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I.C.T.P., P.O. BOX 586, 34100 TRIESTE, ITALY, CABLE CENTRATOM TRIESTE



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**Second Workshop on
Three-Dimensional Modelling of Seismic Waves
Generation, Propagation and their Inversion**

7 - 18 November 1994

*Earthquake Faulting:
The Inverse Problem*

S. Das

University of Oxford
Department of Earth Sciences
United Kingdom

References

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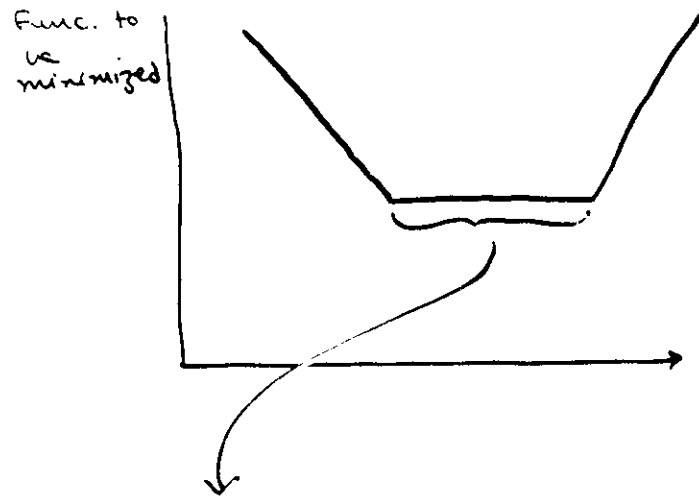
Definition of some common terms used in inverse theory.

STABILITY is defined as the property that a solution is insensitive to small random errors in the data.

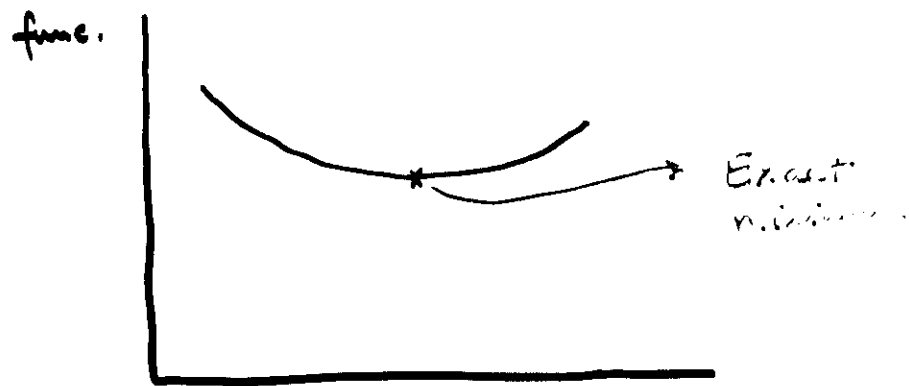
ROBUSTNESS is the property that a solution is insensitive w.r.t. a small # of big error (outliers) in the data.

NON-UNIQUENESS is the property that more than one solution (almost) equally well-fitting the data exists.

A pathological example of non-uniqueness.



Every point here is a valid minimum as shown by the same is.



In geophysics, the data itself contains noise + the models are themselves approximations.

The inverse problem of obtaining the details of the rupture process from an analysis of teleseismically recorded seismograms is an UNSTABLE problem.

Note that the problem is unstable even in the imaginary case of a continuous distribution of seismic stations over the surface of the earth. From the computational point of view, the instability is equivalent to non-uniqueness of the solution.

The real situation is even worse because the # of stations with appropriate records is very limited (10-20 stations even today - cf. 1989 Macquarie Ridge eq.)

Hence, one needs some additional constraints on the soln. (i.e. in addition to the requirement of fitting the seismograms). These constraints should be based on the physics of the earthquake faulting problem.

But knowledge of this physics is rather limited.

Possible physical constraints

- ① limit on fracture propagation speed
- ② less physically founded: Direction of slip vector on fault is parallel to direction of the average stress drop $\rightarrow$ leads to the "no back-slip" constraint.
- ③ Max. slip rate on fault can be constrained based on fracture mechanics results from lab. expts. on rocks.

In order for a particular slip distribution to be an acceptable solution to the inverse problem it must satisfy the following three conditions.

1. The solution must explain the data.
2. The solution must be physically reasonable.
3. If more than one solution fits the data equally well, additional information must be supplied to uniquely define which solution is being obtained and such constraints should be explicitly stated and not hidden in the method of inversion.

Displacement at a station is given by

$$u_k(\bar{x}, t_1) = \int_0^{t_1} dt \iint_{\Sigma} K_{ik}(\bar{x}_1, \bar{x}; t_1, t) a_i(\bar{x}, t) dS$$

where $u_k \rightarrow k$ th comp. of displacement at $(\bar{x}_1, t_1)$

$K_{ik} \rightarrow$ impulse response of medium

$a_i(\bar{x}, t) \rightarrow$ slip at $(\bar{x}, t)$ on fault

$\Sigma \rightarrow$ fault area.

After some simple algebra

(to move derivative from K to a in convoluted)

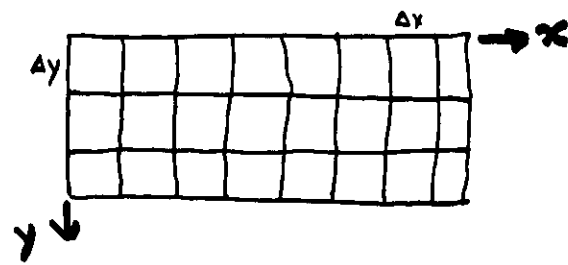
we get

$$S_j(t_1) = \int_0^{t_1} dt \iint_{\Sigma} W_j(\xi, t_1 - t) \dot{a}(\xi, t) dS$$

$S_j(t_1) \rightarrow$ Seismogram at j th stn. at time t_1 $\rightarrow$ DATA

$W_j \rightarrow$ impulse response; direction of slip is taken to be constant + $\parallel$ to the applied stress direction $\rightarrow$ KNOWN

$\dot{a} \rightarrow$ SLIP RATE on fault (UNKNOWN)



Fault is discretized.

In each cell, $\dot{a}$ is a linear function

W_j is discretized by integrating over cells

The source time function is discretized by taking a fixed time step Δt and assuming slip rate varies linearly with time.

Then, in discrete form we get the system of linear eqns

$$Ax \approx b \rightarrow \text{data from seismograms}$$

$\swarrow$ discretized impulse response W_j $\downarrow$ unknown slip rates $\dot{a}$

of eqns = (# of grids along x).
 (# of grids along y).
 (# of source time steps)

CONSTRAINTS

1. No back-slip i.e. $\bar{x} \geq 0$ always
2. Causality condn: grids not allowed to slip until first wave from point of rupture initiation arrives at it
(STRONG CAUSALITY CONSTRAINT)
3. Seismic moment condn.

