



INTERNATIONAL ATOMIC ENERGY AGENCY  
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**INTERNATIONAL CENTRE FOR THEORETICAL PHYSICS**  
I.C.T.P., P.O. BOX 586, 34100 TRIESTE, ITALY, CABLE: CENTRATOM TRIESTE



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## **INTERNATIONAL CENTRE FOR SCIENCE AND HIGH TECHNOLOGY**

c/o INTERNATIONAL CENTRE FOR THEORETICAL PHYSICS 34100 TRIESTE (ITALY) VIA GRIGNANO, 9 (ADRIATICO PALACE) P.O. BOX 586 TELEPHONE 040-224572 TELEFAX 040-224575 TELEX 460449 APH I

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**Research Workshop in Condensed Matter,  
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**"The Electronic Structure of Random  
 $A_{111}B_v$  and  $A_{11}B_{v1}$  Semiconductor Alloys  
by TB-LMTO Method"**

**J. KUDRNOVSKY  
Czechoslovak Academy of Sciences  
Institute of Physics  
Na Slovance 2  
Liben, Prague 18040 (8)  
CZECHOSLOVAKIA**

**These are preliminary lecture notes, intended only for distribution to participants.**

THE ELECTRONIC STRUCTURE OF  
RANDOM  $A'''B^V$  AND  $A''B^{VI}$   
SEMICONDUCTOR ALLOYS BY  
TB-LMTO METHOD

J. Kudrnovský and V. Drchal

Institute of Physics ČSAV, Prague,  
Czechoslovakia

M. Šob

Institute of Physical Metallurgy ČSAV, Brno,  
Czechoslovakia

N.E. Christensen and O.K. Andersen

Max-Planck-Institut FKF, Stuttgart,  
FRG

## ELECTRONIC STRUCTURE OF RANDOM SEMICONDUCTORS

difficult problem, two approaches

A. Configurational averaging (CPA)

B. Representative configuration (supercell)

- concentration trends,  
damping of el. states

- structural distortions  
directly

- minimal basis set

- ab initio approach,

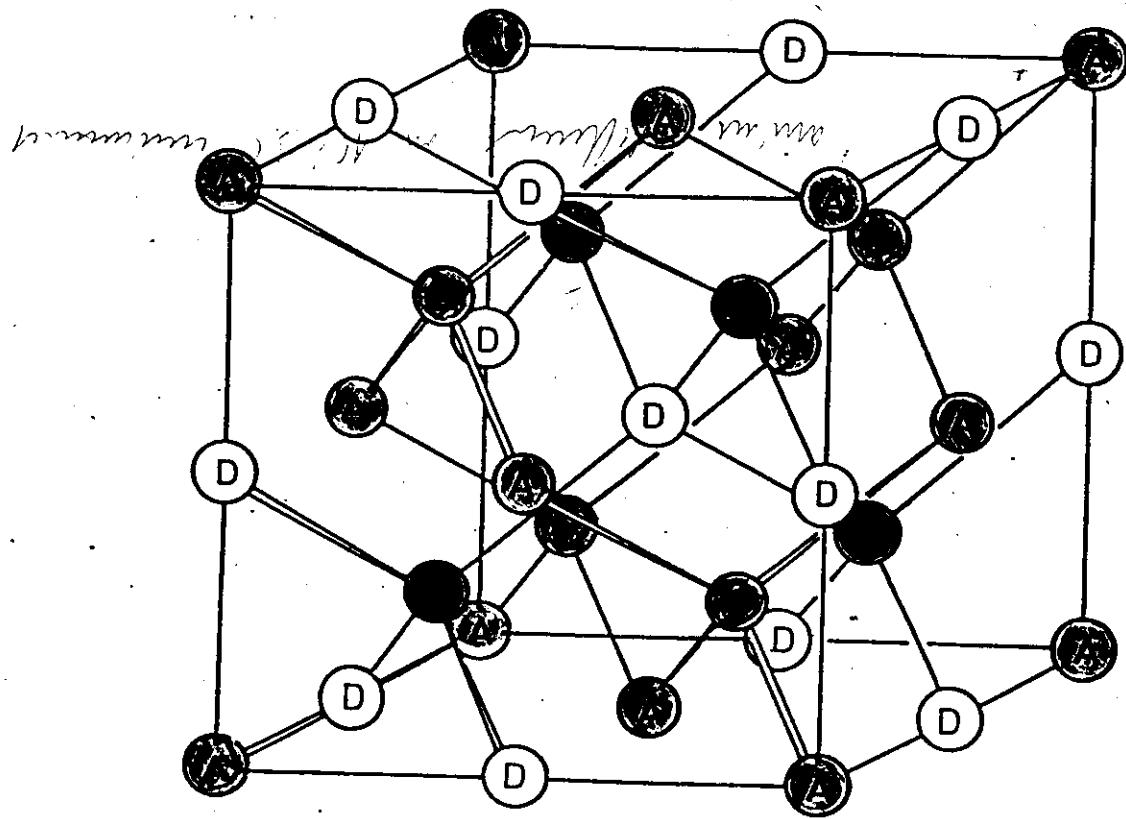
- structural distortions  
via hopping integrals

standard techniques

■ empirical theory,  
off-diagonal disorder

■ artificial geometry,  
no damping

TB-LMTO-CPA



Empty-sphere concept

bcc = 4 fcc sublattices A, B, C, D

### Structure

diamond

A	B	C	D
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ZnS

C	C	E	E
---	---	---	---

NaCl

Zn	S	$E_1$	$E_2$
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$\text{CaF}_2$

Na	E	Cl	E
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( $\text{DO}_3$ )

Ca	F	E	F
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$\text{Fe}^A$	$\text{Fe}^B$	$\text{Fe}^C$	$\text{Si}^D$
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## HAMILTONIAN FOR RANDOM ALLOYS

orthogonal LMO-repres

$$H_{RL,R'L'} = C_{RL} \delta_{RR'} \delta_{LL'} + \Delta_{RL}^{1/2} \left\{ S^o (1 - \beta S^o)^{-1} \right\}_{RL,R'L'} \Delta_{R'L'}^{1/2}$$

$$\Omega_{RL,R'L'} = \delta_{RR'} \delta_{LL'} \quad R/L = \ell m \dots \text{site/orbital index}$$

Empty sphere concept  $\Rightarrow$  close-packed filling

bcc (9/2) 4 fcc, origins at lattice points  
on bcc body-diagonal



$S^o$  - canonical structure constant, do not depend on lattice constant

Example: zinc-blende  $A_x B_{1-x} C$  alloy

fcc(1) : cations A/B

fcc(3) : different ES

fcc(2) : anions C  $\Rightarrow$  AC/BC

fcc(4) : from AC/BC

Unified description: diamond, ZnS, NaCl, CaF<sub>2</sub>

Potential parameters :  $\chi = C, \Delta, \beta$

$x_{RL} \Rightarrow$  randomly  $x_L^{(1)}(x), x_L^{(2)}(1-x)$

Physical meaning :

$$P_e^o(E) = (E - C_e) / (\Delta_e + \beta_e(E - C_e)) \propto \cot \gamma_e(E)$$

PP depend on : - type of atom  
- lattice constant

PP are obtained from first-principles as solutions of SE for LDA-potentials in atomic spheres centred at R

