



INTERNATIONAL ATOMIC ENERGY AGENCY
UNITED NATIONS EDUCATIONAL, SCIENTIFIC AND CULTURAL ORGANIZATION



INTERNATIONAL CENTRE FOR THEORETICAL PHYSICS
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WORKSHOP ON CLOUD PHYSICS AND CLIMATE

23 November - 20 December 1985

ATMOSPHERIC CLOUD PHYSICS MEASUREMENTS -II
(Extra lecture notes)

C. SAUNDERS

University of Manchester, U.K.

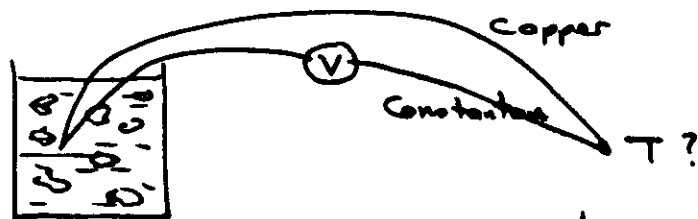


Calibrated Thermometer

Mercury or Alcohol

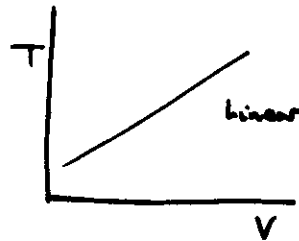
Accuracy 0.1°C

Thermocouple

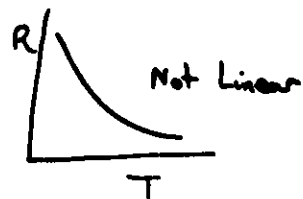
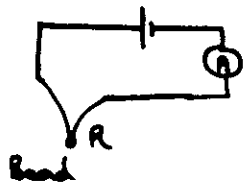


Constant Temperature Bath: Ice/Water at 0°C .

Accuracy 0.01°C

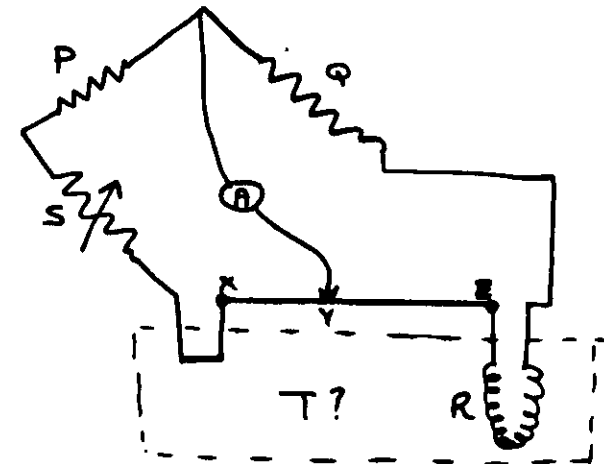


Thermistor



Accuracy 0.1°C

Platinum Resistance Thermometer

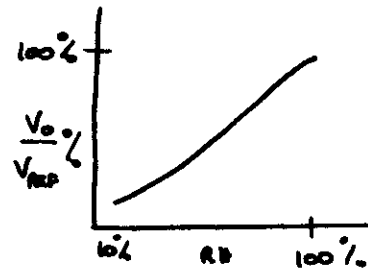
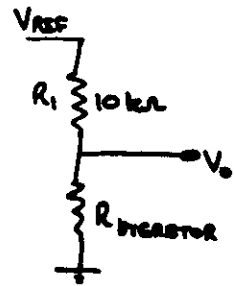


$$\frac{P}{Q} = 1 = \frac{S + (rXY)}{R + (rYZ)} \quad \text{For } A=0$$

r = resistance / length of wire XY .

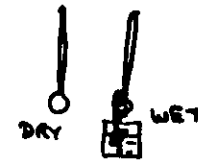
Manufacturers give R/T data in form of polynomial.

Linearising Circuit



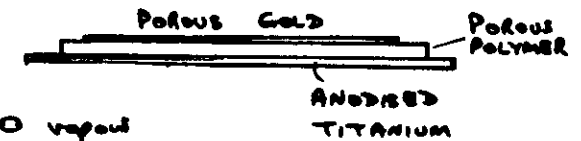
Humidity Measurements

- 1) Wet and Dry bulb.
(Sling psychrometer)



- 2) Lyman α Absorption. 121nm (key)
(Fast response, ≈ 2000 /sensor, optics prone to NaCl damage.)

- 3) Capacitance.

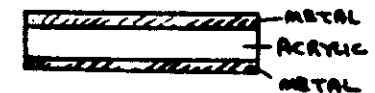


Polymer absorbs H_2O vapour

Known change. $C = 500pF \pm 1pF / \% RH$ change

Linear response. (2 seconds) Constant Sensitive
at ≈ 50 from Lee Integer, Vaisala.

