

704/00
v2
c1
Ref.

0 000 000 034409 K



INTERNATIONAL ATOMIC ENERGY AGENCY
UNITED NATIONS EDUCATIONAL, SCIENTIFIC AND CULTURAL ORGANIZATION



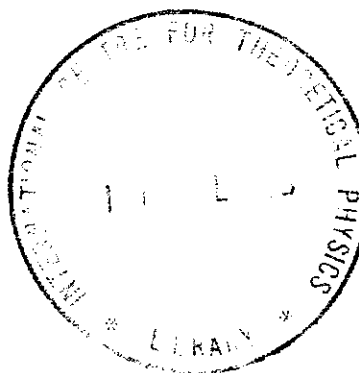
INTERNATIONAL CENTRE FOR THEORETICAL PHYSICS

34100 TRIESTE (ITALY) - P.O.B. 588 - MIRAMARE - STRADA COSTIERA 11 - TELEPHONE: 2240-1
CABLE: CENTRATOM - TELEX 460882-1

HA.SME/285 - 21

WINTER COLLEGE ON
LASER PHYSICS: SEMICONDUCTOR LASERS
AND INTEGRATED OPTICS

(22 February - 11 March 1968)

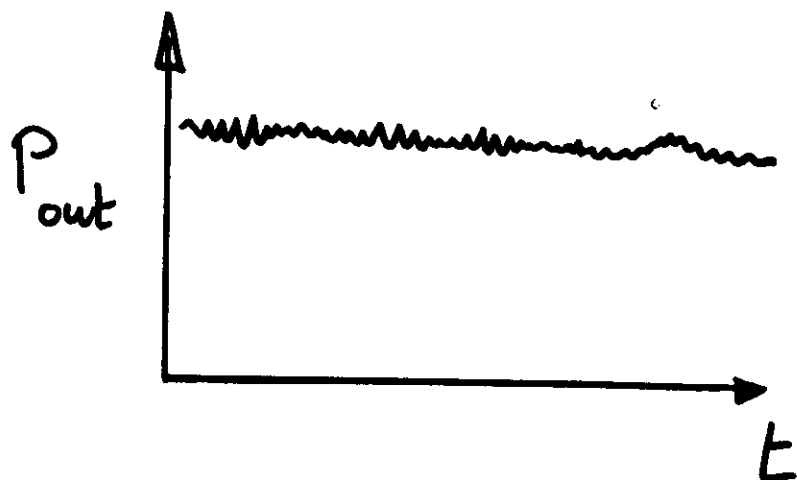


CONFERENCE & NOISE PROPERTIES
OF LASER DIODES
(II)

P. Spano
Fondazione Ugo Bordoni
Rome, Italy

Intensity Noise

- 1 Total Intensity Noise

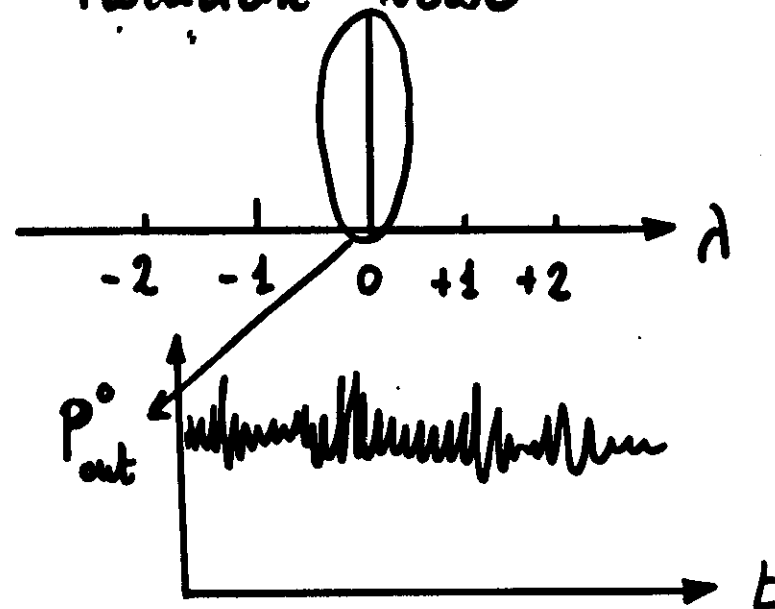


Important in Intensity modulated communication systems

Causes

Amplification of quantum fluctuations of electron and photon population in the resonator.

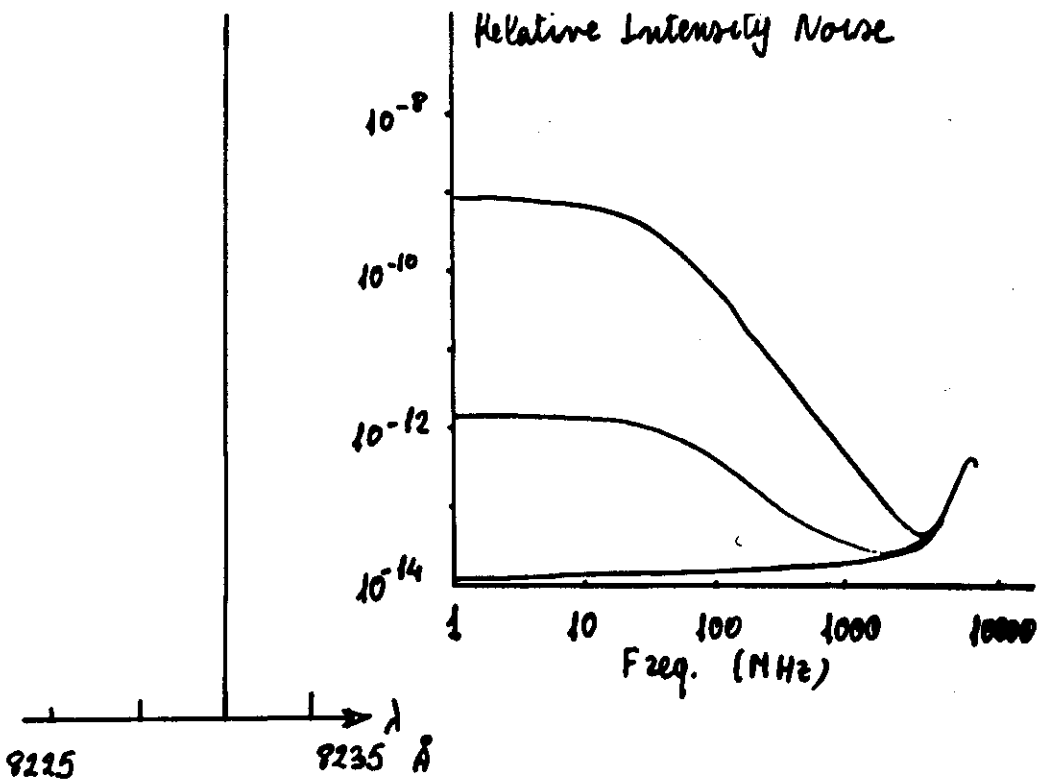
- 2 Partition Noise



Important in High frequency Intensity modulated communication systems (due to chromatic dispersion in fibers)

Causes

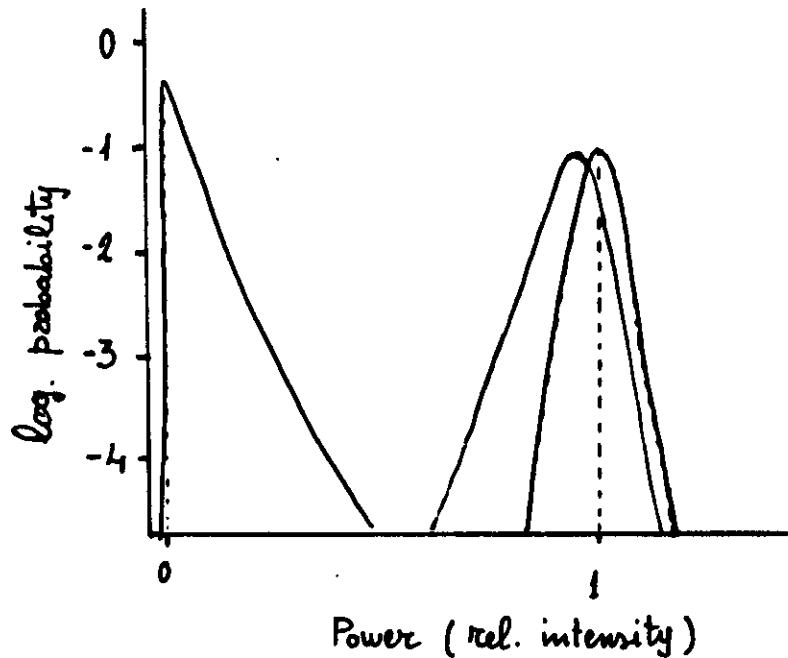
Quantum fluctuations, again.



-3 Phase or frequency noise

$$E(t) = E_0 \exp[i(\omega_0 t + \phi)]$$

$$\omega_{\text{inst}} = \omega_0 + \dot{\phi}$$



Important in coherent communication systems

Causes

Thermal and mechanical deformation of the cavity. (extrinsic noise)

Spontaneous emission ^{of photons} with random phase into coherent field (intrinsic noise)

SLM-LD can be employed as:

- Transmitters
- Modulators
- Local oscillators
- Optical amplifiers

In all these applications phase-noise determines a degradation of the system performances.

(Kikuchi K. et al. J. Lightwave
Tech. 1984)

- General Introduction to the formalism
- Experimental observations
- Theory
- Methods useful for reduction of phase-noise.

Introduction to the formalism.

