



INTERNATIONAL ATOMIC ENERGY AGENCY  
UNITED NATIONS EDUCATIONAL, SCIENTIFIC AND CULTURAL ORGANIZATION  
**INTERNATIONAL CENTRE FOR THEORETICAL PHYSICS**  
I.C.T.P., P.O. BOX 586, 34100 TRIESTE, ITALY, CABLE: CENTRATOM TRIESTE



**H4.SMR/452-60**

**ADRIATICO CONFERENCE ON  
FOURIER OPTICS AND  
HOLOGRAPHY**

**6 - 9 March 1990**

***INTRODUCTION TO LASERS***

**Prof. A. Sona**

**CISE**

**Milan, Italy**

## ■ Introduction to Laser operation

- Rate Equations Description
- Active materials
- Pulsed emission

## ■ Coherence properties of the laser

- Temporal Coherence
- Single Longitudinal Mode Selection
- Spatial Coherence
- Single transverse mode selection

## ■ Applications Requirements

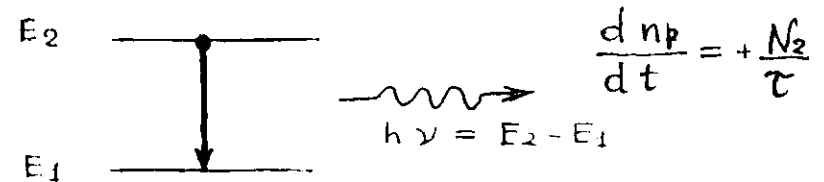
- Interferometry
- Holography
- Optical Computers

## ■ Bibliography:

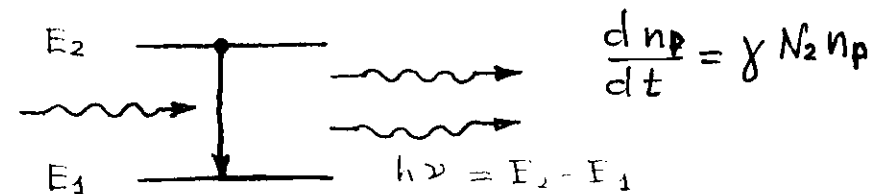
|| O. Svelto "Principles of Lasers" ||  
Plenum Press 1989

R - N INTERACTION  
PROCESSES AFFECTING LASER  
OPERATION

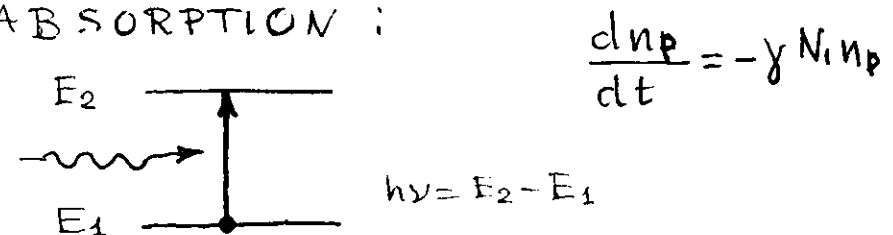
## - SPONTANEOUS EMISSION:



## - STIMULATED EMISSION:



## - ABSORPTION:



$N_2$  - Number of Atoms in the upper level [ $\text{cm}^{-3}$ ]

$N_1$  - Number of Atoms in the Lower Level [ $\text{cm}^{-3}$ ]

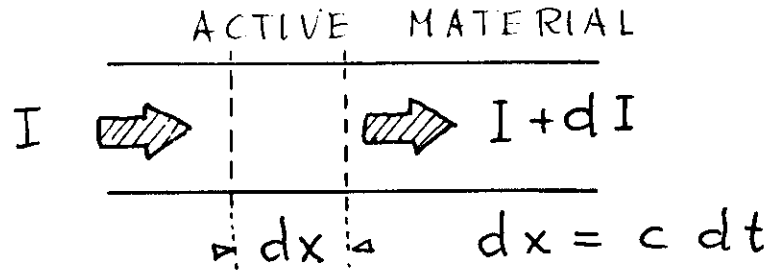
If  $N_2 > N_1$  STIMULATED EMISSION IS LARGER THAN ABSORPTION

$n_p$  - Photons density [ $\text{cm}^{-3}$ ];  $\gamma = \sigma c$

$$\frac{dn_p}{dt} = \gamma n_p (N_2 - N_1) + N_2/\tau$$

# • PHOTONS BALANCE EQUATION

$$\frac{dn_p}{dt} = \sigma c n_p (N_2 - N_1) + N_2/\tau$$



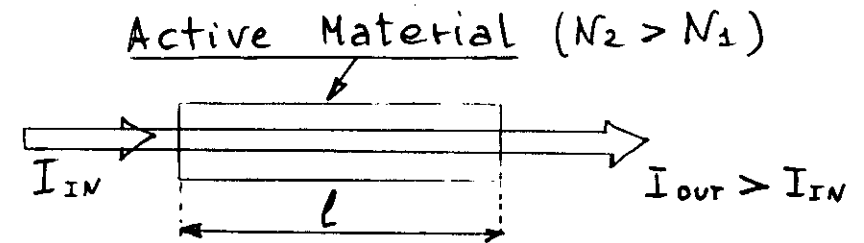
$$I = A h\nu c n_p \quad A - \text{beam cross section}$$

$$\begin{aligned} \frac{dI}{dx} &= A h\nu c \frac{dn_p}{dx} = A h\nu \frac{dn_p}{dt} = \\ &= A h\nu \sigma c (N_2 - N_1) n_p = \\ &= I \sigma (N_2 - N_1) = \alpha_0 I \end{aligned}$$

$$\boxed{\frac{dI}{dx} = \alpha_0 I \Rightarrow I = I_0 e^{\alpha_0 l}}$$

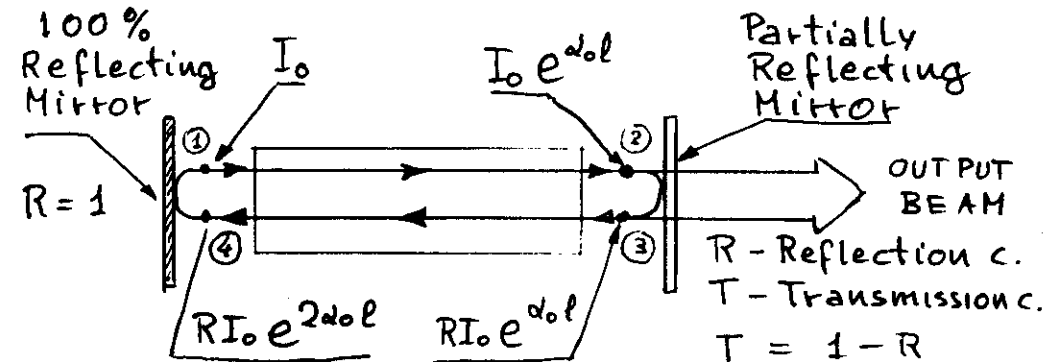
- $\alpha_0 [\text{cm}^{-1}] = \sigma (N_2 - N_1)$  small signal gain
- $\sigma [\text{cm}^2]$  interaction cross section

# — LASER AMPLIFIER:



$$\begin{aligned} I_{OUT} &= I_{IN} e^{\alpha_0 l} & \alpha_0 &= \sigma (N_2 - N_1) \\ I_{OUT} &= I_{IN} G & G &= e^{\alpha_0 l} \end{aligned}$$

# — LASER OSCILLATOR



If  $I_0 e^{2\alpha_0 l} \cdot R \geq I_0$  OSCILLATION STARTS

This means  $2\alpha_0 l \geq \ln 1/R = \ln 1/(1-T)$

and, for  $T \ll 1 \Rightarrow 2\alpha_0 l \geq T$  or  $G^2 \geq T$

The amplification in the active medium compensate for the output coupling losses in a round trip.

