



INTERNATIONAL ATOMIC ENERGY AGENCY
UNITED NATIONS EDUCATIONAL, SCIENTIFIC AND CULTURAL ORGANIZATION
INTERNATIONAL CENTRE FOR THEORETICAL PHYSICS
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**FOURTH ICTP-URSI-ITU(BDT) COLLEGE ON RADIOPROPAGATION:
Propagation, Informatics and Radiocommunication System Planning**

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Miramare - Trieste, Italy

Biological Effects of Electromagnetic Fields

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Biological Effects of Electromagnetic Fields

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2. Emission and coupling parameters
3. Dielectric behaviour of biological materials
4. Dosimetry
5. Biological effects
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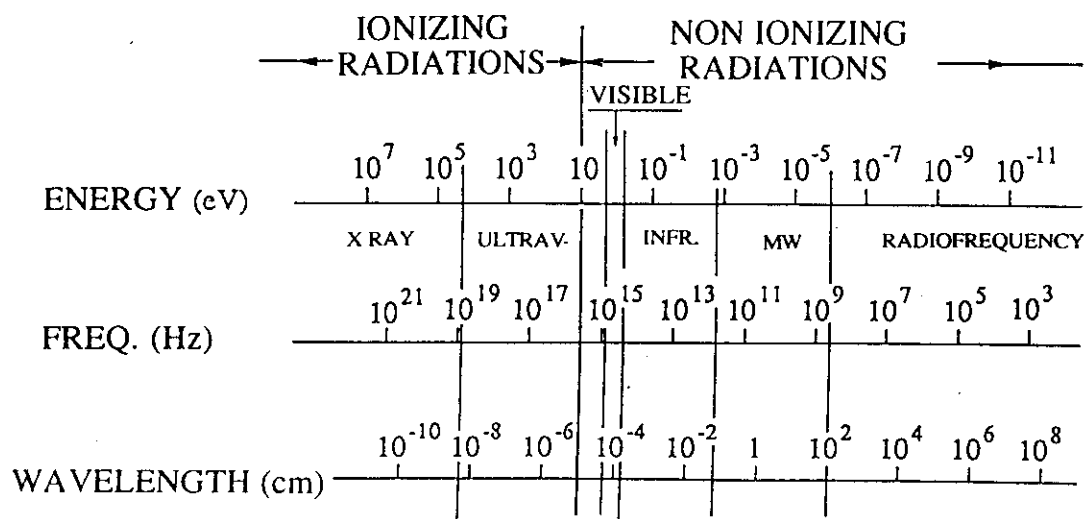


INTRODUCTION

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EM SPECTRUM CHARACTERISTICS



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TYPICAL APPLICATIONS

FREQUENCY	TYPICAL APPLICATIONS	WORKERS	GENERAL PUBLIC
50 Hz	power line carrier radionavigation radiolocation		rural people
< 3 MHz	AM broadcast amateur industrial RF heating	car, ship, air industry	all

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TYPICAL APPLICATIONS

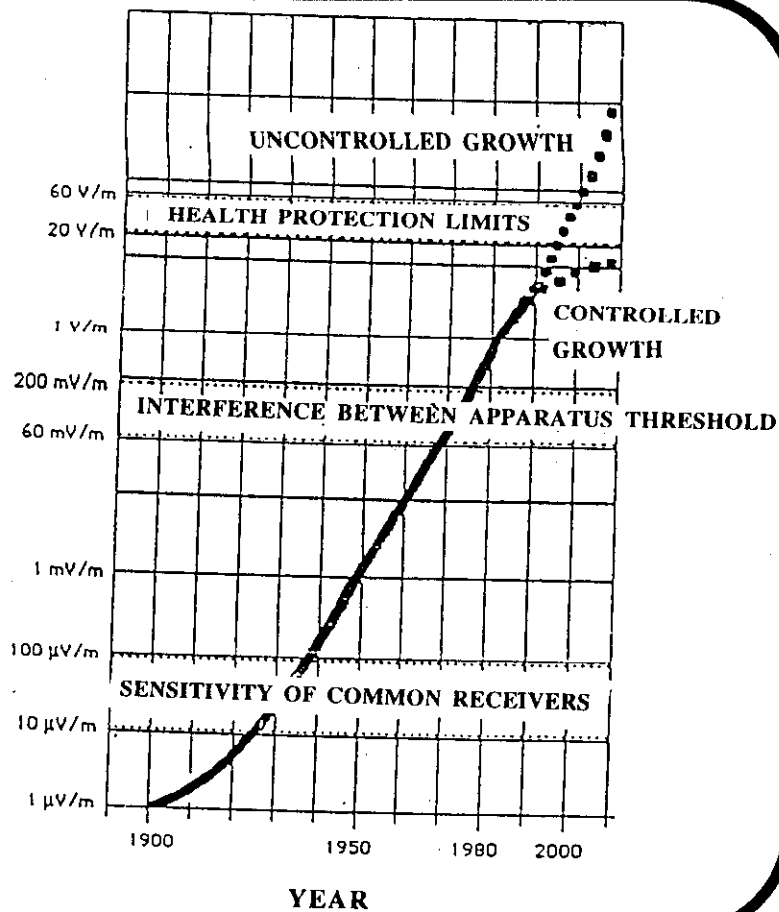
FREQUENCY	TYPICAL APPLICATIONS	WORKERS	GENERAL PUBLIC
3 - 300 MHz	AM, FM broadcast, VHF - TV, citizens band, amateur industrial RF equipment medical applications	chemistry and machinery industry medical and paramedical	all patients
300-3000 MHz (0.3 - 3 GHz) MICROWAVES	mobile communications short range broadcast UHF-TV, citizens band microwave ovens industrial heating medical applications	food industry MW industry medical and paramedical	mobile phone users housewives,
3 - 300 GHz MICROWAVES	satellite communications radar	military researcher	rural people

