



INTERNATIONAL ATOMIC ENERGY AGENCY
UNITED NATIONS EDUCATIONAL, SCIENTIFIC AND CULTURAL ORGANIZATION



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SECOND SCHOOL ON ADVANCED TECHNIQUES
IN COMPUTATIONAL PHYSICS
(18 January - 12 February 1988)

SMR.282/31

ACCELERATOR PHYSICS

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Area di Ricerca Sincrotrone, Trieste, Italy

COMPUTING IN ACCELERATOR PHYSICS

A. Wulich
SINCROTRONE TRIESTE

COMPUTING → Accelerator Design
Accelerator Operation

1. Lesson:

Accelerators, an introduction

Basic equations for transverse motion

Computation of linear optics

2. Lesson:

Basic equations for longitudinal motion

Nonlinear transverse motion

Resonance effects in circular accelerators

Simulation of particle motion, tracking

3. Lesson:

Chaotic trajectories of transverse motion

Collective effects

Beam-beam effect

Beam-environment interaction

Numerical field calculations

ACCELERATORS (introduction)

used for $\rightarrow$

Elementary particle physics,
colliders

Light sources

Health service

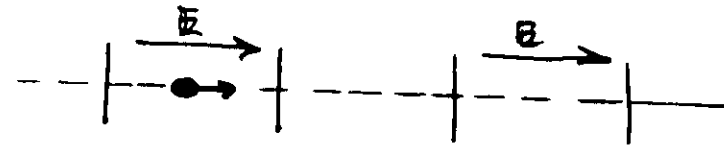
Industry (compact sources)

types of accelerators $\rightarrow$

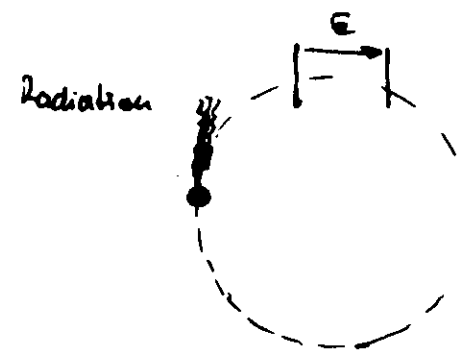
Linear

Circular (synchrotron, storage ring,
cyclotron, microtron, ...)

Linear Accelerator:



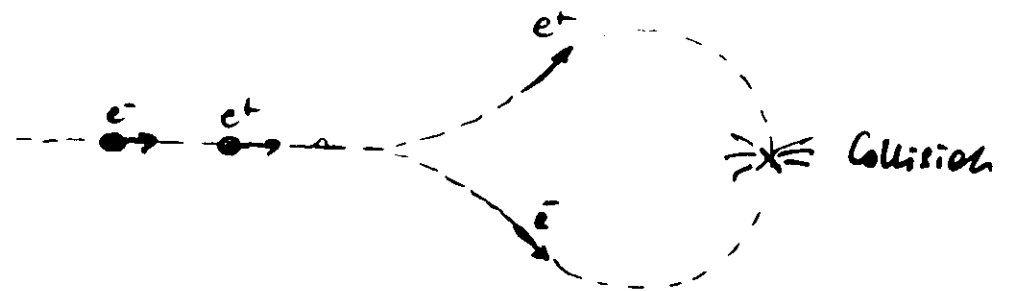
Circular Accelerator:



Storage rings
Synchrotrons

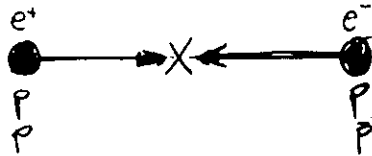
Producers: (e^+e^-)
Synchrotron Radiation
Beam beam effect
(p) large bending
fields

SLC (Stanford):

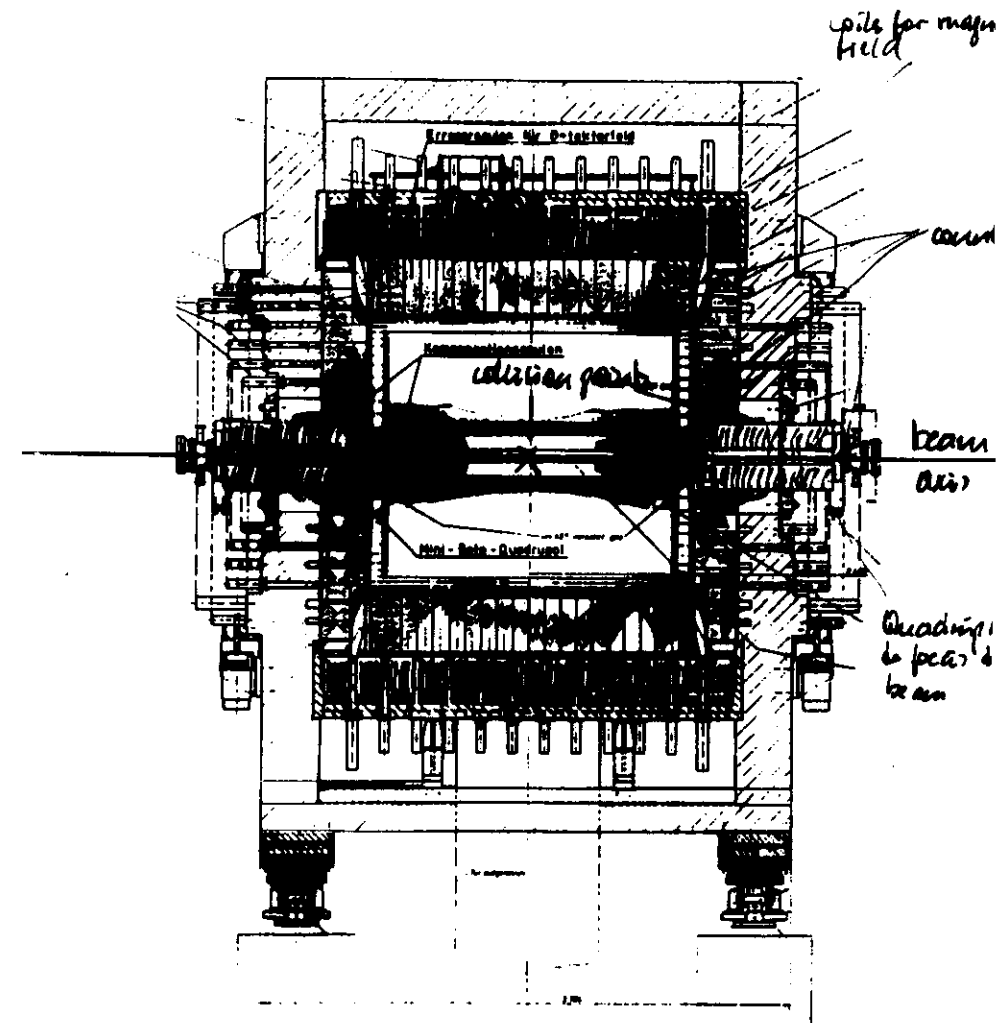


Accelerators for High Energy Physics

Energy of colliding particles



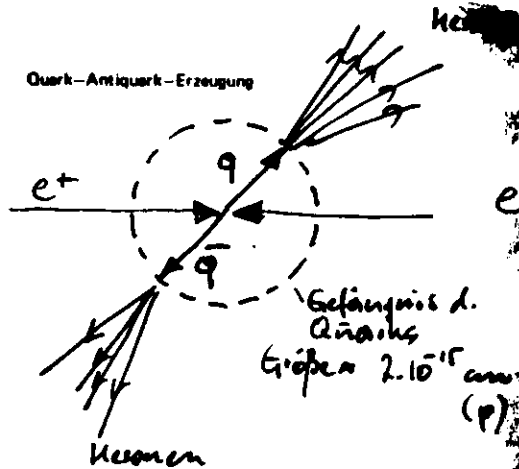
is used to create showers of new particles. Their traces are detected by large apparatuses (DETECTORS) and evaluated by computers.



ARGUS at DORIS II (DESY)

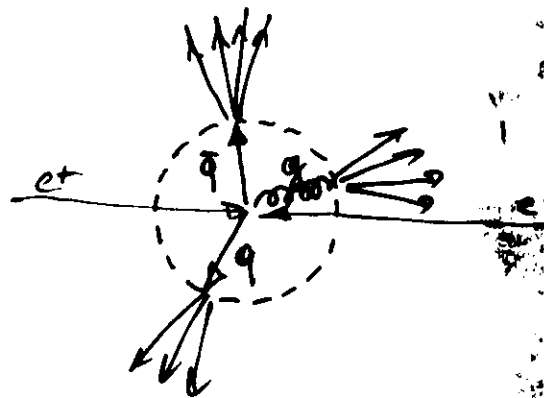
2-jebevent

Quark-Antiquark-Erzeugung



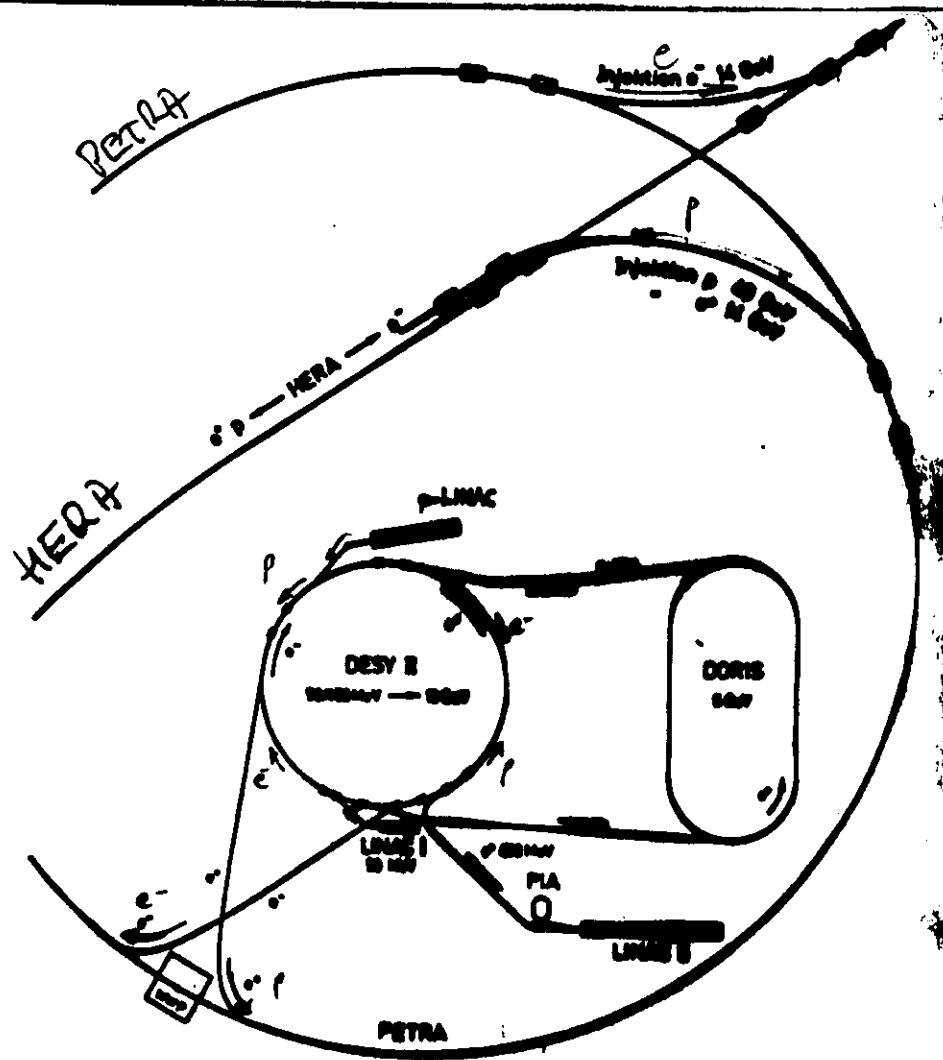
"Multi-Hadron"-Erzeugung

3-jebevent

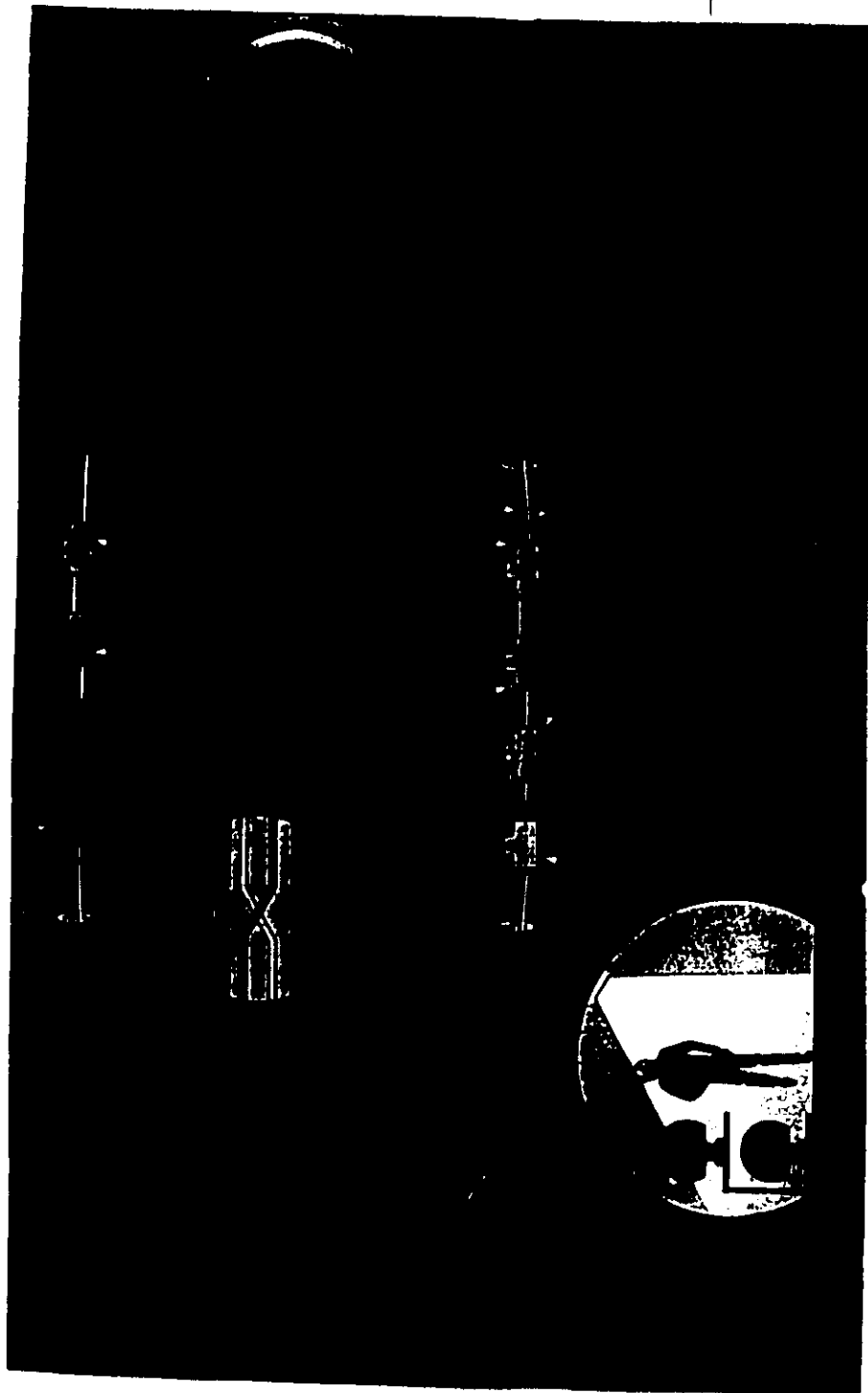


Quark-Antiquark-Erzeugung
mit abgestrahltem Gluon

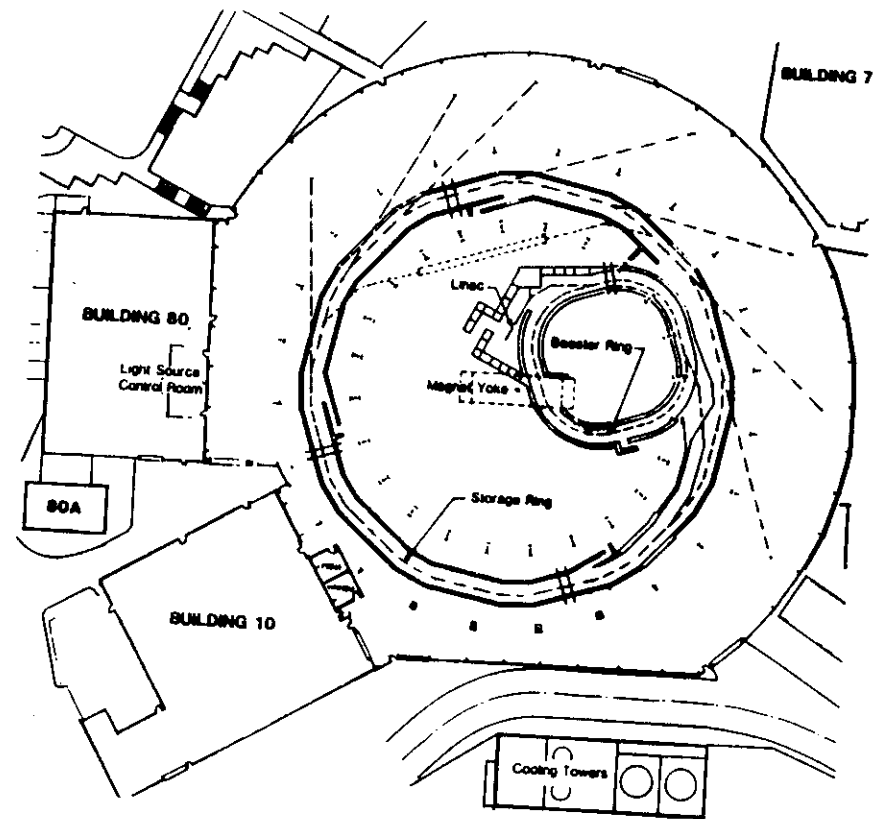
Am Speicherring PETRA registrierte
Computer-Rekonstruktionen von
"Ereignissen" bei der Kollision von
Elektronen mit Positronen.



DESY - accelerator



Radiation Sources:

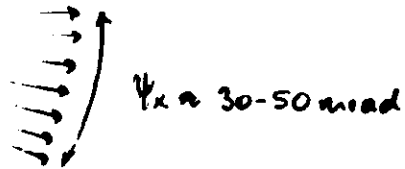
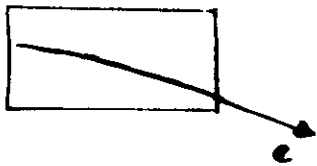


Berkeley 1.5 GeV Light Source

RADIATION

Basic principle: Radiation is emitted by relativistic charged particles circulating in a magnetic field.