The seismic moment resulting from the solution must be consistent with that obtained from long-period data (e.g. the CMT solution M_0 or geodetically obtained moment).

$\sum c_i x_i \approx M_0$, summed over fault with c_i containing rigidity modulus, etc.

So we need to solve a

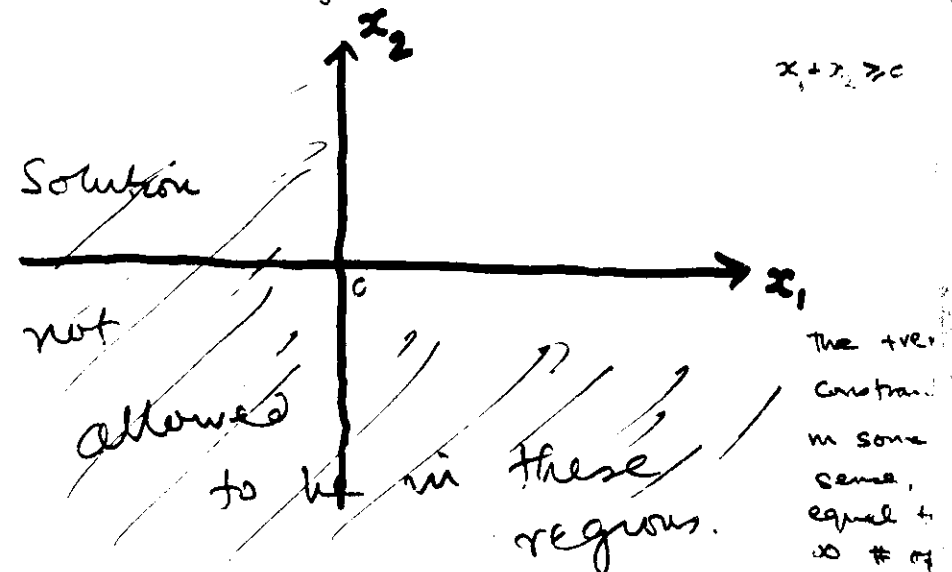
CONSTRAINED linear set of equations.

Please forget, at this point, EVERYTHING you ever learned about solving un constrained linear systems as they are quite IRRELEVANT.

One example: In un constrained systems

$Ax=b$, the # of equations should be $\geq$ # of unknowns.

this is not relevant to the present problem as the constraints provide additional conditions e.g.



Let $\vec{r} = \vec{b} - A\vec{x}$ be the vector of residuals, which we have to minimize. In order to use the linear-programming approach which is very convenient for solving constrained systems, we shall minimize the L_1 -norm of $\vec{r}$:

i.e. minimize $(|r_1| + |r_2| + \dots + |r_m|)$
where $m = \#$ of eqns.

The method of soln. is described in standard text books:

Inverse problem theory by A. Tsvankova

Numerical recipes by Press et al.

1. No Bock-slip condn. is found to be essential (Explain why).

2. Seismic moment constraint may be needed if data is very poor. For the 1986 Andu. Is. eq. (Mw 8.1) it was needed. For the 1989 Macquarie eq., the soln. gave results consistent with CMT moment & the constraint did not need to be applied.

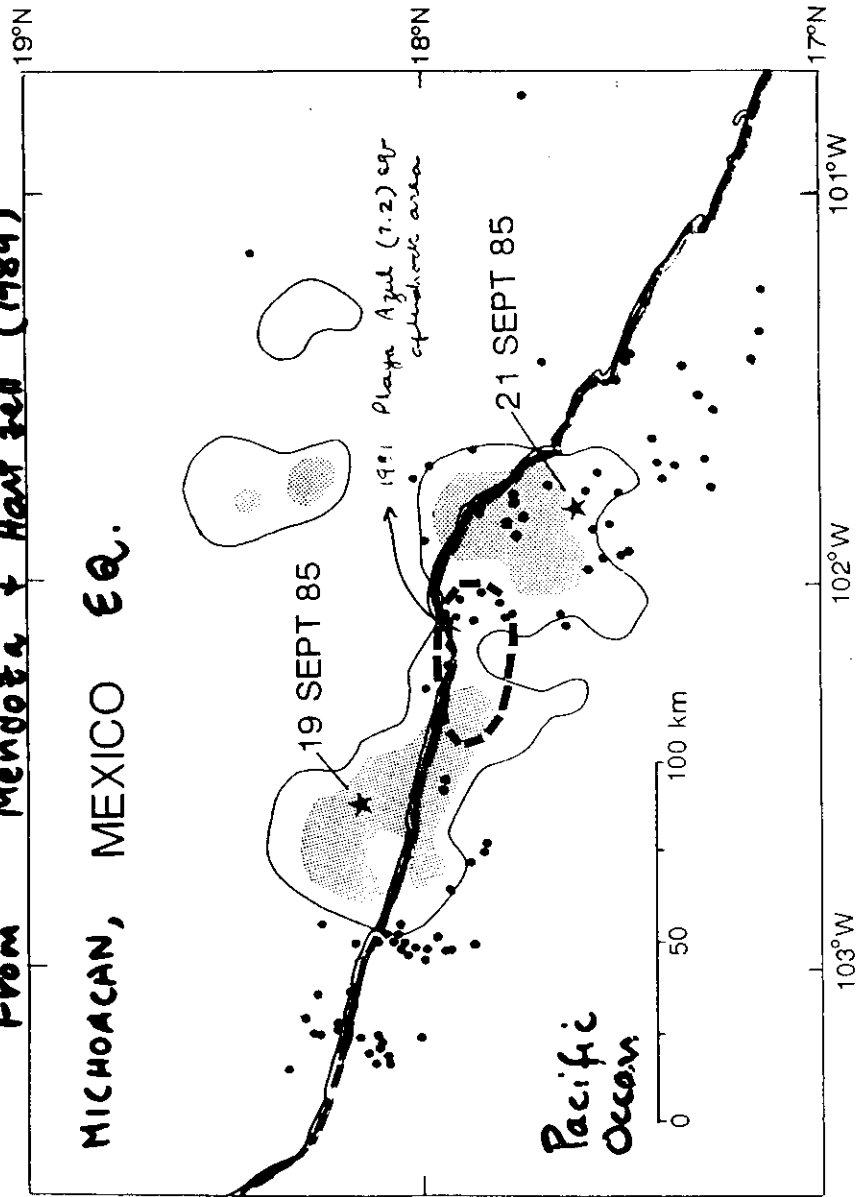
In order to be confident about physical conclusions relating to the fault rupture process, such as the relation between areas of high moment release and aftershock locations, we must examine the reliability of the moment release pattern obtained. (The reliability of the aftershock locations is a separate issue). This problem has not been sufficiently studied for the problem of determination of the earthquake slip rate history and distribution on a fault from inversion of observed seismograms. For the problem of determination of earth structure from seismic observations, the problem has been discussed in the now-classic papers of Backus and Gilbert (1968, 1970) and the same ideas are applicable here.