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FIELDS IN URBAN AREAS

FIELDS IN URBAN AREAS



YEAR

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EMISSION AND COUPLING PARAMETERS

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BASIC DEFINITIONS

EMISSION (from a source)

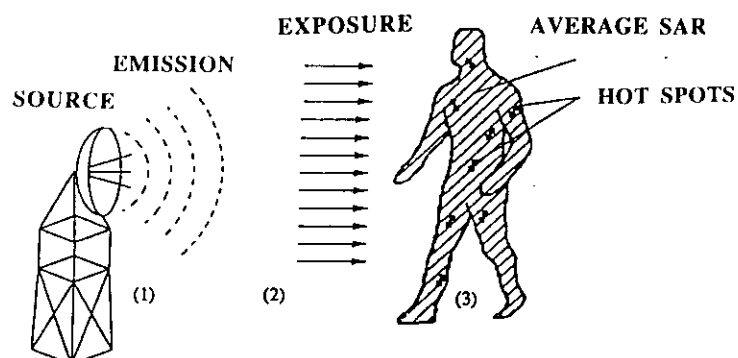
EXPOSURE (of a subject)

ABSORPTION (in the subject)

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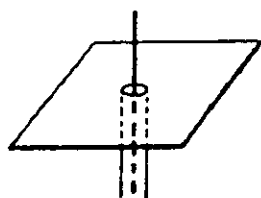
PICTURE OF THE SITUATION



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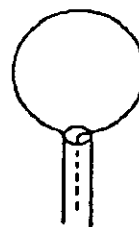
EM SOURCES



MONOPOLE



DIPOLE



LOOP

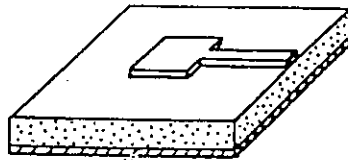
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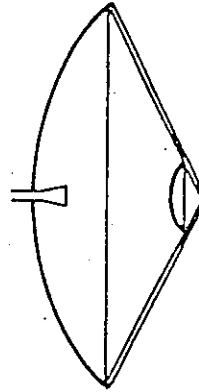
EM SOURCES



HORN



MICROSTRIP PATCH ANTENNA

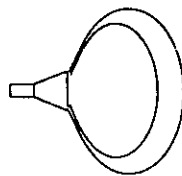


REFLECTOR

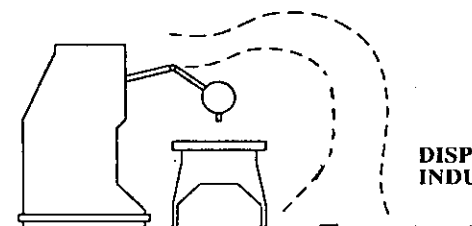
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KINDS OF EMISSIONS



FOCUSED EMISSION

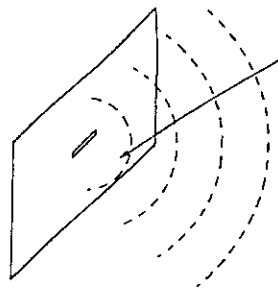


DISPERSION FROM
INDUSTRIAL EQUIPMENT

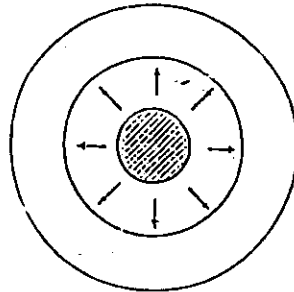
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KINDS OF EMISSIONS



EMISSION FROM
AN APERTURE



OMNIDIRECTIONAL EMISSION

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EXPOSURE OF THE SUBJECT

The exposure is evaluated
in the body-absent situation

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CONSTITUTIVE RELATION

$$\mathbf{D} = \epsilon_0 \epsilon^* \mathbf{E}$$

TOTAL CURRENT

$$\mathbf{J} = g \mathbf{E} + j\omega \mathbf{D} = (g + j\omega\epsilon_0\epsilon^*) \mathbf{E}$$

$$\begin{aligned} \mathbf{J} &= [g + j\omega\epsilon_0(\epsilon' - j\epsilon'')] \mathbf{E} = \\ &= (g + \omega\epsilon_0\epsilon'') \mathbf{E} + j\omega\epsilon_0\epsilon' \mathbf{E} \end{aligned}$$

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RMS VALUE FOR A VECTOR QUANTITY

$$\mathbf{A} = a_x \mathbf{x}_0 + a_y \mathbf{y}_0 + a_z \mathbf{z}_0$$

$$a_{x \text{ eff}} = \sqrt{\frac{1}{T} \int_0^T a_x^2 dt}$$

$$a_{y \text{ eff}} = \sqrt{\frac{1}{T} \int_0^T a_y^2 dt}$$

$$a_{z \text{ eff}} = \sqrt{\frac{1}{T} \int_0^T a_z^2 dt}$$

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RMS VALUE FOR A VECTOR QUANTITY

$$A_{\text{eff}} = \sqrt{\frac{1}{T} \int_0^T \mathbf{A} \cdot \mathbf{A} \, dt} = \sqrt{\frac{1}{T} \int_0^T (a_x^2 + a_y^2 + a_z^2) \, dt} = \\ = \sqrt{a_{x \text{ eff}}^2 + a_{y \text{ eff}}^2 + a_{z \text{ eff}}^2}$$