I. BENDING MAGNETS:



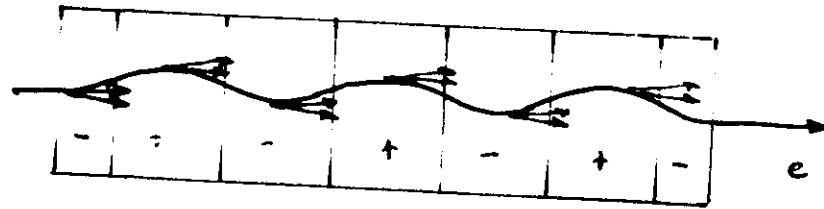
SR is emitted with $\rightarrow$

Horizontal divergence: $\psi_x \approx 30-50 \text{ mrad}$

Vertical divergence: $\psi_z = \pm \frac{1330}{\gamma} \left(\frac{\lambda}{\lambda_c} \right)^{0.43} \dots$
 $\approx \pm \frac{1}{\gamma}$

$E = 2 \text{ GeV}$ ($\gamma = 4000$) $\Rightarrow \psi_z = \pm 0.33 \text{ mrad}$

II. WIGGLER



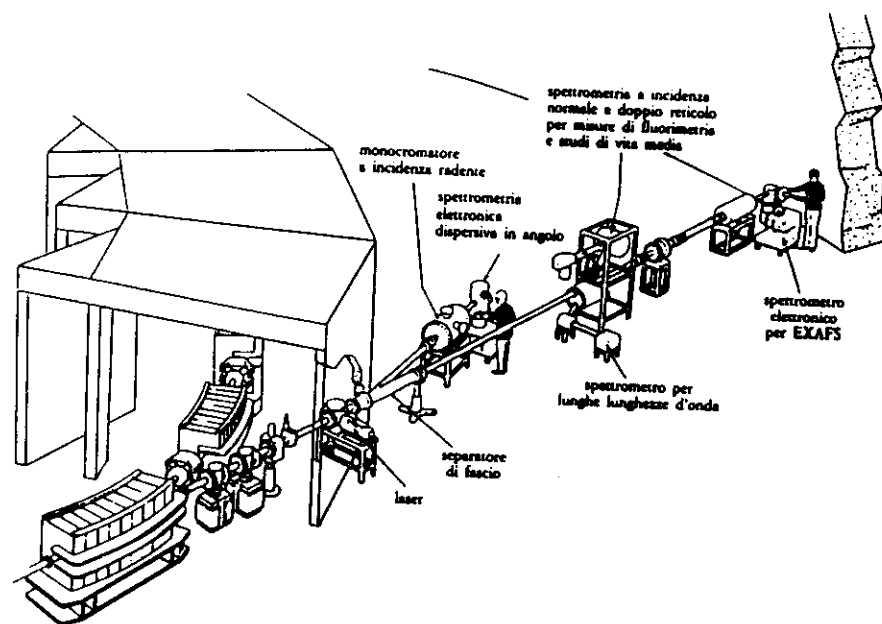
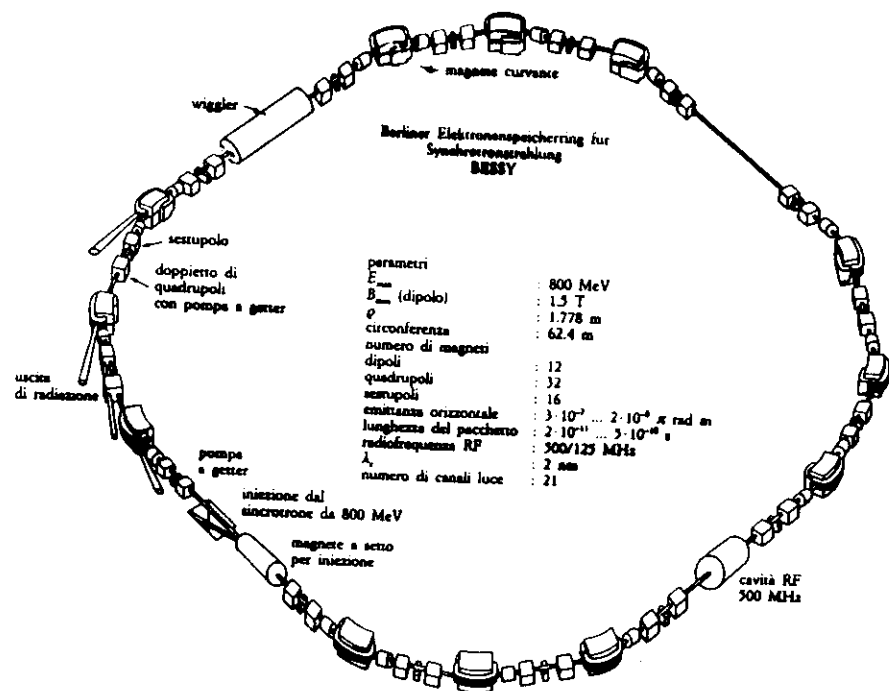
$$\epsilon_c [\text{keV}] = 0.665 \cdot E^2 [\text{GeV}] \cdot B [\text{T}]$$

$\uparrow$
can be chosen independent
of storage ring energy

FLUX is increased due to superposition

injection $\bar{B} = 2 \text{ T}$

$$\left. \begin{array}{l} E = 2 \text{ GeV} \\ \bar{B} = 1.2 \text{ T} \end{array} \right\} \rightarrow \underline{\epsilon_c = 3.2 \text{ keV}}$$



Beam line of radiation source

BESSY - Radiation Source

EQUATIONS OF MOTION

Principle: Charged particles moving in a (constant) magnetic field are bound on a circular orbit

LORENTZ FORCE $\rightarrow$ $\boxed{\vec{K} = e[\vec{v} \times \vec{B}]}$

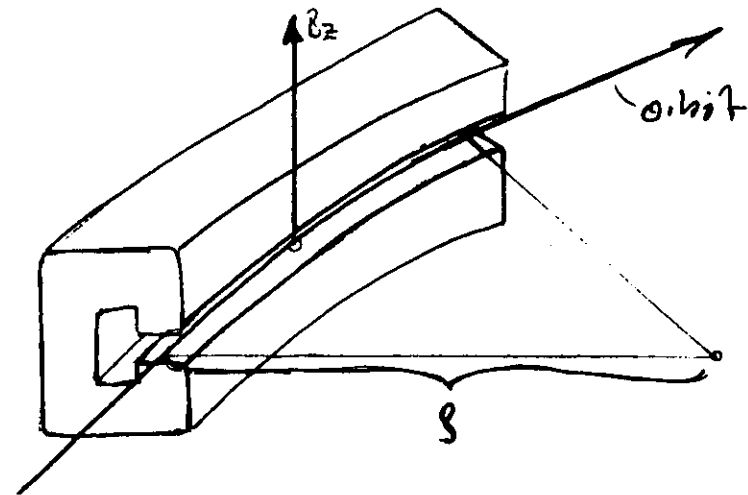
Basic magnetic elements of an accelerator $\rightarrow$

BENDING MAGNETS

Quadrupoles

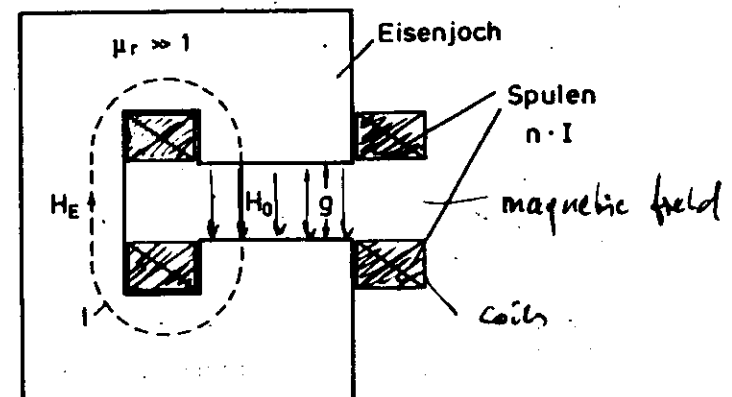
Sextupoles

BENDING MAGNET $\rightarrow$ Guiding Field



$\vec{v} \perp \vec{B}$: $K = e[\vec{v} \times \vec{B}] = \frac{mv^2}{s} \Rightarrow$

$$\boxed{\frac{e}{p_0} B_t = \frac{1}{s}}$$

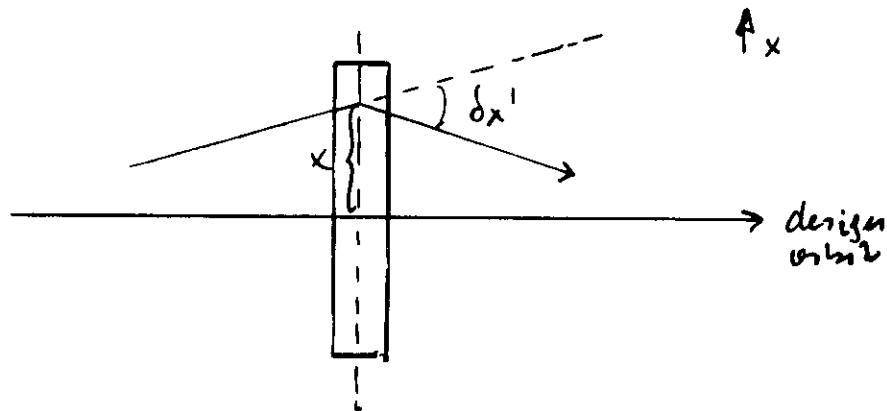


Guiding field only is not sufficient!

→ Original deviations of the particle from the design orbit would lead to a loss after several turns.

THEREFORE →

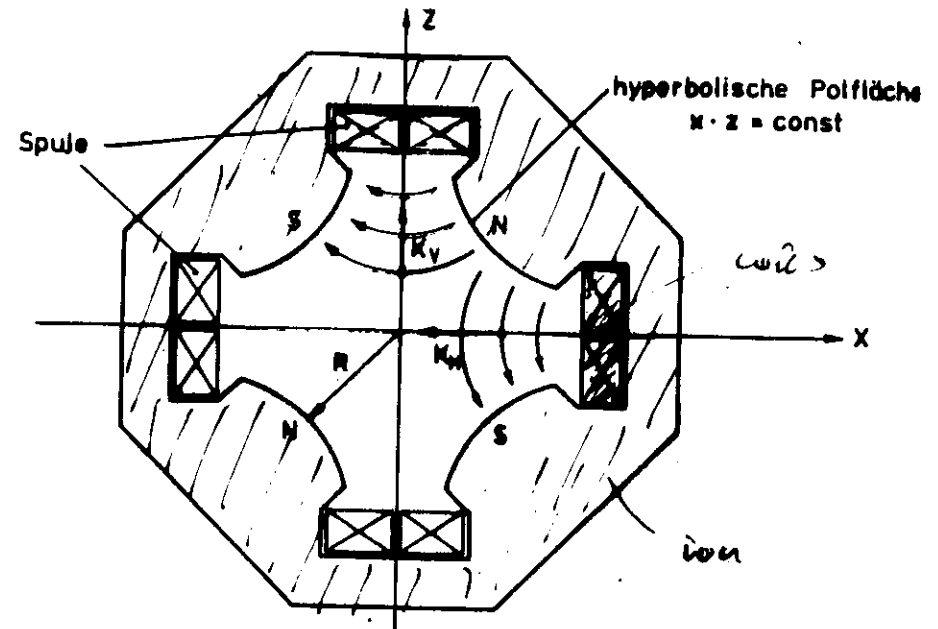
Force is needed to bend the particle back to the design orbit, with strength proportional to the deviation from the design orbit:



FOCUSING:

$$\delta x' = -g \cdot x$$

QUADRUPOLES → Focusing



Potential:
$$V = -g \cdot x \cdot z$$

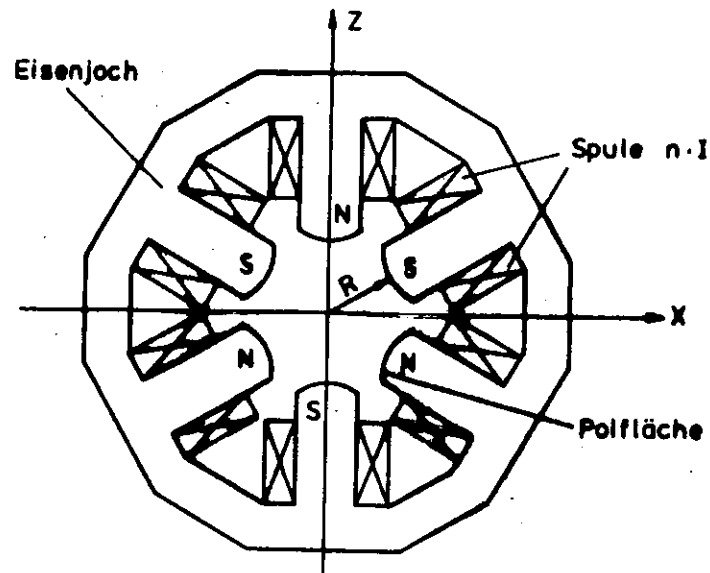
$$\frac{\partial V}{\partial z} = -gx = -\frac{gB_z}{5x} \cdot x$$

DEFLECTION:

$$\delta x' = -\frac{e}{p_0} \frac{gB_z}{5x} L_G \cdot x$$

SEXTUPOLES → for chromatic corrections

to avoid TUNE HIBERAN
HEAD TAIL INST.



If in addition field errors are taken into account, the general expression for the field can be expanded in a Taylor serie (for small deviations from the design orbit) →

ONE PLANE:

$$\frac{1}{\rho} = \frac{e}{\rho} B_z(x) = \frac{e}{\rho} B_{z0} + \left(\frac{e}{\rho} \frac{\partial B_z}{\partial x} \right) x + \left(\frac{1}{2} \frac{e}{\rho} \frac{\partial^2 B_z}{\partial x^2} \right) x^2 + \dots$$

Regular elements of
circular accelerators

$$\Delta x'' = m \cdot x^2 + \left(\frac{1}{2} \frac{e}{\rho} \frac{\partial^2 B_z}{\partial x^2} L_s \right) \cdot x^2$$

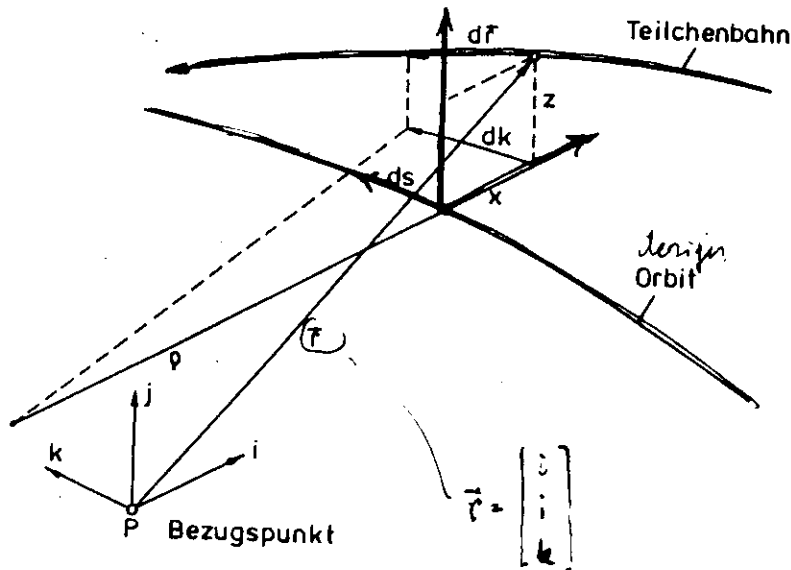
$\frac{\Delta p}{p} \rightarrow$ orbit deviation $x_0 = \frac{4p^2 D}{p}$ $D \dots$ dispersion
 $y \rightarrow \frac{1}{1 + \frac{\Delta p}{p}}$

$$\Delta x' = m (x - x_0)^2 = m x^2 - (2m x_0) x + m x_0^2$$

↓
quadrupole

Equation of Motion:

$$\dot{\vec{p}} = e [\dot{\vec{r}} \times \vec{B}]$$



→ transformation to reference system moving with the particle

⇒

After changing the independent variable from

$$t \rightarrow s$$

we find after a straightforward evaluation of the equations of motion in the new reference frame →

$$\vec{r}'' = \frac{e}{\rho} \left(1 + \frac{x}{\rho}\right) \begin{bmatrix} -B_z \\ B_x \\ x' B_z - z' B_x \end{bmatrix}$$

- for transverse magnetic fields only!

For a linear machine, i.e.

$$\begin{bmatrix} \frac{e}{\rho} B_z = \frac{1}{\rho} + (b_x) x \\ \frac{e}{\rho} B_x = -(b_z) x \end{bmatrix}$$

focusing

bending magnet deflection

→ Equations of motion:

$$\begin{aligned} X'' + (k + \frac{1}{\beta^2})X &= 0 \\ Z'' - k.Z &= 0 \end{aligned}$$

General:

$$\frac{d^2 x}{ds^2} + K(s).x = 0$$

HILL'S differential equation

Solution of any second order differential equation →

$$x(s) = C(s, s_0) x(s_0) + S(s, s_0) x'(s_0)$$

In matrix form, including the derivative →

$$\begin{bmatrix} x \\ x' \end{bmatrix}_s = \begin{bmatrix} C & S \\ C' & S' \end{bmatrix} \begin{bmatrix} x \\ x' \end{bmatrix}_{s_0}$$

To solve the equation, we follow the historical way:

Substitute in the differential equation:

$$\left(u = \frac{x}{\beta} \right), \quad \left(\phi' = \frac{1}{\beta} \right) \quad \text{Floquet transformation}$$

$$\frac{d^2 x}{ds^2} + K(s)x = 0 \quad \rightarrow \quad \frac{d^2 u}{d\phi^2} + u = 0$$



Harmonic oscillator with angular frequency 1

β' - betafunction is defined by

$$\frac{d^2}{ds^2}(\beta^{1/2}) + K(s)(\beta^{1/2}) - \frac{1}{\beta^{3/2}} = 0$$

Solution of the Harmonic oscillator:

$$u(\phi) = A \cos \phi + B \sin \phi$$

Develop the constants by defining the initial conditions $\rightarrow \phi=0 \rightarrow u_0, u'_0$

$$u = \frac{x}{\beta} \quad \rightarrow \quad \underline{\underline{A = u_0}}$$

$$\left(\frac{x}{\beta}\right)' = u' = \frac{1}{\beta} (x' + \alpha \frac{x}{\beta}) \quad \rightarrow \quad \underline{\underline{B = u'_0 \beta}} \quad \alpha = -\frac{1}{2} \beta'$$

$$\begin{bmatrix} u \\ u' \end{bmatrix} = \begin{bmatrix} \cos \phi & \beta \sin \phi \\ -\frac{1}{\beta} \sin \phi & \cos \phi \end{bmatrix} \begin{bmatrix} u \\ u' \end{bmatrix}_0$$

starting vector

$\rightarrow$ back transformation $(u, u') \rightarrow (x, x')$

$$\begin{bmatrix} x \\ x' \end{bmatrix} = \begin{bmatrix} \sqrt{\beta} (\cos \phi + \alpha \sin \phi) & \sqrt{\beta} \sin \phi \\ -\frac{1}{\sqrt{\beta}} [(1-\alpha^2) \cos \phi + (1+\alpha^2) \sin \phi] & \sqrt{\beta} (\cos \phi - \alpha \sin \phi) \end{bmatrix} \begin{bmatrix} x_0 \\ x'_0 \end{bmatrix}$$

α, β ... Courant Snyder parameters

By using the trigonometric identity

$$\cos^2 \phi + \sin^2 \phi = 1$$

We can derive the

Constant Snyder invariant

$$\underline{\underline{I = \frac{x^2 + (x' + \alpha x)^2}{\beta} = \frac{x_0^2 + (x'_0 + \alpha x'_0)^2}{\beta_0}}}$$

- Equation of ellipse with area

$$E = \pi \cdot I$$

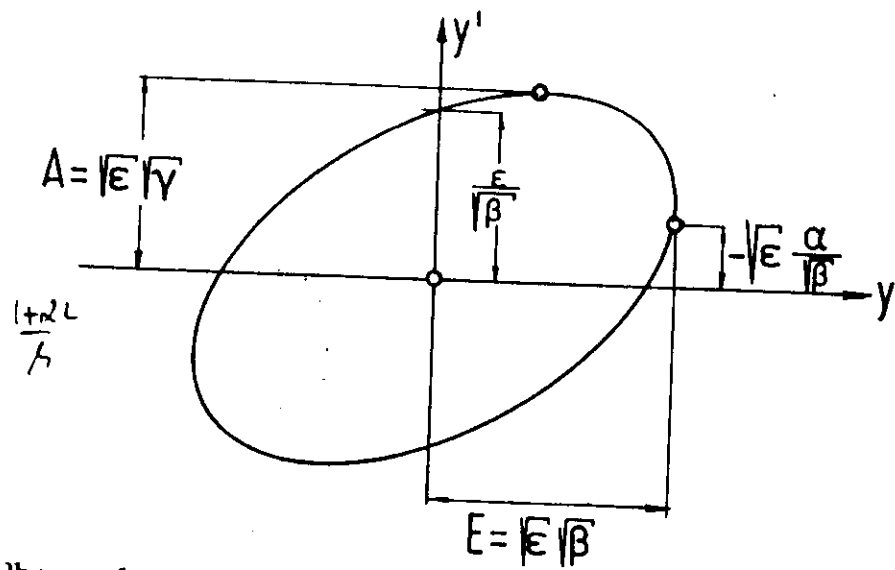
$\uparrow$

Emitance

If we substitute $x = A \cos(\phi + \phi_0)$
we find

$$A = \sqrt{\epsilon \beta}$$

amplitude of
betatron oscillations



phase plane ellipse

use the area of the phase-plane ellipse given the maximum amplitude of a betatron oscillation E becomes smaller (larger) if the beta function becomes smaller (larger).

