



INTERNATIONAL ATOMIC ENERGY AGENCY
UNITED NATIONS EDUCATIONAL, SCIENTIFIC AND CULTURAL ORGANIZATION



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SMR/23/35

AUTUMN COURSE ON APPLICATIONS OF ANALYSIS
TO MECHANICS

22 September - 26 November 1976 - - - -

THEORY OF PLATES

Part IV : An elementary example of buckling for beams

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An elementary example of buckling for beams.

As introduction, we are going to study ~~an~~ example of buckling for beams: we will assume that the beam is simply supported at ends.

$$M(0) = M(L) = 0$$

(+ vertical displacement = 0)

First, we must complete the ^{general} equations written before by constitutive relations; we will consider only the elastic situation.

One knows that linear theories are often adequate in engineering sciences; from the simplicity of these theories, it results they are very used.

But it happens sometimes that linear theories are not adequate; it is the case in the study of buckling phenomena. We illustrate this remark, beginning to study ~~the case~~ of "buckling" an elementary case of buckling for beams.

We consider a beam ($0 < x < L$) with prescribed end thrust

$$(-P\vec{e}_1, P\vec{e}_1) \quad P\vec{e}_1 \xrightarrow{(\rightarrow \vec{e}_1)} -P\vec{e}_1$$

Experimentally, one knows that, when P increases from zero, the beam deforms by shortening: its center line remains straight. But, beyond a critical value $P_{critical} = P_{cr}$, the beam bends.

We recall the equations are

$$\begin{cases} \frac{d\vec{T}}{ds} = 0 \\ \frac{d\vec{M}}{ds} + \vec{T} \wedge \vec{T} = 0 \end{cases}$$



Boundary conditions imply $\vec{T} = \cos \theta = -P \vec{e}_1$

Let be θ the polar angle of unitary tangent vector $\vec{T}$;
then $\vec{T} \wedge \vec{T} = P \sin \theta \vec{e}_3$.

Second equation gives

$$\vec{M} = M \vec{e}_3$$

$$\boxed{\frac{dM}{ds} + P \sin \theta = 0}$$

Only the stress M (bending moment) is unknown. It is impossible to determinate M by the ^{above} equilibrium relation, and we must write a constitutive equation.

For this, first observe that the deformation is characterized by $\frac{d\theta}{ds}$. We take the constitutive equation

$$\boxed{M = EI \frac{d\theta}{ds}}$$

Where E is a Mechanics coefficient (Young modulus), I is a ~~geometrical~~ moment of inertia.

The equilibrium of the beam, ~~is~~ simply supported at ends as described by the problem

$$\begin{cases} EI \theta'' + P \sin \theta = 0 & (0 < s < L) \\ \theta'(0) = 0 \\ \theta'(L) = 0 \end{cases} \quad \left(\text{result from } M(0) = M(L) = 0 \right)$$

hence we have a solution for all P .

This problem is non linear.

We can also consider the linearized problem

$$\begin{cases} EI \theta'' + P \theta = 0 & (0 < s < L) \\ \theta'(0) = 0 \\ \theta'(L) = 0 \end{cases}$$

Observe that $\theta = 0$ is solution for all P . But, can ~~be~~ exist other solutions for suitable P ?

In addition, write the energy functional associated with each problem:

$$W = W(\theta, P) = \int_0^L \left\{ \frac{1}{2} EI \theta'^2 - P(1 - \cos \theta) \right\} ds$$

$$W_L = W_L(\theta, P) = \int_0^L \left\{ \frac{1}{2} EI \theta'^2 - P \theta^2 \right\} ds.$$

First. We study the linearized problem.

$\theta=0$ is solution for all values of P . The question is to know if other solutions can exist.

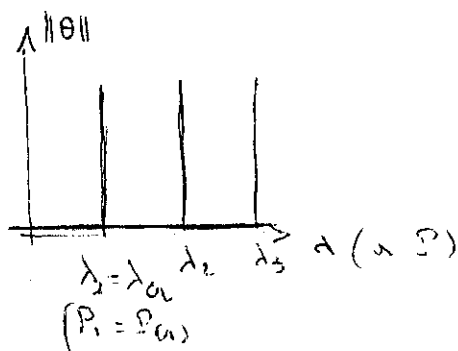
One put $\lambda = \frac{P}{EI} = \omega^2$ (because $\theta=0$ is the unique solution if $\lambda < 0$), and we have

$$\begin{cases} \theta'' + \omega^2 \theta = 0 \\ \theta'(0) = 0, \theta'(L) = 0 \end{cases}$$

