



H4.SMR. 405/18

SECOND WORKSHOP ON TELEMATICS

6 - 24 November 1989

**Single - Mode Fibre Transmissions:
Parameters - Components - Systems**

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These notes are intended for internal distribution only.

SINGLE-MODE FIBRE TRANSMISSIONS:

PARAMETERS - COMPONENTS - SYSTEMS

(R. CAPONI - CSELT - TORINO)



1) SINGLE-MODE FIBRE PARAMETERS:

- CUT-OFF WAVELENGTH
 - MODE FIELD DIAMETER
 - REFRACTIVE INDEX PROFILES
- } $\longleftrightarrow$ FIBRE DESIGN CONSIDERATIONS

2) FIBRE CABLING AND MEASUREMENTS:

- COUPLING LOSS, FIBRE ENDFACE PREPARATION, MAIN CABLE STRUCTURES, FIBRE CHARACTERIZATION

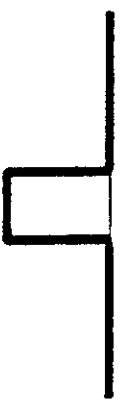
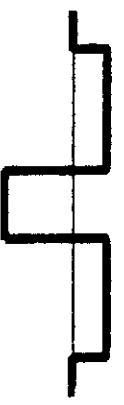
3) ACTIVE COMPONENTS FOR FIBRE TRANSMISSIONS:

- SOURCES
 - LEDs
 - LASERS
- DETECTORS

4) SYSTEM SCHEMES AND PROPERTIES:

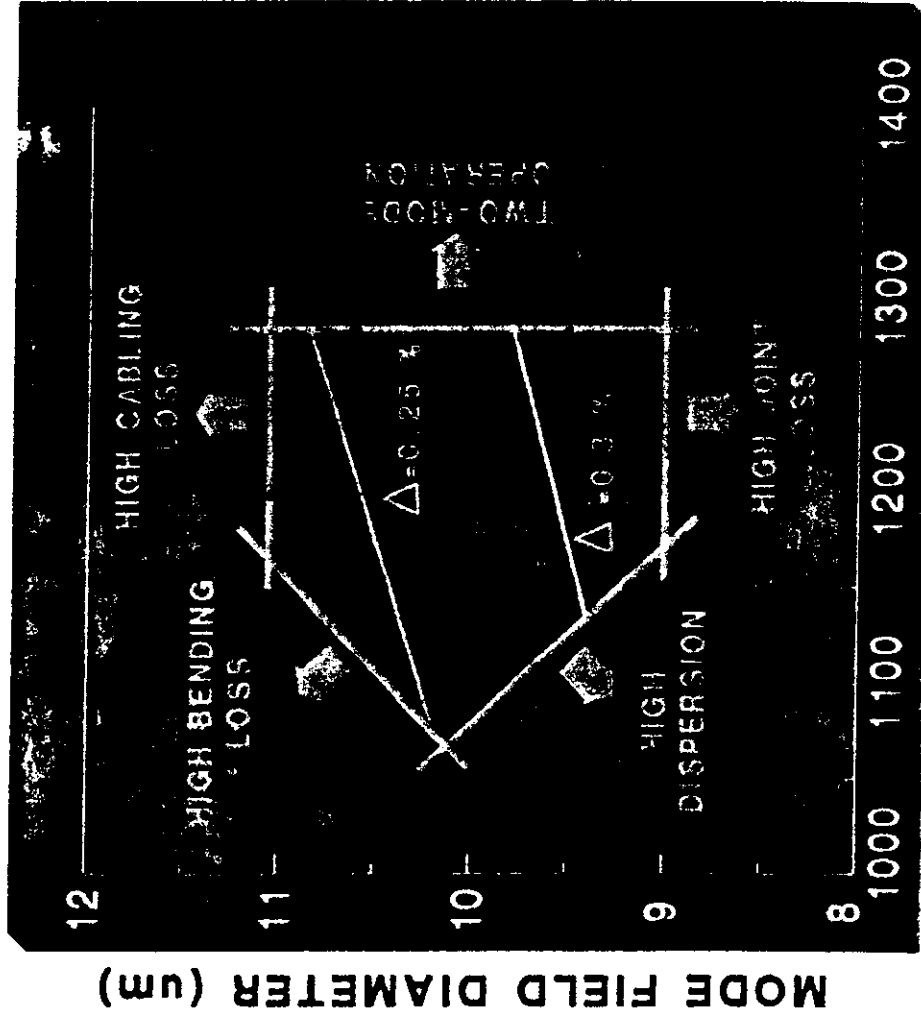
- DIRECT DETECTION SYSTEMS
 - COHERENT SYSTEMS
 - SYSTEM PERFORMANCE EVALUATION AND DEVELOPMENT
- } $\longleftrightarrow$ S/N RATIO

