



the  
**abdu salam**  
international centre for theoretical physics

SMR 1521/18

## **AUTUMN COLLEGE ON PLASMA PHYSICS**

13 October - 7 November 2003

# **ITER**

**K. Lackner**

**Max-Planck Institut fuer Plasmaphysik  
Garching, Germany**

These are preliminary lecture notes, intended only for distribution to participants.



# ITER and the mid & long term physics fusion program



**K.Lackner\*)**

Max-Planck-Institut für Plasmaphysik

D-85748 Garching

\*) previous adress: EFDA Close Support Unit

- why fusion
- ITER
  - role in fusion development strategy
  - ITER as a physics experiments
- fusion physics beyond ITER
  - requirements of a power plant
  - the stellarator alternative

acknowledgements to D. Campbell, S. Günter, W.Suttrop, ASDEX Upgrade Team

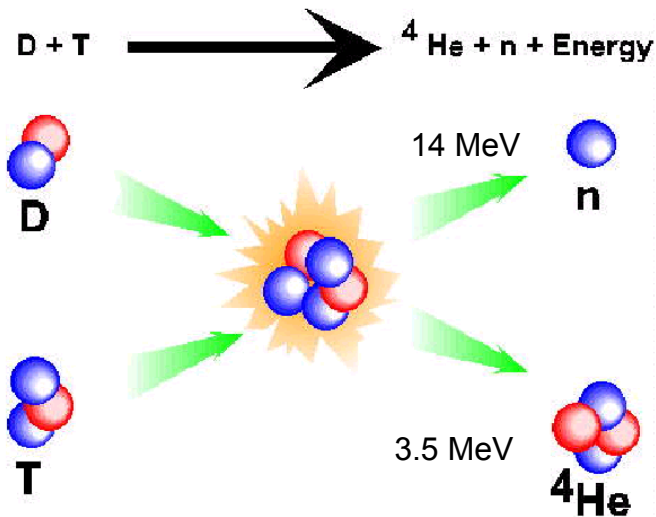
# Fusion Basics: steady state magnetic confinement

**fusion:** fusion is a „burn“ process, with a burn temperature of  $> 100$  Million  $^{\circ}$  K

## DT Fusion Reaction & Fuel Cycle

## principle of toroidal magnetic confinement

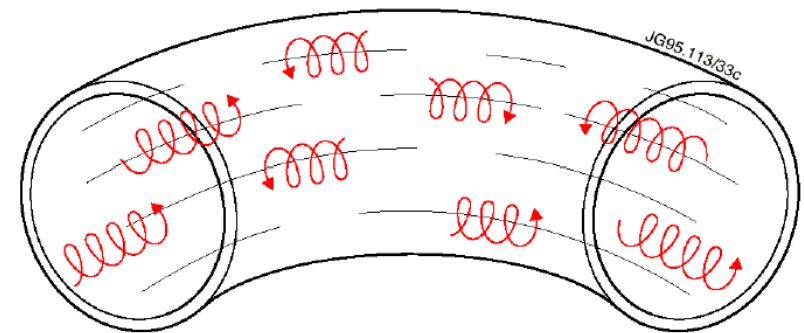
### D-T Fusion Reaction



neutrons recycled for T-production



$$Q = \frac{\text{fusion power produced}}{\text{external heating power applied}}$$



magnetic field reduces drastically perpendicular mobility of particles

balances the plasma pressure (O(10atm))

produces thermal insulation ( 200 Million K)

$$\beta = \frac{k \langle n_e T_e + n_i T \rangle}{B^2 / 2\mu_0}$$

$$\tau_E = \frac{\frac{3}{2} k \langle n_e T_e + n_i T \rangle V_p}{P_{heat}} = H \cdot \tau_{E,scaling}$$

# Fusion Basics: intrinsic properties of magnetic fusion

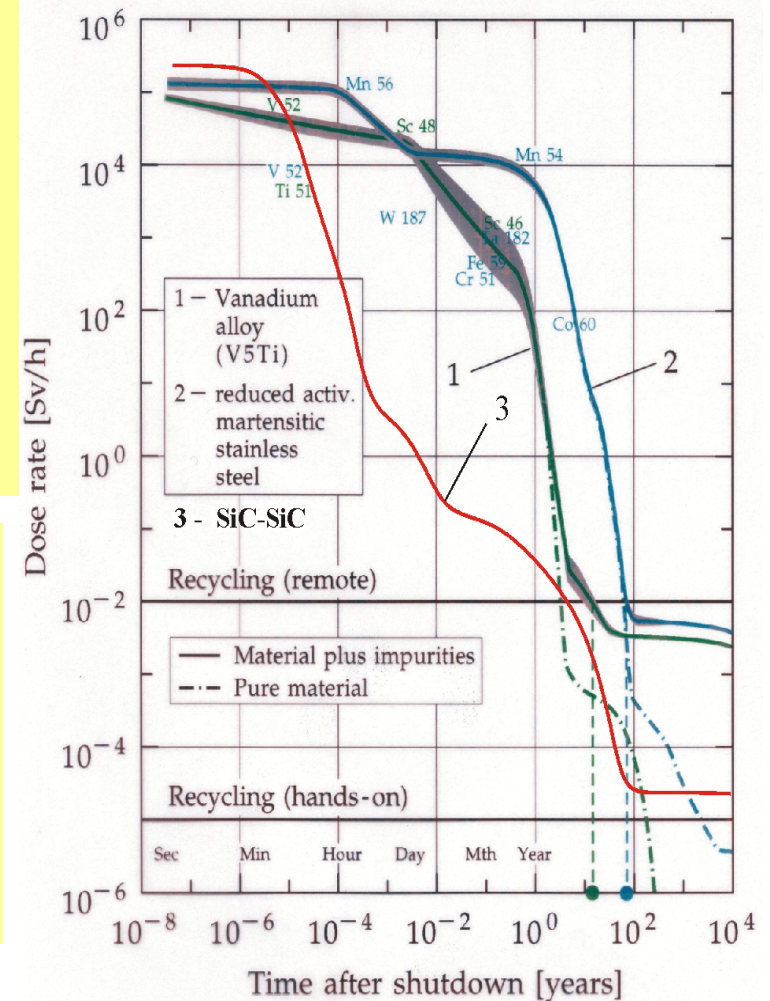


pro:

- abundant, distributed fuel
- fuel cycle closed on site (tritium breeding and burnup)
- safety: low afterheat, fuel inventory for 1' burn, no chain reaction but thermal burn process
- waste only activated structural and functional material: large potential for minimization

con:

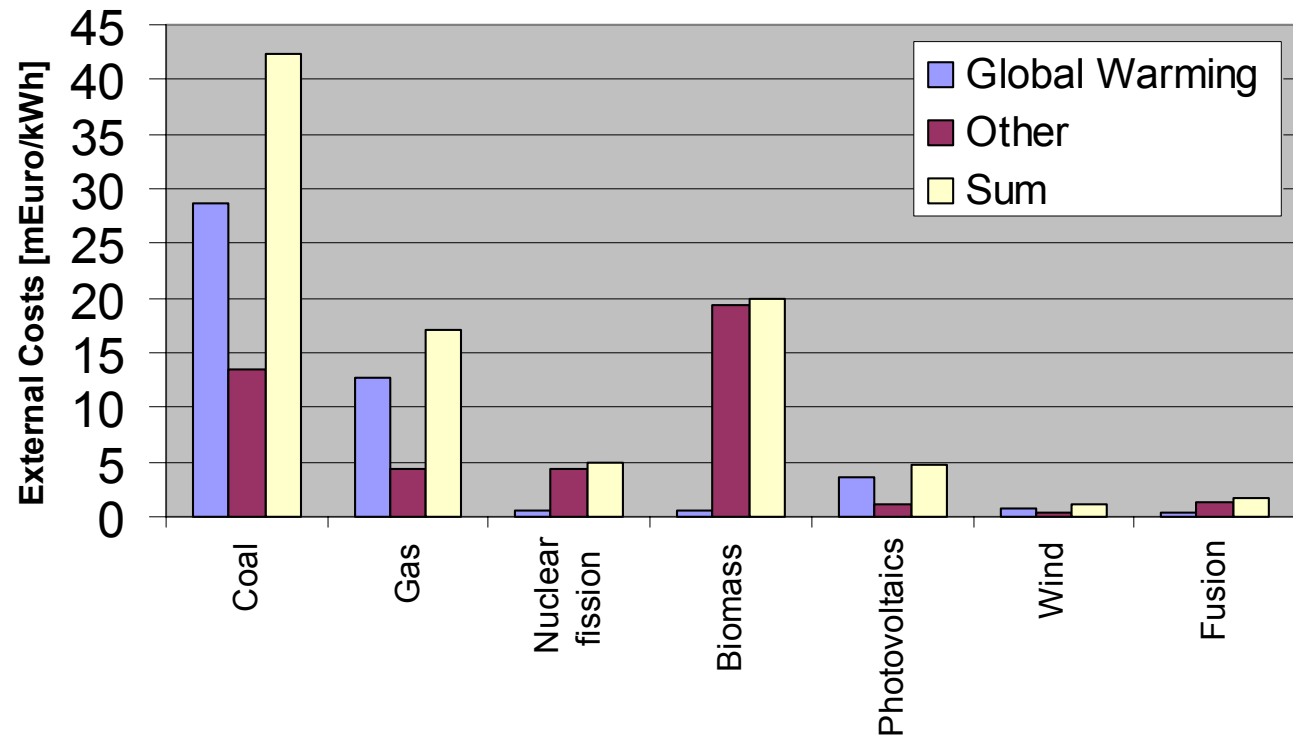
- difficult to initiate and maintain: >100 Mill. K, high energy confinement time, plasma pressure
- complex technology: magnets, remote handling, fuel cycle, power fluxes
- tritium handling



# potential role of fusion: environmental impact of fusion

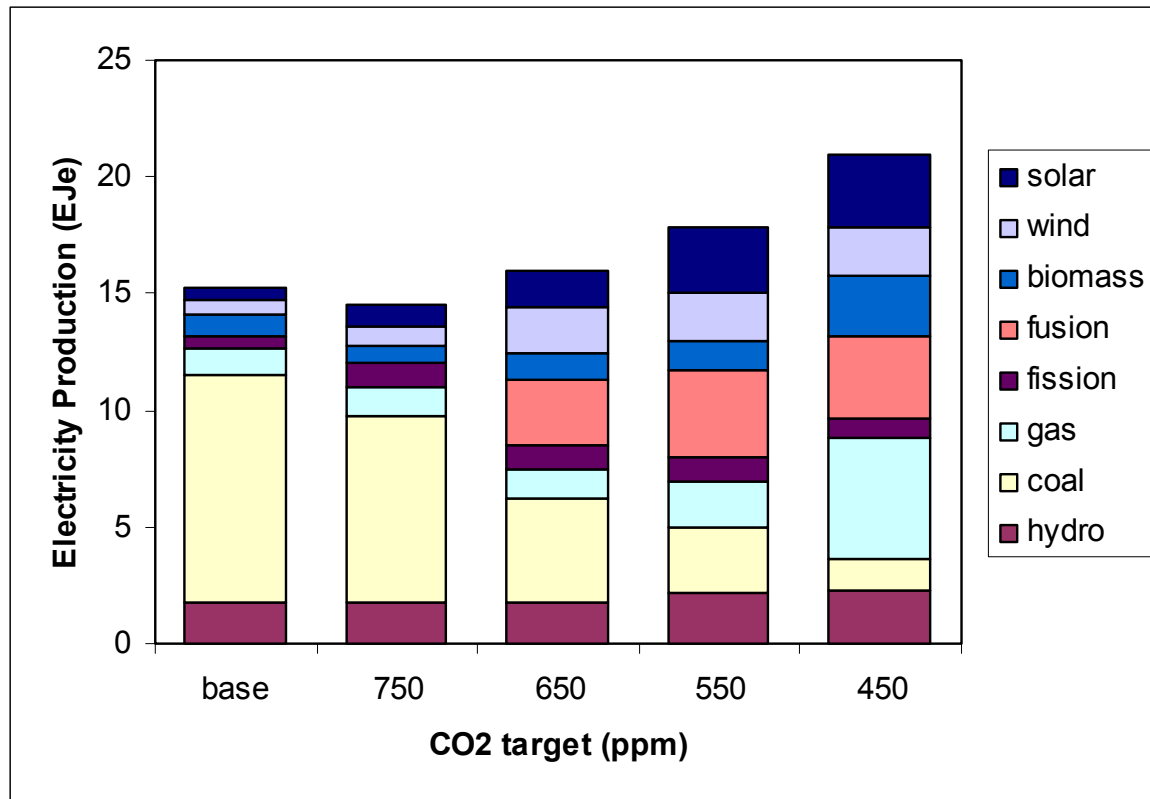


**Externalities:**  
quantify in monetary terms adverse effects on the system (in most cases the environment) not already accounted for in the financial plan



fusion belongs to the class of low environmental impact energy systems

# potential role of fusion: role in energy scenarios for 21st century



electric power production  
in Europe in 2100:

scenarios

- minimizing total (discounted) expenditures for electric energy production in 21st century
- under different constraints on total CO2 production and on acceptance of fission