Feature :

Separability of structural & atom-dependent parts of alloy Hamiltonian

## MODELLING OF BOND-LENGTH VARIATIONS

$S^0$  - same for any lattice constant

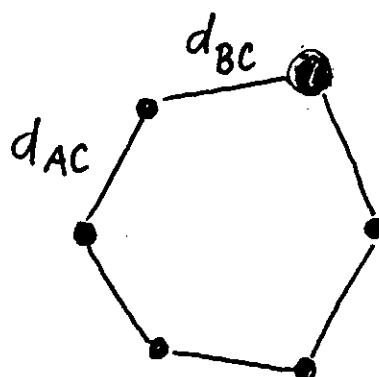
$C, \Delta, \beta$  - evaluated from LDA-potentials in their WS spheres  $\Rightarrow$  bond lengths

Bond-length variations  $\Rightarrow$

differences in AC/BC hopping elements  
via potential parameters

(off-diagonal disorder)

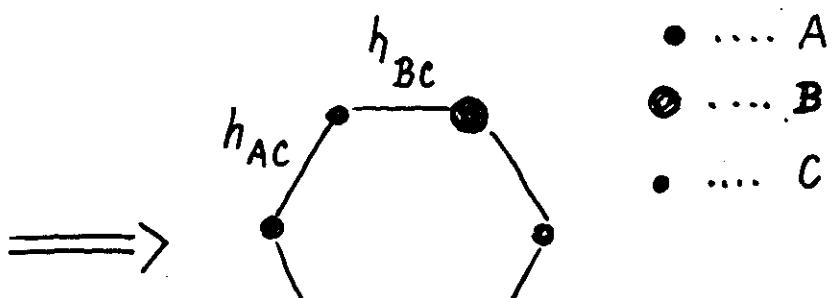
Actual:



different bond-lengths

$$(d_{Ac} \neq d_{Bc})$$

Model:



different hoppings

$$(h_{Ac} \neq h_{Bc})$$

## THEORETICAL TECHNIQUES

Coherent potential approximation :

$$\langle G(z) \rangle = \langle (z. I - H)^{-1} \rangle \Rightarrow \begin{matrix} \text{diagonal / off-diagonal} \\ (\text{bond-length}) \end{matrix}$$

Cannot be treated in CPA without limitations  
in orthogonal LMTO repres

Solution : separability of structural ( $S^\alpha$ ) / atom-dependent parts ( $C, \Delta, \chi$ ) + transformation from orthogonal to auxiliary LMTO repres

$$G(z) \implies g^\beta(z) = (P^\beta(z) - S^\beta)^{-1}$$

(exact scaling transf)

↴ non-random  
 ↴ site-diagonal & random  
 (CPA applies)

$$\text{Final step: } \langle g^\beta(z) \rangle \implies \langle G(z) \rangle$$

(exact scaling transf)

Minimal basis set:

$sp^3d^5$ -LMTO's on each atom/ES  $\Rightarrow$   $36 \times 36$  format of CPA

Use of all orbitals: unphysical & undesirable

$36$  LMTO's =  $\mathcal{L} + \mathcal{H}$  subsets,  $\dim(\mathcal{L}) \approx 3-4$  times less

$\mathcal{L}$ -subset: minimal basis, accurate in a given E-range & treated exactly within CPA

$\mathcal{H}$ -subset: its influence via simplified linearization scheme based on Löwdin downfolding applied in a suitably chosen LMTO repres ; consistent approximate CPA treatment

Properties:

- (i) No loss of accuracy in chosen E-range
- (ii) Theory provides a way how to choose  $\mathcal{H}$ -LMTO repres
- (iii)  $\mathcal{L}$ -sets in alloys same for AC & BC

Division into  $L$  &  $H$  sets depends on:

- (i) Material - elemental,  $A'''B''$ ,  $A''B'''$  etc

(ii) Lattice structure - diamond, ZnS, NaCl, CaF<sub>2</sub>

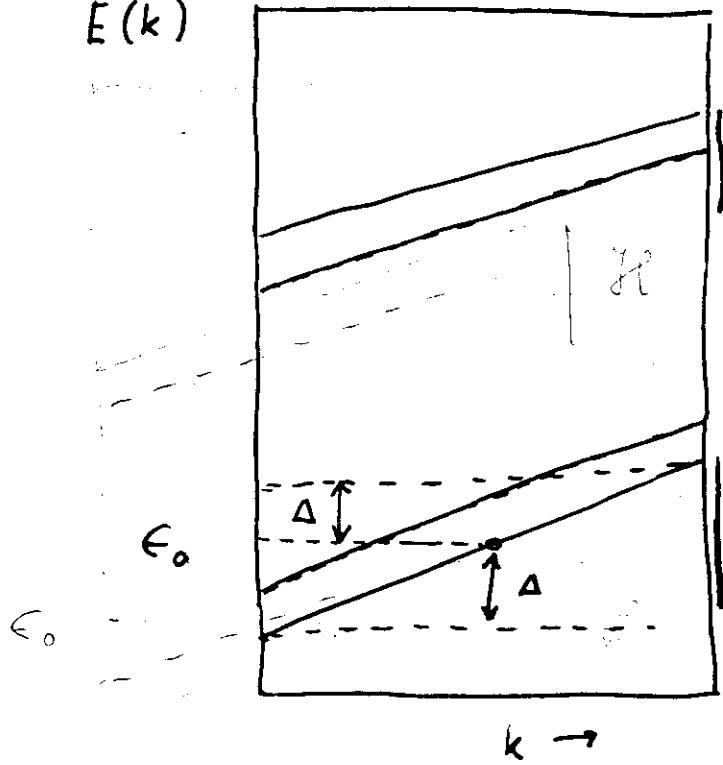
(iii) Energy region - gap, valence bands, conduction states etc

## Examples:

CdTe	$\text{Cd}(\text{sp}^3)\text{Te}(\text{p}^3)E_1(\text{s})E_2(\text{s})$	- $9 \times 9$ , gap
(ZnS)	$\text{Cd}(\text{d}^5)\text{Te}(\text{s})$	- $6 \times 6$ , low valence

$(CdF_2)$        $Cd(sd^5) F(p^3) E(s) F(p^3)$  -  $13 \times 13$ , valence  
 $(CaF_2)$

$E(k)$



— unhybridized  
bands  $\epsilon_x(k), \epsilon_{ye}(k)$

— hybridized bands  
 $E_x(k), E_{ye}(k)$

$$(E - \epsilon_x)^{-1} = (E - \epsilon_{ye})^{-1}$$

L

for  $E \in \epsilon_x$

$\epsilon_x \approx \epsilon_0$   
gives hybridized  
bands  $E_x(k), E_{ye}(k)$

$$G(E) = \begin{pmatrix} E - \epsilon_x(k) & -\frac{\partial}{\partial k} \\ -\frac{\partial}{\partial k} & E - \epsilon_{ye}(k) \end{pmatrix}^{-1}$$

