\Delta'} ds R_A(t,s) C_A^{P2}(t,s) C_A(t,s) + \int_{\Delta'}^{t'} ds R_F(t-s) C_F^{P2}(t-s) C_F(t-s) + \int_{t'}^t ds R_F(t-s) C_F^{P2}(t-s) C_F(s-t') \right]$$

$$\begin{aligned}
 &= \underbrace{\frac{pX}{2T} \int_0^{\Delta} ds C_A^{P_1}(t,s) \frac{\partial C_A(t,s)}{\partial s}}_{(1)} + \underbrace{\frac{p}{2T} \int_{\Delta}^{t'} ds C_F^{P_1}(t-s) \frac{\partial C_F(t-s)}{\partial s}}_{(2)} \\
 &+ \underbrace{\frac{p(p-1)}{2T} \times \int_0^{\Delta} ds \frac{\partial C_A(t,s)}{\partial s} C_A^{P_2}(t,s) C_A(t,s)}_{(1)} \\
 &+ \underbrace{\frac{p(p-1)}{2T} \int_{\Delta}^{t'} ds \frac{\partial C_F(t-s)}{\partial s} C_F^{P_2}(t-s) C_F(t-s)}_{(2)} \\
 &+ \frac{p(p-1)}{2T} \int_{t'}^t ds \frac{\partial C_F(t-s)}{\partial s} C_F^{P_2}(t-s) C_F(s-t') \\
 \\
 &= \frac{pX}{2T} \int_0^{\Delta} ds \frac{\partial}{\partial s} \left(C_A^{P_1}(t,s) C_A(t,s) \right) + \frac{p}{2T} \int_{\Delta}^{t'} ds \frac{\partial}{\partial s} \left(C_F^{P_1}(t-s) C_F(t-s) \right) \\
 &+ \frac{p(p-1)}{2T} \int_{t'}^t ds \frac{\partial C_F(t-s)}{\partial s} C_F^{P_2}(t-s) C_F(s-t') \\
 \\
 &= \frac{pX}{2T} \left[q_{\text{eq}}^{P_1} q_{\text{eq}} \right] + \frac{p}{2T} C_F^{P_1}(t-t') - q_{\text{eq}}^{P_1} q_{\text{eq}} + \\
 &+ \frac{p}{2T} \int_{t'}^t ds \frac{\partial C_F^{P_1}(t-s)}{\partial s} C_F(s-t') \\
 \\
 &= \frac{p}{2T} (X-1) q_{\text{eq}}^P + \frac{p}{2T} C_F^{P_1}(t-t') + \frac{p}{2T} \int_{t'}^t ds \frac{\partial C_F^{P_1}(t-s)}{\partial s} C_F(s-t')
 \end{aligned}$$

Thus,

$$\begin{aligned}
 \frac{dC_F(t)}{dt} &= -z_{\infty} C_F(t) - \frac{p}{2T} (1-X) q_{\text{eq}}^P + \frac{p}{2T} C_F^{P_1}(t) + \\
 &+ \frac{p(p-1)}{2} \int_0^T du R_F(u) C_F^{P_2}(u) C_F(t-u)
 \end{aligned}$$

C_F-EQ

EXERCISE:

• CHECK

$$-\frac{1}{T} \frac{d}{dt} (E_Q - C_F) \Rightarrow E_Q - R_F.$$

OK WITH FOR

- IF $T > T_d$ $X=1$ AND ONE RECOVERS THE HIGH-T EQS.

THESE EQS CONTAIN INFO ABOUT THE AGING REGIME THROUGH z_{∞} !

TO SOLVE THIS, LET US FIRST LOOK AT THE AGING REGIME & THEN COME BACK TO (R_F-EQ) - (C_F-EQ).