β = measure of beam cross section

Periodic structures.

$$\left. \begin{aligned} \beta &= \beta_0 \\ L &= L_0 \\ Q &= 2\pi Q - \mu \end{aligned} \right\}$$

$$\begin{array}{c} \beta_0, L_0, \phi_0 \\ | \\ S_0 \end{array}$$

$$\begin{array}{c} \beta_1, L_1 \\ | \\ S_0 + L \end{array}$$

$$Q - Q_0 = 2\pi Q - \mu$$

Q... turns

$$\begin{bmatrix} x \\ x' \end{bmatrix}_1 = \begin{bmatrix} \cos \mu + 2 \sin \mu & \beta \sin \mu \\ -\frac{1+d^2}{\beta} \sin \mu & \cos \mu - 2 \sin \mu \end{bmatrix} \begin{bmatrix} x \\ x' \end{bmatrix}_0$$

$$\vec{x}_1 = [\mathbb{I} \sin \mu + \mathbb{J} \cos \mu] \vec{x}_0$$

$$\mathbb{I} = \begin{bmatrix} 1 & 0 \\ 0 & 1 \end{bmatrix}, \quad \mathbb{J} = \begin{bmatrix} 2 & \beta \\ -\gamma & -2 \end{bmatrix}$$

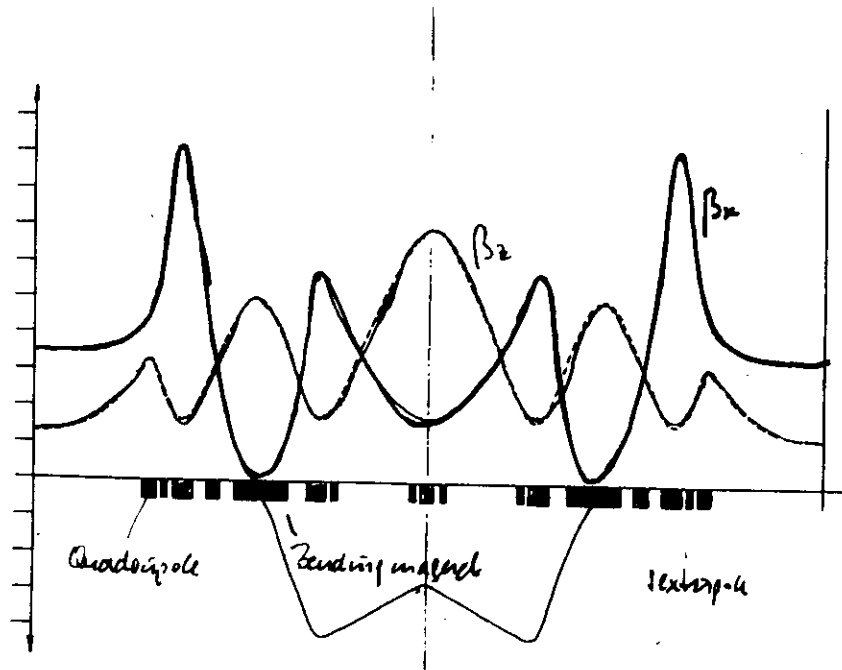
$$\gamma = \frac{1+d^2}{\beta}$$

$$\boxed{\begin{aligned} \vec{x}_n &= M^n \vec{x}_0 \\ &= [\mathbb{I} \sin n\mu + \mathbb{J} \cos n\mu] \vec{x}_0 \end{aligned}}$$

... initial vector $\vec{x}_0$ transformed over n turns in a circular accelerator!

SINCHROTRON TRIESTE

- lattice functions



The Courant-Snyder parameters are the characteristics of a magnet lattice!

How to calculate the structure functions β and α ?

Phase-plane ellipse in parameter form:

$$S=S_0: \vec{X}(s) = \sqrt{\epsilon} [\vec{X}_1(S_0) \cos s + \vec{X}_2(S_0) \sin s]$$

$$0 \leq s \leq 2\pi$$

Ellipse defined by linear independent vectors

$$\vec{X}_1 = \begin{bmatrix} x_1 \\ x_1' \end{bmatrix} \text{ and } \vec{X}_2 = \begin{bmatrix} x_2 \\ x_2' \end{bmatrix}$$

To get the phase plane area ϵ , they must be normalized to give

$$\frac{1}{\sqrt{\epsilon}} \begin{pmatrix} 0 & -1 \\ 1 & 0 \end{pmatrix} \vec{X}_1 = 1$$

i.e. Wronski-determinant = 1

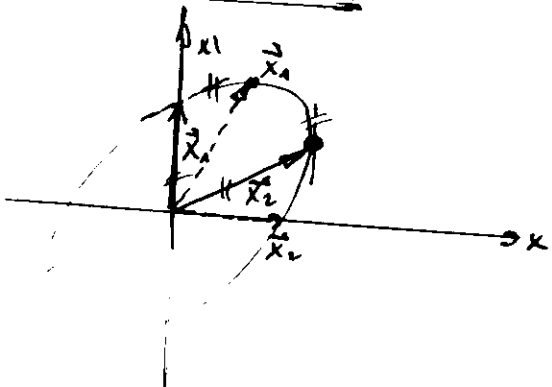
a particle is moving through
magnet structure, the form
an ellipse is changed

$$I = \overline{I} \left[\vec{X}_1(s) \cos d + \vec{X}_2(s) \sin d \right]$$

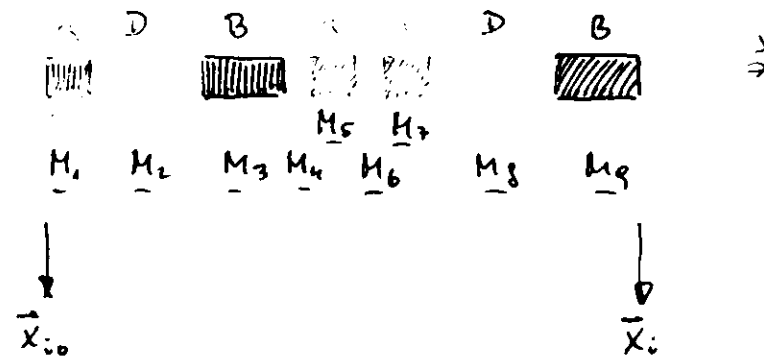
$$\vec{X}_i(s) = M(s|s_0) \vec{X}_i(s_0)$$

evaluated numerically
by transforming element
by element

$$\frac{x_1^2 + x_2^2}{- (x_1 x_1' + x_2 x_2')}$$



To calculate the transfer functions,
the conjugated vectors are transformed
through the structure $\rightarrow$



$$\vec{X}_i = M_9 M_8 M_7 M_6 M_5 M_4 M_3 M_2 M_1 \vec{X}_{i0}$$

To get the transformation matrices the
Differential equation is solved piecewise

$$x'' + K(s)x = 0$$



- $k(s) = k$... Quadrupoles
- $\frac{1}{\rho^2}$... Bending magnets
- c ... Drift spaces

Transformation matrix $\underline{M} \rightarrow$

$$\begin{bmatrix} 1 & s \\ 0 & 1 \end{bmatrix}$$

DRIFT

$$\begin{bmatrix} \cos \frac{s}{\rho} & \rho \sin \frac{s}{\rho} \\ -\frac{1}{\rho} \sin \frac{s}{\rho} & \cos \frac{s}{\rho} \end{bmatrix}$$

BENDING MAGNET

$$\begin{bmatrix} \cos s|\vec{k}| & \frac{1}{|\vec{k}|} \sin s|\vec{k}| \\ -|\vec{k}| \sin s|\vec{k}| & \cos s|\vec{k}| \end{bmatrix}$$

QUADRUPOLE
(FOC)

How to get the initial values
of the conjugated vectors?

Linear machines $\rightarrow \vec{x}_1, \vec{x}_2$ is given by
the initial beam condition

Circular machine $\rightarrow$ Phase plane ellipse
must transform into the
after 1 turn

Rewrite parameter form of phase plane ellipse

$$\begin{aligned} \vec{x}(s_0) &= \sqrt{\epsilon} \left\{ \vec{x}_1(s_0) \cos d + \vec{x}_2(s_0) \sin d \right\} \\ &= \frac{\sqrt{\epsilon}}{2} \left\{ (x_1(s_0) - i\bar{x}_2(s_0)) e^{id} + (x_1(s_0) + i\bar{x}_2(s_0)) e^{-id} \right\} \end{aligned}$$

We have shown before that the transformation
of a vector over one closed turn changes
only the phase, i.e. $\rightarrow$

$$e^{id} = \cos d + i \sin d$$

$$\underline{M}(s_0+L, s_0) [\vec{x}_1(s_0) - i \vec{x}_2(s_0)] = e^{-i2\pi Q} [x_1(s_0) - i x_2(s_0)]$$

Eigenwert-equation of revolution matrix $\underline{M}$

$$\underline{M} \vec{q} = \lambda \vec{q}$$

The motion is stable, $\Rightarrow |\lambda| = |e^{-i2\pi Q}| = 1$,
i.e. $Q = \text{real}!$

ALTERNATIVE METHOD:

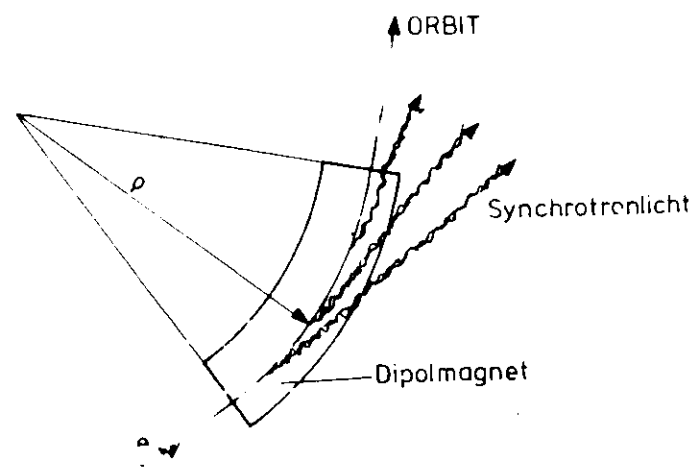
To find the initial conjugate vectors, solve the Eigenwert-equation of revolution matrix.

Transition then occurs through the structure to calculate the structure function (f_s)

$\rightarrow$ defines required magnet aperture!

LONGITUDINAL MOTION:

Emission of Synchrotron Light $\rightarrow$



Radiated power:

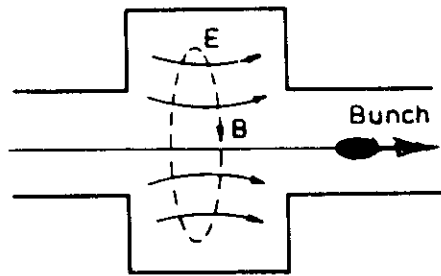
$$P_r = \frac{2e^2 c^2 \gamma^4}{3(m_0 c^2)^3} \cdot E^2 B^2$$

With

$$\frac{1}{\rho} = \frac{e c B}{E} \Rightarrow$$

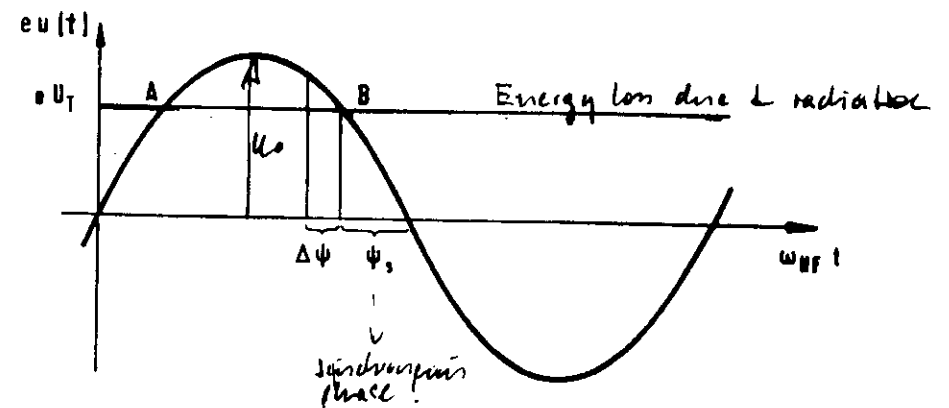
$$P_r = 88.5 \frac{E^4 [\text{GeV}]}{\rho [\text{m}]}$$

Energy lost by synchrotron radiation must be compensated in 'accelerating sections' (cavities)



→ cavity with oscillating field
(350 MHz, 500 MHz, 1-3 GHz)

Accelerating voltage in the cavities →



(eU_T) ... necessary to compensate the radiation losses

Energy gain by accelerating voltage:

$$E = e U_0 \sin(\psi_s + \Delta\psi) \quad \Delta\psi \dots \text{phase deviation}$$

$$E_0 = e U_0 \sin \psi_s \quad \text{exact phase!}$$

$$\frac{E - E_0}{T_0} \approx \frac{d\Delta E}{dt} = e U_0 f_0 [\sin(\psi_s + \Delta\psi) - \sin \psi_s]$$

Period of synchrotron oscillation $\rightarrow$ revolution period!

Phase deviation for particles with wrong revolution time, i.e.

$$T = T_0 + \Delta T$$

⇒

$$\Delta\psi = -\omega_{RF} \cdot \Delta T$$

$$\frac{d\Delta\psi}{dt} = -\omega_{RF} \frac{\Delta T}{T} = -\omega_{RF} \frac{\Delta L}{L}$$

$$\downarrow$$

$$\frac{\Delta L}{L} \approx \alpha_c \frac{\Delta E}{E}$$

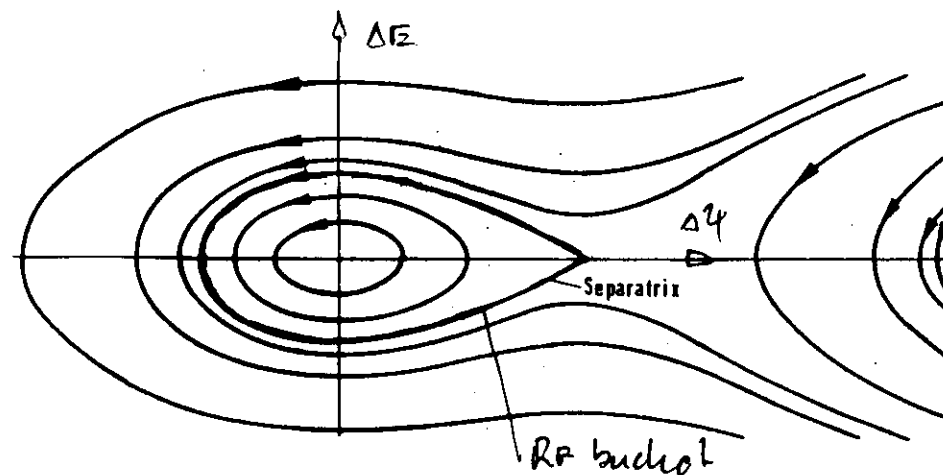
α_c ... momentum compaction

$$\boxed{\frac{d\Delta\psi}{dt} = -\omega_{RF} \alpha_c \frac{\Delta E}{E}}$$

ΔE substituted from previous equation gives →

$$\boxed{\frac{d^2\Delta\psi}{dt^2} + \omega_0 \omega_{RF} \frac{\alpha_c e U_0}{2\pi E_0} [\sin(\psi_s + \Delta\psi) - \sin\psi_s] = 0}$$

Phase-plane of longitudinal motion →



For small amplitudes $\Delta\psi \rightarrow$
Harmonic oscillation

$$\sin(\psi_s + \Delta\psi) - \sin\psi_s \approx (\cos\psi_s) \Delta\psi$$

$$\boxed{\frac{d^2\Delta\psi}{dt^2} + \Omega^2 \Delta\psi = 0}$$

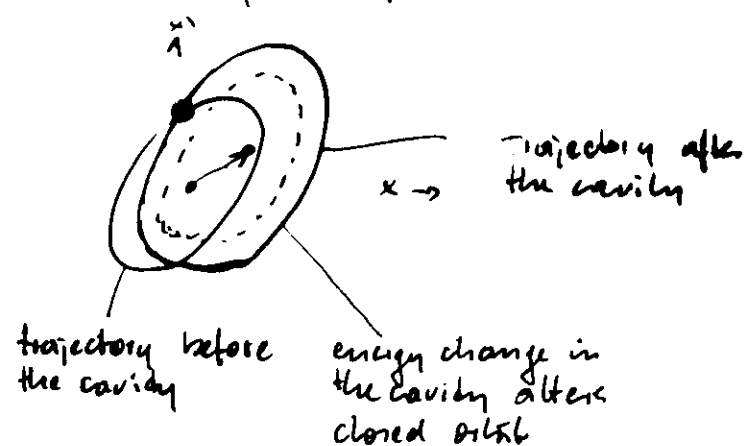
$$\Omega^2 = \omega_0 \omega_{RF} \frac{\alpha_c e U_0 \cos\psi_s}{2\pi E_0}$$

Coupling between transverse (betatron) motion and longitudinal (synchrotron) motion:

Sources: uncompensated chromaticity fields in accelerating structures
beam-beam interactions (crossing angle)
dispersion in the cavity
...

EXAMPLE: Dispersion in the cavity
i.e. orbit displacement in the cavity varies with the momentum of the particle.

Transverse phase space:



$$X = \mathcal{H} T$$

Must be numerically evaluated:

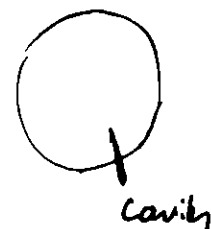
CAVITY - transformation:

$$E_{n+1} = E_n + eU [\sin(\psi_c + \psi_n) - \sin \psi_c]$$

$$\psi_{n+1} = \psi_n$$

$$x_{n+1} = x_n - D \frac{E_{n+1} - E_n}{E_0}$$

$$x'_{n+1} = x'_n - D' -$$



MAGNET STRUCTURE - transformation:

$$E_{n+2} = E_{n+1}$$

$$\psi_{n+2} = \psi_{n+1} - 2\pi f \left[h_e \frac{E_{n+1} - E_0}{E_0} + \underbrace{\{ (x_{n+1}, x'_{n+1}, D) \}}_{=0 \text{ for } D=0} \right]$$

$$x_{n+2} = x_{n+1} \cos \mu + x'_{n+1} \beta \sin \mu$$

$$x'_{n+2} = -\frac{x_{n+1}}{\beta} \sin \mu + x'_{n+1} \cos \mu$$

OSCILLATION AMPLITUDE IS INCREASED!

