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Remote Sensing Techniques"
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1151-22

"Improvements of DOAS"

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Please note: These are preliminary notes intended for internal distribution only.

Improvements of DOAS

Differential Optical Absorption Spectroscopy

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Structure of the presentation

1.) Introduction

What is DOAS about ?

- **principles**
- **list of atmospheric absorbers**
- **absorbers versus wavelength**

2.) Typical questions related to instrumental outline

- **What is the proper spectral resolution ?**
- **What is the best spectral range ?**
- **What is the best light detector (S/N) ?**

3.) Some instrumental characteristics

- **Spectrometers (gratings, FT-IR) (dispersion, light throughput, stray light, etc.)**
- **Detectors (diode array, CCD, slit disks with PMT's) (spectral sensitivity, noise, etc.)**
- **Lights sources (lamps, diodes, laser, Sun, Moon, Stars)**

4.) Problems

- **Imaging (constant T, P's) illumination dependence and causes, sampling rate FWHM/pixel, etc. therapies**
 - **detector noise, linearity**
 - **spectrometer stray light**

5.) Improvements

- **non-linear spectral fitting**

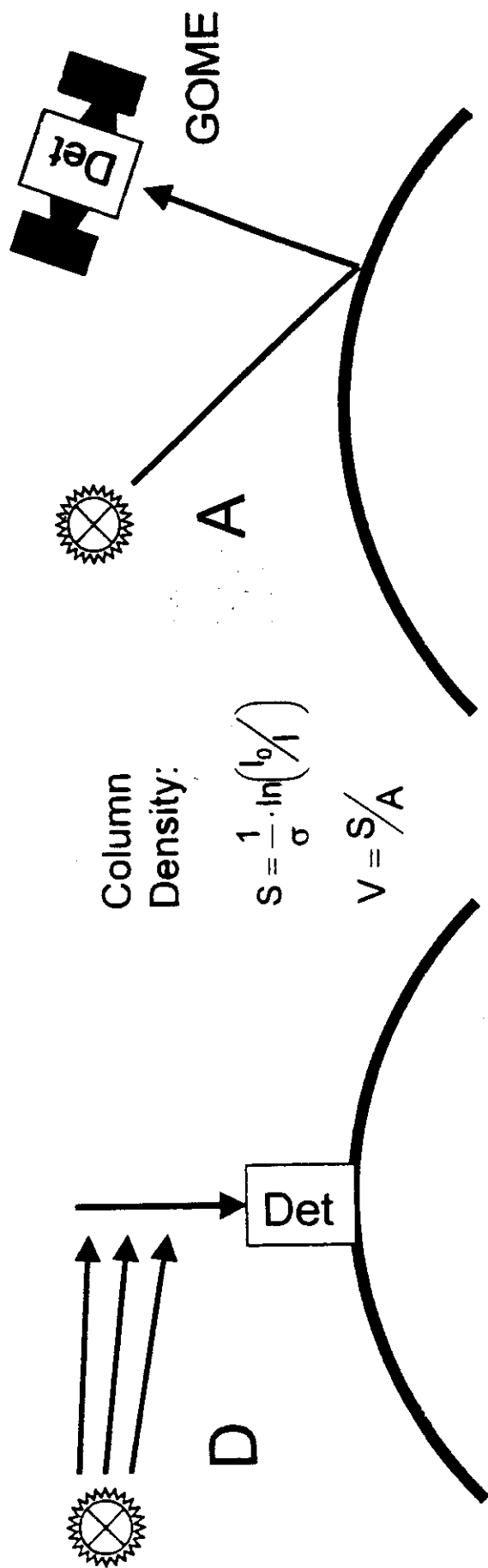
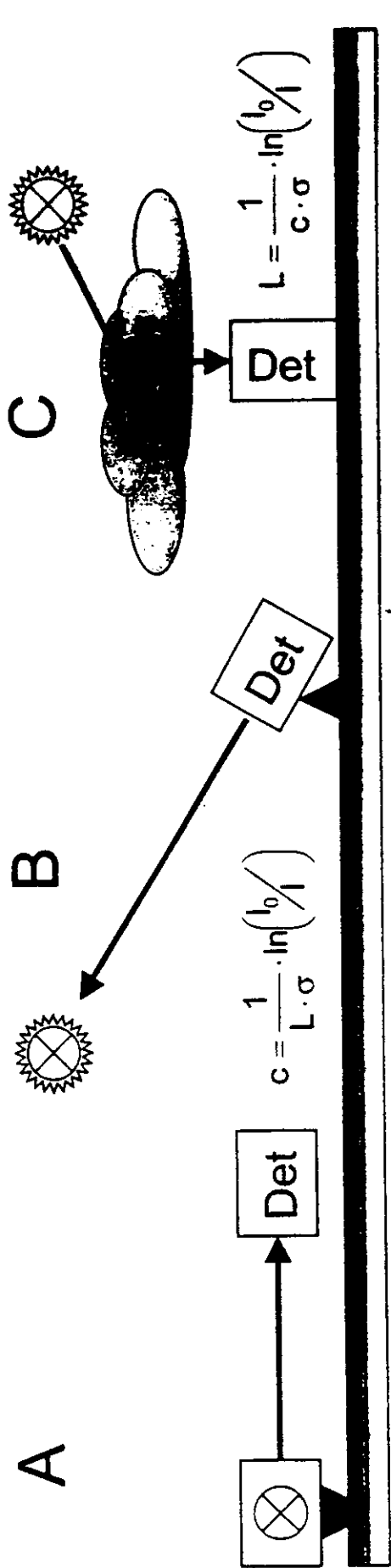
- **MCT - (Multi Channel Technique)**
- **Mode mixing**
- **etc.**

6.) Applications

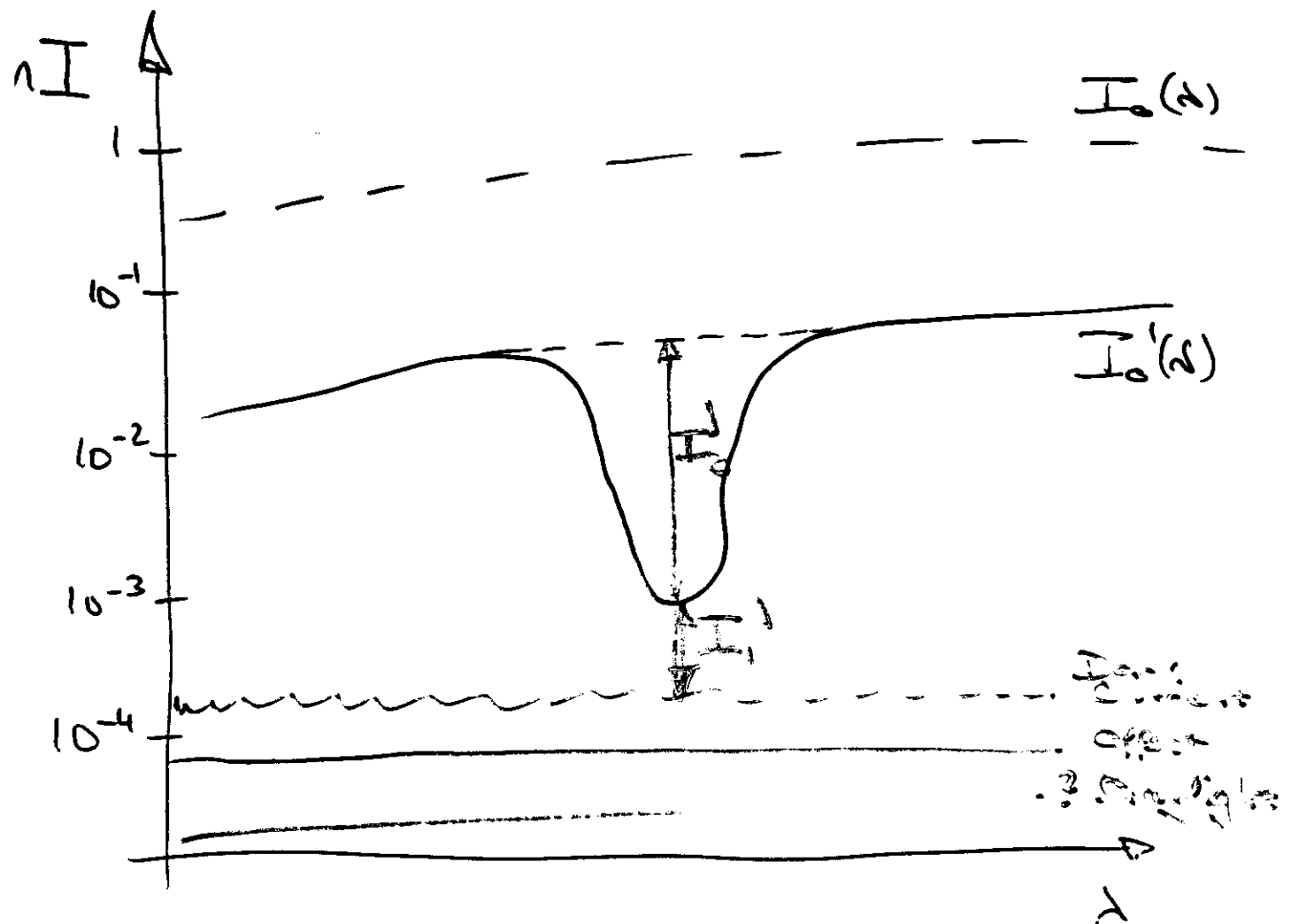
- **zenith, off axis skylight**
- **direct Sun, Moon, Stars**
- **long path absorption**
- **photon path length**
- **satellite (GOME)**

7.) Summary

8.) Literature



The DOAS Principle



Lambert Beer's Law

$$I(\lambda) = I_0(\lambda) \exp(-\sigma(\lambda) \cdot n \cdot l)$$

$\sigma(\lambda)$: cross section

n : gas density (absorber)

l : path length

$$I'(\lambda) = P(\lambda) \cdot I_0(\lambda)$$

$P(\lambda)$: broad band Extinction

$\propto \lambda^{-4}$ Rayleigh Scattering
 $\propto \lambda^{-2}$ Mie Scattering
 $\propto \lambda^{-4}$ broad band absorption

$$\epsilon(\lambda) = \epsilon'(\lambda) + \epsilon(\lambda)$$

Small $\nearrow$ $\epsilon'(\lambda)$ $\uparrow$ $\epsilon(\lambda)$ broad
 Band Absorption

$$I'(\lambda) = \underbrace{I_0(\lambda) \cdot (a\lambda^{-4} + b\lambda^{-2} + \dots)}_{\text{broad band}} \cdot \underbrace{\exp(-\epsilon'(\lambda) \cdot n \cdot l)}_{\text{small band}}$$

$$I'_1(\lambda) = I'_0(\lambda) \exp(-\epsilon'(\lambda) \cdot n \cdot l)$$

Differential Optical Density:

$$\| D' = - \ln \frac{I'_1(\lambda)}{I'_0(\lambda)} = \epsilon'(\lambda) \cdot n \cdot l \|$$

Errors in measured D'

Let ρ be an unknown contribution to the measured I_0' and I_1' i.e. due to

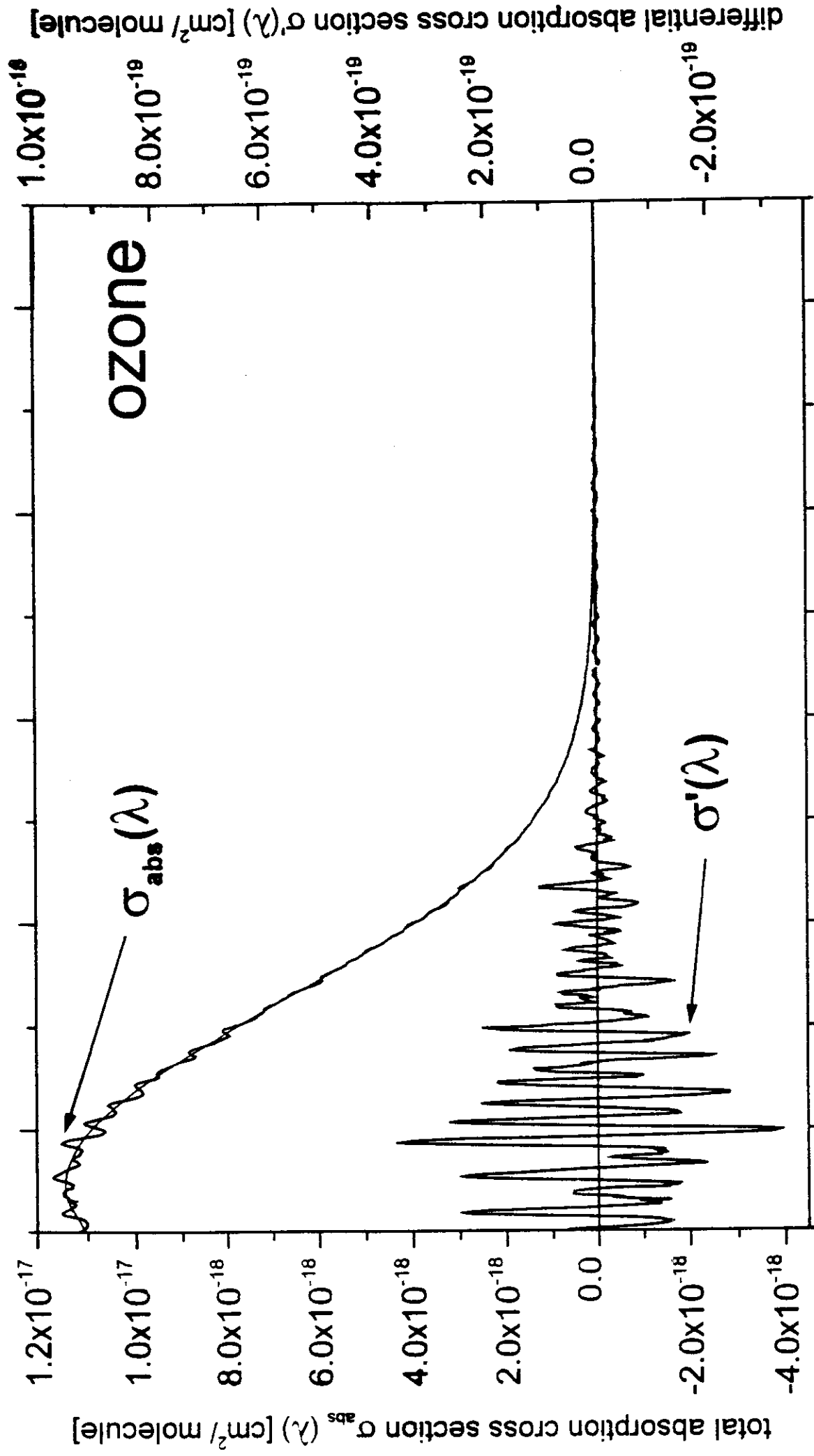
- (1) Noise in the dark current
- (2) electronic effect
- (3) stray light
- (4) etc.

$$D' = - \ln \frac{I_1'(x) + \rho}{I_0'(x) + \rho}$$

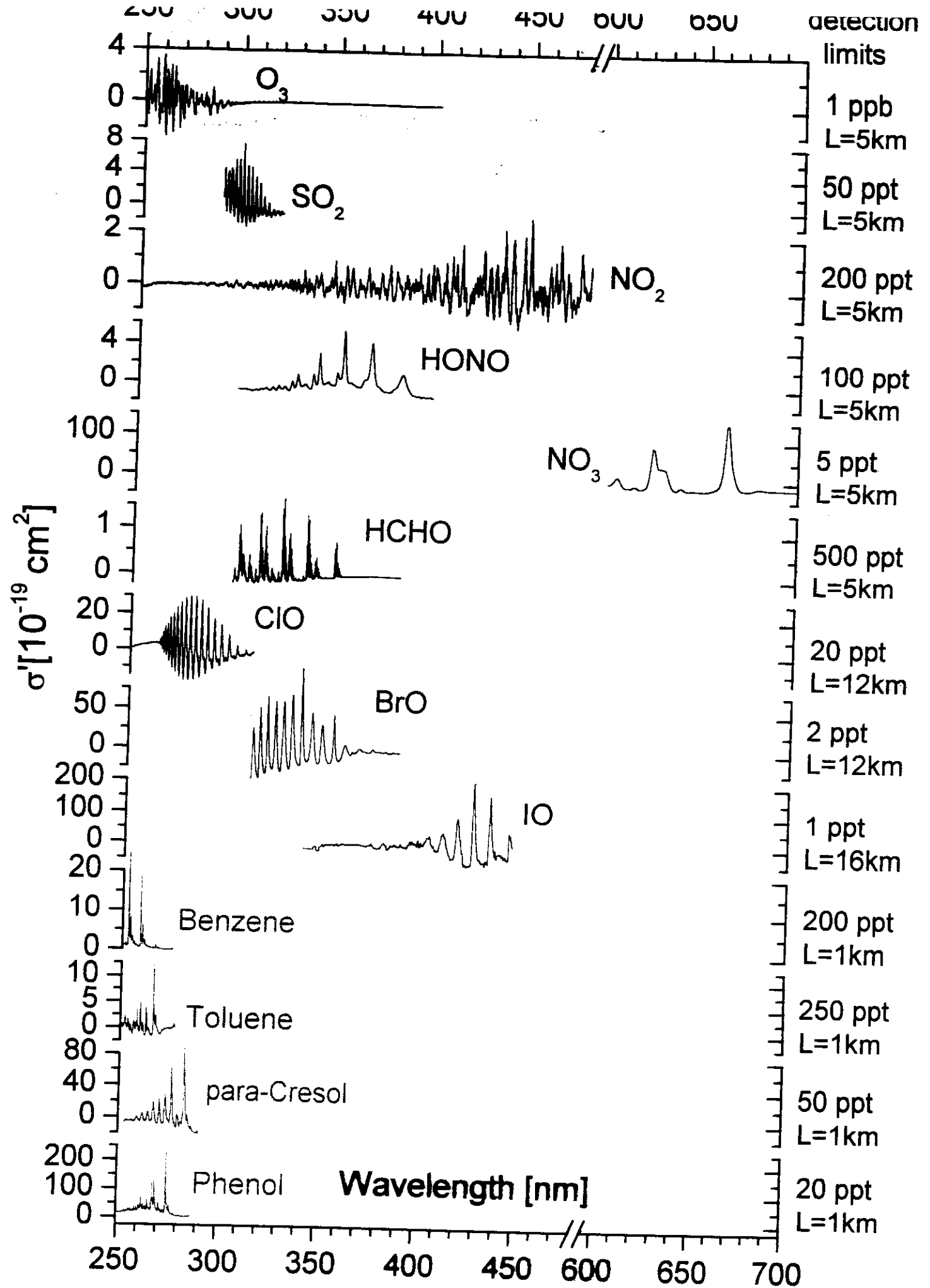
$$\Delta D = \left(\frac{I_1'}{I_1' + \rho} - \frac{I_0'}{I_0' + \rho} \right) \cdot \rho$$

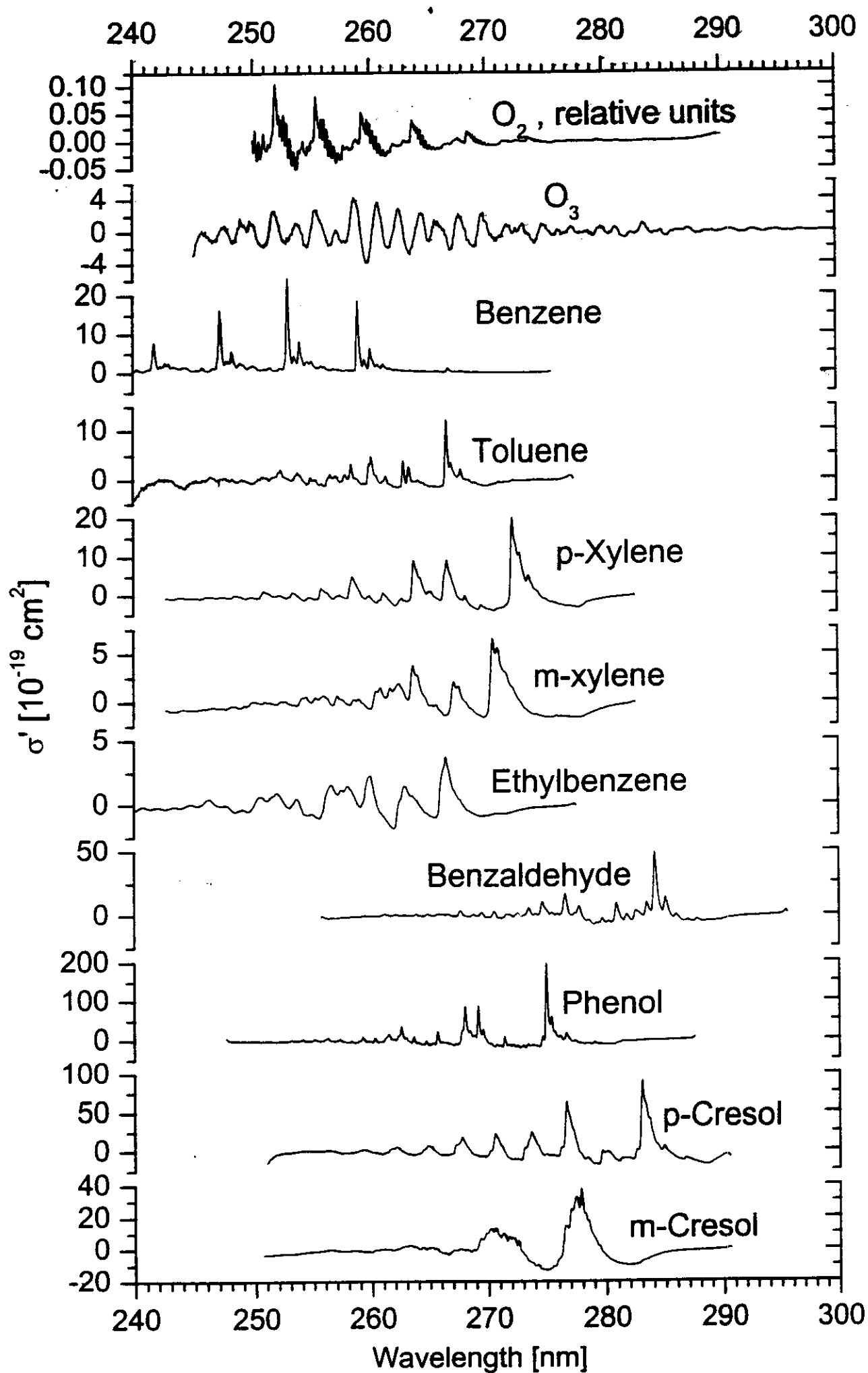
Error ΔD :

Problem: ~~Observations~~ observations may overlap and cover range of $D = \underbrace{1 \dots 10^{-4}}_{\text{dynamic range}}$



wavelength [nm]





Species measurable by UV/vis DOAS

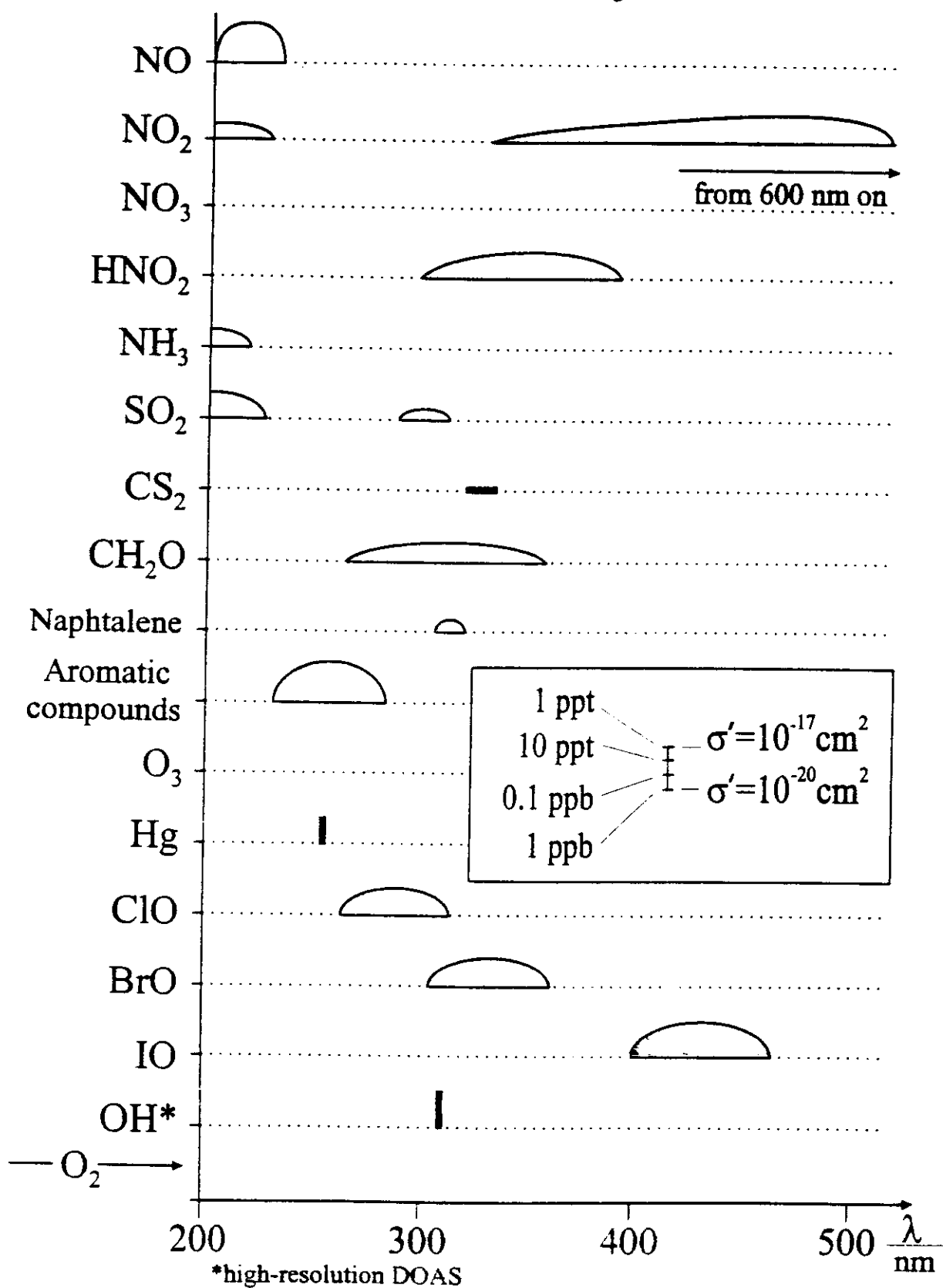
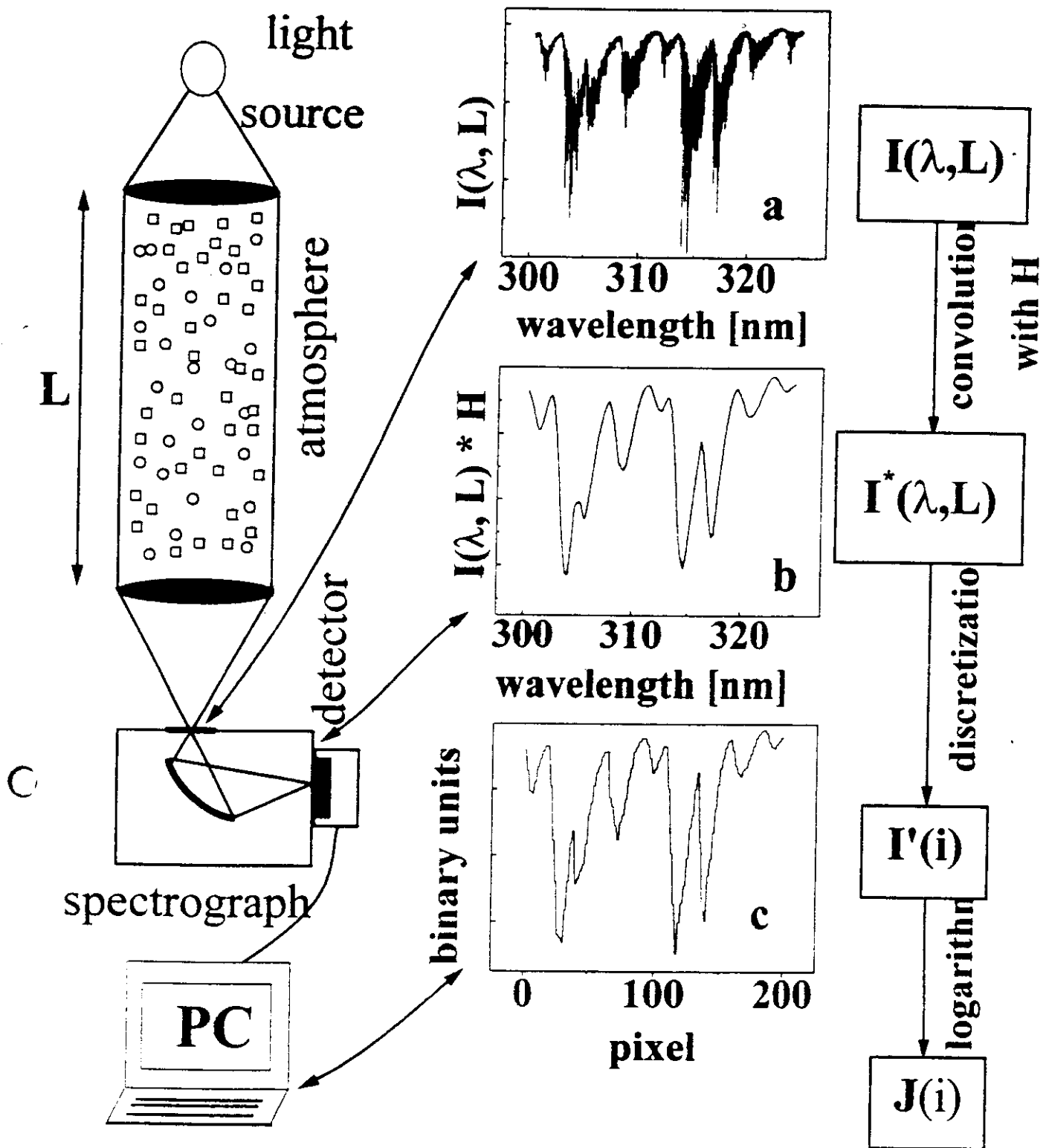