Phase-noise can be characterized by

1) Power spectrum of the field

=
lineshape

$$S_E(\omega) = \int_{-\infty}^{+\infty} R_E(\tau) e^{-i\omega\tau} d\tau$$

2) Power spectrum of instantaneous frequency $\dot{\phi}$

$$S_{\dot{\phi}}(\Omega) = \int_{-\infty}^{+\infty} R_{\dot{\phi}}(\tau) e^{-i\Omega\tau} d\tau$$

3) Variance of the phase difference

$$\sigma_{\Delta\phi}^2(\tau) = \langle [\phi(t) - \phi(t-\tau)]^2 \rangle - \langle \phi(t) - \phi(t-\tau) \rangle^2$$

Power spectrum of the field
 $\Leftrightarrow$ LINESHAPE

$$S_E(\omega) = \int_{-\infty}^{+\infty} R_E(\tau) e^{-i\omega\tau} d\tau$$

$$R_E(\tau) = \langle E(t+\tau) E^*(t) \rangle \approx$$

$$E_0^2 e^{i\omega_0\tau} \langle e^{i\Delta\phi(t)} \rangle =$$

$$= E_0^2 e^{i\omega_0\tau} \left\langle \exp \left[i \int_t^{t+\tau} \dot{\phi}(t') dt' \right] \right\rangle$$

$$\Delta\phi(t) = \phi(t+\tau) - \phi(t)$$

$\dot{\phi}(t)$: normally distributed.
ergodic stationary process

$$R_{\Sigma}(\tau) = E_0^2 e^{i\omega_0 \tau} \exp \left\{ -\frac{1}{2} \int_0^{\tau} dt' \int_0^{t'} dt'' \langle \dot{\phi}(t') \dot{\phi}(t'') \rangle \right\} \sigma_{\Delta_{\tau} \phi}^2(\tau) = \sigma^2(\tau) =$$

$$= E_0^2 e^{i\omega_0 \tau} \exp \left\{ -\frac{1}{2} \sigma^2(\tau) \right\}$$

$$= \frac{1}{2\pi} \int_{-\infty}^{\infty} S_{\Delta_{\tau} \phi}(\Omega) d\Omega =$$

$$\sigma^2(\tau) = \langle [\Delta_{\tau} \phi(t)]^2 \rangle - [\langle \Delta_{\tau} \phi(t) \rangle]^2 =$$

$$= \langle [\Delta_{\tau} \phi(t)]^2 \rangle$$

$$= \frac{1}{\pi} \int_{-\infty}^{\infty} S_{\phi}(\Omega) (1 - \cos \Omega \tau) / \Omega^2 d\Omega$$

$$S_{\Sigma}(\omega) = E_0^2 \int_{-\infty}^{+\infty} e^{-i(\omega - \omega_0)\tau} e^{-\frac{1}{2} \sigma^2(\tau)} d\tau$$

$$\Delta \nu_L (\text{spont.}) = \frac{\hbar \omega_0 (\Delta \nu_c)^2}{P}$$

He-Ne laser:

$$P = 1 \text{ mW}, \quad \omega_0 = 3 \times 10^{15} \text{ rad/sec}$$

$$\Delta \nu_c \approx 10^5 \text{ s}^{-1}$$

$$\Delta \nu_L \approx 10^{-3} \text{ s}^{-1}$$

Ga Al As laser:

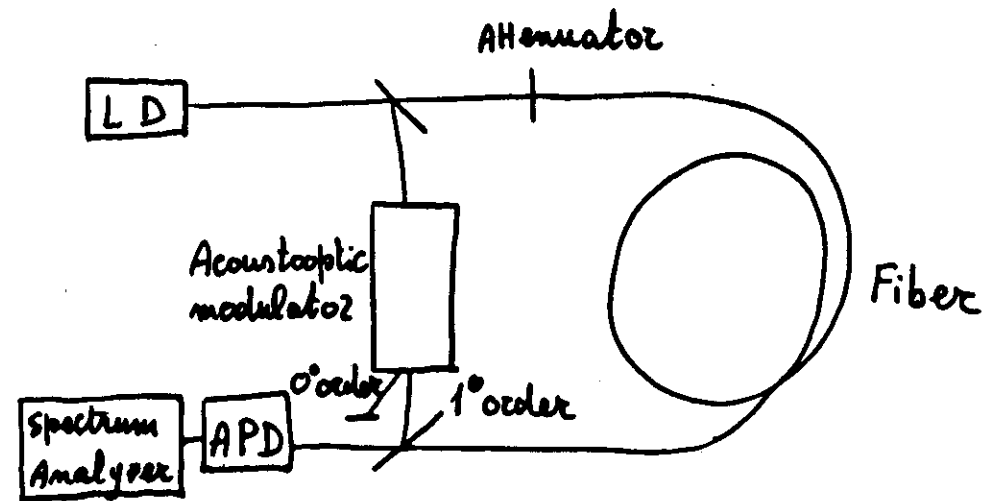
$$P = 1 \text{ mW}, \quad \omega_0 \approx 2 \times 10^{15} \text{ rad/sec}$$

$$\Delta \nu_c \approx 10^{11} \text{ s}^{-1}$$

$$\Delta \nu_L \approx 10^7 \text{ s}^{-1}$$

Experimental results

- 1) Measurement of the linewidth - lineshape
Fabry-Perot interferometer ($\Delta \nu_L \approx 10 \text{ MHz}$)
Self-heterodyne technique ($\Delta \nu_L < 100 \text{ kHz}$,
only linewidth)



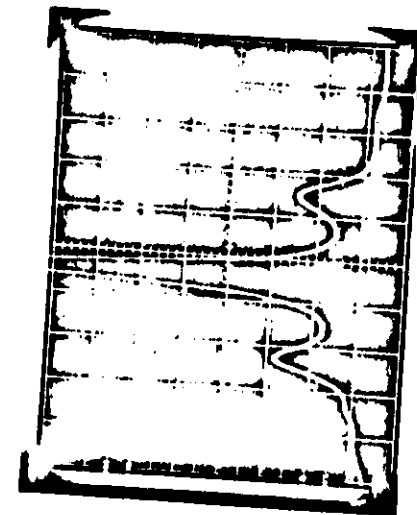
If the emission lineshape is Lorentzian

$$S_{\mathcal{E}}(\omega) = \frac{\delta \omega}{(\omega - \omega_0)^2 + (\delta \omega / 2)^2} \quad \text{and} \quad \tau_2 - \tau_1 > 2\pi / \delta \omega$$

$\Rightarrow$ signal displayed Lorentzian and $\text{FWHM} = 2\delta \omega$

Results

- Linewidth about 20-100 times larger than predicted
(Flaming, Mooradian - Appl. Phys. Lett. 1981)
- Lineshape not Lorentzian:
Presence of satellite peaks at a frequency difference from the center of the spectrum in the range 0.5 - 5 GHz.



1GHz/div
Laser Diode P=3mW

2) Measurement of $S_i(R)$ Unbalanced Michelson interferometer

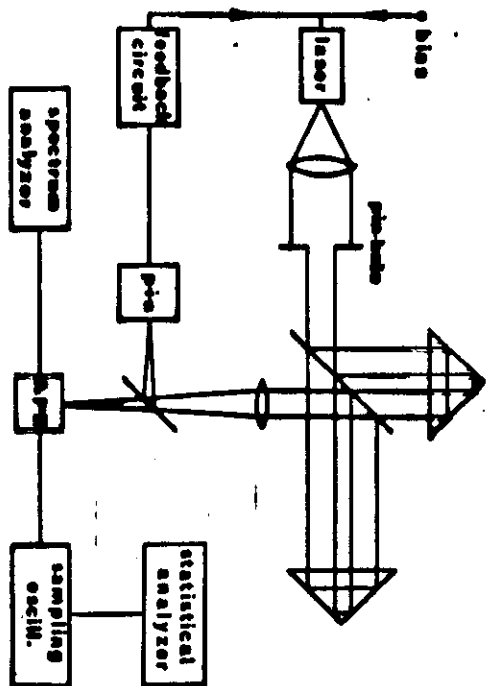


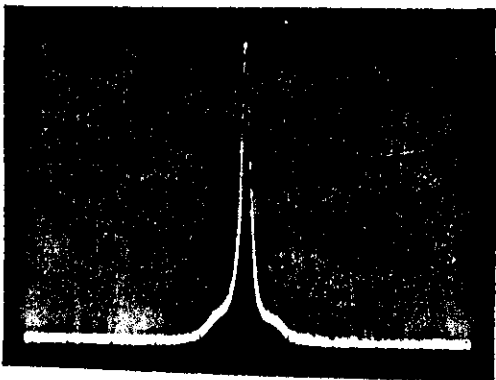
FIG. 3

(Piazzola et al. Appl. Opt. 1982)

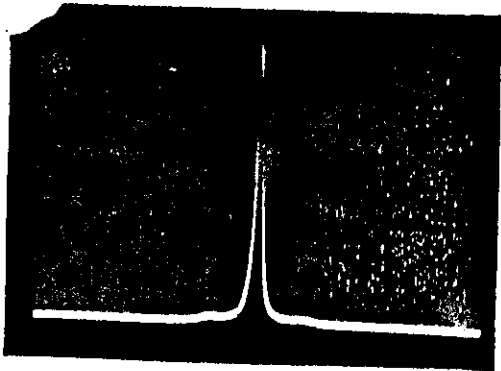
InGaAsP DFB laser

$$I_{th} = 52 \text{ mA}$$

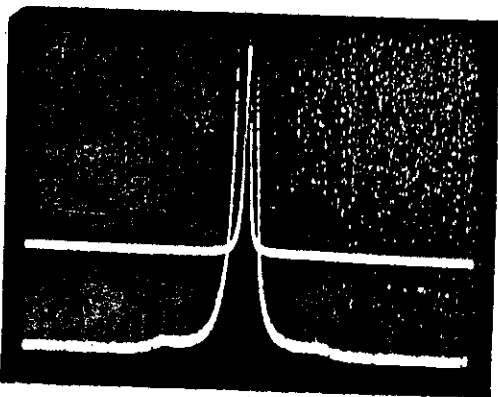
55 mA



60 mA



75 mA



x 20

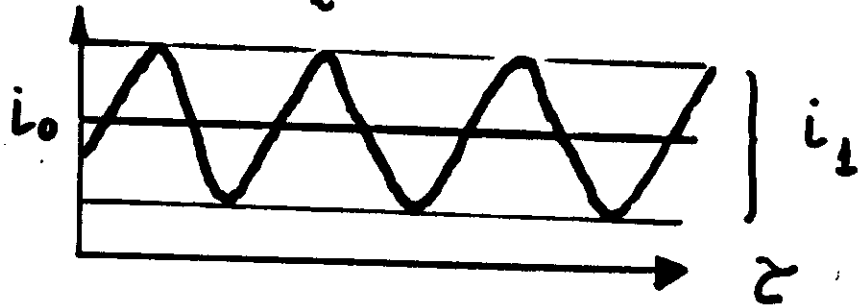
— 2 GHz

Output current from the APD

$$i(t) \propto |\xi(t) + a \xi(t-\tau)|^2$$

a = ratio of attenuation of the two fields

$$i(t) = i_0 + \frac{i_1}{2} \cos[\phi(t) - \phi(t-\tau) - \omega_0 \tau]$$



if $\omega_0 \tau = \frac{\pi}{2}$ and

$$|\phi(t) - \phi(t-\tau)| \ll \pi/2$$

$$i(t) \approx i_0 + \frac{i_1}{2} [\phi(t) - \phi(t-\tau)] = i_0 + \frac{i_1}{2} \Delta \phi$$