As  $\Delta \ll$  separation of  $\epsilon_x, \epsilon_{ye}$  bands, for  
 $E \in \epsilon_0 \pm \Delta$  it holds  $E - \epsilon_{ye} \approx \epsilon_0 - \epsilon_{ye}$

$$\underset{(1 \times 1)}{G(E)} = \frac{1}{E - \epsilon_x(k) - \frac{\partial}{\partial k}} , \quad \underset{x}{\Pi(k)} = \frac{\frac{\partial}{\partial k} \epsilon_{ye} \delta_{xx}}{\epsilon_0 - \epsilon_{ye}(k)}$$

→ band shift

Result:

$\epsilon_x(k)$  nearly exact,  $\epsilon_{ye}(k)$  does not described

# DOWNFOLDING TO MINIMAL ( $\mathcal{L}$ ) BASIS SET

We divide full space:  $\mathbb{H} = \mathcal{L} + \mathcal{H}$

Blocks of averaged resolvent (downfolding).

$$\langle g(z) \rangle_{S,S'} = N_{S,S'}^{\beta}(z) S_{SS'}^{\beta} + M_{S,S'}^{\beta}(z) \langle g^{\beta}(z) \rangle_{SS'} M_{S,S'}^{\beta}(z), \quad S, S' = \mathcal{L}, \mathcal{H}$$

$$\langle g^{\beta}(z) \rangle_{\mathcal{L}\mathcal{H}} = \langle g^{\beta}(z) \rangle_{\mathcal{L}\mathcal{L}} S_{\mathcal{L}\mathcal{H}}^{\beta} F_{\mathcal{H}\mathcal{H}}^{\beta}(z)$$

$$\langle g^{\beta}(z) \rangle_{\mathcal{H}\mathcal{L}} = F_{\mathcal{H}\mathcal{H}}^{\beta}(z) S_{\mathcal{H}\mathcal{L}}^{\beta} \langle g^{\beta}(z) \rangle_{\mathcal{L}\mathcal{L}}$$

$$\langle g^{\beta}(z) \rangle_{\mathcal{H}\mathcal{H}} = F_{\mathcal{H}\mathcal{H}}^{\beta}(z) + F_{\mathcal{H}\mathcal{H}}^{\beta}(z) S_{\mathcal{H}\mathcal{L}}^{\beta} \langle g^{\beta}(z) \rangle_{\mathcal{L}\mathcal{L}} S_{\mathcal{L}\mathcal{H}}^{\beta} F_{\mathcal{H}\mathcal{H}}^{\beta}(z)$$

$$\langle g^{\beta}(z) \rangle_{\mathcal{L}\mathcal{L}} = (\mathcal{P}_{\mathcal{L}}^{\beta}(z) - S_{\mathcal{L}\mathcal{L}}^{\beta} - S_{\mathcal{L}\mathcal{H}}^{\beta} F_{\mathcal{H}\mathcal{H}}^{\beta}(z) S_{\mathcal{H}\mathcal{L}}^{\beta})^{-1} \quad \text{and}$$

$$F_{\mathcal{H}\mathcal{H}}^{\beta}(z) = (\mathcal{P}_{\mathcal{H}}^{\beta}(z) - S_{\mathcal{H}\mathcal{H}}^{\beta})^{-1}$$

Advantage: all blocks are expressed via  $\langle g^{\beta}(z) \rangle_{\mathcal{L}\mathcal{L}}$   
 to be approximated. Specifically, we  
 look for approximate form of  $F_{\mathcal{H}\mathcal{H}}^{\beta}(z)$   
 which is numerically demanding

(repeated evaluation of matrix inversions of dim( $\mathcal{H}$ )  
 for many  $z$  and  $k$ -vectors )

Approximate form of  $F_{ye}^{\beta}(z)$ :

- (i) we choose the energy range of interest for  $\ell$ -states centred around the energy  $\epsilon_0$ , where we need a proper description
- (ii) we transform to a new representation  $\beta = (\beta_x, \beta_{ye})$  such that

$$\bar{P}_{ye}^{\beta-1}(\epsilon_0) = 0 \quad (\text{equation for } \beta_{ye}; \beta_x = \text{screened HTO repres})$$

Solution:  $\ell$ -states lie outside the energy range of  $\ell$ -states (weak hybridization), so that

$$\operatorname{Im} \bar{P}_x^{\beta}(z) \approx 0, \quad \bar{P}_{ye}^{\beta}(z) \approx x \bar{P}_{ye}^{\beta,1}(z) + (1-x) \bar{P}_{ye}^{\beta,2}(z)$$

$$\beta_{ye} = \bar{f}_{ye} + \frac{\bar{\delta}_{ye}}{\epsilon_0 - \bar{c}_{ye}} \quad (\bar{x} = x X^1 + (1-x) X^2)$$

Because  $\|\bar{P}_{ye}^{\beta}(z)\| \gg \|S_{xe}^{\beta}\|$  for  $z$  around  $\epsilon_0$ , we can write

$$F_{ye}^{\beta}(z) \approx \frac{d}{dz} \left( \bar{P}_{ye}^{\beta}(z) \right)^{-1} |_{\epsilon_0} (z - \epsilon_0) \equiv \frac{\bar{V}_{ye}^{\beta} - z}{\bar{P}_{ye}^{\beta}}$$

$$\bar{V}_{ye}^{\beta} = \bar{c}_{ye} - \frac{\bar{\delta}_{ye}}{\bar{f}_{ye} - \beta_{ye}}, \quad \bar{P}_{ye}^{\beta} = \frac{\bar{\delta}_{ye}}{(\bar{f}_{ye} - \beta_{ye})^2}$$

Using this approximate form

$$\langle g_{xx}^{\beta}(z) \rangle = \left( P_{xx}^{\beta}(z) - S_{xx}^{\beta} - T_{xx}^{\beta}(z) \right)^{-1}$$

$$\prod_{\text{xx}}^{\beta}(z) = S_{\text{xx}}^{\beta} \left\{ \bar{V}_{\text{xc}}^{\beta} / \bar{F}_{\text{xc}}^{\beta} \right\} S_{\text{xc}}^{\beta} - z S_{\text{xc}}^{\beta} \left\{ 1 / \bar{F}_{\text{xc}}^{\beta} \right\} S_{\text{xc}}^{\beta}$$

Advantage: trivial  $z$ -dependence of  $\Pi_{\text{ex}}^{\wedge}$  as compared to  $F_{\text{ex}}^{\wedge}$ ; consistent approximation for other blocks of  $\langle G \rangle$

## Features

- (i) The CPA eqs are solved only in the small  $\mathcal{Z}$ -block  
(all other blocks of  $\langle G \rangle$  expressed via  $\langle g^A \rangle_{ZK}$ )
  - (ii) significant numerical simplification while retaining essentially the same accuracy in the energy region of interest around  $\epsilon_0$
  - (iii) Method is inherent to TB-LMTO { change of screening of downfolded  $\mathcal{H}$ -states }
  - (iv)  $\Pi_{ZK}^B = A_{ZK} - z B_{ZK} \leftarrow \text{corrects } O \quad \} \quad \begin{matrix} \text{when going} \\ \text{back to } f\text{-repres} \end{matrix}$   
 $\left[ \begin{matrix} \text{corrects } H \end{matrix} \right]$