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EXPOSURE PARAMETERS

E_{rms} (V/m) rms value of the time harmonic EM field of period T

$$E_{\text{rms}}^2 = \frac{1}{T} \int_0^T |\mathcal{E}(t)|^2 \, dt$$

H_{rms} (A/m) rms value of the time harmonic EM field of period T

$$H_{\text{rms}}^2 = \frac{1}{T} \int_0^T |\mathcal{H}(t)|^2 \, dt$$

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EXPOSURE PARAMETERS

S (W/m²) Time average Power density

$$S = \frac{1}{T} \int_0^T S(t) dt$$

For a TEM plane wave

$$S = H_{\text{rms}} \cdot E_{\text{rms}} = E_{\text{rms}}^2 / 377 = H_{\text{rms}}^2 \cdot 377$$

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EXPOSURE CONDITIONS

Reactive field

radiative field

Near-field

Far-field $\left\{ \begin{array}{l} r \geq \lambda \\ r \geq \frac{D^2}{\lambda} \end{array} \right.$

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ABSORPTION PARAMETERS

SAR (W/Kg) Specific absorption Rate

Absorbed power, per unit of mass

FULL BODY AVERAGE SAR (W/Kg)

Total Absorbed power divided by the total mass of the body

LOCAL SAR (W/Kg)

Absorbed power in an infinitesimal volume at a point in the body divided by the mass of the infinitesimal volume

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SAR EVALUATION

$$SAR = \frac{\omega \epsilon_0 \epsilon'' E_{in}^2}{\rho} = \frac{4.186 \rho c \Delta T}{\Delta t} \text{ (W/kg)}$$

E_{in} = magnitude of the internal field (V/m)RMS

ρ = mass density (kg/m³)

ϵ_0 = free space permittivity (F/m)

ϵ'' = imaginary part of the relative complex permittivity

c = specific heat (cal/Kg °C)

ΔT = temperature variation (°C)

Δt = exposure time (s)

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INDUCED CURRENT DENSITY

$$J_{in} = \sqrt{g^2 + (\omega \epsilon_0 \epsilon')^2} E_{in}$$

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FOOT CURRENT

Total current crossing the feet toward the ground

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DIELECTRIC BEHAVIOUR OF BIOLOGICAL MATERIALS

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DIELECTRIC POLARIZATION

$$\mathbf{P} = \mathbf{P}_1 + \mathbf{P}_2$$

\mathbf{P} = dielectric polarization

\mathbf{P}_1 = atomic and electronic displacement

\mathbf{P}_2 = dipolar reorientation

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DEBYE THEORY

$$\mathbf{P}_1 = \epsilon_0 \chi_1 \mathbf{E}$$

$$\frac{d\mathbf{P}_2}{dt} = \frac{1}{\tau} (\epsilon_0 \chi_2 \mathbf{E} - \mathbf{P}_2)$$

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DEBYE THEORY

For a time harmonic field

$$\mathcal{A}(t) = \text{Real}(\mathbf{E} e^{j\omega t})$$

$$\mathbf{P} = \mathbf{P}_1 + \mathbf{P}_2 = \epsilon_0 \left(\chi_1 + \frac{\chi_2}{1 + j\omega\tau} \right) \mathbf{E}$$

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COMPLEX PERMITTIVITY

$$\mathbf{D} = \epsilon_0 \mathbf{E} + \mathbf{P} = \epsilon_0 \epsilon^* \mathbf{E}$$

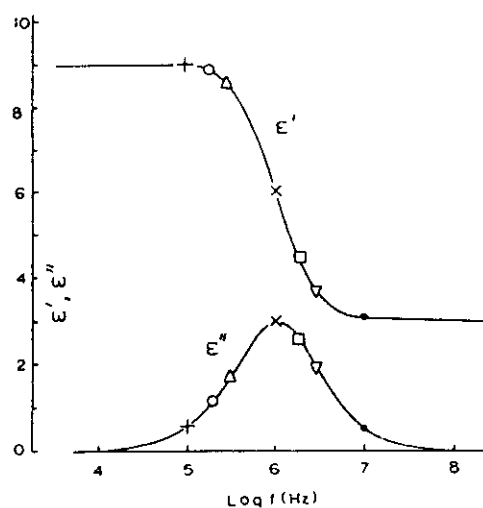
$$\epsilon^* = \epsilon' - j \epsilon''$$

$$\epsilon' = \epsilon_\infty + \frac{\epsilon_s - \epsilon_\infty}{1 + (\omega\tau)^2} \quad \epsilon'' = \frac{(\epsilon_s - \epsilon_\infty) \omega\tau}{1 + (\omega\tau)^2}$$