$$S_i(\Omega) = \frac{i_1^2}{4} R S_{\Delta \phi}(\Omega) =$$

$$= \frac{i_1^2}{4} R S_i(\Omega) (1 - \cos \Omega \tau) / \Omega^2$$

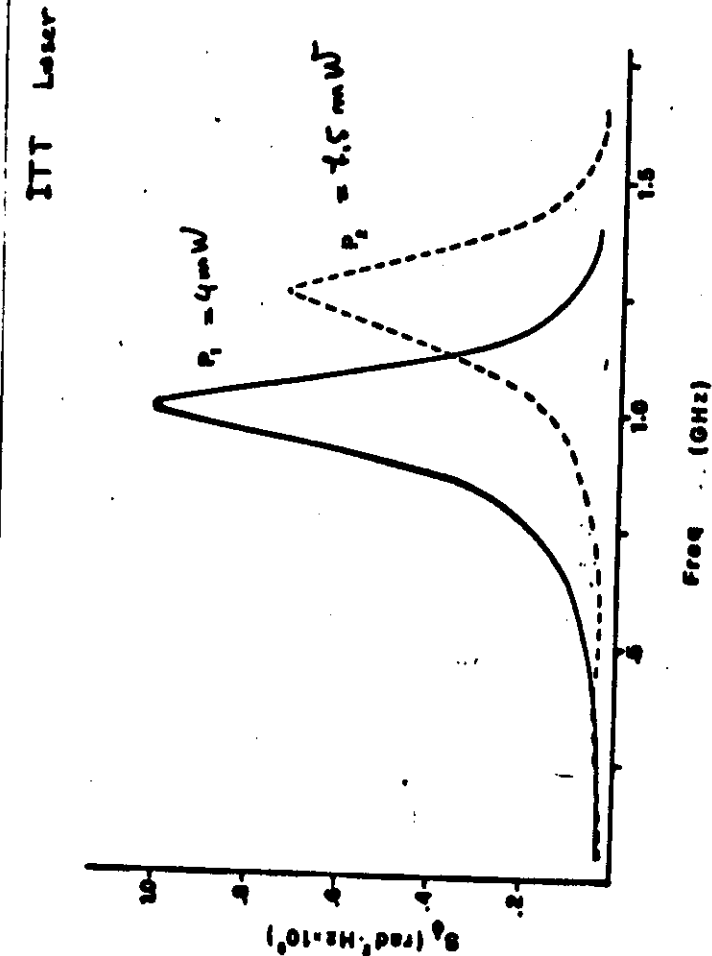
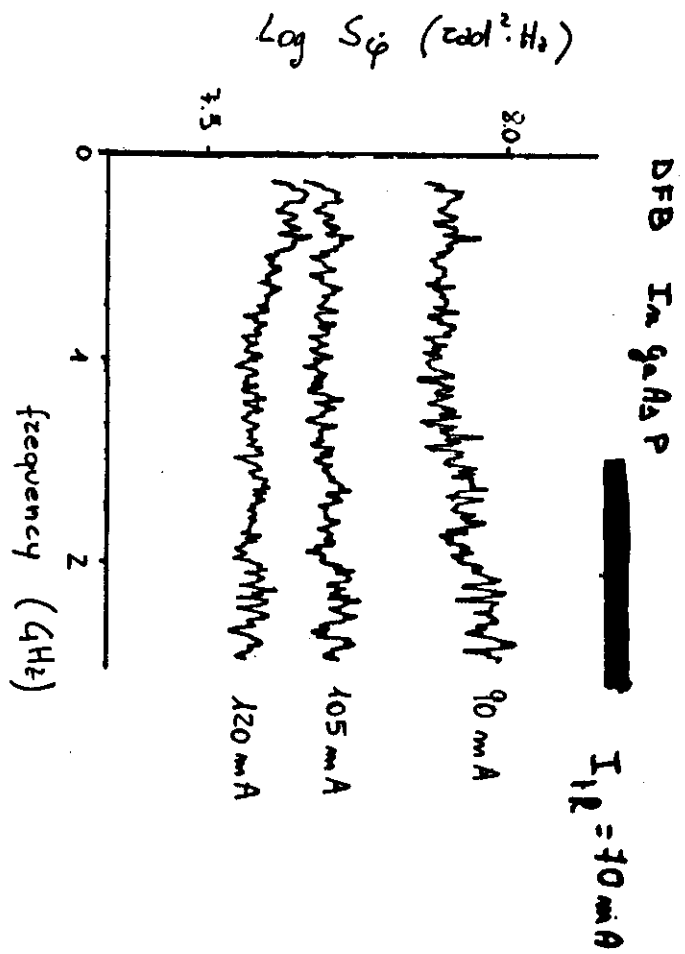
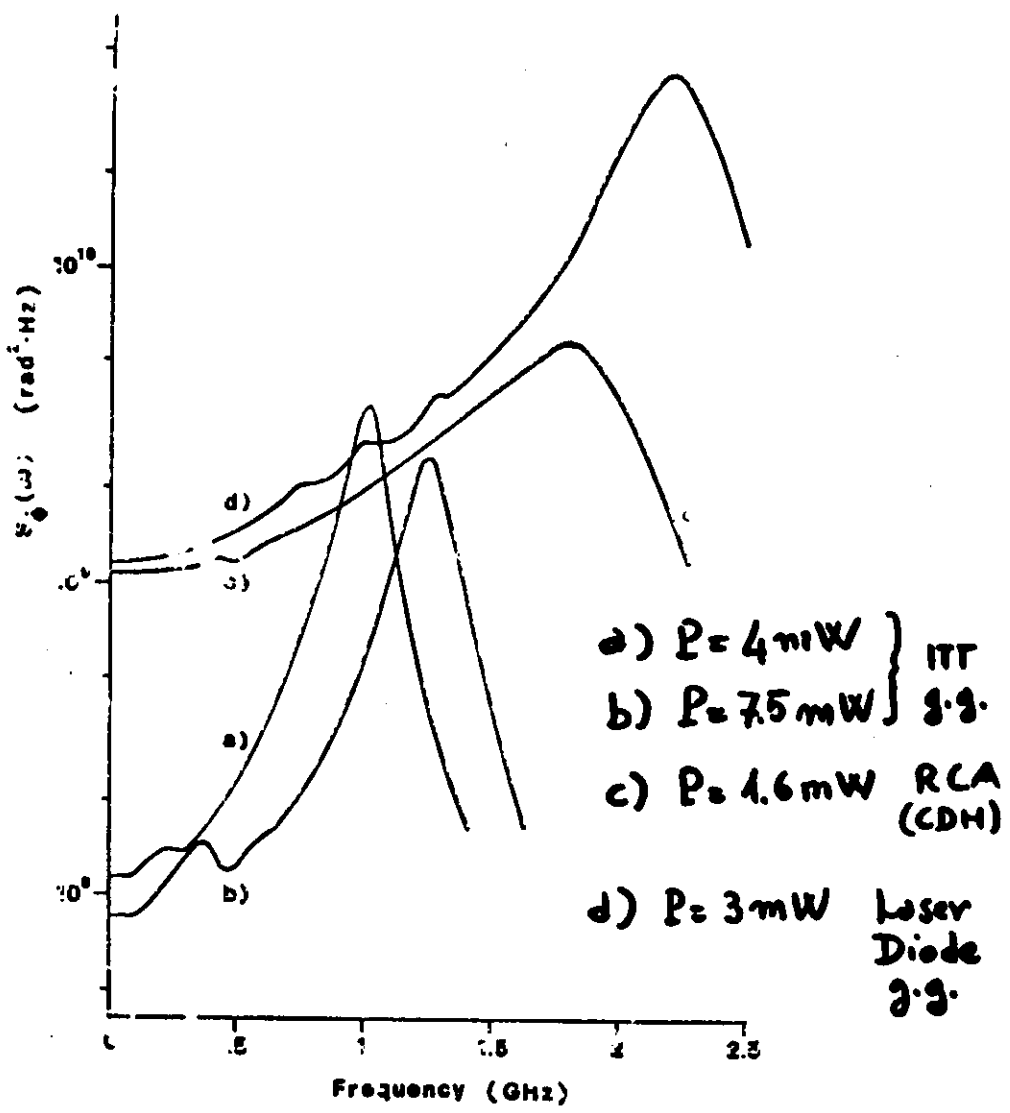


FIG. 2

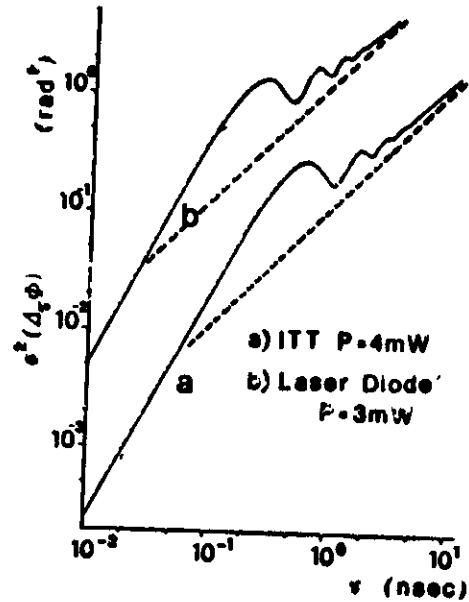


(TRACH and CHAPLYV J.Q.E. 1986)