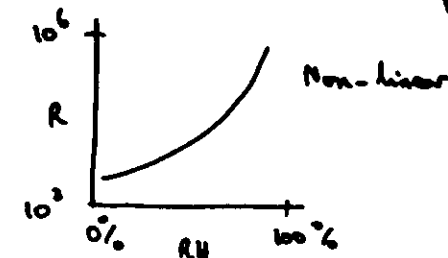
- 4) Carbon Hygriators



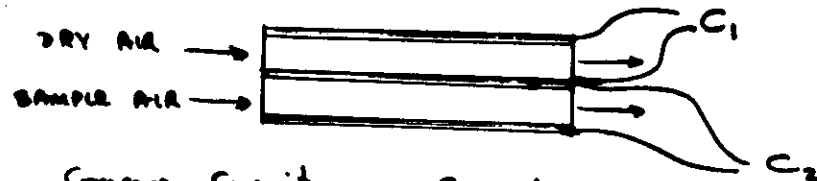
2x6cm.

Acrylic/carbon absorbs H_2O which changes R.

Response Time 0.2s.



- 5) Direct Capacitance Method.



Compare Capacitances C_1 and C_2

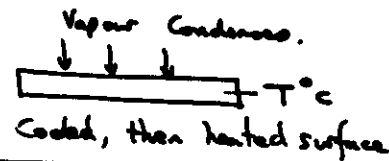
(E-1) for dry air = 6×10^{-4}

(E-1) for H_2O vapour = $1.6 \times 10^{-4} \rho$

$\rho \approx 9 \text{ g cm}^{-3}$

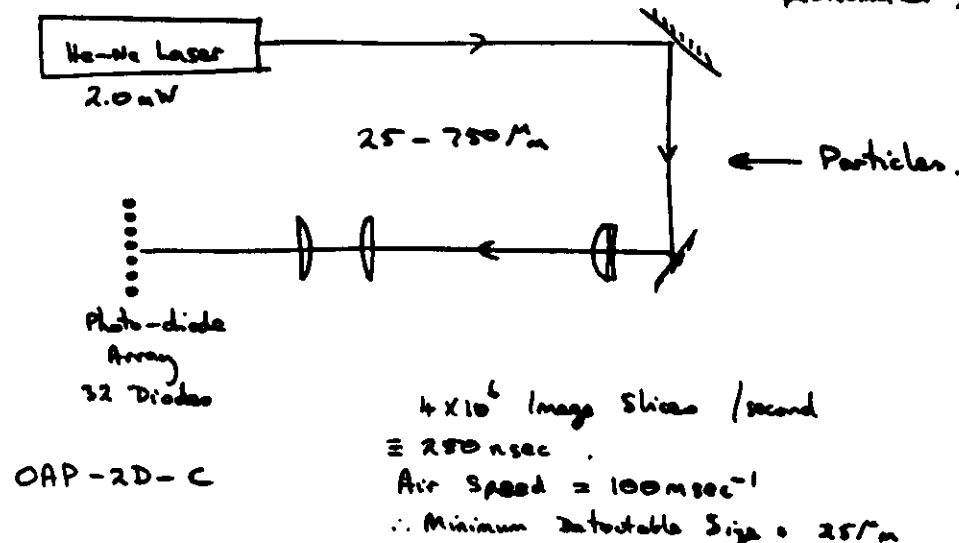
Dew Point (Frost Point)

Cambridge Hygrometer

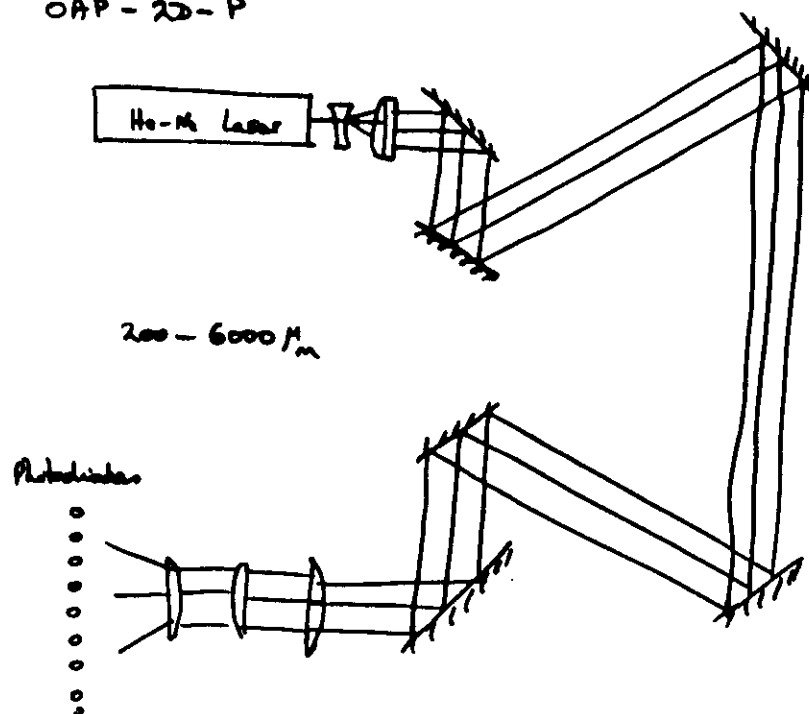


Liquid Water Content

- 1) Psychrometric Method. See Wishart pp 3 and 22
- 2) Rotating Impactor. Need Collision Efficiencies.