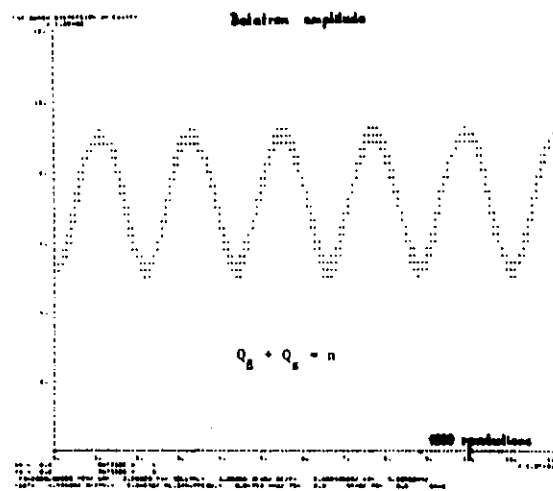


Fig 1

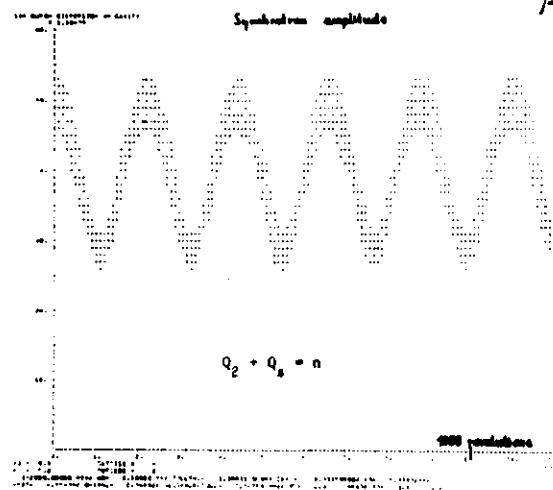


Fig 2

$$A_p^2 + q A_{syn}^2 = \text{const}$$

Exchange of energy only!

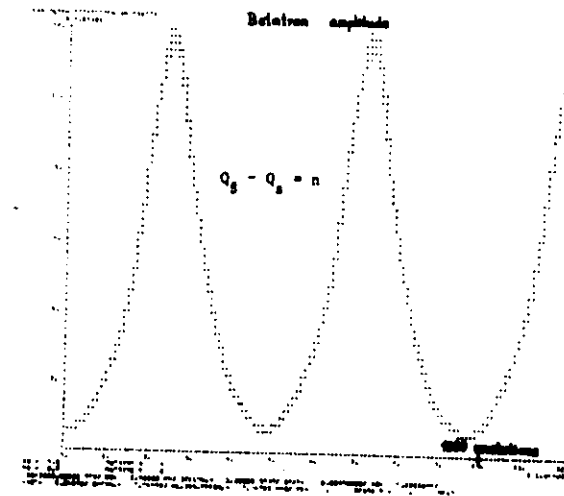


Fig 3

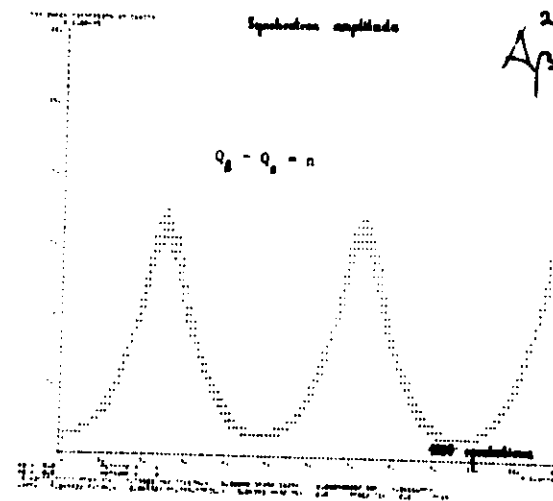


Fig 4

$$A_p^2 - q A_s^2 = \text{const}$$

both amplitudes increase!

NONLINEAR MOTION (transverse)

→ due to sextupoles
or field errors

Equations of motion:

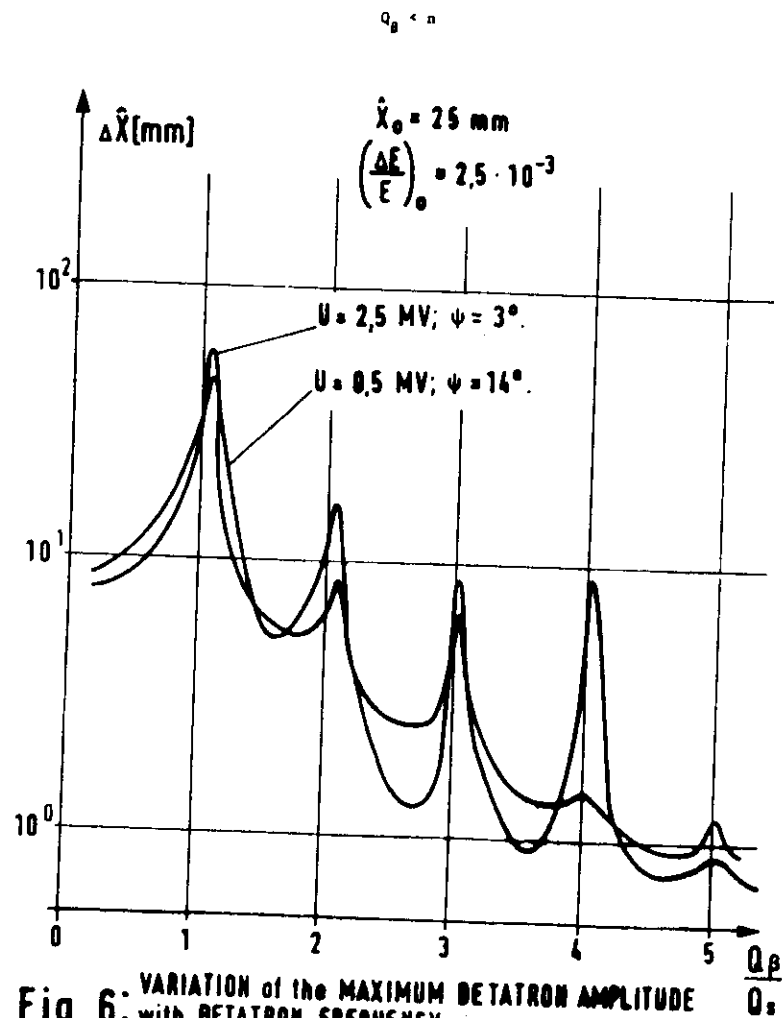
$$\frac{d^2 x}{ds^2} + K(s)x = \frac{e}{p_0} \sum_{n=0} b_n(s) x^n$$

$$b_n = \frac{1}{n!} \frac{\partial^n B}{\partial x^n}$$

b_0 ... dipole

b_1 ... quadrupole

b_2 ... sextupole



In superconducting magnets the
still relevant maximum orders
are 24-poles (usually!)

Transformation to normalized coordinates (as before in the linear case) $\rightarrow$ Floquet transform.

$$u = \frac{x}{\sqrt{\beta}}, \quad \phi = \int \frac{ds}{\beta}$$

$\Rightarrow$

$$\boxed{\frac{d^2 u}{d\phi^2} + u = \frac{e}{p} \sum_n b_n(\phi) \beta^{\frac{n+3}{2}}(\phi) u^n}$$

Periodic function $u \rightarrow$

$$\frac{e}{p} b_n(\phi) \beta^{\frac{n+3}{2}}(\phi) = \sum_k f_{nk} \cos 2\pi k \cdot \frac{\phi}{2\pi Q} \quad \mu = 2\pi Q$$

represented by Fourier series with period $\underline{2\pi Q}$

(Assumption here: even function with zero mean)

Fourier coefficient:

$$f_{nk} = \frac{1}{\pi Q} \int_0^{2\pi Q} \left[\frac{e}{p} b_n(\phi) \beta^{\frac{n+3}{2}}(\phi) \right] \cos \frac{k}{Q} \phi d\phi$$

For small distortions we can substitute the homogeneous solution for u at the right hand side of the differential equation:

$$u = u_0 \cos \phi + \underbrace{u_1 \sin \phi}_{=0}$$

$$\frac{d^2 u}{d\phi^2} + u = \sum_n u^n \sum_k f_{nk} \cos \frac{k}{Q} \phi$$

$$u^n = u_0^n (\cos \phi)^n = \frac{u_0^n}{2^{n-1}} \sum_{p=0}^{n-1} \binom{n}{p} \cos (n-2p)\phi$$

$$\frac{d^2 u}{d\phi^2} + u = \sum_n \frac{U_0^n}{2^{n-1}} \sum_{p=0}^{\frac{n-2}{2}} \binom{n}{p} \cos(n-2p)\phi \sum_k f_{nk} \cos \frac{k}{Q} \phi$$

take one term only $\rightarrow$

$$\frac{d^2 u}{d\phi^2} + u = \frac{U_0^n}{2^{n-1}} f_{nk} \underbrace{\cos n\phi \cos \frac{k}{Q} \phi}_{\downarrow} \quad (p=0)$$

$$\frac{1}{2} [\cos(n - \frac{k}{Q})\phi + \cos(n + \frac{k}{Q})\phi]$$

only $\rightarrow$

$$\frac{d^2 u}{d\phi^2} + u = A \cos(\frac{k}{Q} - n)\phi$$

$$A = \frac{U_0^n}{2^n} f_{nk}$$

Solution:

$$u = u_n + u_p$$

$$u_n = u_0 \cos \phi$$

$$u_p = \frac{A}{1 - (\frac{k}{Q} - n)^2} \cos(\frac{k}{Q} - n)\phi + \dots$$

Resonance term!

i.e. betatron amplitude increases,
if
 $(\frac{k}{Q} - n) = 1$ or

$$(n+1)Q = k$$

Resonance condition for 1-dimensional resonance

e.g. $n=2 \rightarrow$ Sextipole $\rightarrow (\frac{1}{2} \frac{\partial^2 B}{\partial x^2})$

$$3Q = k$$

In the general 2-dimensional case we have the resonances $\rightarrow$

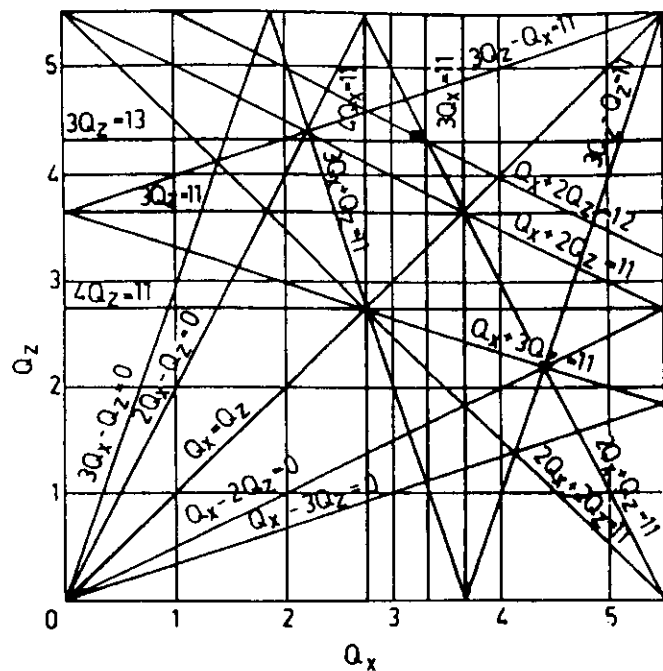
$$\begin{array}{l} 3Q_x \\ 2Q_x \pm Q_z \\ Q_x \pm 2Q_z \\ 3Q_z \end{array}$$

= integer!

$$|u_x Q_x + u_z Q_z = p|$$

Resonances in the presence of sextipole fields!

$$N = |u_x| + |u_z| \sim \text{ord. of resonance}$$



Resonance lines in 2-dimensional
tune diagram
(up to 4th order)

$$n_x Q_x + n_z Q_z = p \quad N = |n_x| + |n_z| \dots \text{order of resonance!}$$

Maximum stable betatron amplitude
can be calculated analytical for
one isolated resonance.

For a realistic pattern of magnet
field errors one has to simulate the
motion with a computer $\rightarrow$

TRACKING

Tracking codes:

PATRICIA
MAD
RACETRACK
DIAMAT
TRANSPORT
:
:

KICK CODES 1

Principle structure of these codes:

INPUT:

Magnet structure
Magnet strengths
Field errors

Tracking parameters:

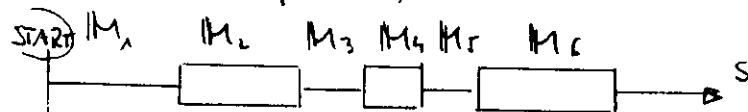
of turns

of particles

initial amplitude

Find Revolution Matrix:

(Linear optics)



$$M = \prod_{n=1}^N M_n$$

M_n ... single element transformation
(6x6)

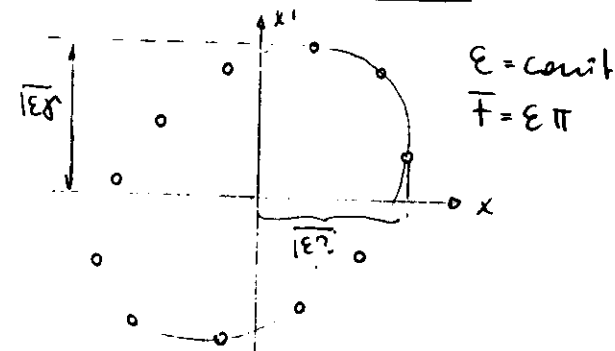
Calculate optical parameters at the starting point,

by solving the Eigenval. equation of the revolution matrix

Initial coordinates:

$$\beta = \frac{1 + \alpha^2}{\beta}$$

$$\alpha = -\frac{1}{2} \frac{d\beta}{ds}$$



Tracking of particle ensemble through the structure:

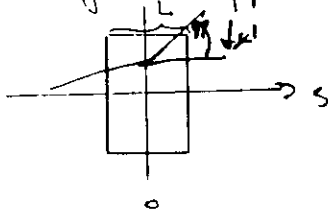
① Linear element: $\bar{x}_f = M \bar{x}_i$

② Nonlinear element:

$$\frac{d^2x}{ds^2} = \frac{e}{p_0} \sum_{n=0} b_n(s) x^n$$

thin magnet approximation

→

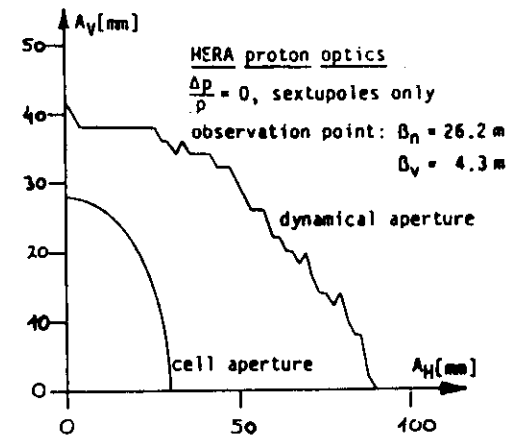


Kick:

$$\frac{dx}{ds} = \Delta x' = \sum_n (b_n L_n) x^n$$

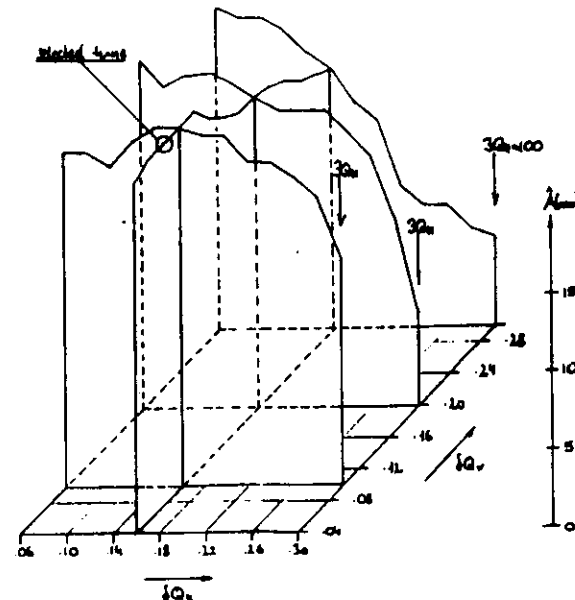


Find maximum stable betatron amplitude by varying the initial value

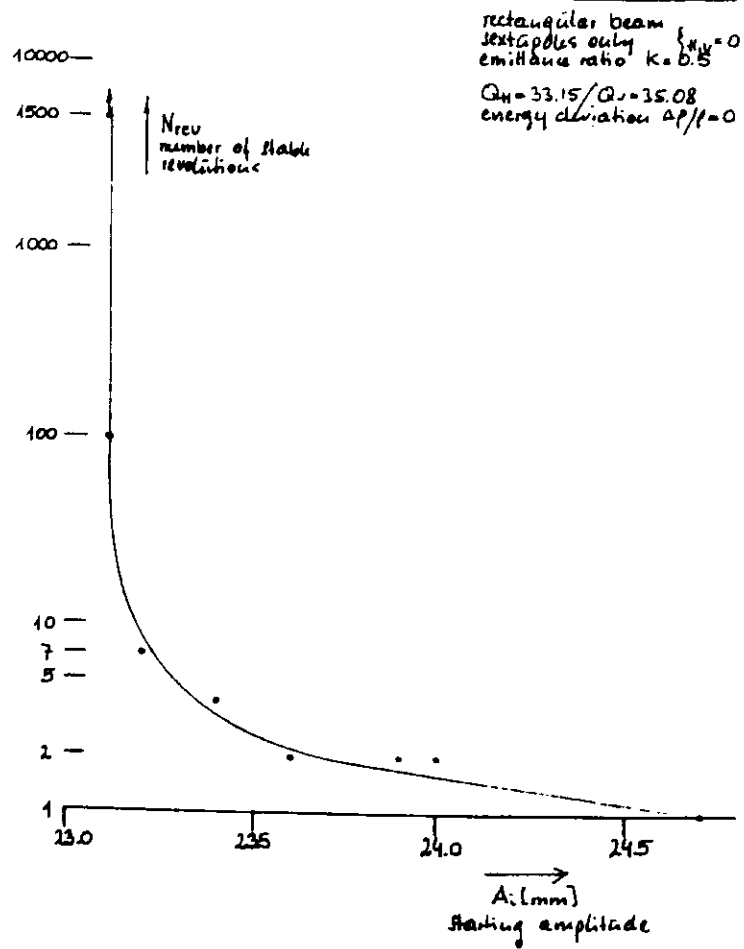


HERA90 - tune variation
 Maximum stable initial amplitude vs. time

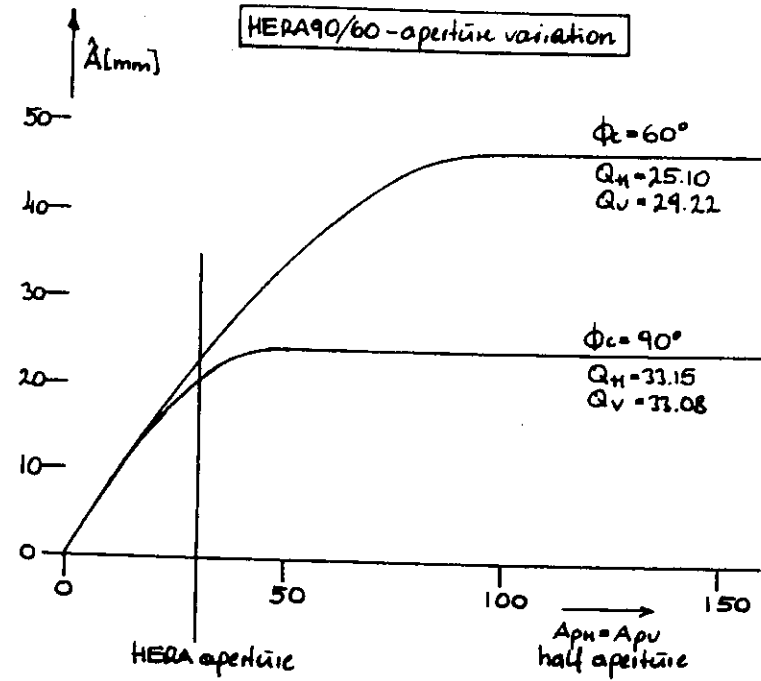
rectangular beam
 sextupoles only $\epsilon_{x,y} = 0$
 emittance ratio $K = 0.5$
 energy deviation $\Delta p/p = 0$
 $Q_x = 33 + \delta Q_x / Q_y = 35 + \delta Q_y$
 $N_{tr} = 100$



HERA90 - number of stable revolutions vs. initial amplitude



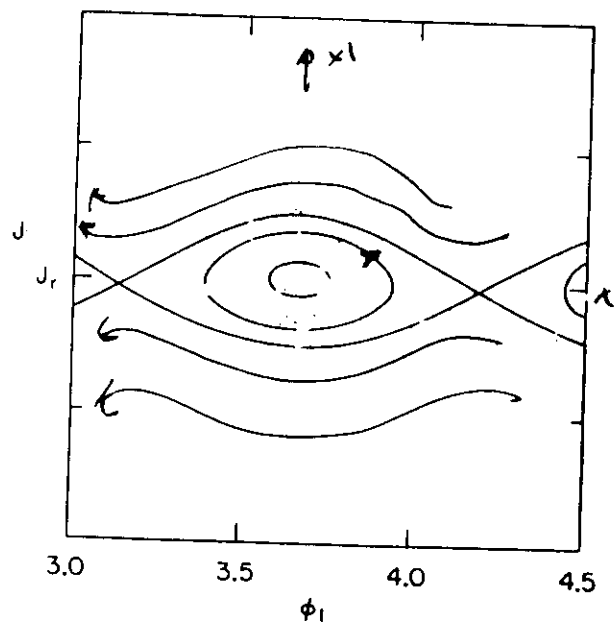
HERA90/60 - aperture variation



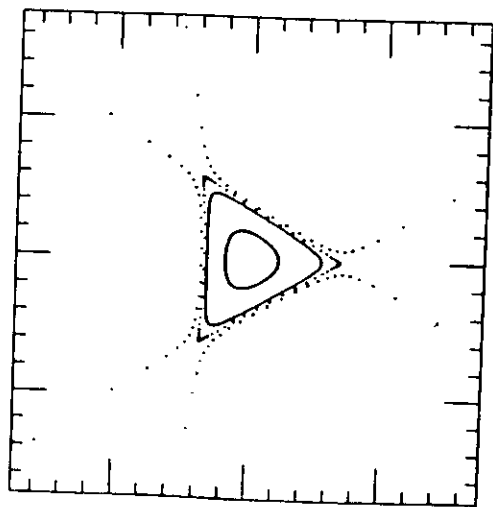
rectangular beam
sextupoles only
emittance ratio $K=1.0$
no energy deviation
 $N_{rev}=30$!