● THRESHOLD CONDITION (AMPLITUDE)

$$2\sigma(N_2 - N_1)l \geq T \quad \text{hence:} \quad T^4$$

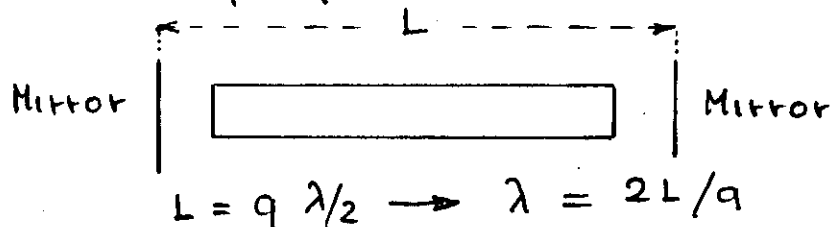
$$N_2 - N_1 \geq T/2\sigma$$

(Threshold inversion)

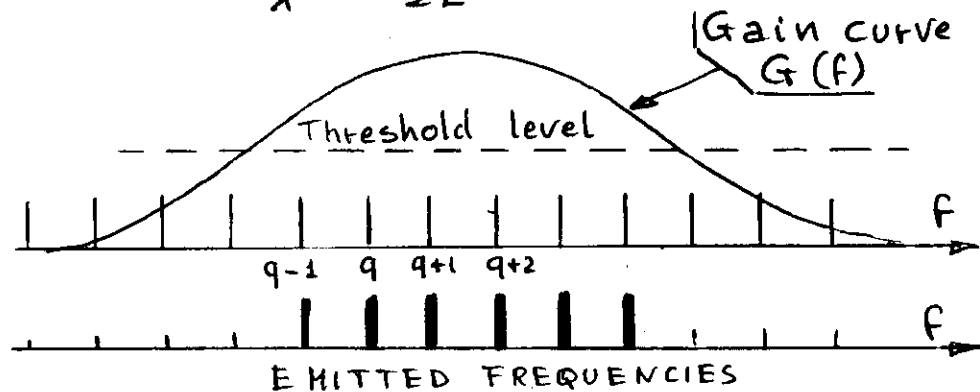
"Pumping" is required to reach the above condition as, in equilibrium,  $N_2 < N_1$  according to Boltzman eq.  $N_2/N_1 = \exp(-\frac{E_2 - E_1}{KT})$

● POS. FEEDBACK CONDITION (PHASE)

The following phase condition has to be fulfilled for oscillation



$$f = \frac{c}{\lambda} = \frac{c}{2L} \cdot q; \quad \Delta f_{q+1, q} = \frac{c}{2L}$$

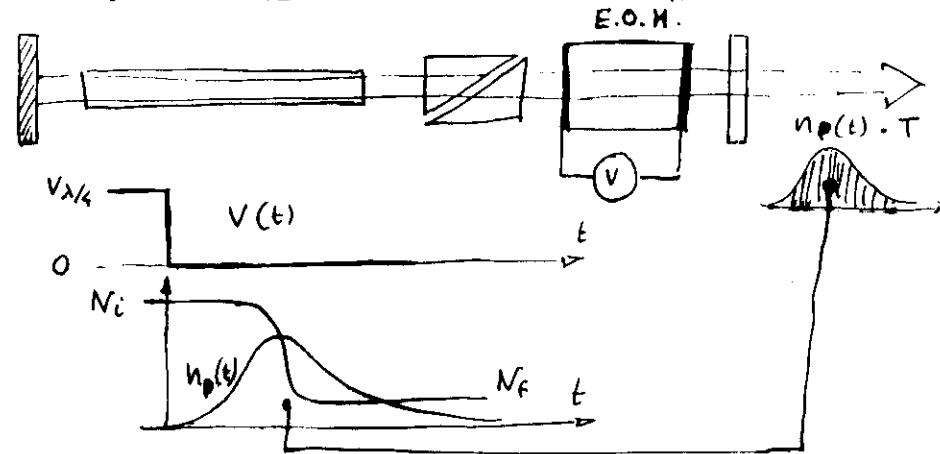


(Ex: for  $L = 0.5m$   $\Delta f = 300 \text{ MHz}$ )

$R = 100\%$

Q-SWITCHING

$R + T = 1$



PULSE TRANSMISSION MODE (CAVITY DUMPING)

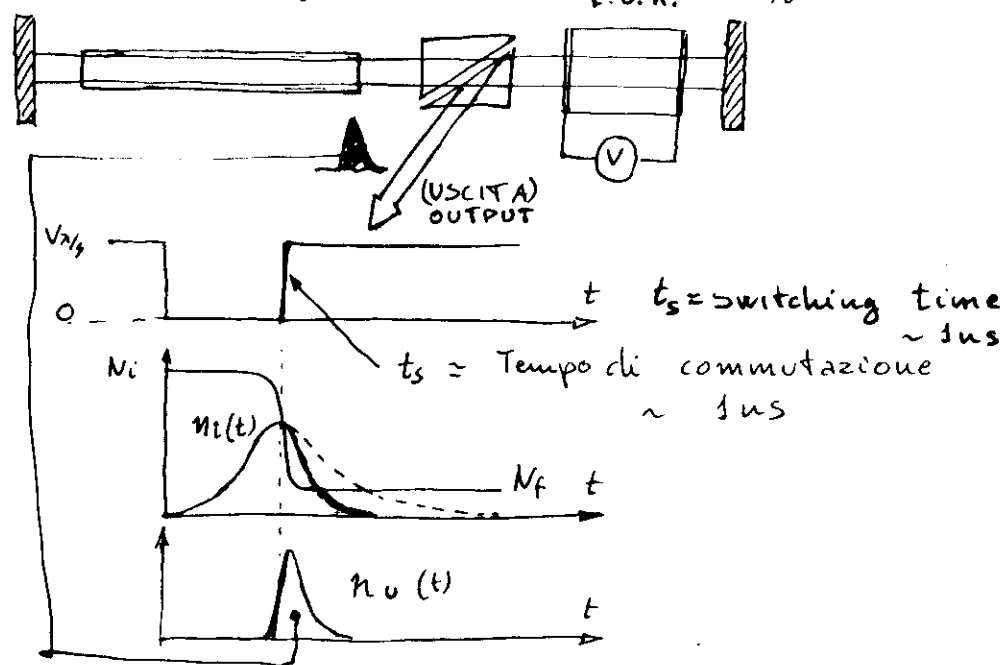
100 %

(P.T.M.)

E.O.M.