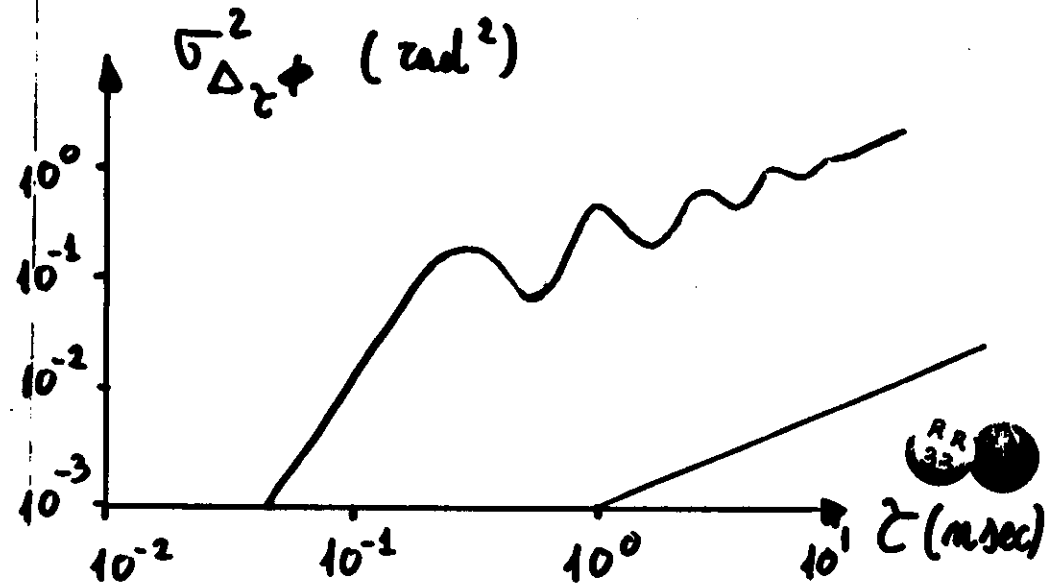
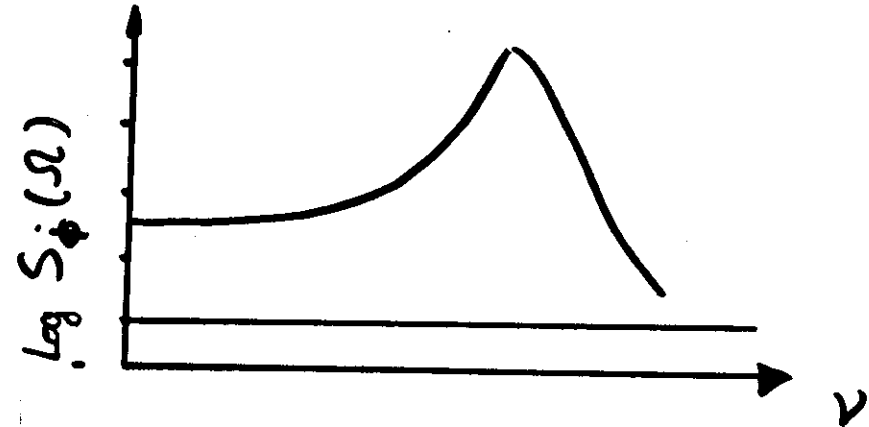
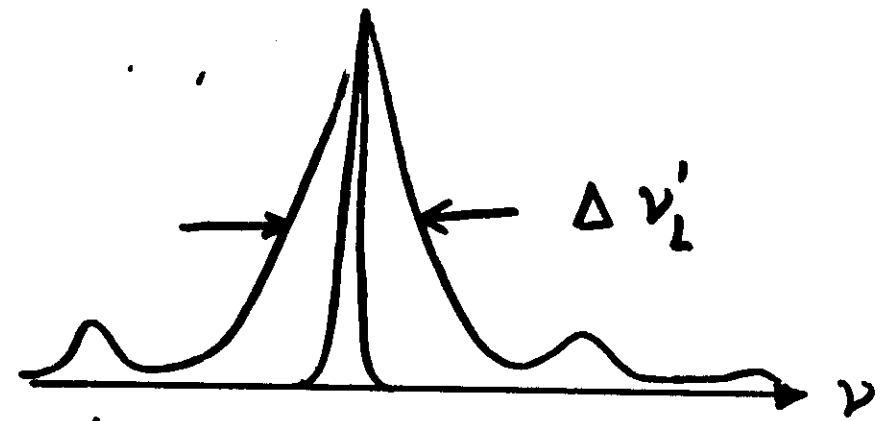


3) Measurement of $\sigma_{\Delta\phi}(\tau)$

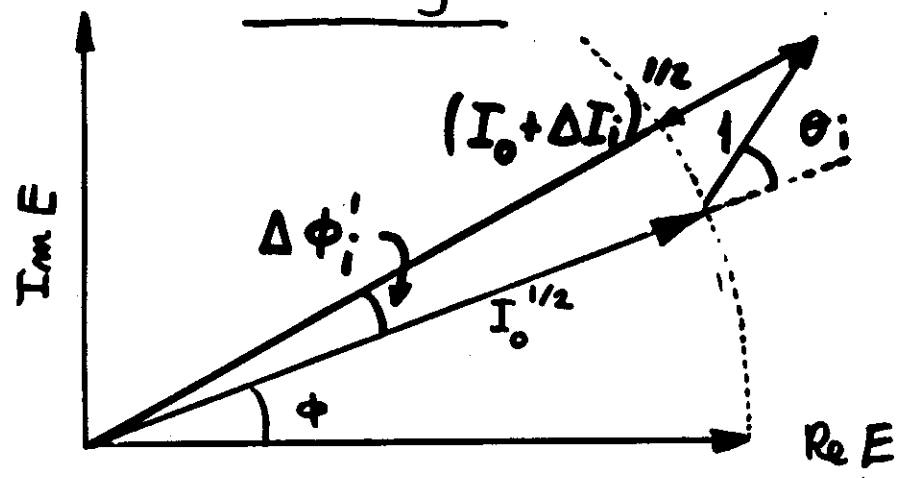
Unbalanced Michelson Interferometer + statistical analyzer



$$\sigma^2(\tau) = \frac{2}{\pi} \int_0^{\infty} \frac{S_{\dot{\phi}}(\omega)}{\omega^2} (1 - \cos \omega \tau) d\omega$$



Theory



$$E = I_0^{1/2} e^{i\phi}$$

$$I_0 = E E^* = \text{average number of photons in the cavity}$$

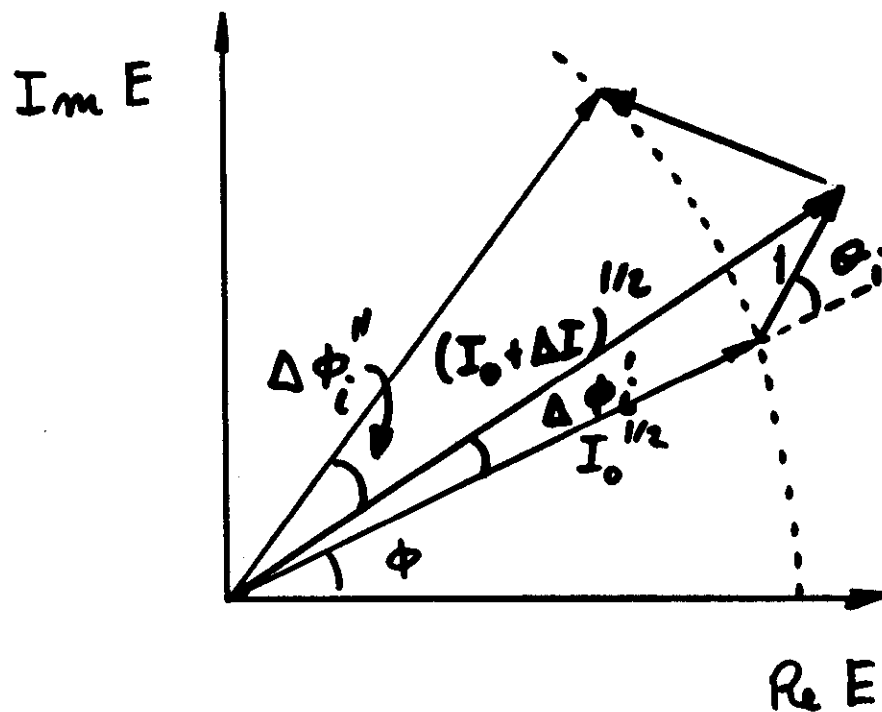
Effect of the emission of the i -th photon spontaneously emitted in the mode.

$$\Delta E_i = e^{i(\phi + \theta_i)}$$

$$\Delta I_i = |E + \Delta E_i|^2 - |E|^2 = 1 + 2I_0^{1/2} \cos \theta_i$$

$$\Delta \phi_i' = I_0^{-1/2} \sin \theta_i$$

What happens if the refractive index n is dependent on the field intensity?



$$\Delta \phi = \Delta \phi_i' + \Delta \phi_i''$$

(Henry J. G. E. 1982)



$$\eta = \eta' + i \eta''$$

$$\alpha = \Delta \eta' / \Delta \eta''$$

$$\Delta I \Rightarrow \Delta n \Rightarrow \Delta \eta'' \Rightarrow \Delta \eta'$$

↓

$$\Delta \phi_i'' = \frac{\alpha}{2I_0} (1 + 2 I_0^{1/2} \cos \theta_i)$$

$$\Delta \phi_i = \Delta \phi_i' + \Delta \phi_i'' =$$

$$= \frac{\alpha}{2I_0} + \frac{1}{I_0^{1/2}} [\sin \theta_i - \alpha \cos \theta_i]$$

R_s = average number of spontaneous emission rate in the lasing mode

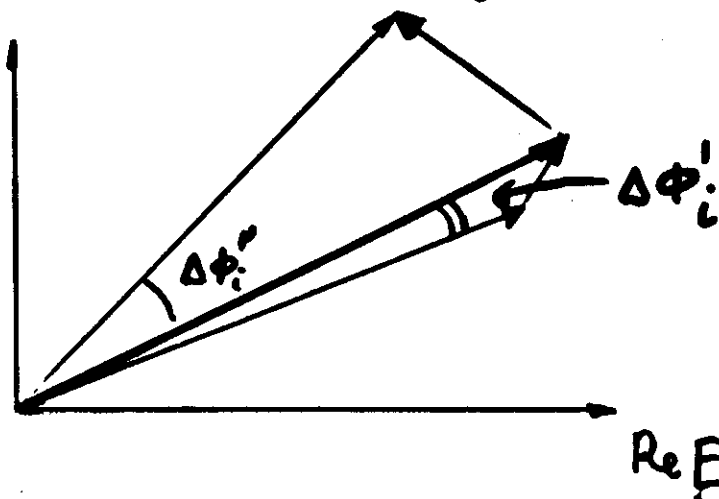
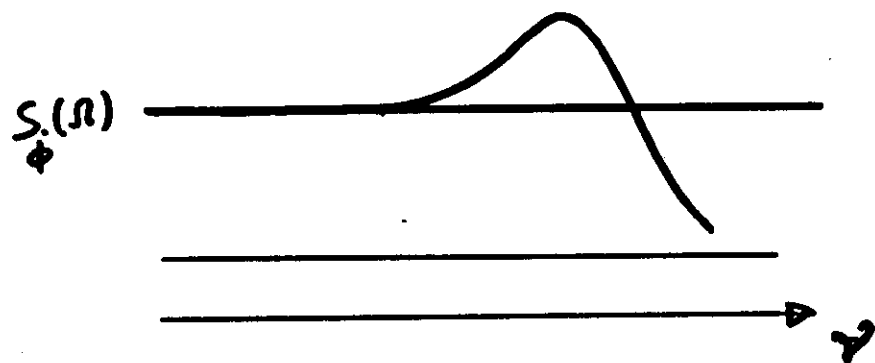
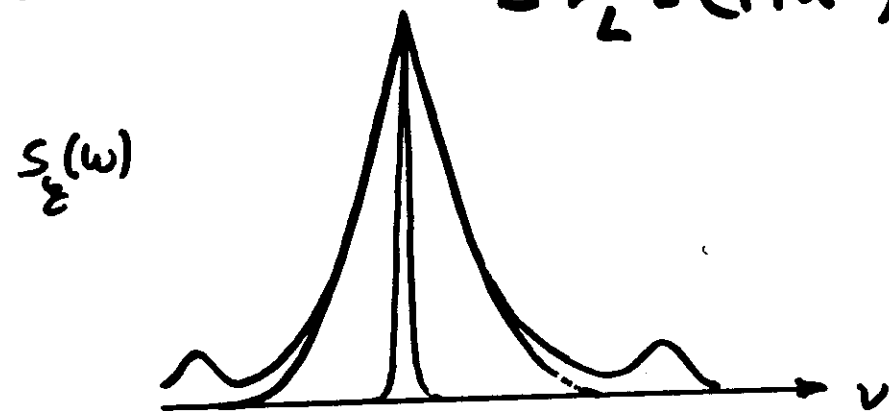
$N = R_s \tau$ = number of spontaneous emission events in a time interval τ