AGING EQUATIONS

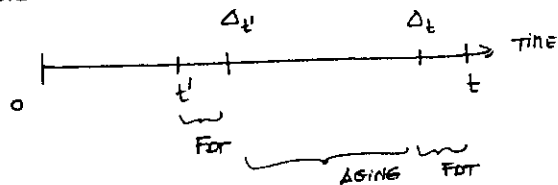
Let's choose $(t, t') / C < q_{ex}$.

$$\frac{\mathcal{W}_A(t, t')}{\partial t} = -z_{\infty} C_A(t, t') + \frac{p}{2} I_{NT}^{(1)} + \frac{p(p-1)}{2} I_{NT}^{(2)}$$

$$\frac{\partial R_\Delta(t,t')}{\partial t} = -2\lambda R_\Delta(t,t') + \frac{P(P-1)}{2} I_{\text{INT}} \quad (3)$$

RA-EQ

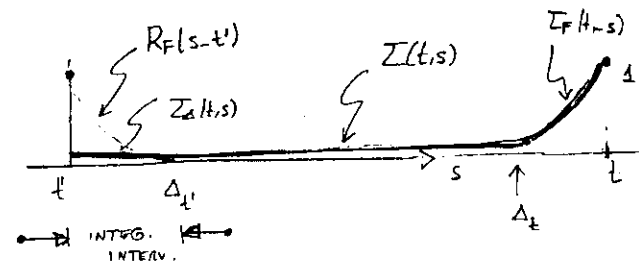
SINCE (t, t') ARE FAR AWAY, EVEN TO INT⁽³⁾ THE AGING PART CONTRIBUTES



$$J_{\text{RF}}^{(5)} = \frac{P(P-1)}{2} \int_{t'}^t ds \, R_A(t,s) C_A^{P-2}(t,s) R_A(s,t') + \frac{P(P-1)}{2} \left\{ \int_{t'}^{t_1} ds \, R_A(t,s) C_A^{P-2}(t,s) R_F(s-t') + \int_{t_1}^{t_2} ds \, R_A(t,s) C_A^{P-2}(t,s) R_A(s,t') + \int_{t_2}^t ds \, R_F(t-s) C_F^{P-2}(t-s) R_A(s,t') \right\} + \frac{1}{T} \frac{\partial \mathcal{L}_F(t-t')}{\partial t'}$$

FIRST TEAM

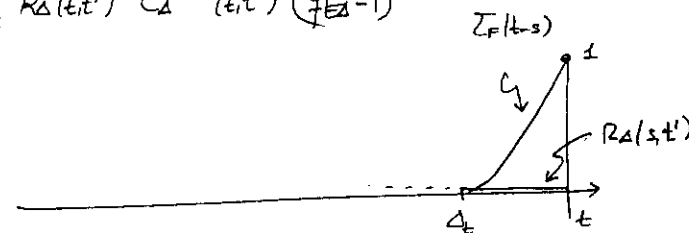
$$Z(t,s) = R(t,s) C^{T-2}(t,s)$$



So, we are convoluting a very 'PEAKED' function $R_F(s-t')$ with a very slowly varying function $\Sigma_L(t,s)$. Thus, we'll take $R_F(s-t')$ to act almost as a δ -function with a width:

$$\begin{aligned}
 \int_{t'}^{\Delta_{t'}} ds \quad R_{\Delta}(t,s) \quad C_{\Delta}^{P-2}(t,s) \quad R_F(s-t') &\approx \\
 R_{\Delta}(t,t') \quad C_{\Delta}^{P-2}(t,t') \quad \int_{t'}^{\Delta_{t'}} ds \quad R_F(s-t') &\stackrel{!}{=} \frac{\partial C_F(s-t')}{\partial t'} \\
 = R_{\Delta}(t,t') \quad C_{\Delta}^{P-2}(t,t') \left(-\frac{1}{T}\right) \left(C_F(\Delta_{t'}-t') - \overset{1}{\cancel{C_F(0)}}\right) \\
 = -\frac{1}{T} R_{\Delta}(t,t') \quad C_{\Delta}^{P-2}(t,t') \left(\frac{0}{\cancel{1}} - 1\right) & \quad T_F(t-s)
 \end{aligned}$$