REFRACTIVE INDEX DESIGNS OF SINGLE-MODE FIBRES

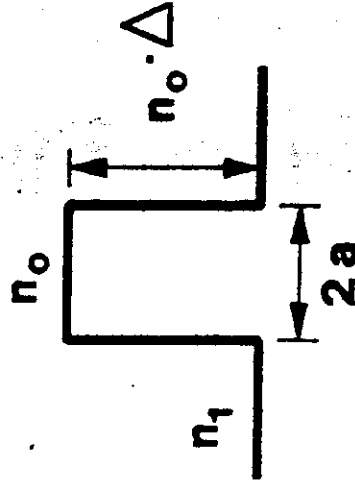
	MATCHED CLADDING	1300 nm OPTIMIZED
	DEPRESSED CLADDING	LOWER BEND LOSSES
	"W" TYPE	DISPERSION MODIFIED
	PURE SILICA CORE	MINIMUM ATTENUATION
	TRIANGULAR CORE	1550 nm OPTIMIZED
	SEGMENTED CORE	1550 nm OPTIMIZED LOWER BEND LOSSES
	QUADRUPLE CLADDING	DISPERSION FLATTENED

[— SIO₂ LEVEL]

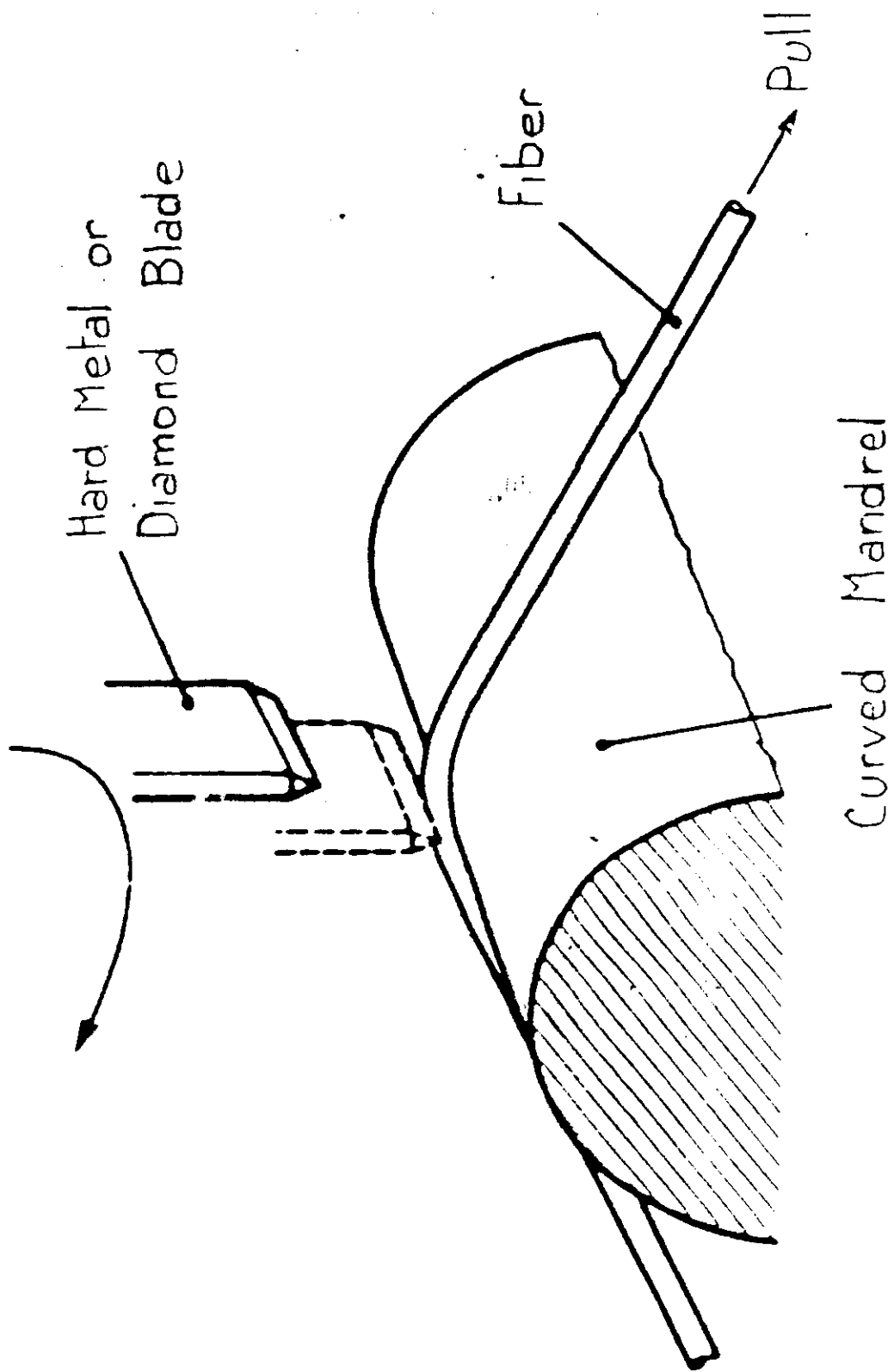
SINGLE-MODE FIBRE DESIGN



MATCHED CLADDING FIBRE:



CUT-OFF WAVELENGTH (nm)



SOURCES

LED

SPONTANEOUS EMISSION

UNIFORM RADIATION

WIDE SPECTRUM

LOW POWER INTO FIBRE

BAND LIMITATIONS

HIGH STABILITY

LONG LIFETIME

LOWER COST

LASER

(STIMULATED EMISSION)
↓
(THRESHOLD CURRENT)

DIRECTIONAL EMISSION

NARROW SPECTRUM

HIGH POWER INTO FIBRE

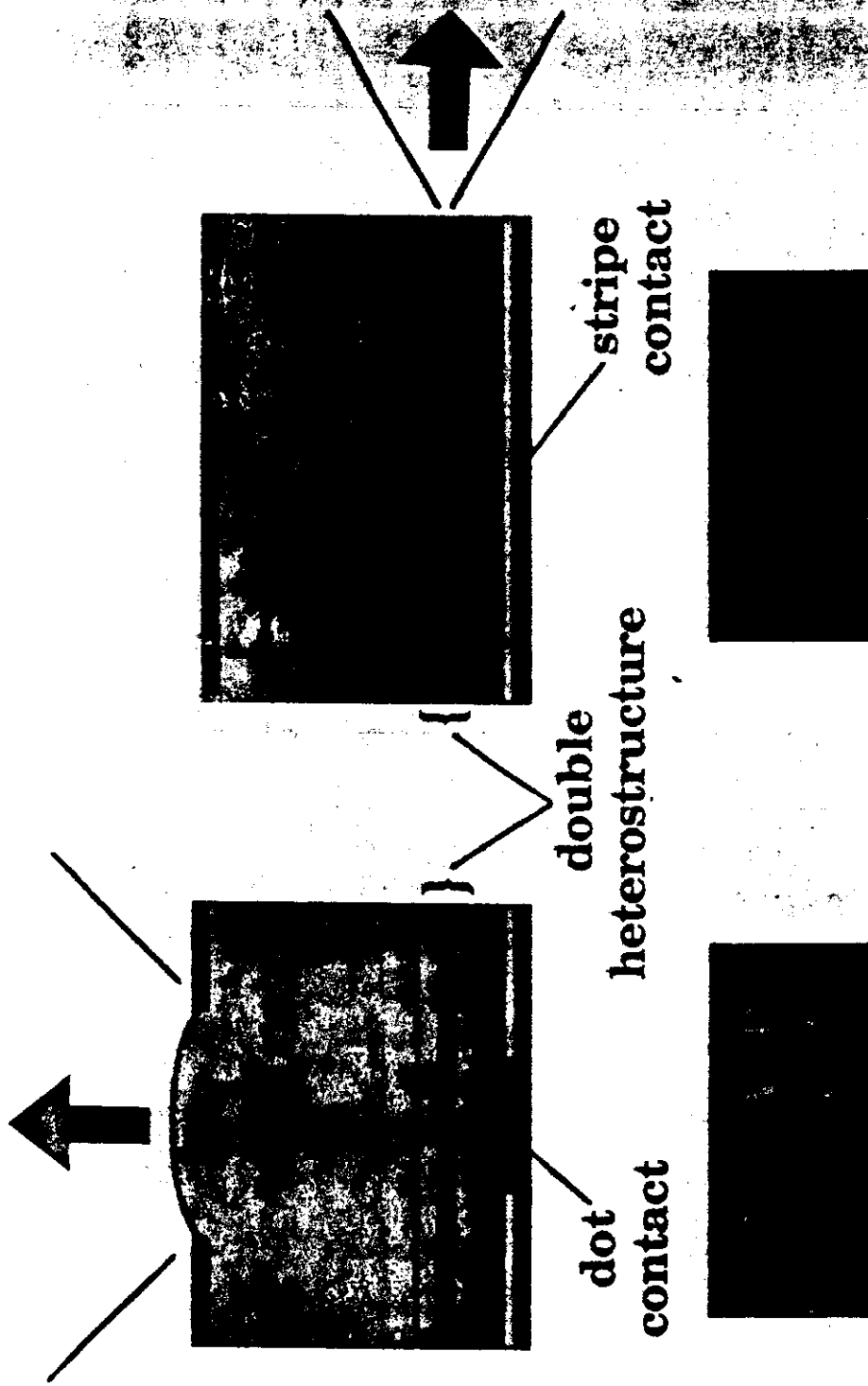
WIDEBAND

TEMPERATURE VARIATIONS

SHORTER LIFETIME

HIGHER COST

LIGHT EMITTING DIODE (LED)



to increase coupling efficiency:

- monolithic lens

to prevent from lasing:

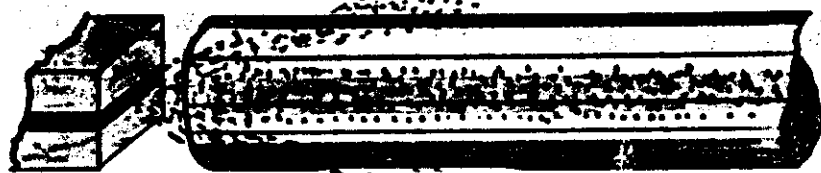
- AR coated facets
- truncated stripe
- thin active layer

Both AlGaAs/GaAs and InGaAsP/InP are used

LASER DIODE



- Double heterostructure, stripe geometry
- Cleaved mirrors (Fabry-Perot resonator)
- AlGaAs/GaAs for 0.85 μm operation
InGaAsP/InP for 1.3 - 1.55 μm operation
- Epitaxial growth: LPE, MO-CVD, MBE, ...



$$W_e = W_o + W_i$$

EMITTED POWER $\longrightarrow$ GUIDED POWER + RADIATED (LOST) POWER

* LAUNCHING EFFICIENCY: $\Lambda = W_o / W_e$ (% typ.)

* COUPLING LOSS: $L = W_i / W_e$ (dB typ.)

SINGLE-MODE FIBRES:

$I_e(r)$ - Emitted power radial distribution

Λ DEPENDS ON THE "LIKENESS" OF $I_e(r)$ AND $I(r)$

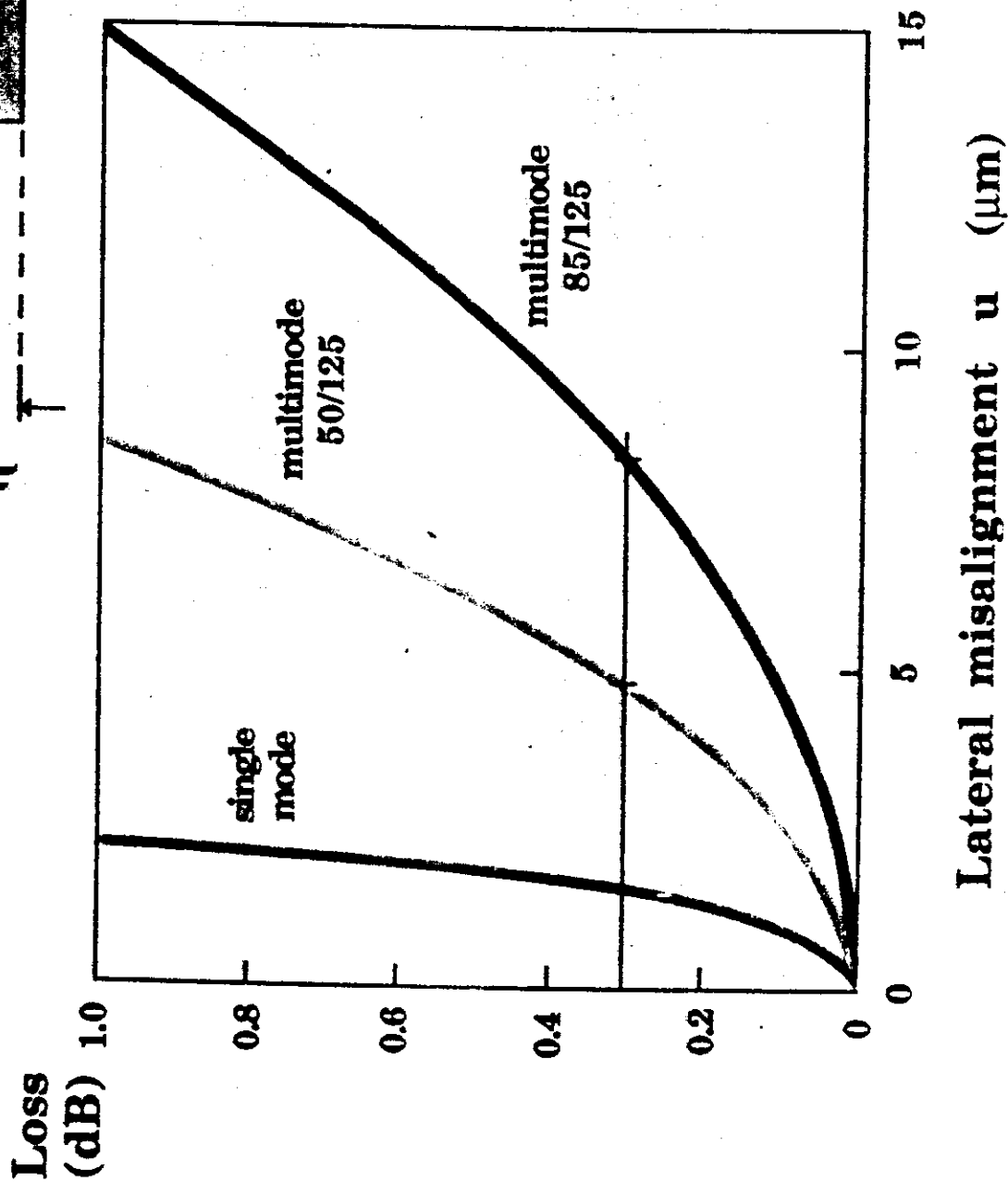
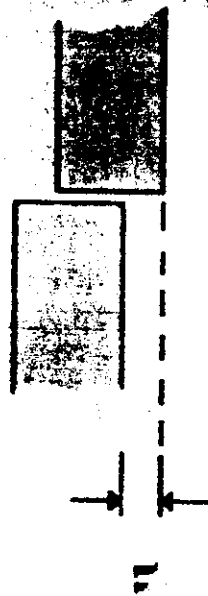
$\Lambda = [\text{Overlap integral between } I_e \text{ and } I]$