OAP - 22 - P



radar pulses. Studies of hydrometeors using airborne imaging devices correlated with one or more radars observing the same region of cloud or precipitation as the aircraft will lead to further understanding of storms.

- Are automatic particle-counting and sizing instruments giving an accurate representation of the cloud being observed? By giving the scientist a "look" at the cloud, imaging devices serve as a check on the integrity of data coming from other counting and sizing instruments. Data from electronic and electro-optical devices may be influenced by electronic noise, icing, or collection efficiency problems that might otherwise go undetected if the data look reasonable. Automatic sizing instruments give the size of the projected image; the measured size depends on orientation of the particles. This orientation can often be determined with imaging instruments. The accuracy and interpretation of impressions or replicas can also be checked by comparison with images obtained using imaging devices.

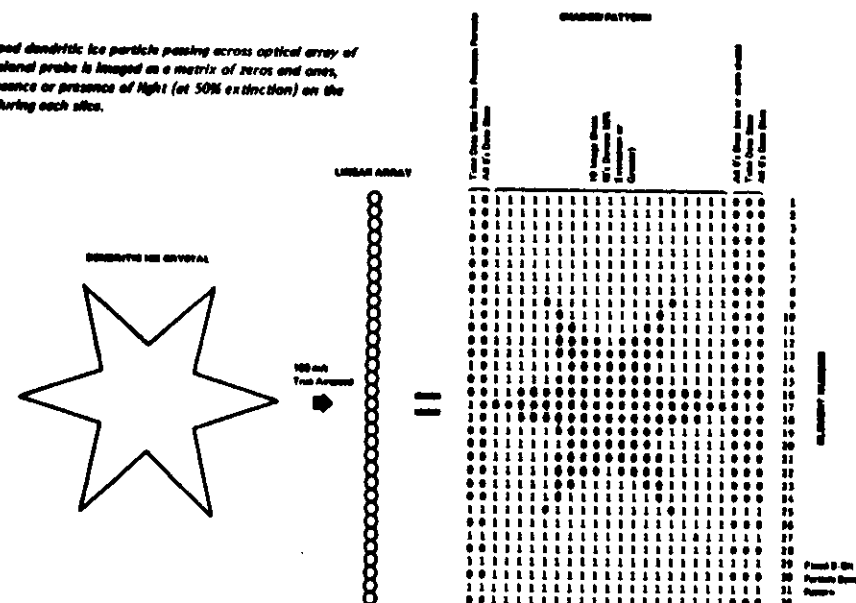
We will describe three imaging devices currently in use--- the two-dimensional optical array spectrometer probe of Particle Measuring Systems (PMS), Boulder, Colorado; the NCAR particle camera; and the airborne holography system of Science Applications, Inc., El Segundo, California.

The Optical Array Spectrometer Probe

The PMS two-dimensional array spectrometer probe, developed under the direction of Robert Knochenberg (of PMS), is a unique variation of the optical array particle-sizing probe described in the article by A. Heymsfield in this issue. In the sizing probe, the particles pass through a parallel light beam from a continuously radiating laser and a shadow is cast on a linear array of light sensors (photodiodes) located in the beam. The size of each particle is determined by electronically counting the number of sensors with light extinguished below a 50% intensity threshold by the shadow. In the two-dimensional probe, the entire array of sensors is sampled at a "slice" rate proportional to the true airspeed. By use of a high-speed, front-end data storage register, each sensor can transmit up to 1,024 bits of shadow information for each particle. A series of "image slices" is recorded across the shadow to develop a two-dimensional image.

Figure 1 illustrates the data format for a dendritic ice crystal. All together in the basic probe there are 32 sensors in the linear array, each imaging a portion of the light beam 25 μm in diameter. Because of the shadow cast by the particle, the light level falls to the threshold of detectability (50%

Fig. 1 Star-shaped dendritic ice particle passing across optical array of PMS two-dimensional probe is imaged as a matrix of zeros and ones, depending on absence or presence of light (at 50% extinction) on the optical sensors during each slice.



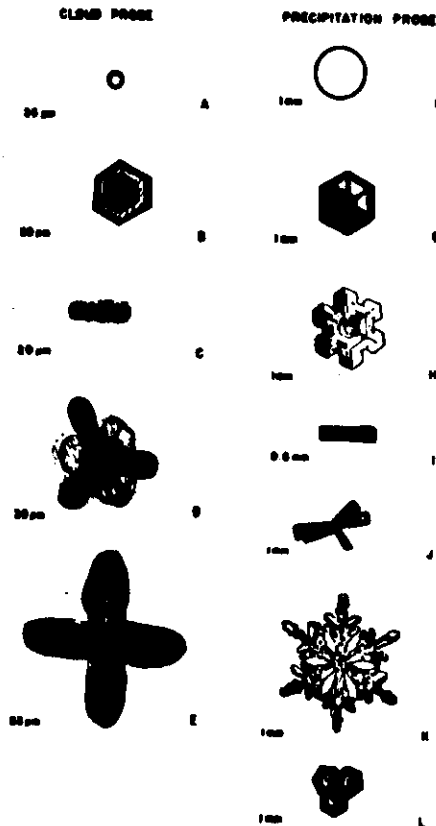


Fig. 4. Parts A-E are tracings of ice crystal microphotographs for sizes smaller than 100 μm as they would appear if viewed from above or focused on the optical array of the probe. Parts F-J are ice crystals larger than 300 μm as they would be focused on the optical array of the precipitation probe.