100 %

DUMPING)



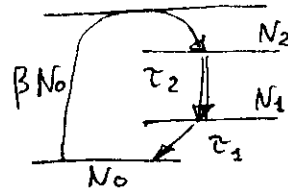
## Q-switching - 4 Levels Laser

Putting:  $N = N_2 - N_1$  (for  $\tau_1 \ll \tau_2$   $N_1 = 0$ )

•  $\tau = \tau_2$  decay time for atoms

•  $T = \frac{2L}{c} \frac{1}{1-R}$  decay time of photons

•  $\beta N_0$  pump term



■ Rate equations:

$$\begin{cases} \frac{dN}{dt} = \beta N_0 - \gamma n_p N - N/\tau \\ \frac{dn_p}{dt} = -\frac{n_p}{T} + \gamma n_p N \end{cases}$$

Not relevant during laser emission; important as a source term

■ Before switching  $\dot{N} = 0$   $n_p = 0$   $N_i = \beta N_0 \tau$

During the transient  $N/\tau$  &  $\beta N_0$  can be neglected

$$\begin{cases} \frac{dN}{dt} = -\gamma n_p N \\ \frac{dn_p}{dt} = -\frac{n_p}{T} + \gamma n_p N \end{cases} \quad \begin{cases} \text{for } \dot{n}_p = 0 \text{ at } N = N_s = \frac{1}{\gamma T} \\ \text{corresponding to } \eta = 1 \\ n_p \text{ reaches its maximum} \end{cases}$$

■ The pulse energy is given by:

$$E = \frac{1}{T} \int_0^\infty n_p dt = \int_0^\infty -\frac{dn_p}{dt} dt - \int_0^\infty \frac{dN}{dt} dt$$

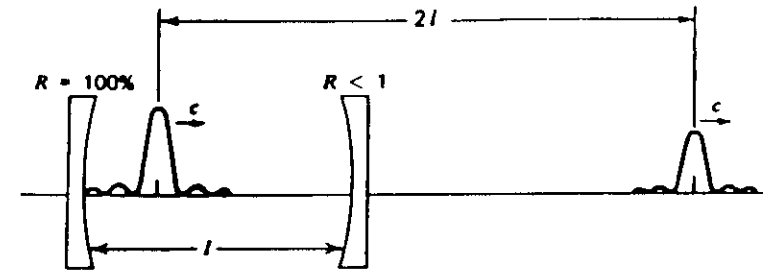
If  $n_p = 0$  for  $t=0$   $n_p \text{ final} = 0$  the first integral vanishes and the energy is

$$E = N_{\text{initial}} - N_{\text{final}} \text{ (energy conservation)}$$

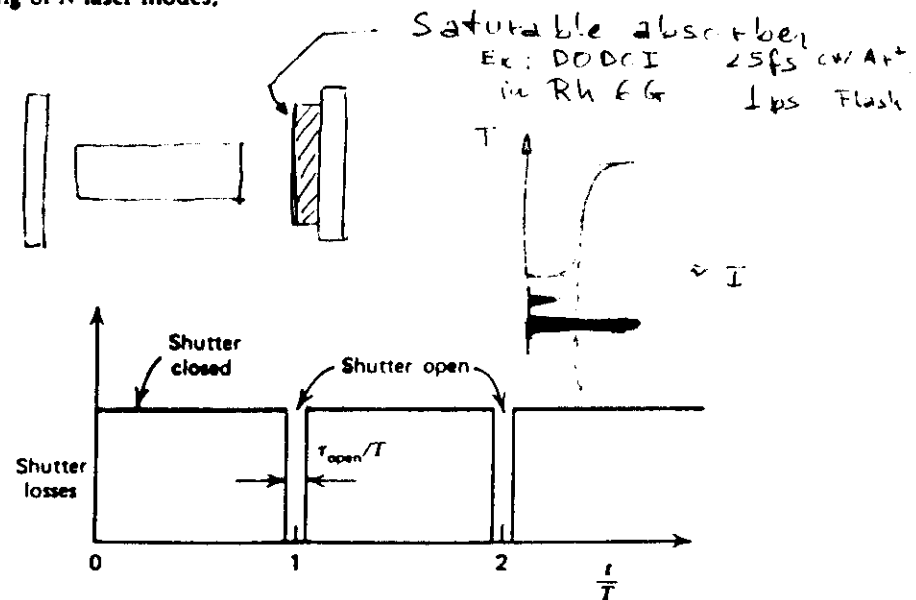
■ By integrating the two equations the value of  $N_{\text{final}}$  can be derived. The energy stored in the active medium will be converted into laser energy with an efficiency

(utilization efficiency)  $\eta_u = \frac{N_{\text{initial}} - N_{\text{final}}}{N_{\text{initial}}}$

## Mode Locking



Traveling pulse of energy resulting from the mode locking of  $N$  laser modes.



Periodic losses introduced by a shutter to induce mode locking. The presence of these losses favors the choice of mode phases that results in a pulse passing through the shutter during open intervals—that is, mode locking.

La struttura dei modi si adatta all'evoluzione delle perdite nel risonatore.

## Mode Locking - $N$ modes!

The set of phase-locked modes can be described by:

$$E(t) = \sum_n E_n e^{j[(\omega_0 + n\omega)t + \phi_n]} \quad (1)$$

where:  $\omega_0 = 2\pi\nu_0$  and  $\nu_0$  is the central mode frequency  
 $\omega = 2\pi c/2L$ ;  $c/2L$  frequency difference between two adjacent modes;  $\phi_n$  phase of the  $n$ th mode.

If  $\phi_n = 0$  (phased modes)  $E_n = \text{const} = E_0$

$$E(t) = E_0 \sum_{-(N-1)/2}^{+(N-1)/2} e^{j(\omega_0 + n\omega)t} = E_0 \frac{\sin(N\omega t/2)}{\sin(\omega t/2)} e^{j\omega_0 t}$$

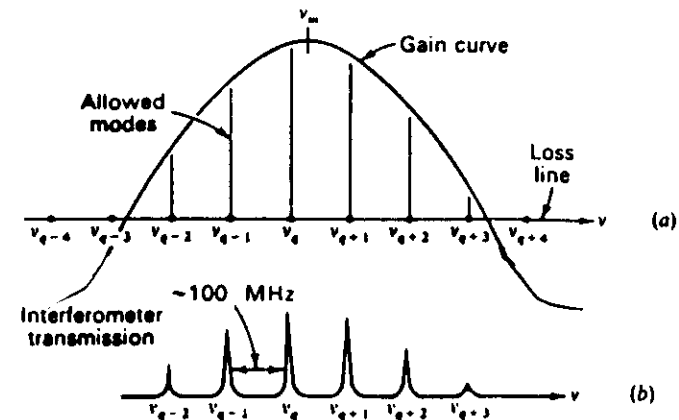
The laser output power is proportional to:

$$P(t) \equiv E(t)E^*(t) = E_0^2 \frac{\sin^2(N\omega t/2)}{\sin^2(\omega t/2)}$$

- The emission consists of a periodic pulse train with period  $T = 2L/c$
- The peak power is  $N$  times the average power  
 $P_{\text{peak}} = N^2 E_0^2$        $P_{\text{ave}} = N E_0^2$
- The peak electric field is  $N$  times the field of the individual mode
- The pulse duration (peak-first zero) is  $\tau = T/N \cdot 0.886$
- The number of modes is  $N \approx \Delta\nu / c/2L$