* TYPICAL Λ -VALUES FOR INT. LASER-FIBRE COUPLING:

~20% from multimode laser

~80% from single-mode laser

COUPLING LOSS DUE TO LATERAL MISALIGNMENT



DETECTORS

PIN PHOTODIODES

HIGH STABILITY

LOW BIAS VOLTAGE

LOW COST

AVALANCHE PHOTODIODES (APDs)

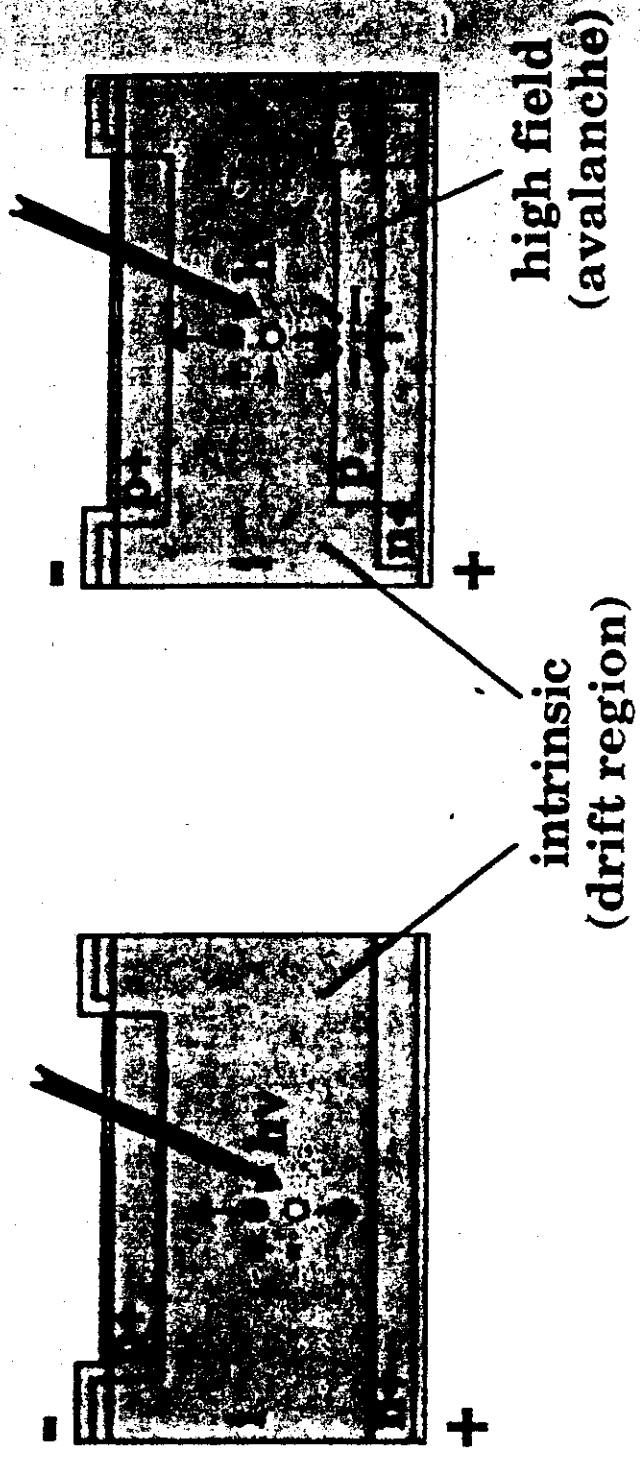
AVALANCHE GAIN

LOWER STABILITY

HIGH BIAS VOLTAGE

HIGHER COST

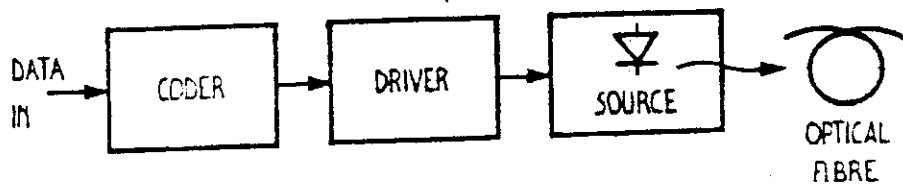
PHOTODETECTORS



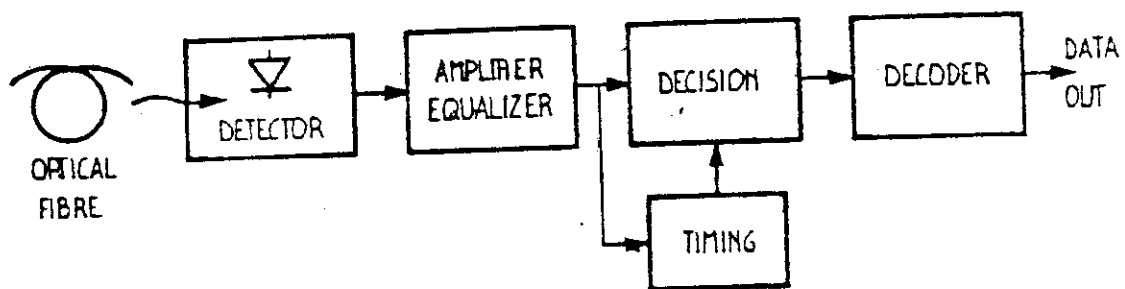
Material:

- | | | |