THIRD TERM



SAME PROCEDURE $\Rightarrow$

$$\begin{aligned} \int_{\Delta_t}^t ds \, R_F(t-s) C_F^{p-2}(t-s) R_A(s, t') &\sim R_A(t, t') \int_{\Delta_t}^t ds \, R_F(t-s) C_F^{p-2}(t-s) \\ &= R_A(t, t') \left(\frac{t}{T}\right) \frac{1}{p-1} \int_{\Delta_t}^t ds \, \frac{\partial C_F^{p-1}(t-s)}{\partial s} \\ &= + \frac{1}{T(p-1)} R_A(t, t') \left[1 - \frac{0^{p-1}}{t^{\frac{p-1}{2}}} \right] \end{aligned}$$

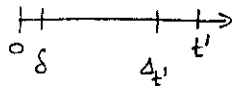
$$INT_2 = \text{LEAVE IT LIKE IT IS.}$$

$$FNAWY \quad \boxed{R_\Delta - EQ.}$$

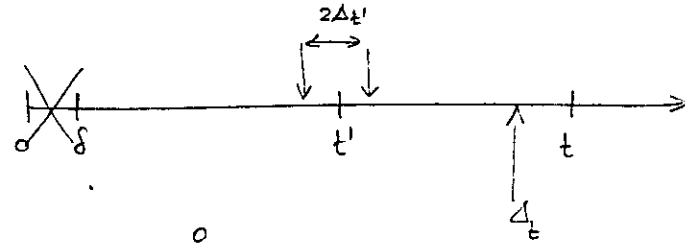
$$\begin{aligned} \frac{\partial R_\Delta(t, t')}{\partial t} = & -Z_\Delta R_\Delta(t, t') + \frac{p(p-1)}{2} \left(\frac{1-q_{\text{ex}}}{T} \right) R_\Delta(t, t') C_\Delta^{p-2}(t, t') \\ & + \frac{p}{2T} R_\Delta(t, t') (1-q_{\text{ex}}^{p-1}) + \\ & + \frac{p(p-1)}{2} \int_{\Delta_t \rightarrow t'}^{\Delta_t \rightarrow t'} ds R_\Delta(t, s) C_\Delta^{p-2}(t, s) R_\Delta(s, t') \end{aligned}$$

$$\boxed{C_\Delta - EQ.}$$

$$\begin{aligned} INT_1 &= \frac{p}{2} \int_0^{t'} ds C_\Delta^{p-1}(t, s) R(t', s) \\ &= \frac{p}{2} \left\{ \left(\int_0^\delta ds + \int_\delta^{\Delta_t} ds + \int_{\Delta_t}^{t'} ds \right) C_\Delta^{p-1}(t, s) R(t', s) \right\} \\ &= \frac{p}{2} \left\{ \int_0^{\Delta_t} ds C_\Delta^{p-1}(t, s) R_\Delta(t', s) + \int_{\Delta_t}^{t'} ds C_\Delta^{p-1}(t, s) R_F(t', s) \right\} \\ &= \frac{p}{2} \left\{ \int_0^{\Delta_t \rightarrow t'} ds C_\Delta^{p-1}(t, s) R_\Delta(t', s) + C_\Delta^{p-1}(t, t') \int_{\Delta_t}^{t'} ds R_F(t', s) \right\} \\ &= \frac{p}{2} \int_0^{t'} ds C_\Delta^{p-1}(t, s) R_\Delta(t', s) + C_\Delta^{p-1}(t, t') \frac{p}{2T} (1-q_{\text{ex}}) \end{aligned}$$



$$INT_2 = \frac{p(p-1)}{2} \int_0^t ds R(t, s) C_\Delta^{p-2}(t, s) C_\Delta(t', s)$$