## CHOICE OF POTENTIAL PARAMETERS

■ Approximate bond-lengths preservation in alloys:

$$d_{AC}(x) \neq d_{BC}(x) \approx \text{const} \implies \text{EXAFS}, A_x B_{1-x} C \text{ alloy}$$

(ZnS :  $A'''B''$ ,  $A''B^{VI}$ )

Modelling : sc pp for AC/BC at experimental  
lattice constants  $a_{AC} \neq a_{BC}$   
(volume varies linearly with  $x$ )

Example: ZnS -  $Cd_x Hg_{1-x} Te$        $CaF_2 - Cd_x Pb_{1-x} F_2$   
 $(a \approx 6.48 \text{ \AA})$        $(a_{CdF_2} \approx 5.40 \text{ \AA}, a_{PbF_2} \approx 5.94 \text{ \AA})$

■ Linear variation of bond-lengths with composition:

$$d_{AC}(x) = d_{BC}(x), \text{ proportional linearly to } x$$

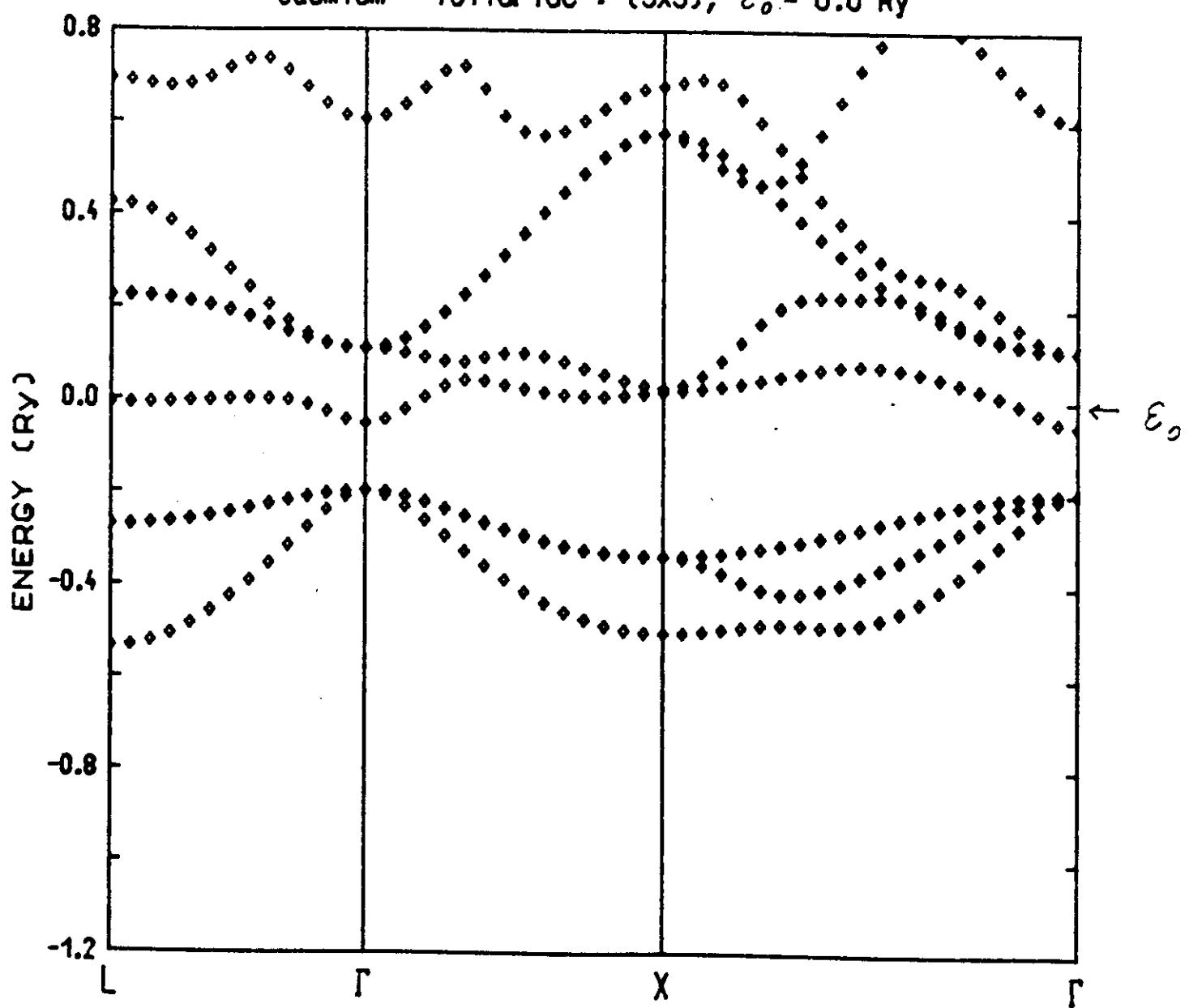
Modelling : sc pp evaluated for experimental  $a(x)$ ,  
same for AC & BC

More sophisticated choice : sc pp for  $A_n B_{4-n} C_4$  ( $n=0,1,2,3,4$ )  
 $\vdots$  supercells at experimental  $a(x)$ ,  
 $x = 0, 0.25, 0.5, 0.75, 1.0$  (16 atoms/cell)

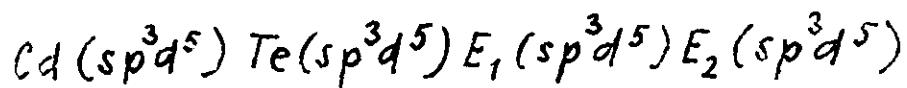
Example:  $CaF_2 - Cd_x Pb_{1-x} F_2, a(x) = x a_{CdF_2} + (1-x) a_{PbF_2}$

$\mathcal{L} : Cd(sp^3) Te(p^3) E_1(s) E_2(s)$

Scalar-relativistic band-structure of  
Cadmium - Telluride : (9x9),  $\epsilon_0 = 0.0$  Ry