|-------------|--------|--------------------|
| • Silicon | up to: | ~1 μm |
| • Germanium | " | ~1.5 μm |
| • InGaAs | " | ~1.6 μm |

OPTICAL SYSTEM BLOCK DIAGRAM



TRANSMITTER



RECEIVER

REPEATER SPACING DETERMINATION

OPTICAL POWER INTO FIBRE

$$P_o = 20 \div 100 \mu W \text{ for LED's}$$

$$P_o = 0.3 \div 2 mW \text{ for LASER's}$$

RECEIVER SENSITIVITY

$$\text{Signal peak current: } I_p = 2 q G P_r$$

Noise currents:

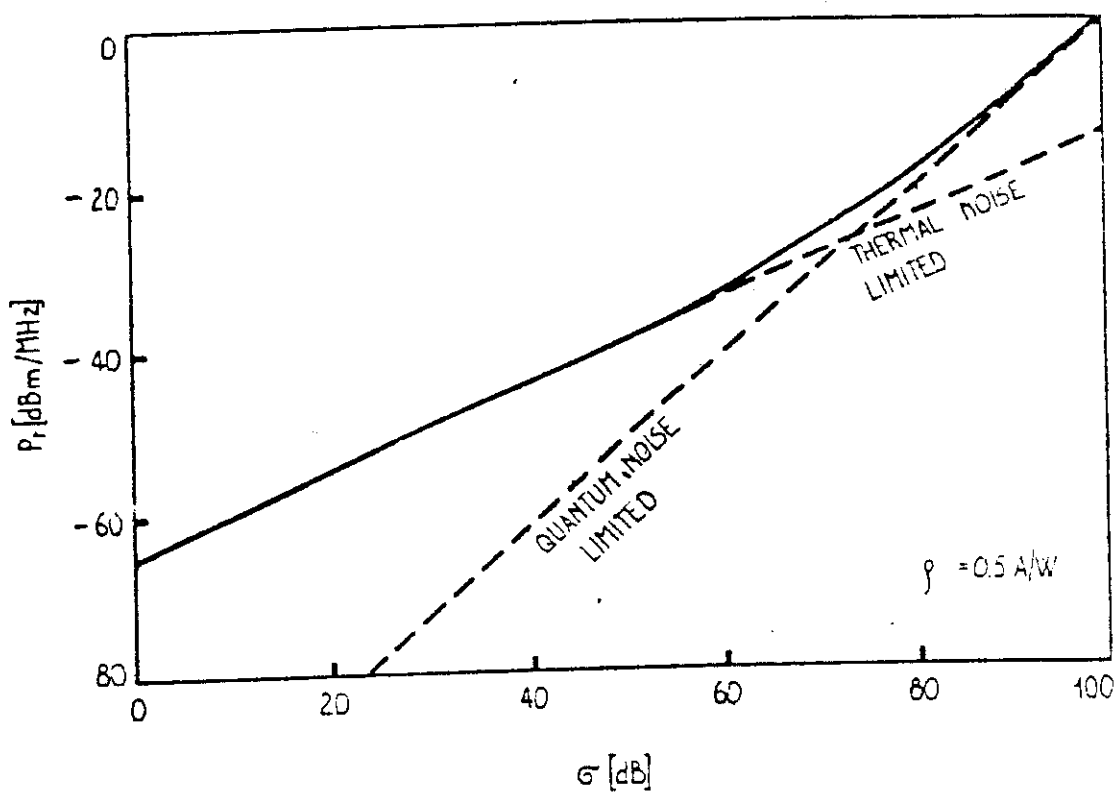
$$\text{thermal: } I_{tn}^2 = \frac{4KTBF}{R}$$