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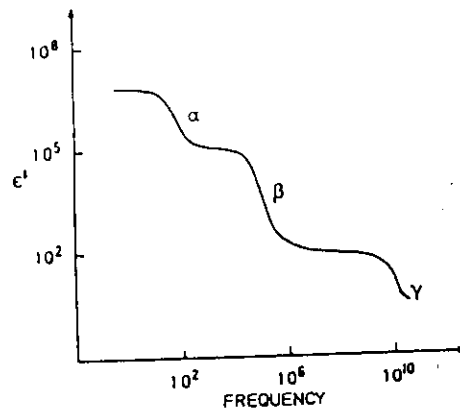
DEBYE-TYPE RELAXATION PROCESS



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TYPICAL TISSUE



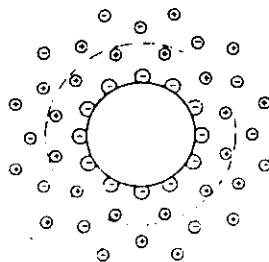
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α - RELAXATION

Counter-ions diffusion polarization

Is associated with the electrical double layer surrounding cells

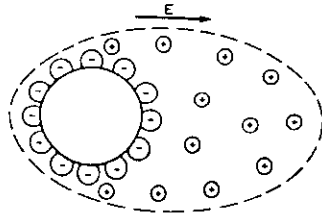


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α - RELAXATION

Polarization results from the net displacement of counterions as a result of the influence of an external electric field



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α - RELAXATION

the relative permittivity may reach values greater than 10^4 at frequencies below 1 kHz.

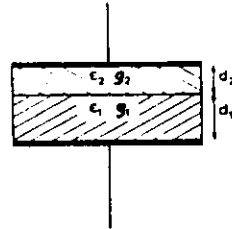
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β - RELAXATION

Interfacial polarization (Maxwell-Wagner effect)

Is associated with the charging of the interfaces within the material



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β - RELAXATION

with $g_2 \approx 0$

$$C_1 = A\epsilon_0 \frac{\left(\epsilon_1 - j \frac{g_1}{\omega\epsilon_0}\right)}{d_1}$$

$$C_2 = \frac{A\epsilon_0\epsilon_2}{d_2}$$

$$C = \frac{C_1 C_2}{C_1 + C_2} = \frac{A\epsilon_0\epsilon_2\left(\epsilon_1 - j \frac{g_1}{\omega\epsilon_0}\right)}{d_2\left(\epsilon_1 - j \frac{g_1}{\omega\epsilon_0}\right) + d_1\epsilon_2}$$

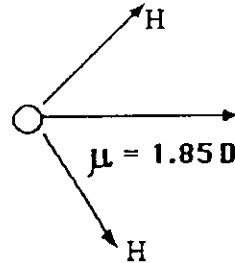
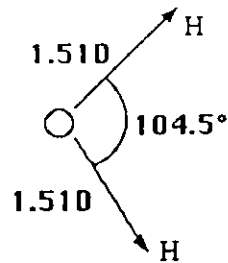
$$\epsilon_s = \epsilon_2 \frac{d}{d_2} \quad \epsilon_\infty = \frac{\epsilon_1\epsilon_2 d}{d_2\epsilon_1 + d_1\epsilon_2}$$

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γ - RELAXATION

Dipolar polarization of free water is associated with the partial orientation of permanent dipoles



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γ - RELAXATION

Considering an ensemble of independent dipoles with moment μ , the externally imposed Electric field will exert a torque of magnitude $\mu E \sin\theta$, where θ is the angle between the dipole and the field.

At equilibrium

$$\langle \cos\theta \rangle \approx \frac{\mu E}{3 K T}$$

$$P \approx \frac{N \mu^2 E}{3 K T}$$

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γ - RELAXATION

After application of the E-field, the ensemble of dipoles approach equilibrium after a time

$$\tau \approx \frac{4 \pi \eta a^3}{K T} \quad (\text{Stokes law})$$

a = radius of the dipole

η = viscosity of the medium

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γ - RELAXATION

For pure water

$$\tau \approx 8 \text{ ps}$$

corresponding to a relaxation frequency of

$$f_r = \frac{1}{2 \pi \tau} \approx 20 \text{ GHz} \quad (\text{at } 25^\circ \text{C})$$

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DOSIMETRY

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DOSIMETRY

$f < 30 \text{ MHz}$

Analytical techniques

Empirical formulation

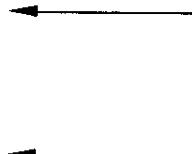
Numerical techniques

$30 \text{ MHz} < f < 300 \text{ MHz}$

Numerical techniques

$f > 300 \text{ MHz}$

Analytical techniques



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$$f < 30 \text{ MHz}$$

Wavelength of the incident radiation large
compared to the size of the body



ANALYTICAL TECHNIQUES

quasi-static solution of Maxwell's equations

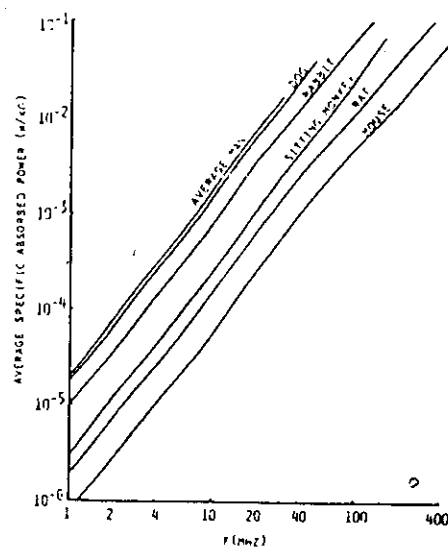
spheroidal and ellipsoidal models of man