Table 1: Substances detectable by UV/visible absorption spectroscopy
Detection limits in ppt (1 ppt = 1 part in 10^{12})

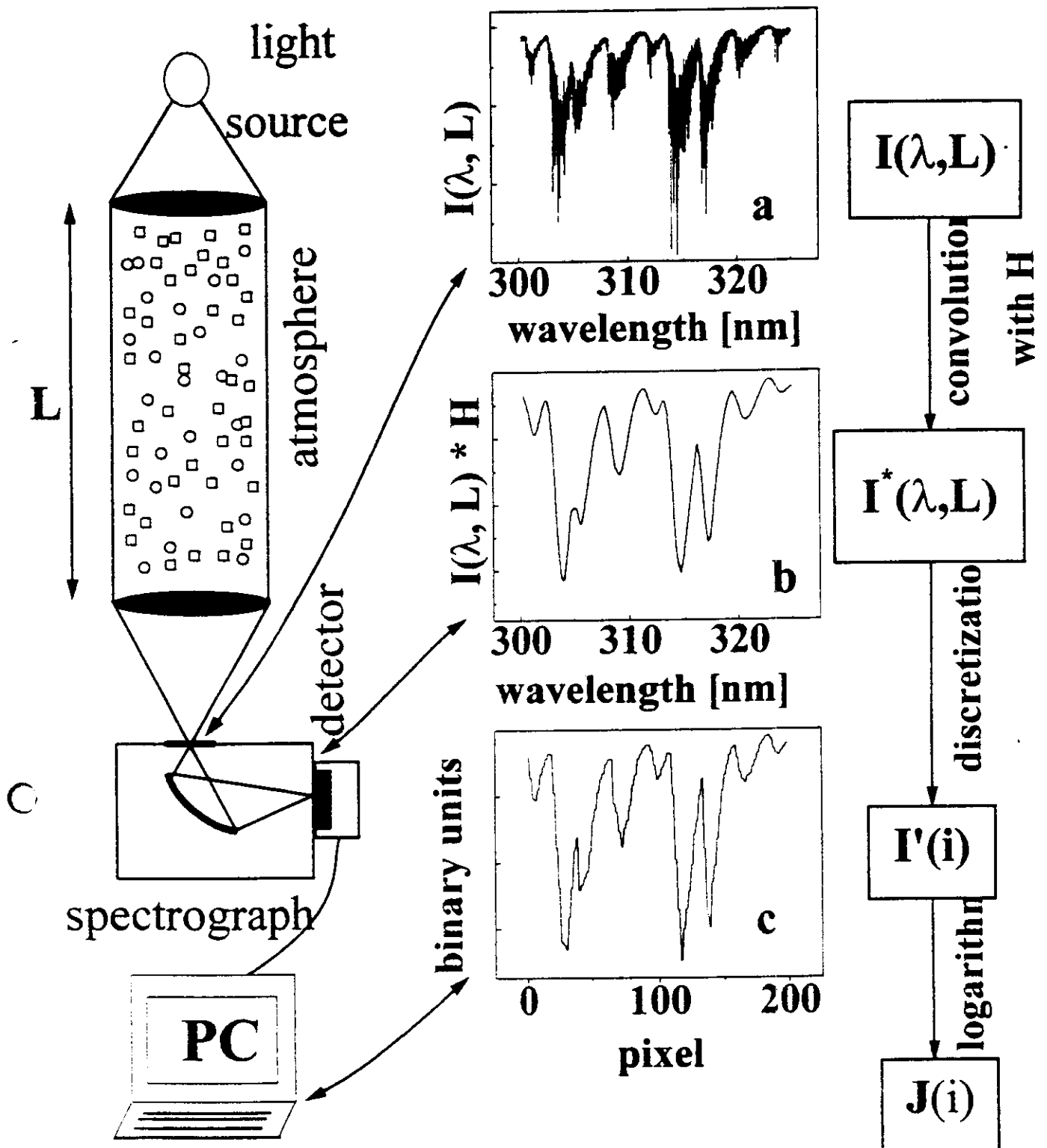
Species	Wavelength interval nm	Differential Absorption Cross section $10^{-19} \text{ cm}^2/\text{Molec.}$	Detection Limit (5km Lightpath) ppt
SO ₂	200-230	65	100 ^a
	290-310	5.7	35
CS ₂	320-340	0.4	500
NO	200-230	24	350 ^a
NO ₂	330-500	2.5	80
NO ₃	600-670	200	1
NH ₃	200-230	180	40 ^a
HNO ₂	330-380	5.1	40
O ₃	300-330	0.045	4000
CH ₂ O	300-360	0.48	400
ClO	260-300	35	6
BrO	300-360	104	2
IO	400-470	170	1
Benzene	240-270?	21.9	400 ^a
Toluene	250-280?	12.8	660 ^a
Xylene (o/m/p) ^b	250-280?	2.1/6.6/20.3	4000/1300/420 ^a
Phenol	260-290?	198	40 ^a
Cresol (o/m/p)		20.1/31.8/87.2	420/270/100 ^a
Benzaldehyde	280-290?	44	200 ^a

a 500m Light path, 0.001 minimum detectable optical density

Principle steps in DOAS Spectrometry



Principle steps in DOAS Spectrometry



How to choose the best spectrometer for the desired application ?

Some Criteria:

1.) What is the typical line width of the absorbers under consideration and what is the required spectral resolution ?

- vibrational lines (0.1 nm to several nm)
- rotational line (several 10^{-3} nm)

Answer: A good choice allows for a sampling of at least 6 data points per full width at half maximum (FWHM) !

2.) What is the light throughput ($TP = A/f^2$) of the required spectrometer ?

(A pupil area and f the spectrometer's f-number)

Answer: The f-number usually increases with decreasing FWHM, hence the TP decreases. Increasing A, i.e. the area of the slit, causes a increase in the FWHM. Hence a cost effective compromise allows for sufficient large A's and small f numbers !

3.) How is the stability of the spectrometer with respect to changing ambient conditions (changes in T, and P) (is that important at all) ?

(an issue addressed in detailed later !)

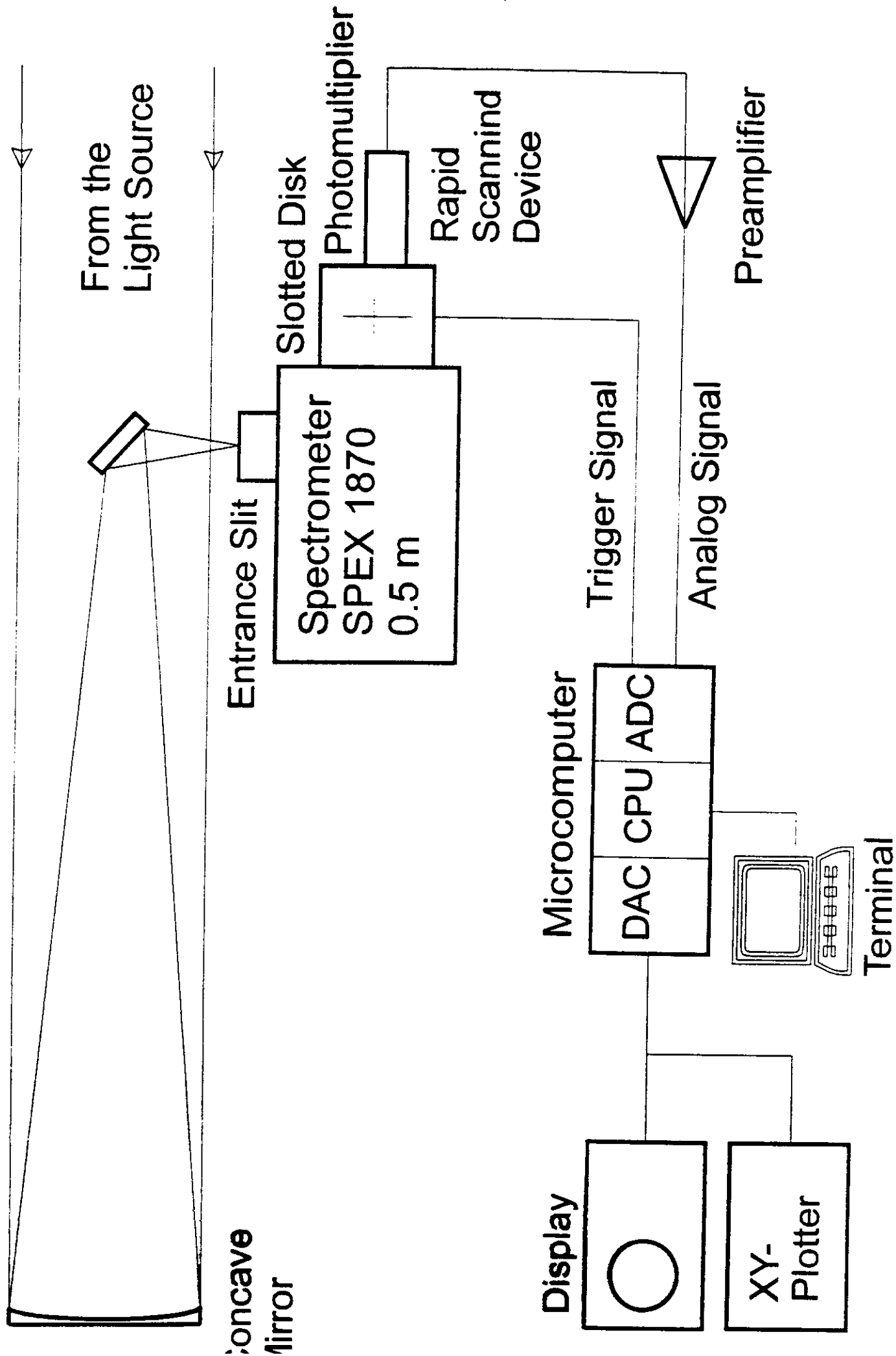
4.) How large is the spectrometer stray light ?

(an issue addressed in detailed later !)

Possible solutions

- FT spectrometer allow for a very high resolution, are very stable respect to the wavelength registration, but tend to use only a small fraction of the light (only the interfering photons) and are not very stable when not operated at constant T and P.
- Grating spectrometers are easy to be operated at constant T and P.
- Both spectrometers do have problems with stray light but FT-spectrometers usually do not process strayed photons.
- FT spectrometer's are much more expensive than grating spectrometer's.

Answer: By far, most DOAS measurements are performed with grating spectrometers !



I. INTRODUCTION

The Digikrom 240 is a classical Czerny-Turner monochromator in its optical configuration, with a 240mm focal length.

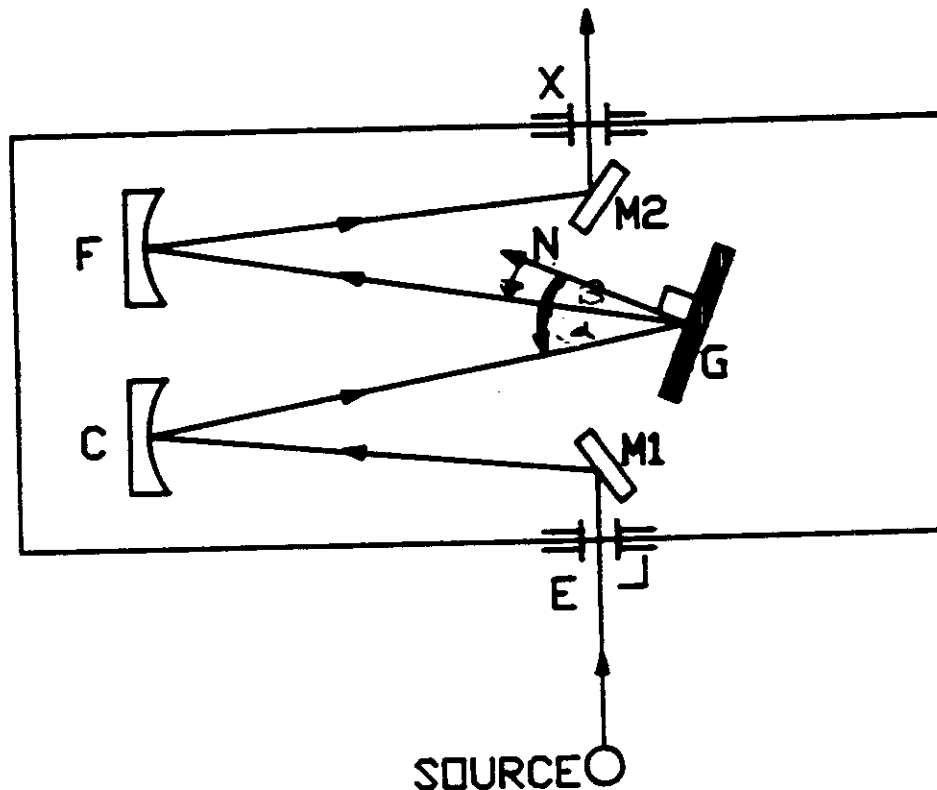


Figure 1. Optical Diagram of Digikrom 240

As indicated in Fig. 1, light from a source is focused on the entrance slit, E, and directed by the turning mirror, M1, to the collimating mirror, C. The focused beam is collimated and directed to the grating, G, which diffracts and reflects the radiation. A particular wavelength of the light, determined by rotation of the grating, is directed to the focusing mirror, F, which focuses it onto the exit slit, X, via the second turning mirror, M2.

Optical baffles are utilized to minimize stray light due to scattering from slit edges and dust or imperfections in the optical elements.

Gratings

■ Positive interferences?

$$d \sin \alpha + d \sin \beta = \frac{k \cdot d}{n} = k \cdot n \cdot d !$$

d : wave length

k : order $0 \pm 1 \pm 2 \dots$

n : number of grooves per unit length

■ Resolution:

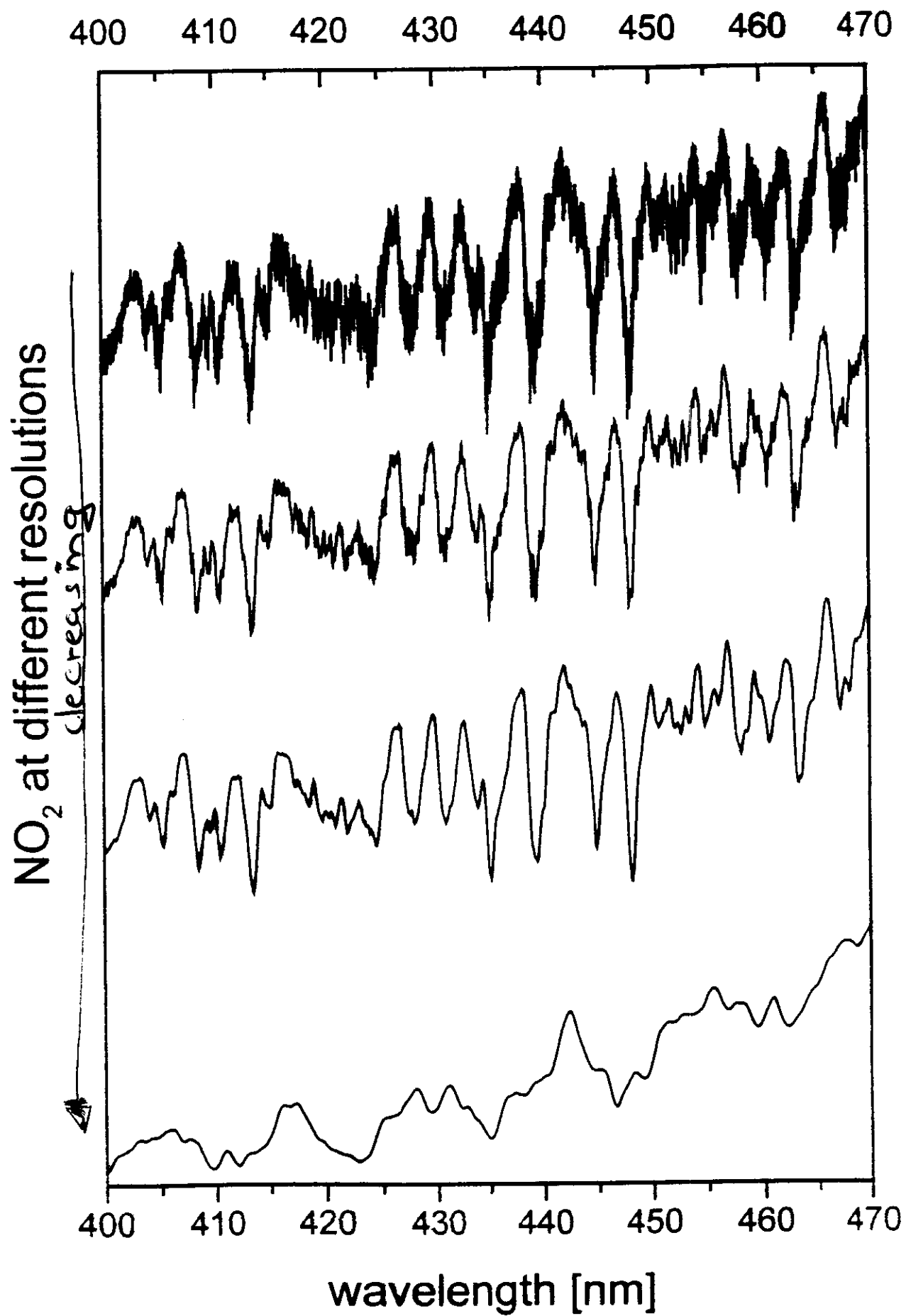
$$\frac{\Delta \lambda}{\lambda} = k \cdot N !$$

■ Dispersion:

$$\frac{d\beta}{d\lambda} = \frac{1}{d} \cdot \frac{d \sin \alpha + d \sin \beta}{\cos \beta} !$$

$$\text{or } \frac{dd}{dx} = \frac{\cos \beta}{k \cdot n \cdot f} !$$

f : Focal length



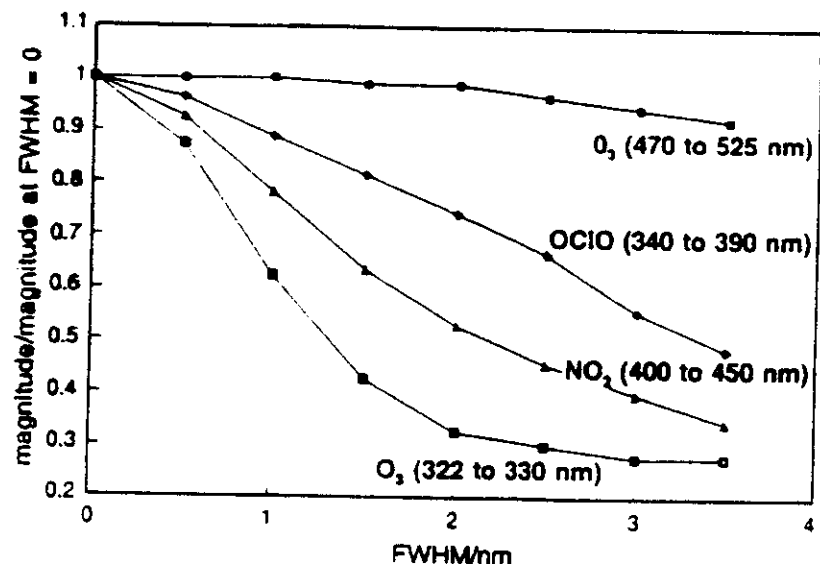


Fig. 10. Ratio of the average magnitude of differential cross sections of O₃, NO₂, and OCIO, after smoothing with Gaussian functions, to those at high resolution. This magnitude is proportional to the amount of signal available for spectral analysis. Except for UV measurements of O₃, smoothing must reach 1 nm FWHM before the magnitude is reduced by 1/4.

Rescoe et al (1996)
Appl. Optics 35, 427

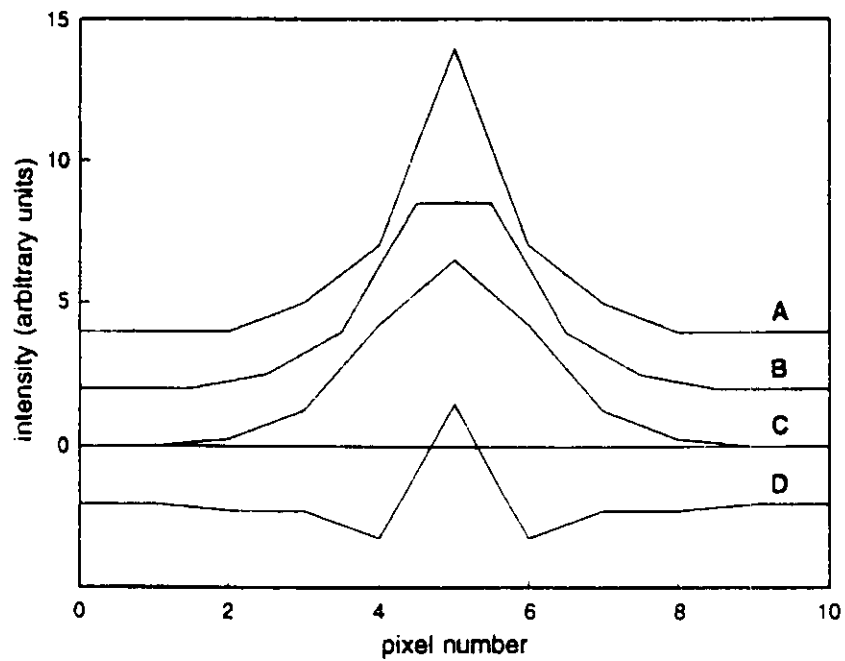


Fig. 1. Illustration of how the initial spectrum of a single Gaussian line (curve A) is degraded through two successive linear interpolations (curves B and C) to a much broader spectrum. The difference between curves A and C (i.e., the residual after interpolation) is plotted as curve D. In each case, the values at each pixel are joined by straight lines to illustrate linear interpolation. The curves are vertically displaced by 2 units for clarity.

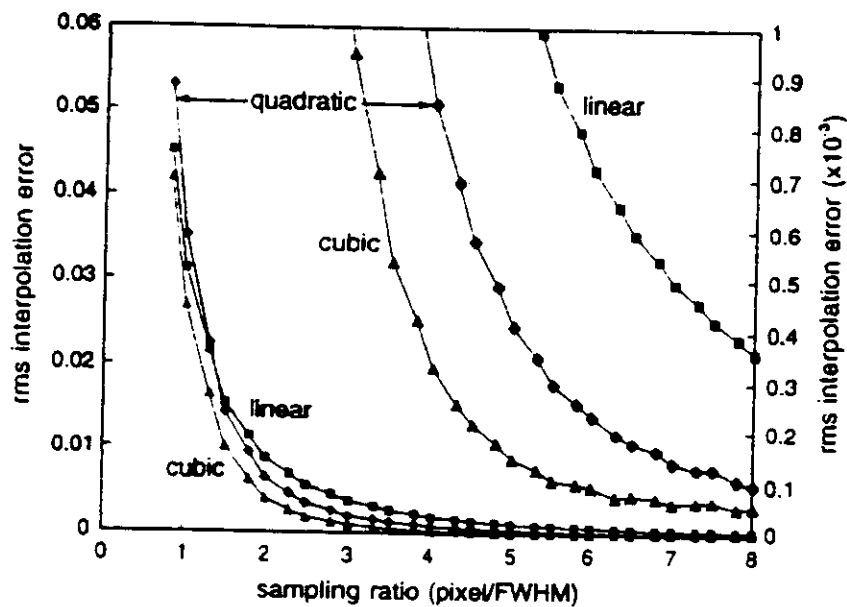
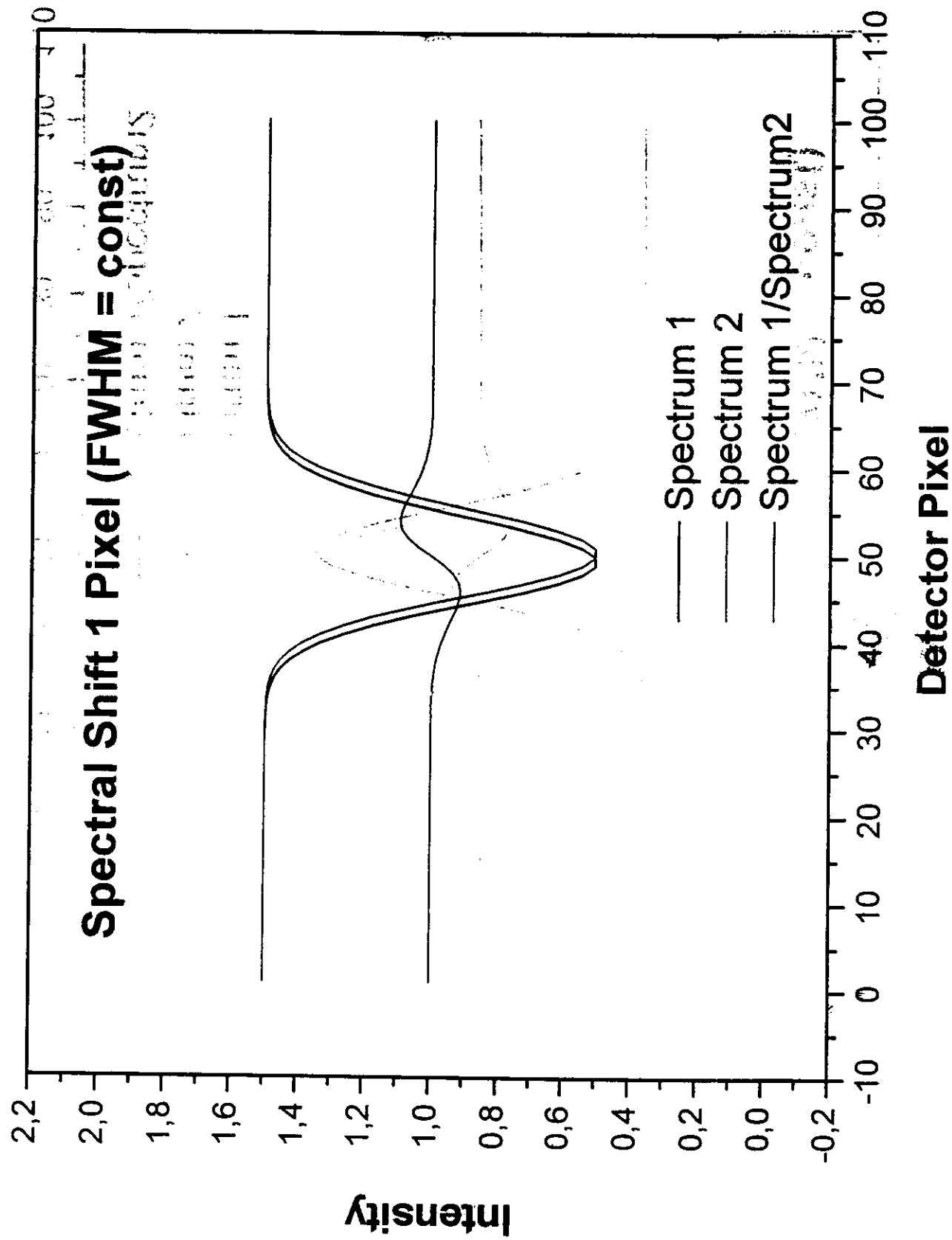


Fig. 3. Root-mean-square interpolation error for linear, quadratic, and cubic interpolation schemes as the number of pixels in each FWHM, commonly called the sampling ratio, increases. The errors shown are for a shift of 0.5 pixels, hence they are the maximum errors. A Gaussian slit function was used. The curves are expanded on the right-hand y axis. Note that the scale for errors is arbitrary relative to those of a real spectrum.

Reswe et al (1996)
 App. Optics 35; 427



Imaging

The spectrometer imaging may change with changing atmospheric/lab pressure (P) and (T). This is because $\Delta n/n = 2.7 \cdot 10^{-4}$ (n refraction index) for a $\Delta p = 1$ atm, and likewise ΔT 's cause thermal expansions of the optical setup.