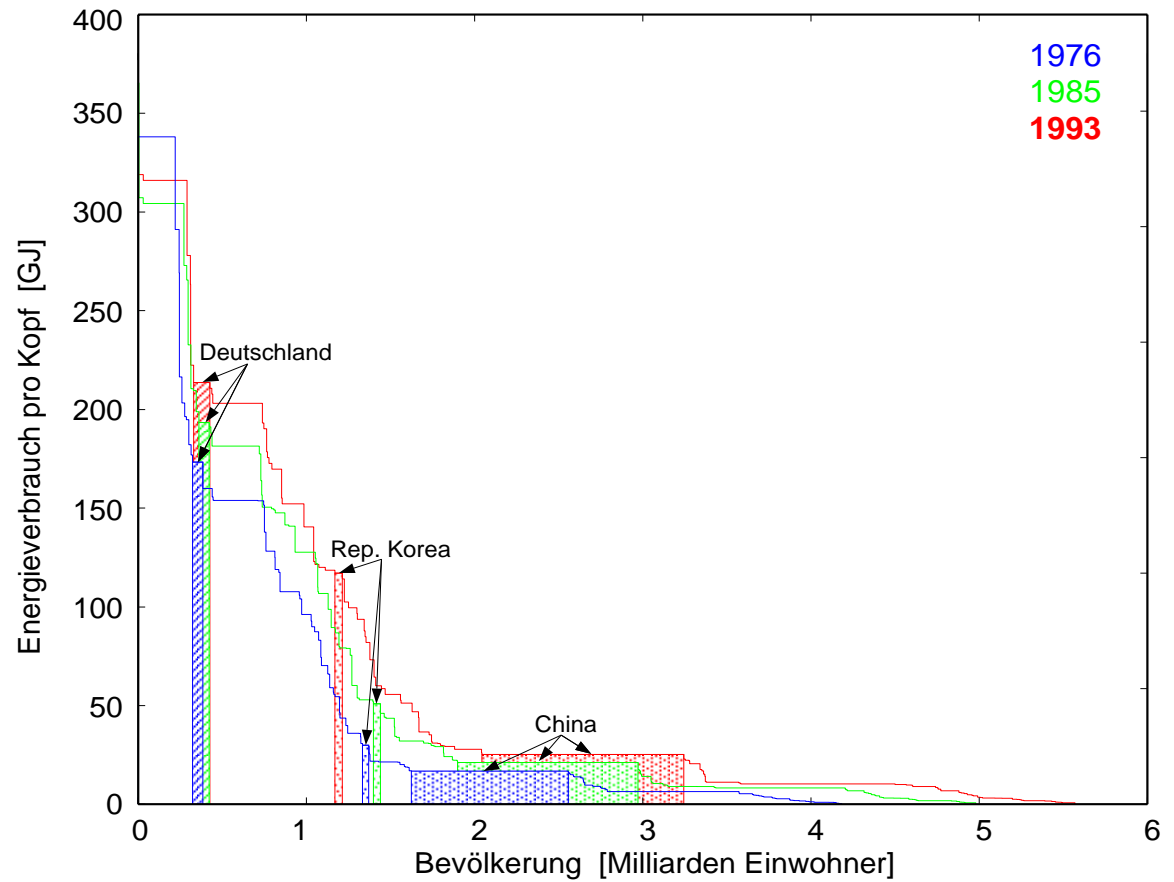
under CO2 emission constraints

- fusion could gain significant market share
- complimentary to classical renewables: fusion satisfies base-load demands

# energy consumption growth: total and per capita

dramatic per-capita energy consumption growth at transition to highly developed country

at high per-capita consumption, a country has also technology capability for fusion



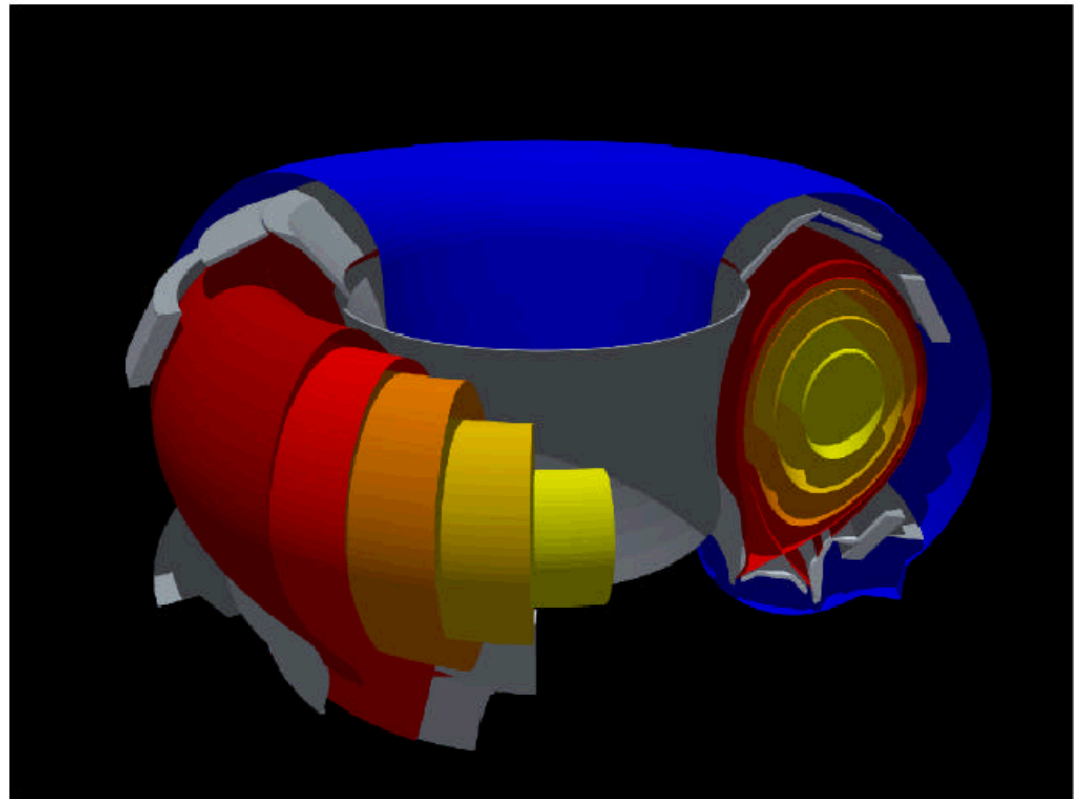
CarolusMagnus 1999



## nested magnetic flux surfaces

large anisotropy of  
heat conductivity:

$$\chi_{\text{par}}/\chi_{\text{perp}} > 10^{10}$$



# electromagnetics of a tokamak

Fully axisymmetric configuration

Toroidal field coils:

⇒ Toroidal magnetic field

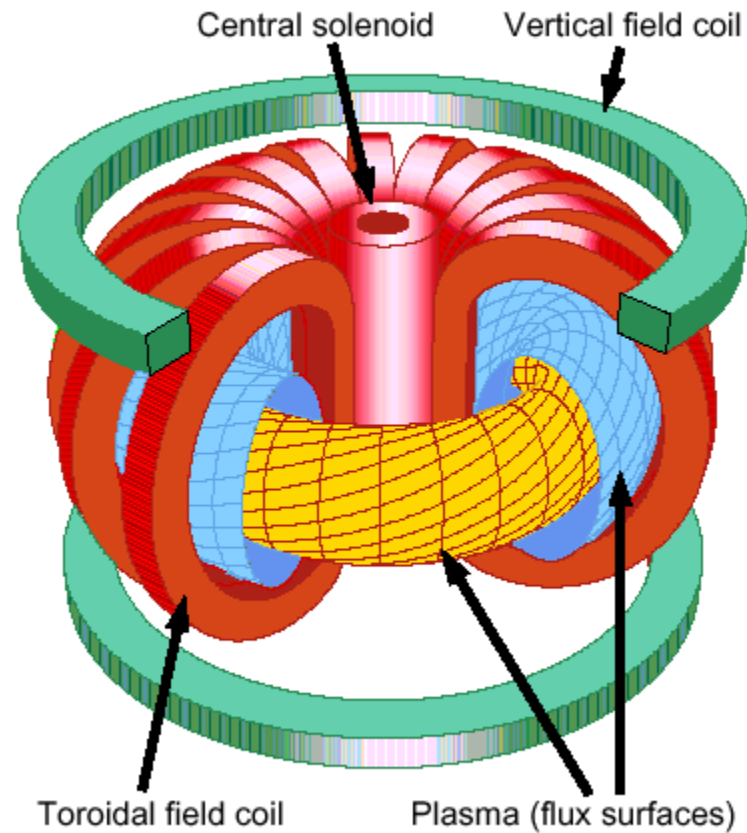
Central solenoid:

⇒ Inductively driven plasma current  
 ⇒ Poloidal magnetic field

Vertical field coils:

"Equilibrium" - balance of hoop force

Shape of flux surfaces  
 (poloidal cross section)

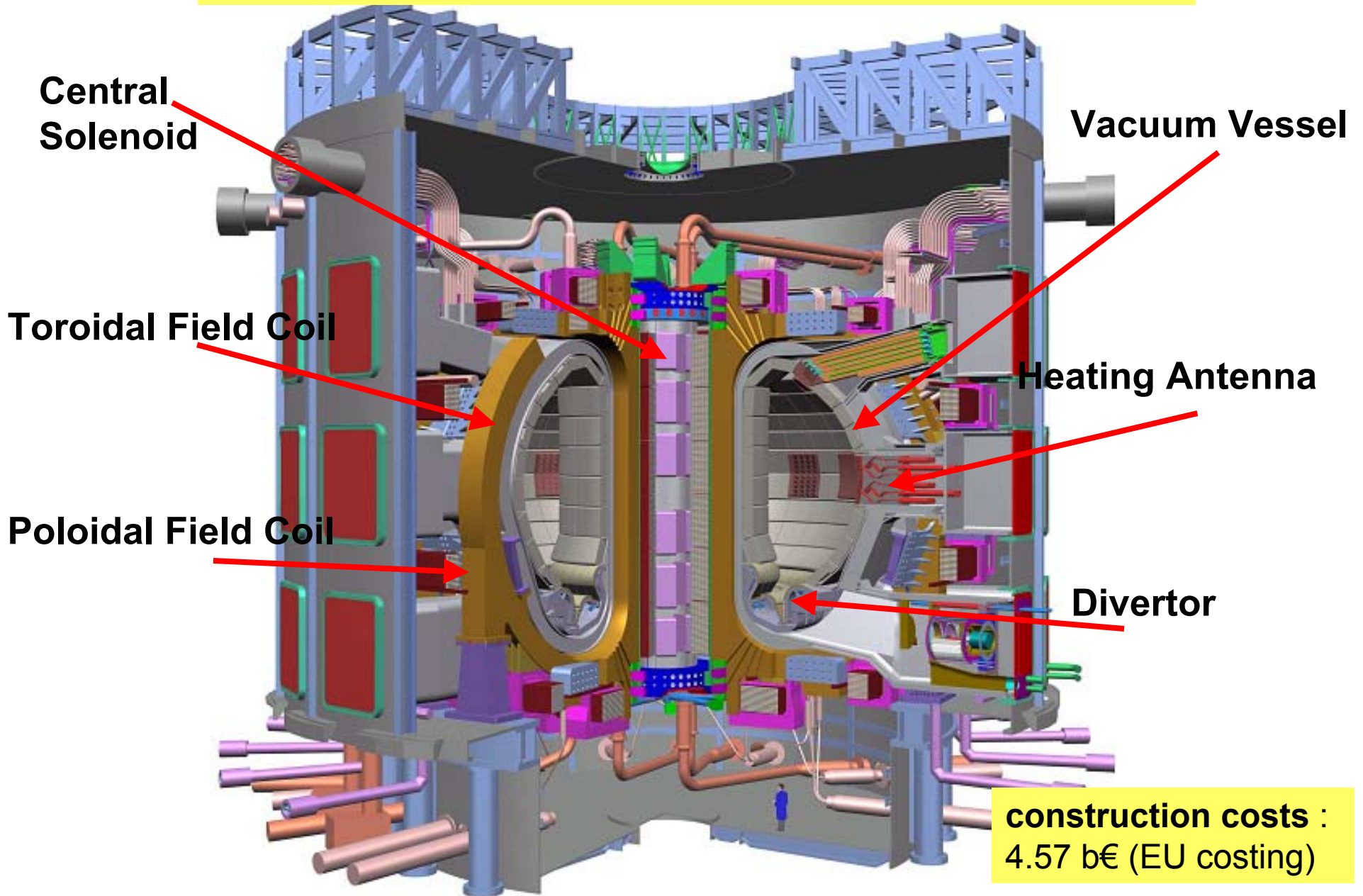


# ITER

Engineering Design Phase (1992 – 2001)