useful information about the average SAR

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AVERAGE SAR

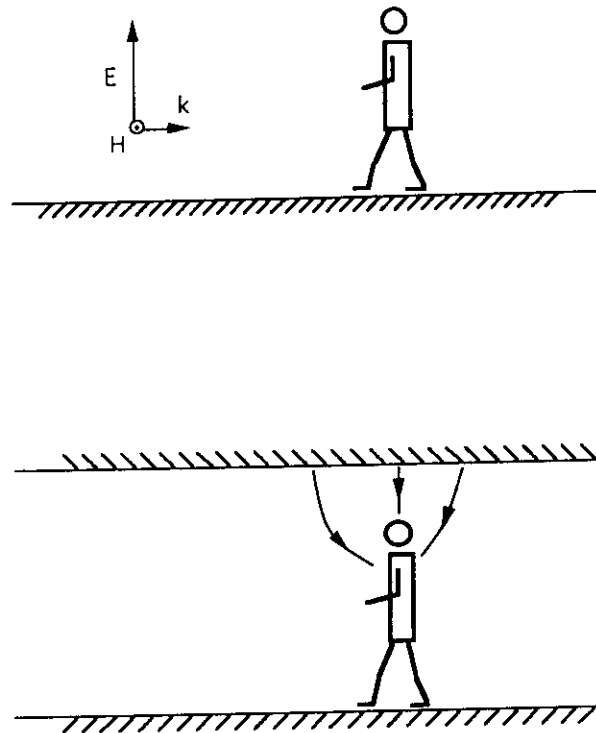


The average SAR increases proportionally
to the square of the frequency

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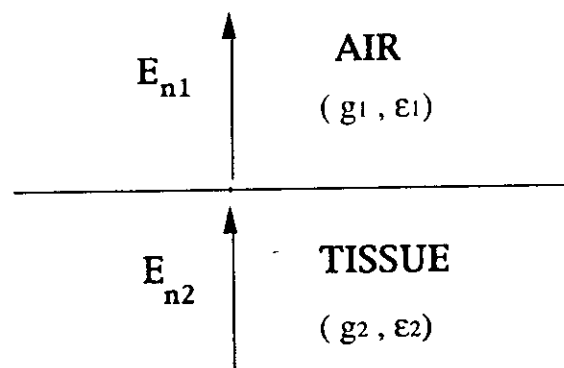
EMPIRICAL FORMULATION



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PLANAR SIMULATION



$$E_{n2} = \frac{g_1 + j\omega\epsilon_1}{g_2 + j\omega\epsilon_2} E_{n1}$$

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$$f = 50 \text{ Hz}$$

$$1 = \text{Air} \quad g_1 = 10^{-13} (\text{S/m}) \quad \epsilon_0 \epsilon_1 = 10^{-11} (\text{F/m})$$

$$2 = \text{Tissue} \quad g_2 = 10^{-1} (\text{S/m}) \quad \epsilon_0 \epsilon_2 = 10^{-5} (\text{F/m})$$

$$E_{n2} = \frac{j\omega\epsilon_1}{g_2} E_{n1}$$

$$\frac{E_{n2}}{E_{n1}} = \frac{E_{IN}}{E_{OUT}} \cong 4 \cdot 10^{-8}$$



EMPIRICAL FORMULA

$$|J_{IN}| = \omega \epsilon_0 E_{OUT} = 0.108 h_m^2 \frac{f_{MHz}}{A_{eq}}$$

$$SAR = \frac{J_{IN}^2}{g \rho}$$

h_m = human height

A_{eq} = Equivalent area of the cross section of the body

ρ (kg/m³) is the density of the considered tissue

g (S/m) is the conductivity of the considered tissue

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SAR AVERAGE

$$SAR_{av} = \frac{\text{Total power absorbed}}{\text{Weight}} =$$
$$= \frac{(0.108 h_m^2 f_{MHz} E_{OUT})^2 h_m}{70 g A} \cdot 10^{-2} \quad \frac{W}{kg}$$

$$f = 20 \text{ MHz}; \quad A = 400 \text{ cm}^2; \quad h_m = 1.75 \text{ m}$$

$$g = 0.5 \text{ S/m}; \quad E_{OUT} = 61.4 \text{ V/m}$$

$$SAR_{AV} = 0.21 \text{ W/kg}$$

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SAR PEAK

$$\text{SAR}_{\text{peak}} = \frac{(0.108 h_m^2 f_{\text{MHz}} E_{\text{OUT}})^2}{g \rho A_{\text{eq}}^2(0)} \cdot 10^2 \quad \frac{\text{W}}{\text{kg}}$$

$A_{\text{eq}}(0)$ = Equivalent area of the ankle

Under plane wave exposure the SAR_{peak}
is ever located in the ankles

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FOOT CURRENT

The current flowing through the feet
into a conductive ground

$$\frac{I_f}{E_{\text{inc}}} = 0.108 h_m^2 f_{\text{MHz}} \quad \frac{\text{mA}}{\text{V/m}}$$