Changing T's and P' causes imaging two effects:

- (a) Resolution (FWHM) changes due to a change (ΔL) in the focal length:

$(n - 1) \cdot L = \Delta L$, i.e., for $L = 30$ cm and $\Delta p = 1$ atm

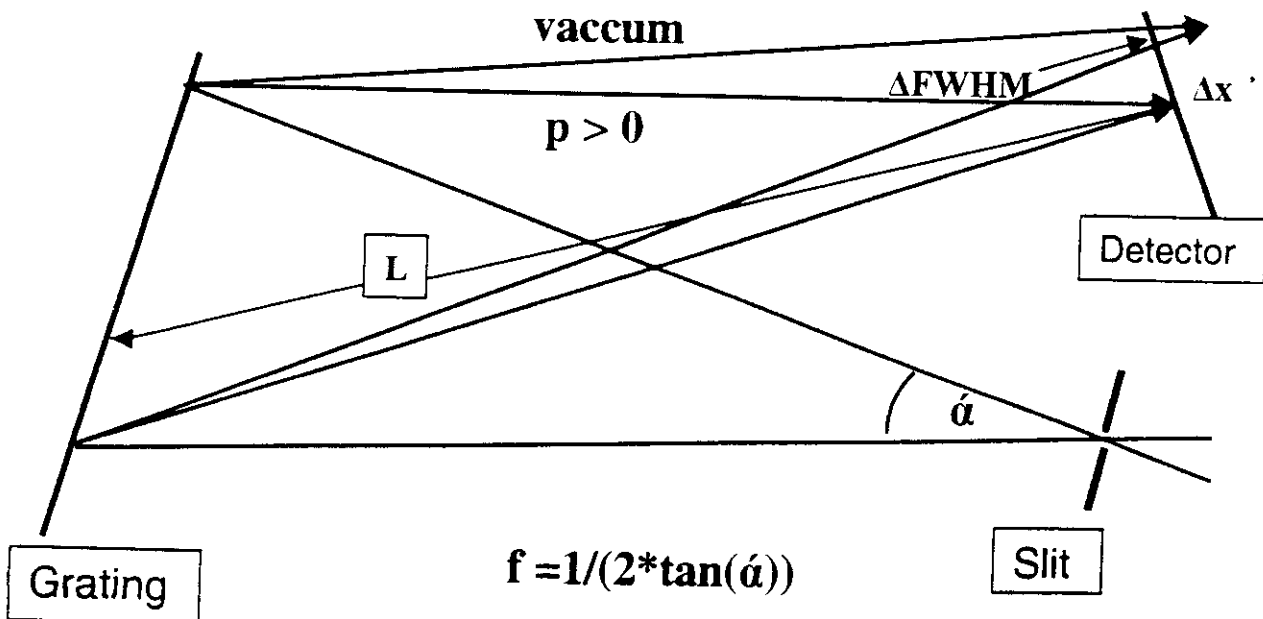
$$\Delta L = 80 \mu\text{m}$$

$\Delta \text{FWHM} = \Delta L / f\text{-number}$, i.e., by assuming $f/3$

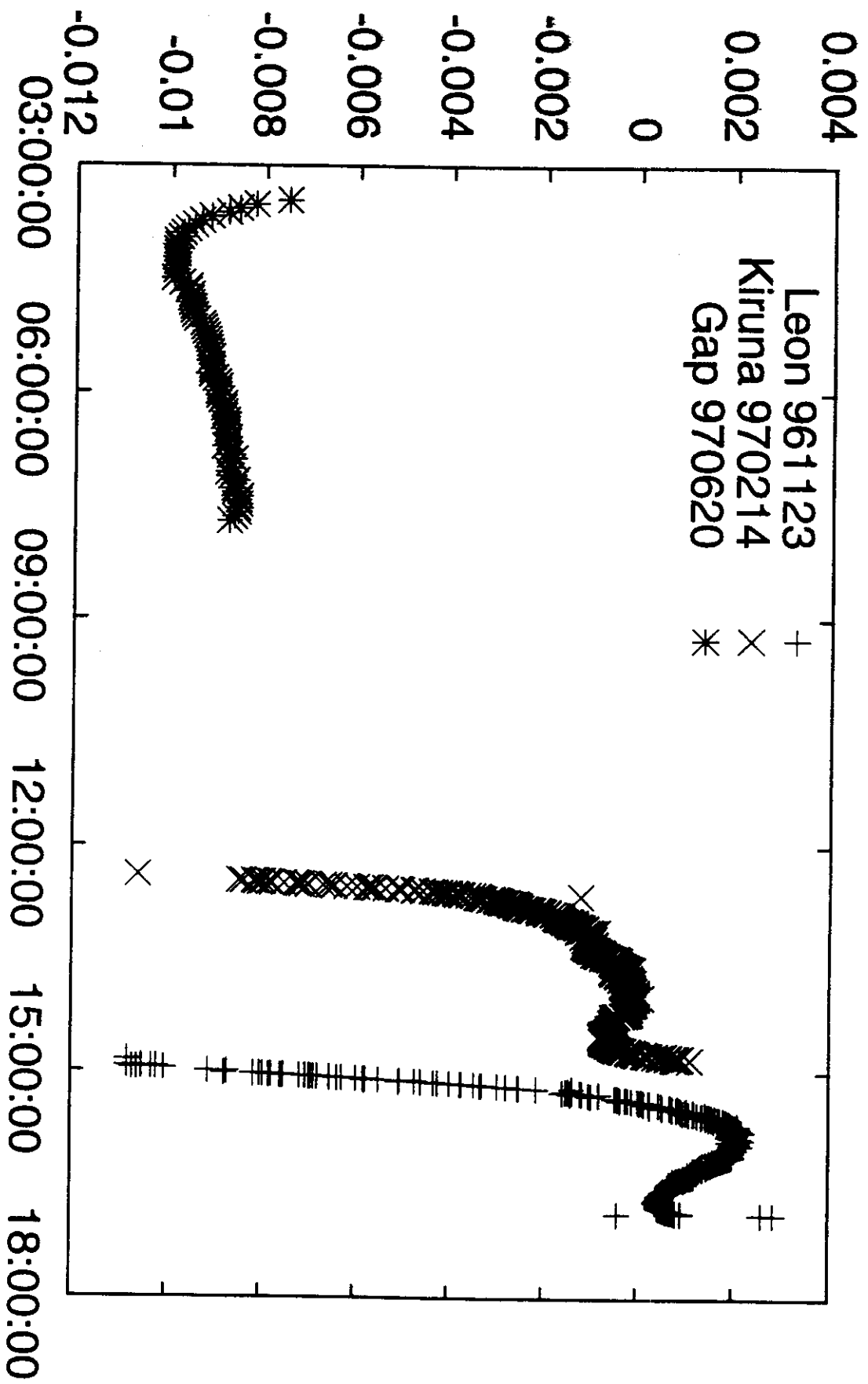
$$\Delta \text{FWHM} = 24.2 \mu\text{m}$$

- (b) Spectral Shift:

$\Delta \lambda / \lambda = \Delta n / n = 2.7 \cdot 10^{-4}$ or $\Delta x = 0.16$ nm at $\lambda = 430$ nm.



Shift UV-spectrograph [nm]



UT

Effect of Shifting the Fraunhofer Reference Spectrum

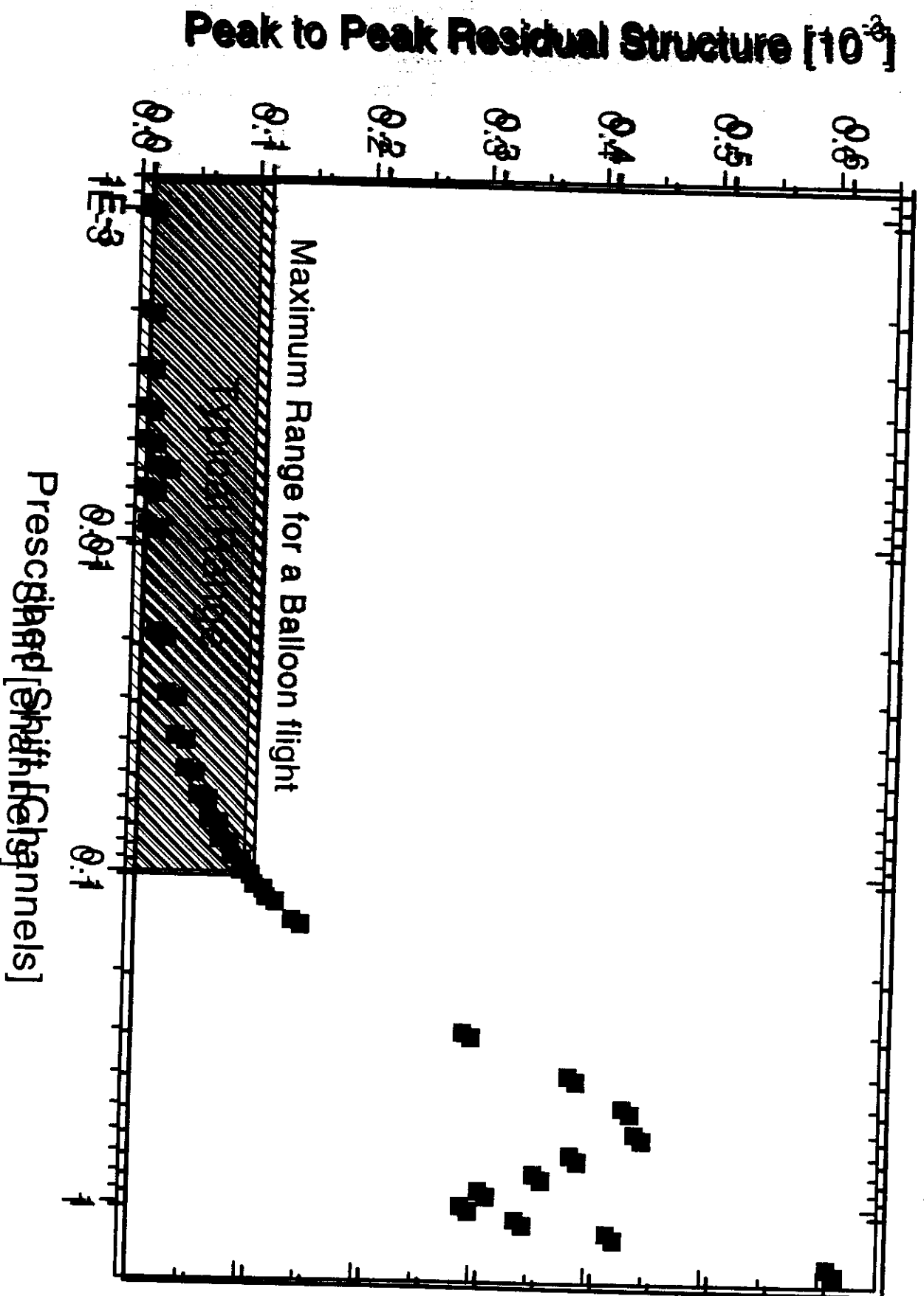
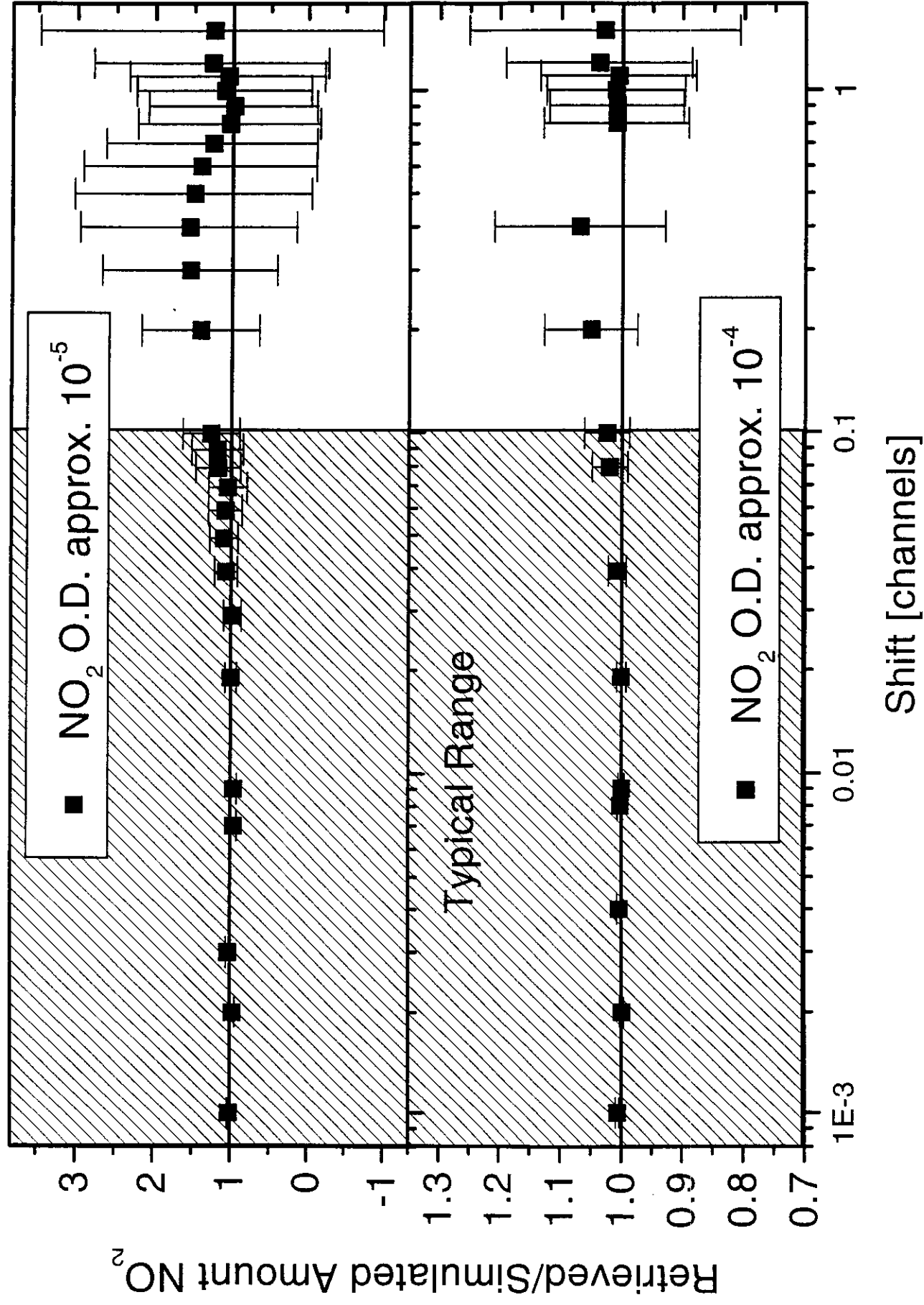
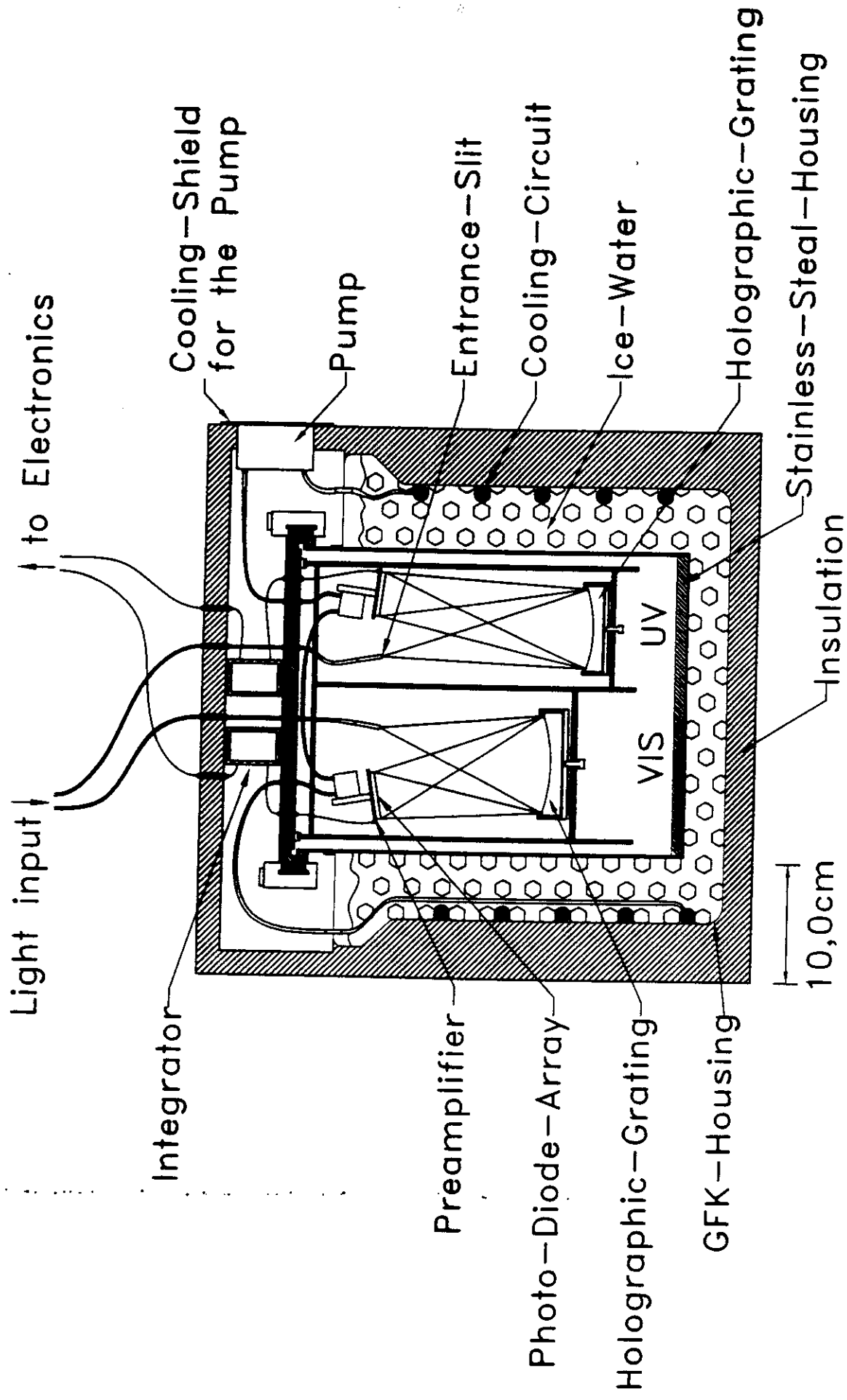


Fig. 34

Influence of Interpolation on Retrieval





Ferlemaun et al,
 Ann Optics (in press)

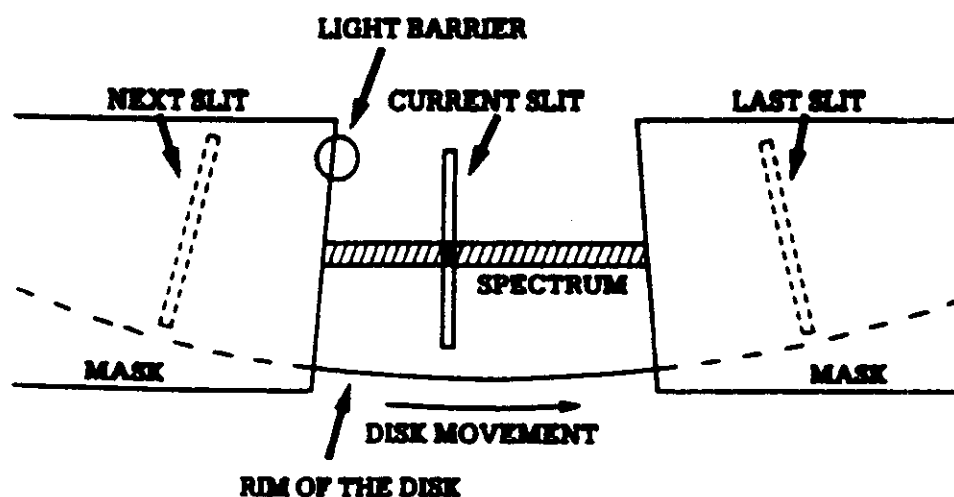


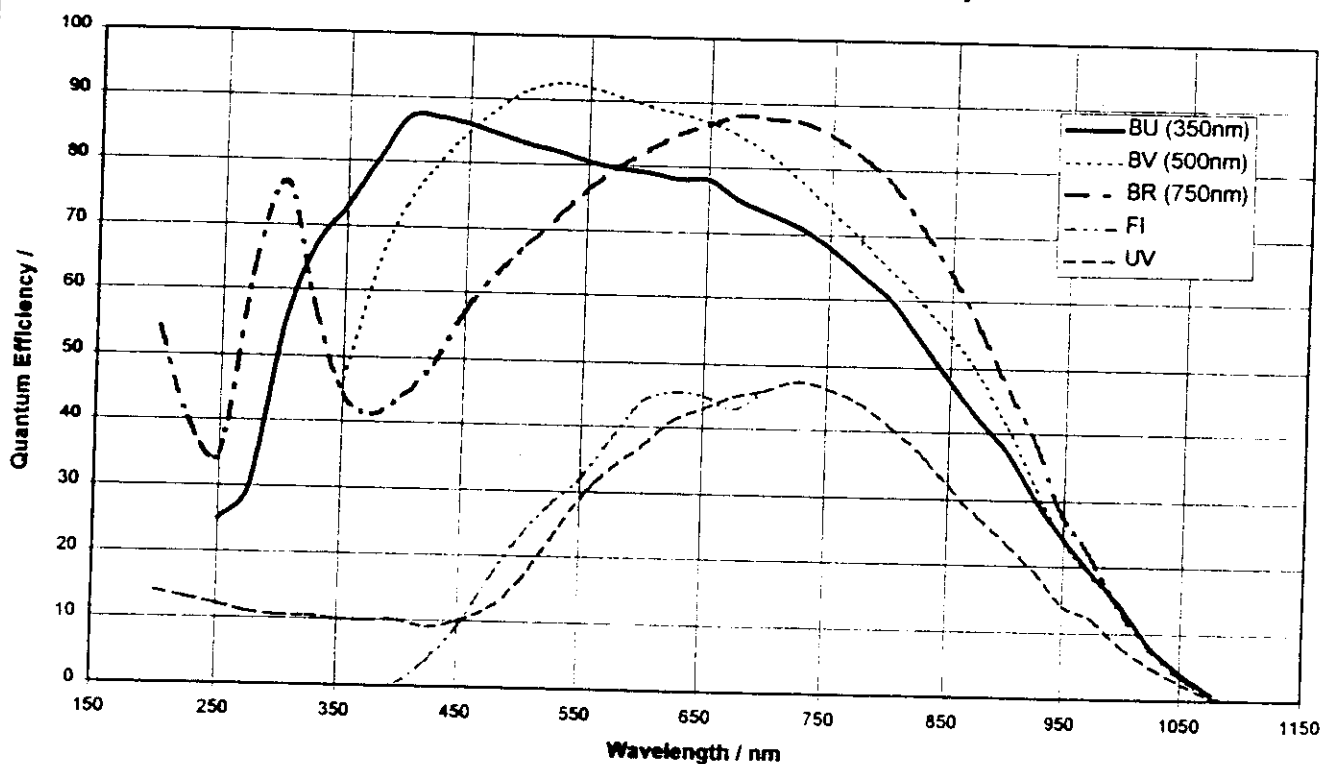
Figure 2.11. Optomechanical rapid scanning device. At any given moment one of the radial slits etched into a thin metal disk ("slotted disk") rotating in the focal plane of the spectrometer acts as an exit slit sweeping over the spectrum. A photomultiplier receives the portion of the spectrum falling through that slit.

CCD Specifications	
Pixels	2048 x 512, 13.5 μm^2
Pixel Well depth	Typical 150,000 e^-
Readout Register Well Depth	600,000 e^-
Node Well Depth (Low Noise) $\#1$	300,000 e^-
Node Well Depth (High Signal) $\#1$	900,000 e^-

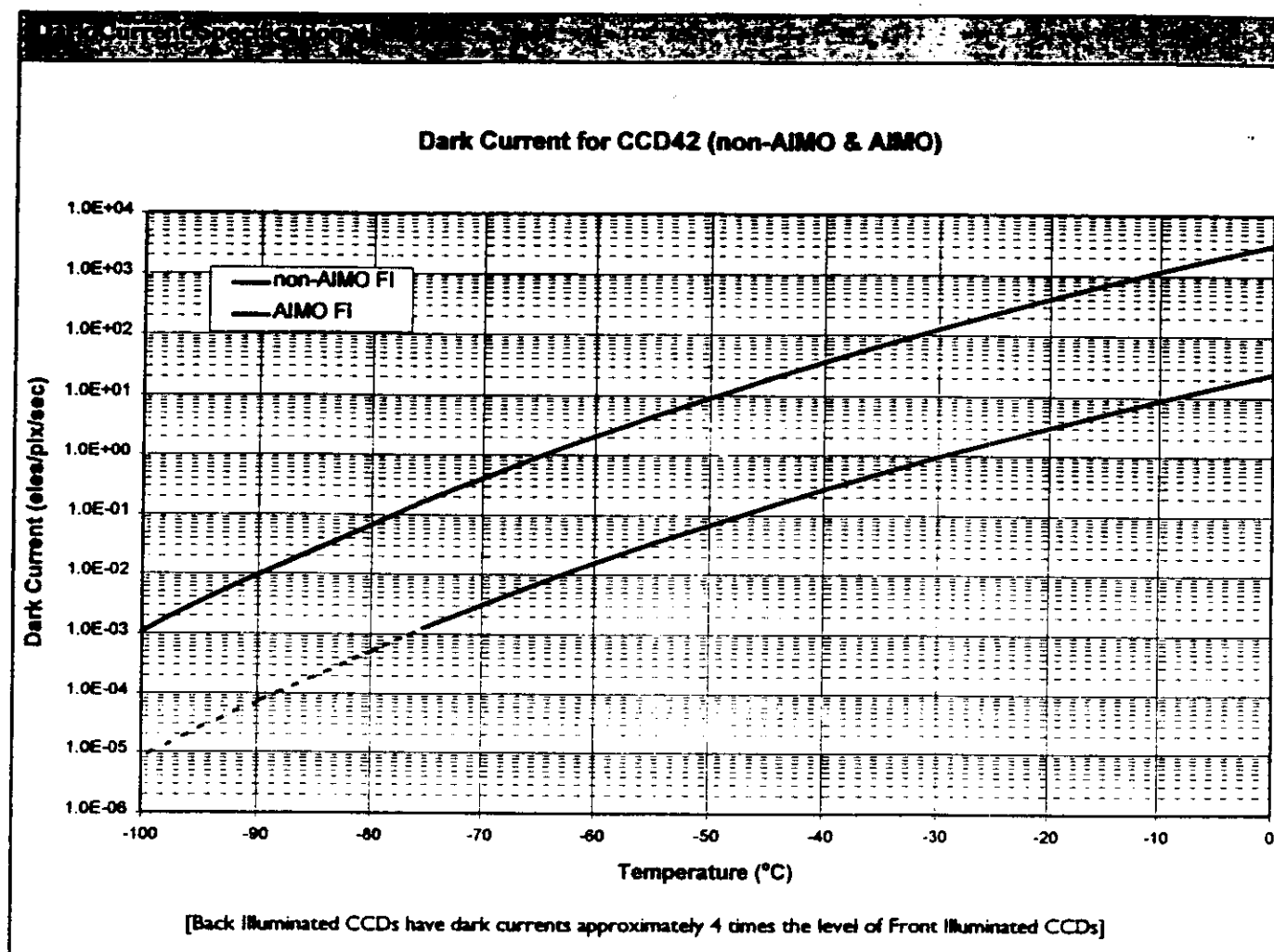
Readout Noise Specifications		
CCD Readout Noise $\#2$	2 electrons @ 20 kHz	6 electrons @ 1MHz

Response Specifications	
-------------------------	--

Quantum Efficiency for CCD's at Room Temperature



	Minimum	Typical	Maximum
Peak Quantum Efficiency $\#3$ FI [BI]	40% [78%]	47% [85%]	
Linearity $\#4$			1%



Performance Specification #6	Spectroscopic Mode #7		Image Mode #8	
	Front Illuminated	Back Illuminated	Front Illuminated	Back Illuminated
Dark Current	0 columns	1 columns #9	30 spots #10	30 spots
Response	2 columns	2 columns #11	80 spots #12	80 spots
	over 10 % contrast	over 10 % contrast	>25% contrast	>25% contrast
	2 traps	2 traps #13		
	over 200 electrons	over 200 electrons		
	Minimum separation between column defects is 50 pixels			

DIFFERENTIAL OPTICAL ABSORPTION SPECTROSCOPY

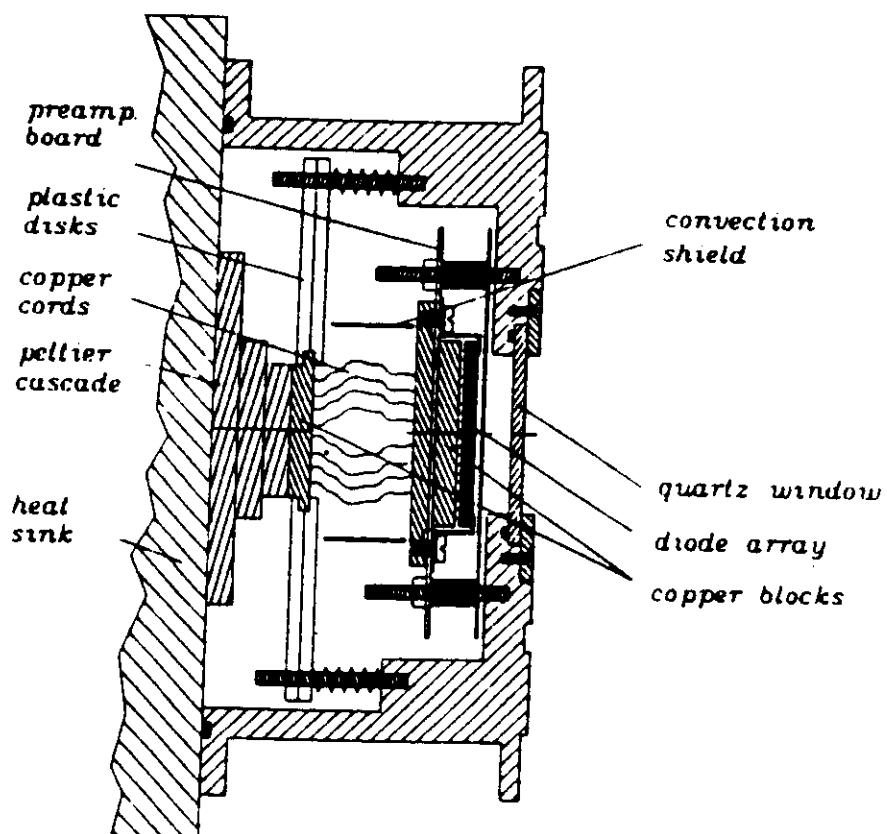


Figure 2.12. Cross section of a solid state photodetector (photodiode array). An air-cooled three-state Peltier device allows cooling to about -40°C . Adapted from Stutz and Platt (1992).