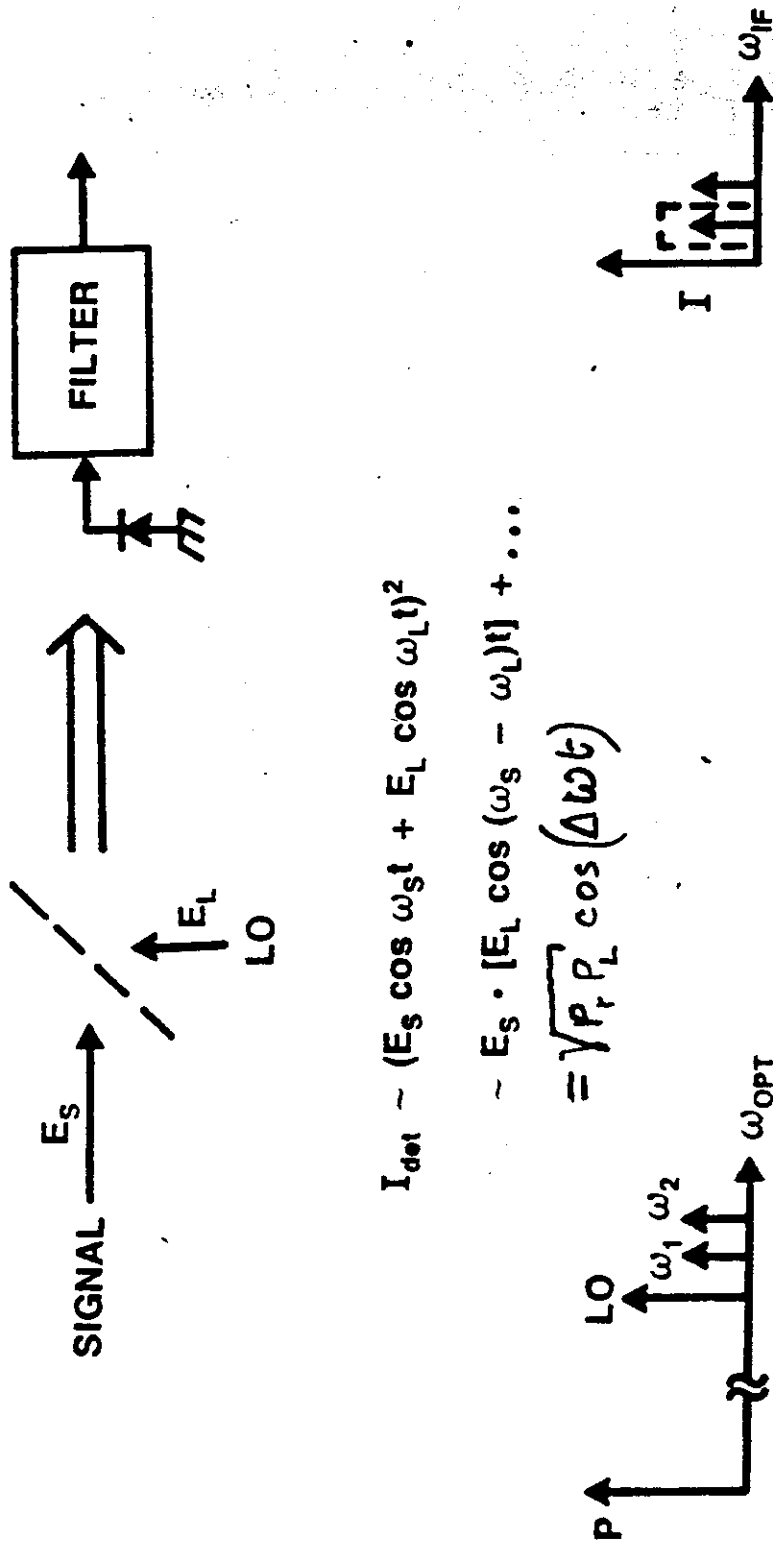
$$\text{quantum: } I_{qn}^2 = 2q^2 G^2 F_G B P_r$$