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$30 < f < 300 \text{ MHz}$

Body resonance region

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NUMERICAL TECHNIQUES

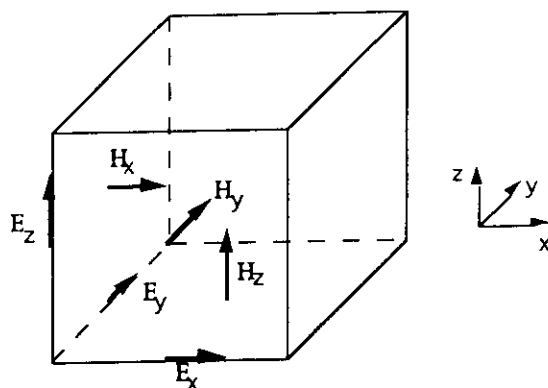
FDTD METHOD

MOMENT METHOD

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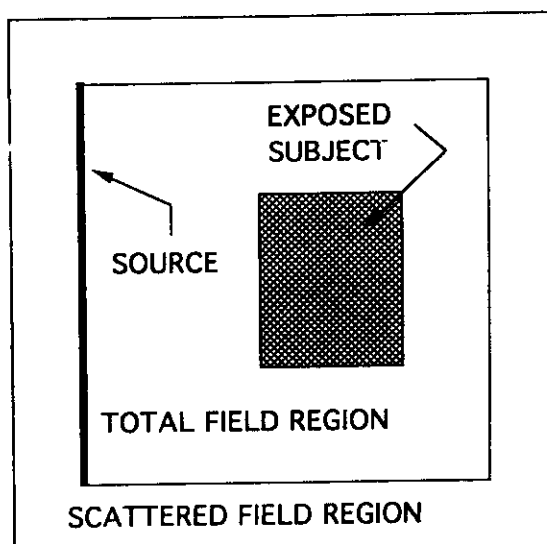
FDTD METHOD



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FDTD / CONSIDERED GEOMETRY



LATTICE
TRUNCATION



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BASIC ABSORPTION PARAMETERS

$$SAR(i,j,k) = \frac{g \left[\left(\widehat{E}_x^2 + \widehat{E}_y^2 + \widehat{E}_z^2 \right) \right]}{2 \rho}$$

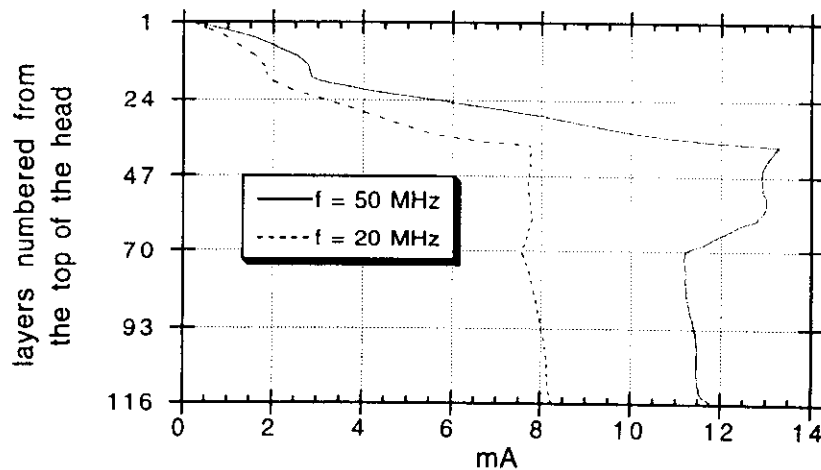
$$\hat{I}(h) = \sum_{i,j} \delta^2 \widehat{E}_z(i,j,h) \sqrt{g^2 + [2 \pi f \epsilon_0 \epsilon_r]^2}$$

$$I(h, n) = \sum_{i,j} \delta^2 \left[E_z(i,j,h,n) s + \epsilon_0 \epsilon_r \frac{E_z(i,j,h,n) - E_z(i,j,h,n-1)}{\delta t} \right]$$

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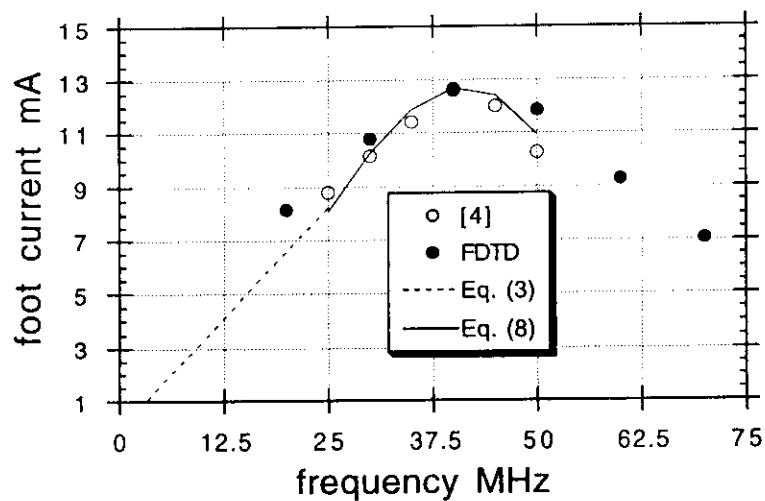
INDUCED CURRENT DISTRIBUTION