Detector Noise:

a.) Photon Shot Noise N_{ph} (Poisson statistics)

$$N_{ph} = \sqrt{S} = \sqrt{C_{diode} * U * \dot{\alpha} / e^-} = 10^4 e^-$$

With signal ($S * \dot{\alpha} = 10^8$ photons), diode or full well capacity ($C_{diode} = 10$ pF), voltage ($U = 2.06$ V), e^- electron charge, saturation ($\dot{\alpha} = 0.8$)

b.) Dark Current Noise N_{dark} (manufacturing dependent, for Hamamatsu S5931)

$$N_{dark} = \sqrt{S_{dark}} = 8296 e^- / \text{sec}$$

c.) Preamplifier Noise (N_{pre})

$$N_{pre} = 1/ e^- \sqrt{(i_n * t_n)^2 + (u_n * C_t)^2} = 249 e^-$$

For current and voltage noises ($i_n = 3.5 * 10^{-13}$ A - for OPA 627 - and $u_n = 1 * 10^{-6}$ V and for a read out time (t_n) (or bandwidth) of 20 μsec

d.) Read-out Noise (N_{read})

$$N_{read} = 1/ e^- \sqrt{k * T * (2 * C_{diode} + C_{vc})} = 4124 e^-$$

with cross talk capacity ($C_{\text{vc}} = 20 \text{ pF}$), k Boltzmann Constant and T temperature

e.) ADC Noise (N_{ADC})

$$N_{\text{ADC}} = 2694 \text{ e}^-$$

Total Noise (N_{read})

$$\underline{N_{\text{total}} = 10983 \text{ e}^- \text{ or } 5.3 \text{ binary Units}}$$

(for a 16 bit AD converter with the given numbers above)

Questions:

- (1) What is the determining noise contribution.
- (2) How can you measure it ?
- (3) How can you reduce ?

7.) DOAS Bibliography, August 1999

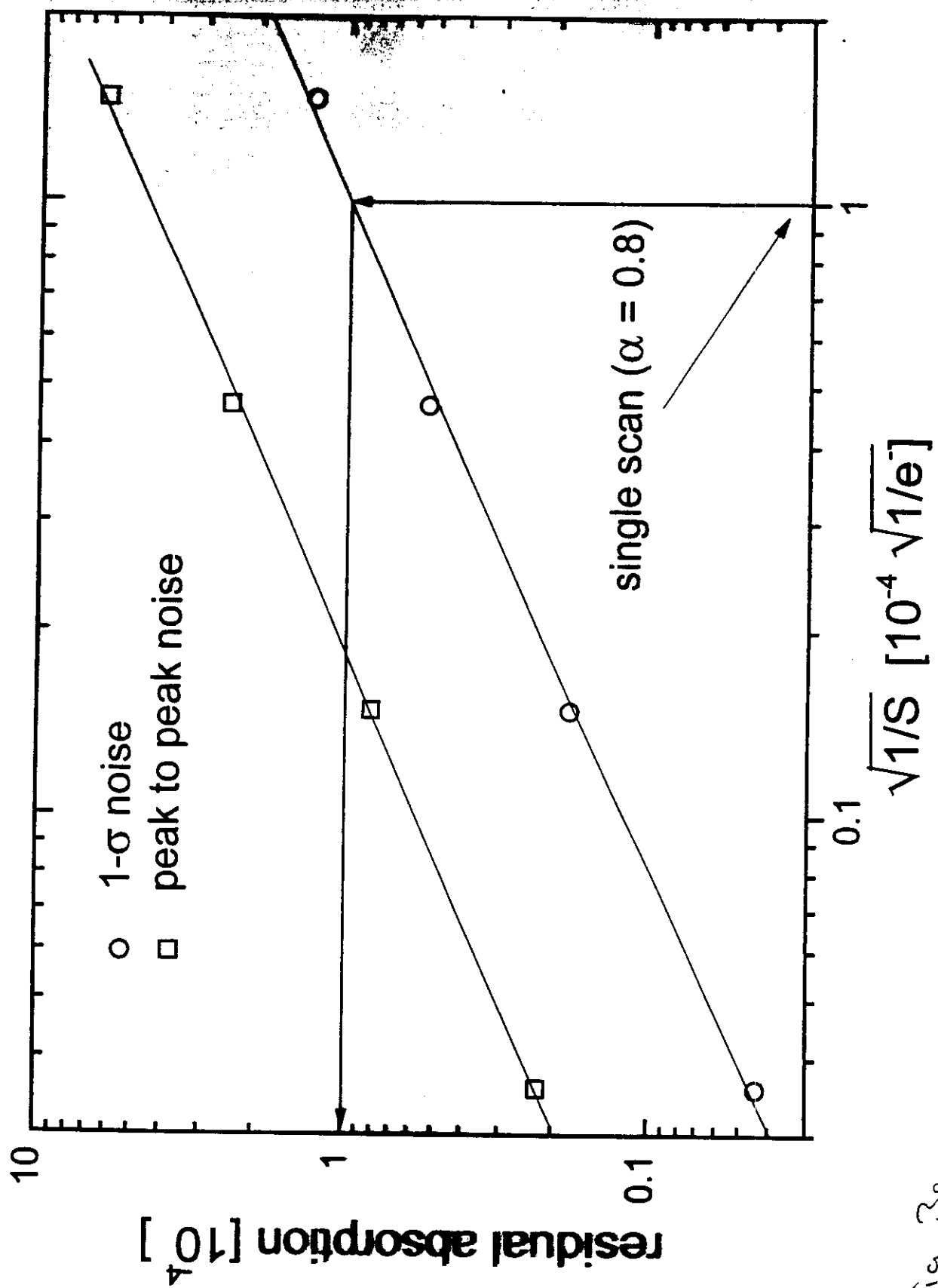


Fig. 3a

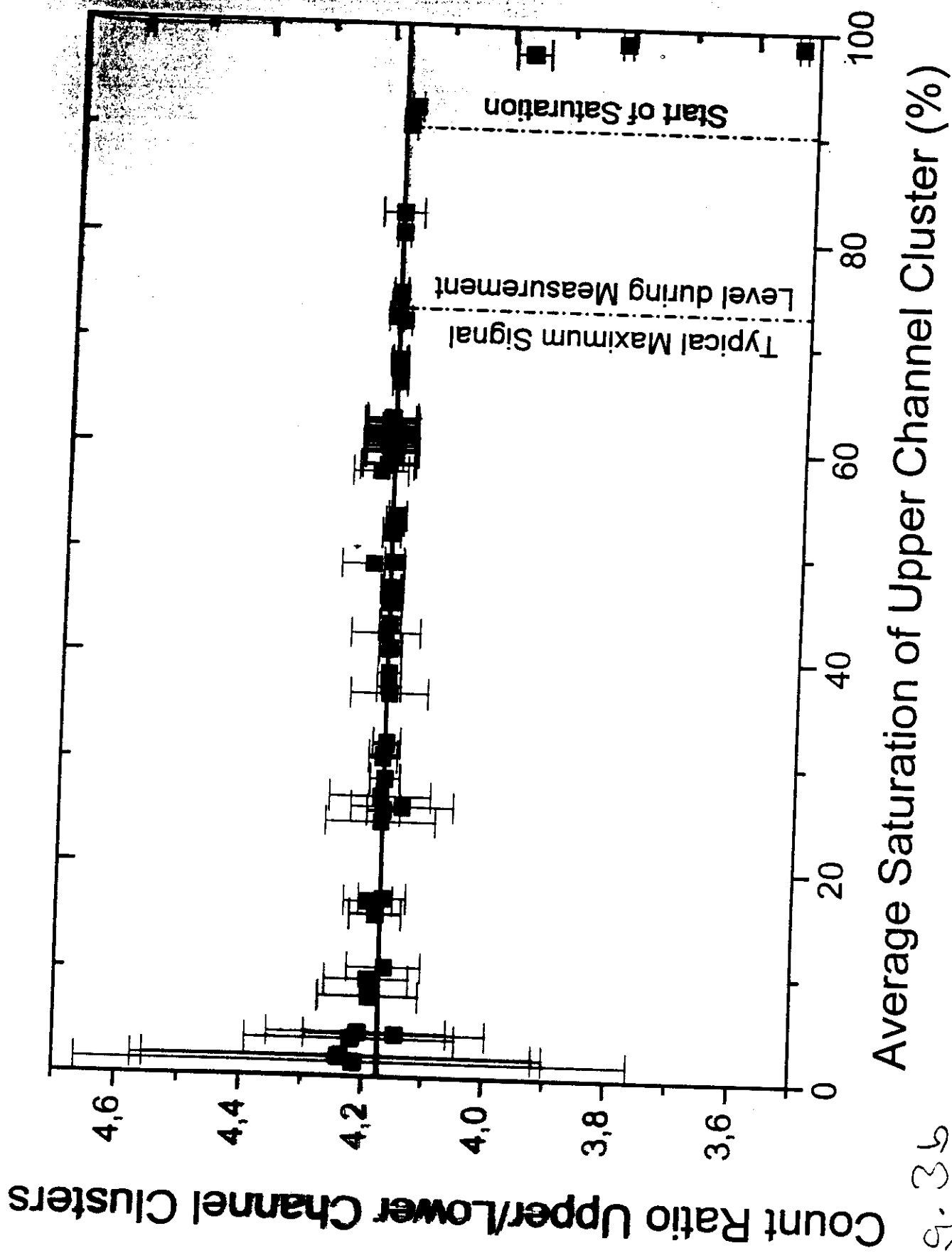
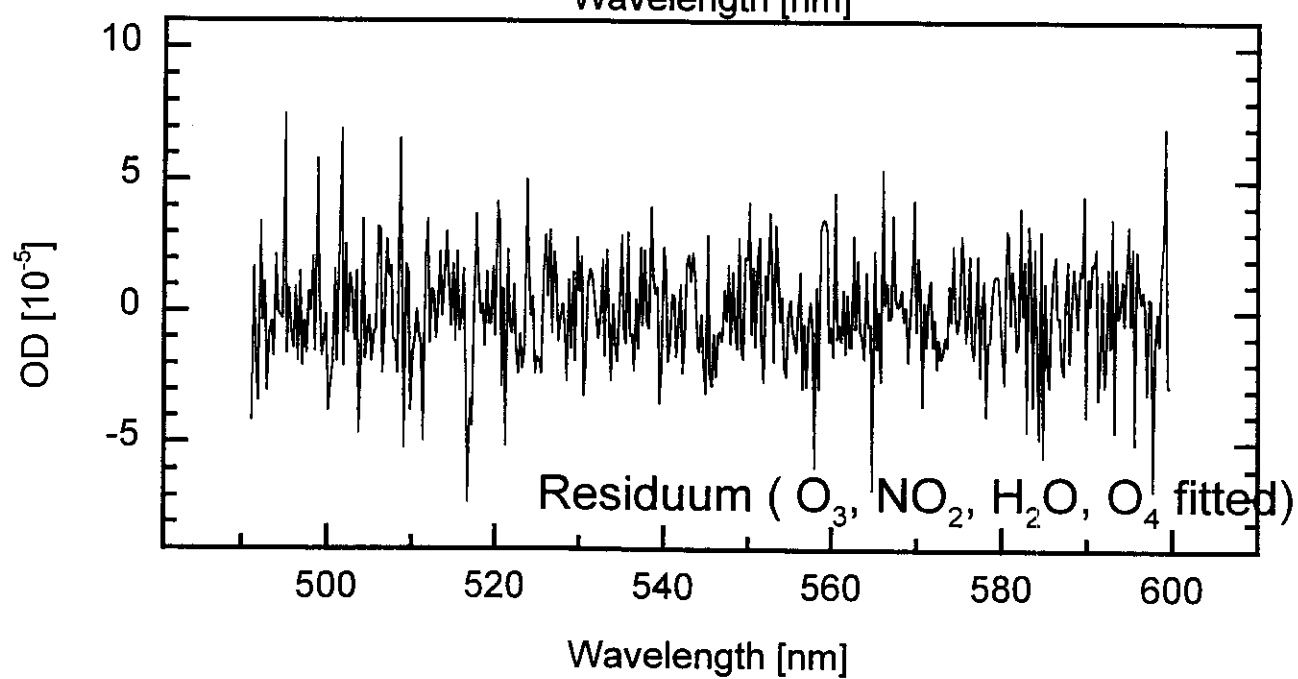
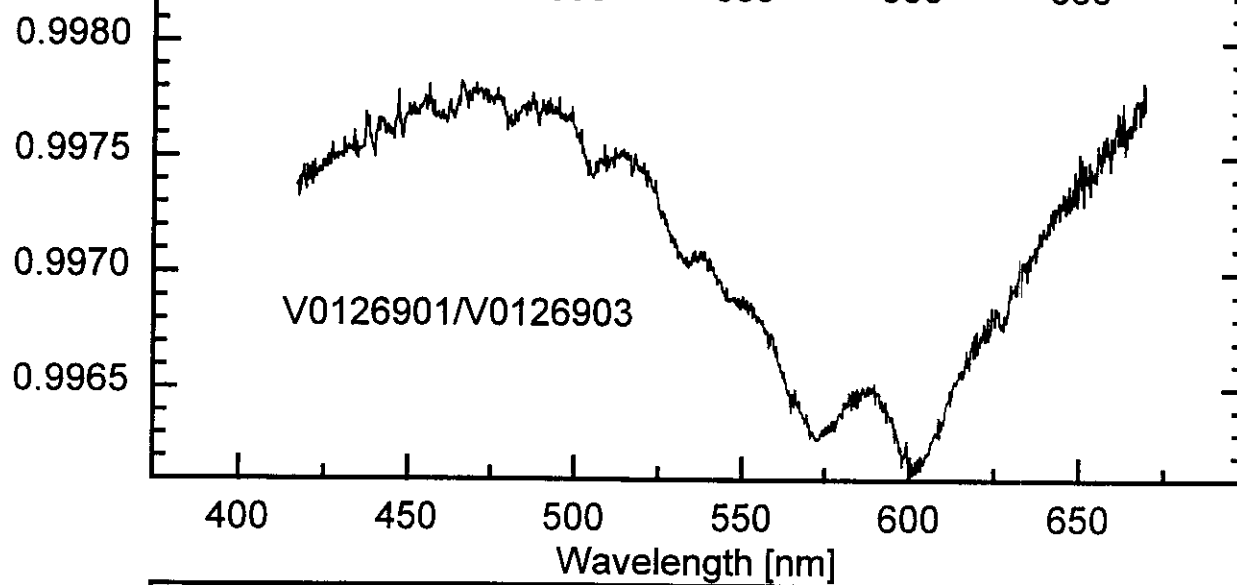
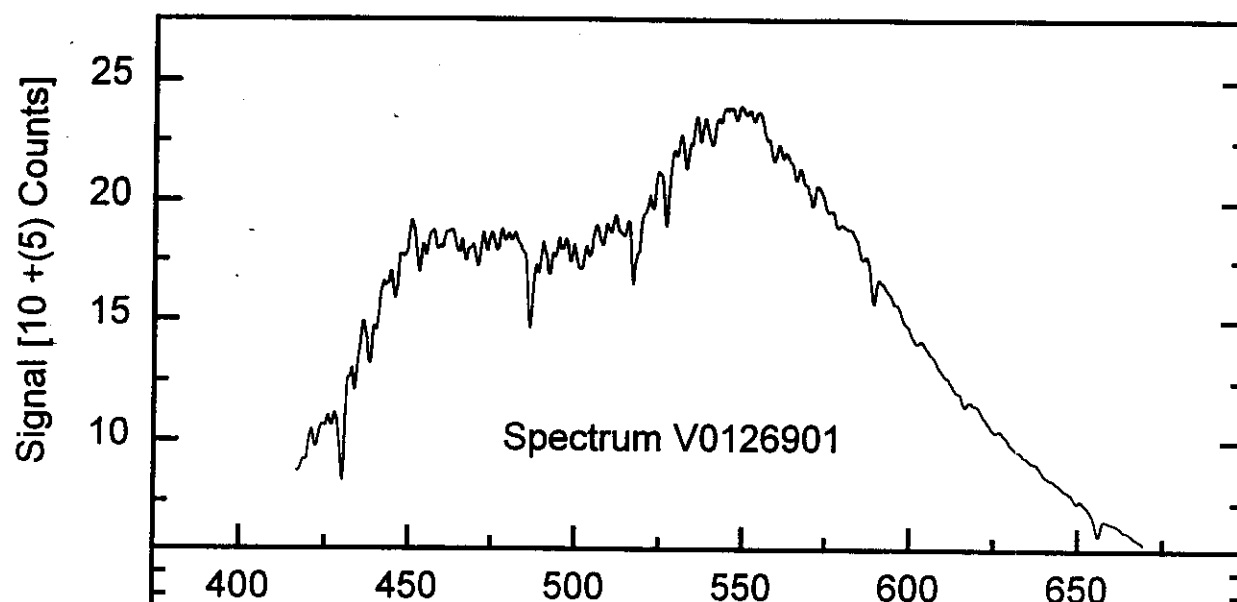
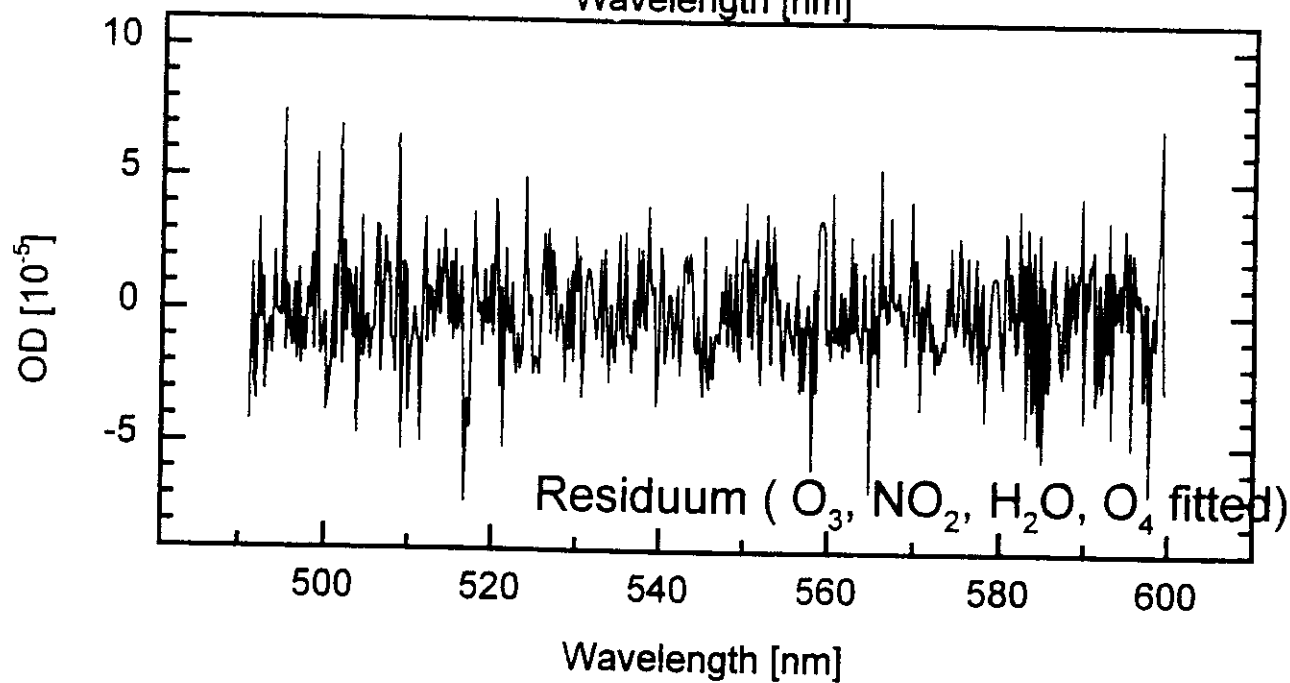
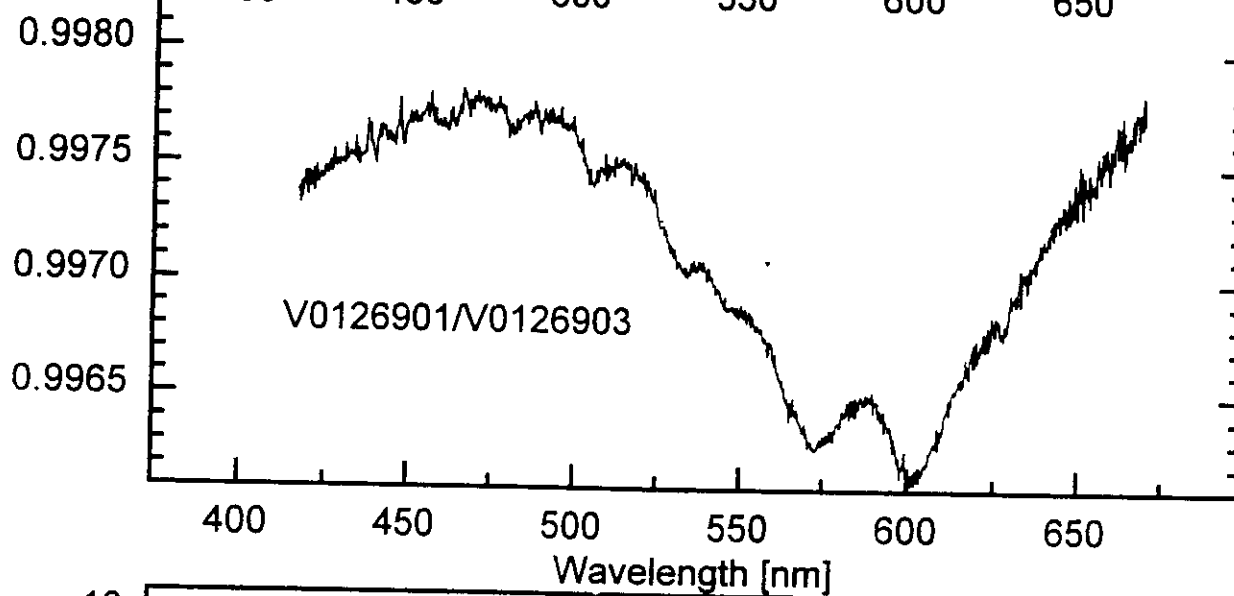
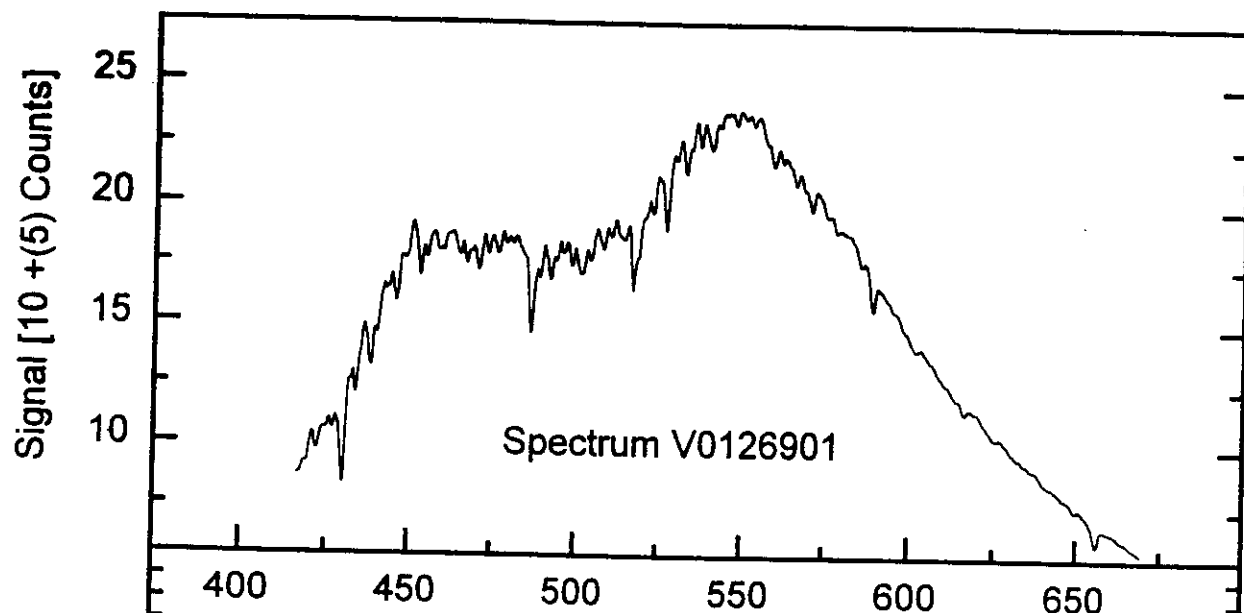


Fig. 3b





Principle of MCT technique

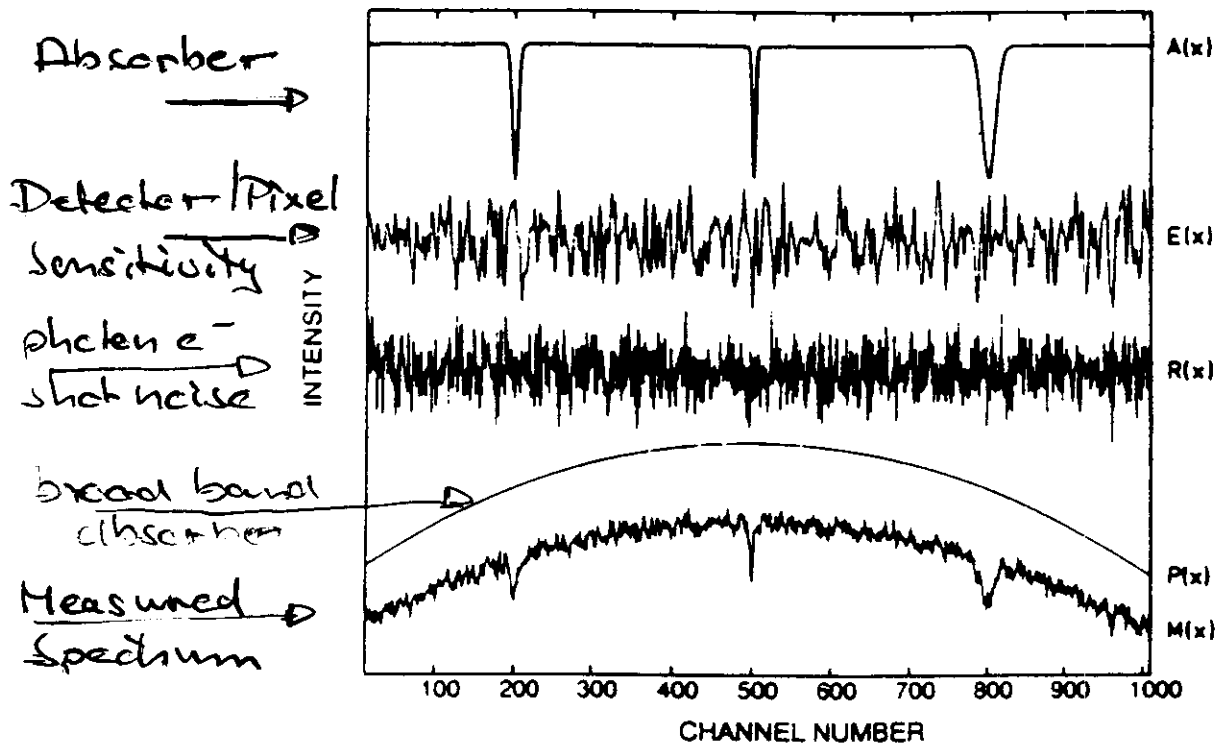


Fig. 2. Breakdown of the individual contributions to an example DOAS spectrum of atmospheric trace species as it is recorded with an OMA as a spectral detector (from top to bottom): Simulated differential absorption spectrum $A(x)$, where the differential optical density of all bands is 1×10^{-3} ; pixel sensitivity pattern $E(x)$ of a photodiode array having 1024 pixels (peak-to-peak variation $p/p = 1\%$); photoelectron shot noise $R(x)$ ($p/p = 6.5 \times 10^{-4}$); broadband term $P(x)$ ($p/p = 26\%$) containing the wavelength dependence of the light source, unstructured absorptions, and scattering; product $M(x)$ of all contributions, which is the observed spectrum.