The general solution of this differential equation is $\theta = A \cos \omega x + B \sin \omega x$. We have $\theta' = \omega (-A \sin \omega x + B \cos \omega x)$ and the first boundary condition furnishes $B=0$. The second one gives $A \sin \omega L = 0$ or (to obtain non trivial solutions) $\omega = \frac{n\pi}{L}$ $n \in \mathbb{Z}$, $n \neq 0$, and

$$\boxed{\lambda = \lambda_n = \frac{n^2 \pi^2}{L^2} \quad n \neq 0, n \in \mathbb{Z}} \quad \circ$$

Conclusions. (i) $\theta=0$ is the unique solution, ~~except~~ if $\lambda \neq \lambda_n$
(ii) if $\lambda = \lambda_n$, there exist non trivial solutions, which are undetermined



Physically, the beam remains straight except for exceptional thrusts $P_n = EI \frac{n^2 \pi^2}{L^2}$. This result is not acceptable: when P increases, we have, only for P_{cr} , solutions $\neq 0$, which are undetermined. Beyond P_1 , $\theta=0$ is again the unique solution, until P_2 !

Third conclusion. The linearized problem (hence a linear problem) cannot describe buckling phenomena.

To study buckling phenomena, it is absolutely necessary

Now, we study the non-linear problem.

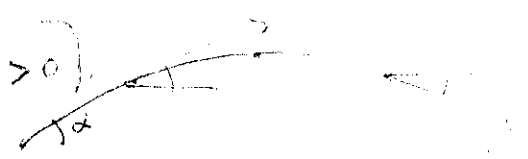
$$(1) \quad \begin{cases} \theta'' + \lambda \sin \theta = 0 & (0 < s < L) \\ \theta'(0) = 0 \\ \theta'(L) = 0 \end{cases} \quad \left| \begin{array}{l} \text{Observe that} \\ \theta = 0 \text{ is a solution} \\ \text{for all } \lambda \in \mathbb{R} \\ \text{(i.e. for each} \\ \text{thrust } \Xi) \end{array} \right.$$

We are going to search a non trivial solution $\theta(s)$ with following properties:

$$(2) \quad \theta \text{ is decreasing} \quad (\theta' \leq 0)$$

$$(3) \quad \begin{cases} \text{symmetry with regard to } s = \frac{L}{2} \\ \theta\left(\frac{L}{2} + \sigma\right) = -\theta\left(\frac{L}{2} - \sigma\right) \end{cases}$$

Therefore, $\left[\theta\left(\frac{L}{2}\right) = 0 \text{ and } \theta(0) = \alpha > 0 \right]$



We obtain, by multiplying (1) by θ' :

$$\frac{d\theta}{ds} = -\sqrt{\lambda} \sqrt{2(\cos \theta - \cos \alpha)}$$

where α is a suitable integration constant: $\alpha = \theta(0)$ (which is supposed > 0)

We obtain

$$(4) \quad \left[s = -\frac{1}{\sqrt{\lambda}} \int_0^\theta \frac{d\varphi}{\sqrt{2(\cos \varphi - \cos \alpha)}} + \frac{L}{2} \right]$$

But $s = 0$ for $\theta = \alpha$, hence

$$\boxed{0 = -\frac{1}{\sqrt{\lambda}} \int_0^\alpha \frac{d\varphi}{\sqrt{2(\cos \varphi - \cos \alpha)}} + \frac{L}{2}}$$

which is an equation for α . From a solution α of this equation, we obtain, via (4), a non trivial solution of the problem (1)

More precisely, introduce a new unknown ψ by

$$\begin{cases} \sin \frac{\alpha}{2} = k \\ \sin \frac{\theta}{2} = k \sin \psi \end{cases}$$

Then :

$$(i) \quad \frac{1}{2} \cos \frac{\theta}{2} \theta' = k \cos \psi \psi'$$

$$\frac{\theta'}{2} \text{ and } \boxed{\theta'^2 = \frac{4k^2 \cos^2 \psi}{1 - k^2 \sin^2 \psi} \psi'^2}$$

$$(ii) \quad \cos \theta = 1 - 2 \sin^2 \frac{\theta}{2} = 1 - 2k^2 \sin^2 \psi$$

$$\cos \alpha = 1 - 2 \sin^2 \frac{\alpha}{2} = 1 - 2k^2$$

$$\Rightarrow 2\lambda (\cos \theta - \cos \alpha) = 4\lambda k^2 (1 - \sin^2 \psi) = 4\lambda k^2 \cos^2 \psi$$