$$\sigma^2(\tau) = \langle \Delta \phi_i^2 \rangle - \langle \Delta \phi_i \rangle^2 =$$

$$= \frac{R_s \tau}{2 I_0} (1 + \alpha^2)$$



This variance linear in τ corresponds why the simple model does not to an emission lineshape Lorentzian, explain the presence of satellite peaks? with a width $\Delta \nu'_L = (1 + \alpha^2) \Delta \nu_L$



$$\Delta \Phi = \Delta \Phi'_i + \Delta \Phi''_i$$

$\Delta \Phi'' =$ phase shift after relaxation

$$\tau > \tau_r$$

If $\tau > \tau_r$ $\phi(t)$ and $\phi(t-\tau)$ are uncorrelated, $\phi(t)$ executes a Brownian motion and

$$\sigma^2(\tau) \propto \tau$$

$$\underline{\tau < \tau_r}$$

We can expect

- Correlation between $\phi(t)$ and $\phi(t-\tau)$

- Characteristics of correlation affected by oscillation in relaxation phenomenon

$$\begin{cases} \frac{d}{dt} \left\{ E(t) e^{i\omega_0 t} \right\} = \left\{ i\omega_N(n) + \frac{1}{2} [G(n) - \Gamma_0] \right\} E(t) e^{i\omega_0 t} \\ \frac{d}{dt} n(t) = -\gamma n(t) - G(n) |E(t)|^2 + P \end{cases}$$

$$\omega_N(n) = \frac{N \pi c}{\tau l} : \text{resonant frequency of the } N\text{-th diode cavity longitudinal mode}$$

$$G(n) : \text{gain coefficient}$$

$$\Gamma_0 : \text{cavity loss}$$

$$\gamma : \text{inverse of the spontaneous lifetime of the excited carriers}$$

$$P = \frac{j}{ed} : \text{number injection rate per unit volume of the excited carriers}$$

(Schimpe, Harth - Electron. Lett. 1983

Vahala, Yariv J. Q. E. 1983

Spano, Piazzetta, Tamburini J. Q. E. 1983

The stationary solution (i.e. $E(t) = E_0$) gives (1st eq.)

$$\begin{cases} G_1(n_0) = G_0 = \Gamma_0 \\ \omega_N(n_0) = \omega_0 \end{cases}$$

n_0 : stationary value of the carrier density (obtained through 2nd eq.)

Small variations $\Delta n(t) = n(t) - n_0$ will change the values of the gain and of the refractive index. In a first order approximation

$$\begin{cases} G_1 = G_0 + G_n \Delta n + G_I \Delta I \\ \eta = \eta_0 + \eta_n \Delta n \end{cases}$$

$$\begin{aligned} G_n &= \left[\frac{\partial G(n)}{\partial n} \right]_{n=n_0} & \eta_n &= \left[\frac{d}{dn} \eta(n) \right]_{n=n_0} \\ \eta_0 &= \eta(n_0) & G_I &= \frac{\partial G}{\partial I} \end{aligned}$$

$$E(t) = [E_0 + e(t)] e^{i\phi(t)}$$

Substituting into the 1st eq. of the previous system gives

$$\begin{cases} \dot{e}(t) = \frac{1}{2} [G - \Gamma_0] [E_0 + e(t)] \\ \dot{\phi}(t) = \omega_N(n) - \omega_0 \end{cases}$$

Let us introduce the new variables

$N = nV$: the number of carriers

$$I(t) = V |E(t)|^2 \approx V [E_0^2 + 2e(t)E_0] =$$

$= I_0 + \Delta I(t)$: the number of photons belonging to the mode in the cavity

V : mode volume
filling factor = 1

Within a first approximation

$$\boxed{\omega_N^{(n)} = \omega_0 - \frac{\omega_0}{\eta_0} \left[\eta_n \Delta n + \frac{\partial \eta}{\partial \omega} \bigg|_{\omega=\omega_0} \dot{\phi}(t) \right]}$$

so that

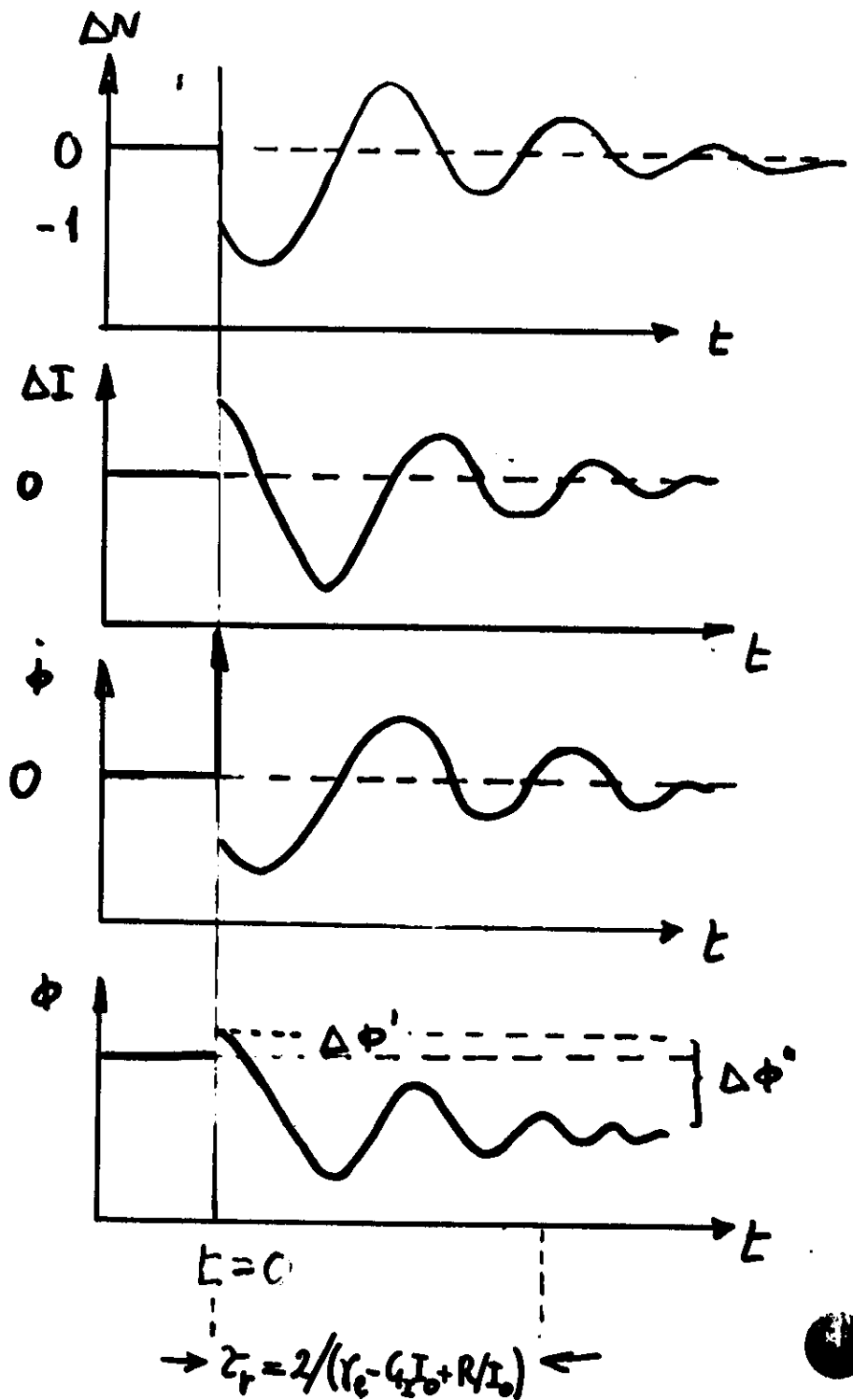
$$\begin{cases} \Delta \dot{I}(t) = \frac{G_n I_0}{V} \Delta N(t) + (G_I I_0 - \frac{R}{I_0}) \Delta I \\ \dot{\phi}(t) = \frac{G_n \alpha}{2V} \Delta N(t) \\ \Delta \dot{N}(t) = -\gamma_e \Delta N(t) - (G_0 + G_I I_0) \Delta I \end{cases}$$

$$\boxed{\alpha = - \frac{2\omega_0 \eta_n V_g}{G_n c}}$$

R = rate of spont. emission into the mode

$$\boxed{\gamma_e = \gamma + \frac{G_n I_0}{V}}$$

$$\boxed{\nu_g = \frac{c}{\left[\eta_0 + \frac{\partial \eta}{\partial \omega} \bigg|_{\omega=\omega_0} \right]}}$$



In order to describe noise in the system under study we must add Langevin terms which take into account the randomness of the spontaneous emission events

$$\begin{cases} \Delta \dot{I}(t) = \frac{G_m I_0}{2V} \Delta N(t) + F_{\Delta I}(t) \\ \dot{\phi}(t) = \frac{G_m \alpha}{2V} \Delta N(t) + F_{\Delta \phi}(t) \\ \Delta \dot{N}(t) = -\gamma_c \Delta N(t) - G_0 \Delta I(t) + F_{\Delta N}(t) \end{cases}$$

$$F_{\Delta I}(t) = \sum_i (2I_0^{1/2} \cos \theta_i + 1) \delta(t - t_i)$$

$$F_{\Delta \phi}(t) = \sum_i I_0^{-1/2} \sin \theta_i \delta(t - t_i)$$

$$F_{\Delta N}(t) = -\sum_i \delta(t - t_i)$$

From the complete set of equations it is possible to evaluate the autocorrelation function of the variables $\phi, \Delta I, \Delta N$.

The Fourier transform of these functions gives the power spectral densities.