Bowers et al. (1995)
 App Optics, 34, 4472

SIMULATED SPECTRA

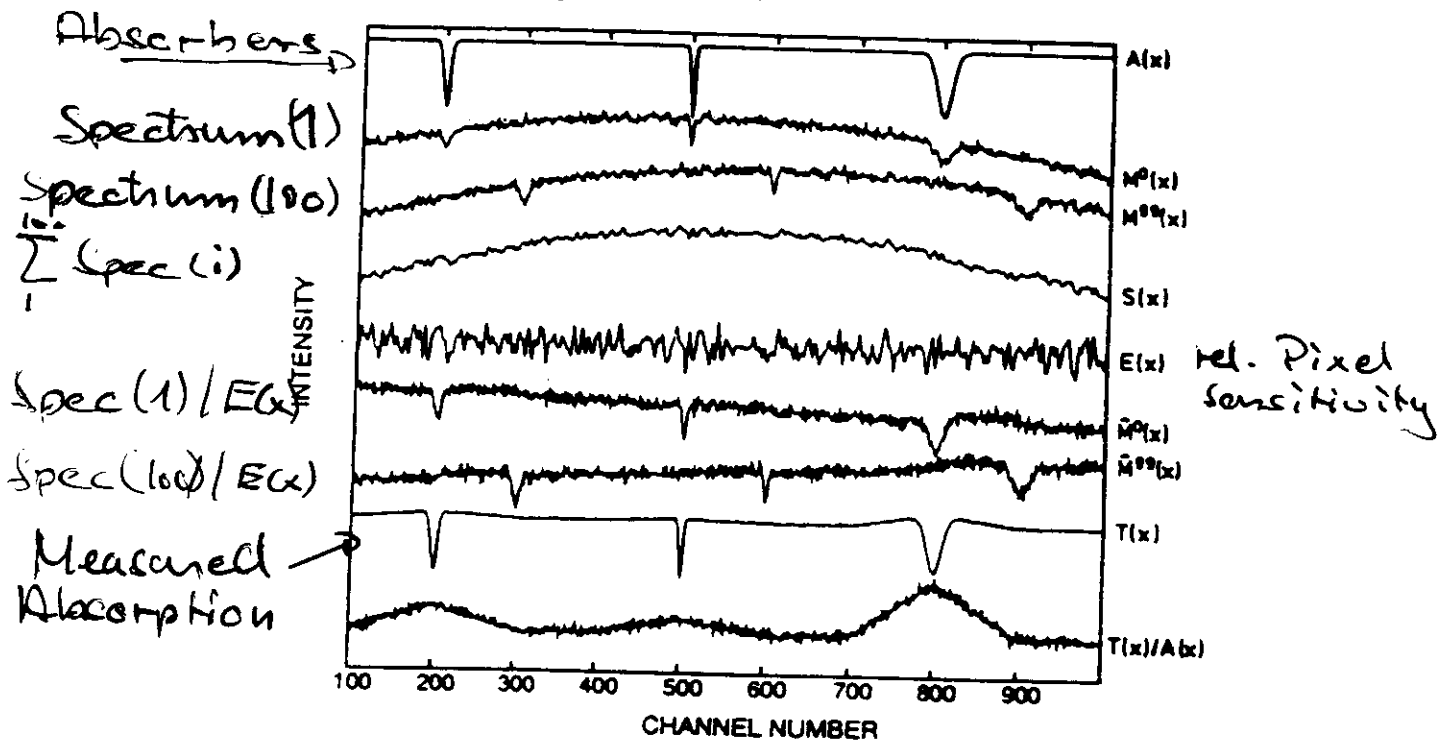


Fig. 3. Principle of the MCST with $N = 100$ simulated readouts containing three absorption lines ($D' = 0.001$) of different half-widths (10, 5, or 20 pixels). The lines are centered at pixels 200, 500, 800 at the first readout ($j = 0$) and at pixels 299, 599, 899 for the last readout ($j = 99$). A fixed pattern structure $E(x)$ ($p/p = 0.001$) and random noise $R^k(x)$ ($p/p = 6 \times 10^{-4}$) were also applied. Top to bottom, sample absorption $A(x)$ (from Fig. 2); $M^0(x)$ and $M^{99}(x)$, first and last readouts of the set, where the spectral shift between two consecutive readouts was 1 pixel channel ($\alpha = 1$); sum $S(x)$ of all readouts of the set according to Eq. (10); relative pixel sensitivity $E(x)$ for comparison (different scaling); new readouts $\tilde{M}^0(x)$ and $\tilde{M}^{99}(x)$, where any contribution of $E(x)$ was removed according to Eq. (11); final spectrum $T(x)$ after the spectra $\tilde{M}^k(x)$ were reshifted and added at the spectral position of the first spectrum. The optical densities in this spectrum D' (at $x = 200, 500$, and 800) are reduced by 1.3%, 0.7%, and 6%, respectively, compared with the original values, depending on the half-width of the original line (see Table 1 for details). From the residual (magnified 10 times) it becomes obvious that the MCST generates no spurious narrow-band modulations. Compared with the random noise added to each spectrum at the beginning of the procedure, the final noise level is reduced by a factor of $\sqrt{N} = 10$.

Reuser and, (1995)
Appl. Optics, 34, 4472

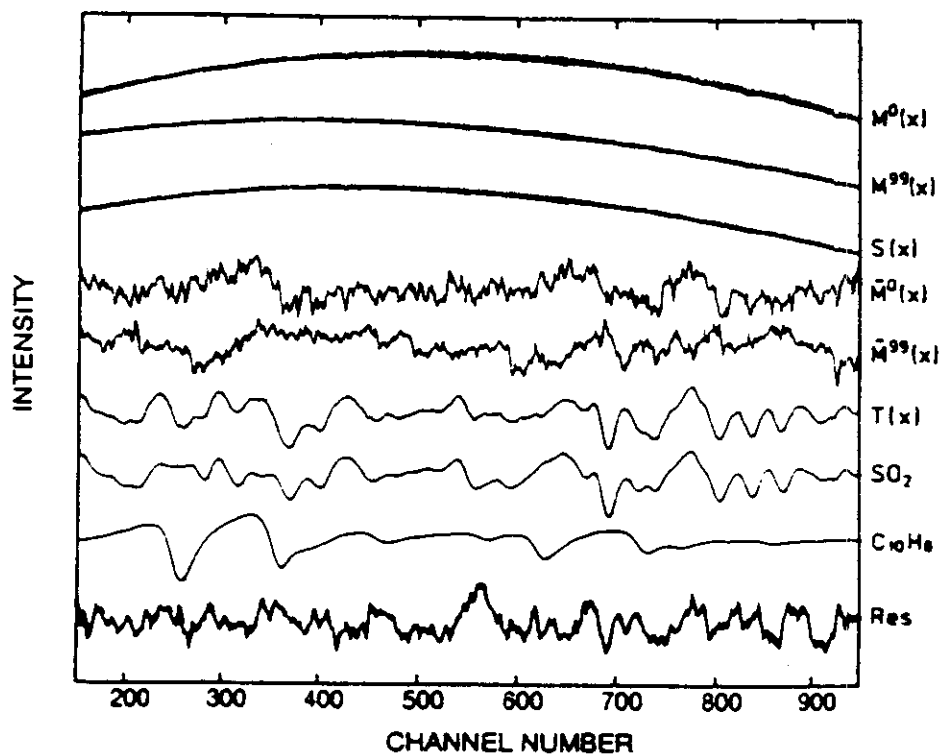


Fig. 5. Example of an air spectrum recorded with our OH-DOAS instrument by the use of the MCST. Top to bottom, the first $M^0(x)$ and the last readout $M^{99}(x)$, which were shifted by 0.94 channels after each readout; the sum $S(x)$ of the 100 readouts according to Eq. (10); $\bar{M}^0(x)$ and $\bar{M}^{99}(x)$ with $E(x)$ removed according to Eq. (11); the final spectrum $T(x)$ after the individual quotient spectra $\bar{M}^k(x)$ are shifted back to the spectral position of the first spectrum and added up; SO_2 reference spectrum recorded with the same procedure of MCST; naphthalene reference spectrum; residual spectrum after removal of the atmospheric SO_2 and naphthalene absorptions, where the peak-to-peak value is 7×10^{-5} .

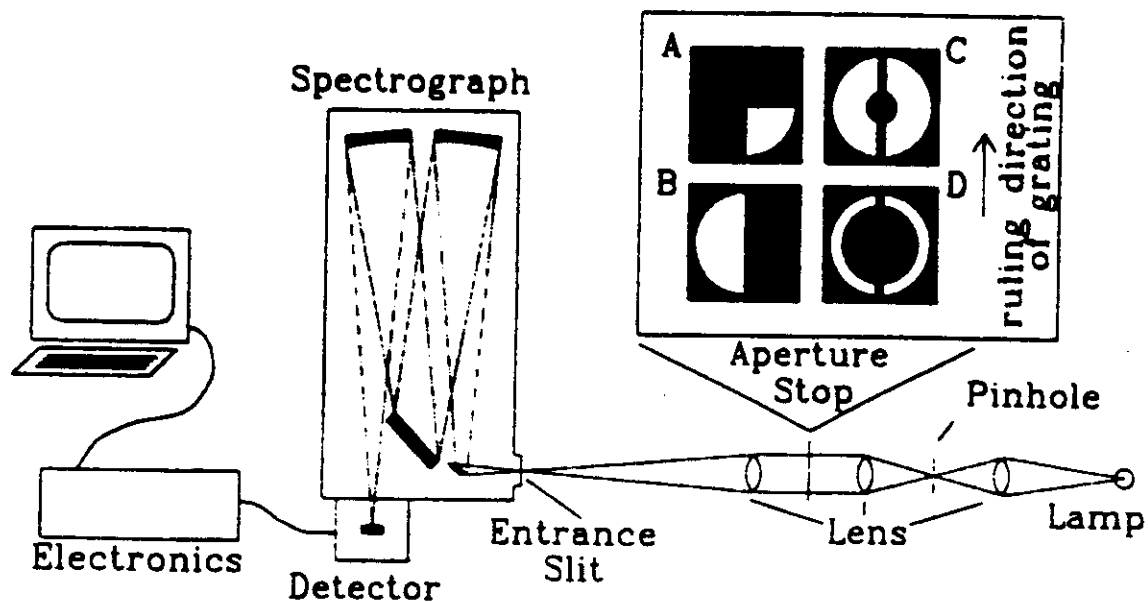


Fig. 1. Experimental setup to investigate the dependence of the spectrograph-detector system on the illumination. The aperture stops *A*, *B*, *C*, and *D* are inserted into the collimated light beam, which is produced by two lenses and a 200- μm pinhole. The light is focused on the entrance slit of the spectrograph by another lens.

Stutz and Platt (1997)
 App Opt. 36, 1-105

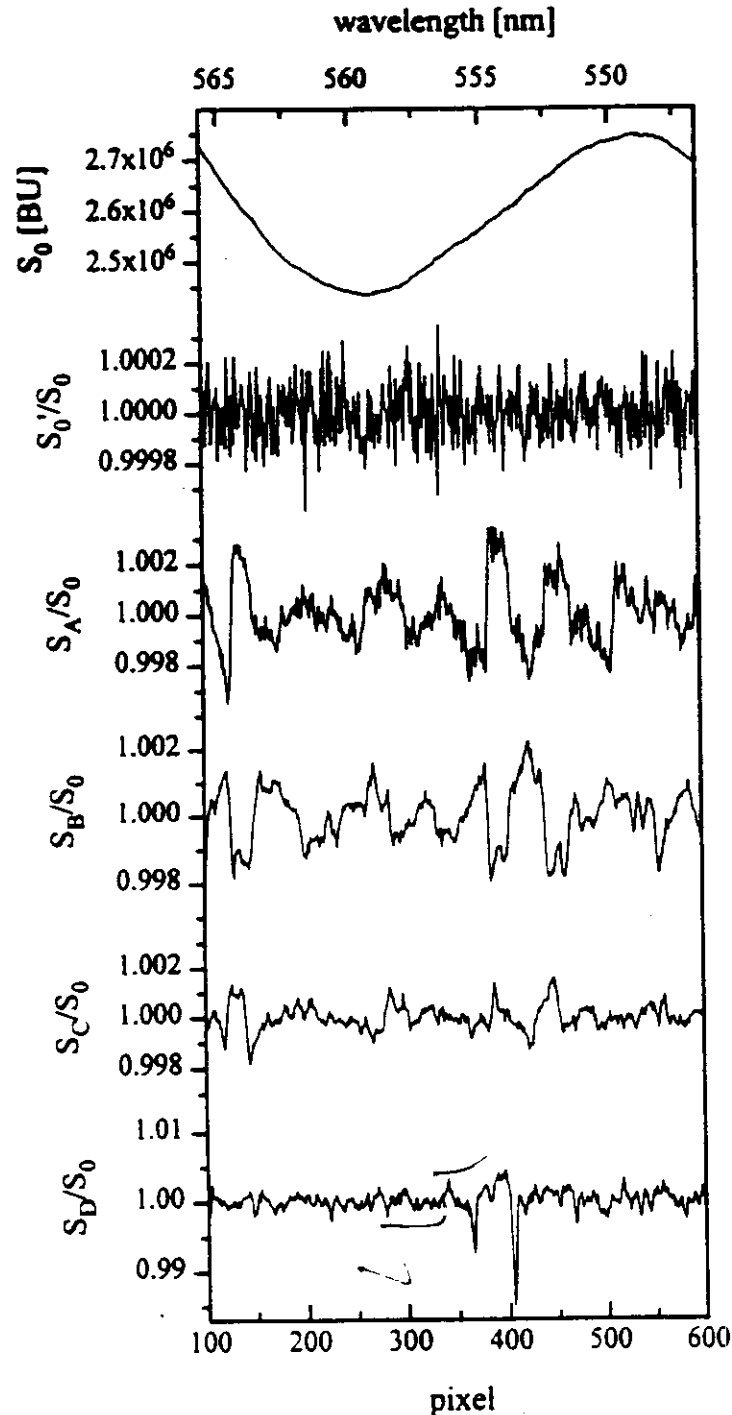


Fig. 2. Structures produced by changes in illumination of the spectrograph-detector system. The top spectrum shows a typical lamp spectrum with its sinusoidal étalon structure. The noise level in the ratio of two spectra taken under identical conditions without aperture stop S_0'/S_0 is lower than the spectral structures found in the ratios of spectra taken with different illuminations (i.e., aperture stops A-D inserted), S_A/S_0 , S_B/S_0 , S_C/S_0 , and S_D/S_0 . The y scale of S_D/S_0 was changed to show the complete spectrum. The aperture stops used to change the illuminations are shown in Fig. 1.

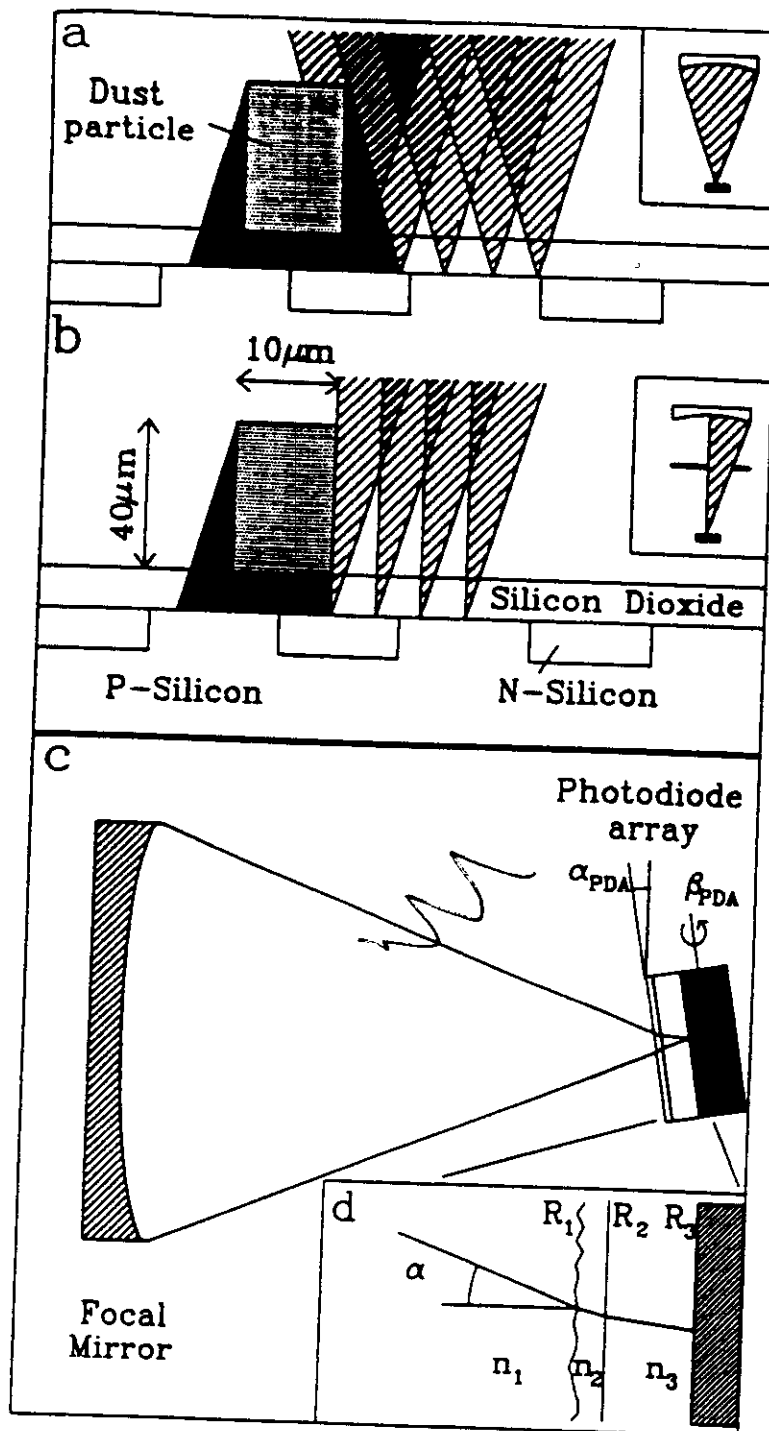


Fig. 3. Effects that give rise to illumination-sensitive response of the diode of a PDA: a, a dust particle illustrated with a rectangular cross section throws a shadow on the diode on the right of the particle. The diode is illuminated by a full cone of light (i.e., no aperture stop present); b, if only the right half of the cone is illuminated (e.g., owing to the presence of aperture stop A or B) the shadow is not present; c, d, an irregular surface changes the interferences in the protective layer of the PDA. The figure explains the model calculations performed to investigate this effect in two dimensions: A ray enters the layers on the PDA with angles α ; the light path in the layer is therefore longer compared with a vertical ray; as a cone of light is thrown from the focusing mirror of the spectrograph on the PDA, the intensity must be integrated over all angles to derive the total intensity I_{tot} .

Stutz and Plett (1997)
 App. Opt. 36: 1405

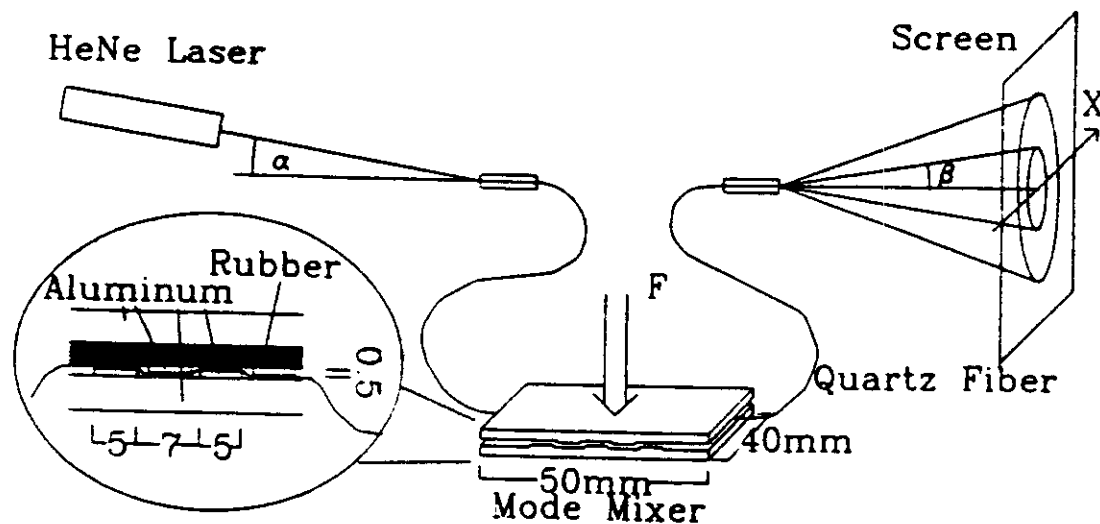


Fig. 5. Experimental setup to investigate mode coupling in a multimode quartz fiber. The light beam of a helium-neon laser is fed into the fiber at an angle α . The fiber is placed between two plates with a step profile. A sheet of rubber is placed between the top aluminum plate and the profile to protect the fiber. The plates can be pressed together with a force F to introduce microbending to the fiber. The light intensity leaving the fiber is measured with a photoresistor on a screen at a 15-cm distance from the fiber end along the X axis.

Stutz and Patti (1997)
 App. Optics, 36, 15

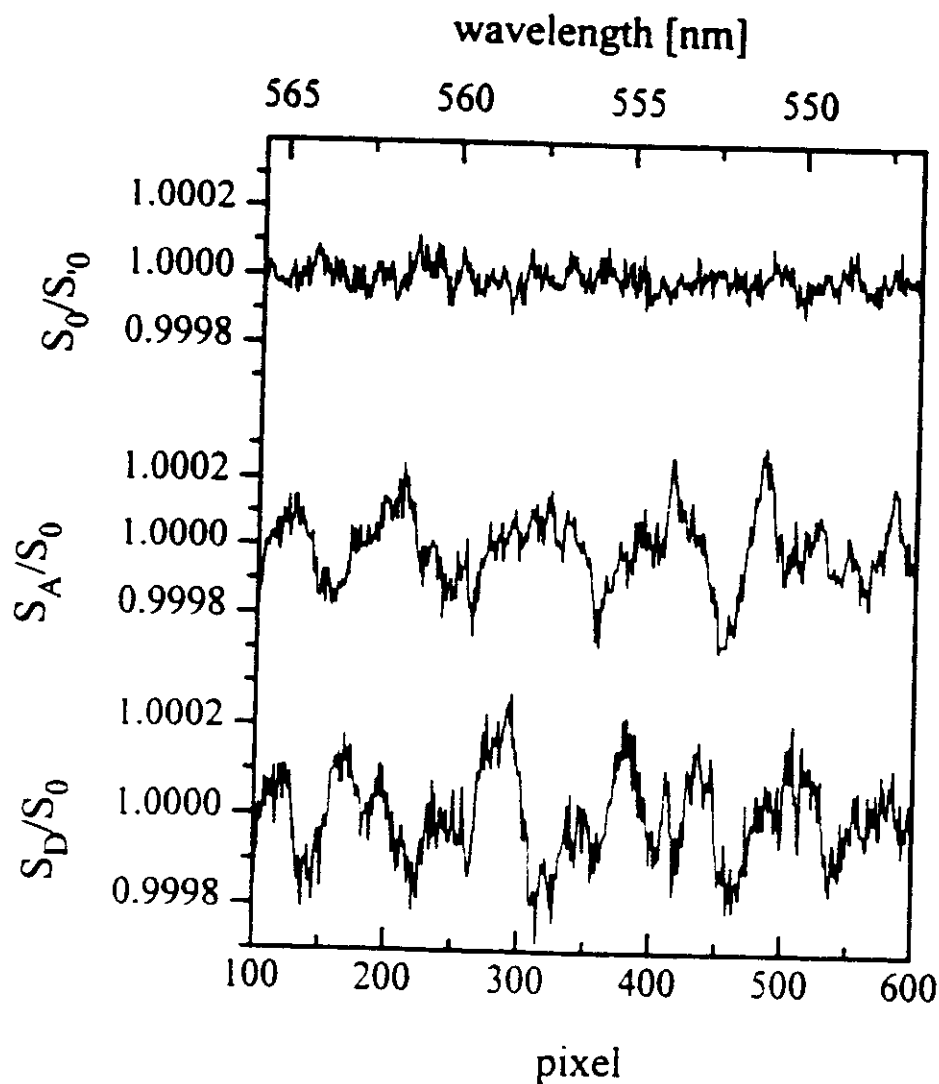
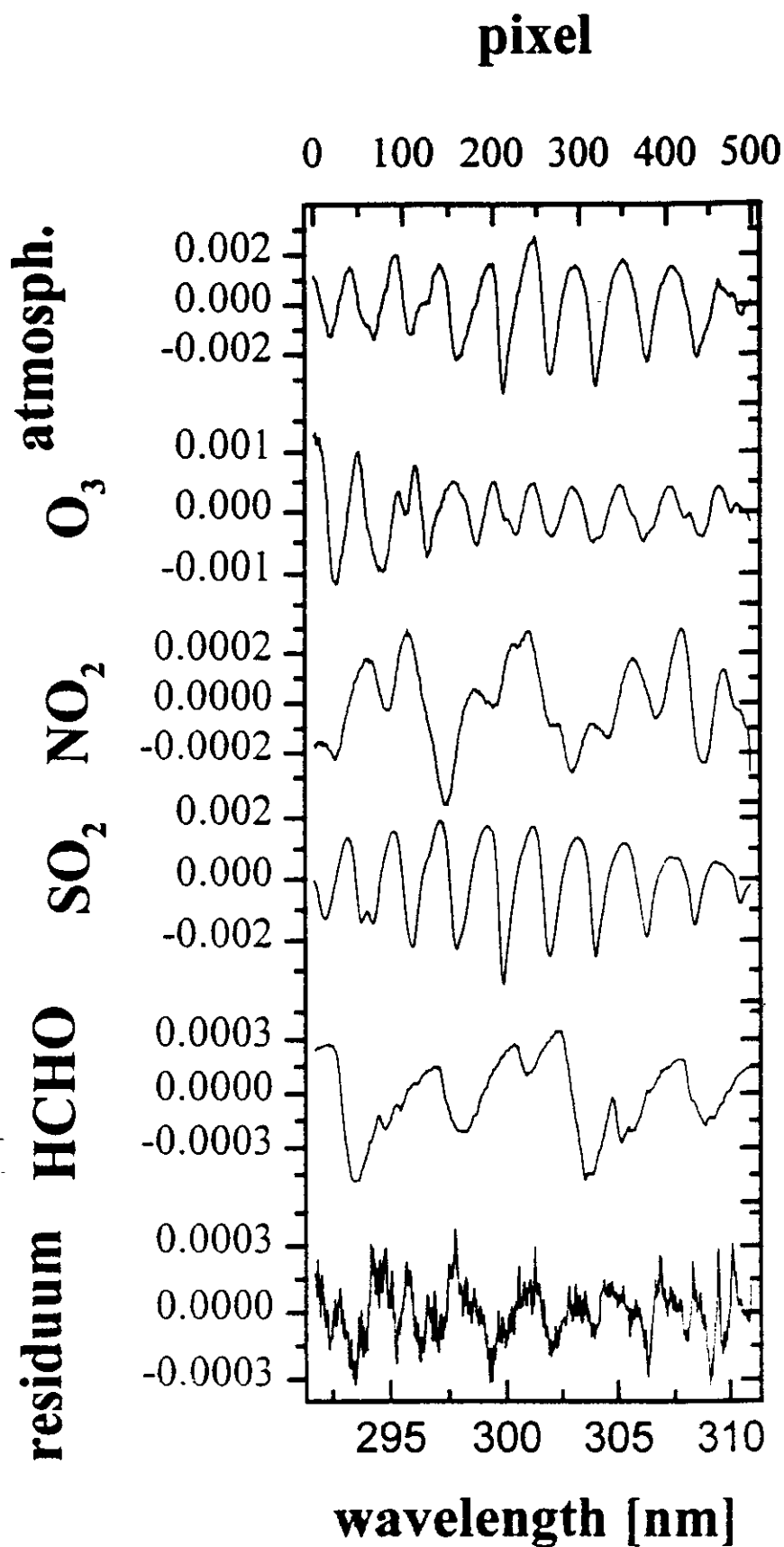
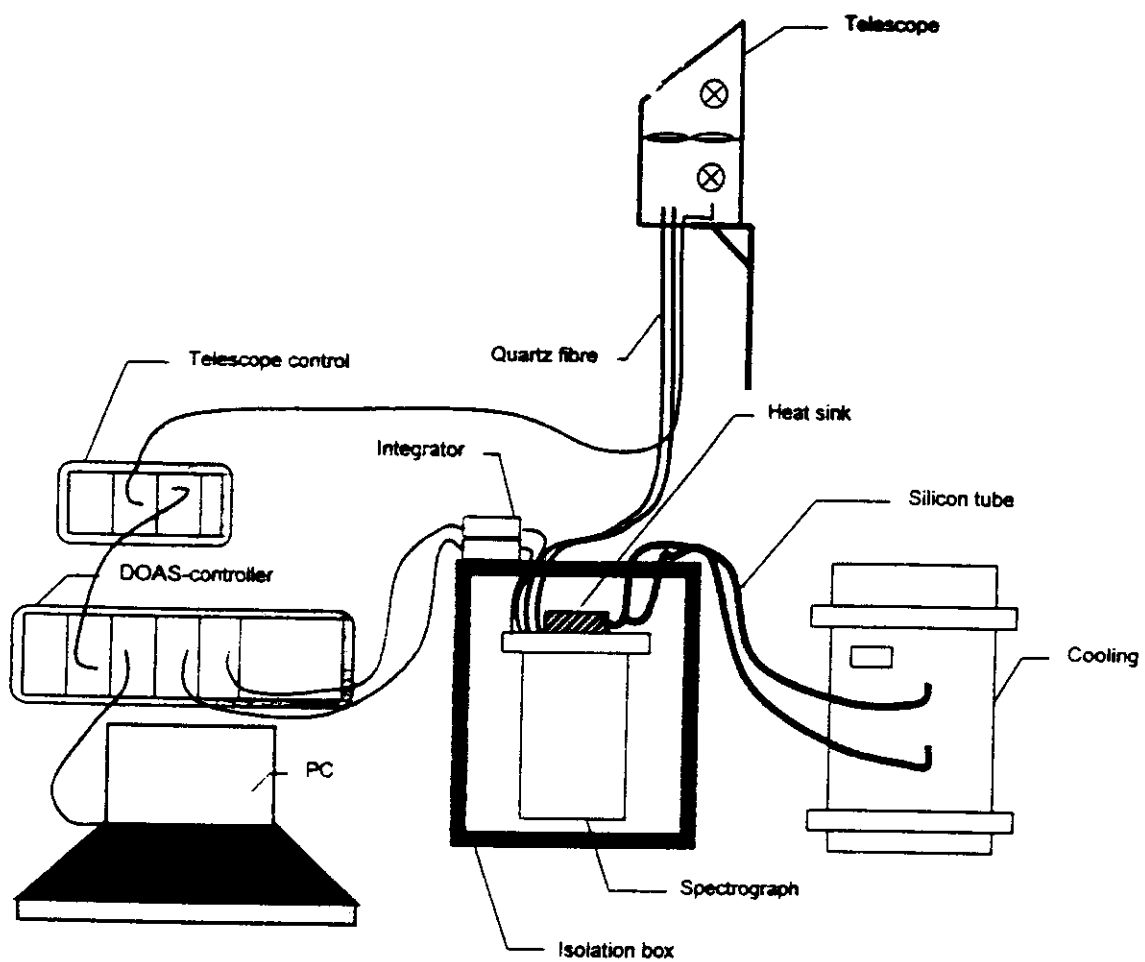


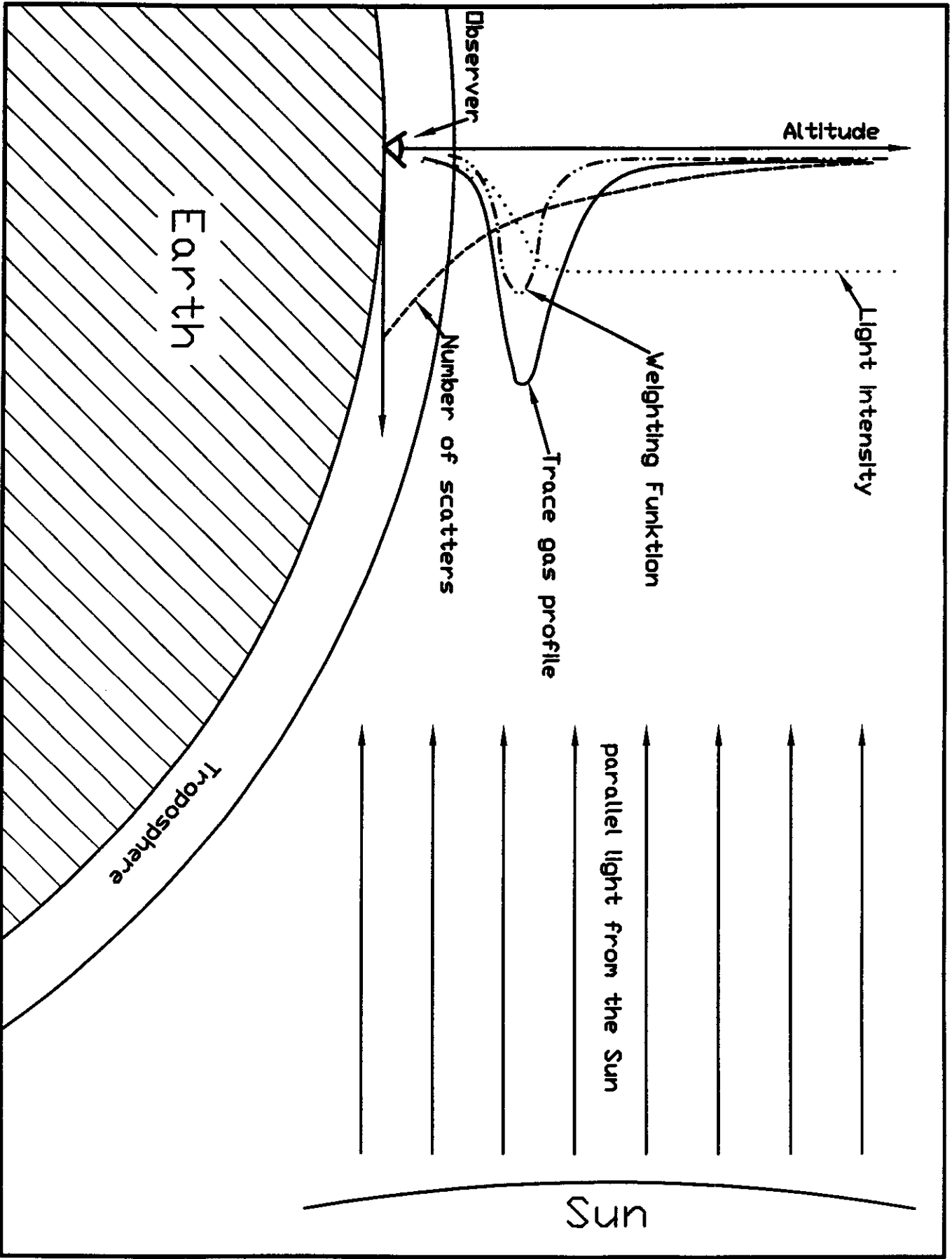
Fig. 8. Noise and residual spectral structure of a system, including a mode mixer (Figs. 5 and 7). The structures S_A/S_0 and S_D/S_0 are smaller by a factor of more than 10 compared with the results without a mode mixer (Fig. 2).