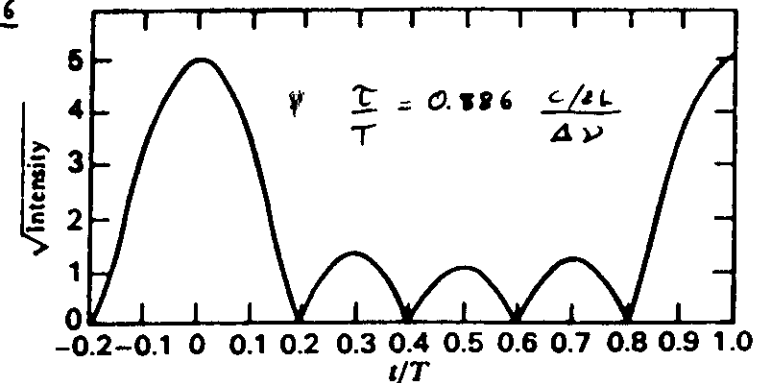
| LASER                  | He-Ne                | Nd:YAG                | Ruby                  | Nd:Glass              | Rh 6G         |
|------------------------|----------------------|-----------------------|-----------------------|-----------------------|---------------|
| Wavelength             | 632.8 nm             | 1.06 $\mu\text{m}$    | 694.3 nm              | 1.06 $\mu\text{m}$    | $\sim 550$ nm |
| $\Delta\nu$ (Hz)       | $1.5 \cdot 10^9$     | $1.2 \cdot 10^{10}$   | $6 \cdot 10^{10}$     | $3 \cdot 10^{12}$     | $10^{13}$     |
| $\Delta\nu^{-1}$ (sec) | $6.6 \cdot 10^{-10}$ | $8.34 \cdot 10^{-11}$ | $1.66 \cdot 10^{-11}$ | $3.33 \cdot 10^{-13}$ | $10^{-13}$    |
| $\tau$ (sec)           | $6 \cdot 10^{-10}$   | $7.6 \cdot 10^{-11}$  | $1.2 \cdot 10^{-11}$  | $4.0 \cdot 10^{-13}$  | $10^{-13}$    |

The minimum pulse duration is of  $\approx 8$  femtosec  
 $\tau_{\text{min}} \approx 5$  cycles of the optical radiation



(a) Inhomogeneously broadened Doppler gain curve of the 6328 Å Ne transition and position of allowed longitudinal mode frequencies. (b) Intensity versus frequency profile of an oscillating He-Ne laser. Six modes have sufficient gain to oscillate. Source: Reference 9.

$$\tau = \frac{0.886}{\Delta\nu}$$

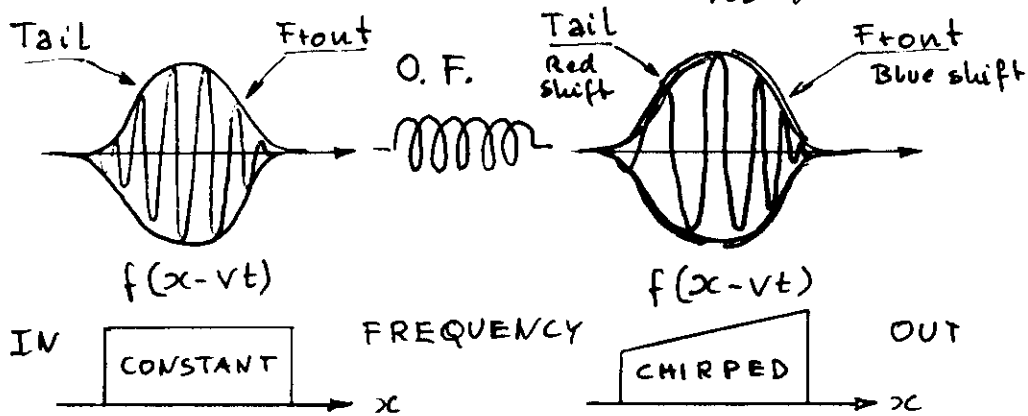


Theoretical plot of optical field amplitude  $[\sqrt{P(t)} \propto \sin(N\omega t/2) \sin(\omega t/2)]$  resulting from phase locking of five ( $N = 5$ ) equal-amplitude modes separated from each other by a frequency interval  $\omega = 2\pi/T$ .

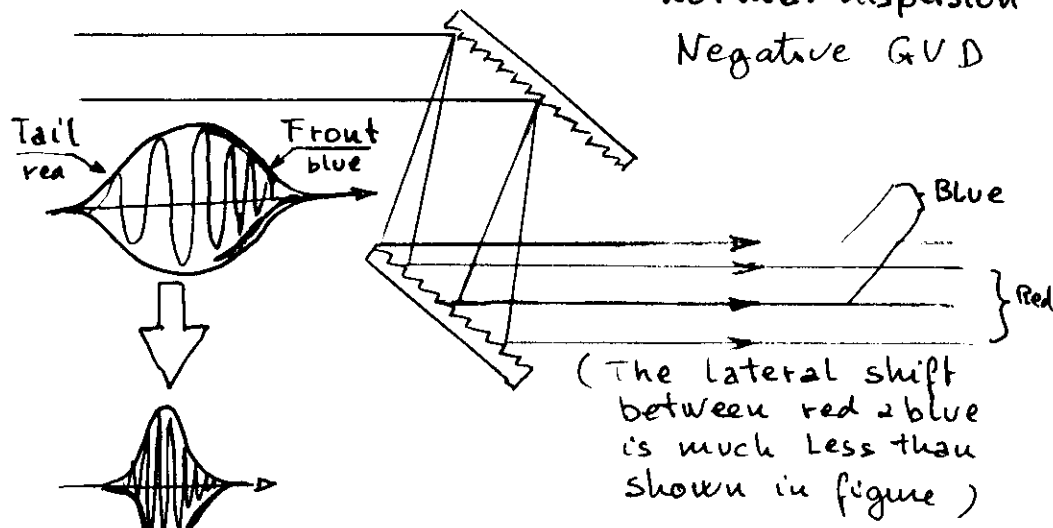
From "Principles of Lasers" O. Svelto

# Pulse Compression

I<sup>st</sup> Step - Optical Fiber - Non Linear effects in propagation induce a frequency modulation (CHIRP).  
Optical Kerr Effect  
Positive GVD