Parts B-E of Fig. 4 show tracings of ice particles smaller than 100 μm in length, which one would expect to be sized by the cloud probe. The plate ice crystal (B) is generally oriented with its long axis horizontally aligned to the array, and its cross section is therefore read as nearly spherical. The depth of field will be the same as that for a sphere of equivalent diameter, it will be sized properly, and the calculated concentration will be correct. But consider the column in part C. Its long axis will be horizontal in the atmosphere, but its orientation will be random when it passes through the linear optical

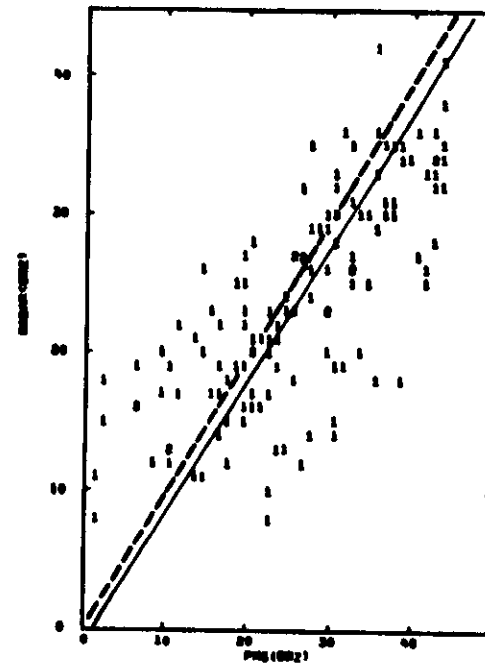


Fig. 5. Radar reflectivity factor measured by NSSL radar ($\text{dBZ} = 10 \log Z$) and calculated from PMS precipitation probe in nearly the same region of the cloud. Each 1 point is a 1 km average, and a 2 point indicates two 1 km points on top of each other. The dashed line is at 45° , and the solid line is a least-squares curve through the data points.

PROBE/RADAR comparison in rain.

array. Therefore, it will be read at values ranging from its full length (20 μm) to its width (6 μm) when passing through the array. A 100 μm column with a similar length-to-width ratio may be sized anywhere from 100 μm to about 30 μm . The distributions can be "transformed" on the basis of this random columnar crystal orientation (Heymsfield and Knollenberg, 1972) if all the particles are columnar.

Other problems may be associated with measuring the columnar particle in part C. Assume that it passes through the array at its full length. Even if in perfect focus on the array, its cross-sectional area per channel will be $6 \times 20 = 120 \mu\text{m}^2$, compared to the channel cross-sectional area of $20 \times 20 = 400 \mu\text{m}^2$. Therefore, the reduction of light intensity will be $120/400 = 30\%$, not enough to trigger the flip-flop switch or to register a count as a particle. In addition, the

Slide Impactors

• **Oil-Coated Slides.** One of the earliest measurements of cloud droplet sizes was made by Fuchs and Petajanoff (1937). A clean glass slide coated with a mixture of light mineral oil and petroleum jelly was used to capture cloud droplets and keep them submerged until they had been photographically recorded. The method was improved and used in an aircraft by Mazur (1943), who saturated the mineral oil with distilled water to prevent the droplets from diffusing into the oil.

Slides coated with castor oil were used in the first extensive set of measurements of droplet sizes in cumuliiform clouds by Weickman and Aufm Kampe (1953). With this method it was possible to collect droplets as large as 200 μm in diameter with no apparent shattering if the impact velocity was less than 100 m/s.

A large amount of droplet data was obtained by an automated sampler designed by Brown and Willett (1955). In their sampler three slides coated with silicone oil moved in rapid succession through an airstream and were photographed under a microscope in a cold cabin. The results for mean droplet distributions in trade-wind and summertime U.S. continental cumuli were reported by Braham, Battan, and Byers (1957) and by Battan and Reitan (1957).

These methods gave us the first details of the droplet spectrum at different geographical locations. A disadvantage of using them is that the sample must be recorded immediately, a procedure which is difficult in turbulent air. It is also necessary to know the exact time that elapsed between sampling and recording in order to apply diffusion corrections.

• **Magnesium Oxide Method.** Another widely used method involves coating a clean glass slide with a thin film of magnesium oxide. Droplets impinging on the film leave round holes which are proportional to their size.