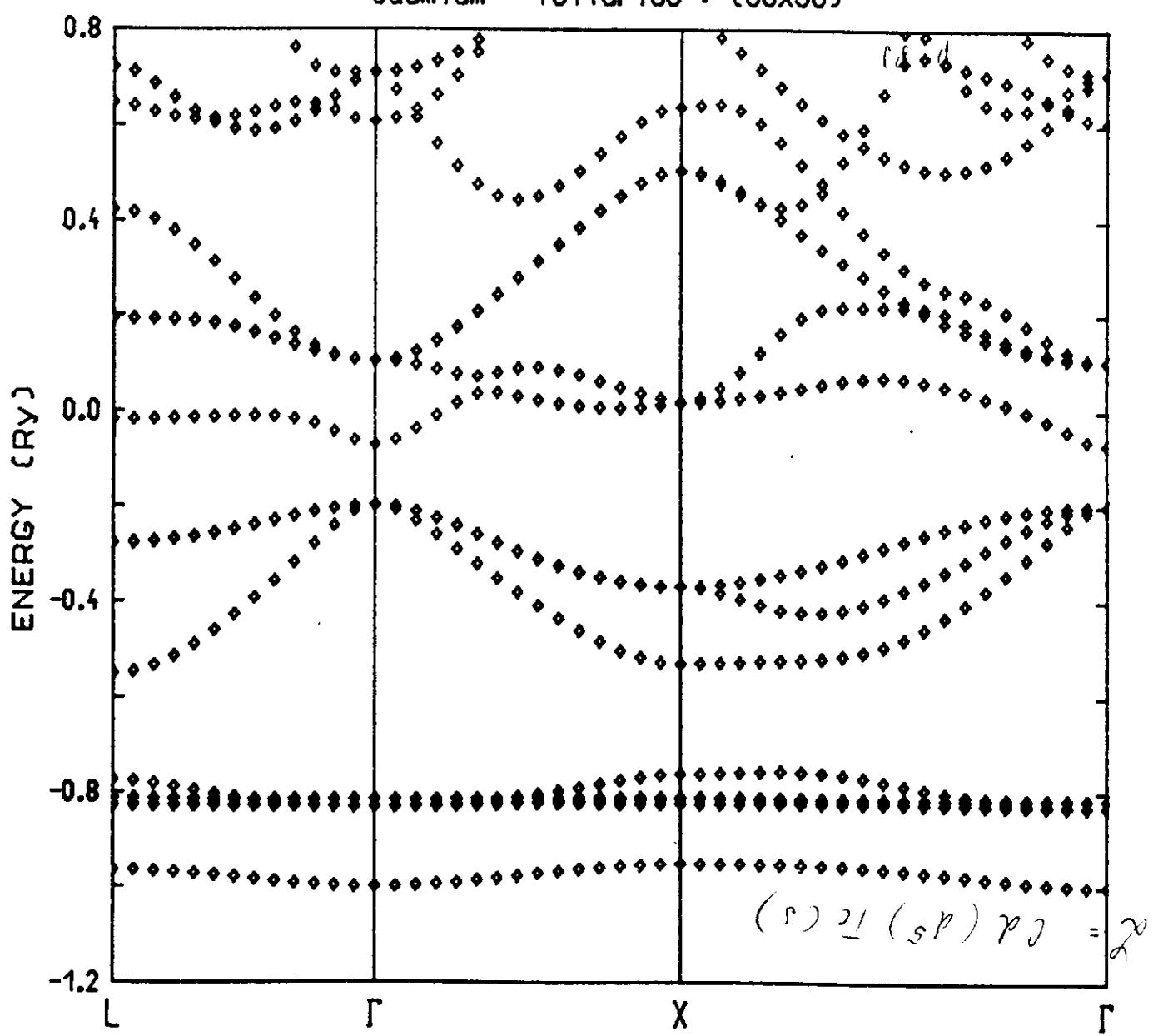
Full basis set :