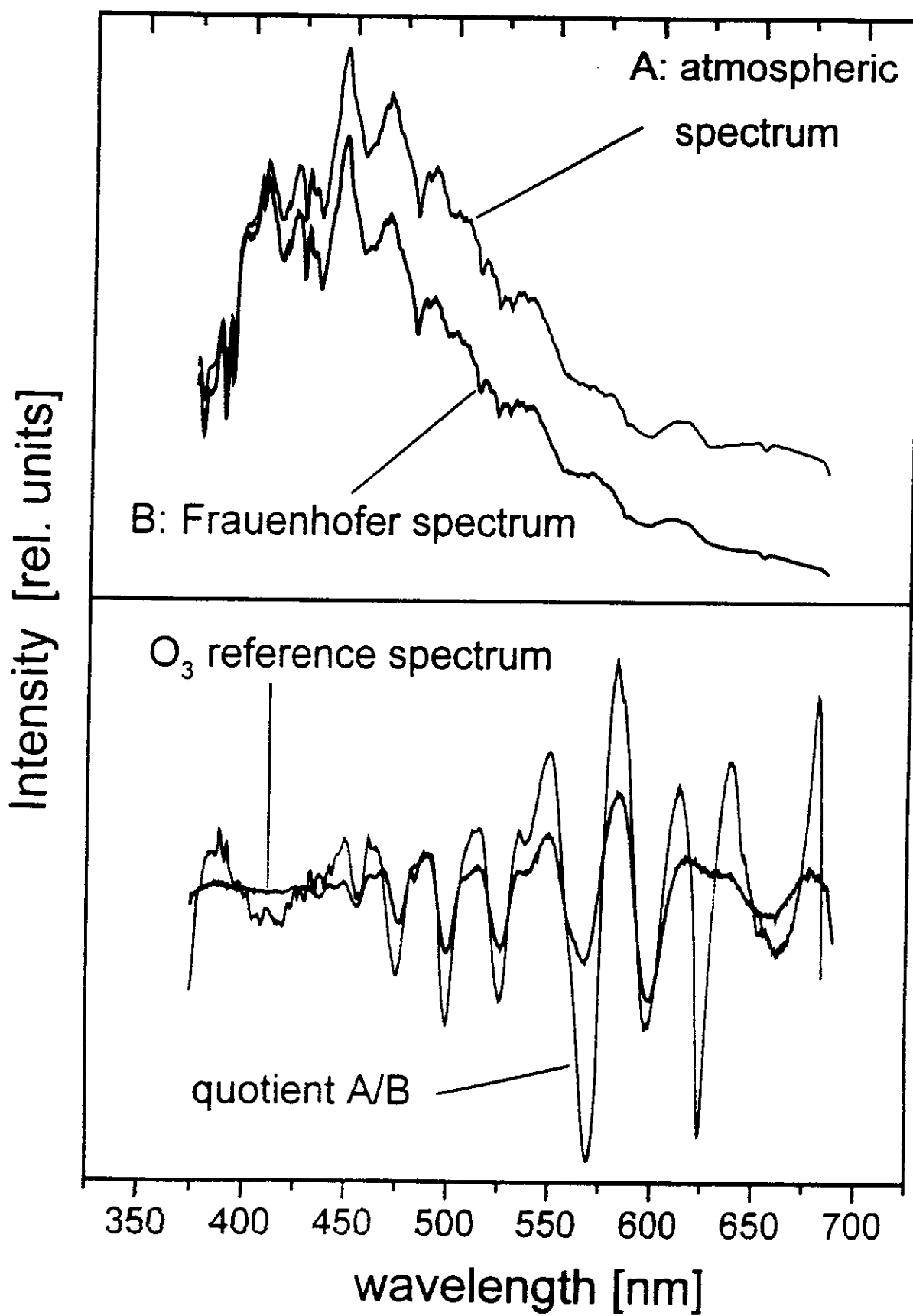
Stutz and Platt (1991)
 App. C. Optical Spectroscopy



Deming et al. (1992)
Fig. 9







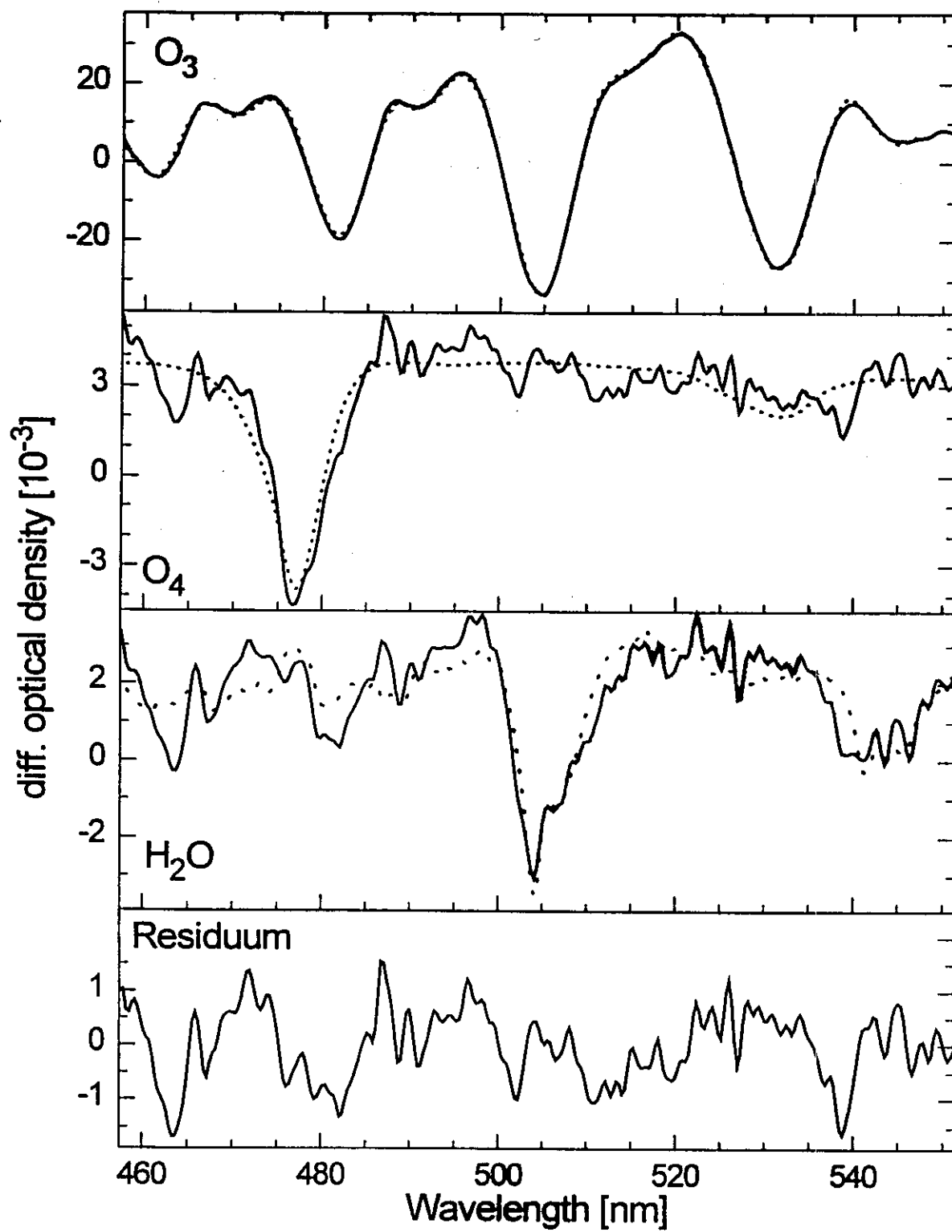


Fig. 1

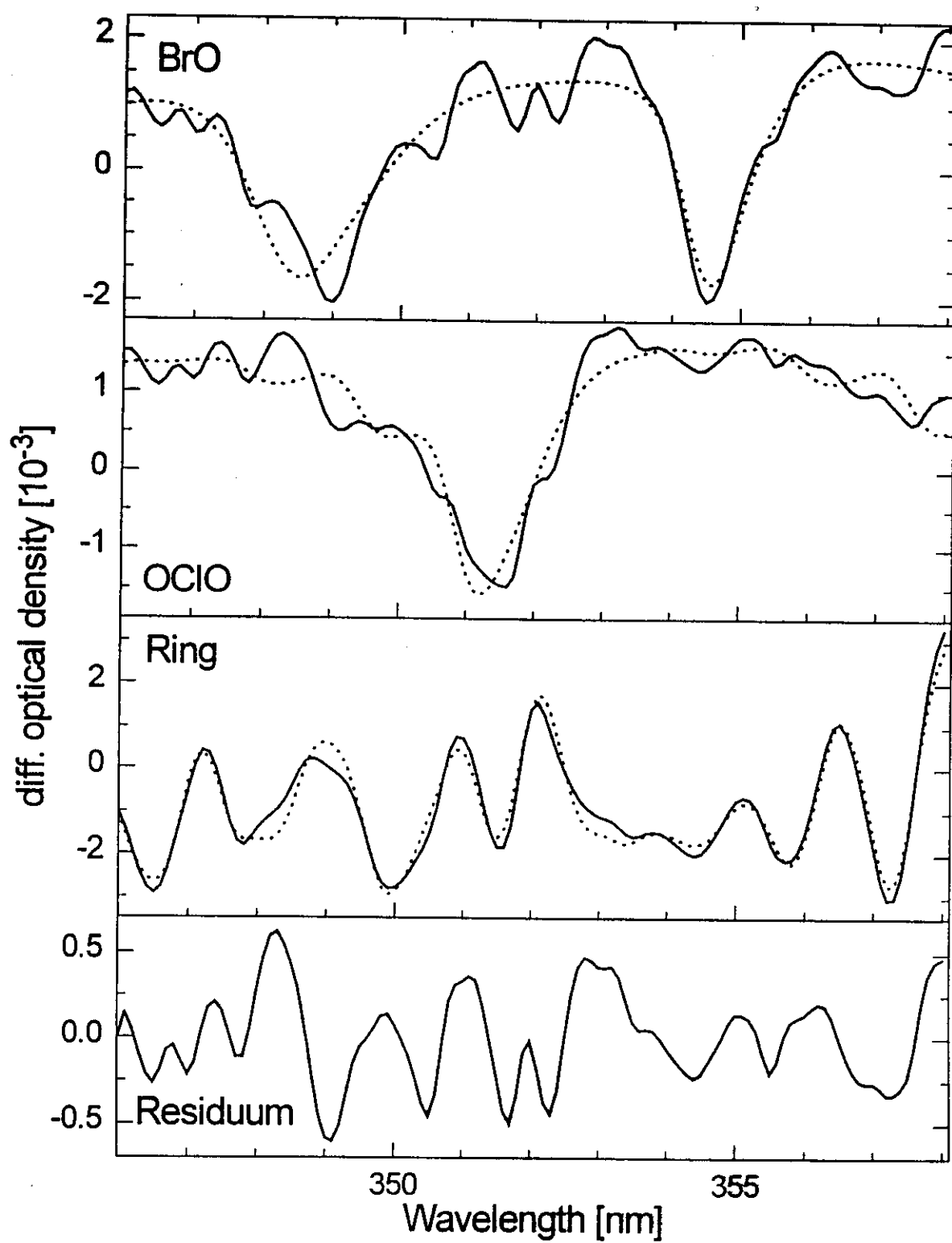
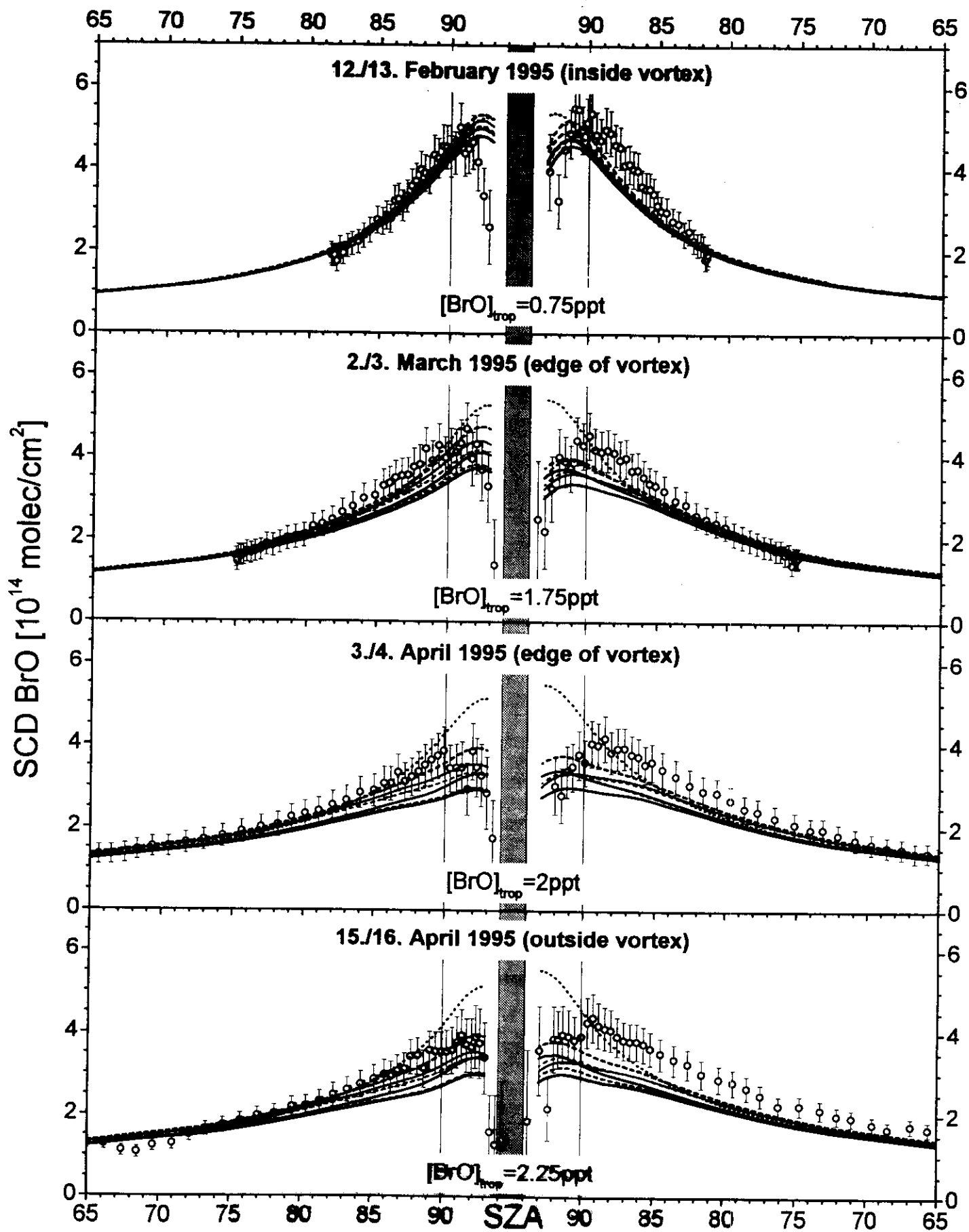


Fig - 3

○ DOAS measurements
 ----- model without stratospheric chemistry

model results with constant tropospheric BrO mixing ratio:

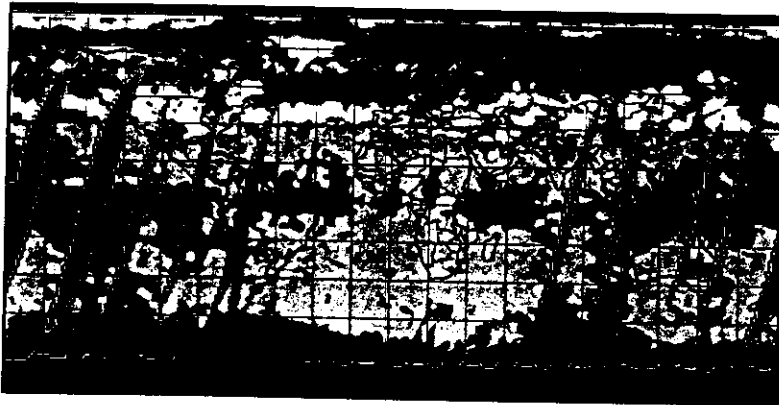
- 1) Control. JPL 1997 kinetics
- 2) as 1) but with $\text{BrONO}_2 + \text{O}$
- 3) as 1) but with $\text{BrO} + \text{NO}_2 + \text{M} \rightarrow \text{BrONO}_2 + \text{M}$ reduced to JPL 97 lower limit
- 4) as 3) but also with $\text{BrONO}_2 + \text{O}$
- 5) as 1) but with J_{NO_2} increased by factor 4
- 6) as 1) but with J_{NO_2} increased by factor 1.4



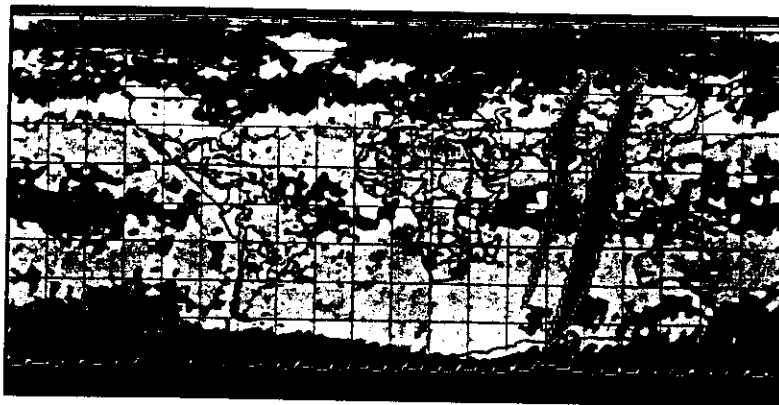
Gene total NO₂



24.08.95 - 27.08.95

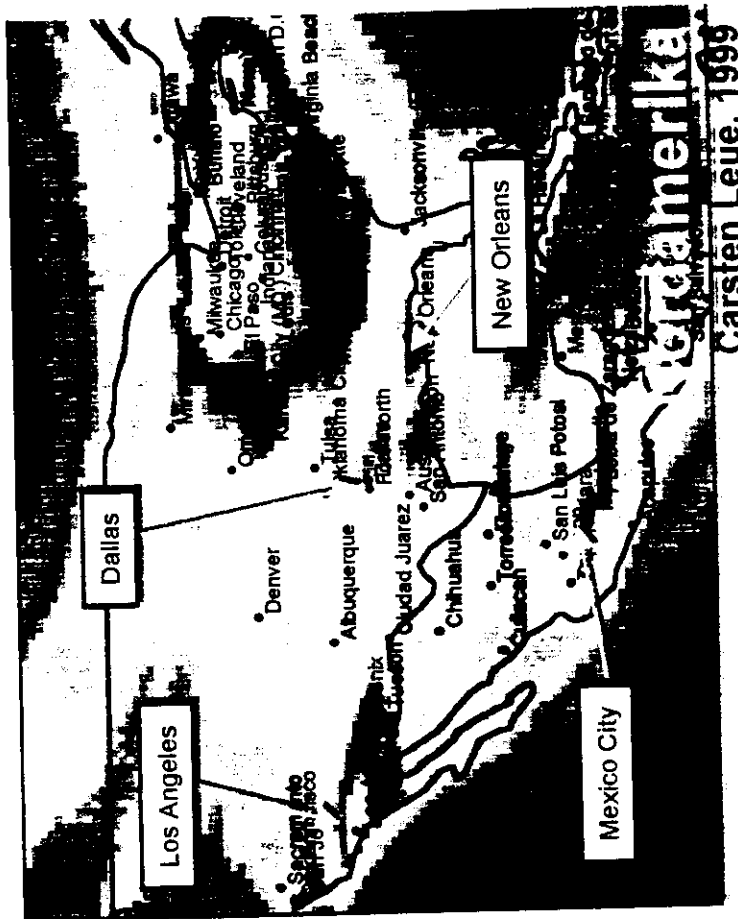
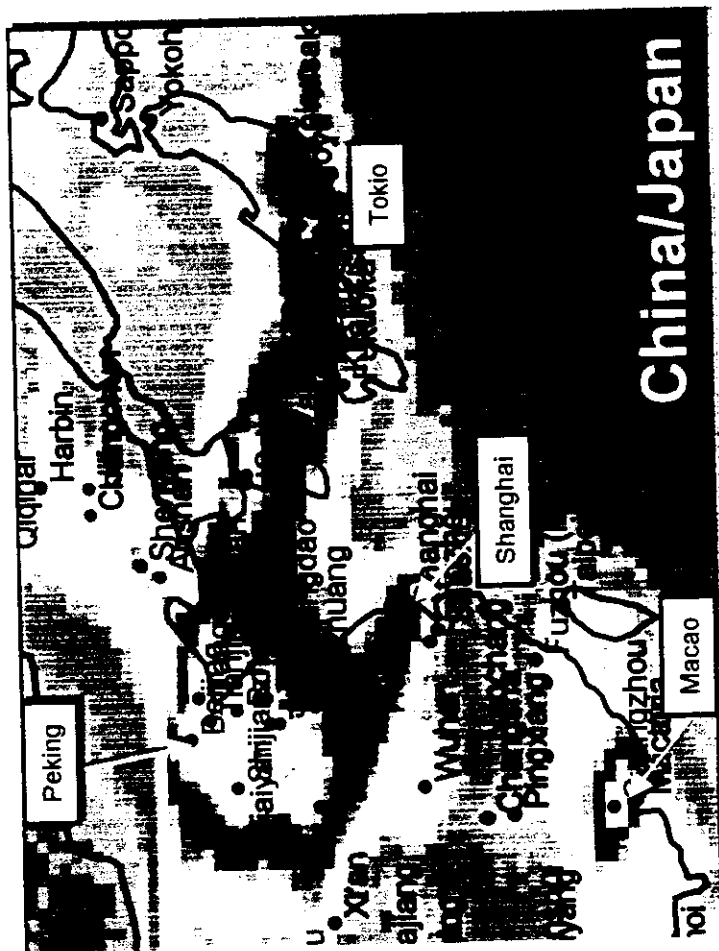
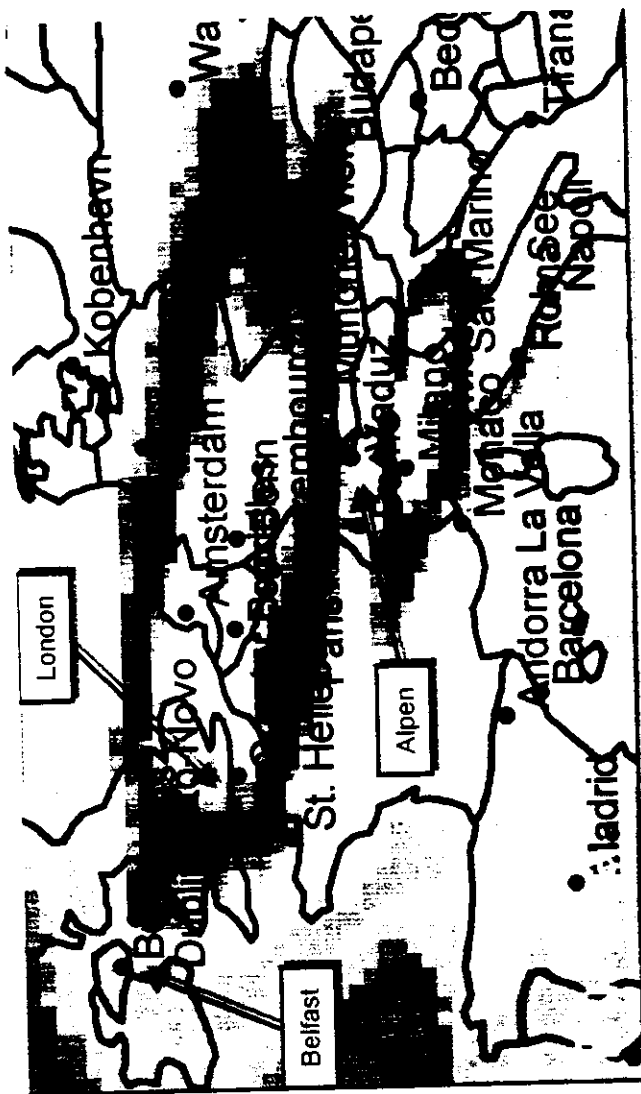
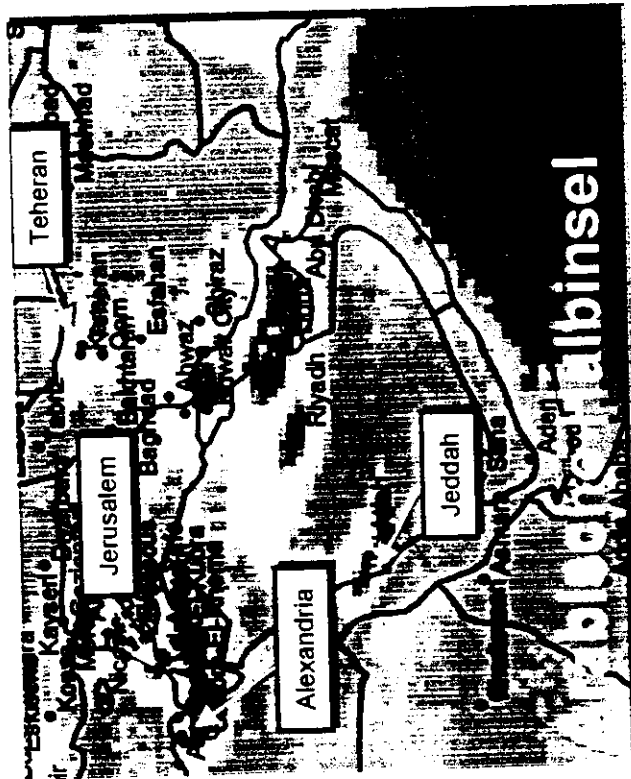