This technique was developed and calibrated by May (1950) for drop diameters between 10 and 240 μm . For droplets larger than 20 μm in diameter, the ratio of droplet diameter to impression diameter was found to be 0.86; it remains constant with droplet size. Data reduction requires the investigator to examine the slide surfaces by microscope with a strong transmitted light and record the images photographically. This method is not affected by drop diffusion and droplets cannot coalesce, so the samples can be preserved. One disadvantage is that this layer is rather fragile in texture and can break off because of buffeting by the airstream. Another is that drops below 8 μm in diameter cannot be sized with certainty because the texture and grain size of the magnesium oxide interferes. Squires and Gillespie (1952) used this technique in a gun-type sampler which could be reloaded in about 50 s during flights. They exposed ten rods 3 mm wide (yielding a high collection

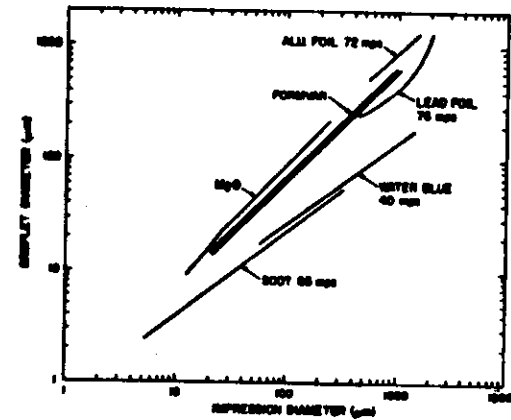


Fig. 6. Relation between droplet diameter and impression diameter for various sampling media.

Fig. 7. Drop impressions in coat layer. (Photo courtesy of J. Dye, NCAR.)



The foil impactors provided our first drop-size distributions for precipitation-sized particles ($>250 \mu\text{m}$ in diameter) in natural clouds. Yet there are still problems with these devices. One is that it is difficult to obtain a representative sample of large drops if they occur in low concentrations. Increasing the sampling volume yields an overexposure of the smaller drops, resulting in overlapping of the imprints. Moreover, during icing conditions instrument reliability depends on how successfully deicing elements were employed. It is not always possible to make a clear distinction between liquid and solid hydrometeors from impressions obtained in a mixed-phase cloud. Calibration of imprints is not available for solid particles. Under all conditions, data handling and analysis are tedious and subjective.

Replicator Devices

Replicator devices have been widely used in cloud physics studies. They are mechanized sampling devices using the well known Formvar technique to capture and permanently

encapsulate cloud particles (see MacCreedy and Todd, 1964; Spysers-Duran and Braham, 1967; Spysers-Duran, 1972a). They utilize a Mylar tape (usually a 16 mm polyester leader) which is coated with a solution of Formvar plastic and chloroform. (For airborne use, chloroform is preferred since it is nonflammable.) The continuously moving ribbon of Formvar is exposed in a cloud through a sampling slit several millimeters wide and then carried into a drying compartment where the plastic sets quickly. There, the encapsulated particles evaporate, leaving behind permanent replicas which can be sized and counted after suitable magnification. Since it is possible to obtain a continuous record through a cloud, the replicas can provide small-scale resolution of changes in cloud microstructure. Recently developed devices have the capability of viewing the replicas shortly after exposure so that tape speed and Formvar thickness can be adjusted in flight, as reported by Christensen, Keller, and Hallett (1974). Another major advantage of this method is that simultaneous recording of cloud droplets and ice crystals is possible (see Fig. 5).

Basically these devices are simple; however, they require a great deal of design compromise. In designs in which coatings

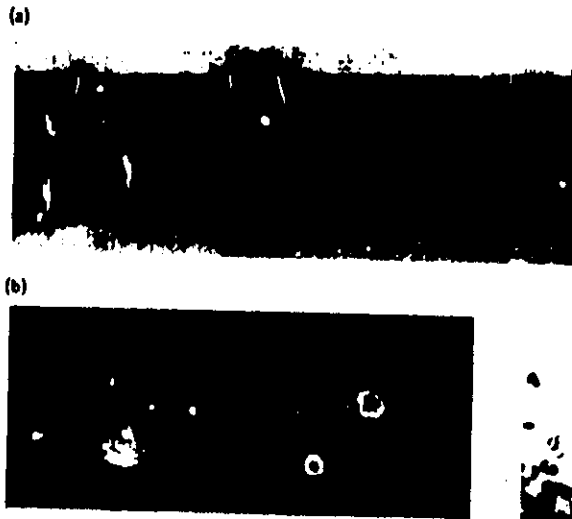


Fig. 4 Impressions of precipitation-sized particles in a lead foil exposed on the University of Chicago Lodestar aircraft (a), and in aluminum foil exposed on the South Dakota School of Mines and Technology T-28 aircraft (b). Smallest diameter is $250 \mu\text{m}$. (Sample a, courtesy of E. Brown, NCAR; sample b, courtesy of C. Knight, NCAR.)

Fig. 5 Replicas of supercooled droplets (A), a snow pellet (B), and ice crystal columns (C).



Radke-Turner Ice Crystal Probe

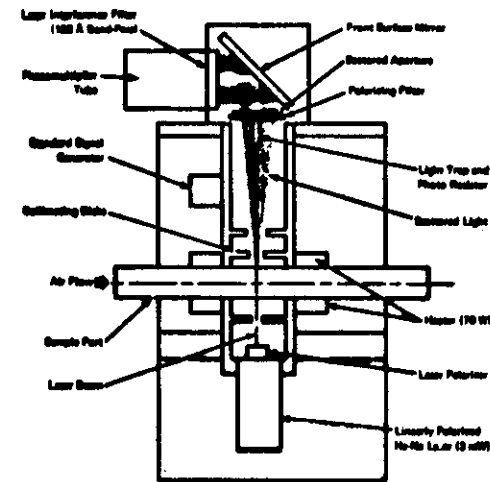


Fig. 1 Schematic representation of the University of Washington's automatic optical ice particle counter.

system so that linearly polarized infrared light is incident on particles passing through the sample pipe. The light sensor (solid-state device) detects the infrared light that is scattered at an angle of 90° (actually a cone of light around a scattering angle of 90°) after the light passes through an optical system containing a polarizing filter set for maximum extinction.