S/N ratio:

$$\sigma = \frac{2qGP_r}{\sqrt{2q^2G^2F_GB P_r + 4KTBF/R}}$$

$P_r(\sigma)$ FOR A PIN DETECTOR

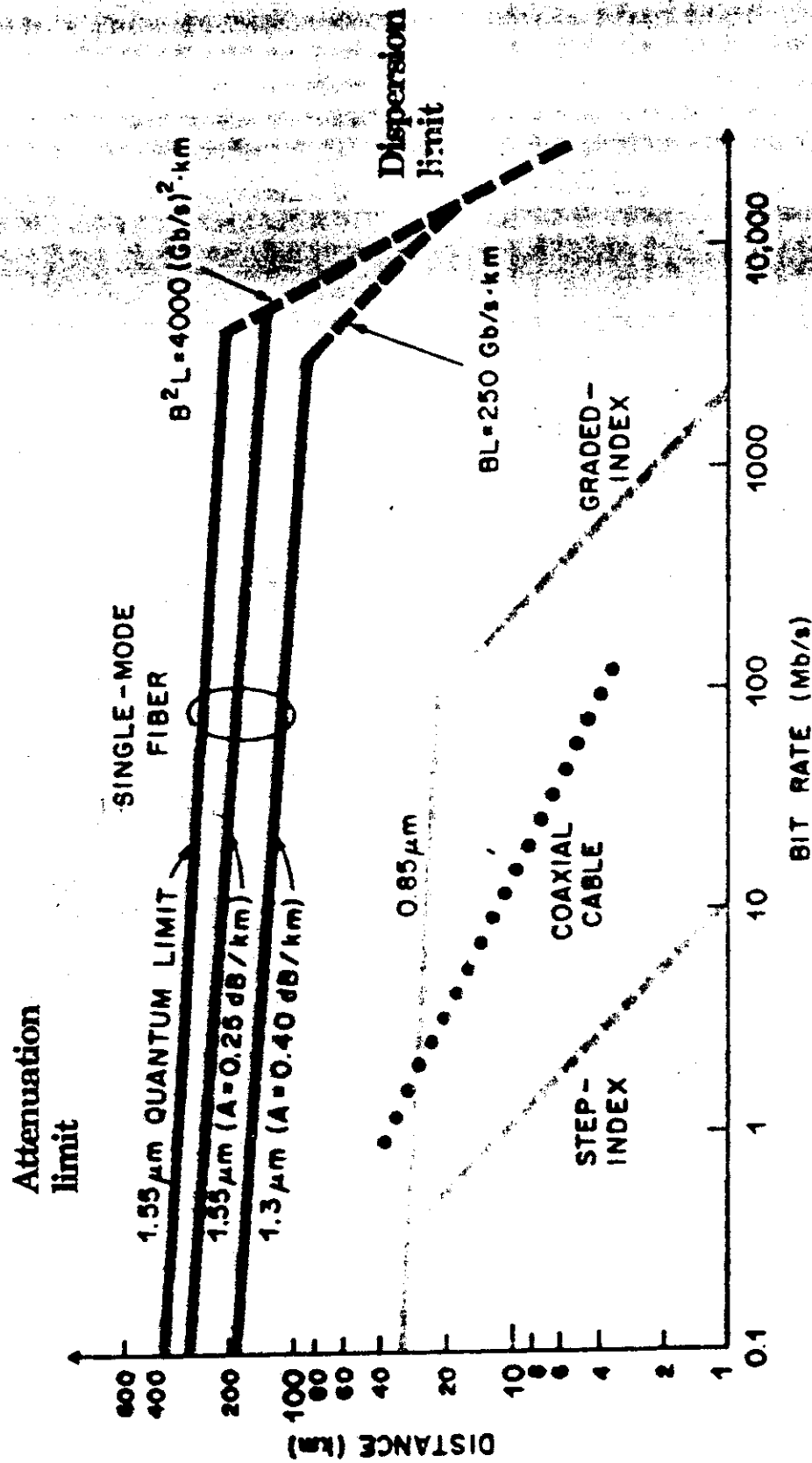




$$\begin{aligned}
 I_{det} &\sim (E_s \cos \omega_s t + E_L \cos \omega_L t)^2 \\
 &\sim E_s \cdot [E_L \cos (\omega_s - \omega_L)t] + \dots \\
 &= \sqrt{P_r P_L} \cos(\Delta \omega t)
 \end{aligned}$$

- SEPARATING ω_1 and ω_2 AT OPTICAL FREQUENCIES REQUIRES $\sim 0.1 \text{ \AA}$ RESOLUTION;
- SAME TASK AT I-F REQUIRES $\sim 1 \text{ GHz}$ FILTER

REPEATER SPACING VS. BIT RATE



LIGHTWAVE PROGRESS