28.08.95 - 30.08.95



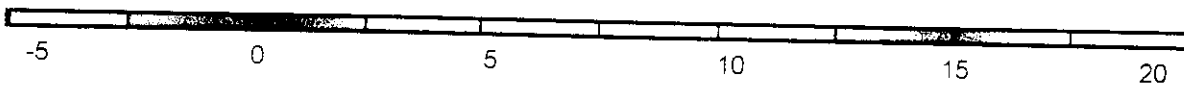
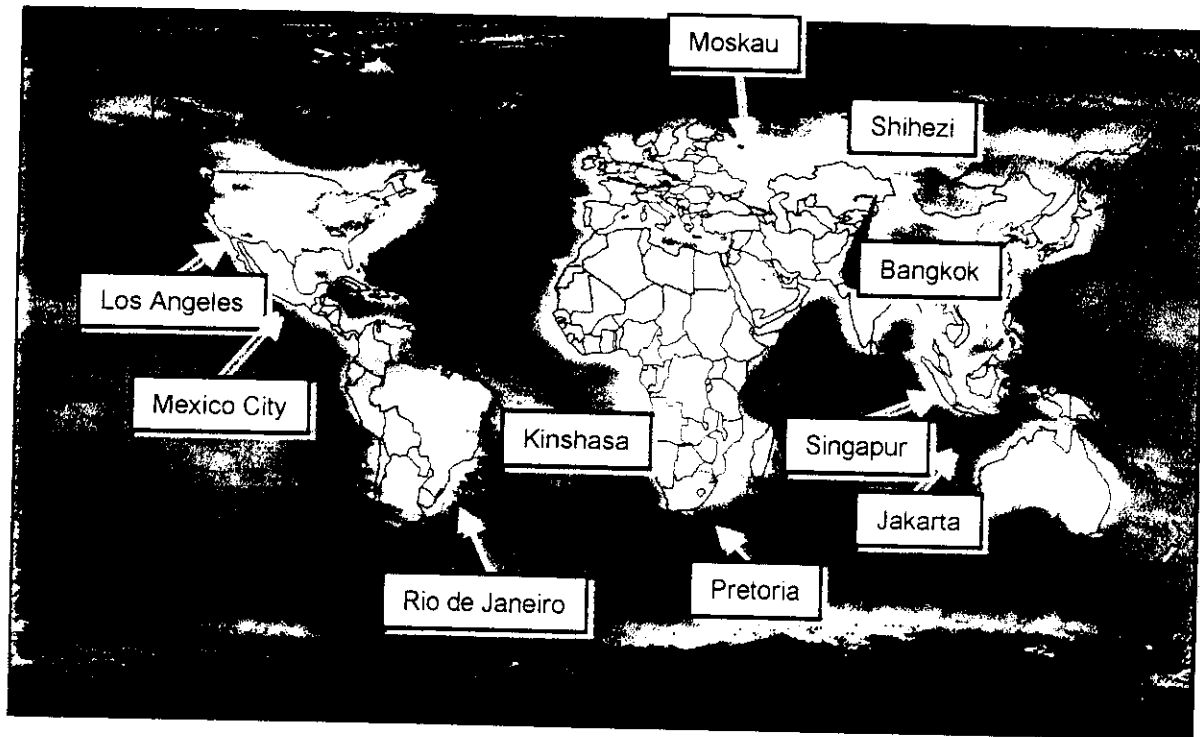
31.08.95 - 02.09.95

-Eure et val (1999)

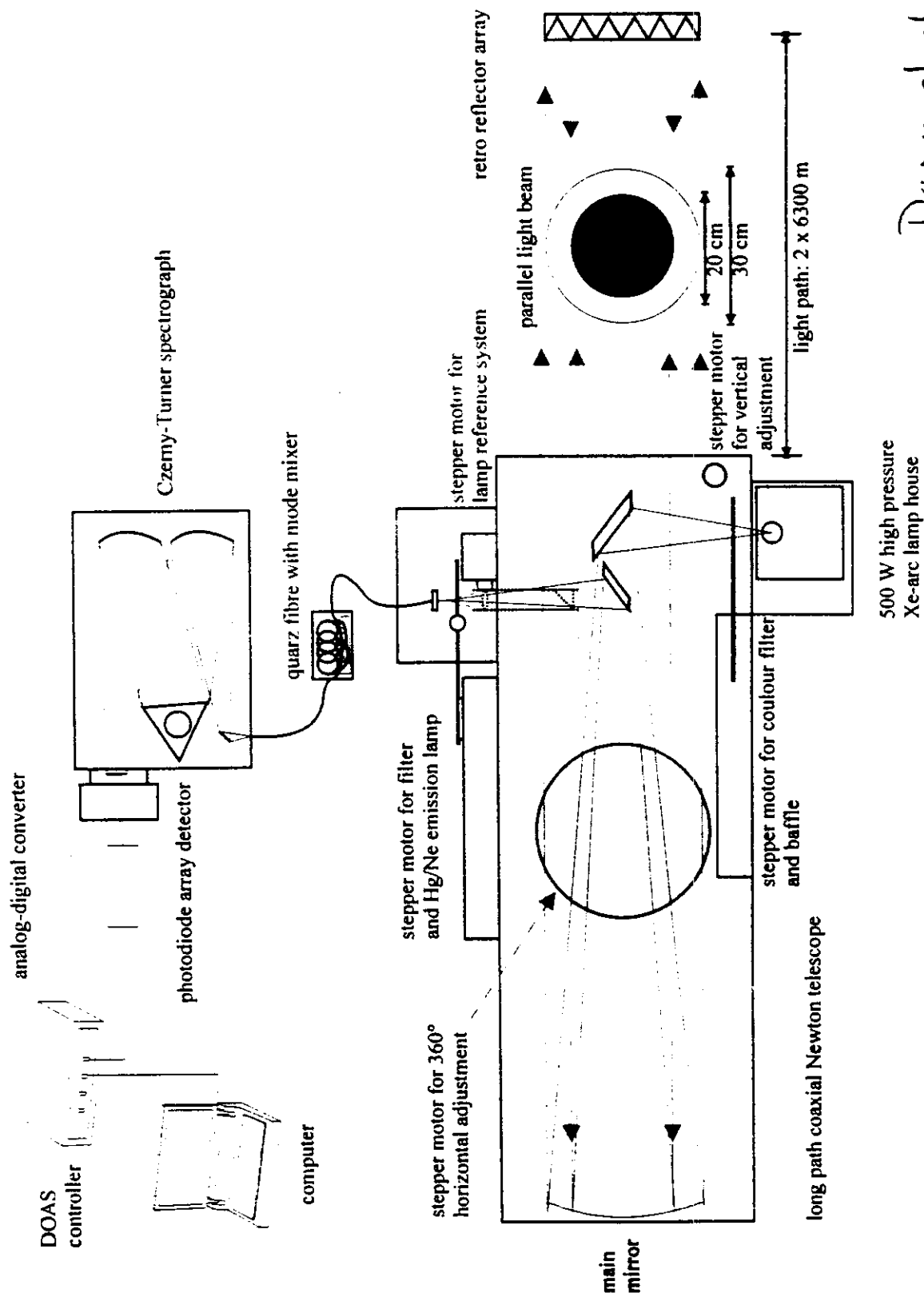


China/Japan

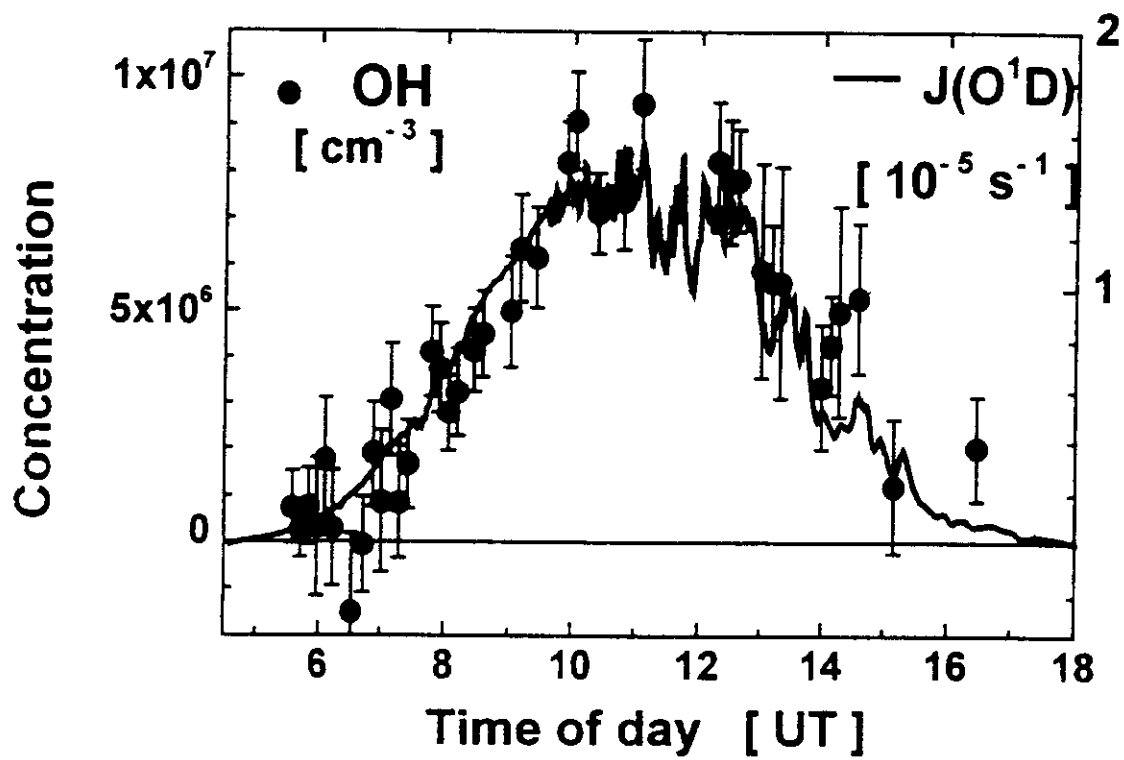
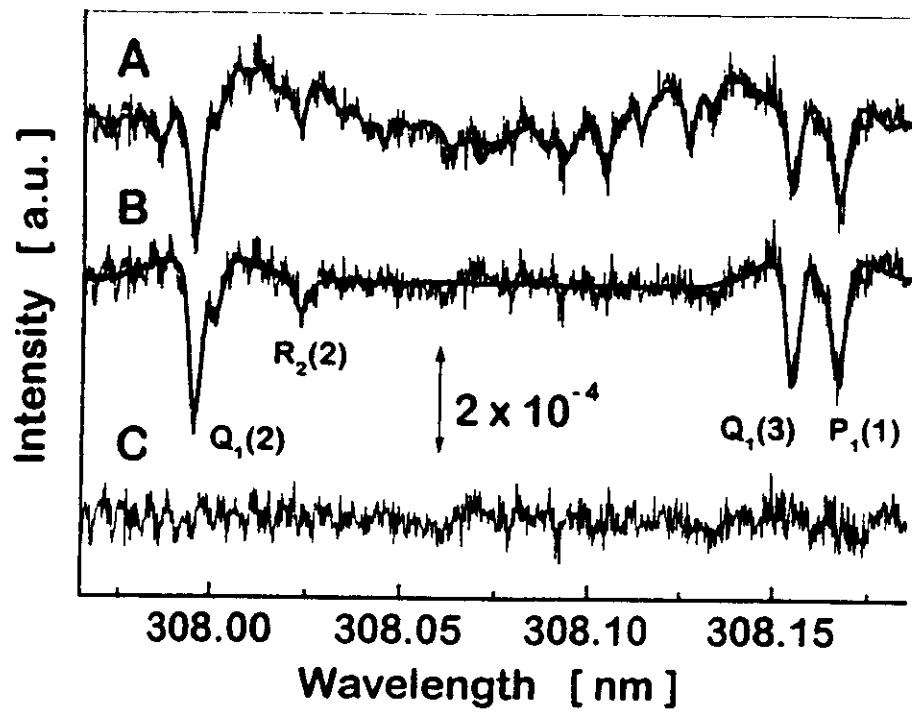
Carsten Leue, 1999



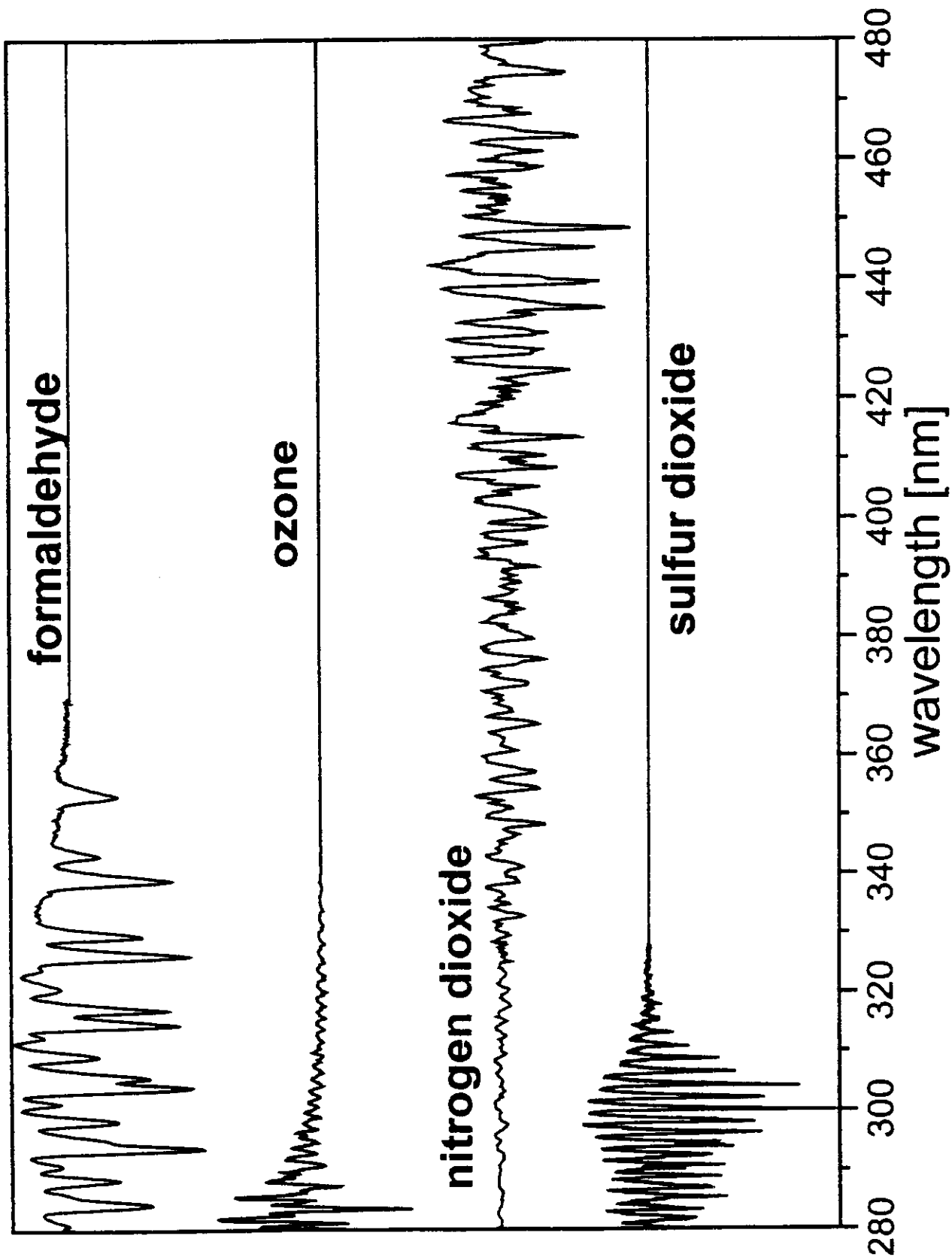
Vertical column of NO₂ [10^{14} molec/cm²]

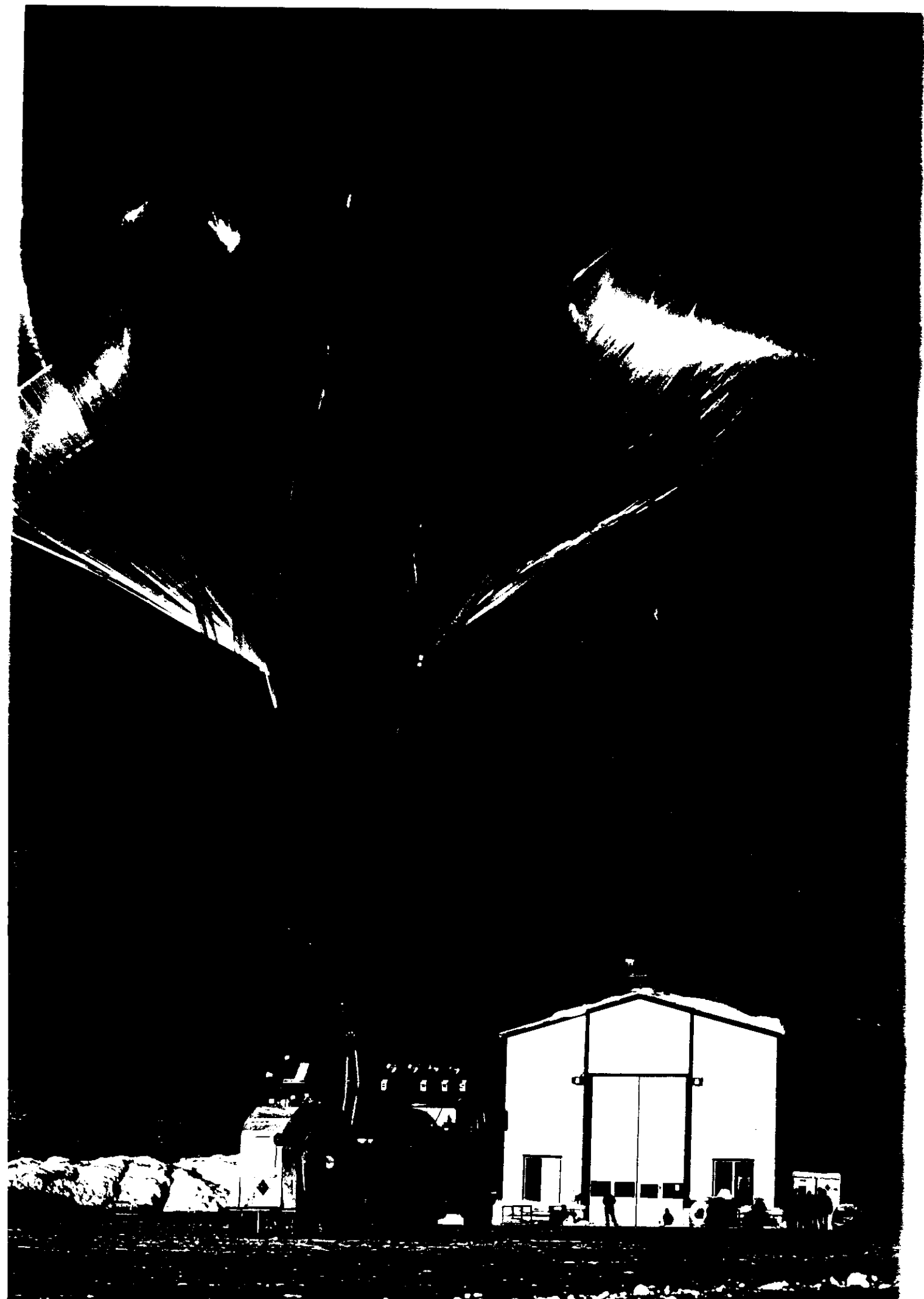


Darn et al. (1997)

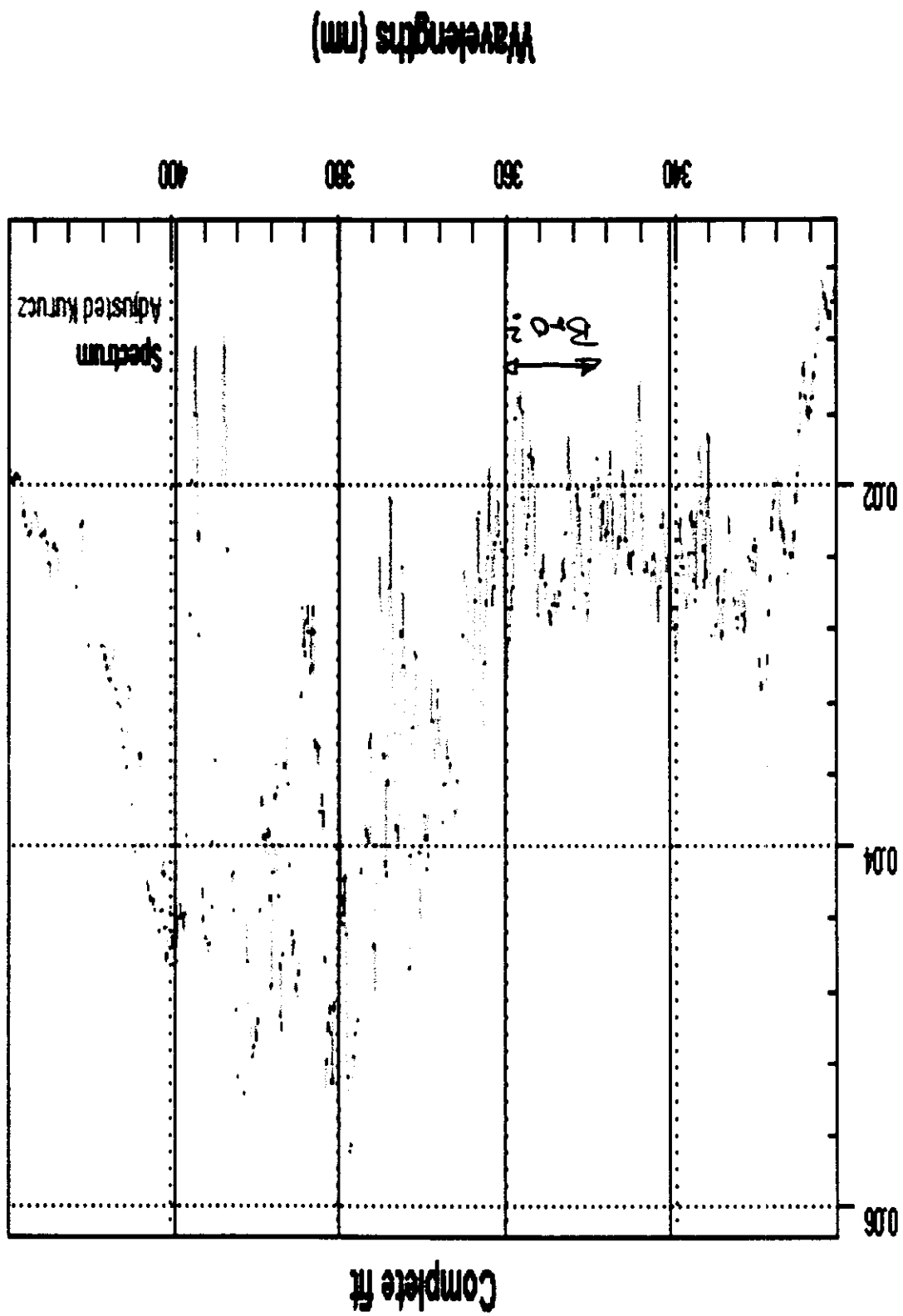


Dec 11, 2013 (G67)





Signal (counts)



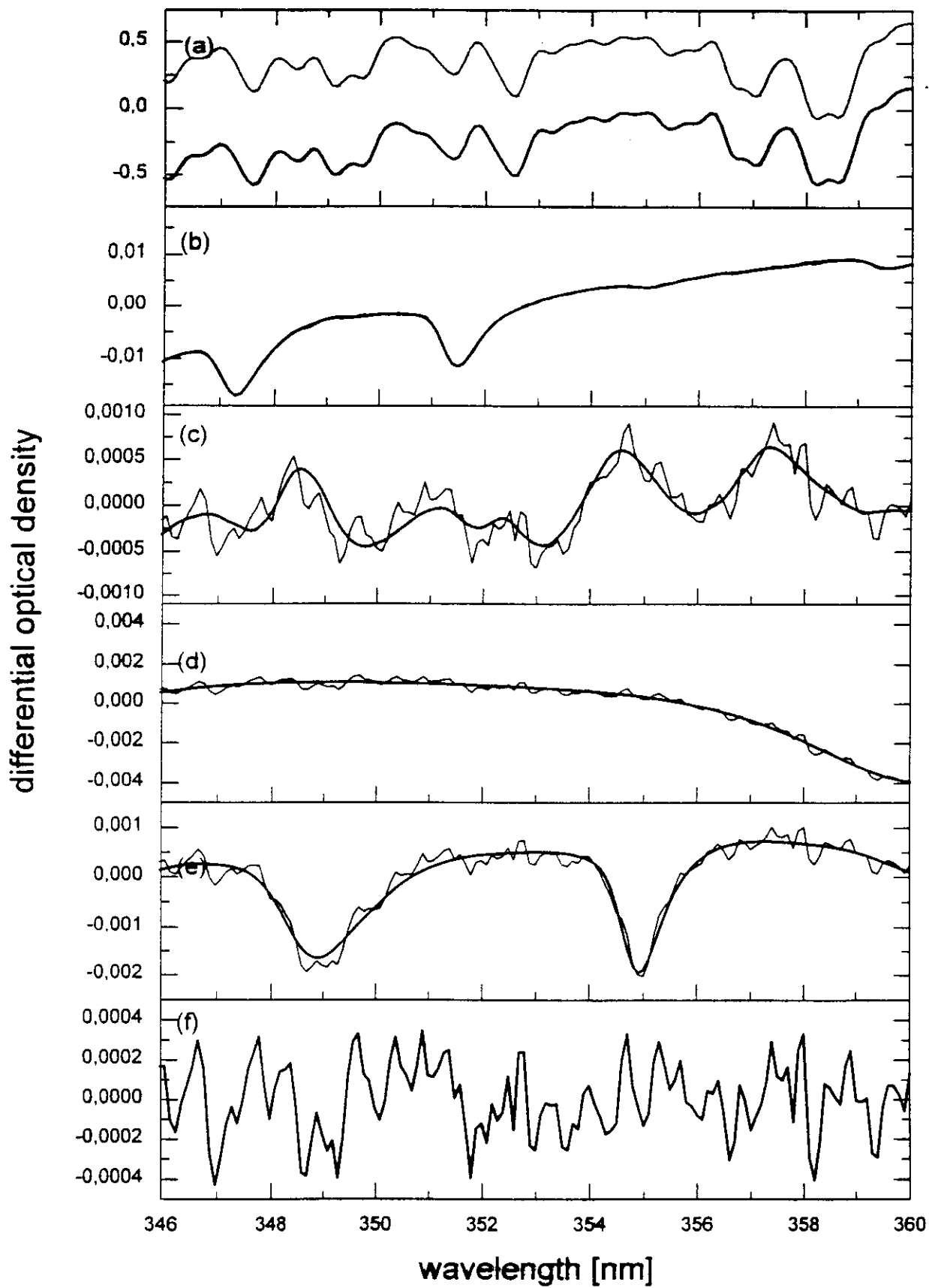
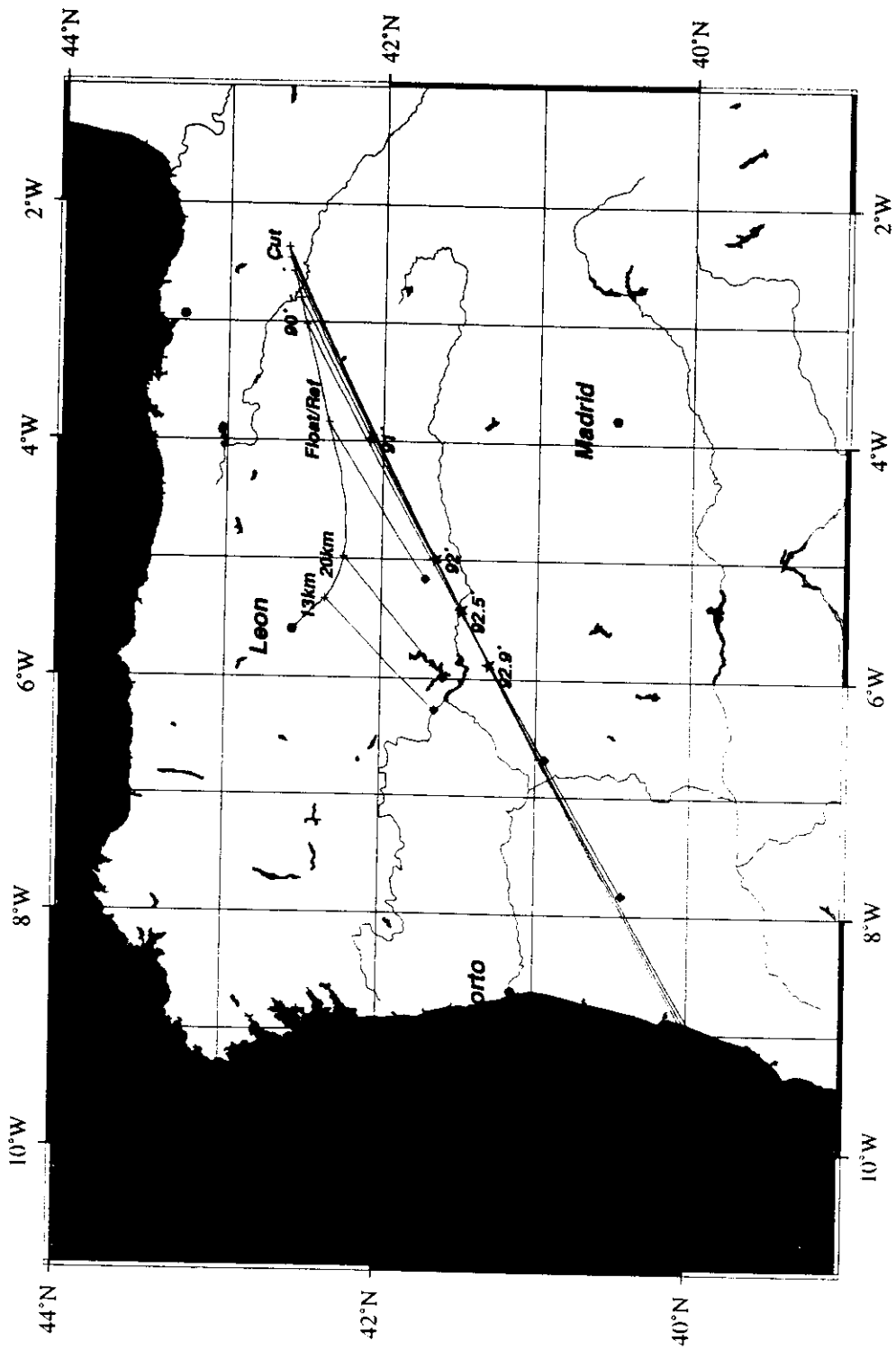
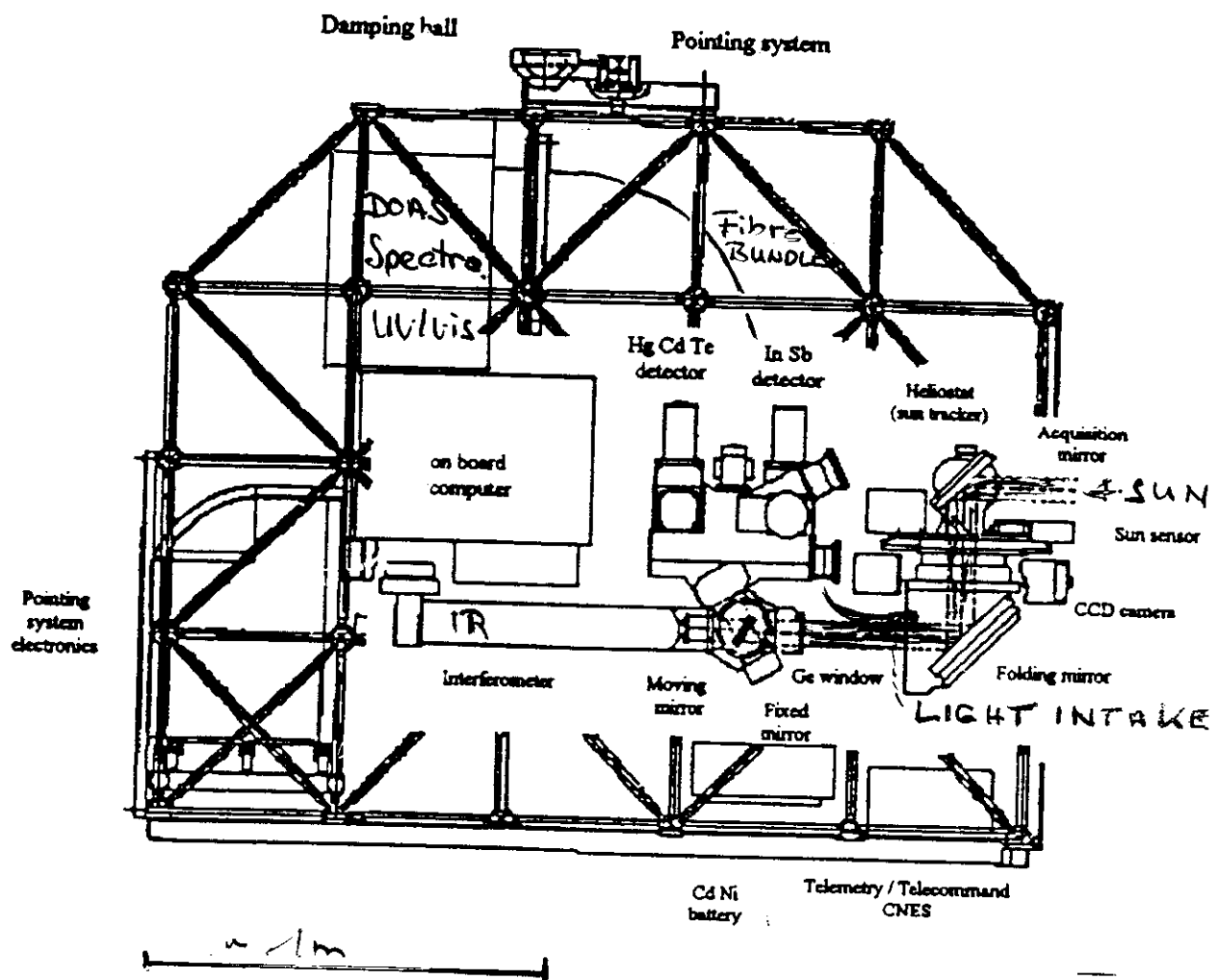