The inverse problem is unstable and in order to stabilize it one has to introduce stabilizing constraints. This can be done either by reducing the number of unknown being solved for by making a priori assumptions about the solution or by introducing additional constraints based on physical considerations. Das and Kostrov (1990) have discussed why the latter approach is preferable. Once the solution has been stabilized, the question of resolution arises and the well-known trade-off between stability and resolution (Backus and Gilbert, 1968) has to be considered. That is, stabilizing the solution too much may result in poor resolution.

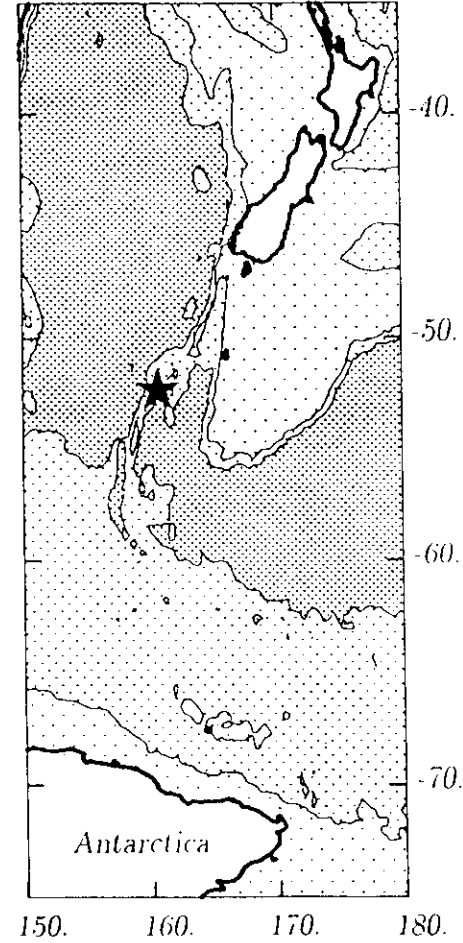
In the present context, the question comes down to this: by how much can we displace the areas of high and low moment and by how much can we change their areal extent and the amount of moment released and yet obtain almost equally good fits to the seismograms. We shall stabilize the solution by introducing additional constraints and examine their effect on the solution.

From Mendoza & Hart 200 (1989)

①



The 1989 Macquarie Ridge eq.
($M_w = 8.2$)





$\Delta x = 10 \text{ km}$ fault length = 450 km

$\Delta \tau = 3 \text{ secs}$ (source step time interval)

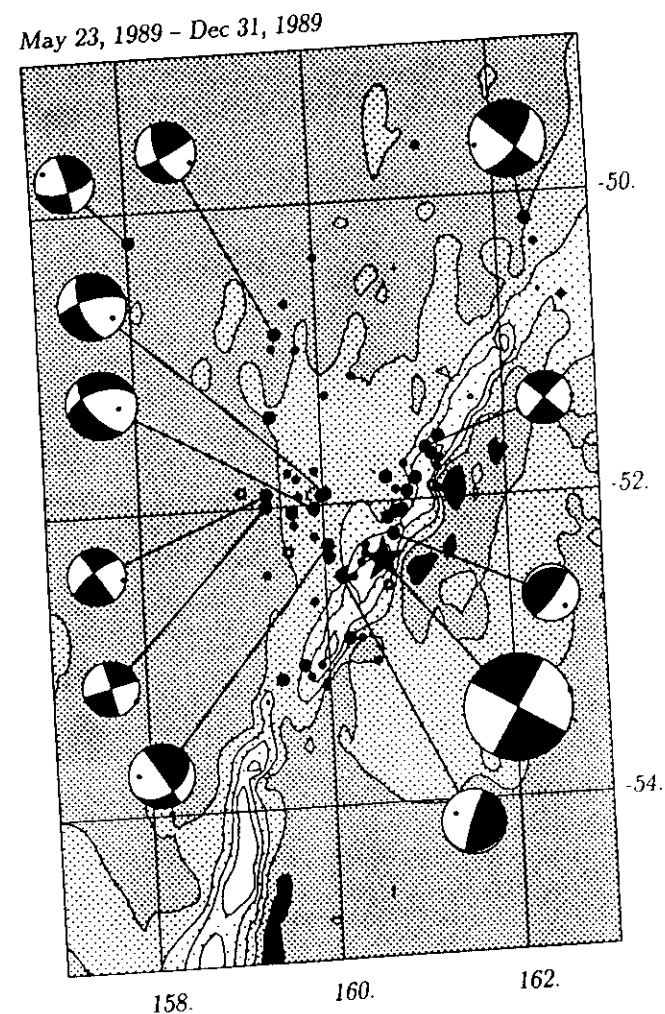
Source time = 63 secs.

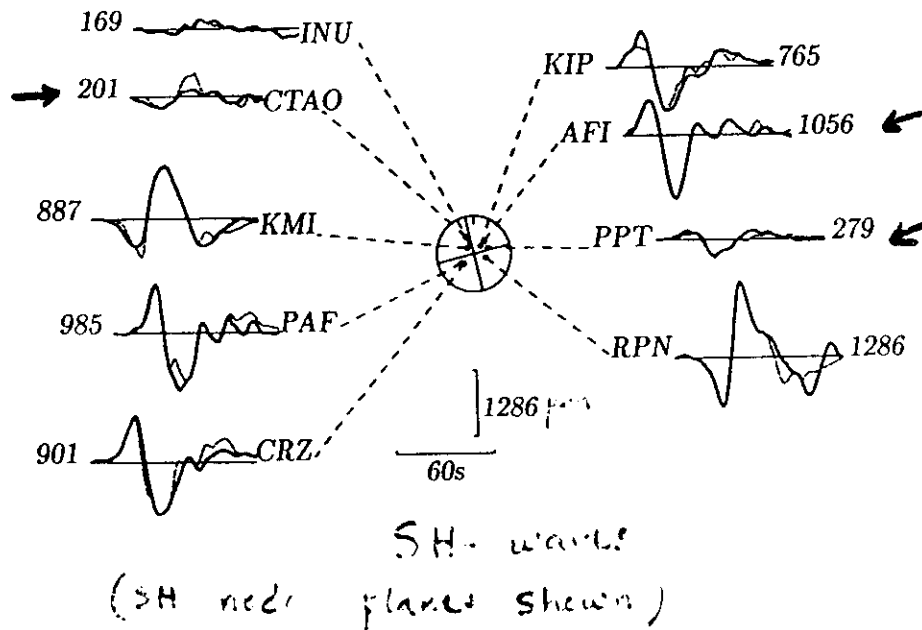
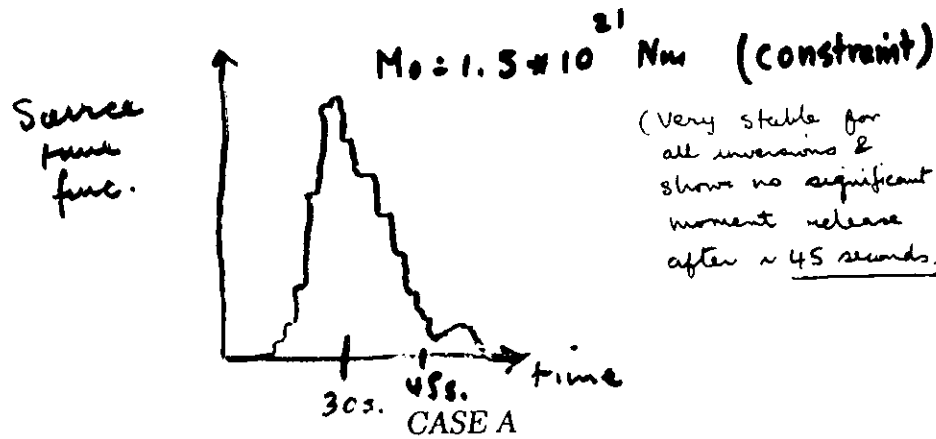
We find that even with a large # of unknowns, the amplitude at some stations are always pretty fit (though the fit is fit very well).