Japan + European Union + Russian Federation + (US until 1999)

negotiations among partners: above + (Canada) + China + USA(again)+ S. Korea



## ITER Design Goals

- burning plasma physics
- integration of technology with physics
- demonstrate and test fusion power plant technologies

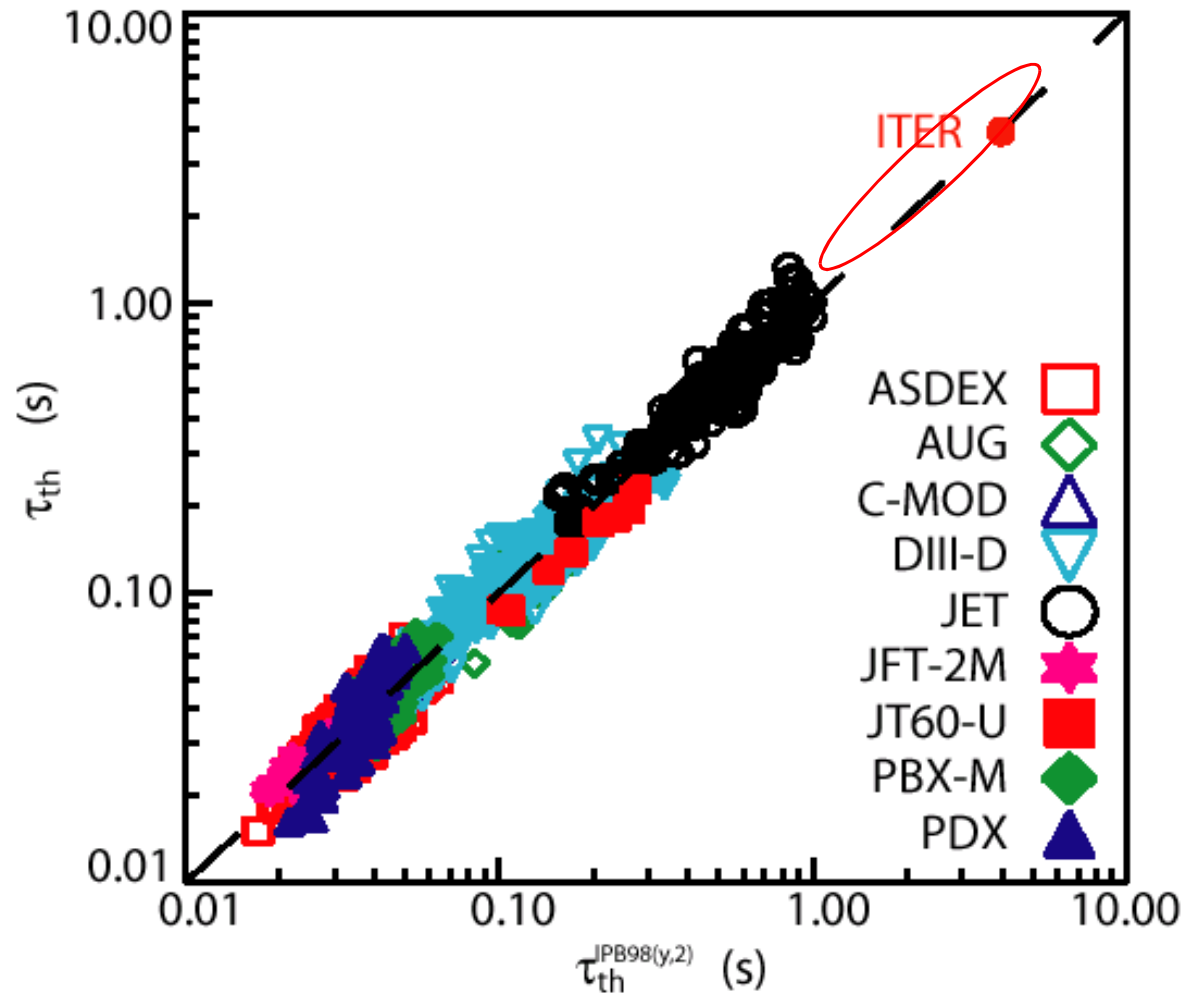
### Physics:

- produce a plasma dominated by  $\alpha$ -particle heating
- a significant fusion power amplification factor ( $Q \geq 10$ ) in long-pulse operation
- aim to achieve steady-state operation of a tokamak ( $Q = 5$ )
- possibility of exploring 'controlled ignition' ( $Q \geq 30$ )

### Technology:

- demonstrate integrated operation of technologies for a fusion power plant
- test components required for a fusion power plant
- test concepts for a tritium breeding module

# ITER's Mission: physics of burning plasma - confinement in power plant grade (size) plasmas



# Burning Plasma Physics

## (1) explore plasma regime of a reactor

- Quasineutral plasma state characterized by 3 dimensionless parameters

$$\rho_i = \rho / R = 0.0032 \sqrt{\mu_i T} / (R B_t)$$

$$\nu^* = Rq / \lambda_{mfp} = 10^{-22} R n_e q / T^2$$

$$\beta_t = 8 \times 10^{-22} n_e T / B_t^2$$

$$n_e = 1.3 \times 10^{16} \left( \frac{\mu}{R^2} \times \frac{\beta}{\rho^2} \right)$$

$$B_t = 1.1 \times 10^{-4} \left( \frac{q \mu^3}{R^5} \times \frac{\beta}{\nu \rho^6} \right)^{1/4}$$

$$T = 0.0011 \left( \frac{q \mu}{R} \times \frac{\beta}{\nu \rho^2} \right)^{1/2}$$

- 4 dimensional ones: R, n, T, B
- dimensionless identity experiments
- a compact device with same plasma physics would require higher heating power, higher current than a reactor!

$$\begin{aligned} P_{heat} &\propto R^{-3/4} \\ I_p &\propto R^{-1/4} \end{aligned}$$

- Fusion heating does not obey plasma physics constraints

$$\frac{P_\alpha}{P_{heat,tot}} \propto n T \tau_E = f(\rho^*, \nu^*, \beta) \times R^{-5/4}$$

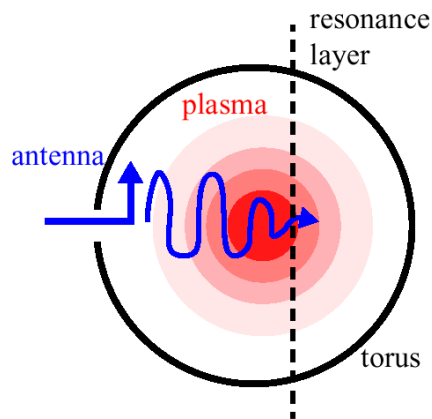
Device	R[m]	a[m]	Bt[T]	Ip[MA]	Pheat	nTτ (rel)
JET ext.	3	1.1	4	6	40	1
Ignitor	1.32	0.48	11.2 (<13)	7.4 (<11-12)	74 (35)	2.8

# ITER's Mission: physics of burning plasma - nuclear self-heating

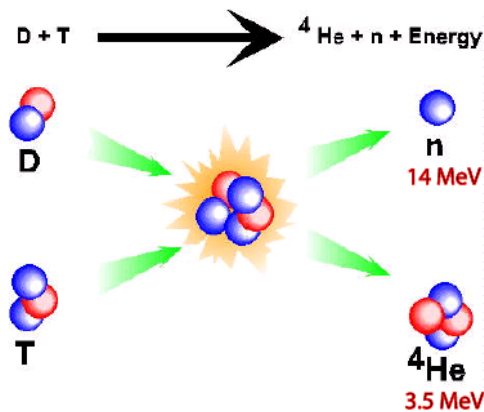


tokamak operation so far:  
external heating

e.g. wave heating



ITER:  $nT\tau$  sufficient for  
dominant self-heating



$$Q = \frac{\text{fusion produced power}}{\text{externally applied heating power to plasma}} \rightarrow 10$$

dynamics of burn:  
determined by

$$\gamma_b = \frac{1}{\tau_E} \left( \frac{d \log \langle \sigma v \rangle}{d \log T} + \left( 1 + \frac{5}{Q} \right) \left( \frac{d \log \tau_E}{d \log T} - 1 \right) \right)$$

## (2) physics of fusion self-heating global dynamics of ignition



- Global dynamics of ignition depends on plasma physics ( $\rho^*, v^*, \beta$ ) and T
- burn stability depends on confinement “law” and T;

$$\gamma_b = \frac{1}{\tau_E} \left( \frac{d \log \langle \sigma v \rangle}{d \log T} + \left( 1 + \frac{5}{Q} \right) \left( \frac{d \log \tau_E}{d \log T} - 1 \right) \right)$$

- for T-independent additional heating (not true, e.g. for Ohmic heating, which stabilizes due to opposite T-dependence)
- for physics of late 70ies (Alcator-Intor scaling, or even more CMG) and low temperature ignition a major issue.

$$\left( \frac{d \log \tau_E}{d \log T} \right)_{\text{Alcator-Intor}} = 0 \quad \left( \frac{d \log \tau_E}{d \log T} \right)_{\text{CMG}} = 1 \quad \left( \frac{d \log \langle \sigma v \rangle}{d \log T} \right) > 2$$

- for scaling laws accounting for power degradation, and the higher operating temperatures forced by Greenwald limit - no issue

$$\left( \frac{d \log \tau_E}{d \log T} \right)_{\text{H98(y)}} = -1.7 \quad \left( \frac{d \log \langle \sigma v \rangle}{d \log T} \right) \leq 2$$



## (2) physics of fusion self-heating

### $\alpha$ – particle physics

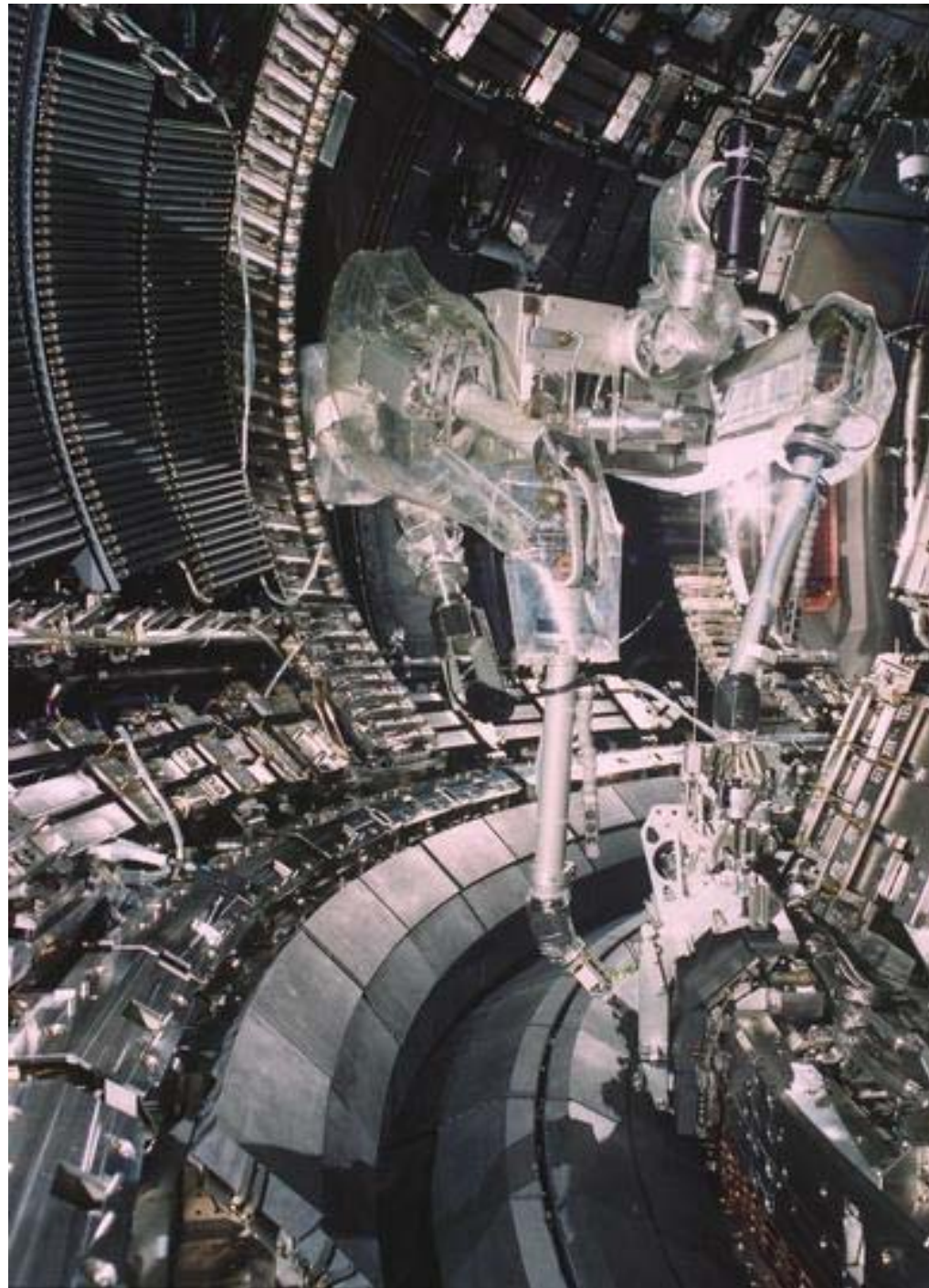
- Sufficient Q needed to dominate heating (Q=10, concur with Ignitor)
- $\alpha$ -particle physics (via MHD-instabilities) depends (for given Q) on T,  $\beta$