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FOOT CURRENT

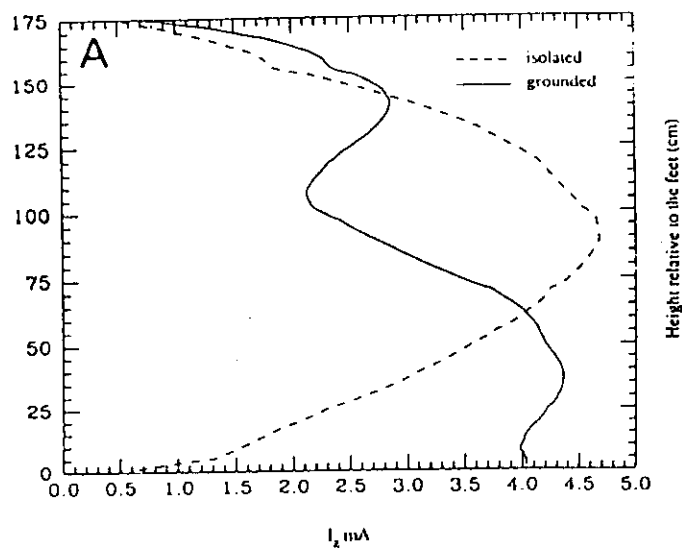


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CURRENT DISTRIBUTION

($f = 100$ MHz)

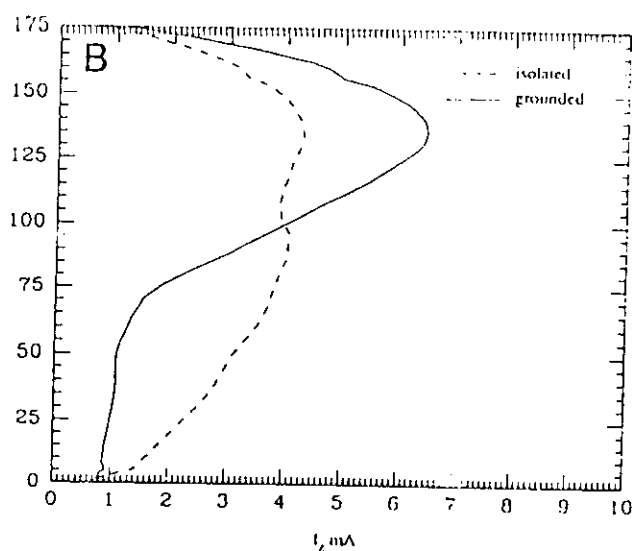


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CURRENT DISTRIBUTION

($f = 160$ MHz)

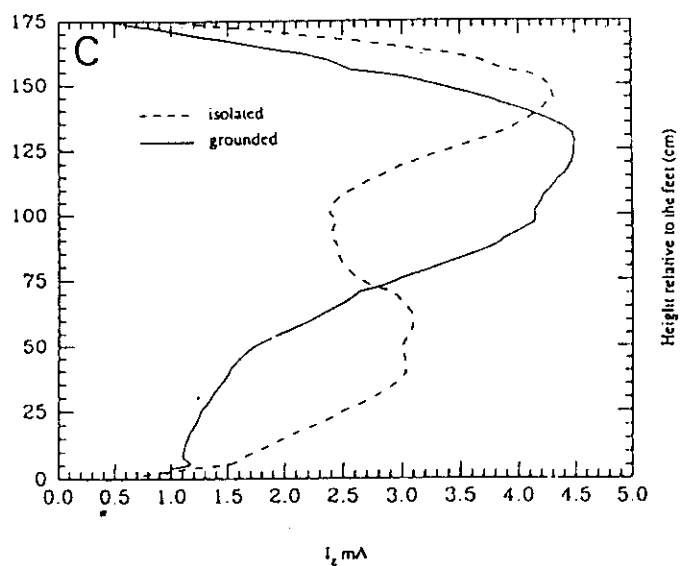


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CURRENT DISTRIBUTION

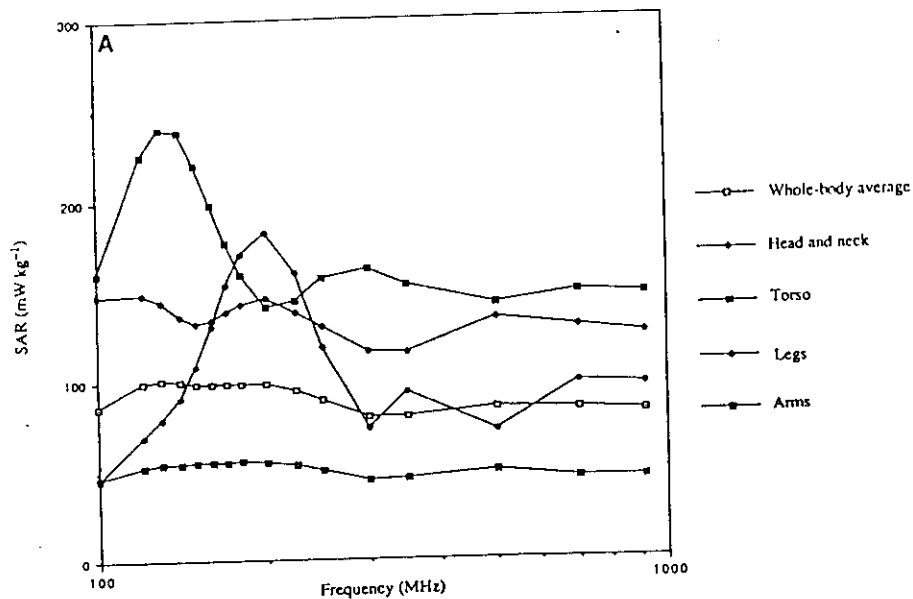
($f = 200$ MHz)