This suggests that the instrument responses at some stns. may have some inconsistencies. In order to overcome this, we include a station scaling factor for the problem stations + solve for these scale factors as part of the soln.

It was found that the scale factor was often close to 2. or $\frac{1}{2}$ suggesting a missing scale factor in the instrument response !

A weak causality condn. is used, viz. we assume that slip rate is zero at a cell and time step which would produce a signal before the first arrival at any station from the hypocentral grid.



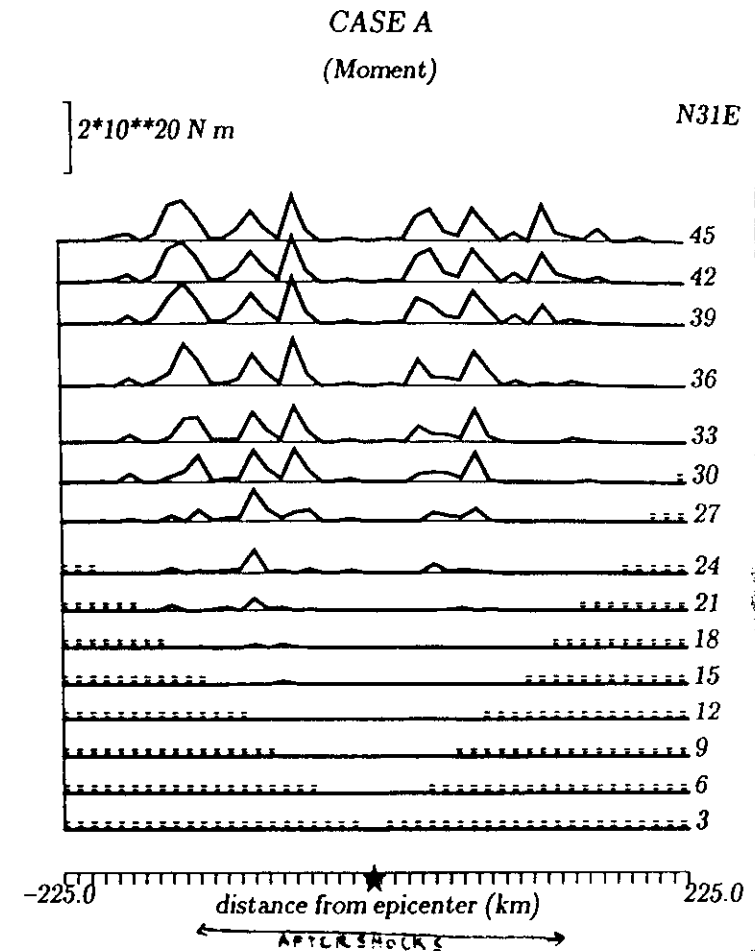


L_1 error of fit = .28 (I use $\sqrt{\quad}$ in the error of fit formula whereas most people find $\sqrt{\quad}$ so that in other people's error = .28² = .08 !)

Fig 5

Note: Hypocentral region is a region of low moment release.

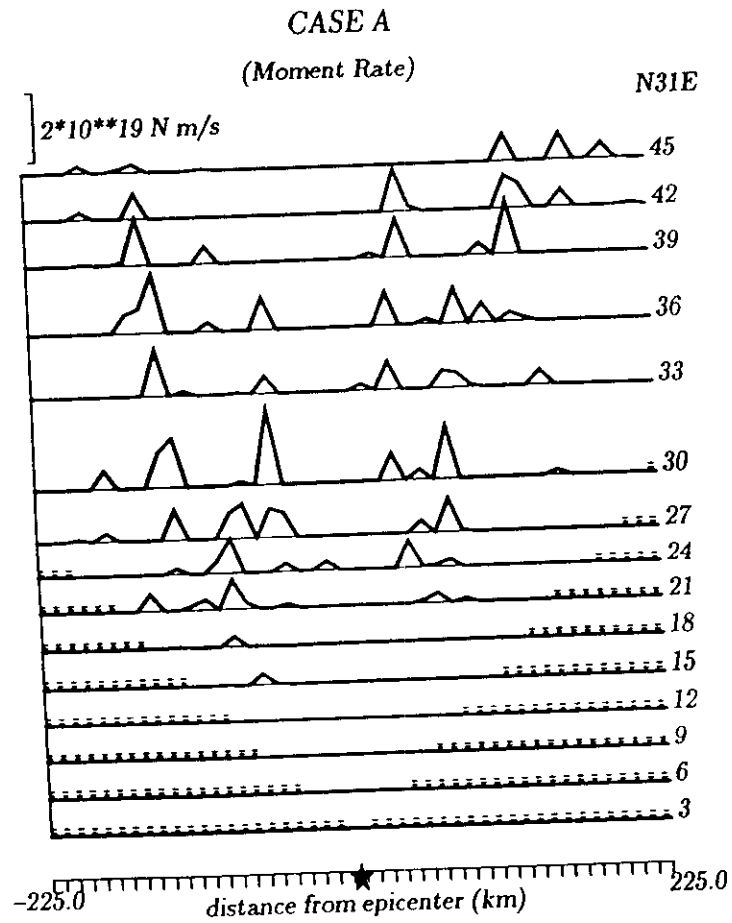
Slightly more moment released in the SW direction from the hypocenter than in NE direction.



|| Moment spreads along fault BEYOND area delineated by aftershocks!