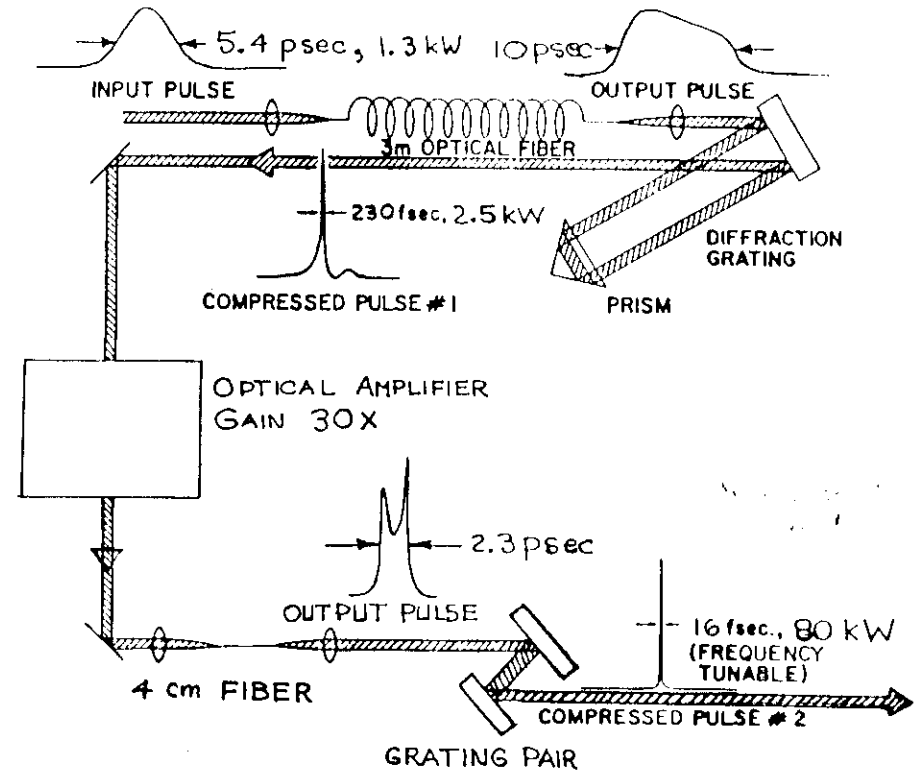


II<sup>nd</sup> Step - Two Gratings - A frequency dependent optical path difference is introduced: short  $\lambda \Rightarrow$  longer path normal dispersion  
Negative GVD



# Concentration in Time

CLEO 85 TH224-5



$$\frac{1}{\tau} = T = 3.33 \text{ fs}$$

$$v = \frac{c}{\lambda} = \frac{3 \cdot 10^{10} \text{ cm/s}}{10^{-4} \text{ cm}} = 3 \cdot 10^{14}$$

$$1 \text{ fsec} = 10^{-15} \text{ s}$$

FIGURE 1

(from S.L. Palfrey et al. IBM)

## Temporal Coherence & Monochromaticity

- First order correlation function between the field amplitudes at the same point at different times (ensemble (or time) ave.)

$$\Gamma_{11}^{(1)}(\bar{r}_1, \tau) = \langle E_1(\bar{r}_1, t) E_1^*(\bar{r}_1, t + \tau) \rangle$$

- The normalized function is called the "degree of temporal coherence" defined as:

$$\gamma_{11}^{(1)}(\bar{r}_1, \tau) = \Gamma_{11}^{(1)}(\bar{r}_1, \tau) / \Gamma_{11}^{(1)}(\bar{r}_1, 0) \leq 1$$

(in general is a complex quantity)

the value  $\tau_{coh}$  for which  $|\gamma_{11}^{(1)}(\bar{r}_1, \tau_{coh})| = 1/2$  can be assumed as the "coherence time" and correspondingly  $l_{coh} = \tau_{coh} \cdot c$  as the "coherence length"

- For a pure sinusoidal wave  $\tau_{coh} = \infty$
- For a conventional monochromatic source having a spectral linewidth  $\Delta\nu$   
 $\tau_{coh} \approx 1/\Delta\nu$  and  $|\gamma_{11}^{(1)}(\tau)| = e^{-\ln 2 \tau^2 / \tau_{coh}^2}$

In a Michelson interferometer the fringe intensity is given by

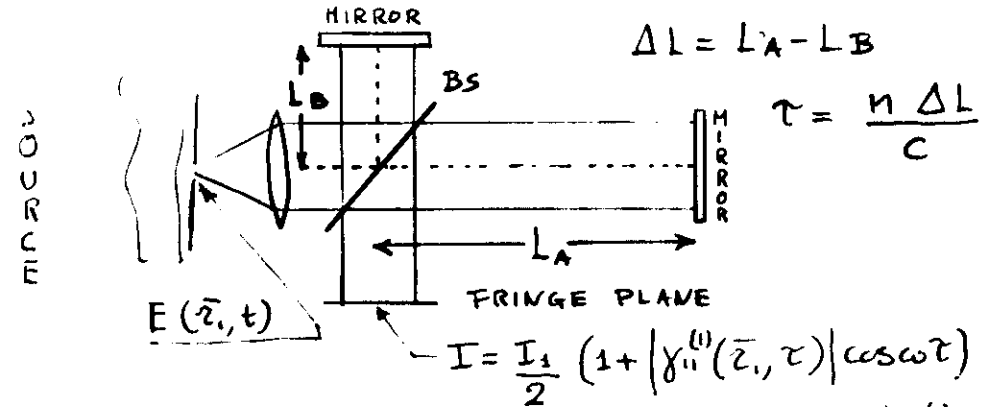
$$I = \frac{1}{2} I_1 \{ 1 + |\gamma_{11}^{(1)}(\tau)| \cos \omega \tau \}$$

where

$I_1$  is the beam intensity  $I_1 = \Gamma_{11}^{(1)}(\bar{r}_1, 0)$

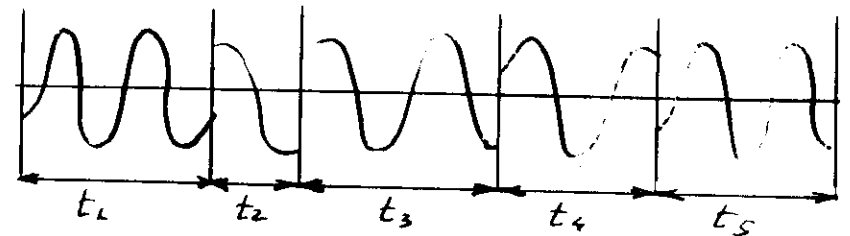
$\tau = n \Delta L / c$  is the difference in the propagation times of the two beams due to an optical path difference

## Temporal Coherence & Monochromaticity



The fringe visibility  $V = \frac{I_{MAX} - I_{MIN}}{I_{MAX} + I_{MIN}} = |\gamma_{11}^{(1)}(\bar{r}, \tau)|$

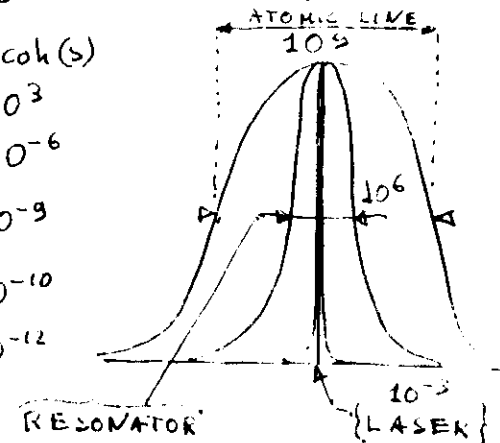
Ex. 1 Non coherent "Monochromatic" source (Equivalent to "white noise" filtered)



$$\tau_{coh} = \text{Average } t_i \approx 1/\Delta\nu$$

|               | $\Delta\nu(\text{Hz})$ | $\tau_{coh}(\text{s})$ |
|---------------|------------------------|------------------------|
| Laser         | $10^{-3}$              | $10^3$                 |
| Resonator     | $10^{+6}$              | $10^{-6}$              |
| Atomic line   | $10^{+9}$              | $10^{-9}$              |
| (Nd-YAG) XTAL | $10^{10}$              | $10^{-10}$             |
| Nd GLASS      | $10^{12}$              | $10^{-12}$             |

( $10^{-9} \text{ s} \rightarrow 30 \text{ cm}$ )



frequency selective optical elements (FSO)

frequency selective optical elements are included in the resonator to allow single frequency oscillation such as: PRISMS - GRATINGS - SMITH CAVITY BIREFRINGENT FILTERS - WEDGES - ETALONS SEEDING OR INJECTION LOCKING.