The equation $\theta'^2 = 2\lambda (\cos \theta - \cos \alpha)$ gives

$$\boxed{\psi'^2 = \lambda (1 - k^2 \sin^2 \psi)}$$

If we assume $0 < \alpha \leq \pi$, we have $0 \leq \frac{\theta}{2} \leq \frac{\alpha}{2} \leq \frac{\pi}{2}$.
on $0 < \lambda < \frac{L}{2}$, and ψ (as θ) is decreasing, hence $\psi' < 0$
and

$$\psi' = -\sqrt{\lambda} \sqrt{1 - k^2 \sin^2 \psi}$$

$$d\lambda = -\frac{1}{\sqrt{\lambda}} \frac{d\psi}{\sqrt{1 - k^2 \sin^2 \psi}}$$

Boundary conditions are

$$\theta = 0 \Rightarrow \begin{cases} \lambda = \frac{L}{2} \\ \psi = 0 \end{cases}$$

$$\theta = \alpha \Rightarrow \begin{cases} \lambda = 0 \\ \psi = \frac{\pi}{2} \end{cases}$$

We obtain

$$\lambda = -\frac{1}{\sqrt{\lambda}} \int_0^{\psi} \frac{d\psi}{\sqrt{1 - k^2 \sin^2 \psi}} + \frac{L}{2}$$

and, for $\psi = \frac{\pi}{2}$:

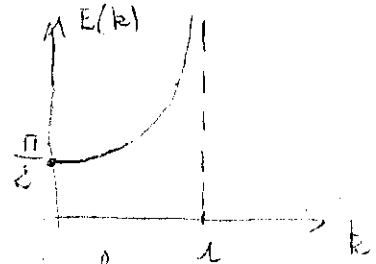
$$0 = -\frac{1}{\sqrt{\lambda}} \int_0^{\pi/2} \frac{d\psi}{\sqrt{1-k^2 \sin^2 \psi}} + \frac{L}{2}$$

or, it is the same :

$$(5) \quad \boxed{\frac{L\sqrt{\lambda}}{2} = \int_0^{\pi/2} \frac{d\psi}{\sqrt{1-k^2 \sin^2 \psi}} = E(k)}$$

which is an equation for k , hence for α .

It is very simple to observe that the graph of $E(k)$ as the following form



Therefore, if $\frac{L\sqrt{\lambda}}{2} > \frac{\pi}{2}$, there exists a solution k for this relation

Consequence

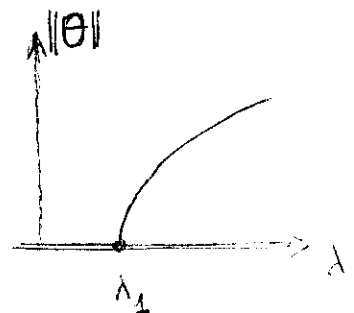
If $\lambda > \frac{\pi^2}{L^2} = \lambda_{cr}$ (or if $P > \frac{EJ\pi^2}{L^2} = P_{cr}$),

there exists a non trivial solution of the ^(non linear) problem, given by

$$\delta = \frac{L}{2} - \frac{1}{\sqrt{\lambda}} \int_0^{\psi} \frac{d\psi}{\sqrt{1-k^2 \sin^2 \psi}}$$

with k is given by (5).

Such a solution can be schematized on the picture :



In addition, observe that the critical thrust P_{cr} is the first "eigenvalue" of the linearized

Physically, the ^{exhibited} solution of non linear problem is acceptable, contrary to the linearized problem.

Now, we have (for $\lambda > \lambda_{cr}$) 2 solutions : the trivial one and the non trivial one. We are going to compare the value of energy for these solutions.

We have $W(0, \lambda) = 0$.

$W(\theta, \lambda)$ is proportional to

$$\bar{W}(\theta, \lambda) = \frac{1}{2} \int_0^L \{ \theta'^2 + 2\lambda (\cos \theta - 1) \} ds = \int_0^{\frac{L}{2}} \{ \theta'^2 + 2\lambda (\cos \theta - 1) \} ds$$

but, for the solution, we have

$$\theta'^2 + 2\lambda (\cos \theta - 1) = 4\lambda k^2 \cos^2 \psi$$

with previous notation ; and

$$ds = -\frac{1}{\sqrt{\lambda}} \frac{d\psi}{\sqrt{1 - k^2 \sin^2 \psi}}$$

We obtain

$$W(\theta, \lambda) = 4\sqrt{\lambda} k^2 \int_0^{\pi/2} \frac{\cos 2\psi d\psi}{\sqrt{1 - k^2 \sin^2 \psi}}$$

It is not difficult to observe that

$$\boxed{W(\theta, \lambda) < 0 = W(0, \lambda)}$$

This inequality shows that the non trivial solution is more ~~can~~ stable than the trivial one, ~~can~~ from an energy point of view.