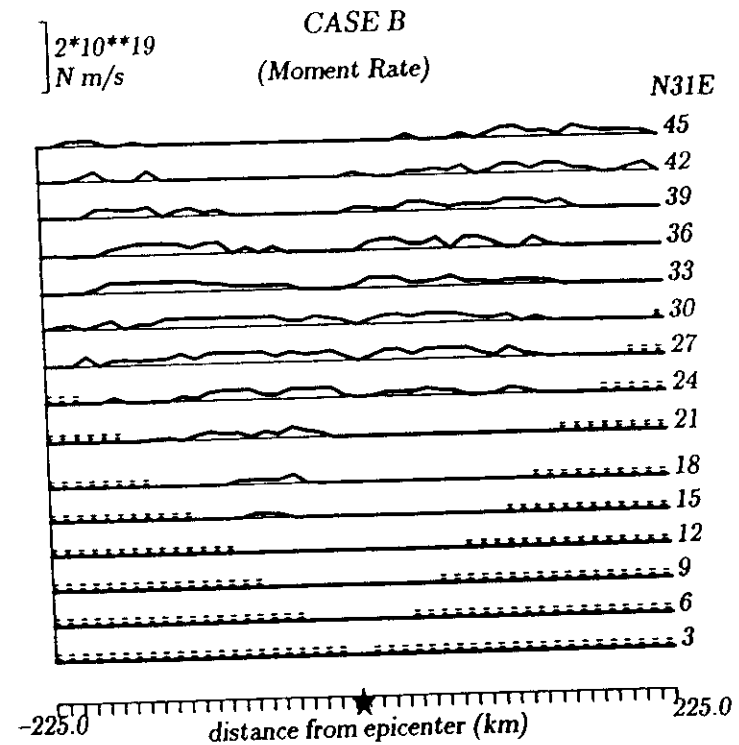
No simple rupture propagation

Looks like "asperities" breaking but is this an artefact?



Acausal regions (constraint)

Solution constrained to have most uniform moment rate distribution, with the error of misfit being allowed to increase by 10% of previous case (A).



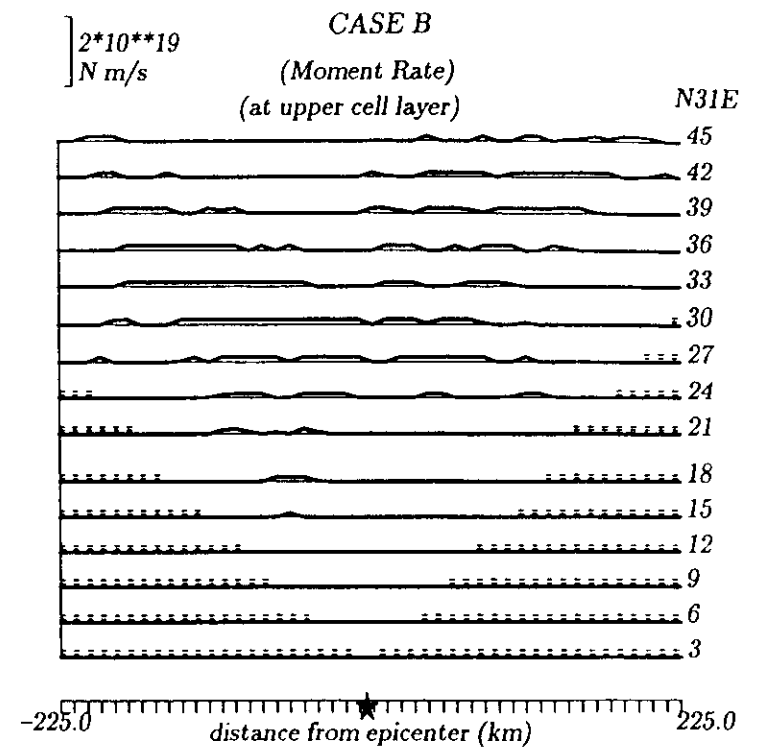
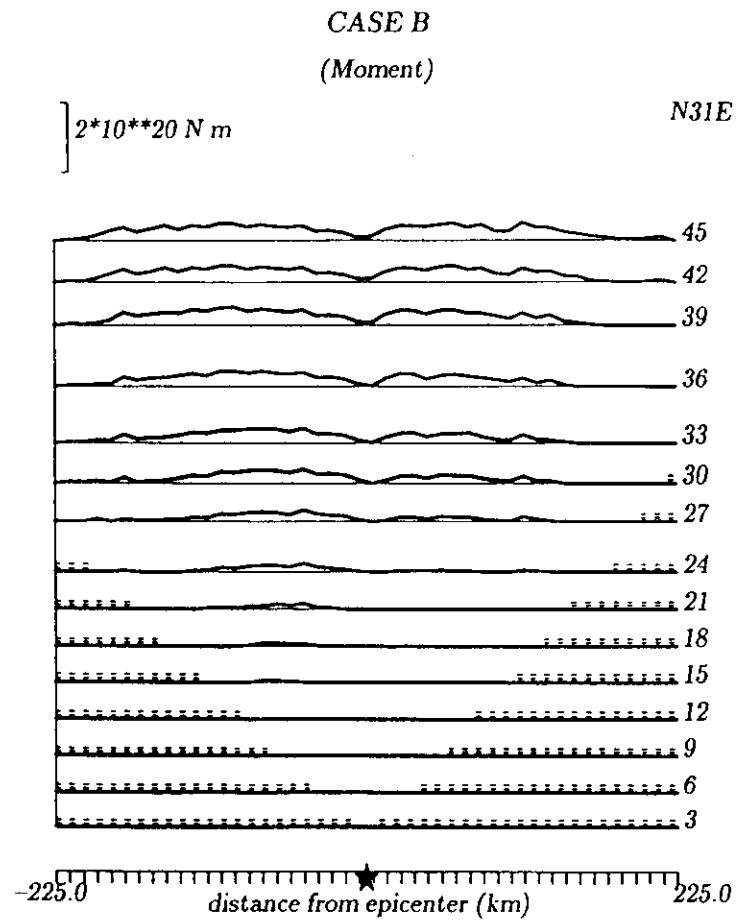