## LIMITS TO THE COHERENCE TIME

### Oscillation Frequency

$$\nu_{osc} = \frac{\nu_o / \Delta \nu_o + \nu_c / \Delta \nu_c}{1 / \Delta \nu_c + 1 / \Delta \nu_o}$$

### Quantum Limit

$$\Delta \nu_{osc} = \frac{N_2}{N_2 - N_1} \frac{2\pi^2 h \nu_{osc} \Delta \nu_c^2}{P} = \frac{2\pi^2 N_2}{N_2 - N_1} \frac{\Delta \nu_c}{N_p}$$

where  $N_p = \frac{P}{h \nu_{osc} \Delta \nu_c}$  is the number of photons inside the cavity.

In practice for  $P = 1 \text{ mW}$ ,  $\Delta \nu_c = 10^7 \text{ Hz}$

$$\Delta \nu_o / \nu_{osc} = 10^{-15}$$

### Thermal Fluctuations Limit

$$\Delta \nu_{osc} / \nu_{osc} = -\Delta L / L = -\Delta \lambda / \lambda = \sqrt{\frac{2kT}{VY}}$$

V Volume of the spacers; Y Young's modulus

In practice  $\Delta \nu_{osc} / \nu_{osc} = 10^{-11} - 10^{-10}$

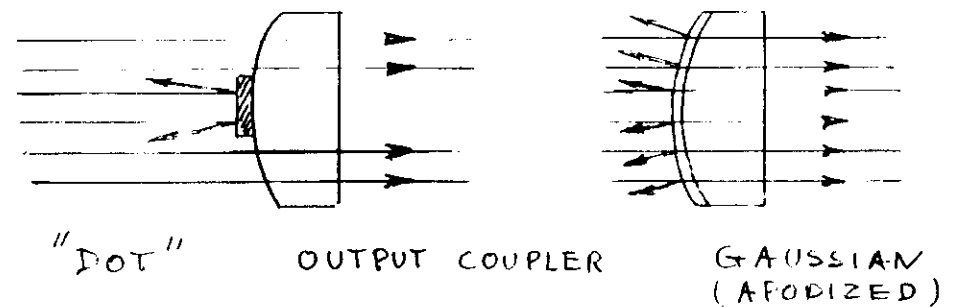
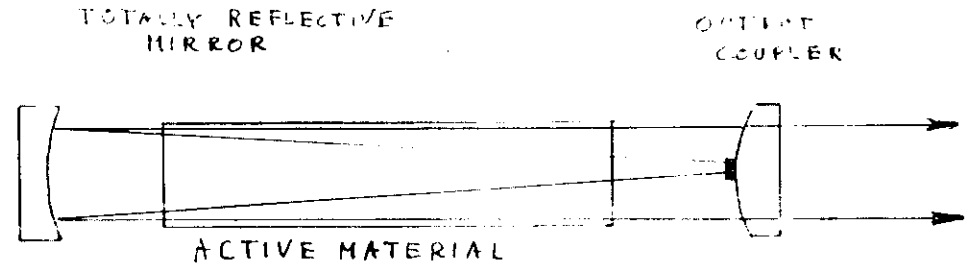
### Drifts due to change in Temperature

$$\Delta \nu_{osc} / \nu_{osc} = \alpha \Delta T$$

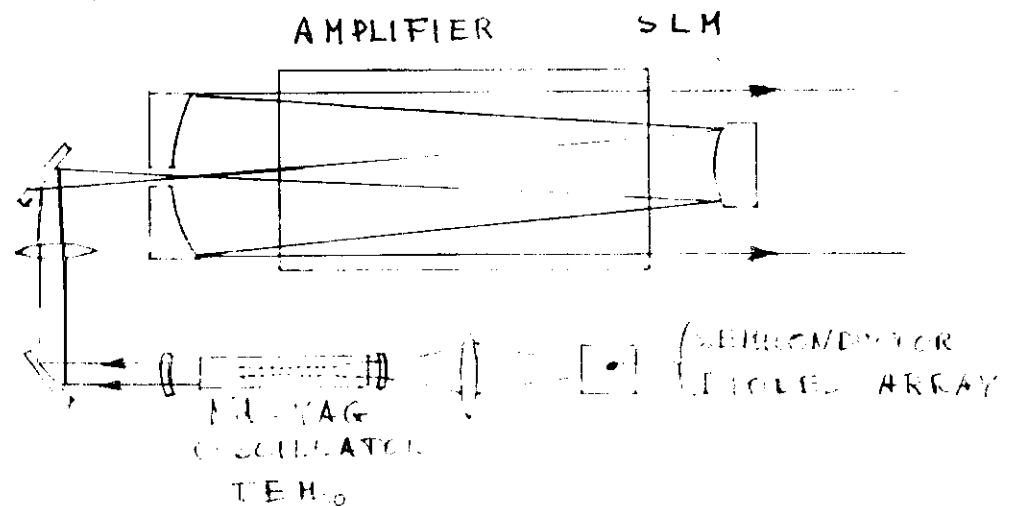
$$\alpha = 10^{-6} / ^\circ\text{C}$$

limits set by gain fluctuations thermal frequency pulling effects

## MODE SELECTION

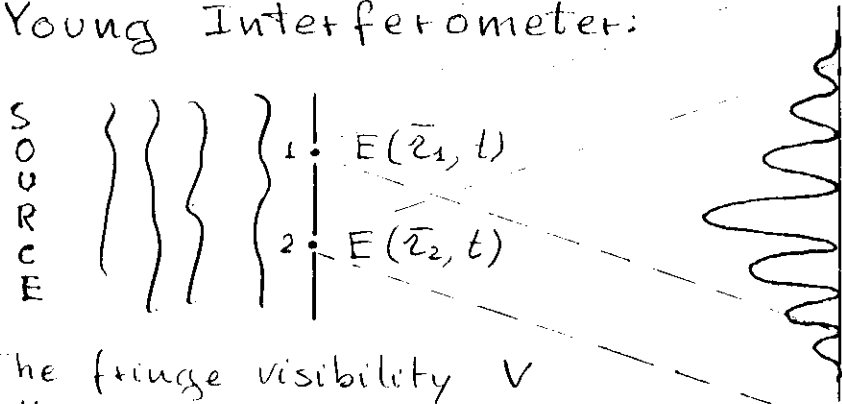


## INJECTION LOCKING (SEEDING)



## Spatial Coherence & Directionality

### Young Interferometer:



The fringe visibility  $V$  allows the measure of the "coherence radius" and "coherence area"

Beams with partial spatial coherence have a divergence greater than for a spatially coherent beam with the same intensity distribution.