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PART-BODY AVERAGE SAR

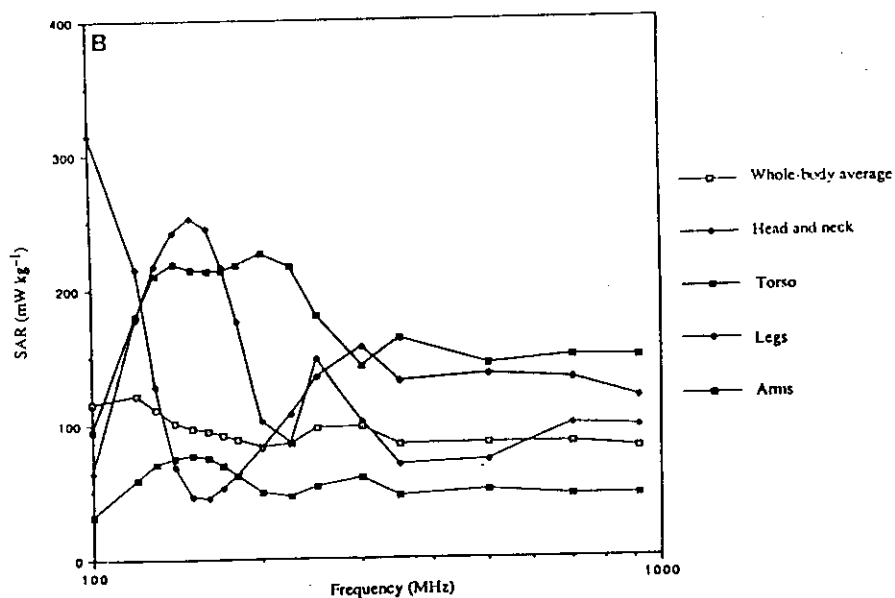
ISOLATED



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PART-BODY AVERAGE SAR

GROUNDING



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$f > 300 \text{ MHz}$



ANALYTICAL TECHNIQUES

Analytical solution of Maxwell's equations
for cylindrical models

This solution appear to be a good
approximation beyond 400 MHz

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AVERAGE SAR

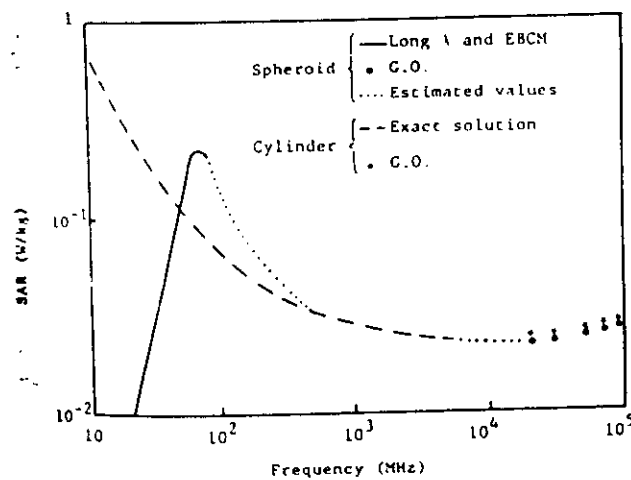
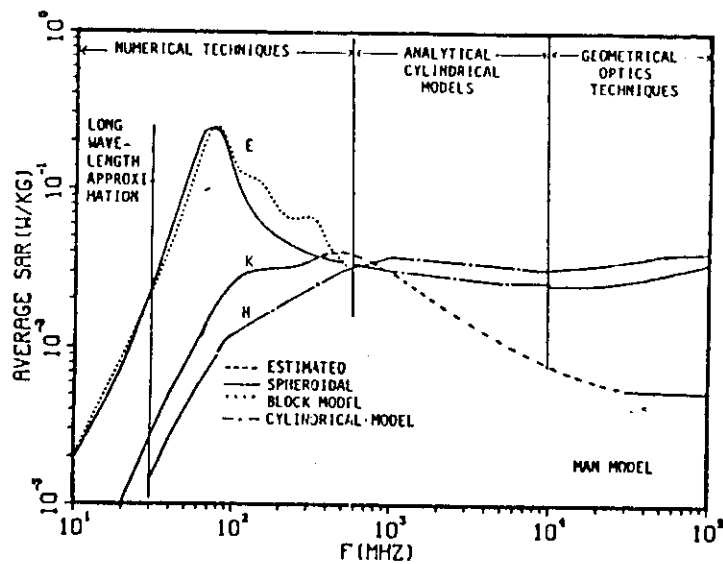


Fig. 4. Average SAR in 70-kg prolate spheroidal and cylindrical models of man (electric polarization). The radius of the cylinder is 11.28 cm, the length is 1.75 m, and the spheroid has the same height as the cylinder; the power density of incident radiation is 1 mW cm^{-2} . G.O. = geometrical-optics solution; EBCM = extended-boundary-condition method.

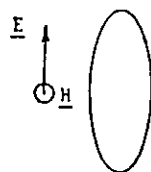
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AVERAGE SAR



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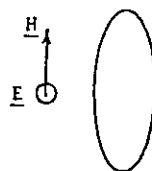
TYPES OF INCIDENCE



E Polarization

E_e strong

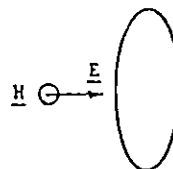
E_h strong



H Polarization

E_e weak

E_h weak



K Polarization

E_e weak

E_h strong

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NEAR FIELD EXPOSURE

CELLULAR PHONES