Fig
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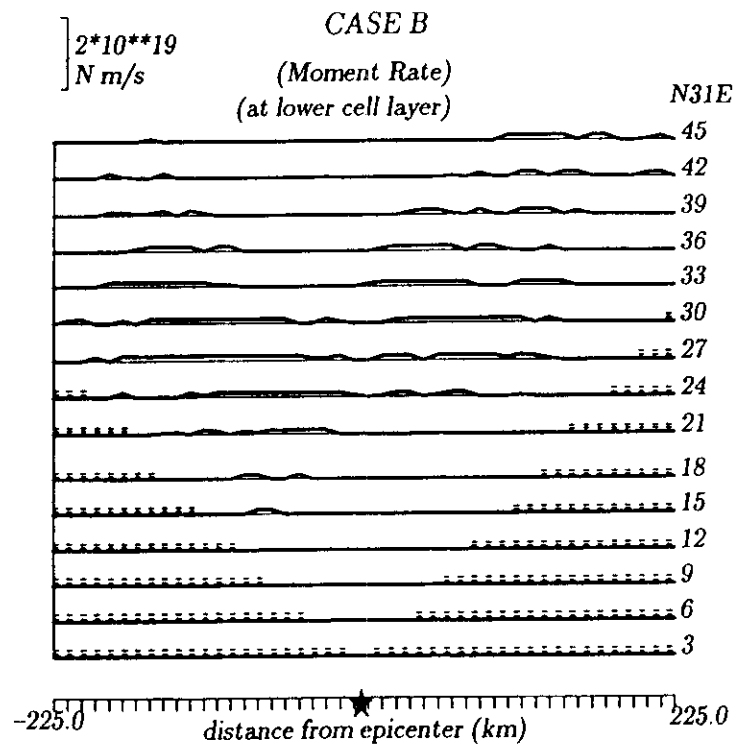
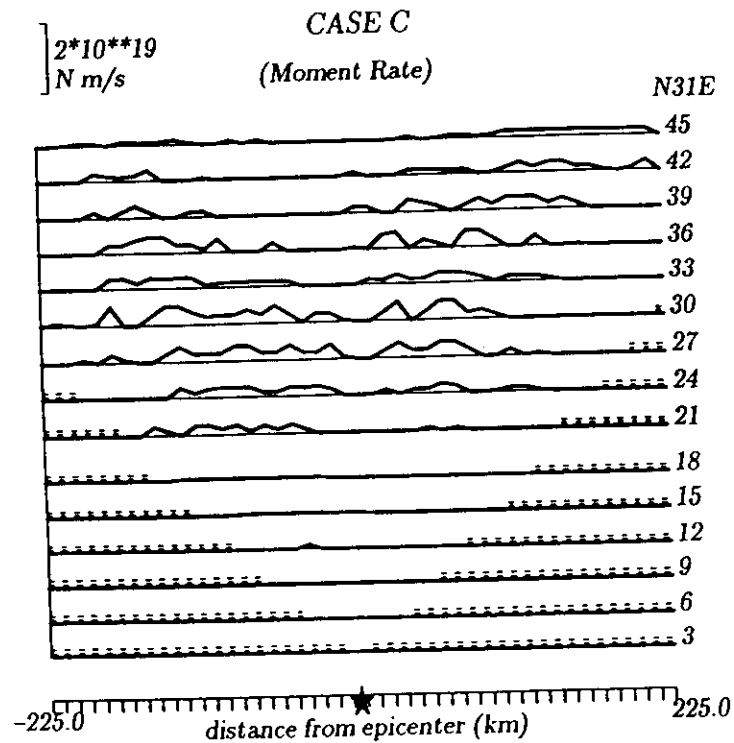


Fig
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Case B shows that the distribution of moment rate is still more uniform (with moment rates over the fault) having comparable values — unlike what is expected for a propagating crack, say, where much higher values of slip (/moment) rates would be seen near the leading rupture edge).

Thus, the soln. cannot be made completely uniform + still satisfy the data.

Solution constrained to be uniform
in space only.



Note very little moment release at
last few time steps.

Fig
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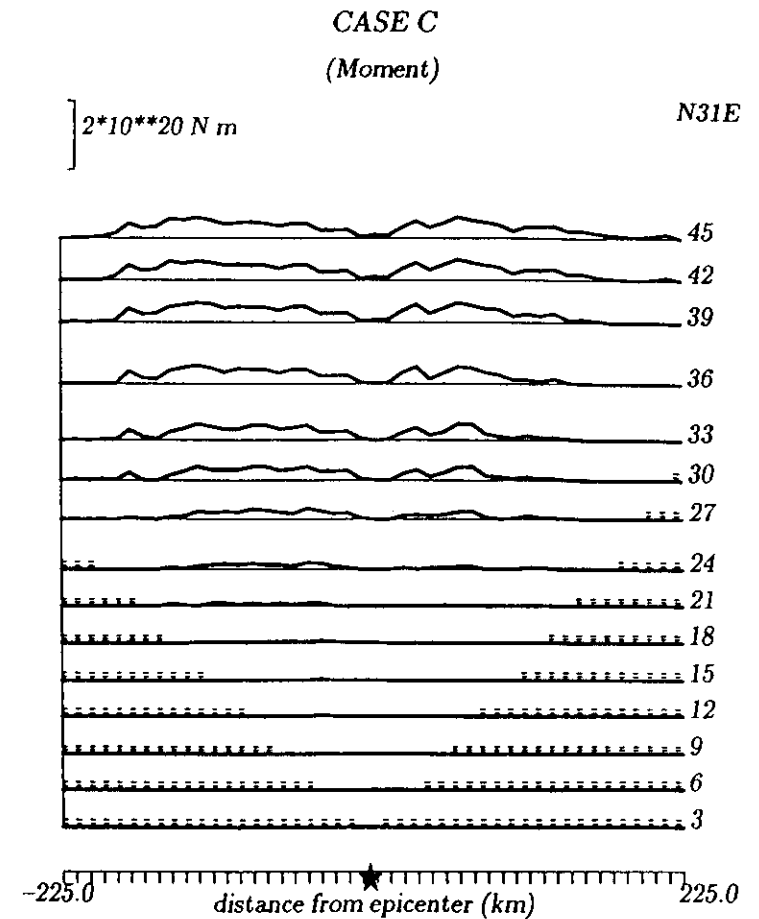
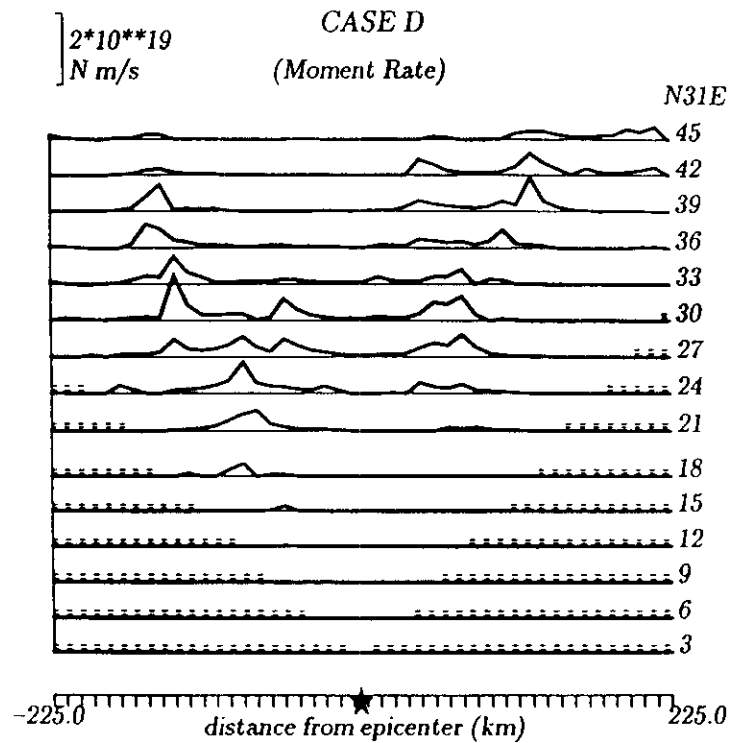


Fig 16

Solution constrained to be as smooth as possible (+ yet satisfy data) along fault strike — i.e. we minimize the sum of moduli of the second difference of slip rate along strike.