Phase space motion:

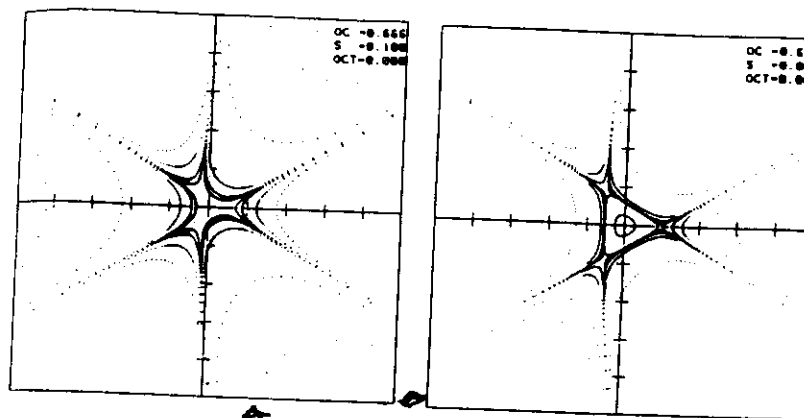
Resonance



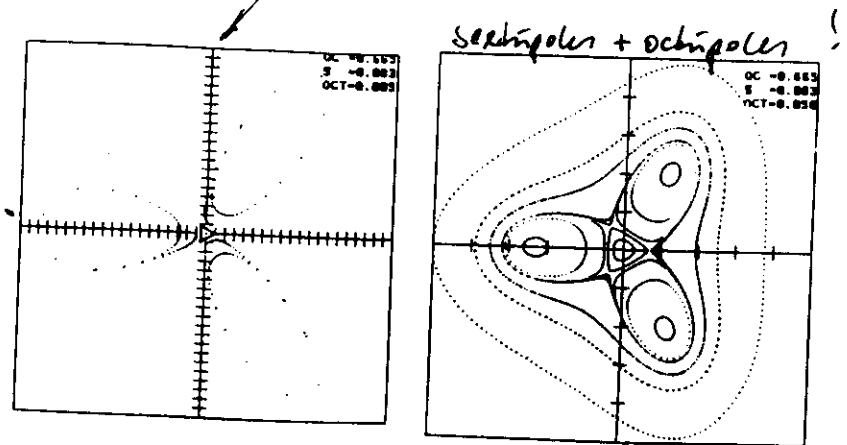
Motion near a third integer resonance in a circular accelerator:



Unstable motion due to sextupole nonlinearities, stabilized by octupoles $\rightarrow$

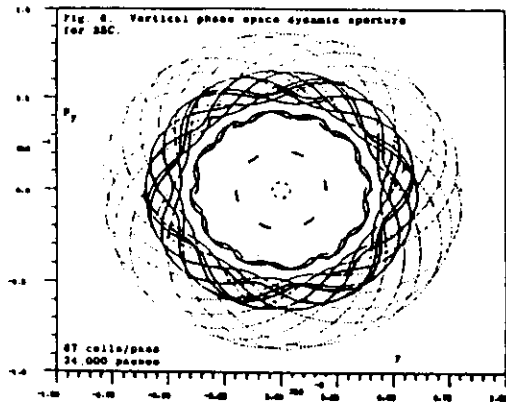


sextupole resonances for various damping

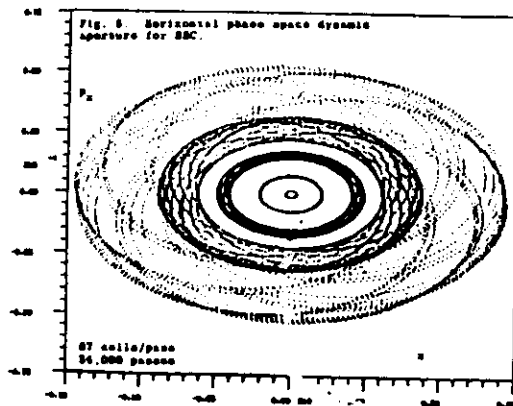


(Landau damping due to octupoles !)
Turn variation with amplitude $\rightarrow$
particle falls out of the resonance !

Perm: MARYLI

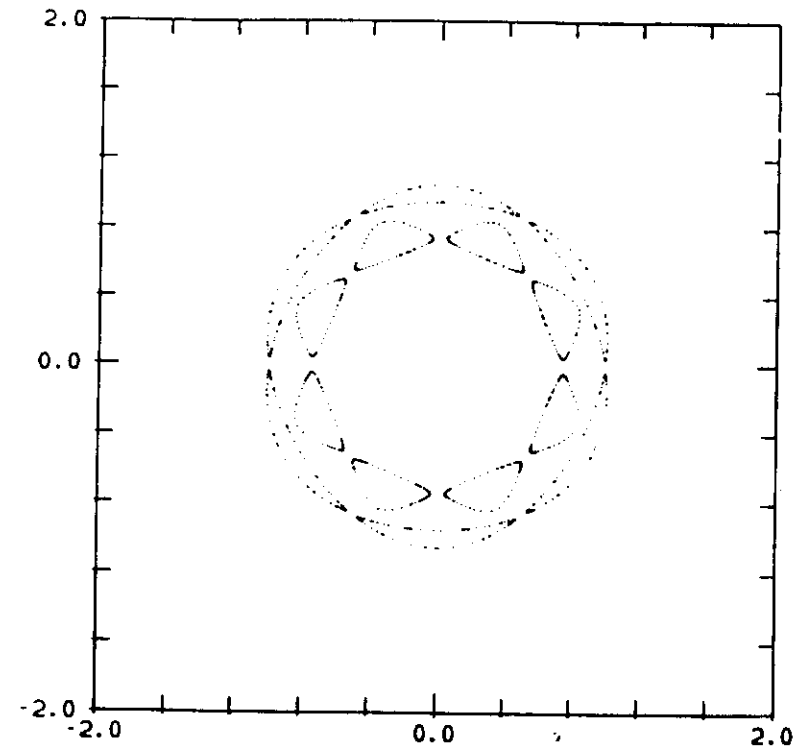


Vertical



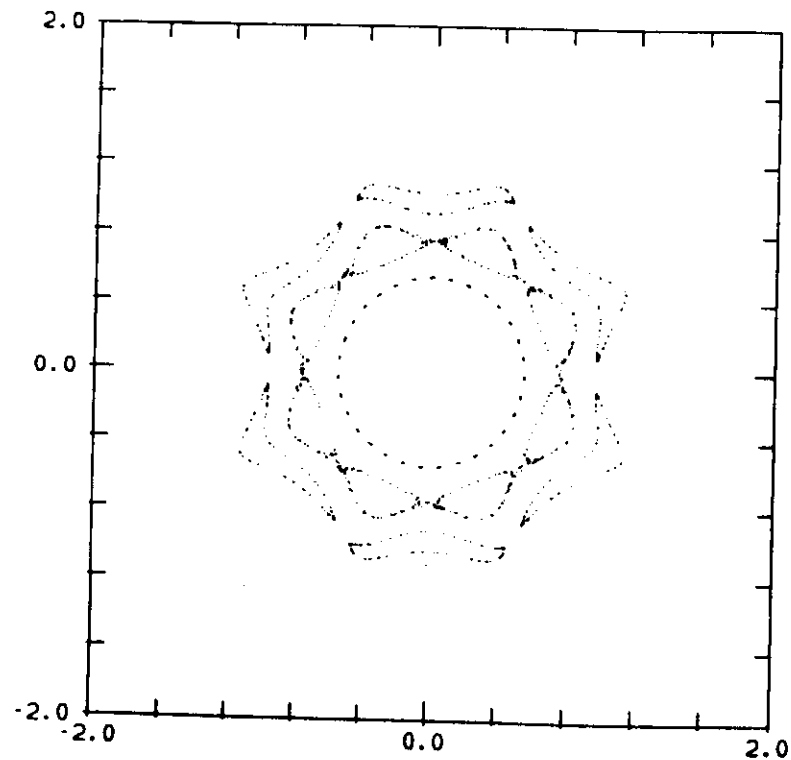
Horizontal

Isolated resonances plotted together →

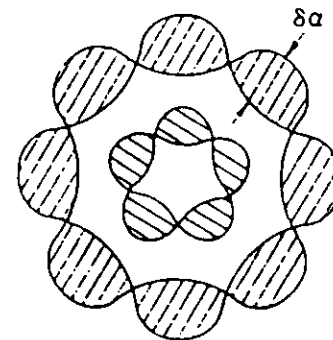


Situation becomes complicated if the particle motion is influenced by more than one resonance!

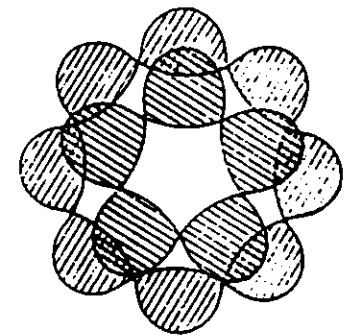
Actual phase space for these
resonances $\rightarrow$



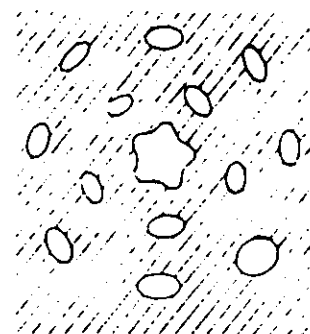
If the resonances start to
overlap, the particle can easily
become chaotic $\rightarrow$



Single Resonances



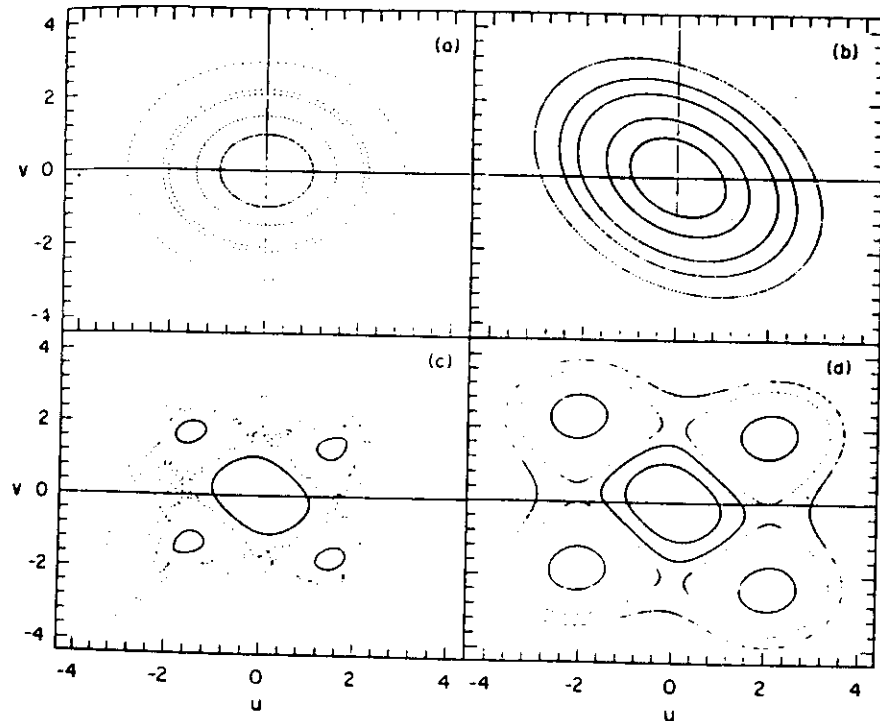
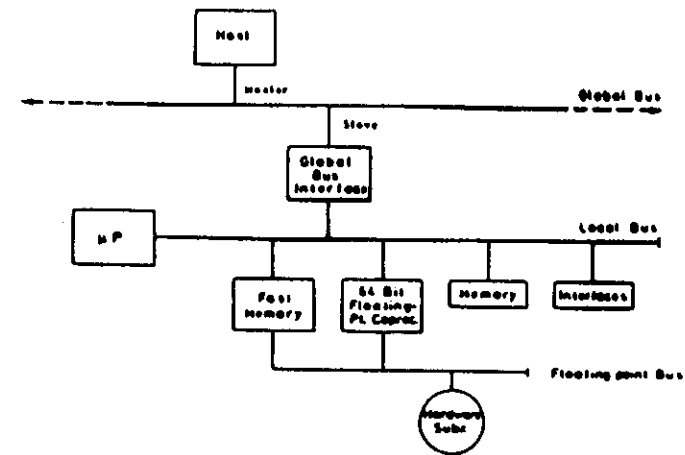
Overlapping Resonances



Actual phase space

To perform long time tracking, a dedicated computer has been developed →
parallel microprocessors (one for each particle)

Conceptual design →



Regular motion → concentric curves
 or islands

Chaotic motion → 'randomly' distributed
 orbits

Host computer - programs compiled and linked
 then can directly run on the μP
 μP - connected with global bus interface to host
 local bus to other interface

μP : MC 68000
 double precision floating point unit
 controller
 memory with 128 kBytes

Long-term stability

Even though particles may be chaotic, they may nevertheless survive for the limited number of revolutions normally accessible

To distinguish regular from chaotic motion use concept of characteristic Lyapunov exponent $\rightarrow$

$$\lambda = \lim_{\substack{d_0 \rightarrow 0 \\ N \rightarrow \infty}} \left(\ln \left| \frac{d_N}{d_0} \right| \right)$$

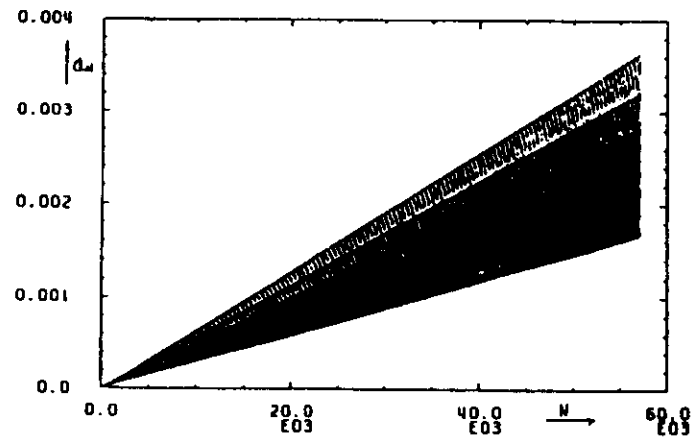
d ... separation in phase space
 N ... revolution number

For chaotic motion the distance in phase space of two neighbouring trajectories increases exponentially with the Lyapunov exponent.

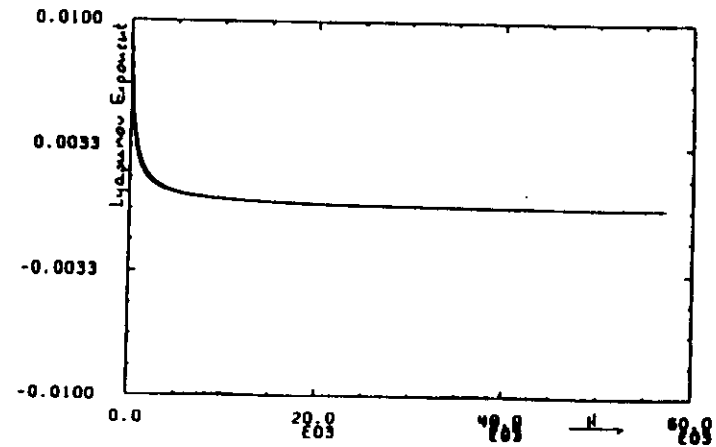
$\rightarrow$ BREAK OF STRONG CAUSALITY!

Regular motion

$\rightarrow$ distance in phase space increases linearly
 $\rightarrow$ Lyapunov exponent = 0

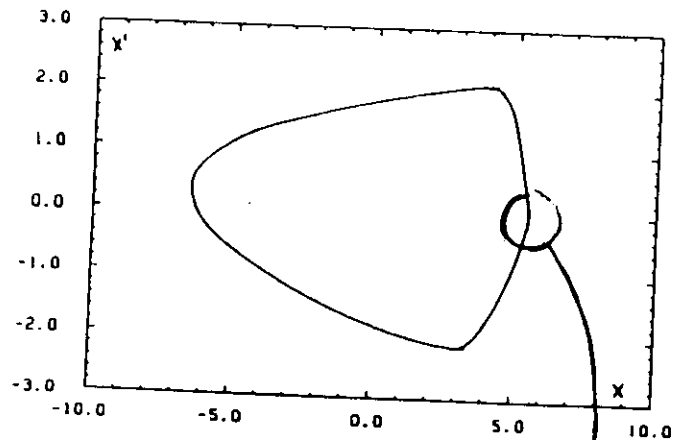


Trajectory separation for regular motion.

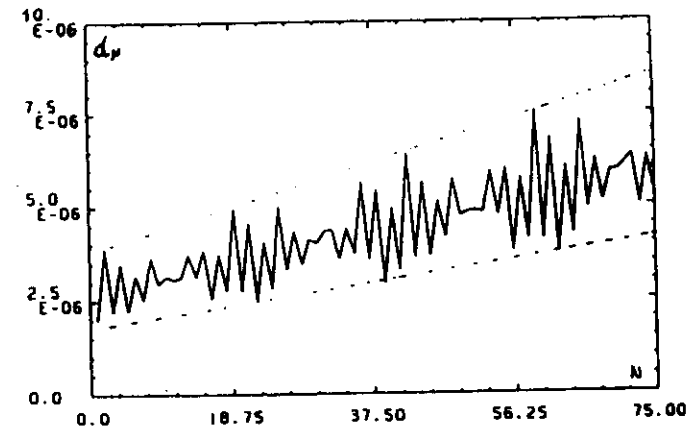


Lyapunov exponent for regular motion.