It can be seen from the description of the two instruments that the UW-IPC detects forward-scattered light while the Meo-IPC detects light scattered at an angle of 90° . As we see below, this difference becomes important in discussing mechanisms for the detection of ice particles in the two systems.

Mechanisms for Ice Detection

There are three possible mechanisms for the detection of particles in the two devices described above (see Turner and Radke, 1973, for a more detailed discussion):

- The rotation of the plane of polarization of the light beam, produced by the birefringent property of ice, as passes through the ice particles
- The detection of specularly reflected light from the external faces of ice crystals
- The detection of light scattered at a preferred angle by the ice particles.

Owing to the birefringent (or double refracting) property ice, linearly polarized light that is transmitted through ice will generally, be rotated in such a way that although the light

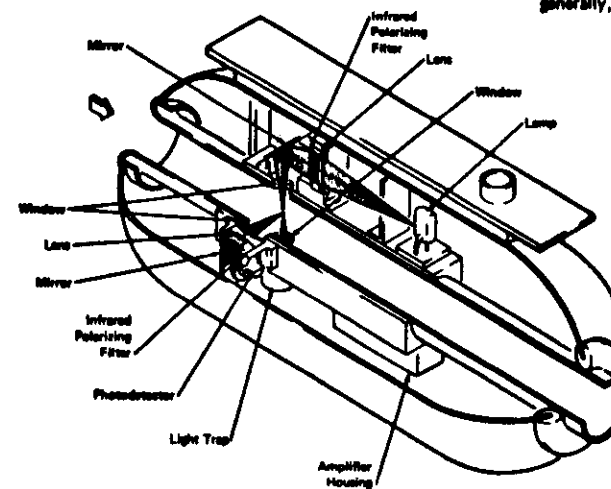
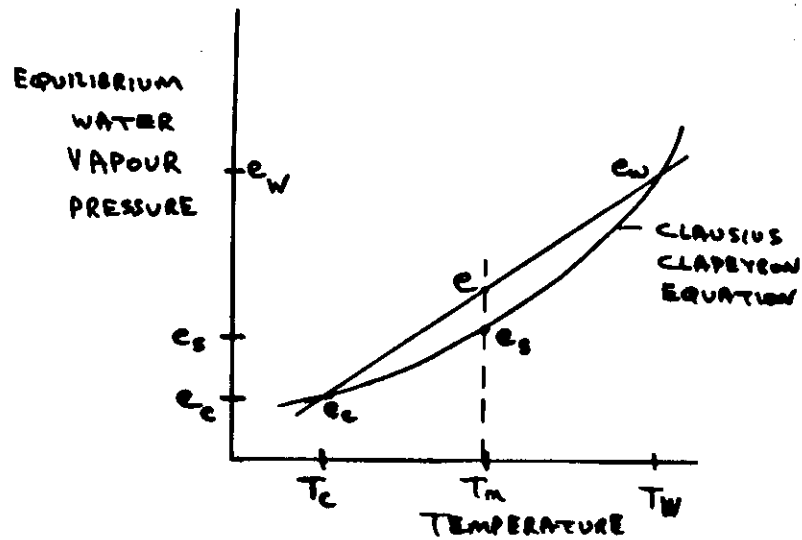


Fig. 2 Schematic diagram of the Meo Industries automatic optical ice particle counter. The pad is 45.7 cm (18 in.) long and 17.8 cm (7 in.) in diameter. The cylindrical opening in its center is 5.1 cm (2 in.) in diameter.

STATIC DIFFUSION CHAMBER FOR CCN

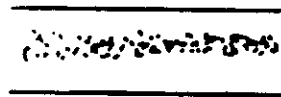


$$\text{Saturation Ratio, } s_w = \left(\frac{e_w - e_c}{2} + e_c \right) / e_s$$

$$s_w = (e_w + e_c) / 2e_s$$

$$\text{Supersaturation \%} = (s_w - 1) \times 100$$

$$S_w = \left(\frac{e_w + e_c}{2e_s} - 1 \right) \times 100 \%$$



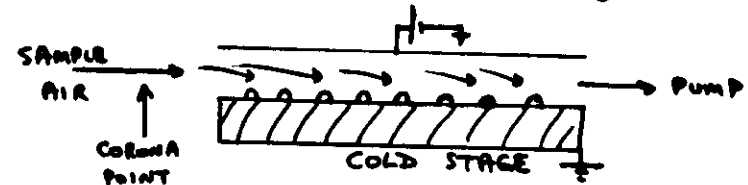
Camera views drops.

Ice Nuclei Detection.

Deposition Nuclei : Filters + Static Diffusion Chamber or Continuous Flow Chamber below water saturation.

Condensation Freezing Nuclei : Continuous Flow chamber above water saturation.