Example: Semiconductor lasers or solid state lasers with "hot spots". The divergence is  $\theta_d' \approx 1.22 \lambda / d$



instead of  $\theta_0 = 1.22 \lambda / D$ . Multimode lasers have a divergence larger than the single mode case.

$$\theta_{e,m} = \theta_{e,m} \cdot \frac{\lambda}{\pi w_0} \quad \text{--- } m = 1, 16$$

(if the spot size  $\approx 90\%$  of beam power is considered)  $\quad C_{00} = 1.16$

The lack of spatial coherence reduces the fringe visibility and consequently the efficiency f.e. of an hologram

## Spatial Coherence & Directionality

- First order correlation function between the field amplitudes at the same time in different points {ensemble (or time) ave.}

$$\Gamma_{12}^{(1)}(\vec{r}_1 - \vec{r}_2, t) = \langle E_1(\vec{r}_1, t) E_2^*(\vec{r}_2, t) \rangle$$

- The normalized function is called the "degree of spatial coherence" defined as:  

$$\gamma_{12}^{(1)}(\vec{r}_1 - \vec{r}_2, 0) = \Gamma_{12}^{(1)}(\vec{r}_1 - \vec{r}_2, 0) / \left\{ \Gamma_{11}^{(1)}(\vec{r}_1) \cdot \Gamma_{22}^{(1)}(\vec{r}_2) \right\}^{1/2} \leq 1$$
 (in general is a complex quantity)
- The value  $|\vec{r}_1 - \vec{r}_2|$  for which  $|\gamma_{12}^{(1)}(\vec{r}_1 - \vec{r}_2, 0)| = 1/2$  defines the "coherence radius" and the related "coherence area".
- For an ideal unlimited wave (f.e. coming from a single spatial mode of a laser) the coherence radius  $\rightarrow \infty$ .
- NF • For a wavefront limited by an aperture with a diameter  $D$  the propagation vector  $\vec{k}$  is affected by a spread  $\Delta k = k \cdot \Delta \theta$  where  $\Delta k = 1.22 \cdot 2\pi / D$ .
- FF • If the apertured beam is focused by a lens of focal length  $f$  the spot size is defined by  $\Delta s = f \Delta \theta = f \cdot 1.22 \lambda / D$  and again the limitation due to diffraction holds:  

$$\frac{1}{\lambda} \cdot \frac{D}{f} = \frac{1}{\lambda} \frac{\Delta k}{k} = \frac{\Delta k}{2\pi} = 1.22 / \Delta s$$

$$\left( \frac{D}{f} = \frac{\Delta k}{k} = \frac{k \Delta \phi^{FF}}{k} = F\text{-number} \right)$$
- The space concentration limit is  

$$\Delta s \approx 1.22 \frac{f}{D} \lambda \quad (\text{a few } \lambda\text{'s}).$$

## LONGITUDINAL MODE OPERATION

(Prerequisite for single frequency oscill.)

Mode selection can be accomplished by:

1. Exploiting diffraction losses

in stable resonators. Low Fresnel numbers ( $\approx 1$ );  $F = a^2/L\lambda$

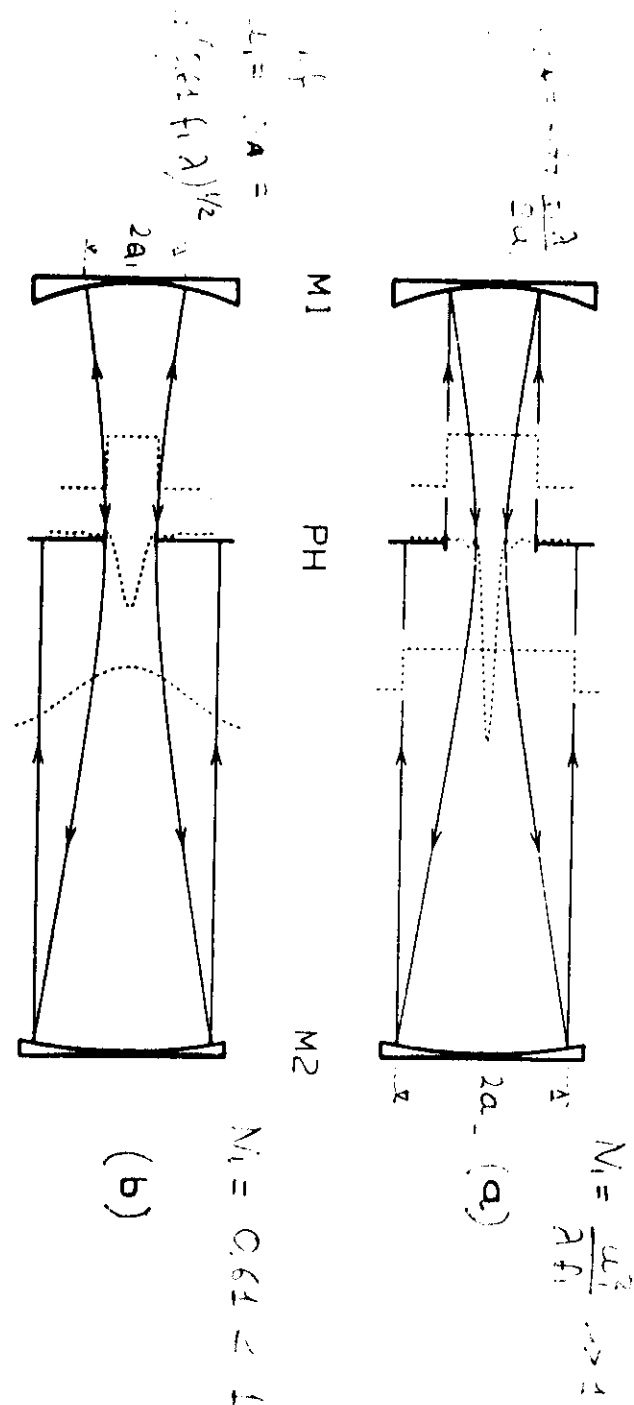
( $a$  - radius of the aperture;  $\lambda$  wavelength  
 $L$  - cavity length) allow the selection of the TEM<sub>00</sub> mode.

2. If large power or energy are requested large active volumes and, in practice, high Fresnel numbers are needed. Special mode selecting cavities must be used such as:

- Self Filtering confocal Unstable Resonators (SFUR) - negative branch
- Unstable confocal resonators with Variable Reflectivity Mirrors (VRM):
  - Dot mirrors
  - Hard Edge phase unified couplers
  - Mirrors with Gaussian or SuperGaussian reflectivity profiles.
  - Ring cavities with expanders
  - Phase conjugated Mirrors