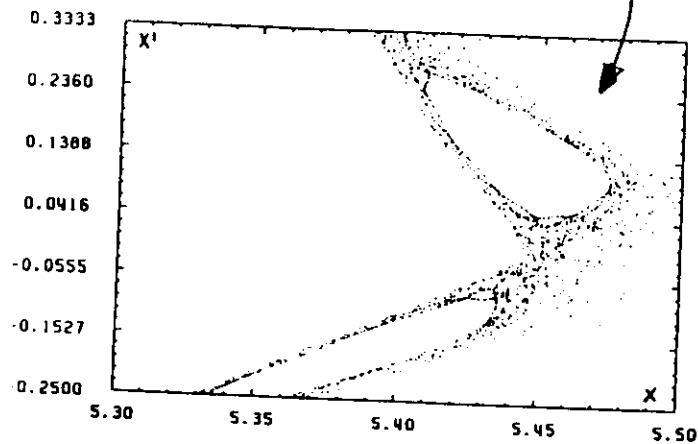
Regular motion



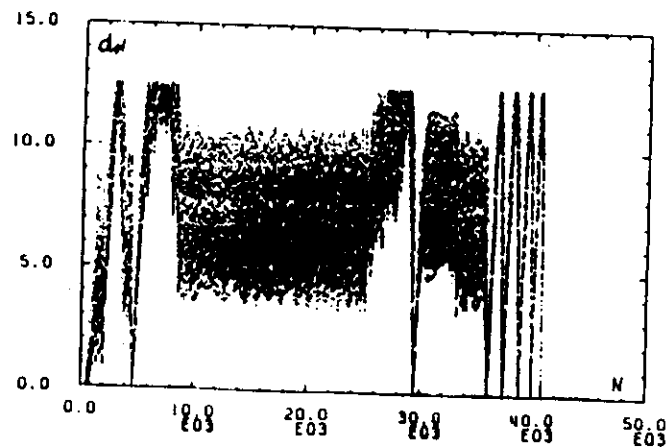
Trajectory close to the dynamic limit



Distance of trajectories in phase space for regular motion

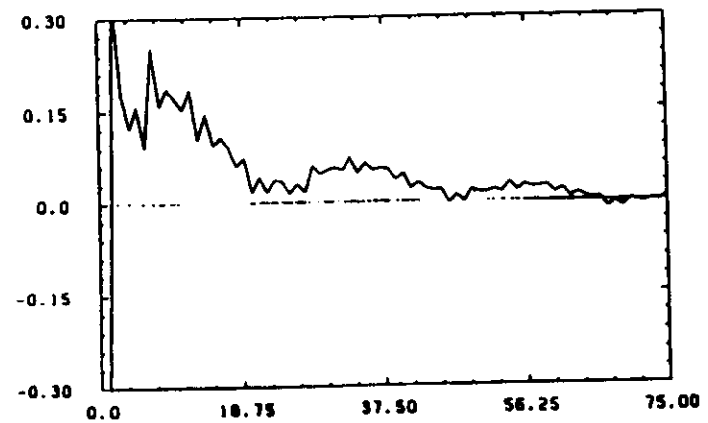


Chaos



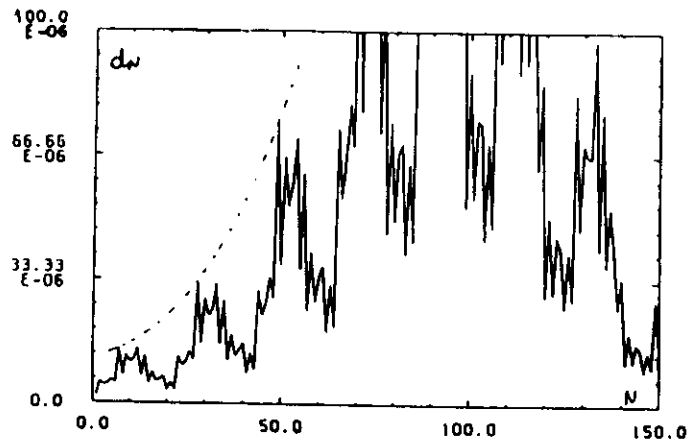
Distance in phase space!

Lyapunov-Exponent

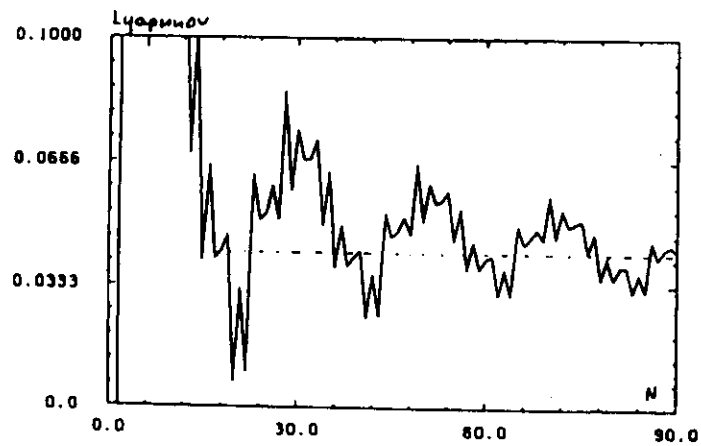


Lyapunov exponent for regular motion.

Chaotic motion

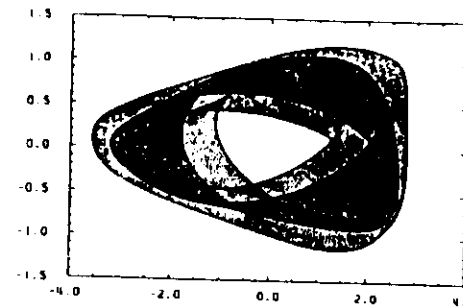


Distance of trajectories in phase for chaotic motion

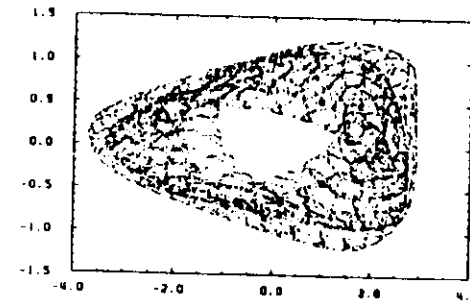


Lyapunov exponent to chaotic motion.

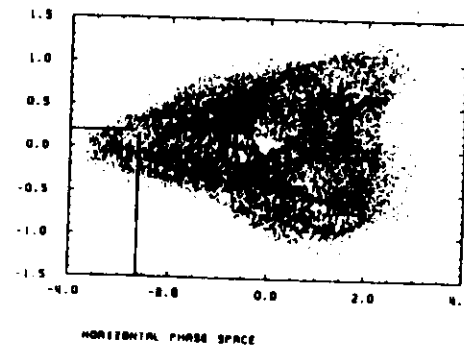
4-dimensional phase space



Projection onto the horizontal plane



increasing nonlinearities



← CHAOS

For systems with $N > 2$, degrees of freedom
the stochastic layers are connected together
and form the ARNOLD WEB

For an initial condition within the
WEB, the chaotic motion on the
WEB can carry the particle to
large amplitudes

⇒ ARNOLD DIFFUSION

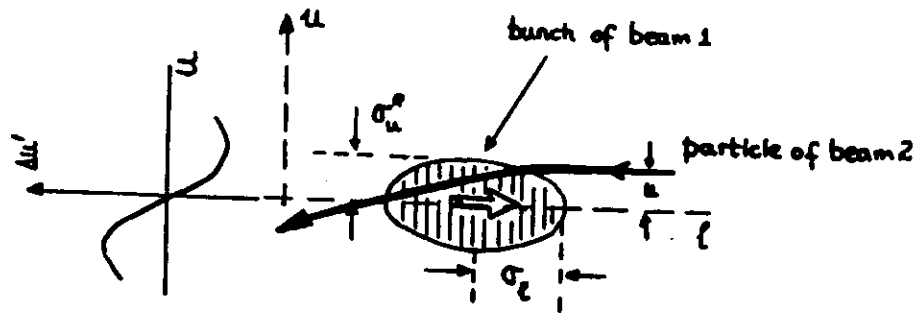
(Some) Collective Effects

So far → only single particle
dynamics has been
considered

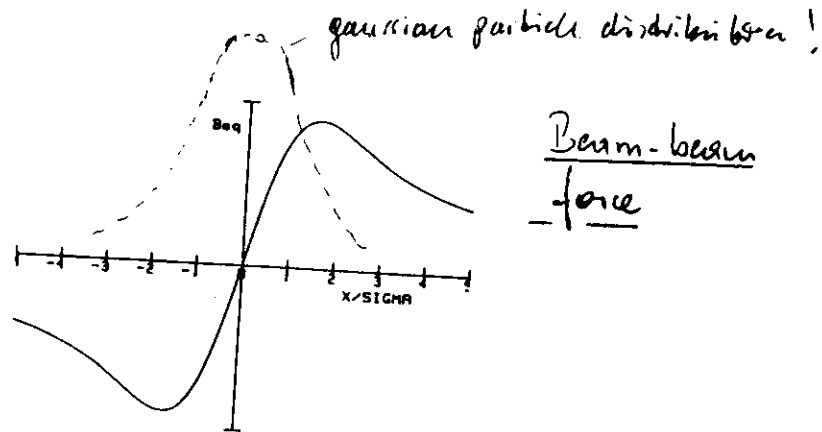
BUT! Particle ensemble (bunch)
as a whole acts via the environment
(vacuum chamber) or directly
on particles of the same bunch
or particles in other bunches in
the ring.

FORCE $\sim$ Intensity, i.e. number
of particles in the bunch

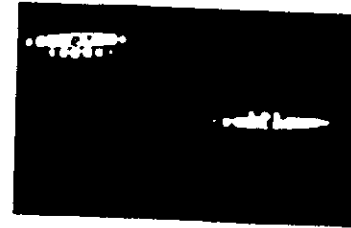
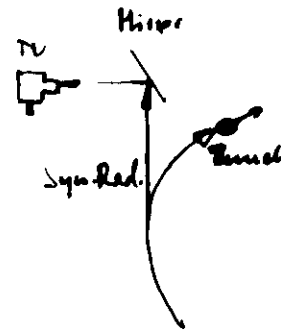
① Beam-beam effect in colliders



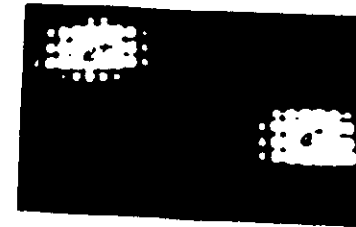
Particles experience a transverse deflecting force due to the charge of the colliding bunch $\rightarrow$



For high intensities (number of particles per bunch) the beams blow up transversely $\rightarrow$



beams separated



colliding beams

i.e. the luminosity is decreased!

$$\text{Events/sec} \quad \frac{dN}{dt} = L \cdot \sigma$$

Luminosity cross section

Low beta optics for high luminosity

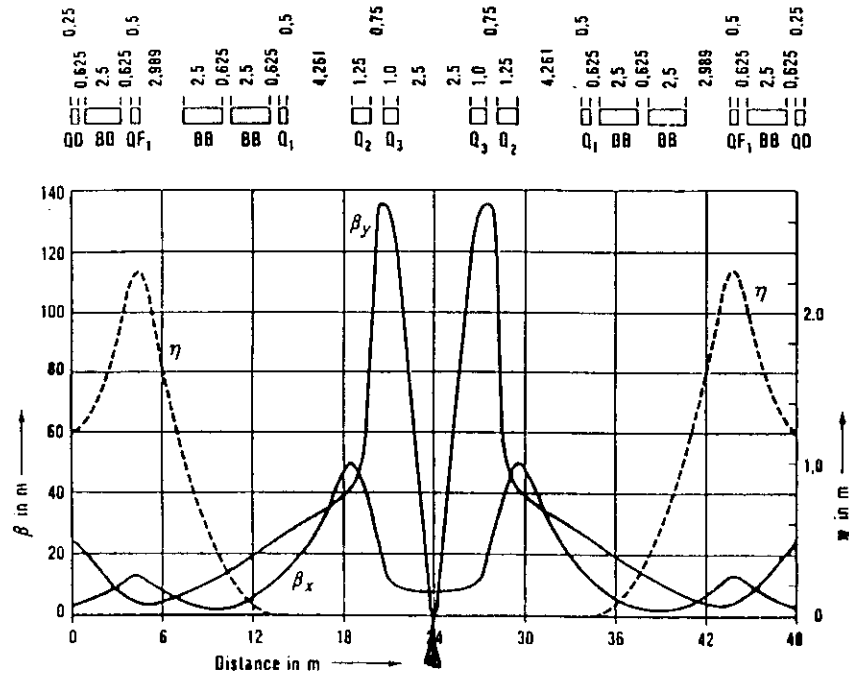


Fig. 3: Betatron functions β_x , β_y (left scale) and momentum function η



interaction
point

Luminosity is inversely proportional
to beam cross section $\rightarrow$

$$L = \underbrace{\frac{1}{4\pi e^2 f_0}}_{\text{const.}} \cdot \frac{I^+ I^-}{\sigma_x \sigma_z}$$

needed:
high current
small beam size

Deflection kick due to the beam-beam force:

In e^- rings the unperturbed charge
distribution is gaussian $\rightarrow$

$$\rho(x, z, s) = \frac{N_B e}{2\pi^{3/2} \sigma_x \sigma_z \sigma_s} \exp \left\{ -\frac{x^2}{2\sigma_x^2} - \frac{z^2}{2\sigma_z^2} - \frac{s^2}{2\sigma_s^2} \right\}$$

$\sigma_x, \sigma_z, \sigma_s$ -- rms beam dimensions
 N_B -- particles per bunch

Electric potential:

$$V(x, z, a) = \frac{Ne}{4\pi^2 \epsilon_0} \int_0^\infty \frac{\exp \left\{ -\frac{x^2}{(2a^2+q)} - \frac{z^2}{(2b^2+q)} - \frac{a^2}{(2c^2+q)} \right\} dq}{\{(2a^2+q)(2b^2+q)(2c^2+q)\}^{\frac{1}{2}}}$$

Integrated transverse deflection $\rightarrow$

$$\Delta \left(\frac{dz}{ds} \right) = \frac{e}{\gamma m_0 c^2} \int_{-\infty}^{+\infty} E_z ds = - \frac{e}{\gamma m_0 c^2} \int_{-\infty}^{+\infty} \frac{\partial V}{\partial z} ds$$

$\rightarrow$

$$\Delta z' = \frac{2Nre}{\gamma} \frac{z}{\sqrt{\pi}} \int_{-\infty}^{\infty} \int_0^\infty \frac{\exp \left\{ -\frac{x^2}{(2a^2+q)} - \frac{z^2}{(2b^2+q)} - \frac{a^2}{(2c^2+q)} \right\} dq da}{(2a^2+q)^{\frac{1}{2}} (2b^2+q)^{\frac{1}{2}} (2c^2+q)^{\frac{1}{2}}}$$

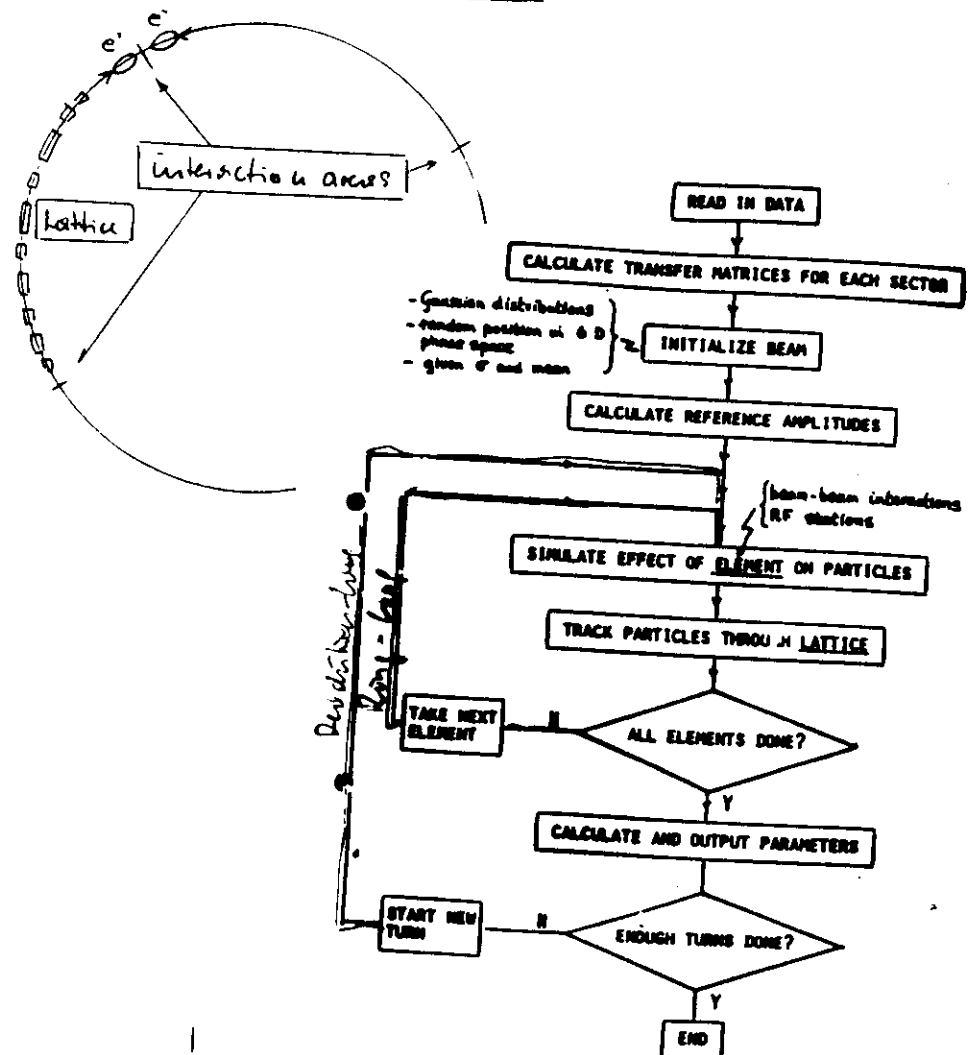
$\Downarrow$ Etkin, Baccelli

$$\Delta z' = \frac{Nre}{\gamma} \sqrt{\frac{2\pi}{a^2-b^2}} R \left[w \left(\frac{x+iz}{\sqrt{2(a^2-b^2)}} \right) \exp \left\{ -\frac{x^2}{2a^2} - \frac{z^2}{2b^2} \right\} \cdot w \left(\frac{x \frac{b}{a} + iz \frac{a}{b}}{\sqrt{2(a^2-b^2)}} \right) \right]$$

w... complex error function!

Beam-beam effect must be simulated, usually several hundred of particles are tracked over several thousands of turns.