$$\frac{\beta_{fast}}{\beta} = \frac{P_{fus} \tau_{sd}}{P_{fus} \tau_E (1+Q/5)} \propto (\text{for fixed Q}) \frac{T^{3/2}}{n \tau_E} = \frac{T^{5/2}}{n T \tau_E} \propto T^{5/2} \left( \frac{T^2}{\langle \sigma v \rangle} \right)$$

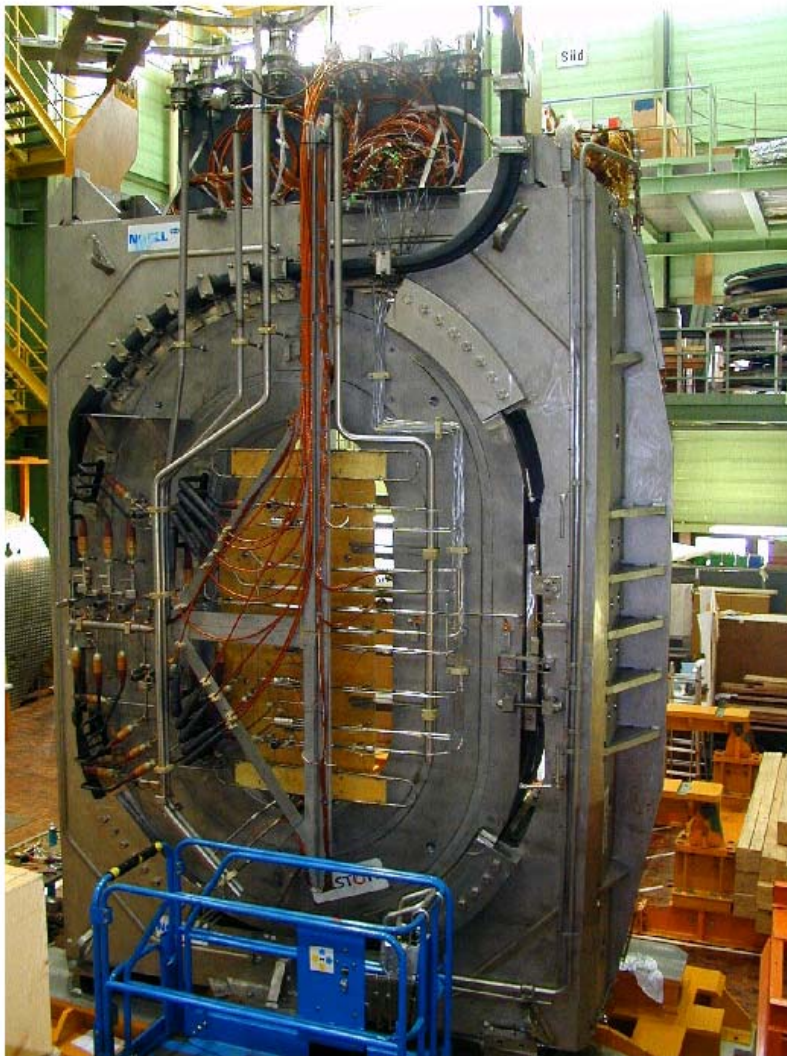
- i.e. ignition temperature regime is essential for relevance of studies

**Preparatory R&D:  
(some) key reactor  
technologies already on  
present devices**

e.g.on JET: fully  
remote substitution  
of divertor structure  
under activated  
conditions (after  
DTE1)



## Preparatory R&D: superconducting magnets (in burning plasma environment) - L1/L2



specific fusion technology had to be developed:

high field, high stress ( $\text{Ni}_3\text{Sn}$ )

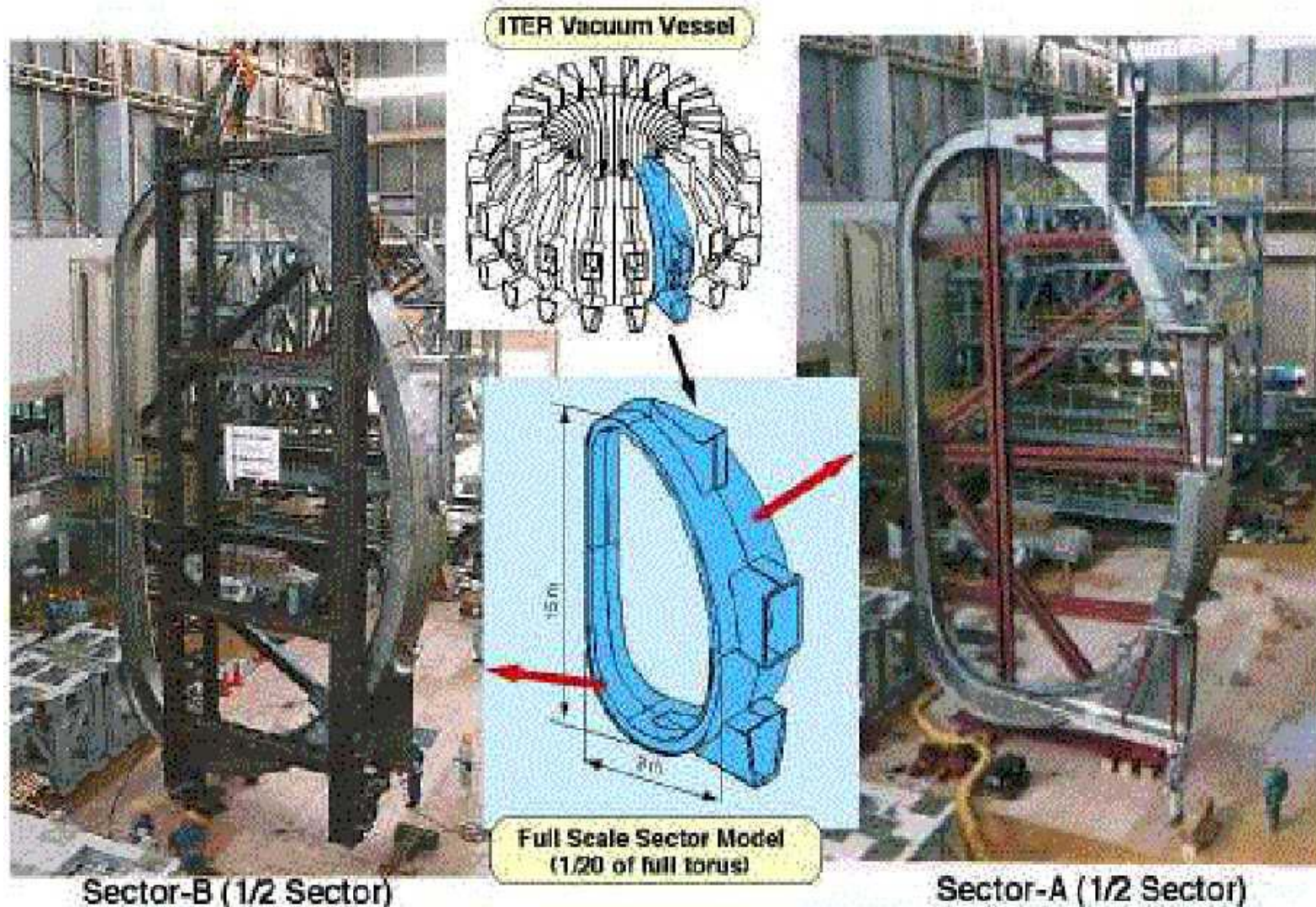
rapidly time - varying magnetic fields

R&D for ITER (with strong involvement of industry and all 4 partners):

test coils fabricated with record parameters (e.g. raised record for stored energy for  $\text{Ni}_3\text{Sn}$  **by factor of 21**, pulsed operation)

developed industrial fabrication techniques

# Preparatory R&D: Vacuum Vessel (L-3)



- View of full-scale sector model of ITER vacuum vessel completed in September 1997 with dimensional accuracy of  $\pm 3$  mm

# Preparatory R&D: Physics and technology cannot be separated:

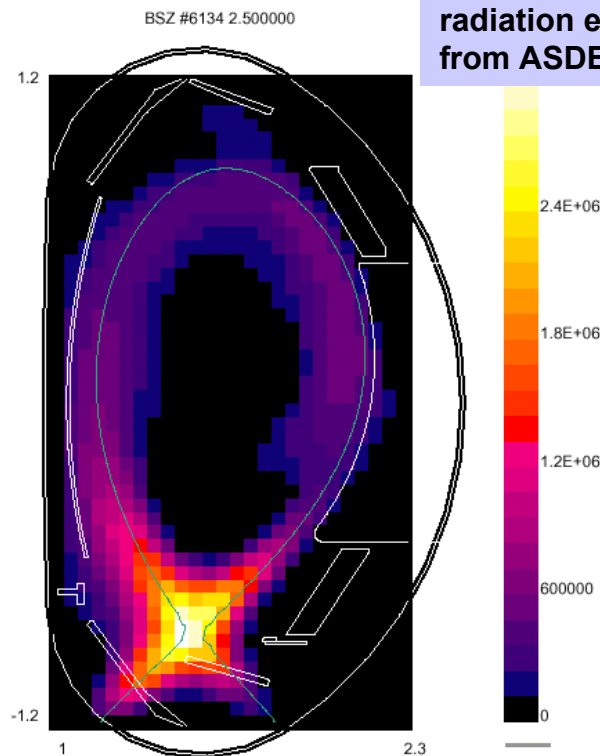


e.g.: plasma-wall interaction

at plasma-wall contact large heat fluxes

unmitigated -> 60 MW/m<sup>2</sup>  
(comparable to sun surface)

through plasma control (divertor)  
-> 5-10 MW/m<sup>2</sup>



# Preparatory R&D: ITER component prototype development



## Resource Allocation Summary for the Seven Large R&D Projects

(Unit: kIUA)

Projects	EU	Japan	RF	US*	Total
L1 - Central Solenoid Model Coil	10	<b>61</b>	4	<b>22</b>	97
L2 - Toroidal Field Model Coil	<b>40</b>	0	0	1	41
L3 - Vacuum Vessel Sector	4	<b>19</b>	4	2	29
L4 - Blanket Module	<b>29</b>	14	<b>12</b>	9	64
L5 - Divertor Cassette	13	12	9	<b>21</b>	55
L6 - Blanket Module Remote Handling	3	<b>18</b>	0	0	21
L7 - Divertor Remote Handling	<b>26</b>	3	0	0	29
Total	125	127	29	55	336

\* US contributed until July 1999

Status: June 2000

The 1B\$ ITER design effort and the 0.4 B\$ spent on dedicated component development have produced a solid fundament and are a highly tangible asset of the ITER-project