For instance when $G_I = 0$

$$\Downarrow$$

$$S_{\phi}(\Omega) = \frac{R_s}{2I_0} \left\{ \frac{\alpha^2 \Omega^4}{2I_0} \frac{(2I_0 + 1 + \frac{\Omega^2}{G_0^2})}{[(\Omega_k^2 - \Omega^2)^2 + \gamma_c^2 \Omega^2]} + 1 \right\}$$

At $\Omega = 0$ we have

$$S_{\phi}(0) = \frac{R_s}{2I_0} (1 + \alpha^2)$$



ITT laser

$$P = 4 \text{ mW}$$

$$\lambda = 865 \text{ nm}$$

$$I_0 = 4.5 \cdot 10^5$$

$$V = 2.2 \cdot 10^{-9} \text{ cm}^{-3}$$

$$R_s = 1.4 \cdot 10^{12} \text{ s}^{-1}$$

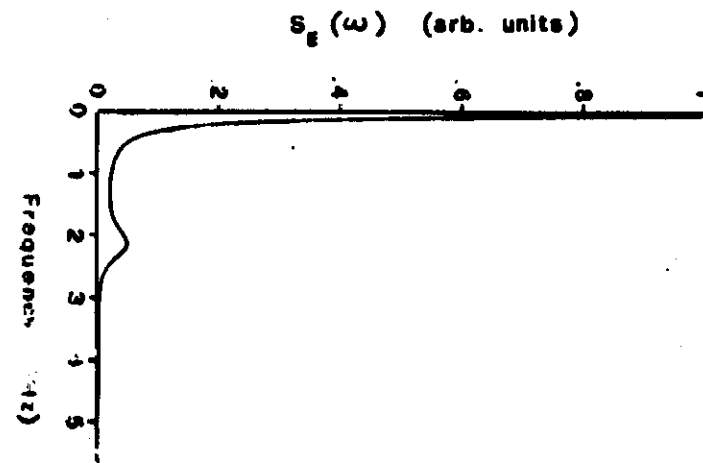
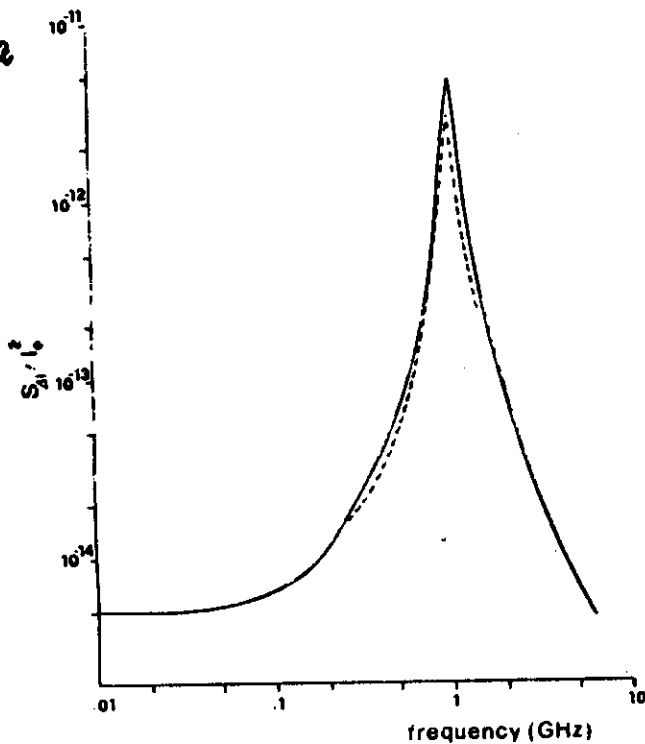
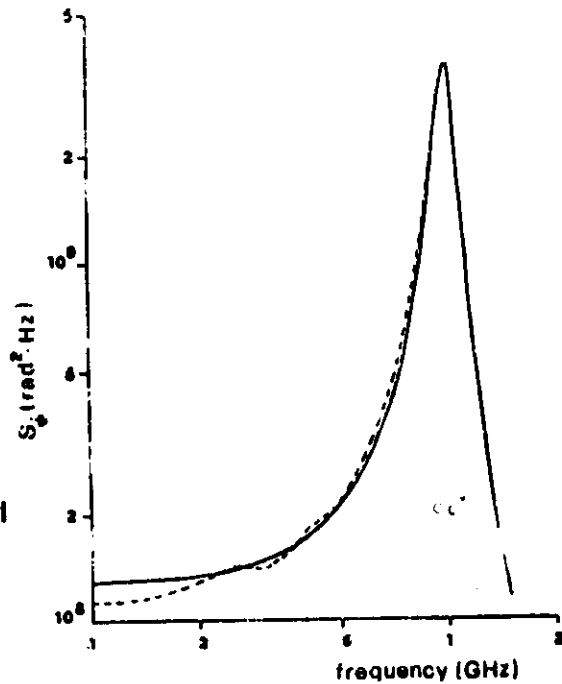
$$G_m = 8.3 \cdot 10^{-7} \text{ cm}^{-3} \text{ s}^{-1}$$

$$G_0 = 2.5 \cdot 10^{11} \text{ s}^{-1}$$

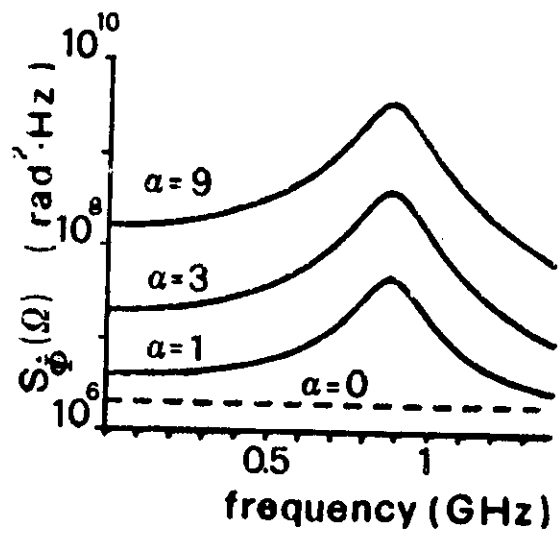
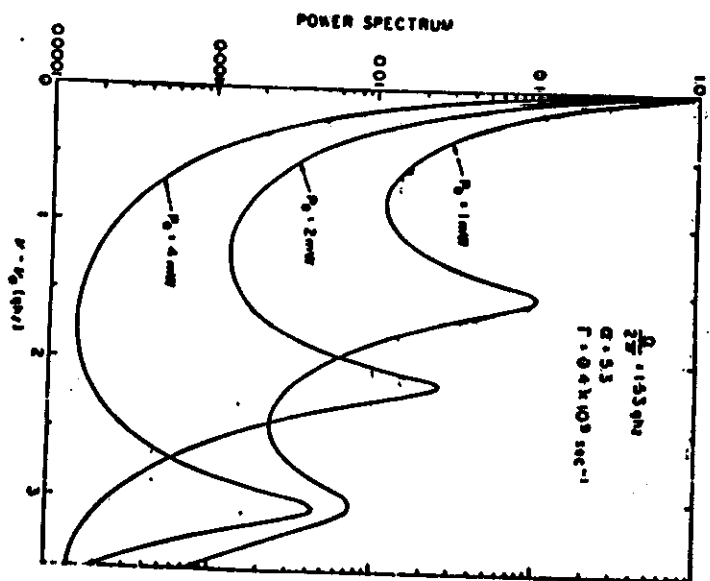
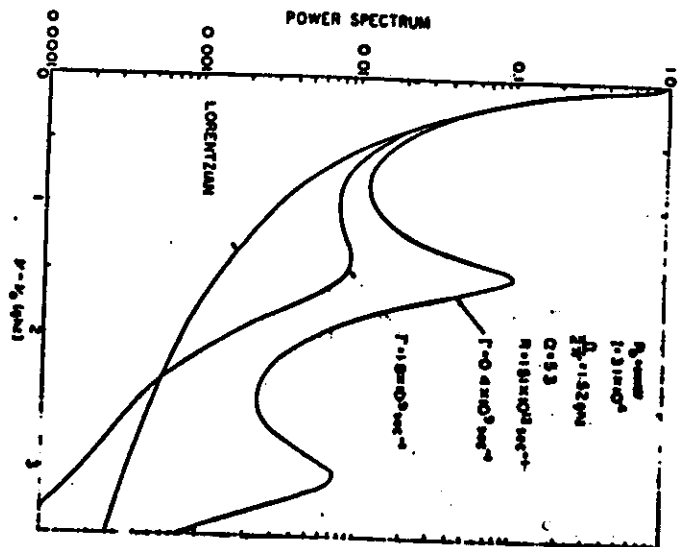
$$\gamma_e \approx 10^9 \text{ s}^{-1}$$

$$\alpha \approx 9$$

$$\nu_R = \frac{\Omega_R}{2\pi} = 1.02 \text{ GHz}$$

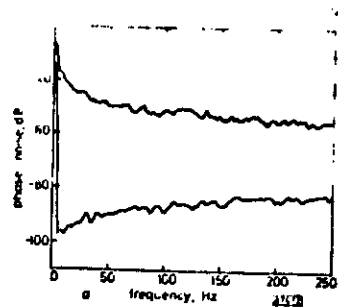
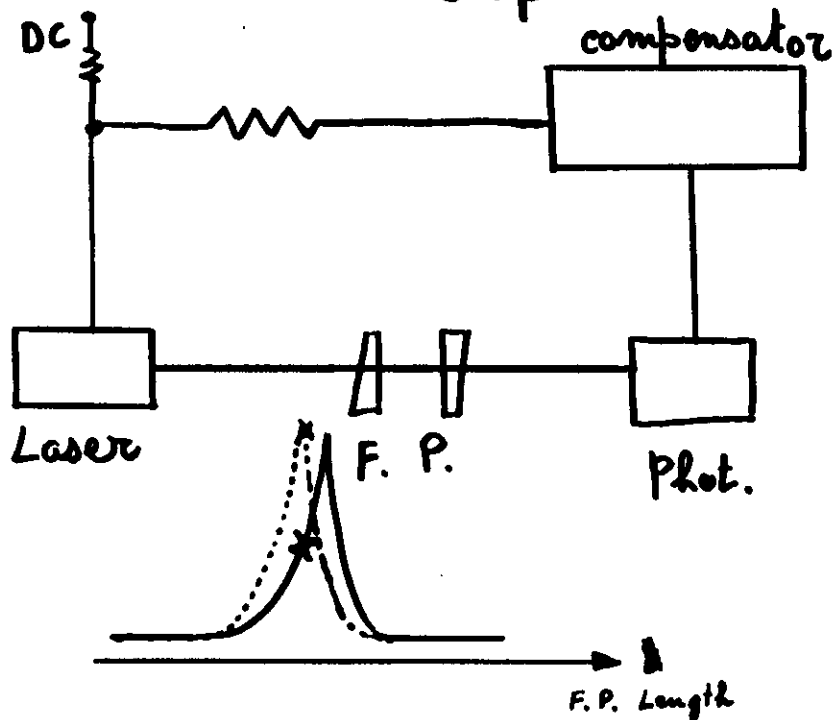


Laser Diode
P = 3 mW



Linewidth reduction

- 1) Electrical loop



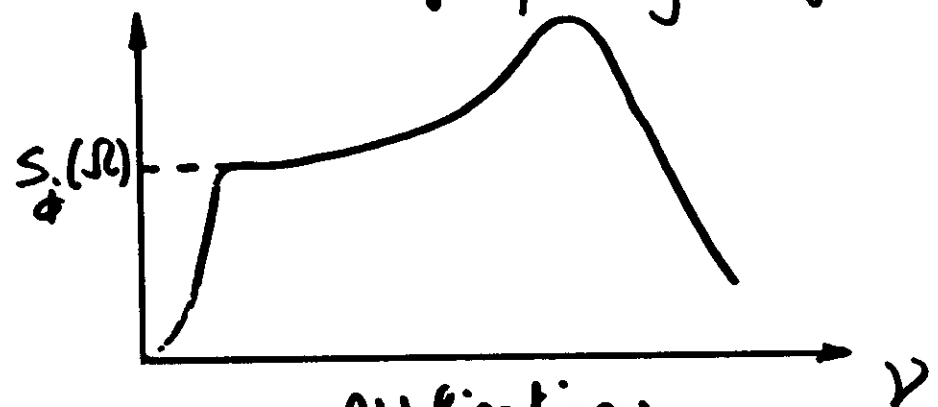
(Dandridge, Tsvetkov, Electron. Lett. 1981)

Advantages

- Good stability.
- High reduction of $S_{\phi}(\Omega)$.
- ~~easy~~ easy to make.