$$\begin{aligned} &= \frac{p(p-1)}{2} \left\{ \int_0^\delta ds + \int_\delta^{t'-\Delta_t'} ds + \int_{t'-\Delta_t'}^{t'+\Delta_t'} ds + \int_{t'+\Delta_t'}^{\Delta_t} ds + \int_{\Delta_t}^t ds \right\} \\ &= \frac{p(p-1)}{2} \left\{ \int_0^{t'-\Delta_t'} ds R_\Delta(t, s) C_\Delta^{p-2}(t, s) C_\Delta(t', s) + \right. \\ &\quad + \int_{t'-\Delta_t'}^{t'+\Delta_t'} ds R_\Delta(t, s) C_\Delta^{p-2}(t, s) \left(C_F(t'-s) \right) + \cancel{C_\Delta(t'-s)} + C_\Delta(t') \\ &\quad + \int_{t'+\Delta_t'}^{\Delta_t} ds R_F(t, s) C_\Delta^{p-2}(t, s) C_\Delta(s, t') + \\ &\quad + \left. \int_{\Delta_t}^t ds R_F(t, s) C_\Delta^{p-2}(t, s) C_\Delta(s, t') \right\} \\ &\approx \frac{p(p-1)}{2} \left\{ \int_0^{\Delta_t} ds R_\Delta(t, s) C_\Delta^{p-2}(t, s) C_\Delta(t', s) + \right. \\ &\quad + \left. C_\Delta(t, t') \int_{\Delta_t}^t ds \frac{1}{T} \frac{\partial C_F(t-s)}{\partial s} C_F^{p-2}(t-s) \right\} \\ &= \frac{p(p-1)}{2} \int_0^{\Delta_t \rightarrow t} ds R_\Delta(t, s) C_\Delta^{p-2}(t, s) C_\Delta(t', s) + \frac{p}{2T} C_\Delta(t, t') \left[1 - \frac{p-1}{q_{\text{ex}}} \right] \end{aligned}$$

Finally, the C_A-eq reads:

$$\begin{aligned} \frac{\partial C_A(t,t')}{\partial t} = & -z_{00} C_A(t,t') + \frac{p}{2T} (1-q_{\text{EA}}) C_A^{p-1}(t,t') + \\ & + \frac{p}{2T} C_A(t,t') \left[1 - q_{\text{EA}}^{p-1} \right] + \\ & + \frac{p}{2} \int_0^{t+t'} ds C_A^{p-1}(t,s) R_A(t,s) + \\ & + \frac{p(p-1)}{2} \int_0^{t+t'} ds R_A(t,s) C_A^{p-2}(t,s) C_A(t,s) \end{aligned}$$

CHECK: (EXERCISE) IF $\frac{\partial C_A(t,t')}{\partial t} \ll \text{rhs}_C$ AND THEREFORE $\frac{\partial R_A(t,t')}{\partial t} \ll \text{rhs}_R$

THEN $R_A(t,t') = \frac{\chi}{T} \frac{\partial C_A(t,t')}{\partial t'}$ REDUCES THE SET OF EQS (R_A-EQ) - (C_A-EQ) TO A SINGLE ONE FOR C_A.

WE NOW HAVE 4-EQS (FOR C_F, R_F, C_A, R_A) WITH THE MATCHING CONDITIONS $C_F \rightarrow q_{\text{EA}}$ as $t, t' \rightarrow \infty$, ETC.

Let's try to find a sol

• WE START BY ANALYSING THE R_A-EQ

Let's assume $\frac{\partial R_A(t,t')}{\partial t} \ll \text{rhs}_R$ (TO BE VERIFIED POSTERIORI BY THE SOL) & THEN lhs_R VS rhs_R :
ALSO, REM THE NUMERICAL SOL $\Rightarrow$ THE 'VELOCITY' BECOMES SLOWER & SMALLER.