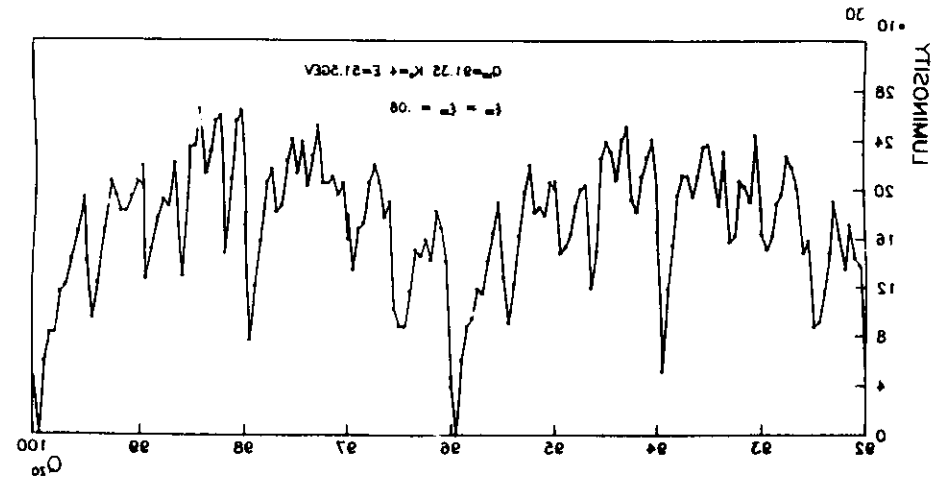
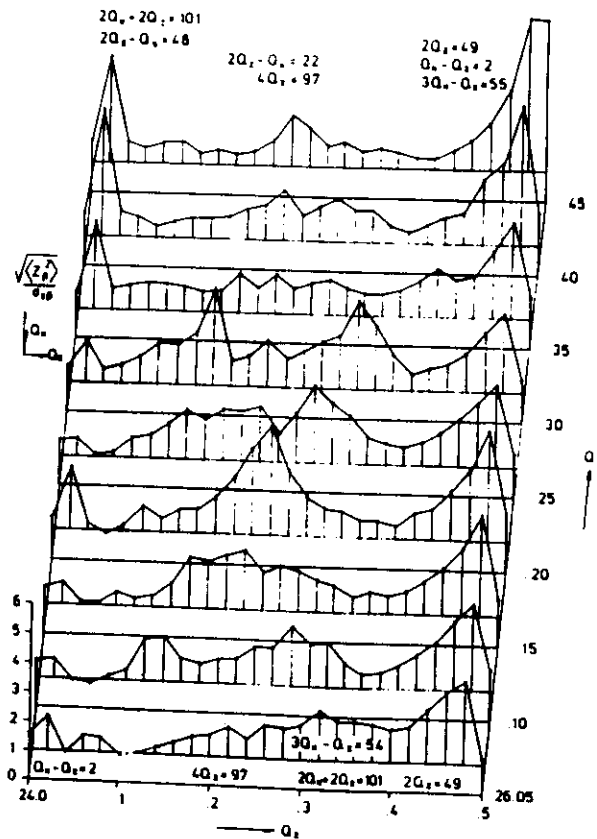
Principle of simulation:



Purpose of simulation $\rightarrow$

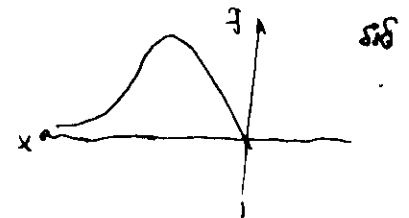
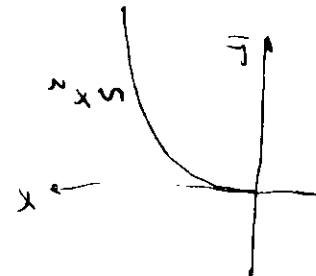
prediction of suitable working parameter
for minimum beam-beam blow up:

minib laser to minimum

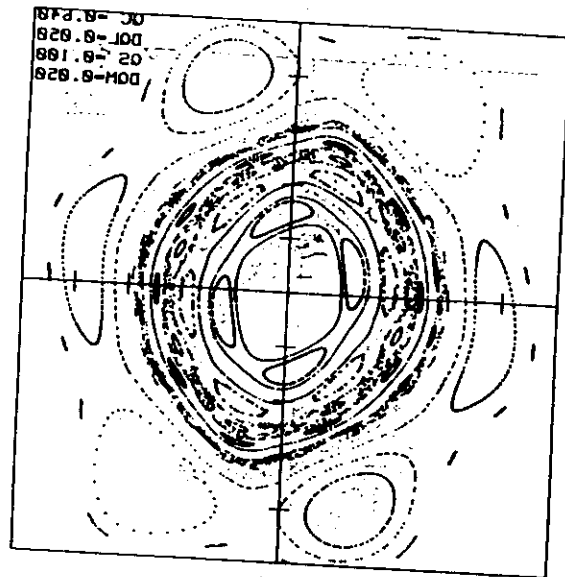


Beam-beam blow up: $F \rightarrow 0$ for $x \rightarrow 0$

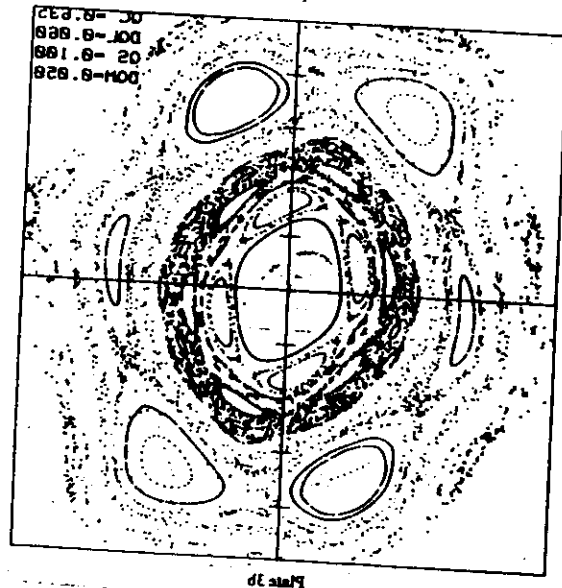
Minimum beam-beam blow up: $F \rightarrow 8$ for $x \rightarrow 0$



beam-beam resonance

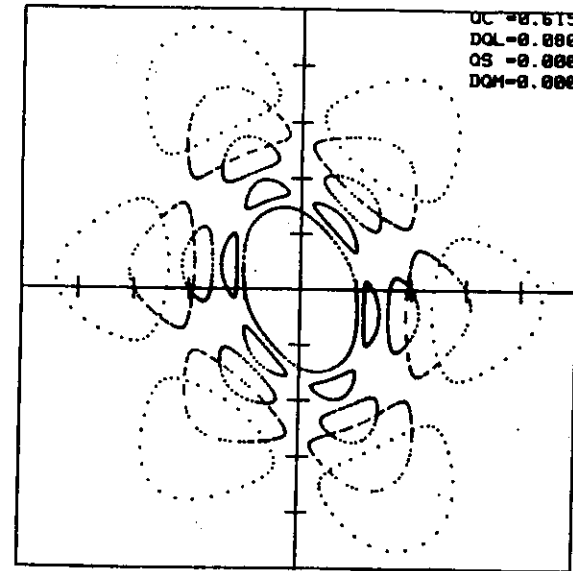


12
x

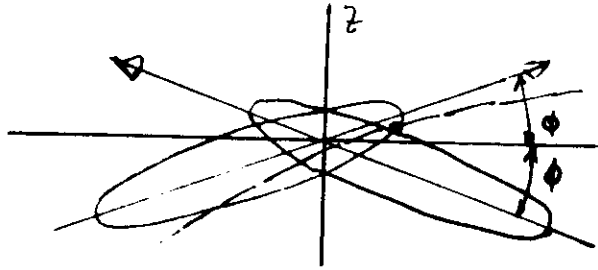


beam-beam resonance

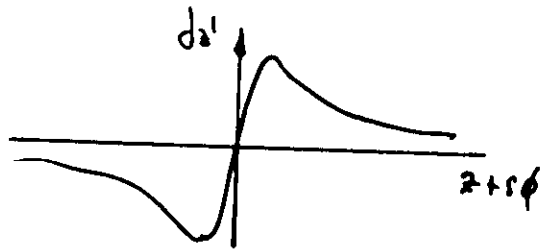
Phase space topology near a 6th order beam-beam resonance as the tune is changed:



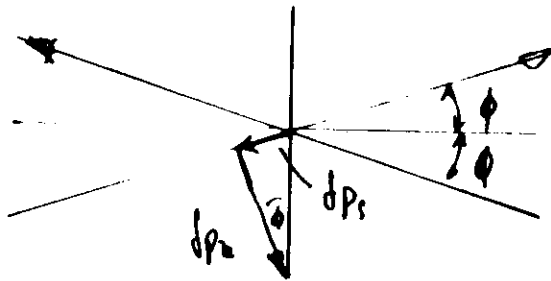
BEAM-BEAM interaction at crossing angle



Deflection: $\underline{dz' = f(z + s\phi)}$



Energy change:



$$dp_s = \phi dp_z$$

$$\left| \frac{dE}{dz} \approx \frac{dp}{l} = \phi \frac{dp_z}{p_z} = \phi dz' = \phi f(z + s\phi) \right|$$

COMPUTER SIMULATION!

→ only weak strong
intra-beam radiation &
+ feedback kicked

At the interaction point:

$$z_{n+1} = z_n$$

$$z'_{n+1} = z'_n + f(z_n + \phi s_n)$$

$$\left(\frac{\Delta E}{E} \right)_{n+1} = \left(\frac{\Delta E}{E} \right)_n + \phi f(z_n + \phi s_n)$$

$$s_{n+1} = s_n$$

Between interaction points:

$$z_{n+2} = z_{n+1} \cos \mu + z'_{n+1} \beta \sin \mu$$

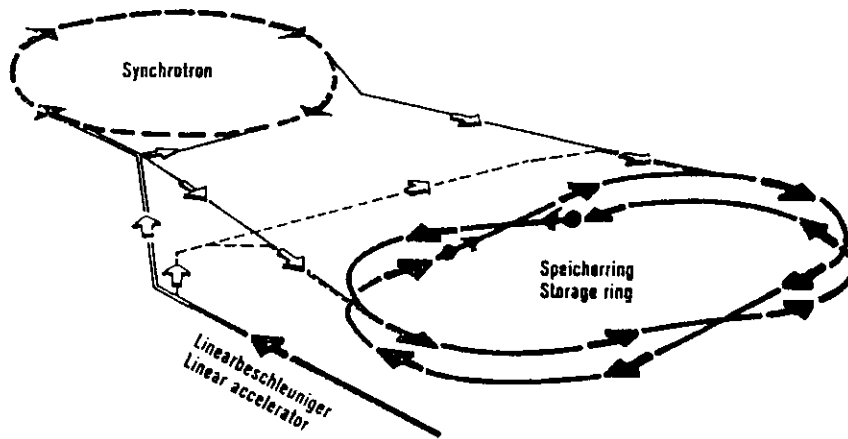
$$z'_{n+2} = -z_{n+1} \frac{\sin \mu}{\beta} + z'_{n+1} \cos \mu$$

$$\left(\frac{\Delta E}{E} \right)_{n+2} = \left(\frac{\Delta E}{E} \right)_{n+1} + \frac{eU}{E} \left[\sin(\psi_s + \frac{2\pi}{\lambda_{RF}} s_{n+1}) - \sin \psi_s \right]$$

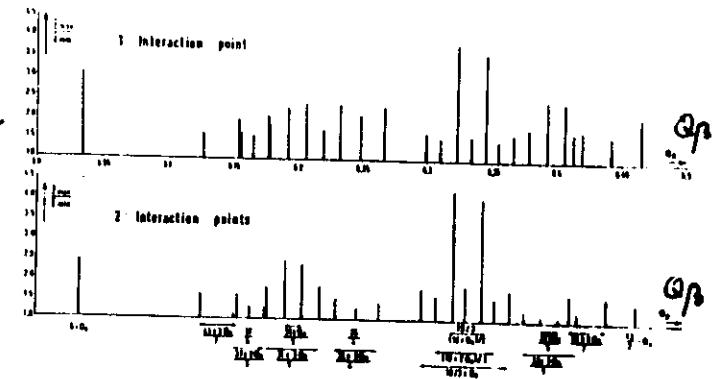
$$s_{n+2} = s_{n+1} - 2c \cdot C_0 \left(\frac{\Delta E}{E} \right)_{n+2}$$

DOUBLE RING STORAGE

Resonances due to collision with crossing-angle



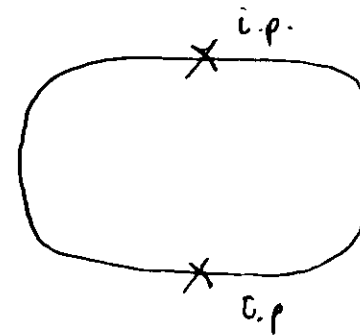
interaction point



DORIS I: $\phi = 30 \text{ mrad}$... crossing angle

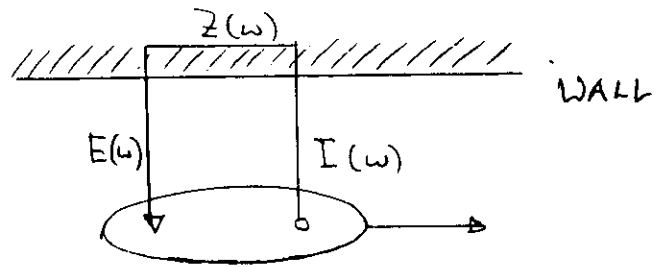
$\Rightarrow$ CURRENT LIMITING EFFECT
WITH COLLIDING BEAMS

SLC: 2 p-rings? was also a
small crossing angle



beams separated
during injection
and ramping!

② Interaction of beam with environment



$$E_{\parallel} \sim Z_{\parallel} \cdot I_{\text{beam}} \rightarrow \text{takes energy out of the beam}$$

$$F_{\perp} \sim Z_{\perp} \cdot I_{\text{beam}} \rightarrow \text{deflects the beam}$$

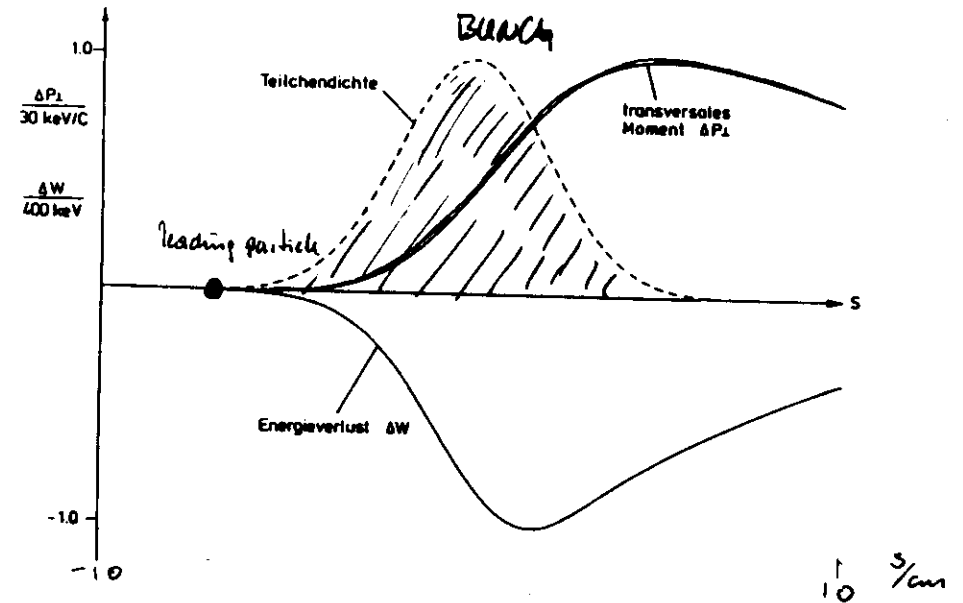
To evaluate the effect of the beam via the environment on itself $\rightarrow$

Maxwell's equations must be solved with boundaries as given by the beam environment

Numerical solution of Maxwell's equation leads to

$\rightarrow$ WAKE Potentials

$\rightarrow$ inside a Gaussian bunch ($\rho = 1 \mu\text{C}$, $\sigma = 2 \text{ cm}$) after passage of a single cell 500 MHz cavity, 0.5 cm off axis

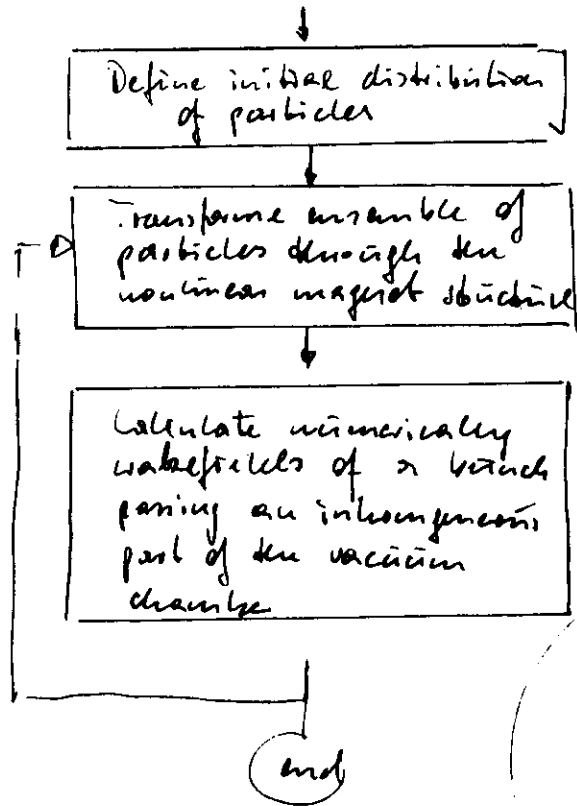


(ΔW) energy loss due to axis-symmetric (monopole fields)

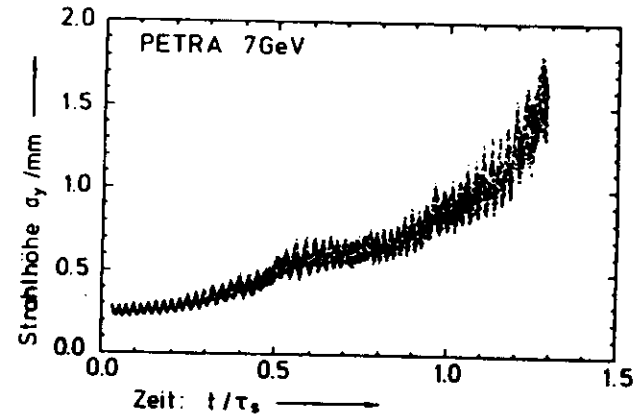
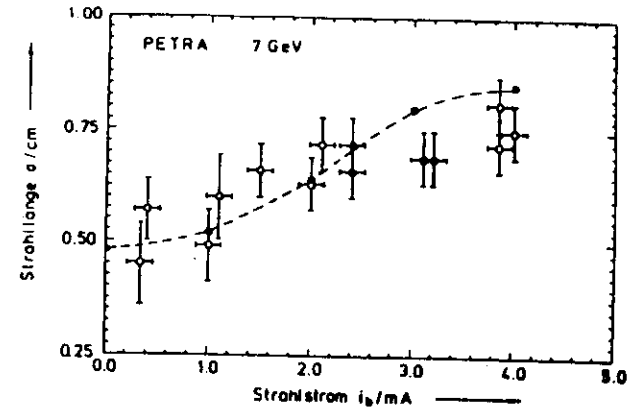
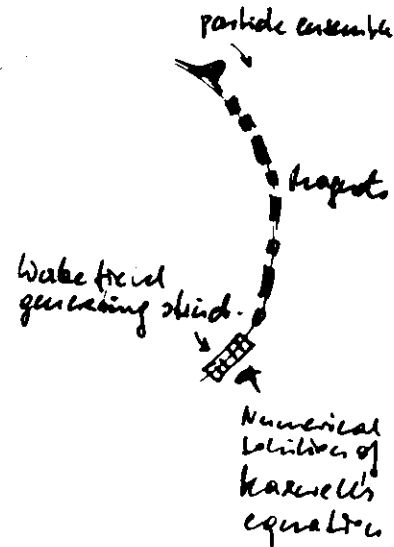
($w_{\perp}$) transverse change in momentum due to dipole fields

Simulator code can made or include
 WAKE fields in tracking codes: to
 simulate the FAST TRANSVERSE BLOW UP

Principle of Simulation:



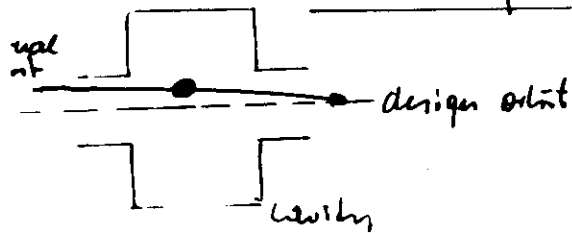
CIRCULAR ACCELERATOR



SIMULATION OF FAST TRANSVERSE
 BLOW UP !

Collective Effect generating satellite resonances:

→ needs a transverse field with a longitudinal gradient, which is produced by the BUNCH CURRENT in the accelerating structure due to displacement of the beam in the cavity



Transverse kick (z):

$$\delta z' = \frac{e}{p} \int (\vec{E}_z + v \vec{B}_x) dt$$

$$\delta z' = s \cdot \frac{e}{p} \int \left(\frac{\partial E_z}{\partial s} + v \frac{\partial B_x}{\partial s} \right) dt$$

$$\delta z' = A \cdot s$$

linear in s

Energy gain:

$$\frac{\delta E}{E} = \frac{e}{E} \int \vec{E}_s \cdot \vec{v} dt$$

$$= 2 \frac{e}{E} \int \frac{\partial E_s}{\partial z} v dt$$

$$\frac{\delta E}{E} = A \cdot z$$

$$\vec{\nabla} \times \vec{E} = \frac{\partial \vec{B}}{\partial t}$$

are equal!