Disadvantages

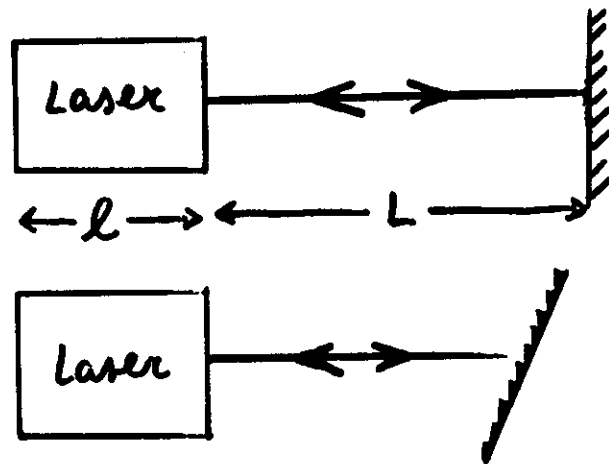
- Reduction of $S_{\phi}(\Omega)$ only in the low frequency region.



Applications

- Optical sensors

2) External Cavity

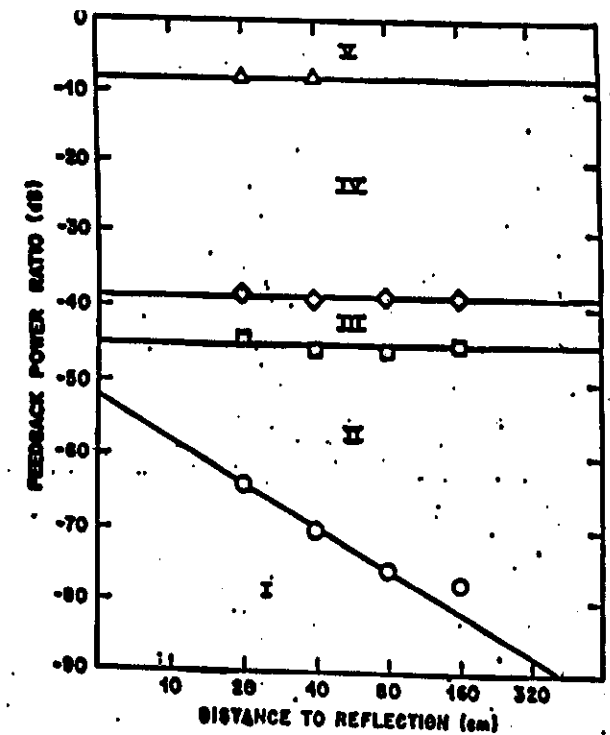
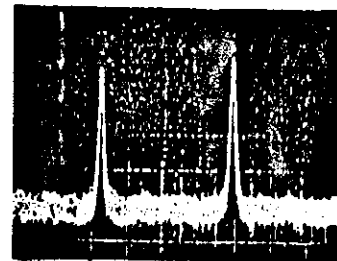
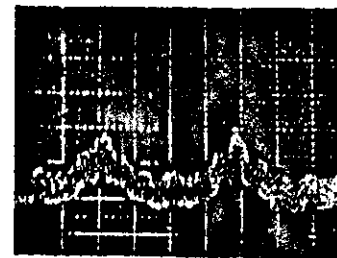
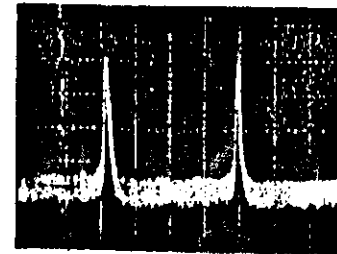
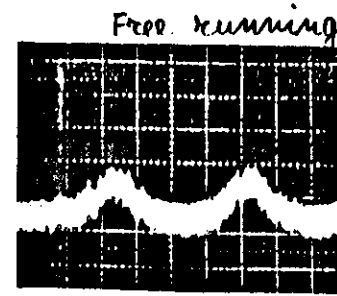


Mirror

Grating

2 cases

- Laser A.R. coated and strong feedback
- Laser without A.R. coating low feedback



- I) reduction or broadening of the emission linewidth depending on the phase of the reinjected field
- II) reduction of the linewidth or splitting in two lines
- III) reduction but with high sensitivity to external unwanted reflections
- IV) broadening of the linewidth
- V) very sensitive reduction of the linewidth

Laser A.R. coated, strong feedback
(Mooradian JQE, 1981; Matthews et al)
Electron. Lett. 85)

$$\frac{d}{dt} \left\{ E(t) e^{i\omega_0 t} \right\} = \left\{ i\omega_N(m) + \frac{1}{2} [G(m) - \Gamma_0] \right\} E(t) e^{i\omega_0 t} + K E(t - \tau) e^{i\omega_0(t - \tau)}$$

- Reduction of α of the order of
 $l / (l + L)$

$$\frac{d}{dt} n(t) = -\gamma n - G(n) |E(t)|^2 + P$$

Experimental results available
only for the linewidth value

$$\Delta \nu_L \approx 20 \text{ KHz (short term)}$$

$$150 \text{ MHz (long term)}$$

Advantages

- Very good short term linewidth

Disadvantages

- Mechanical complexity

- Mechanical and thermal noise

$$K = \frac{c}{2\eta l} (1 - R_2) \sqrt{\frac{R_3}{R_2}}$$

τ : round-trip time of the ext. cavity

Now, the stationary solution
($E(t) = E_0$) gives

$$\begin{cases} G(n_0) \equiv G_0 = \Gamma_0 - 2K \cos \omega_0 \tau \\ \omega_N(n_0) = \omega_0 + K \sin \omega_0 \tau \end{cases}$$

$\omega_0 \tau$: phase of the reinjected field

choosing the length of the external cavity in such a way that

$$|\Delta_z \phi(t)| = |\phi(t) - \phi(t-\tau)| \ll \pi/2$$

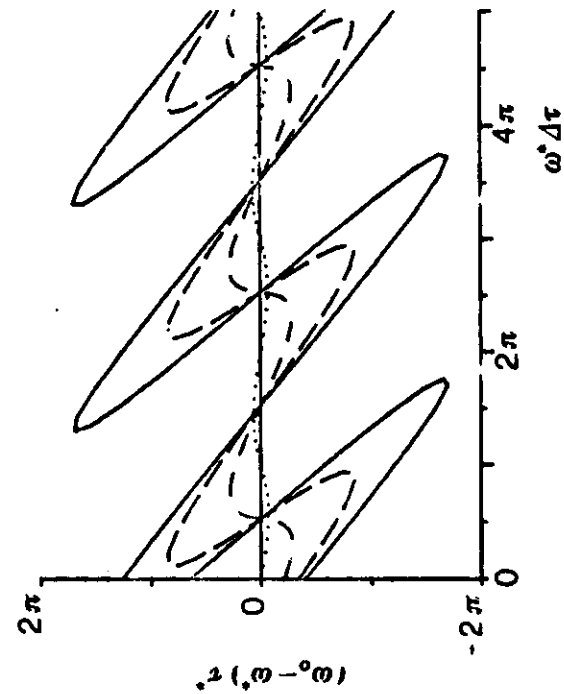
we have

$$\begin{cases} \Delta \dot{I}(t) = -2kI_0 \Delta_z \phi(t) \sin \Psi \\ \quad - k [\Delta I(t) - \Delta I(t-\tau)] \cos \Psi \\ \quad + (q_m I_0 / \phi_V) \Delta N(t) + F_{\Delta I}(t) \\ \dot{\phi}(t) = -k \Delta_z \phi(t) \cos \Psi + (\alpha q_m / 2 \phi_V) \Delta N(t) \\ \quad + \frac{k}{2I_0} [\Delta I(t) - \Delta I(t-\tau)] + F_{\Delta \phi}(t) \\ \Delta \dot{N}(t) = -\gamma_e \Delta N(t) - q_0 \Delta I(t) + F_{\Delta N}(t) \end{cases}$$

$$\Psi = \omega_0 \tau$$

$$\begin{array}{l} \kappa \tau = 0.1 \\ \kappa \tau = 0.2 \\ \kappa \tau = 0.4 \\ \alpha = 8.9 \end{array}$$

$$\begin{array}{l} \dots \kappa \tau = 0.3 \\ \alpha = 0 \end{array}$$



Two values of k

$$k_1 = [(\alpha^2 + 1)^{1/2} z]^{-1}$$

$$k_2 \cong \frac{3}{2} \pi k_1$$

can be found such that

- a) when $K < k_1$ the operating regime is strictly single-mode
- b) when $k_1 < K < k_2$ the laser can oscillate on a single mode or not depending on z
- c) when $K > k_2$ the regime is multimode whatever the value of z