def. Energy

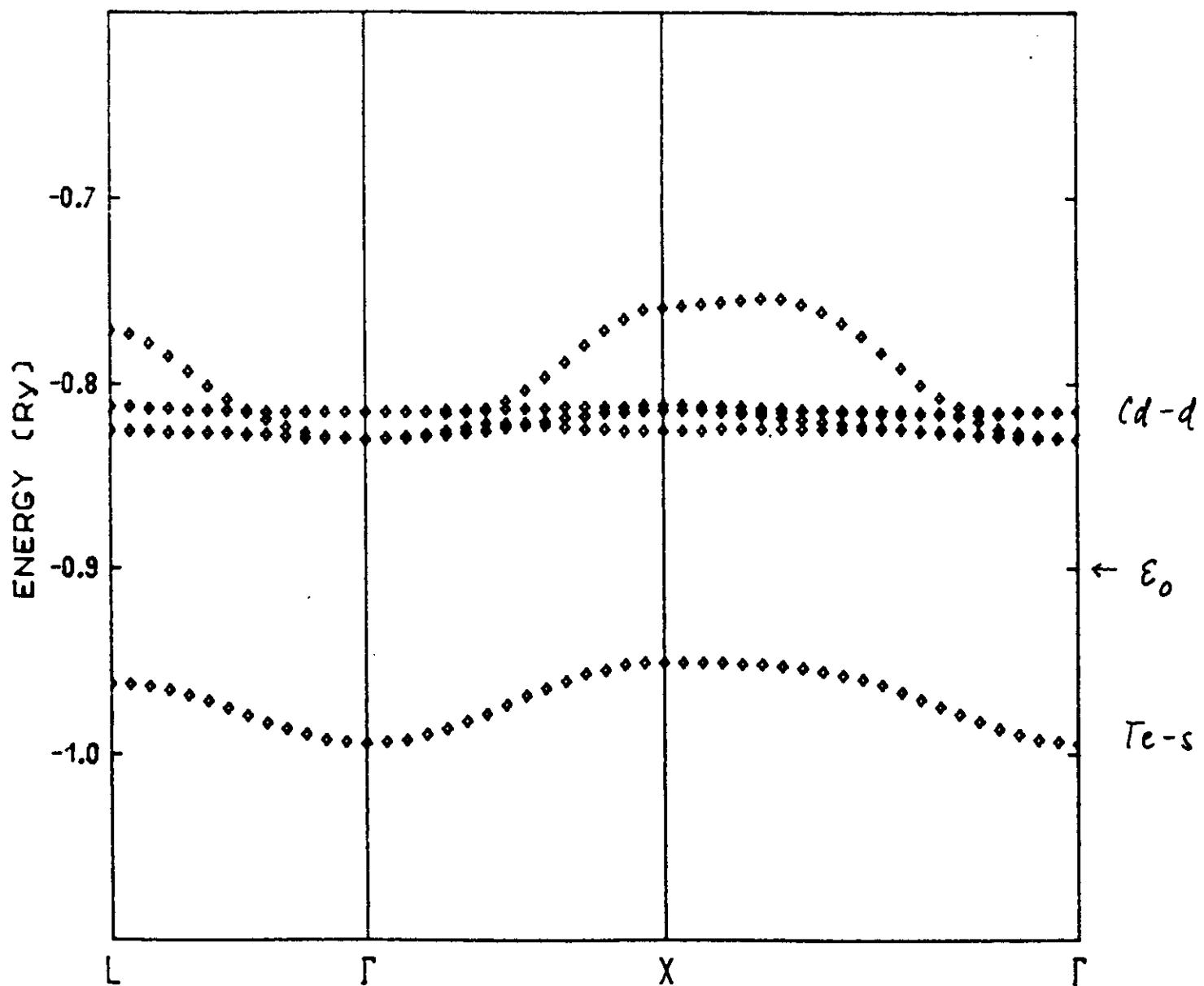
valence states

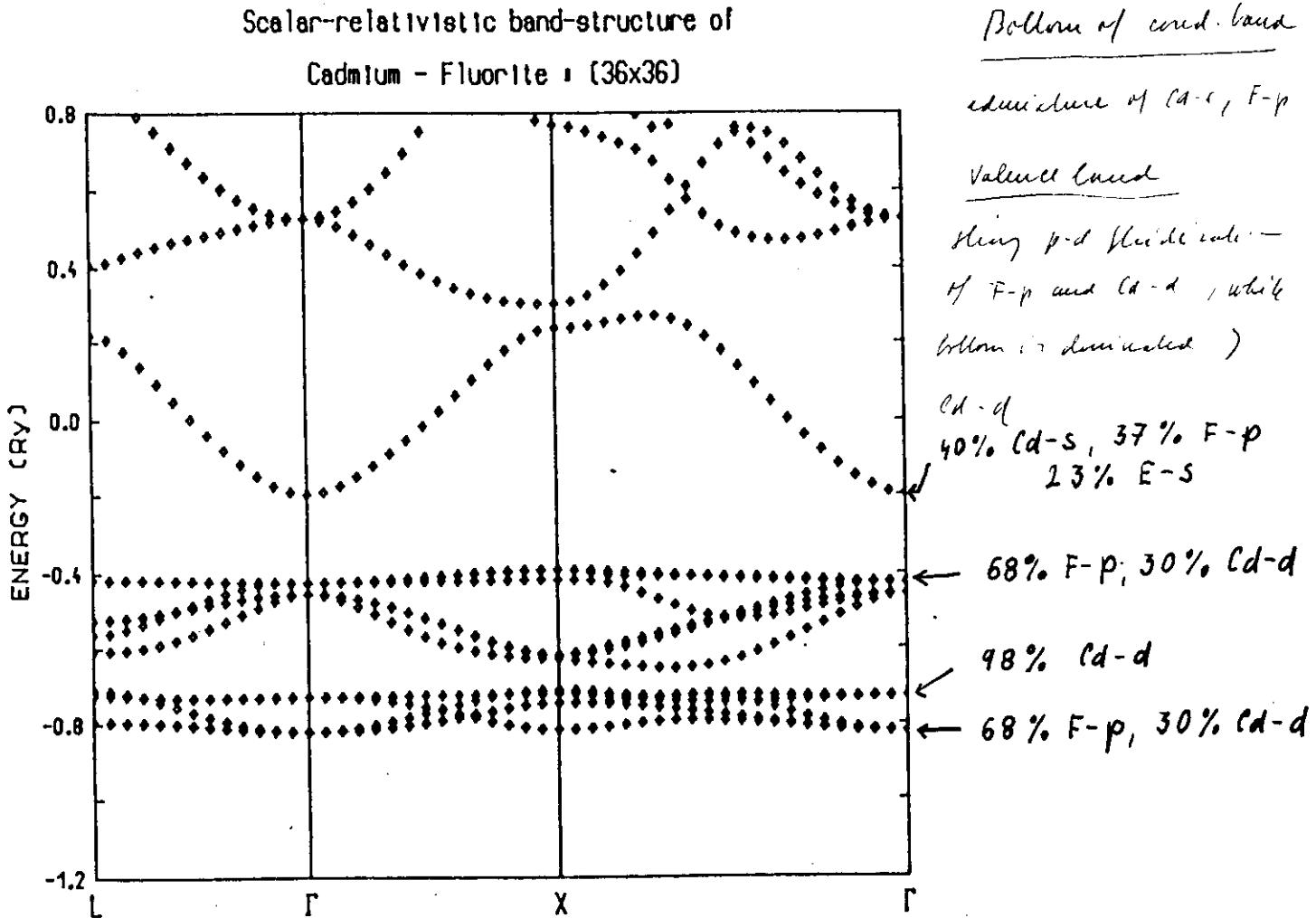
Scalar-relativistic band-structure of  
Cadmium - Telluride : (36x36) - i.e. (lower) are



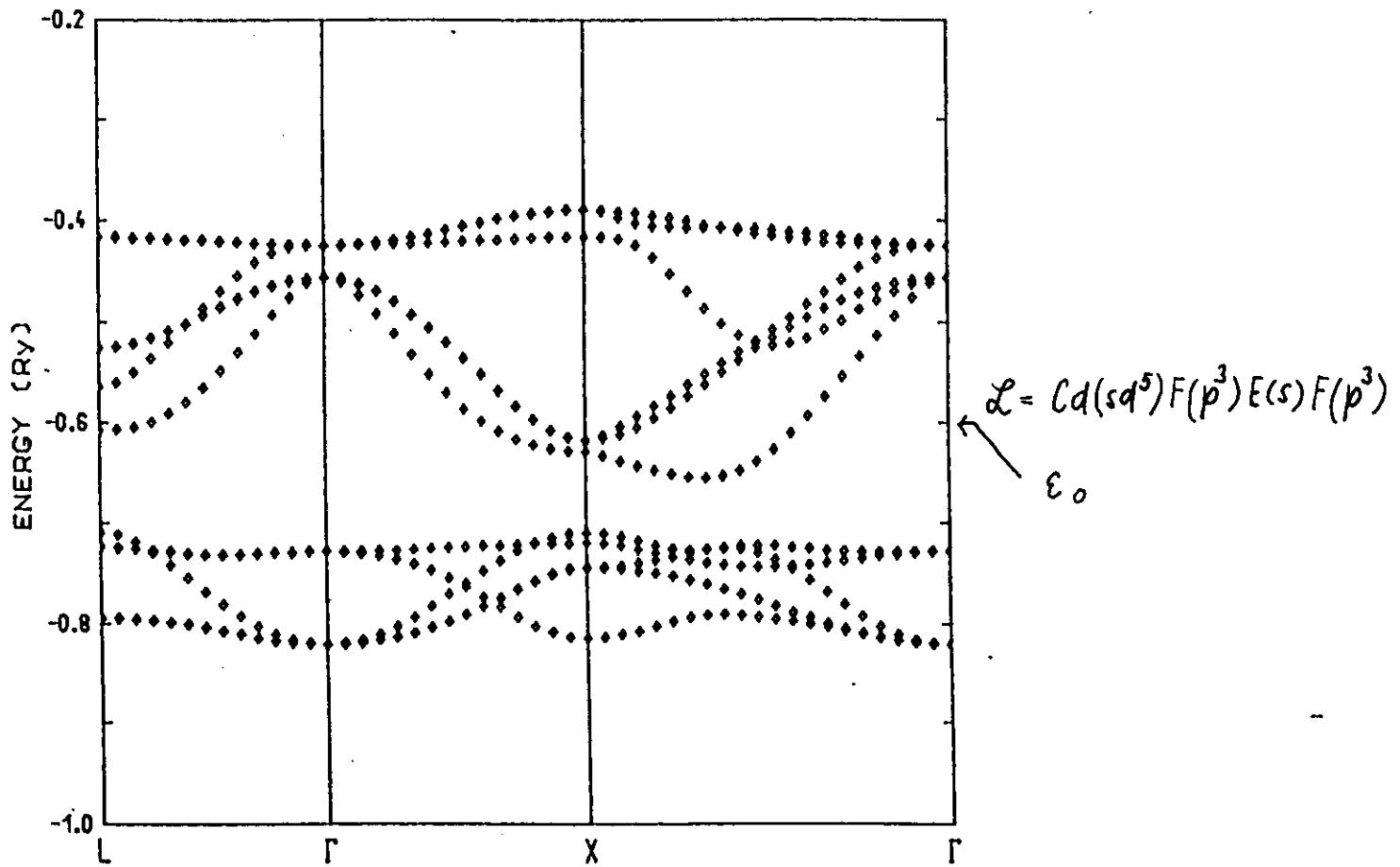
$\mathcal{L} : Cd(d^5) Te(s)$

Scalar-relativistic band-structure of  
Cadmium - Telluride : (6x6),  $\epsilon_0 = -0.9$  Ry