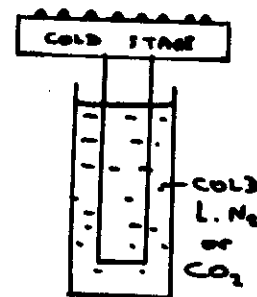
Contact Nuclei : Drop Freezing (Vali)



Charged nuclei are deflected in field onto supercooled (pure) water drops.

Immersion Nuclei

Sample Drop Freezing (Vali)



Cool drops containing the nuclei and watch for them to freeze. Note the number freezing at each temperature.

Contact Nuclei

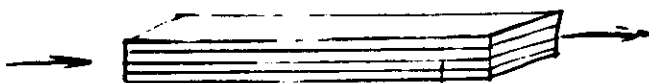
Spray Technique

Water Droplet Spray (20µm)

COLD STAGE

Filter + Sample.

DIFFUSION BATTERY



Many plates. Small particles diffuse to the plates and are captured. Only the large particles pass through.

Cascade Impactor

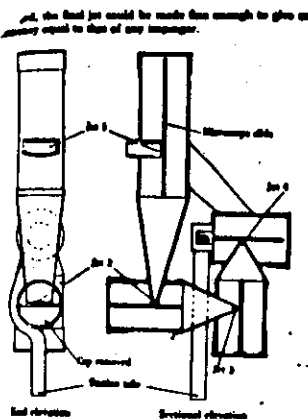


Fig. 2. Diagram of constant inventory

The latitude effect is situated hypothetically in the centre of the focal distribution because here the streamlines approximating the central region are undistorted in the plane of the measurement. This point is well shown in the wind-sandwich photograph reproduced in Fig. 1 (a), where the streamlines can be seen entering the orifice of the cylinder without any appreciable distortions near the top or bottom of the measurement area. After either the wind-sandwich or the wind-tunnel measurements, and it would therefore be impossible to get such good sampling with an orifice situated near one side. Streamlines in places remote to the paper from the top-left corner of a flow round a cylinder, but the orifice differs forwards into them and the distortions are not very large for better entry. It is found that when the impinger is situated at the centre of a cylinder, the streamlines are in a pattern over the orifice are most satisfactory when the size of the stream is moving at about 3 g g./min. (25 g.p.h.). The distance in space along the streamlines in the plane of the measurement also shows a decrease when near the cylinder decreasing to zero at the stagnation point), and the impinger is situated at the centre of the cylinder. With the orifice further from the centre of the cylinder, the sampling is found to follow in about two-thirds of the original value. The orifice is not selected enough above, therefore, the sampling is approximately halved, at any rate in the centre of the orifice, and realizes what is thought to be the best compromise between the conflicting requirements outlined in the preceding paragraphs.

The orifice has been made as large as the average capacities of the original impinger used for suction would allow. An attempt has been made to coverage the sides of the first impinger by means of tubes and impinger efficiency is thus increased. It is not possible to coverage the sides of the larger particles. It is, of course, not possible to coverage the sides of the smaller particles large enough to be removed by the orifice, but these have already been shown to be of great importance.

Wind vanes and anemometer. For use in the field the anemometer is fixed with the detachable wind vane vanes on top of Fig. 3. The vane is made from thin sheet metal with an area of 22 sq. cm. and three light steel rods support it rigidly 12 cm. to the rear. The three uppermost ends of these rods are a push for 100 cm. diameter of small-bore tubing attached to the body of the anemometer, i.e., the vanes can be readily detached. If the anemometer is to be used in the laboratory, the vane is about 10 cm. Fig. 3 also shows the method of suspension in the field. The structure is suspended from gillnets by means of a light cord attached to the point of balance. Lateron currents are prevented by the weight of the rubber cushion tubing, which hangs freely below the anemometer so that the latter may swing free despite wind.

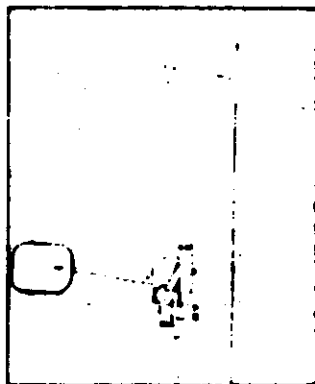


Fig. 1. Field sampling equipment.

Source of motion. A compressed air-operated injector unit similar to that described by Katherham is a very convenient portable apparatus for providing motion. Such an injector is capable of drawing up to 20 l./min. through the aspirator with ease and at an expenditure of only 4 l./min. of air from the bottle.

In the laboratory a small motor-driven pump may be used, and a convenient way to maintain any desired rate of flow is to fit a curved pressure orifice immediately behind the impinger. These orifices are described in Perry's *Chemical Engineers' Handbook*, 4th ed., p. 10-10. The orifice should be cut in a plate of brass or steel of such thickness that the orifice should be no less than half an inch square. Each orifice should be calibrated when in position behind the impinger. The orifice diameter required to give 175 l/min is about 1.3 mm. By breaking the last impaction jet sufficiently small it may be possible to make this jet perform the function of the second impaction jet. This is not recommended, as the *Orifice* chapter for use on still air. When sampling in still air conditions are very different from those shown in Table 10. As for the construction of the body of the impinger proper, tests of four approaches the orifice from all directions radially. The orifice should be cut in a plate of brass or steel, half an inch and less, whose products are in the orifice.