Analysis of the results

The lineshape of a single mode injection laser is determined by the form of $S_{\phi}(\Omega)$. In particular, to determine the linewidth $S_{\phi}(0)$ is important. Were the lineshape Lorentzian

$$\Delta\nu = \frac{S_{\phi}(0)}{2\pi}$$

$$S_{\phi}(0) = \frac{R_s}{4I_0^2} \left\{ \frac{\alpha^2(2I_0+1) + 2I_0}{[1 + Kz(\cos\psi - \alpha\sin\psi)]} \right\}$$

$$|\psi = \omega_0 z|$$

The minimum of $S_{\phi}(0)$ is attained at the value

$$\psi_{\min} = -\tan^{-1}(\alpha)$$

$$\frac{3\pi}{2} \leq \psi_{\min} \leq 2\pi$$

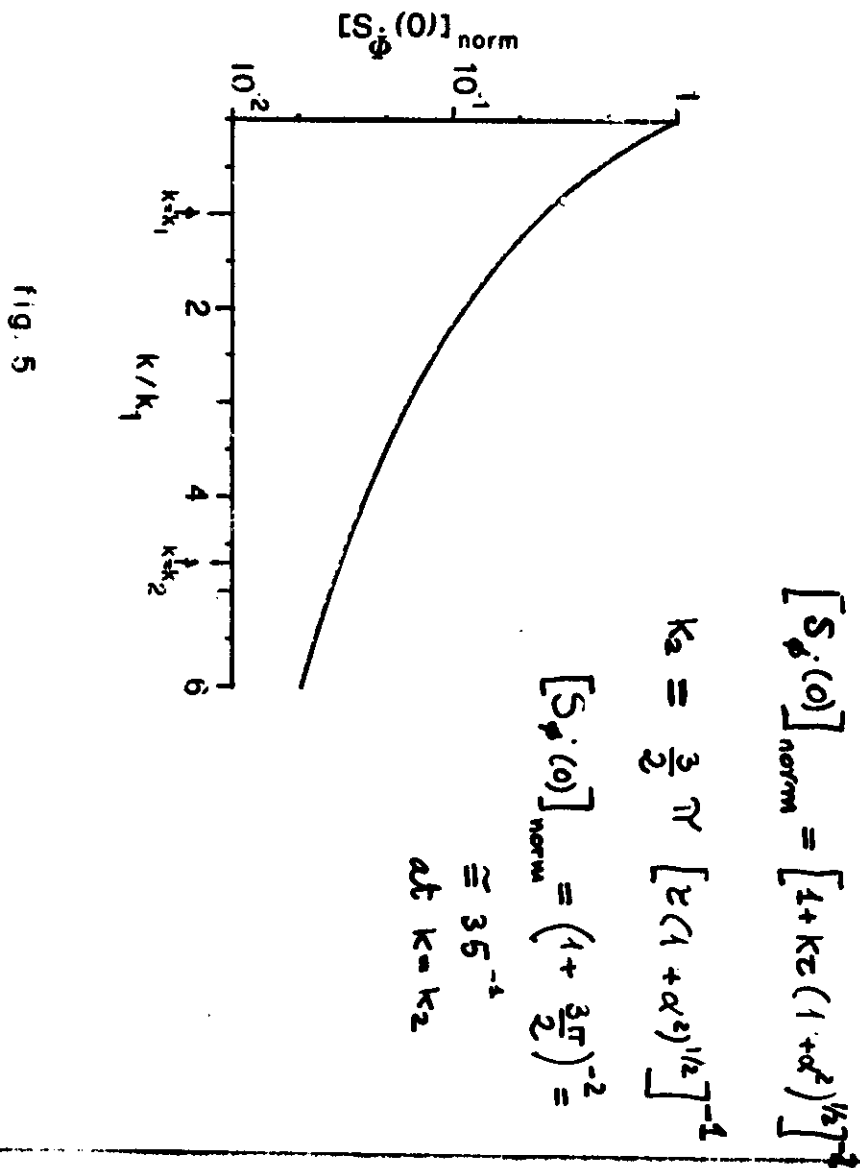
- Reduction of the quantity $S_{\phi}(0)$ depending on kz

- Maximum reduction of $S_{\phi}(0)$ in a single mode operation equal to

$[1 + 3\pi/2]^{-2}$ obtainable

a value $kz = \frac{3\pi}{2[\alpha^2 + 1]}$

- Shape of $S_{\phi}(\Omega)$ strongly dependent on z at the same value of kz



$$\psi = -fg^{-1} \left(\frac{\alpha}{a} \right)$$

- $\tau = 1.6 \nu_c^{-1}$
- $\tau = \nu_c^{-1}$
- $\tau = 0.5 \nu_c^{-1}$
- $\tau = 0.1 \nu_c^{-1}$

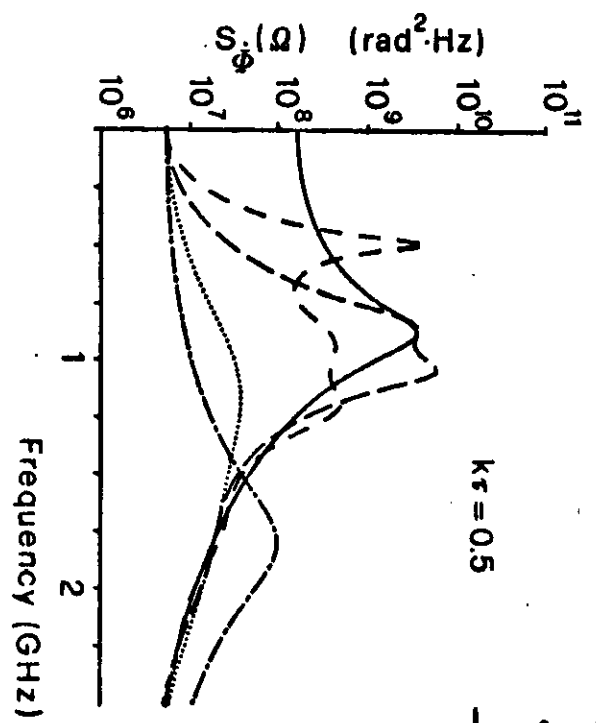
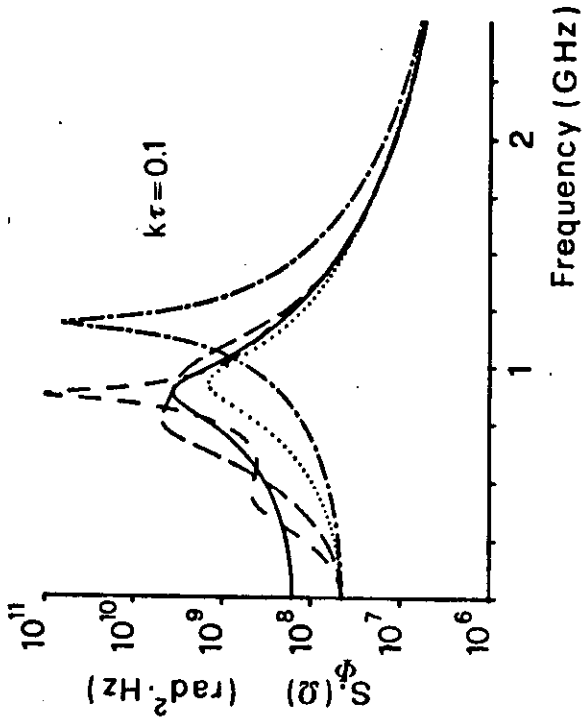


fig. 6b

fig. 6a



- $\tau = 1.6 \nu_c^{-1}$
- $\tau = \nu_c^{-1}$
- $\tau = 0.5 \nu_c^{-1}$
- $\tau = 0.1 \nu_c^{-1}$

$$\psi = -fg^{-1} \left(\frac{\alpha}{a} \right)$$

Advantages of the method Untill now we considered only the linewidth or equivalent quantities to characterize phase noise.

— Simplicity

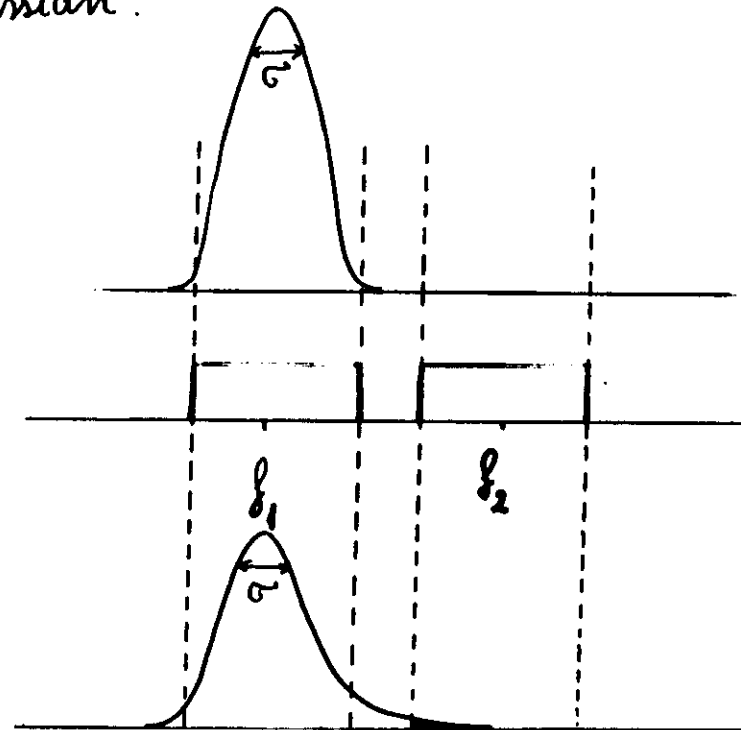
Disadvantages

— Noise Reduction too much sensitive to variations of the phase of the reinjected field

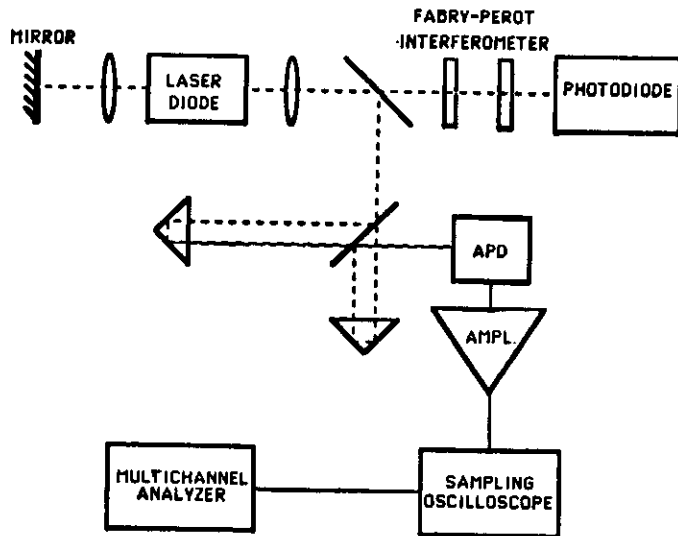


Mechanical and Thermal noise

In coherent optical systems and in other applications one usually assumes the statistics of phase noise to be Gaussian.



Experimental set up



If $\omega_c \tau = \frac{\pi}{2}$, $|\Delta_c \phi| \ll \pi$ and

$$\tau < \frac{1}{\Omega_{\max}}$$

$$\Delta_c \phi(t) = \int_{t-\tau/2}^{t+\tau/2} \dot{\phi}(t') dt' \approx \dot{\phi}(t) \tau$$

so that one can measure the statistical distribution of $\dot{\phi}(t)$ by measuring the statistical distribution of $\Delta_c \phi$.