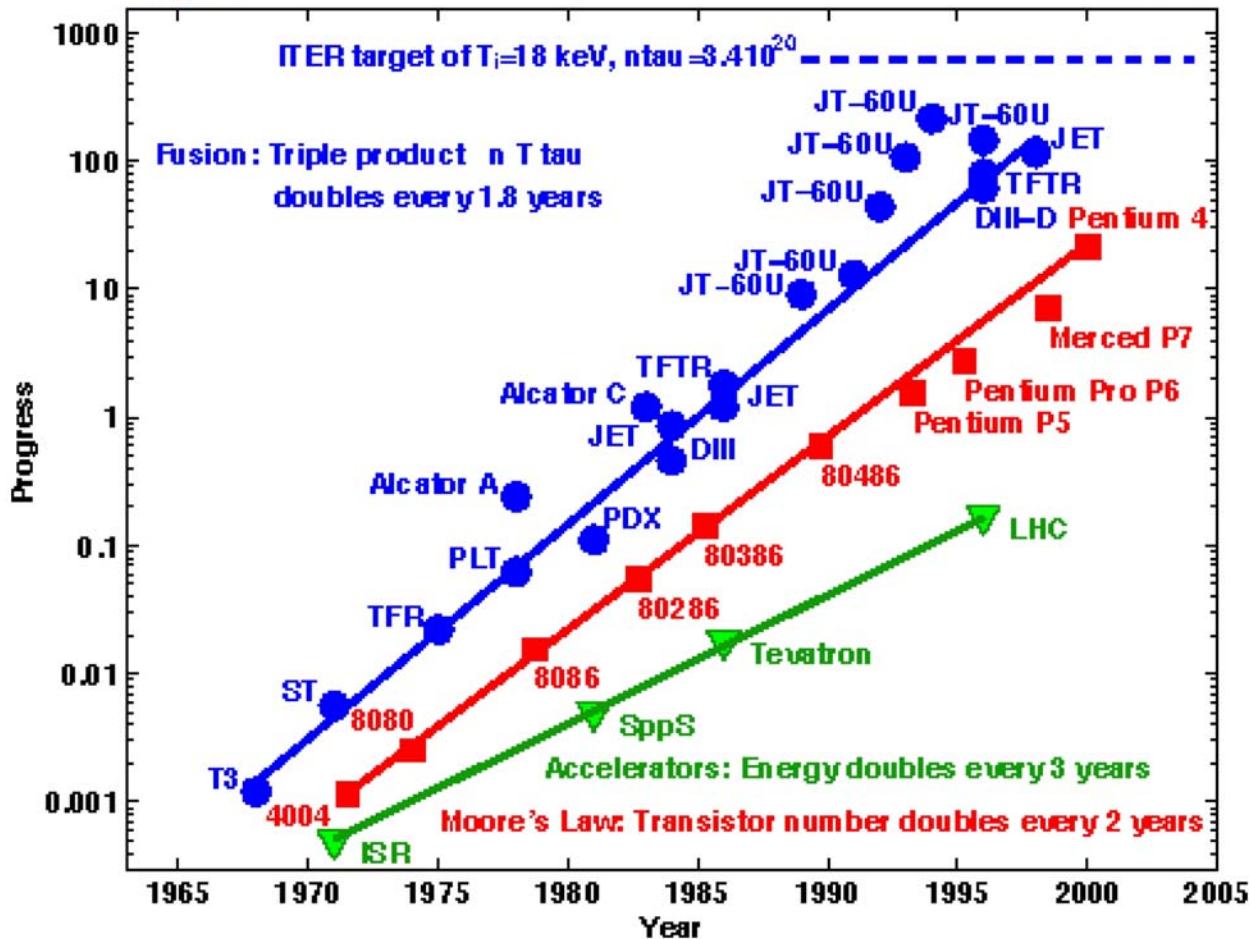
# Readiness for ITER: Fusion Research Performance can be measured in the „triple product“ $n T \tau$

$$Q = \frac{\text{fusion power produced}}{\text{external heating power applied}} \sim n_{i0} T_{i0} \tau_E \quad (\text{for } Q \ll 5)$$



J B Lister, April 2001

Rapid progress in different high technology fields



$n$ ... plasma density  
 $T$ ... plasma temperature  
 $\tau$  ... energy confinement time  
 (a measure of the quality of the thermal insulation)

steady, rapid progress of tokamak performance

natural next step:  
 burning plasma

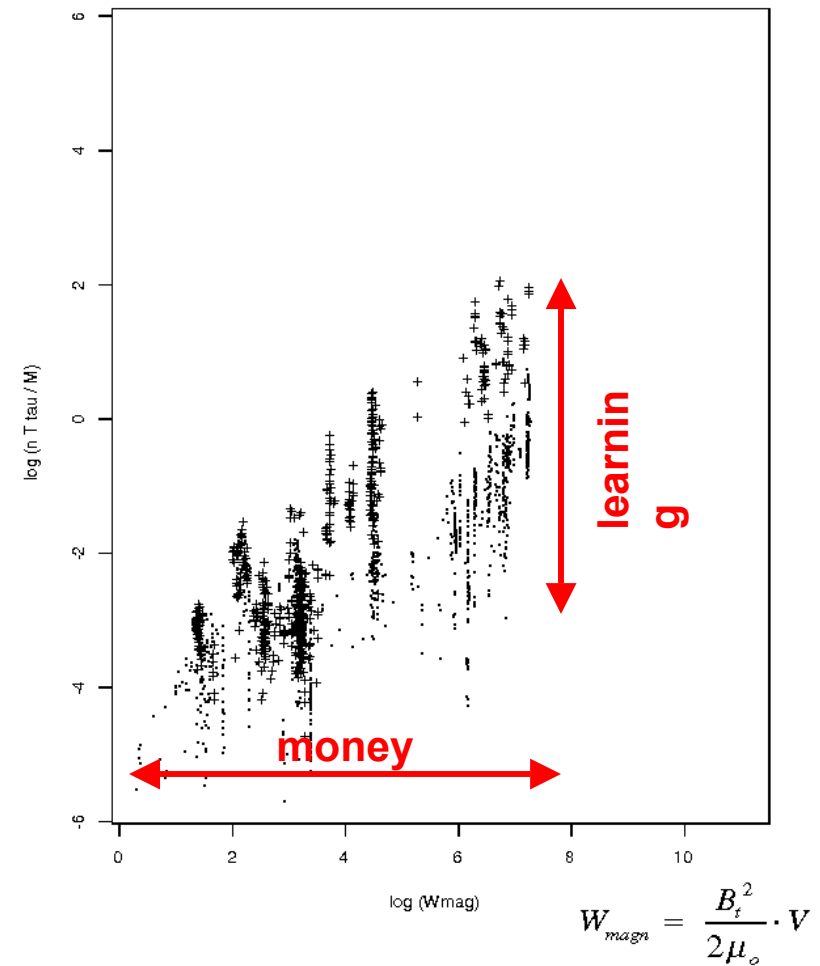
tokamak research is mature for the step to a burning plasma - the progress in performance measure  $n T \tau$



progress by:

- increased size of devices
- by improvements in design & operation

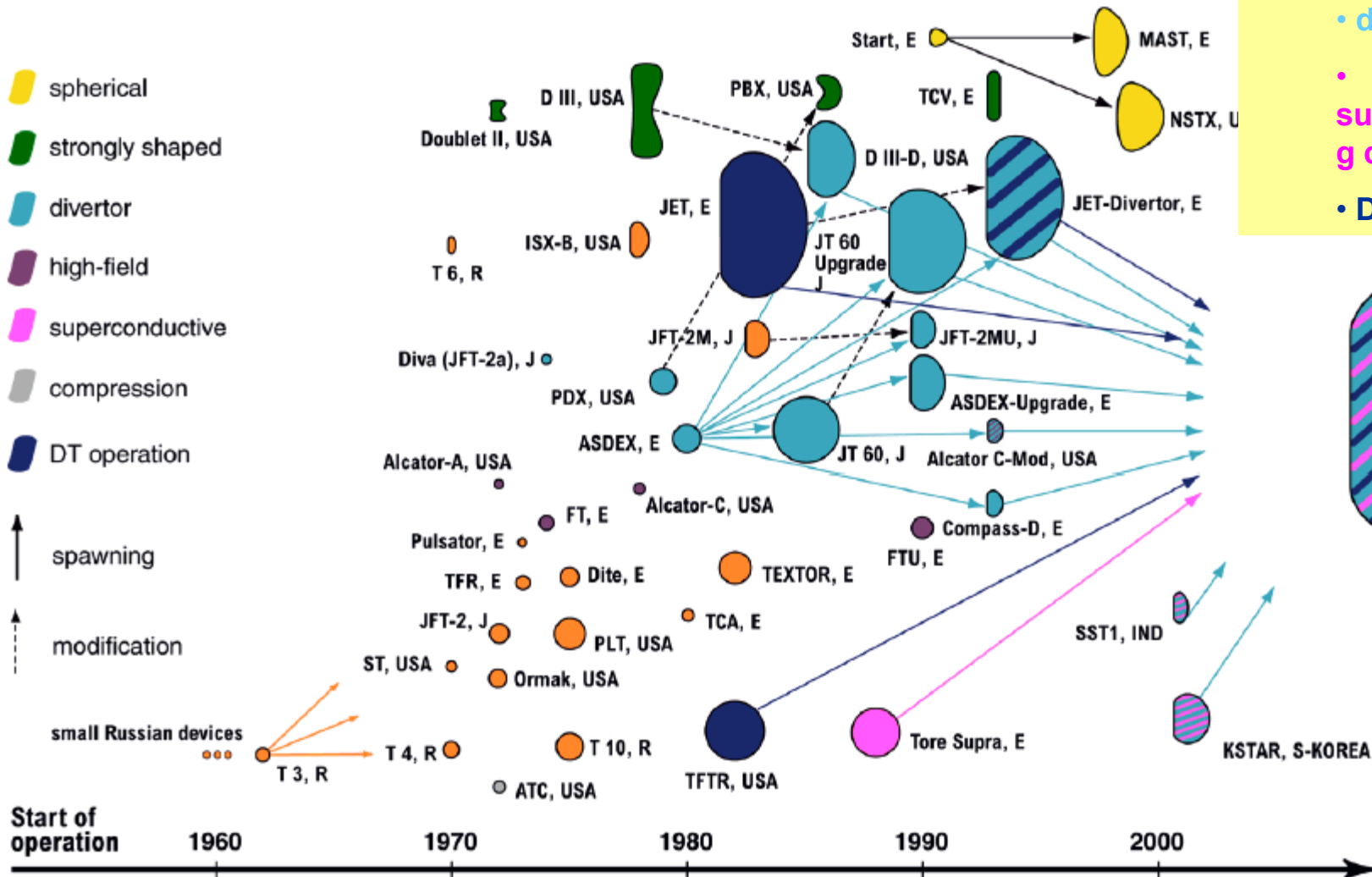
ITER L- mode and ELMy H - mode Dataset





# Readiness for ITER: the (Darwinian) development of the tokamak concept

## Major Tokamak Facilities



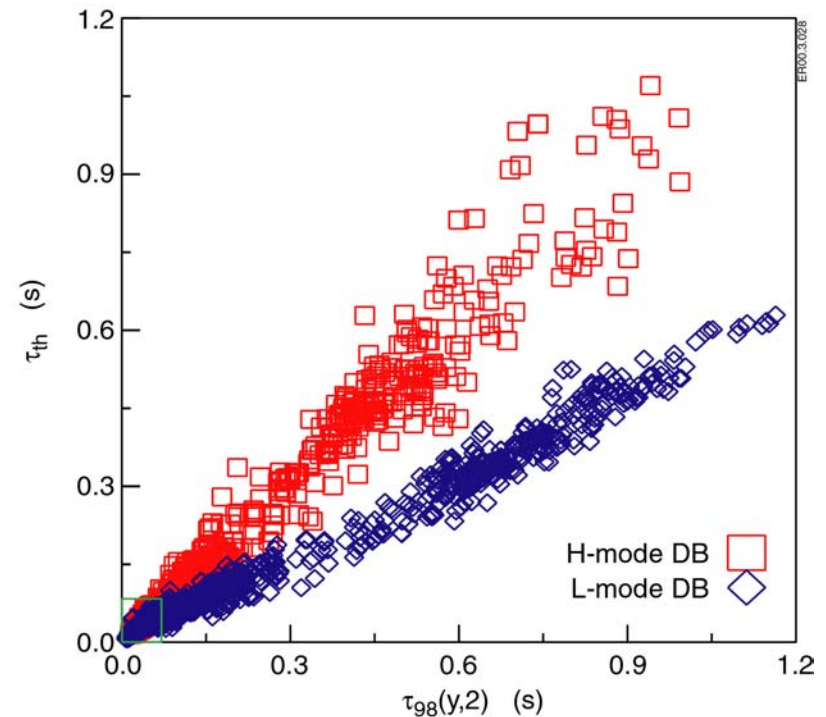
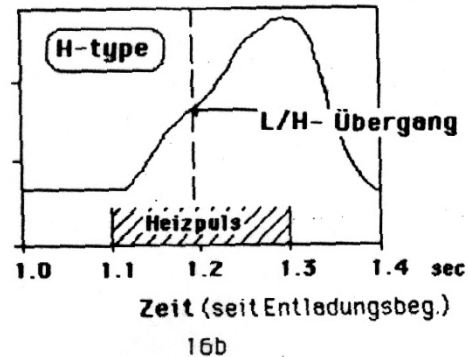
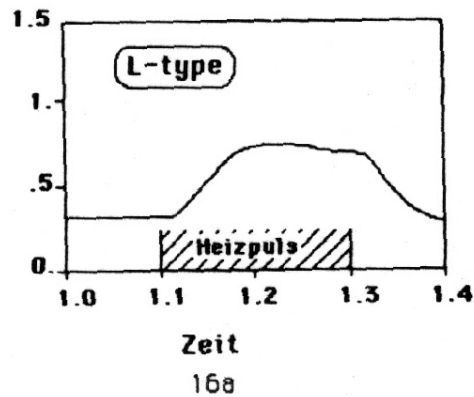
- ITER incorporates all successful developments:**
- elongated (D-shaped) cross-section
  - divertor
  - superconducting coils
  - DT operation