Aircraft Measurements

a) Vertical Wind ~ 1 second (100m) resolution.

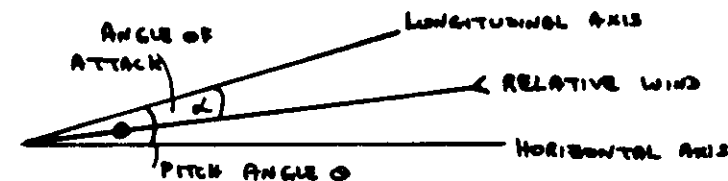
i) Clamp method: Slow down and let the plane "follow" the air vertical velocity. Find the vertical velocity from the altimeter rate of change.

ii) Accurate method : $W_{ag} = W_{ap} + W_{pg}$

w_{ap} = Air vertical velocity with respect to plane:

$w_{p2} = \text{Plane " " " " " " " ground.}$

Wag = Air " " " " " "



$$W_{ay} = \underset{\substack{\uparrow \\ \text{True Air Speed}}}{TAS} \sin(\theta - \alpha) + \int \underset{\substack{\uparrow \\ \text{Vertical Acceleration}}}{a_z} dt$$

$$TAS = IAS \left(\frac{0.1309 (^{\circ}K)}{\text{Pressure Alt in " of Hg}} \right)$$

IAS = Indicated Air Speed.
(from Pitot Tube)

Pitch, ϕ , Vertically stabilised accelerometer. (VSA)

α , Vane on nose boom, or side of aircraft.

Wpg, from the VSA.

b) Horizontal Wind . Doppler System + Yaw Vane.

$$\text{Wind} = \text{Air relative to ground} \quad V_{ag} = V_{ap} + V_{pg} \leftarrow \begin{array}{l} \text{'plane relative to ground'} \\ \text{Air relative to plane} \end{array}$$

Doppler radar $\rightarrow V_{pg}$ TAS + Yaw Vane Angle $\rightarrow V_{ap}$

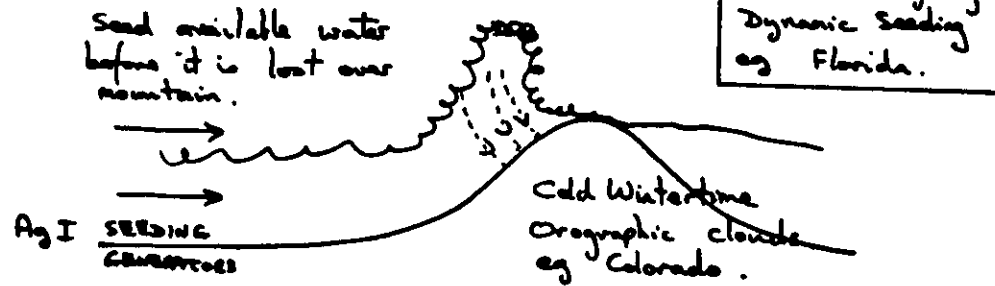
Objective To increase ice particle concentration.

Aims 1) Ice clouds are more efficient than water clouds at producing precipitation. [Increased Rainfall]

2) To reduce damage to crops from hail. [Hail Suppression.]

1) To Increase Precipitation:

a) Cloud physics study of clouds - is there water available in the cloud? Can this water be frozen by seeding? Will the precipitation fall where you want it?



2) To Reduce Hail:

Methods 1) Total Glaciation - Ice Crystals blow away. $> 10 \text{ gms AgI/min/km}^2$. Too Expensive.

2) Beneficial Competition. Many small particles compete for available water - so insufficient water for large hail to grow.

Works best for storms with warm cloud bases - frozen-drop embryos are efficient hail producers - so artificially seeded frozen-drop embryos give competition. Storms with cold bases have graupel embryos which start on small crystals higher up - competition seems inadequate. [eg Colorado]

Cloud Seeding (2)

Agents AgI - NH_4I - Acetone. (Better epitaxial fit than AgI.) still active 90km downwind. (4hrs) No deactivation. Cheaper is Titanium Oxide coated with AgI (25% cost)

Pyrotechnic flares at cloud base - 400 xtal / l after 4 mins. Aggregates in 13 mins. Traced by glider. 10" particles / gm of AgI.

Burn a AgI-acetone mixture on the ground or on aircraft generators. (400gm/hr.)

Top seeding, -14°C , 16-20,000', into feeder towers. 50gm droppable pyrotechnic flares.

Tracers To check whether seeding agent would get into the cloud at the right place.

eg Tag AgI with Titanium Dioxide. Detect on captured precipitation with ion probe analysis.

Other Methods

Carbon black, 0.1Mn particles - absorb solar energy.

Cool by releasing compressed air or gas.

Warm Rain - Hygroscopic seeding - NaCl - Langmuir chain reaction - drop breakup. Models show need for $\geq 10 \text{ ms}^{-1}$ updraught. No results yet.

Fog - Helicopter Downwash - Mixing. - Water jets to wash-out fog.