Soln. is smoother than that in Case A.

Fig

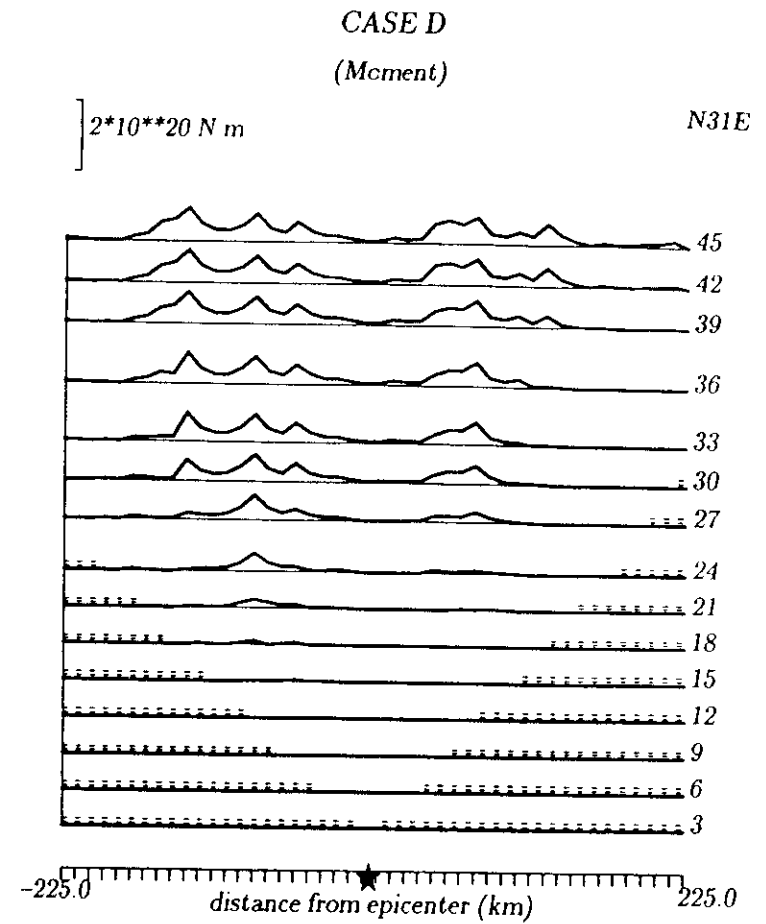
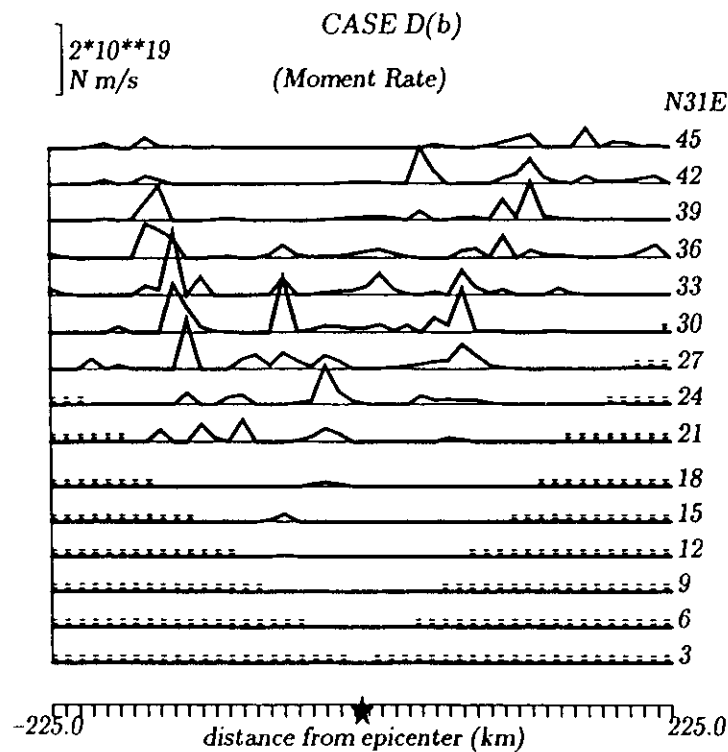


Fig 18

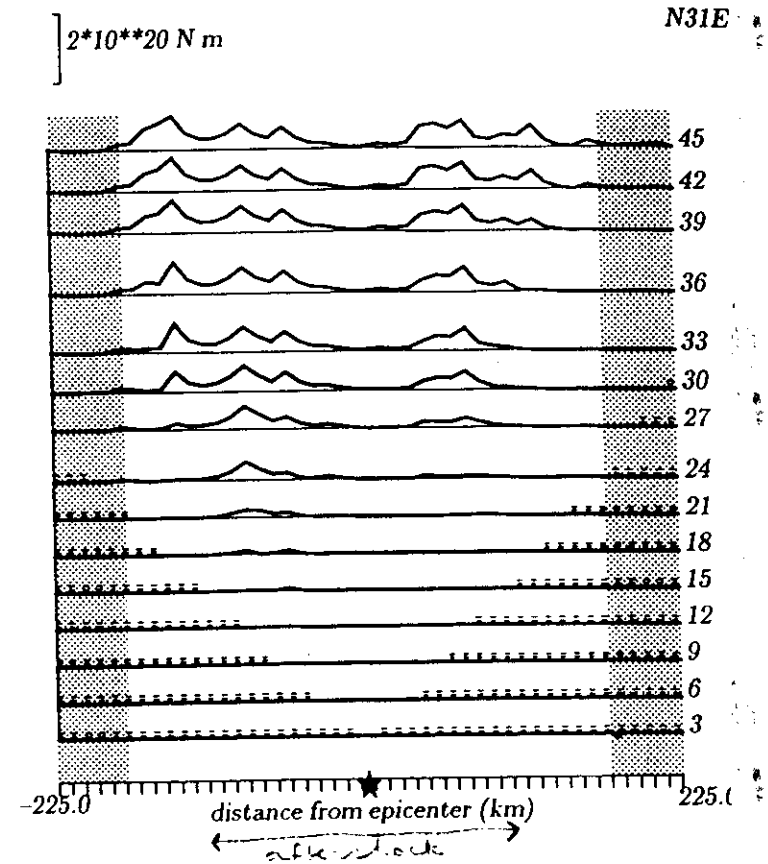
Example of incomplete optimisation



Search for the smoothest soln.
was stopped too soon without
reaching the minimum & shows that
the smooth soln. indeed
was not reached!