$$\begin{aligned} 0 \simeq & -z_{00} R_A(t,t') + \frac{p(p-1)}{2} \left(\frac{1-q_{\text{EA}}}{T} \right) R_A(t,t') C_A^{p-2}(t,t') - \\ & + \frac{p}{2T} R_A(t,t') \left(1 - q_{\text{EA}}^{p-1} \right) + \\ & + \frac{p(p-1)}{2} \int_{t'}^t ds R_A(t,s) C_A^{p-2}(t,s) R_A(s,t') \end{aligned}$$

CONSIDER NOW $\lim_{t' \rightarrow t} \dots$ REM $\lim_{t' \rightarrow t} C_A(t,t') = q_{\text{EA}}$

$$\begin{aligned} 0 \simeq & \left[-z_{00} + \frac{p(p-1)}{2} \left(\frac{1-q_{\text{EA}}}{T} \right) q_{\text{EA}}^{p-2} + \frac{p}{2T} (1 - q_{\text{EA}}^{p-1}) \right] R_A(t,t) \\ & \Downarrow \\ & \frac{p}{2T} \left((p-1) q_{\text{EA}}^{p-2} - (p-1) q_{\text{EA}}^{p-1} + 1 - q_{\text{EA}}^{p-1} \right) \\ & \frac{p}{2T} \left((p-1) q_{\text{EA}}^{p-2} - p q_{\text{EA}}^{p-1} + 1 \right) \end{aligned}$$

TWO SOLUTIONS = $\begin{cases} R_A = 0 \\ R_A \neq 0 \end{cases} \Leftrightarrow [] = 0 \rightarrow \begin{matrix} T > T_d \\ T < T_d \end{matrix}$

THE BRACKET $\Rightarrow \Rightarrow$ AN EQ. FOR (q_{FEA}, X, T)

LV (39)

ONE CAN DO THE SAME TRICK IN THE C_A -EQ

$$\lim_{t' \rightarrow E} C_A\text{-EQ} = \text{ANOTHER EQ FOR } (q_{\text{FEA}}, X, T)$$

COMPATIBILITY $\Rightarrow$

$$\frac{X}{T} = \frac{(p-2)(1-q_{\text{FEA}})}{q_{\text{FEA}} T} \rightarrow \text{EQ-X}$$

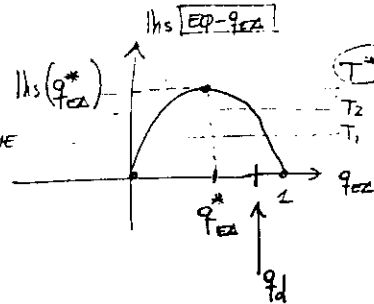
$$\frac{p(p-1)}{2} q_{\text{FEA}}^{p-2} (1-q_{\text{FEA}})^2 = T^2 \rightarrow \text{EQ-} q_{\text{FEA}}$$

(NB $\begin{cases} X=0 & p=2 \\ q_{\text{FEA}}=1-T & p \end{cases}$
OR, CAN BE OBTAINED SOLVING EXACTLY THE LENS-EQ

AND X IS $0 < X \leq 1$! (AS A FUNCTION OF T)

TRANSITION:

Let's look at $\text{EQ-} q_{\text{FEA}}$ $[p > 2]$
ONE WAY OF TRYING TO FIND A TRANS. IS TO STUDY WHEN $\text{EQ-} q_{\text{FEA}}$ DOES NOT HAVE A SOL.

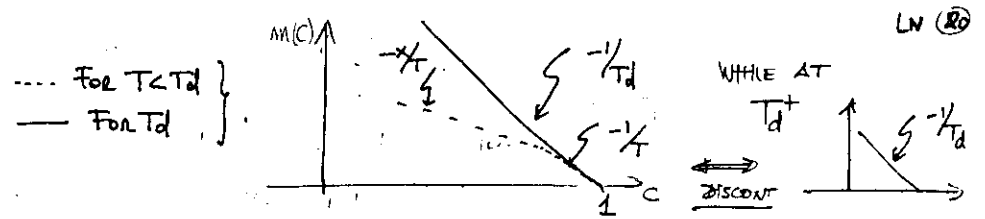


$$q_{\text{FEA}}^* = \frac{p-2}{p}$$

$$\text{lhs}(q_{\text{FEA}}^*) = \frac{2(p-1)(\frac{p-2}{p})^{p-2}}{p} = T^2 \rightarrow d$$