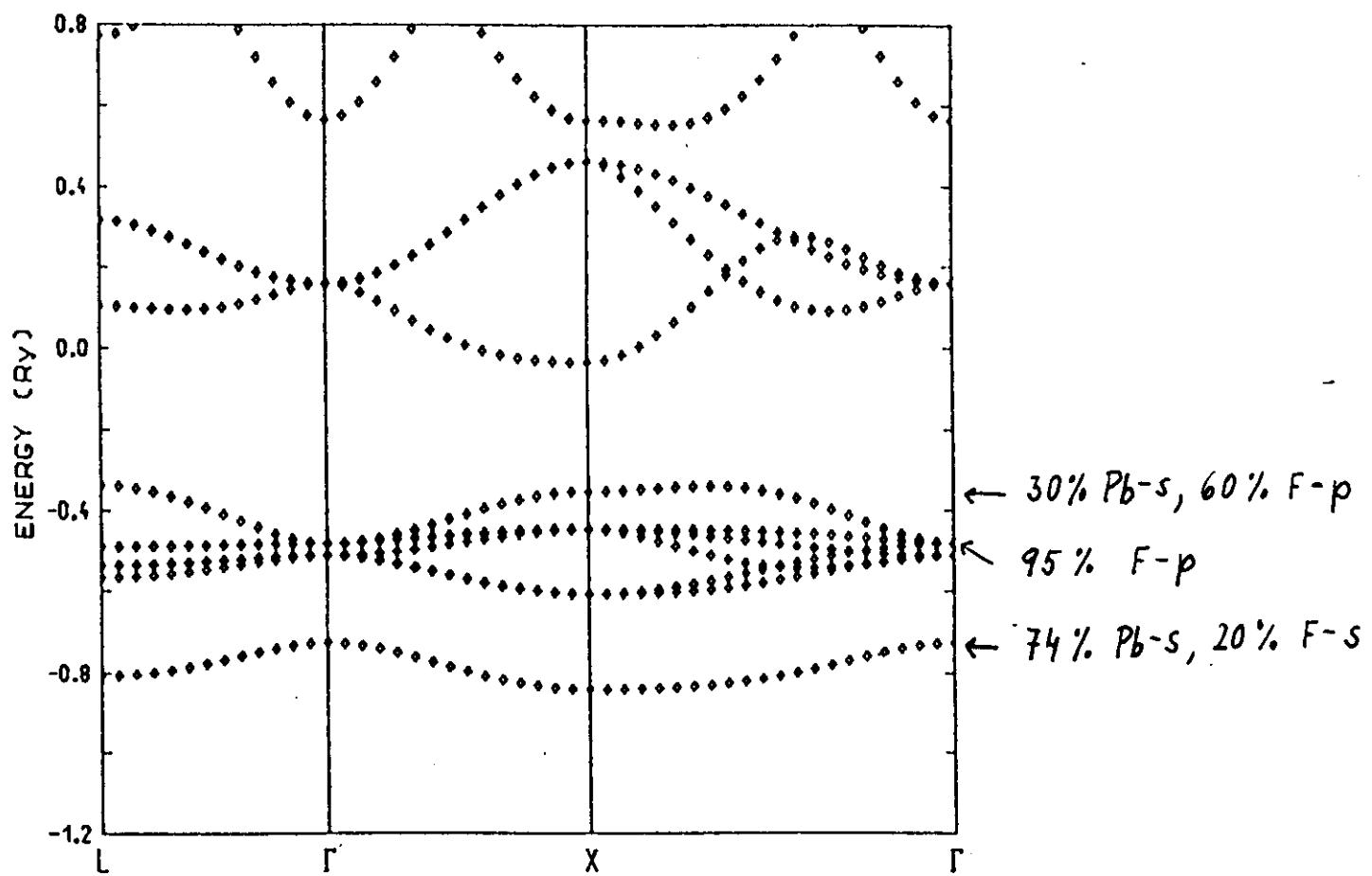




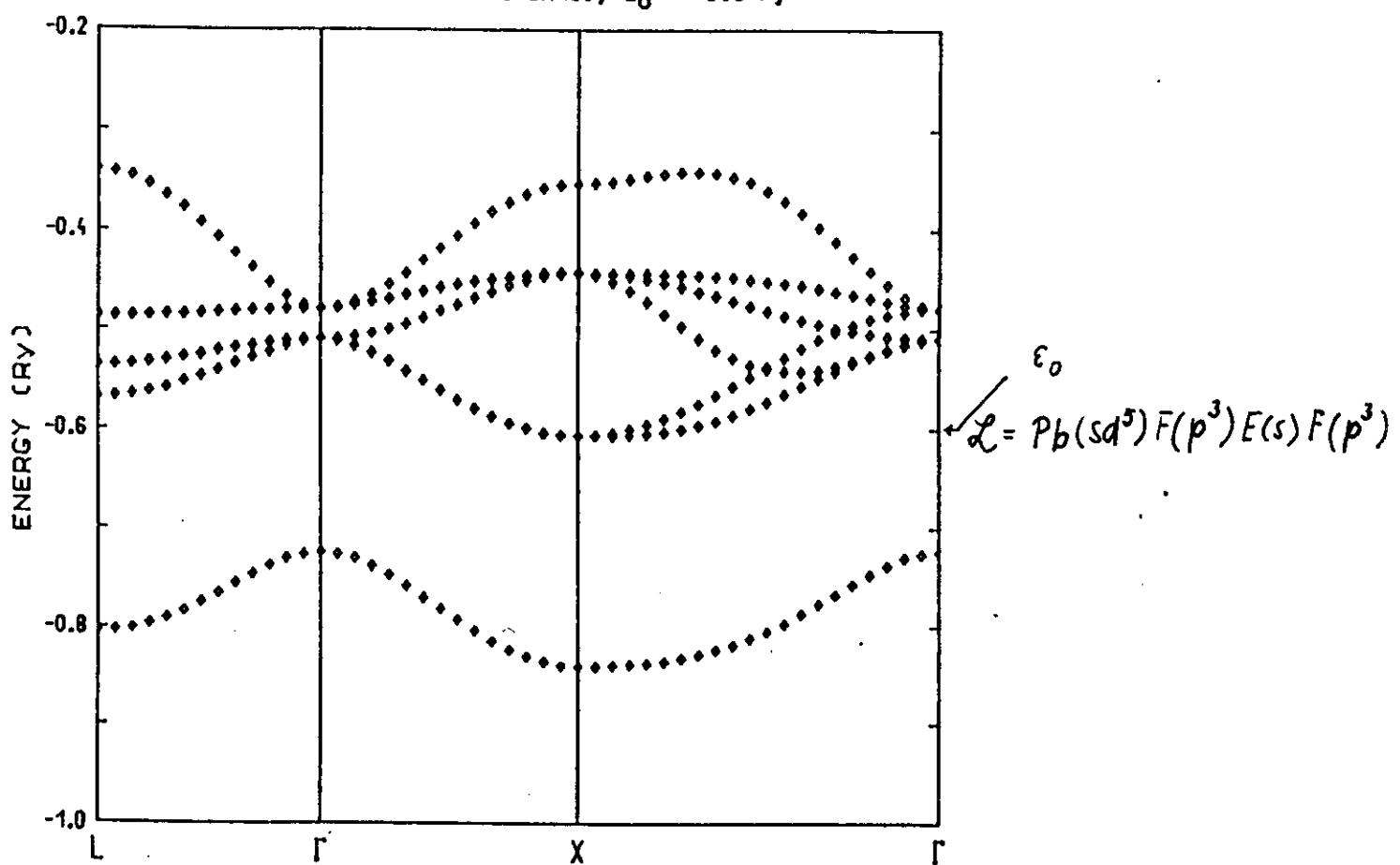
Scalar-relativistic band-structure of  
Cadmium - Fluorite : (13x13),  $\epsilon_0 = -0.6$  Ry