In general the solution can only be found numerically →

NUMERICAL SOLUTION OF MAXWELL'S EQUATION

T. WEILAND

$$\text{curl } \vec{E} = - \frac{\partial \vec{B}}{\partial t}$$

$$\text{curl } \vec{H} = \vec{J} + \frac{\partial \vec{D}}{\partial t} + \rho \vec{v}$$

$$\text{div } \vec{D} = \rho$$

$$\text{div } \vec{B} = 0$$

rewrite in integral representation →

$\vec{E}, \vec{H} \dots$ fields
 $\vec{D}, \vec{B} \dots$ flux densities

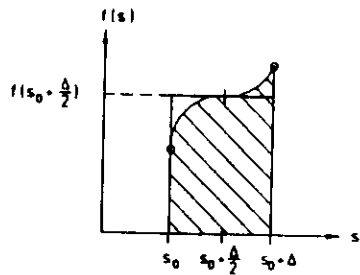
$$\oint_A \vec{E} d\vec{s} = - \iint_A \frac{\partial \vec{B}}{\partial t} d\vec{A} \quad (I)$$

$$\oint_A \vec{H} d\vec{s} = \iint_A \left(\vec{J} + \frac{\partial \vec{D}}{\partial t} + \rho \vec{v} \right) d\vec{A} \quad (II)$$

$$\iint_V \vec{B} d\vec{A} = 0 \quad (III)$$

$$\iint_V \left(\frac{\partial \vec{D}}{\partial t}, \vec{J} \right) d\vec{A} = 0 \quad (IV)$$

Integral approximation in lowest order:

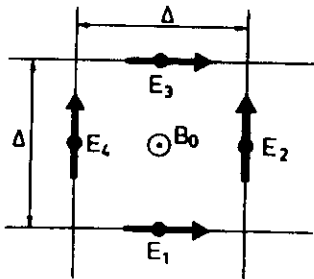


$$\int_{s_0}^{s_0 + \Delta} f(s) ds = \Delta \cdot f\left(s_0 + \frac{\Delta}{2}\right) + O(\Delta^2)$$

gives for e.g. $\rightarrow$

$$\int_A \vec{E} ds = - \int_A \frac{\partial \vec{B}}{\partial t} d\vec{A} \Rightarrow$$

$$\Delta(E_1 + E_2 - E_3 - E_4) = \dot{B}_0 \cdot \Delta^2$$



2nd Maxwell equation $\rightarrow$

$$\oint_A \vec{H} ds = \iint_A \left(\frac{\partial D}{\partial t} + \vec{j} + \rho \vec{v} \right) d\vec{A}$$

$\rightarrow$

$$\frac{1}{\mu} (B_1 + B_2 + B_3 + B_4) = \Delta^2 (\epsilon \dot{E}_0 + \vec{j} E_0 + \rho \cdot \vec{v})$$

$$\vec{D} = \epsilon \vec{E}$$

ϵ permittivity

$$\vec{B} = \mu \vec{H}$$

μ permeability

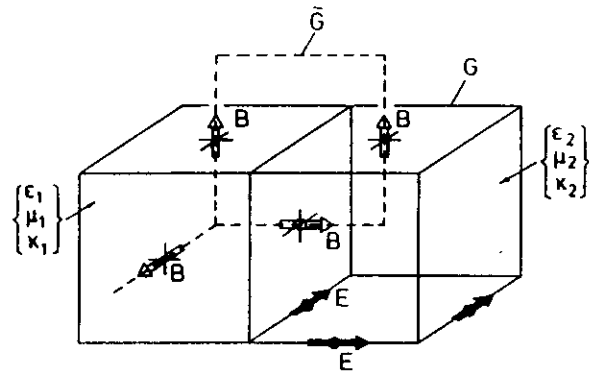
$$\vec{j} = \gamma \vec{E}$$

γ conductivity

(here ϵ, μ, γ = constant!)

The choice of a DUAL GRID implicitly satisfy Maxwell's Equation 3 and 4.

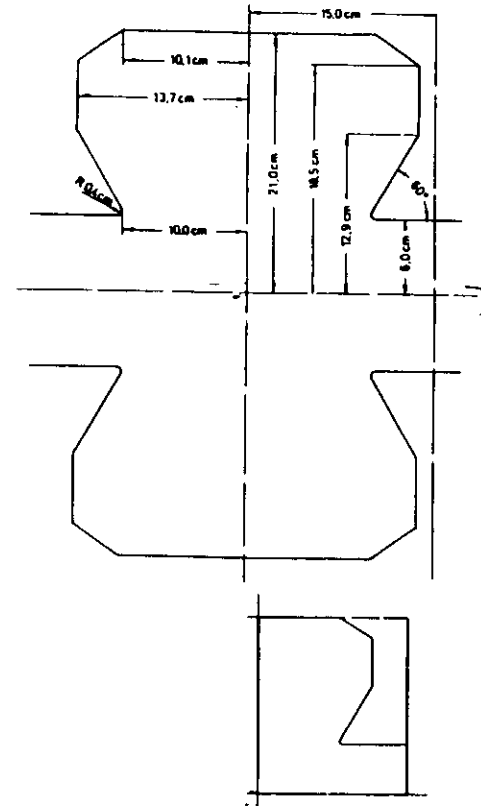
DUAL MESH $\rightarrow$



With time discretization we get for the Maxwell's equations in the mesh $\rightarrow$

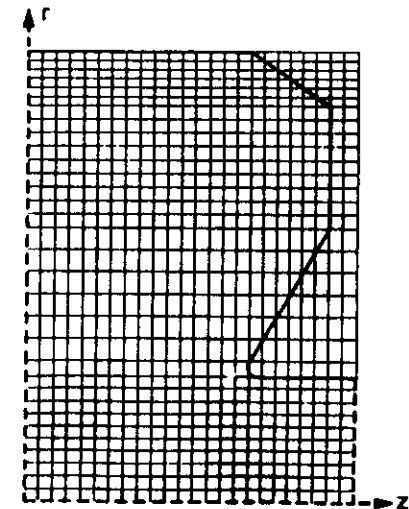
$$\begin{aligned} \vec{B}_o(t=T+\frac{\Delta t}{2}) \cdot \vec{B}_o(t=T-\frac{\Delta t}{2}) - \frac{\Delta t}{\Delta} (\vec{E}_1 + \vec{E}_2 - \vec{E}_3 - \vec{E}_4)(t=T) \\ \vec{E}_o(t=T+\Delta t) \cdot \vec{E}_o(t=T) + \frac{1}{\mu\epsilon} \frac{\Delta t}{\Delta} (\vec{B}_1 + \vec{B}_2 - \vec{B}_3 - \vec{B}_4)(t=T+\frac{\Delta t}{2}) \end{aligned}$$

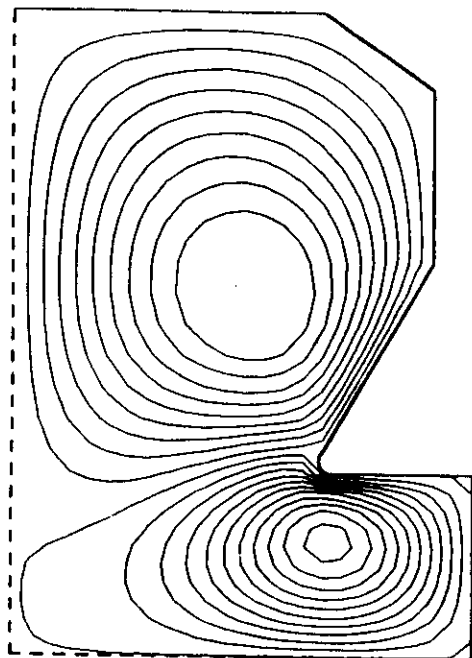
(here $\vec{T}, \vec{f} \rightarrow 0$)



Mesh generation!

Dynamic MESH for cavity

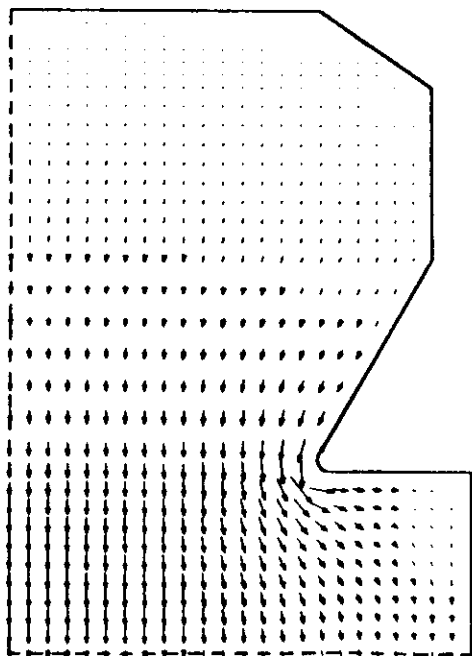




Contour plot

E_y (at $\phi = 90^\circ$)

- for the lowest dipole mode in a 500 MHz PETRA cavity

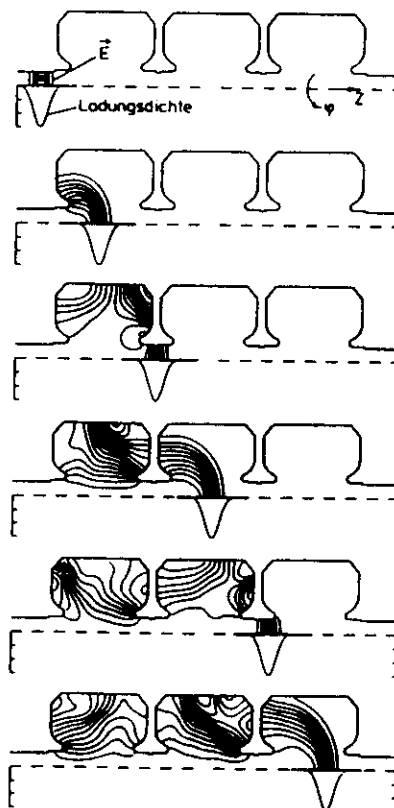


Magnetic field (at $\phi = 90^\circ$)

of the lowest dipole mode in a 500 MHz

PETRA cavity

WAKEFIELDS DUE TO MOVING CHARGES

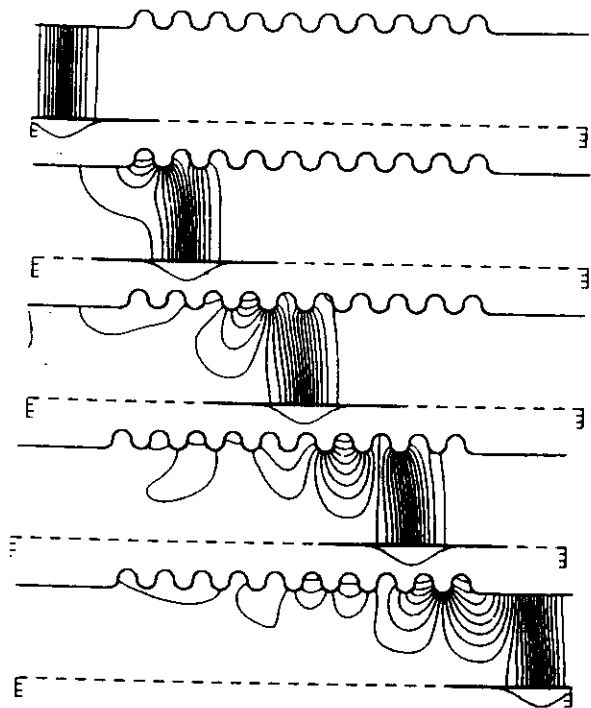


Bunch passing
a 3-cell
accelerating
structure

T. WEILAND

A

leads to coupled bunch instabilities
→ dangerous for radiation sources !!



Electromagnetic field of a Gaussian bunch of charged particles traversing a bellow.

⇒ they must be shielded!

To find the modes of a cavity, Maxwell's equations can be solved in frequency domain:

$$\frac{\partial}{\partial t} \rightarrow i\omega \quad (\text{SUPERFISH})$$

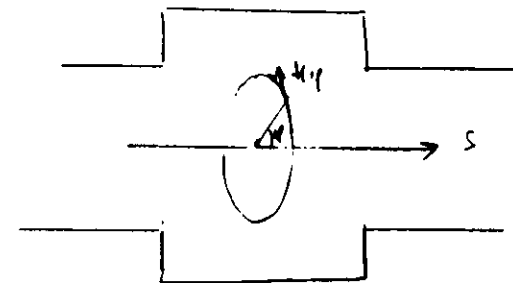
$$\left. \begin{array}{l} \nabla \times \vec{H} = k \vec{E} \\ \nabla \times \vec{E} = -k \vec{H} \end{array} \right\} \rightarrow \boxed{\nabla \times (\nabla \times \vec{H}) = k^2 \vec{H}}$$

$$k = \frac{\omega}{c}$$

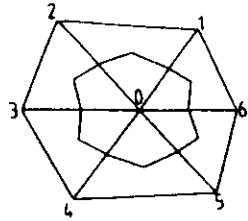
Difference equations

$$\int \nabla \times (\nabla \times \vec{H}) d\vec{A} = k^2 \int \vec{H} d\vec{A}$$

For objects with cylindrical symmetry the only nonvanishing component is $d\phi$



Triangular MESH:



Assuming: H_q = linear inside each triangle $\Rightarrow$

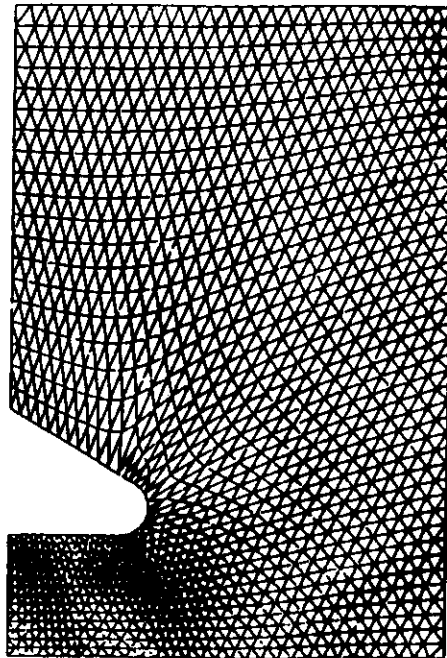
H_q is uniquely determined everywhere in the triangle by its values at the corners.

Equation for each interior mesh point:

$$\sum_{u=0}^6 H_q n (a_u + b_u^2) = 0$$

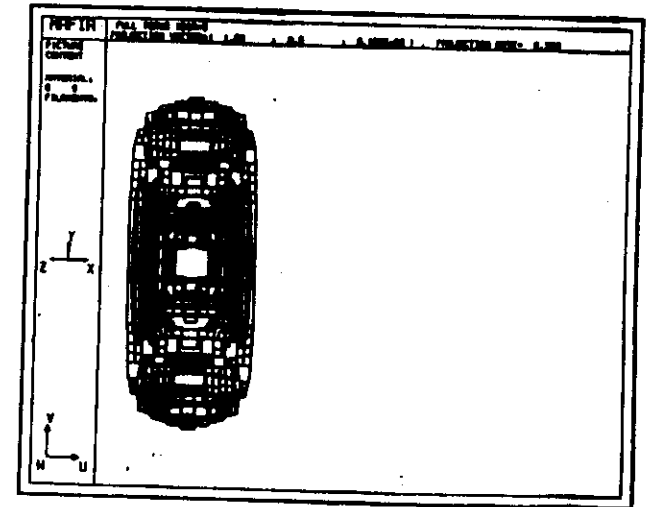
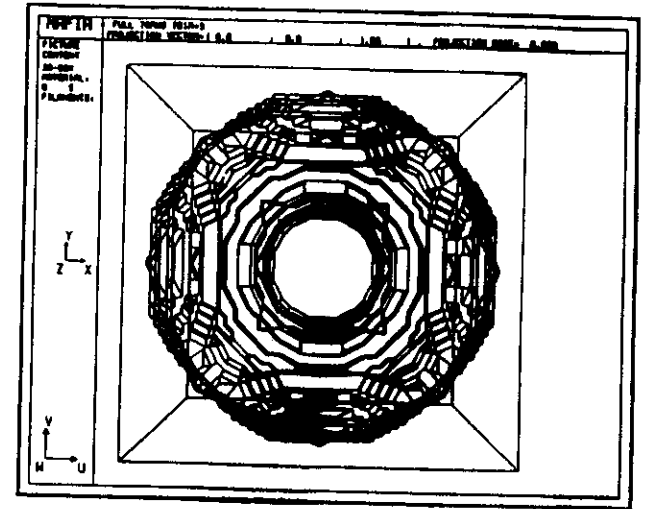
$a_u, b_u \dots$ depend on meshpoint coordinates only

triangular mesh for cavity $\rightarrow$



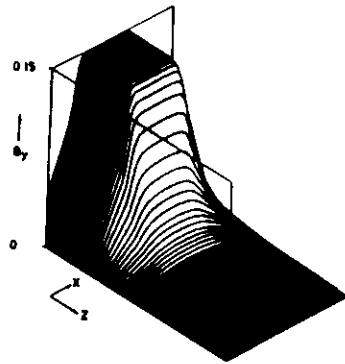
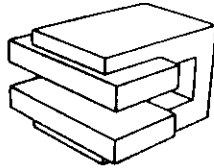
3-dimensional field calculation
(MAFIA)

Mesh generator for Torus $\rightarrow$



Correction dipole magnet field (vertical)
in the midplane:
(Pgm. PROF1) W.R. NOVEMBER

W.R. NOVEMBER



Median plane field!

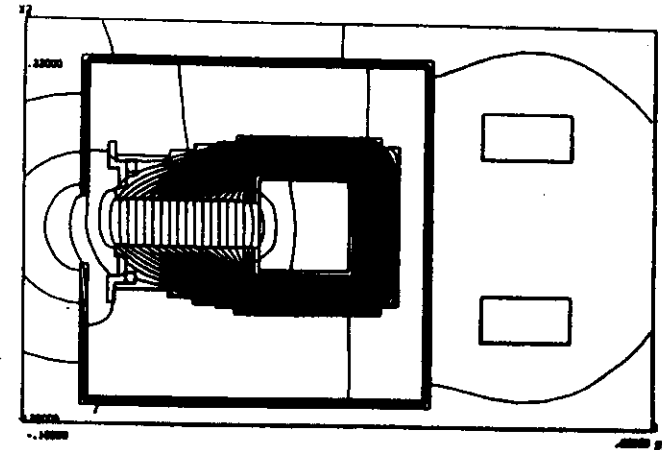


Fig. 3.6. HERA e^- arc bending magnet

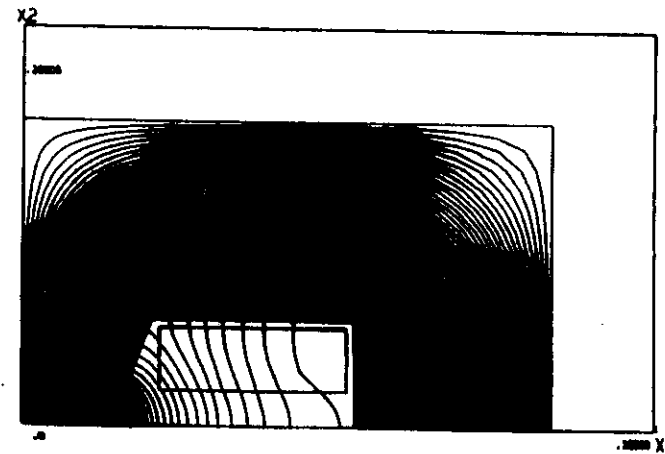


Fig. 3.7. HERA injection magnet