BUT $\frac{X(q_{\text{FEA}}^*)}{q_{\text{FEA}} T} = \frac{2(p-2)}{p^2} \frac{1}{T} > \frac{1}{T}$! WE DON'T LIKE $X > 1$.
(UNPROVEN, BUT WE THINK X MUST BE < 1) [FORMAL PROOF?]

THUS, THERE'S A TRANSITION BEFORE ARRIVING AT q_{FEA}^* , AT A GIVEN q_d , $q_{\text{FEA}}^* < q_d < 1$, AT WHICH $X=1$.



(COULD BE SEEN IN AN EXP...)

FINALLY SOLUTION. WE HAVE NOW (X, q_{FEA}) . LOOKING AT

C_A -EQ - R_A -EQ. ONE SEES THAT:

$$C_A(t, t') = f\left(\frac{h(t')}{h(t)}\right)$$

IS A SOLUTION. $\forall h(t)$. f IS DETERMINED BY THE APPROX. EQ (WHERE WE'VE THROWN $\frac{\partial C_A h(t')}{\partial t}$ WRT t) BUT $h(t)$ IS INDETERMINED.

MATCHING PROBLEM

OPEN.

WHAT DOES

$$R_A(t) = \frac{X}{T} \frac{\partial C_A(t)}{\partial t}$$

with: $C_A(t) = f\left(\frac{h(t)}{h(t_0)}\right)$

IMPLY FOR THE EXPERIMENTAL MEASUREMENTS?

A SIMPLE CALCULATION OF M^{TM} OR M^{ZFC}

YIELDS

NON-TRIVIAL AGING

IF $h(t) = \exp \ln^k(t/t_0)$ $\Rightarrow$

BACK TO LI & LAST FIGURE.

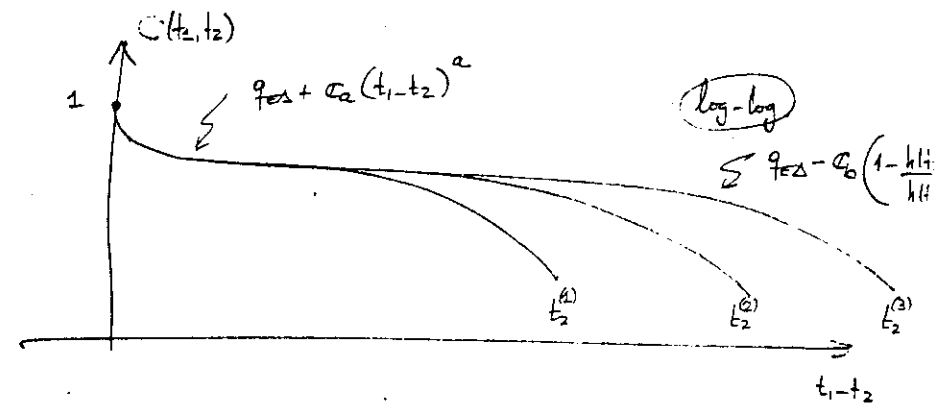
ACTUALLY, FOR THIS MODEL $h(t)$ IS MOST PROBABLY A POWER LAW (FROM NUMERICS). BUT ONE CAN CONSTRUCT OTHERS WHICH COULD LEAD TO

$$h(t) = \exp \ln^k(t/t_0)$$

SUMMARY

TCTd

FOR THE FAMILY OF MODELS



$a \geq b$ ARE THE LOW-T COUSINS OF (a,b) IN TSTD (REH MCT). BELOW T_d THEY DEPEND UPON T