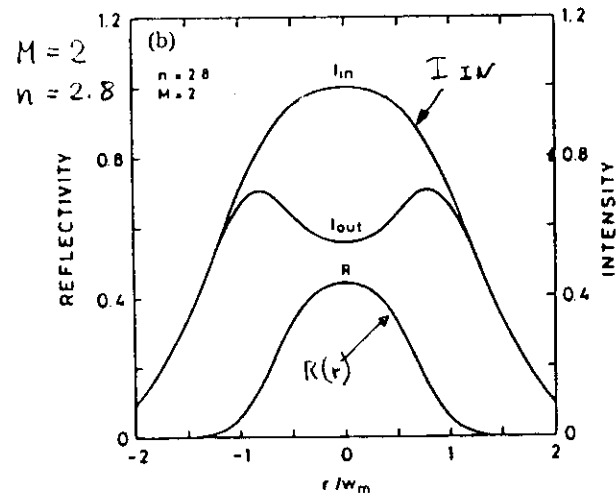
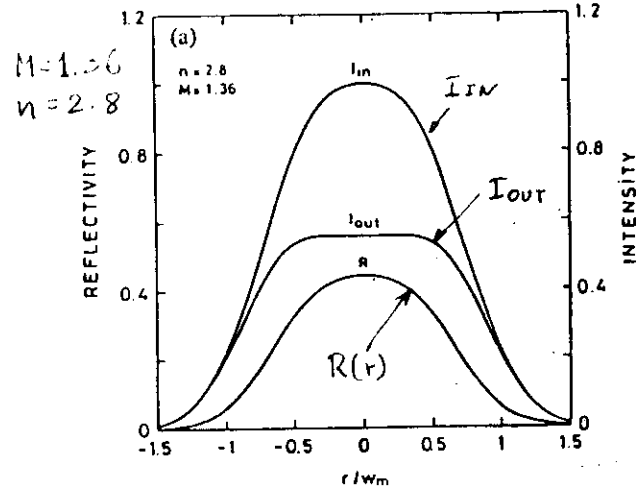
Fig. 1. Schematic of the self-imaging (a) and self-filtering (b) unstable resonators:  $M_1, M_2$ , fully reflecting concave mirrors of focal lengths  $f_1, f_2$ ; PH, pinhole of diameter  $2a$  placed in the common focal plane of the two mirrors.

(P. G. Gobbi et al. Appl. Opt. 24, 26 Jan 1985)



$R(r) = R_0 \exp \left[ -2 \left( r/w_m \right)^n \right]$

$n$  - ORDER  
OF Super-  
Gaussianity

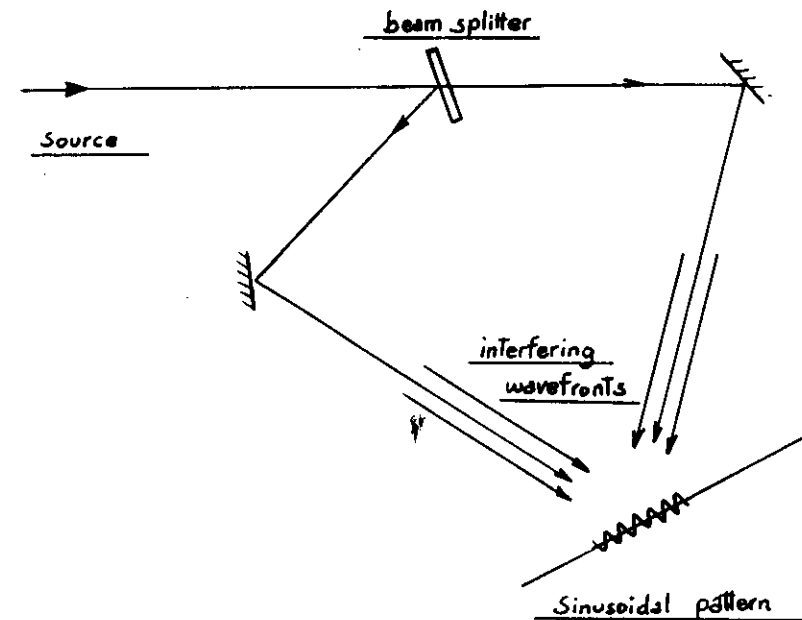


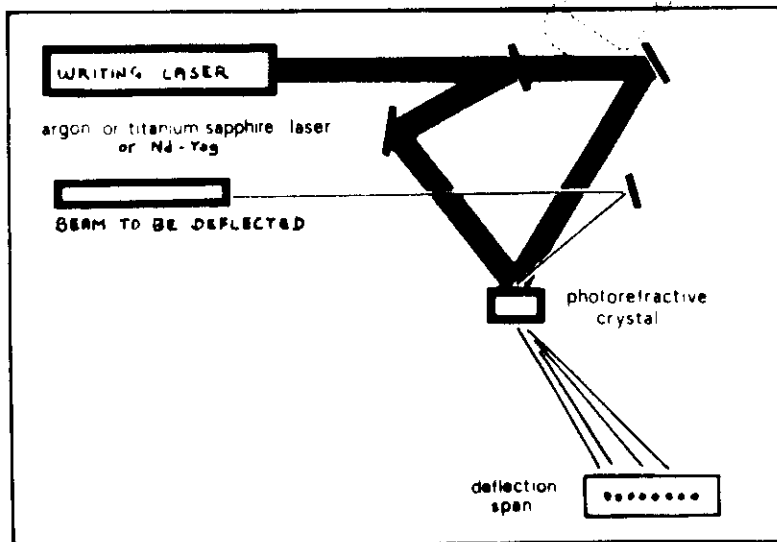
Theoretical intensity profiles of the wave incident  $I_{in}$  on a super-Gaussian reflectivity mirror of order  $n = 2.8$ , and of the transmitted beam  $I_{out}$  as a function of radial coordinate  $r$  normalized to the mirror spot size  $w_m$  for two resonator magnifications: (a)  $M = 1.36$ . (b)  $M = 2$ . The reflectivity profile of the mirror  $R$  is also reported.

IEEE J. QE Vol 24 6 (1988)

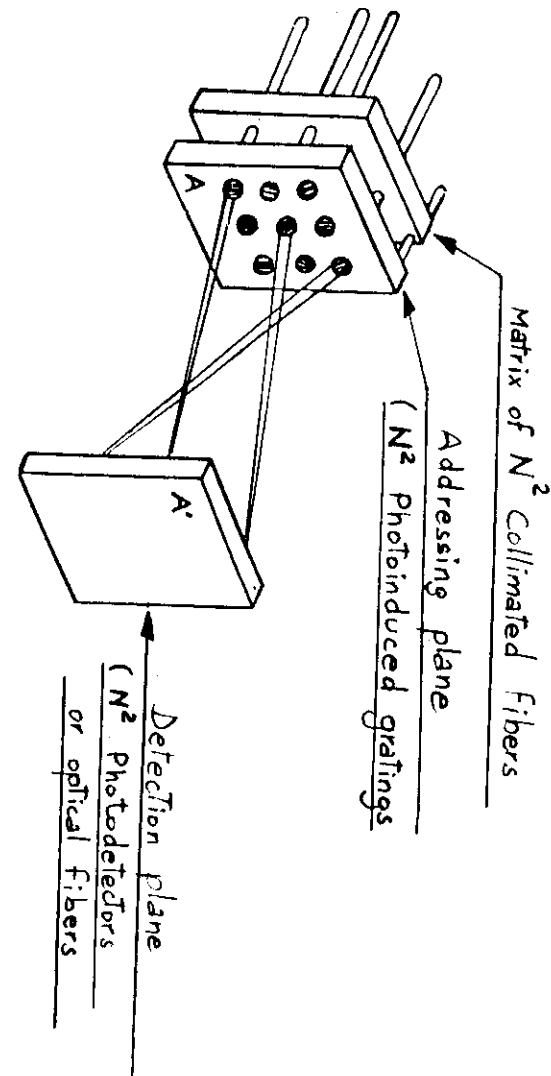
S. DE SILVESTRI, P. LAPORTA, V. MAGGI, O. SVELTO

## Generation of grating pattern





Scheme showing variable spacing grating recording in a photorefractive material and related deflection undergone by a signal beam.



1000  
1000  
1000