ITER II

# H-mode confinement or the unexpected side of plasma boundary physics - the tail wags the dog!

consequences on global confinement beyond those via impurity balance



historic questions:

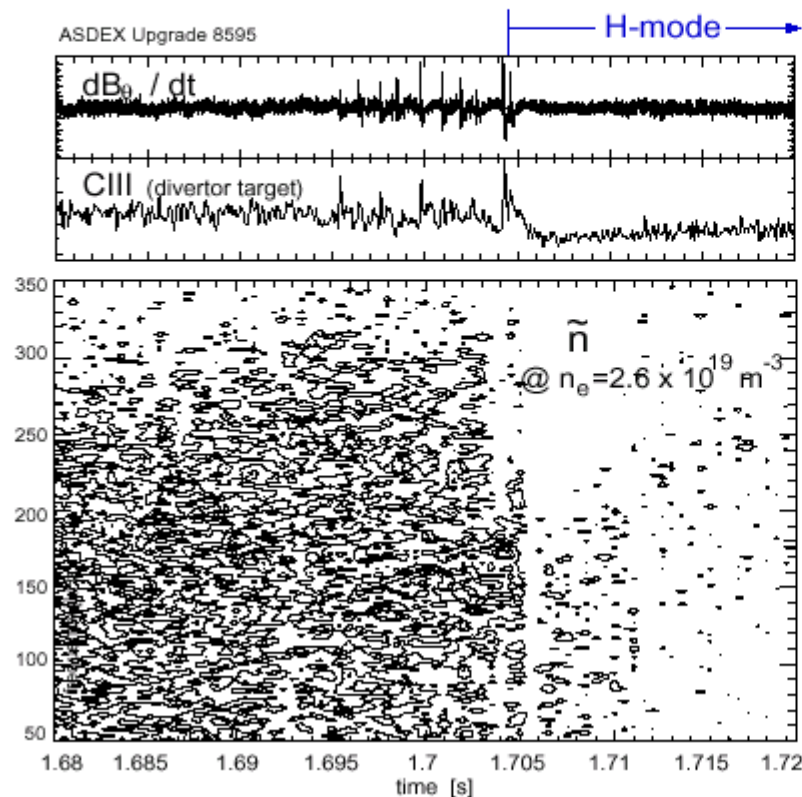
why only in divertors ?

why not internal barriers ?

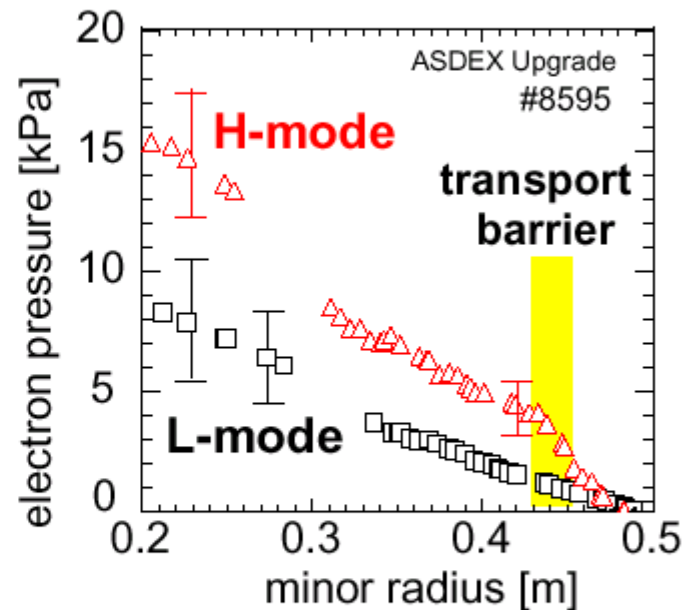
# Transport barriers due to suppressed turbulence

1984 ASDEX:

Transition to H-mode = state with reduced turbulence at the plasma edge



Formation of an edge "transport barrier"  
= steep pressure gradient at the edge

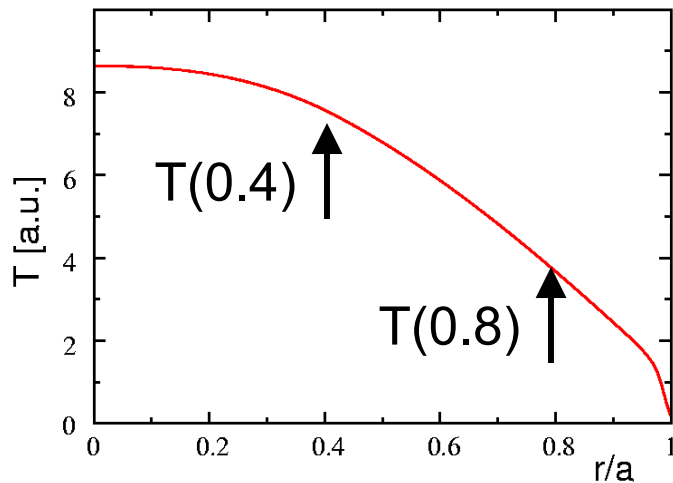


Reduction of transport coefficients to "neoclassical" level often found

Edge pressure limited by stability

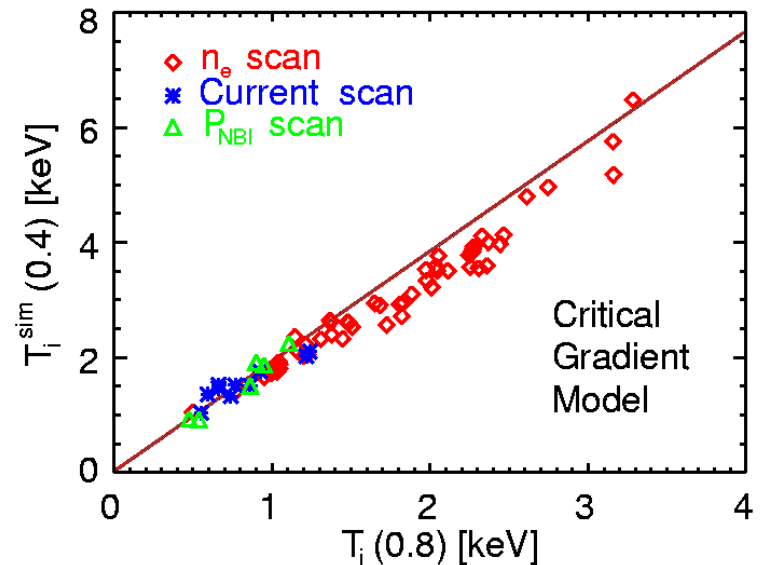
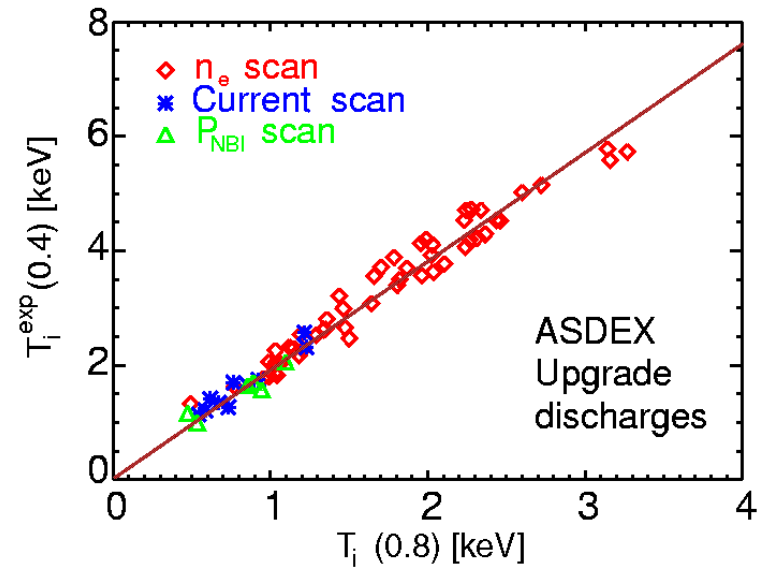
# Theoretical understanding critical gradient modes causes “stiff” temperature profiles

“Stiff” temperature profile found in experiment:  
 temperature at half radius proportional to edge temperature



Simulation results reproduce measured temperatures

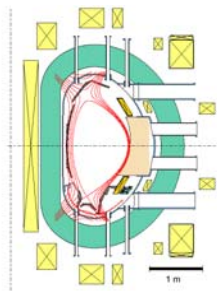
A. Peeters, G. Tardini



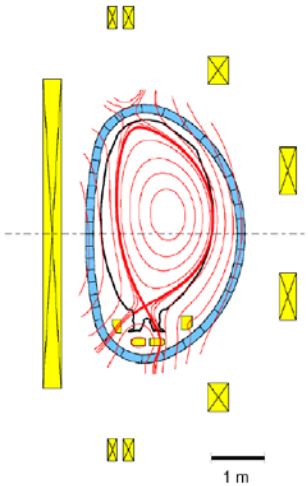
preparatory R&D in physics  
 „scaled versions of ITER “ available

ITER  
 R = 6 m

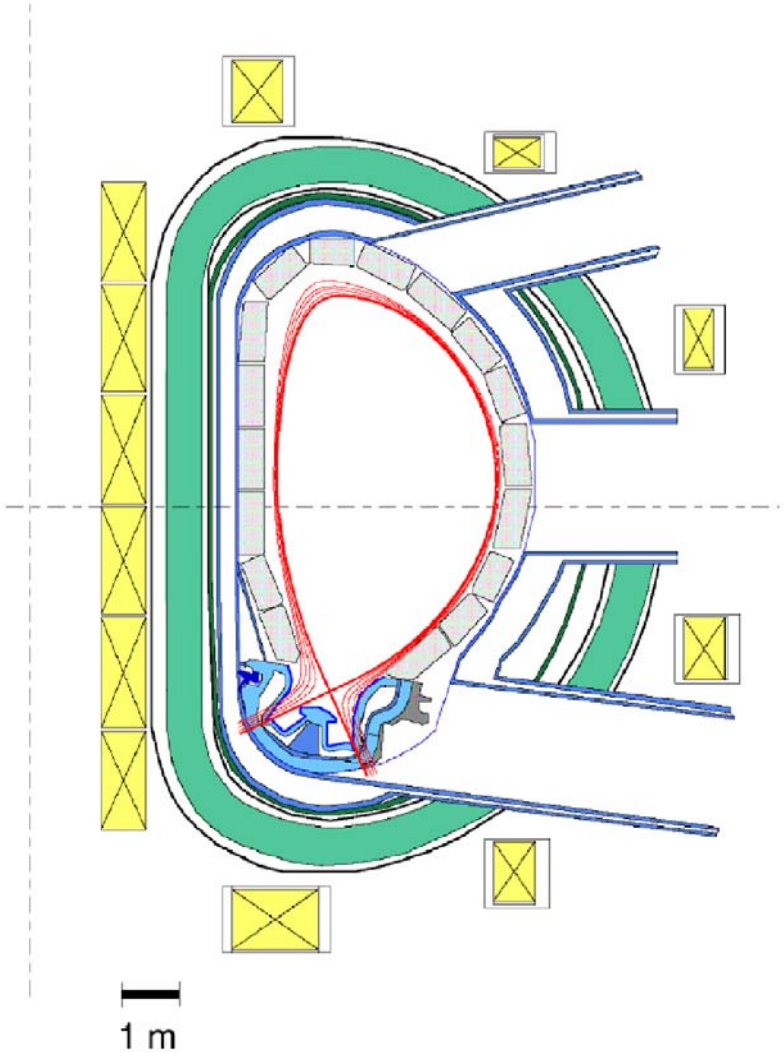
(examples EU)