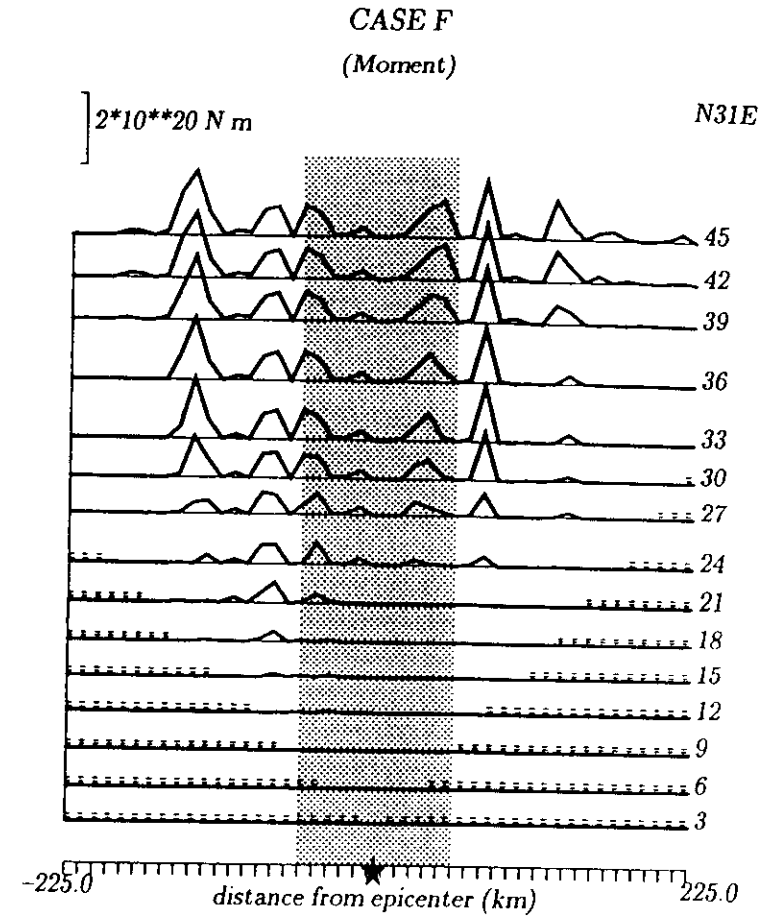
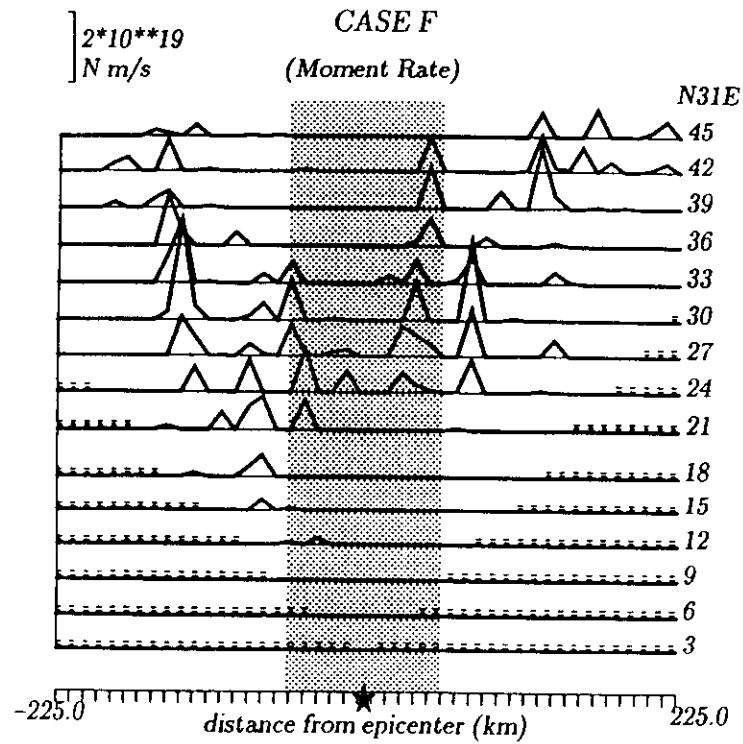
To check if the moment on the
aftershock zone is truly there, we minimize the
moment release in the shaded areas, after obtaining
the smoothest soln. (previous Case D).

CASE E
(Moment)



Result: We are unable to remove
moment outside aftershock area & still
fit seismic groups well. We even increase
tolerance of fit to 30% (instead of 21
10%) & were still unable to suppress
moment outside aftershock area.

to increase moment at 11 central grids along strike.

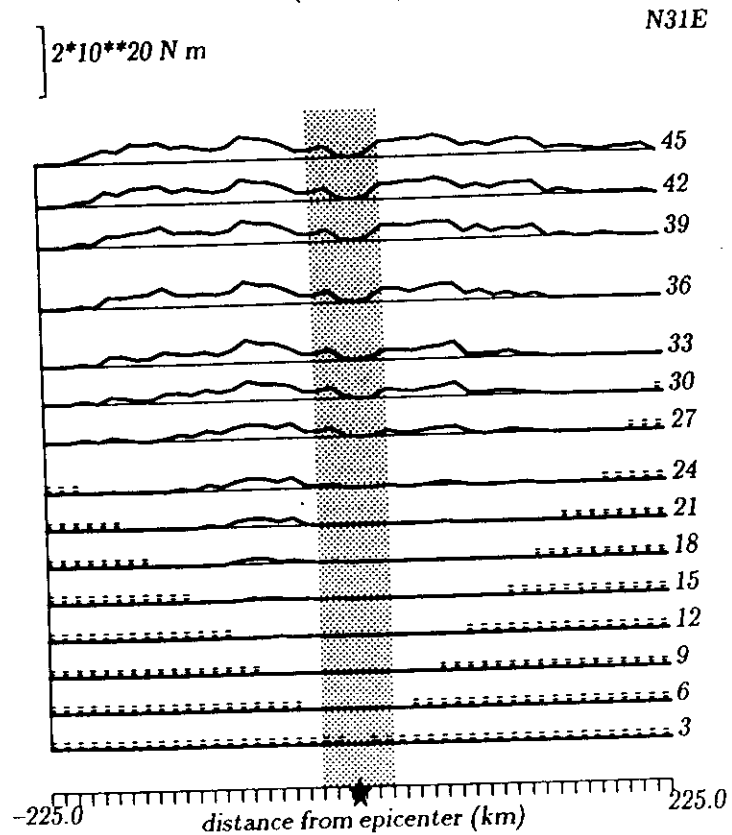


Result: We do increase moment
in central area (comp. Case D)
but hypocentral area is still
region of low
moment release.

Fig 23

Try to maximise moment in central
5 grids but start from most
uniform soln. (case c).

CASE G
(Moment)



again: unable to remove moment
outside aftershock area!
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