Scalar-relativistic band-structure of  
Lead - Fluorite : (36x36)



Scalar-relativistic band-structure of  
Lead - Fluorite : (13x13),  $\epsilon_0 = -0.6$  Ry

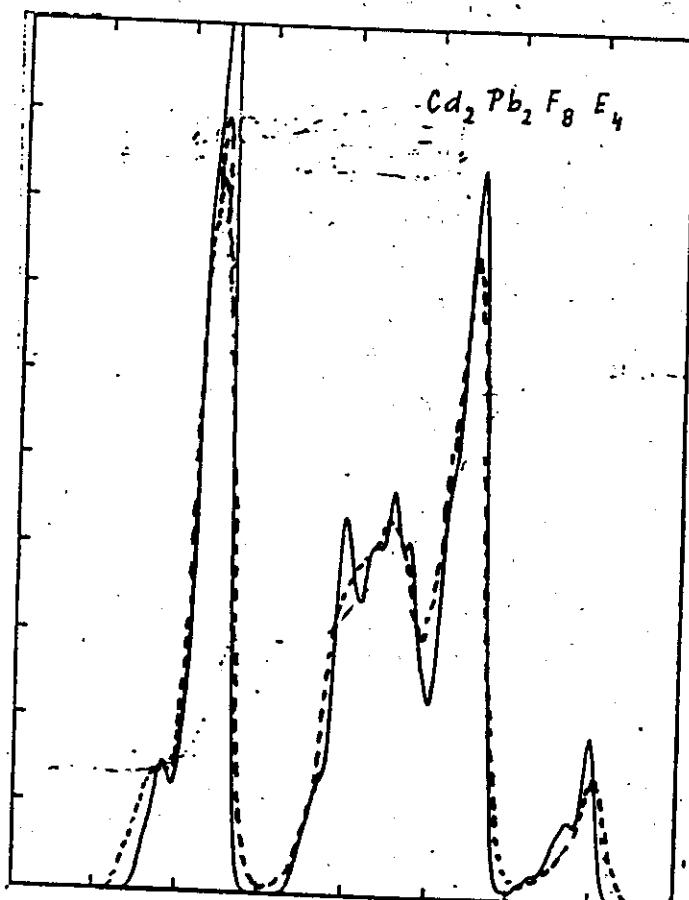


LMTO CPA :

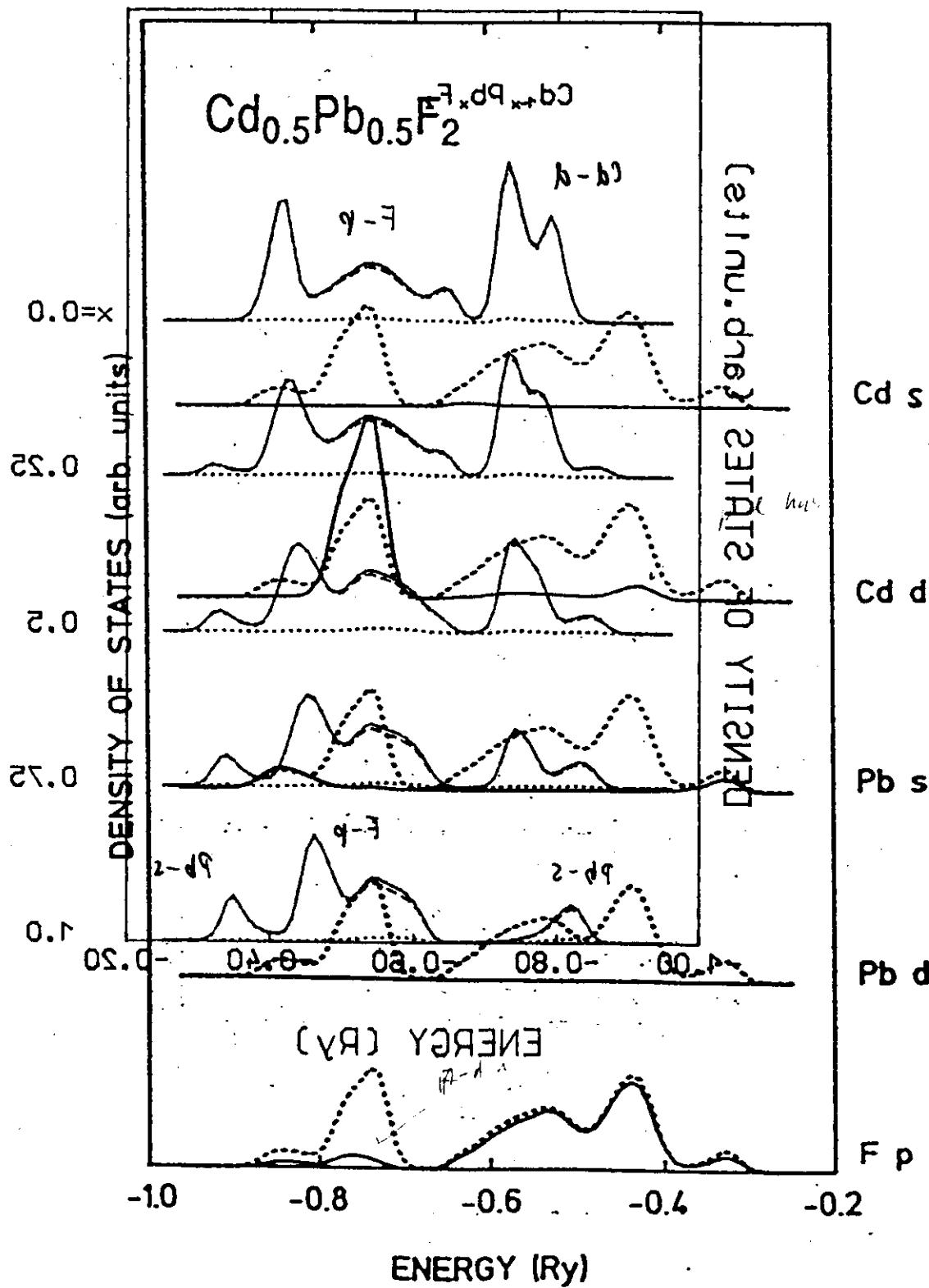
---  $Cd_{0.5} Pb_{0.5} F_2$

LMTO supercell :

—  $Cd_2 Pb_2 F_8 E_4$



$\sqrt{3} \times \sqrt{3}$  model,  $e_0 = -0.6$  Ry



$Cd_{0.5}Pb_{0.5}F_2$