ASDEX-Upgrade  
 R = 1.6m

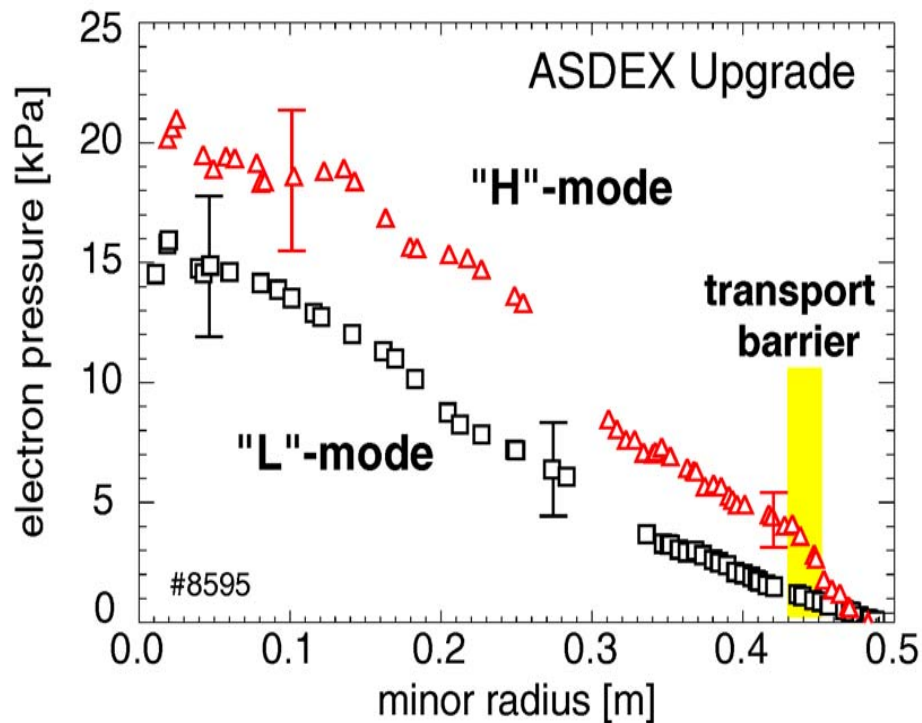


JET  
 R = 3m

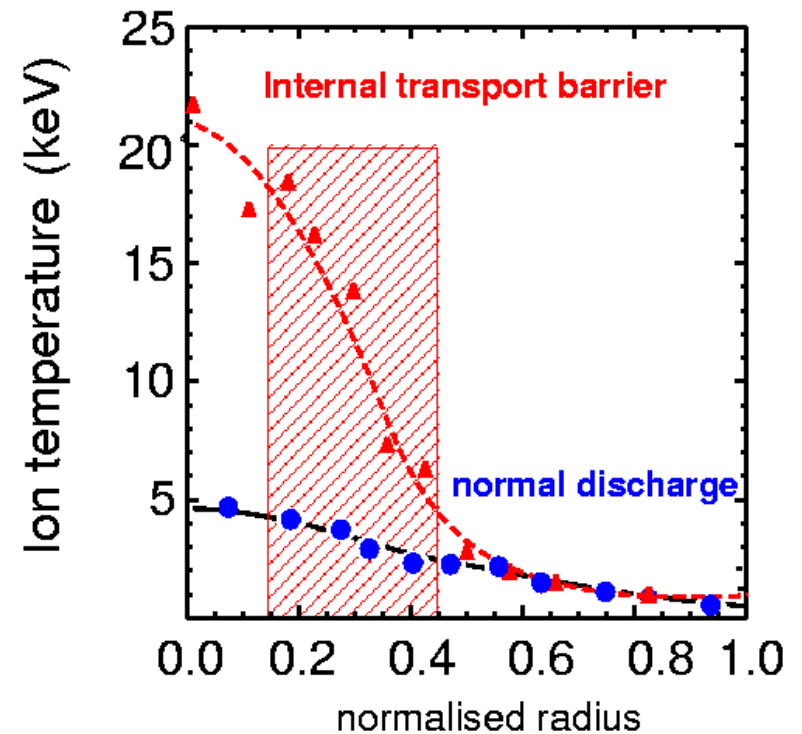


# Transport barriers due to suppressed turbulence

## Conventional Tokamak



## „Advanced Tokamak“



**For non-monotonic current profiles non-stiff profiles  
Ignition Temperature on ASDEX Upgrade!**

- baseline („conventional“) scenarios: Elmy H-mode  $Q = 10$  and „hybrid“ scenario

## single confinement barrier

physics: extrapolation of well understood regime to/in

- self heating
  - physics of  $\alpha$ -particles
  - divertor & PSI
- 
- identifiable milestone
  - technology - physics integration
  - technology test & demonstration

- advanced scenarios:

## multiple confinement barriers

develop physics: (a range of scenarios exist)

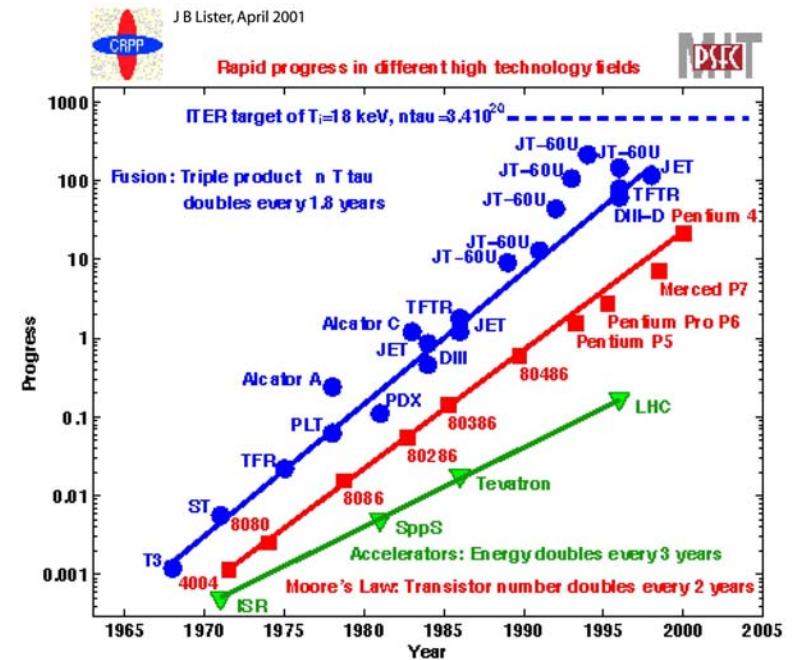
- extrapolation of regime
  - self-consistency of equilibria
  - MHD stability
  - compatibility with divertor requirements and impurity concentrations
  - compatibility with satisfactory  $\alpha$ -confinement
  - controllability
- 
- satisfy steady state objective
  - prepare DEMO

# Standard inductive scenarios



maintain momentum:

- 1) verify & extend our scalings and theory models  
(confinement, H-mode access, ELMs, NTMs..)
- 2) qualify  $\alpha$ -particle heating as a heating method
- 3) high power/long pulse (on wall equilibration time) test of plasma wall interaction (incl. tritium inventory control)



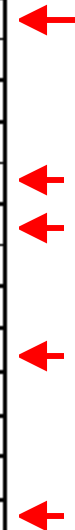


# Q= 10 reference scenario(s): milestone



Parameter	400 MW	560 MW	260 MW
R/a (m/m)	6.2/2.0	←	←
$\kappa_{95}/\delta_{95}$	1.7/0.33	←	←
$B_T$ (T)	5.3	←	←
$I_p$ (MA)	15.0	←	←
$q_{95}$	3	←	←
$\langle n_e \rangle$ ( $10^{20} \text{ m}^{-3}$ )	1.01	1.18	0.83
$\langle n_e \rangle / n_G$	0.85	1.0	0.7
$\langle T_e \rangle$ (keV)	8.8	9.0	8.7
$\langle T_i \rangle$ (keV)	8.0	8.2	7.9
$P_{FUS}$ (MW)	400	560	260
$P_{NB} + P_{RF}$ (MW)	33 + 7	33 + 23	17 + 9
Q	10	←	←
$P_{RAD}$ (MW)	47	71	30
$P_{LOSS}/P_{L-H}$	1.8 (87/48)	2.4 (124/53)	1.3 (55/42)
$\beta_N$	1.8	2.1	1.4
$\beta_P$	0.65	0.77	0.52
li (3)	0.84	0.84	0.85
$\tau_E$ (s)	3.7	3.1	4.7
$H_{H98(v,2)}$	1.0	←	←
$\tau_{He}^+ / \tau_E$	5.0	←	←
$f_{He, axis/ave}$ (%)	4.3/3.2	4.1/3.1	4.1/3.1
$f_{Be, axis}$ (%)	2.0	←	←
$f_{Ar, axis}^{*1}$ (%)	0.12	0.16	0.10
$Z_{eff, ave}$	1.66	1.77	1.60
$V_{loop}$ (mV)	75	75	82

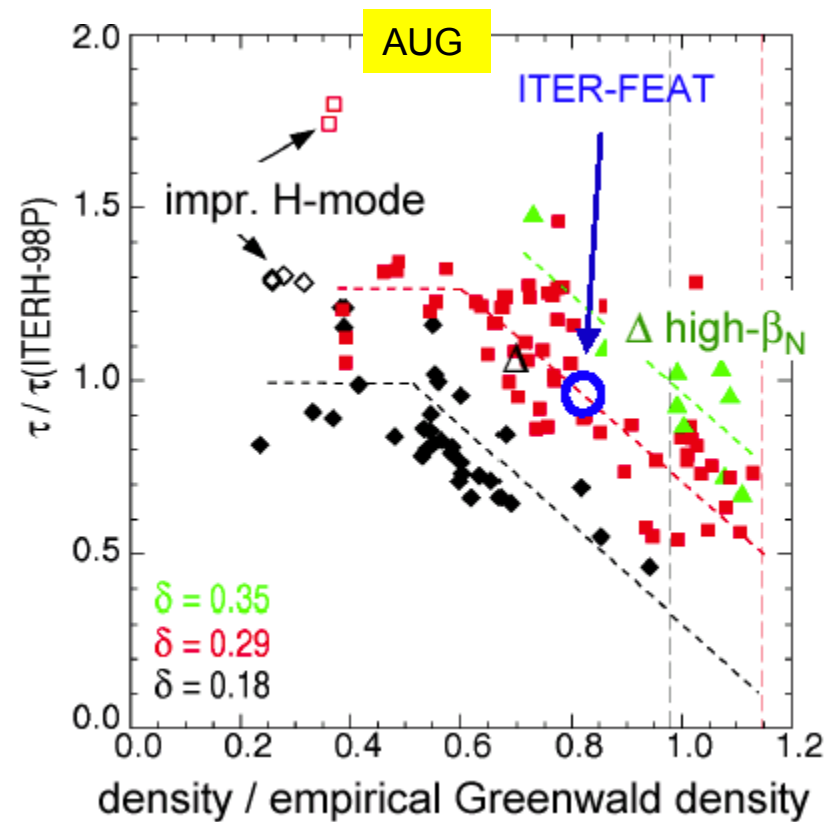
conservative requirements



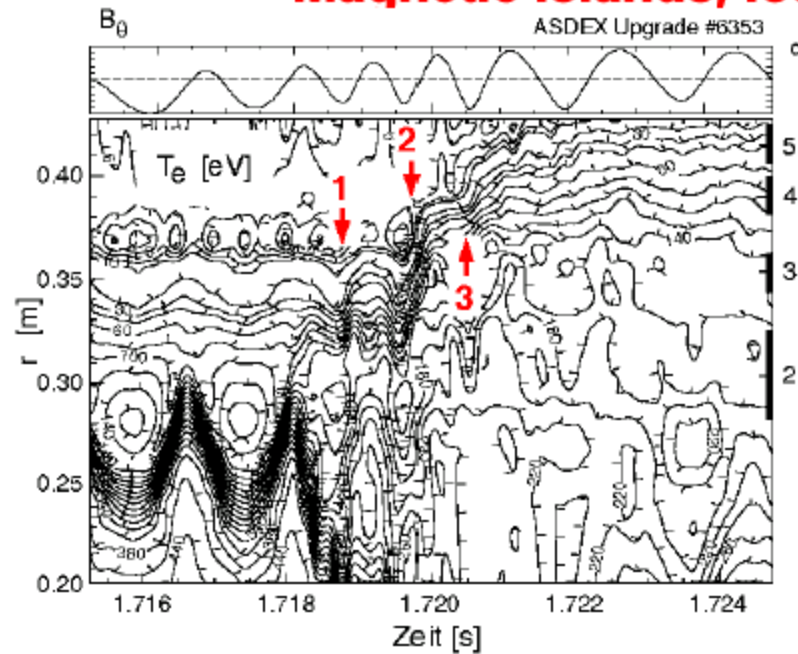
# high confidence level in attainment of $Q = 10$ results of targeted R&D