Fig: 2 a
Fitaenberger et al. (1998)



LPMA/DOAS PAYLOAD



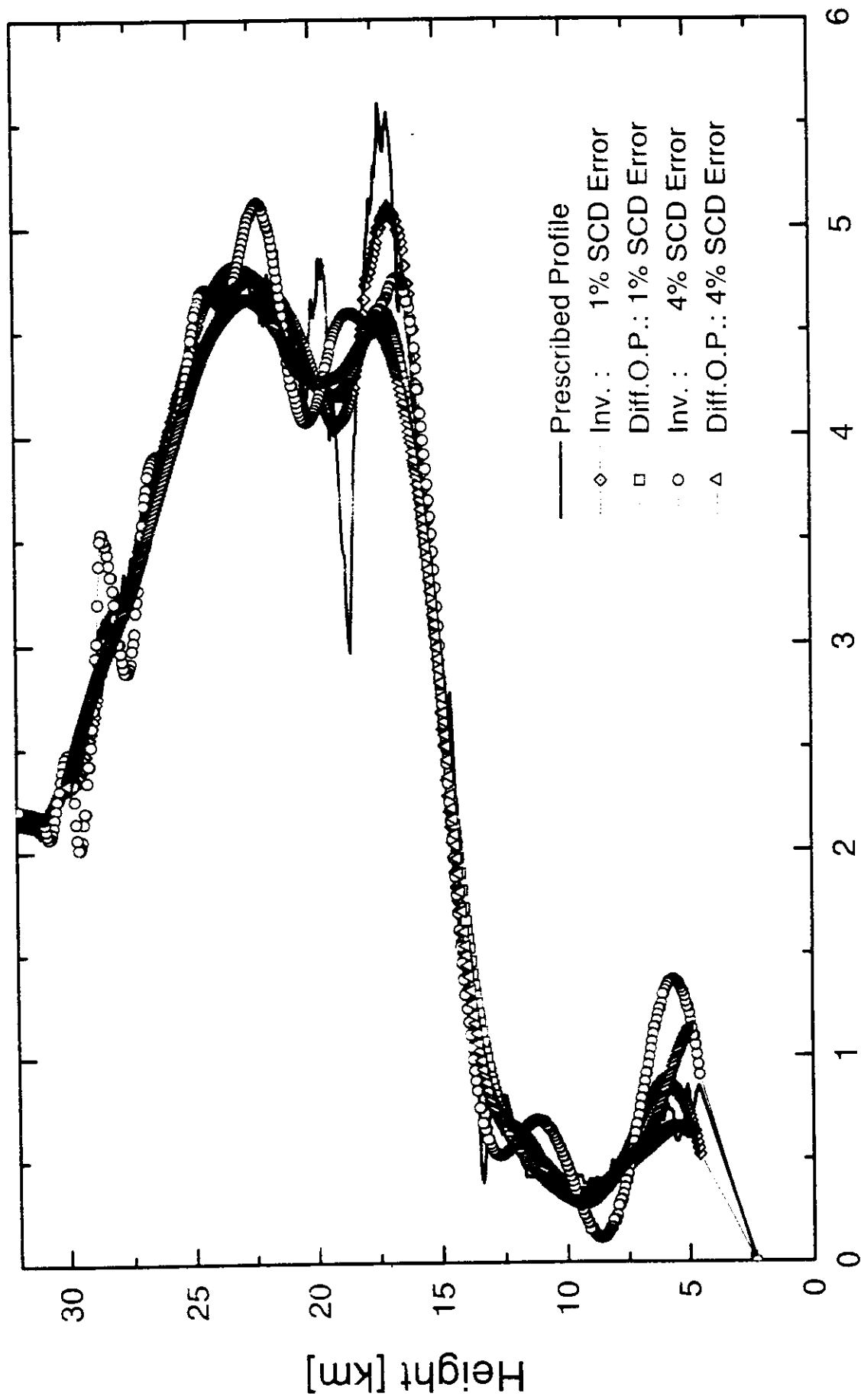


Fig. 6

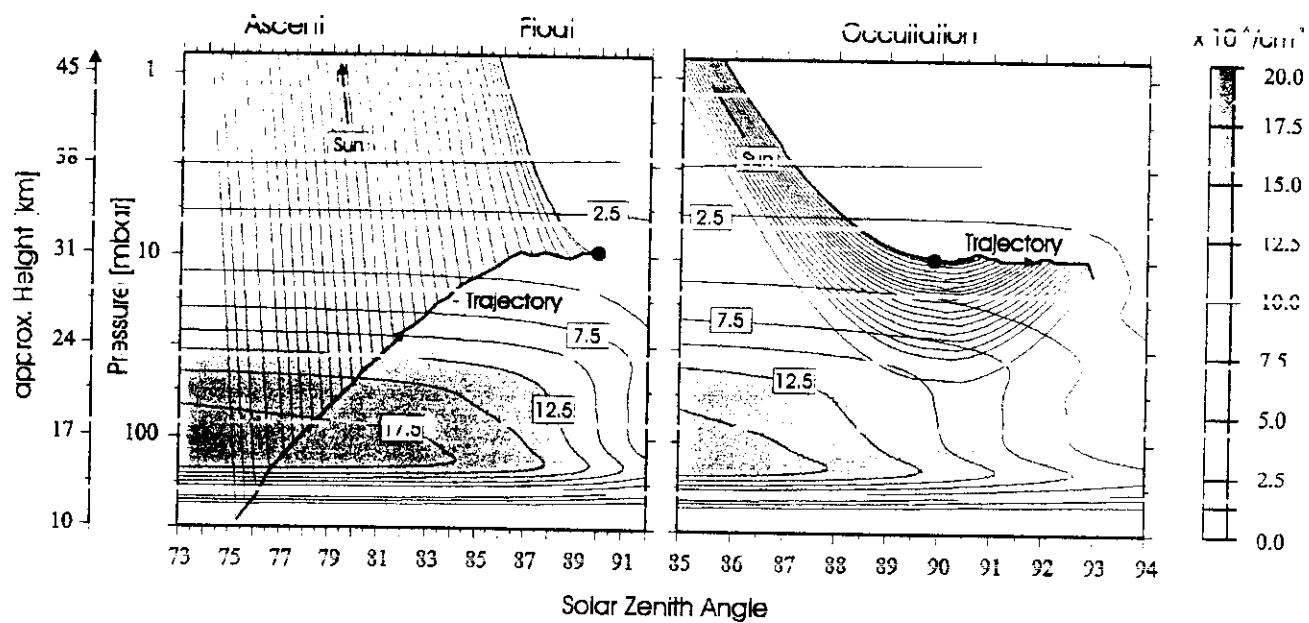


Figure 1: Harder et al.,

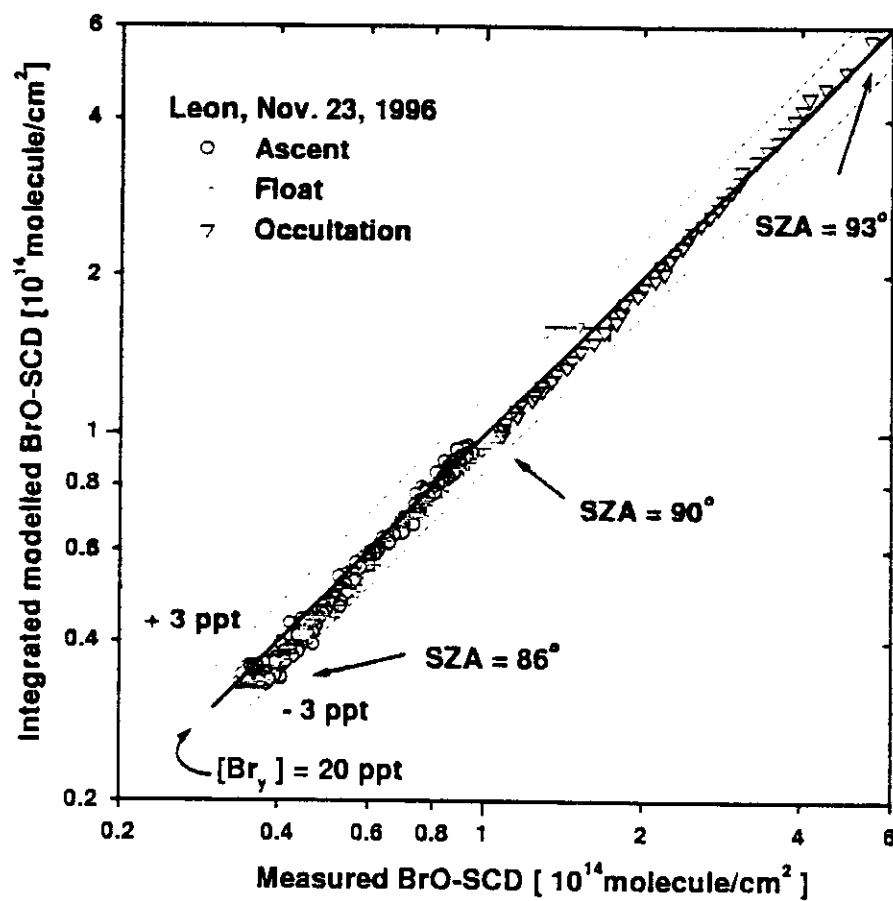
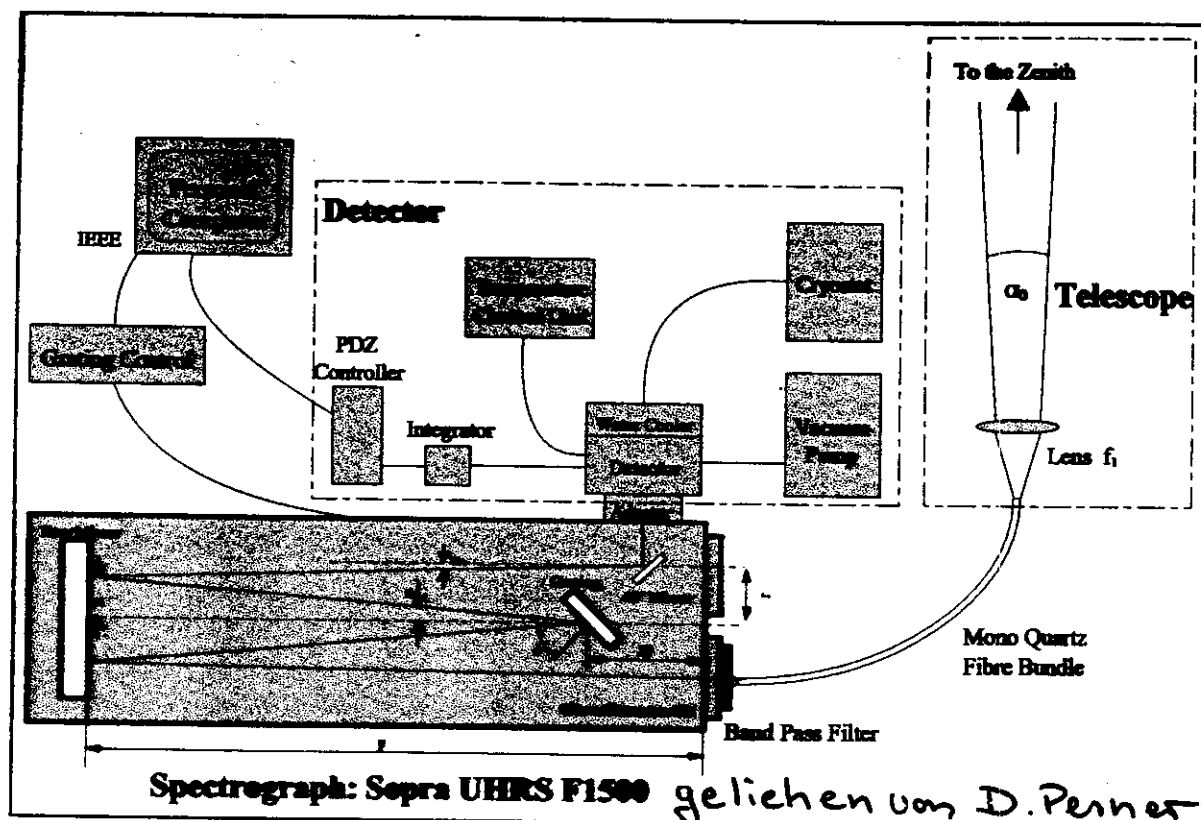


Fig. 2: Harder et al., 1999



Instrumental Set-Up



geliehen von D. Perner
(MPI-Chemie, Mainz)

Spectrograph:

Spectral Range	763.0-778.0 nm
Field of View	0.86°
Focal Length	1500 mm
Aperture	f/13.5
Blazed Grating	316 rules/mm
Resolving Power(770 nm, 7th Order)	$\Delta\lambda = 19.5 \text{ pm}$
Transmission	5.3 %

Detector:

Photo Diode Array Dimension	1x1024, 2.5x 25.4 mm
Quantum Yield (770 nm)	40 %



Institut für Umweltphysik, University of Heidelberg

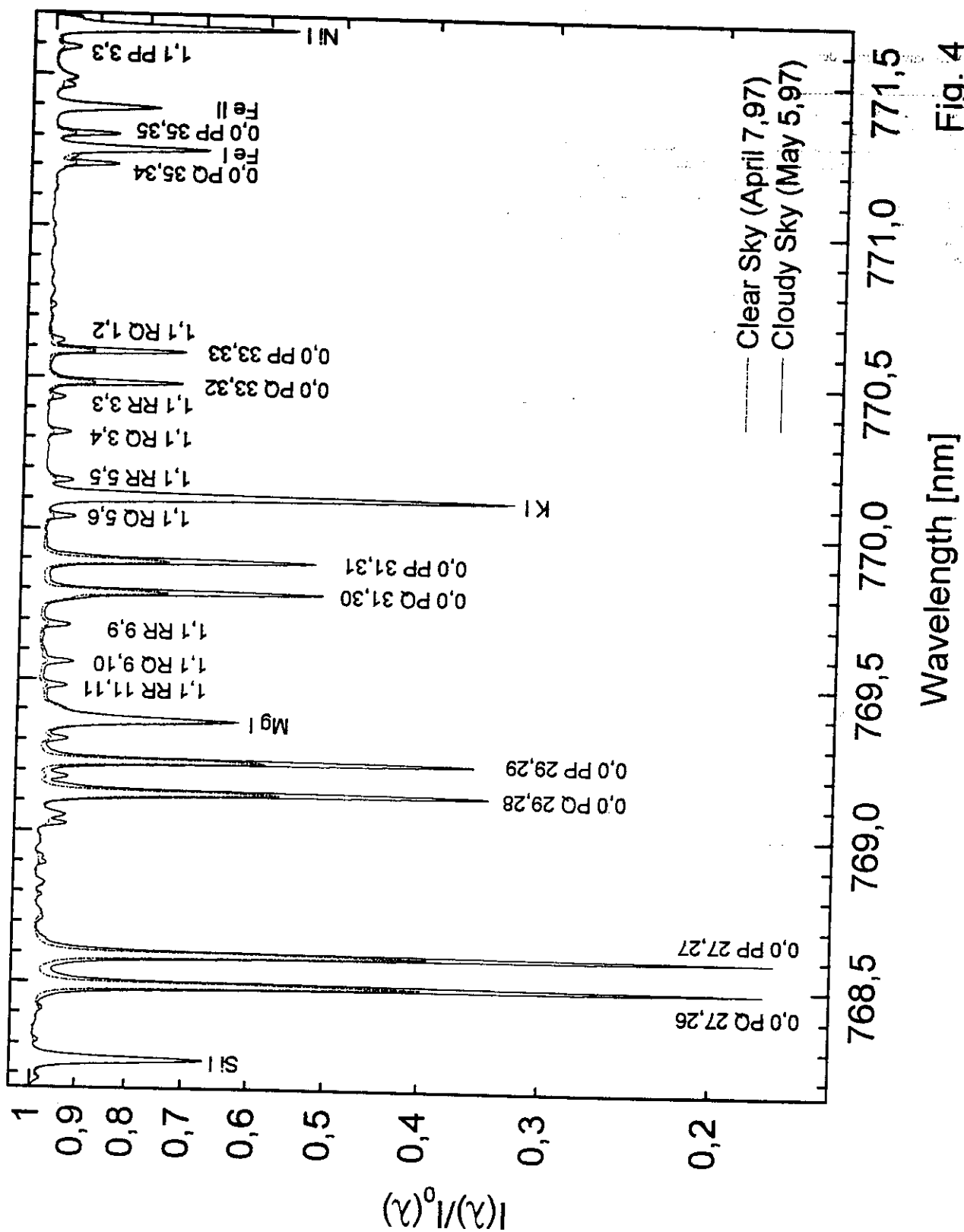


Fig. 4

Pfeilstädter et al. (1998)

"A) Other: (atmospheric noise) ...
 From: D. Pfeilstädter, W. ...
 Date: 12.04.98 (09:00) ...
 Subject: F7710: 0.000 ... (atmospheric noise)"

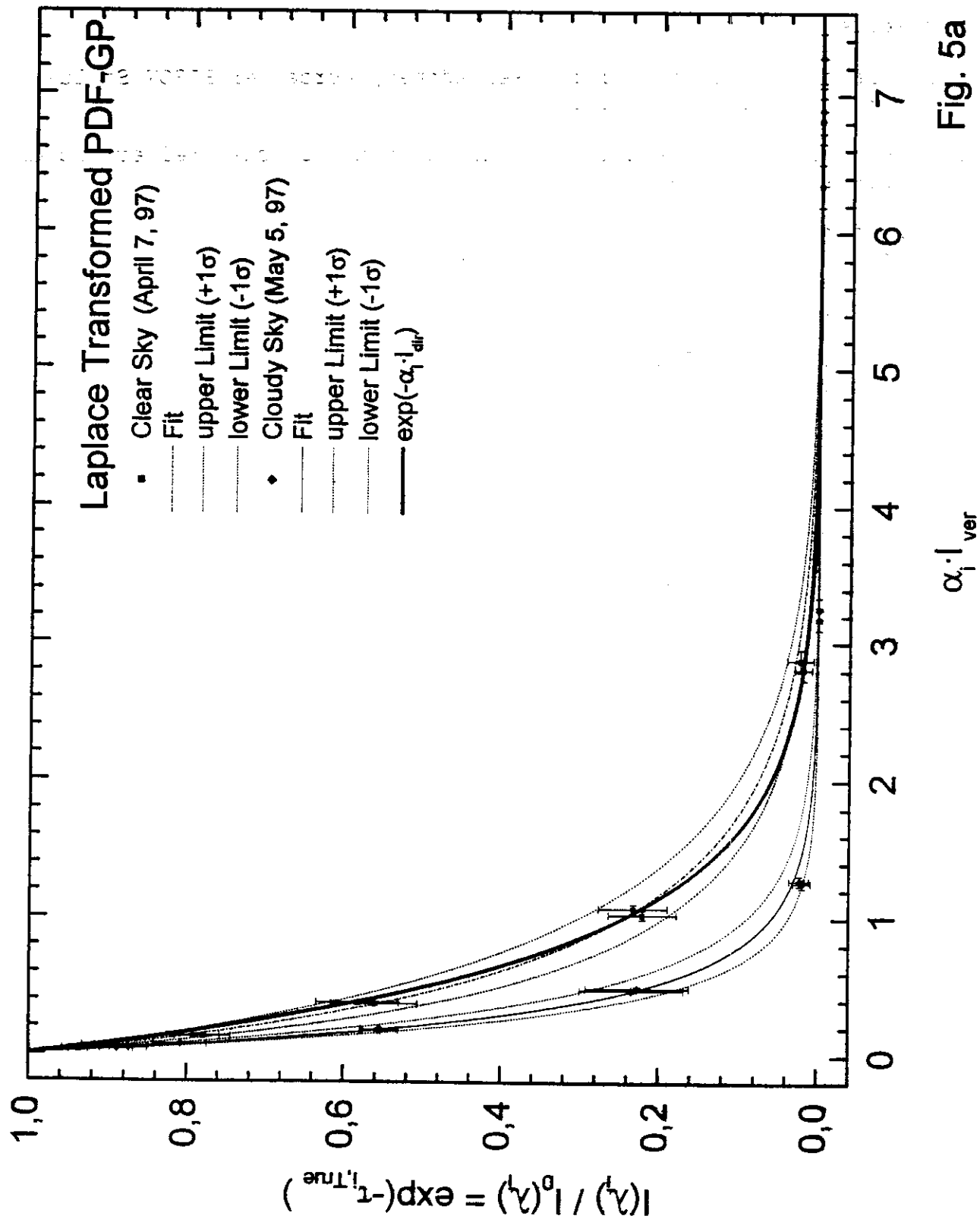


Fig. 5a

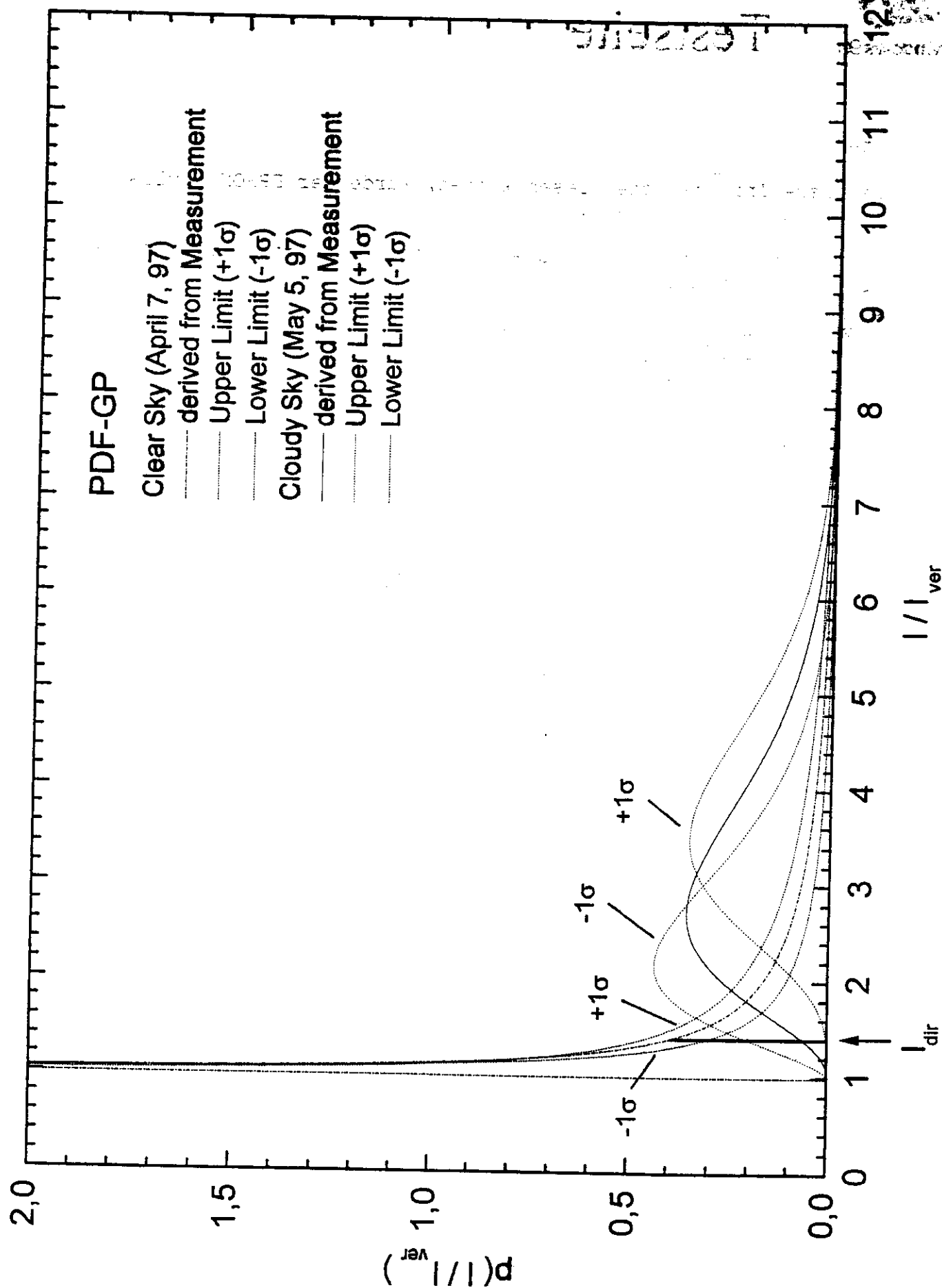


Fig. 5b
Pfeilschneider et al. (1998)

PDF-GPs for typical summer and winter cloudiness