- previous major concern: high H-factor at  $n/n_{GR} > 0.85$



## Magnetic islands, loss of confinement

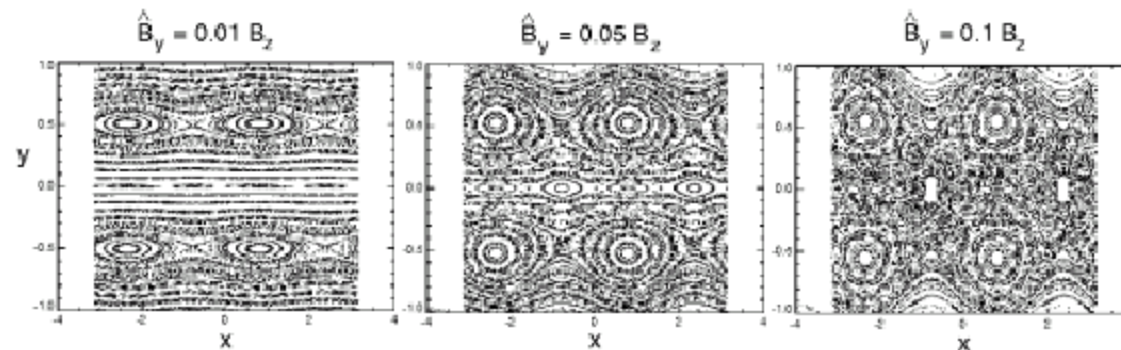


Diagnostic:  $T_e$  constant on flux surface  
Rotating islands give 2D "image"

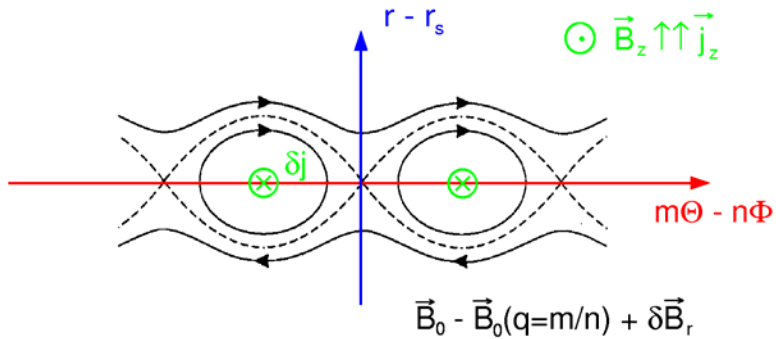
Temperature profile flattens between islands

Possible reason:  
Large islands with different helicity  
→ Ergodisation of field lines

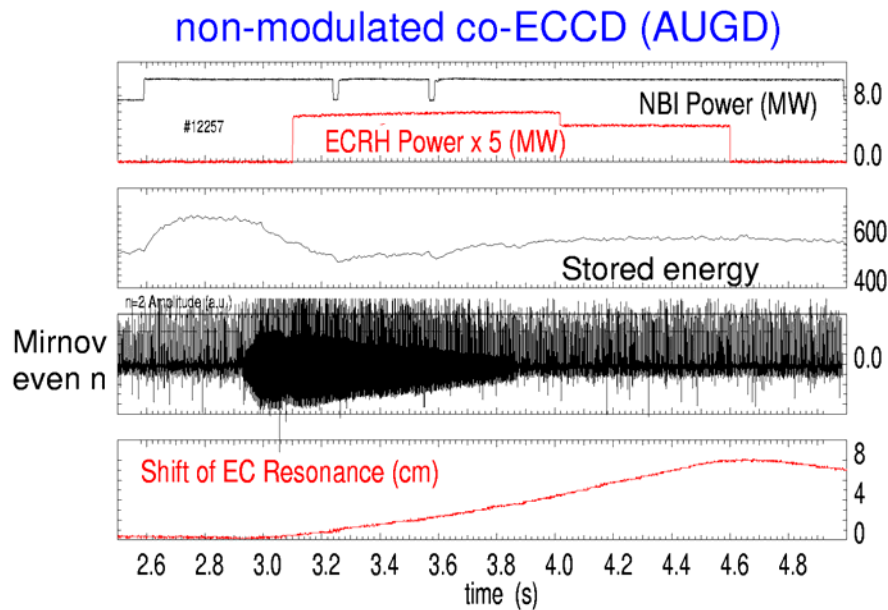
Field line tracing model (slab):



# active stabilization of NTMs



Missing bootstrap current inside island can be replaced by localised external current drive.



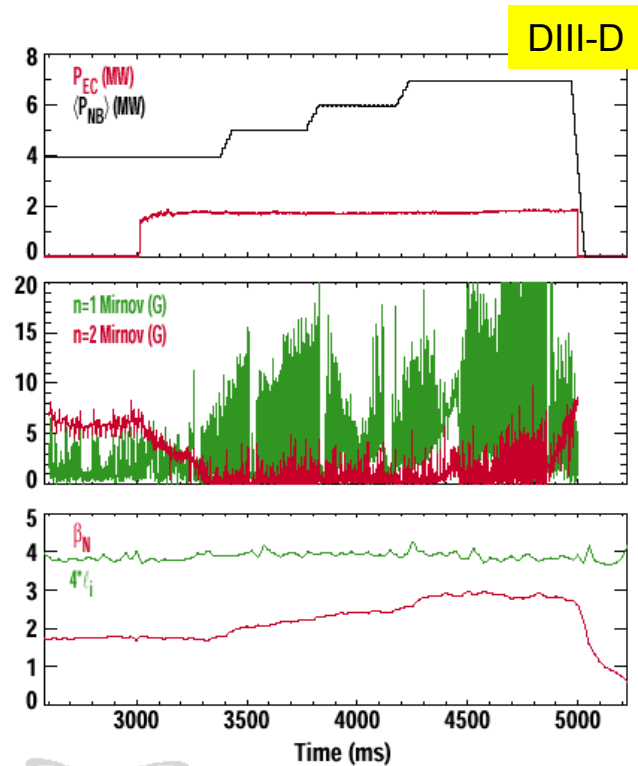
Complete stabilisation in quantitative agreement with theory!

high confidence level in attainment of  $Q = 10$   
results of targeted R&D



- NTMs:

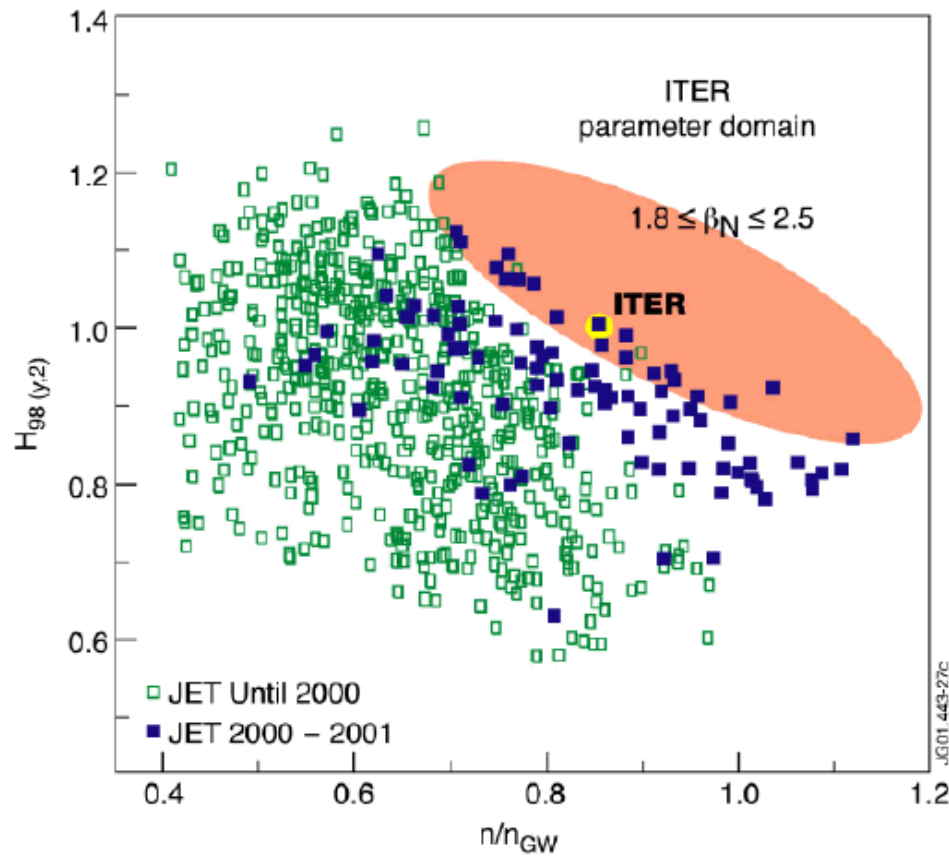
- 1) active ECRH-feedback



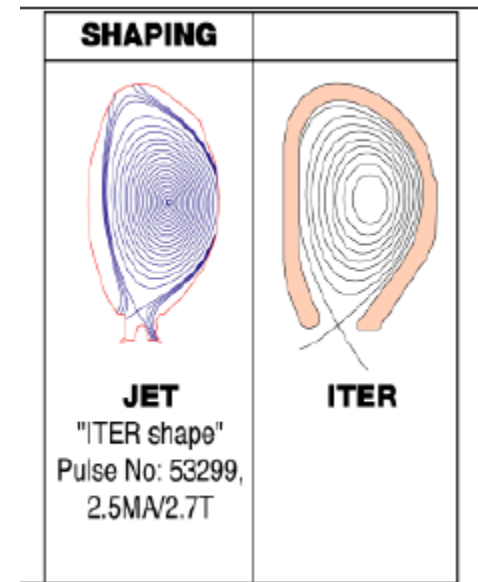
- 2) self-limitation: FIR-modes (AUG/JET)

- 3) control of sawteeth (JET)

# Q = 10: ITER-simulation discharges on JET



**JET-operating space**



$H_{98}(y,2)$	<b>0.91</b>	<b>1.0</b>
$\beta_{N,th}$	<b>1.90</b>	<b>1.81</b>
$n_e / n_{GW}$	<b>1.1</b>	<b>0.85</b>
$Z_{eff}$	<b>1.5</b>	<b>1.7</b>
$P_{rad} / P_{tot}$	0.40	<b>0.58</b>
$\kappa, \delta$	1.74, <b>0.48</b>	<b>1.84, 0.5</b>
$q_{95}$	<b>3.2</b>	<b>3.0</b>
$\tau_{pulse} / \tau_E$	15	<b>110</b>

# Preparatory R&D: Physics and technology cannot be separated:

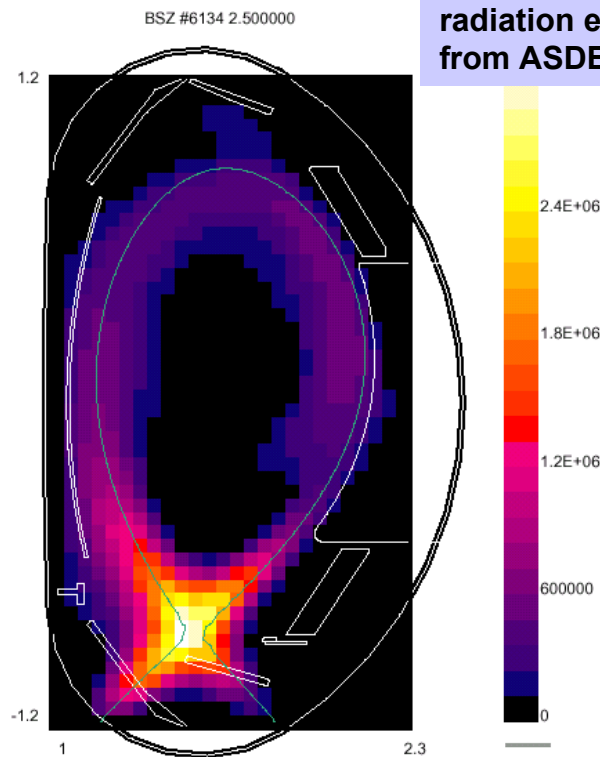


e.g.: plasma-wall interaction

at plasma-wall contact large heat fluxes

unmitigated -> 60 MW/m<sup>2</sup>  
(comparable to sun surface)

through plasma control (divertor)  
-> 5-10 MW/m<sup>2</sup>

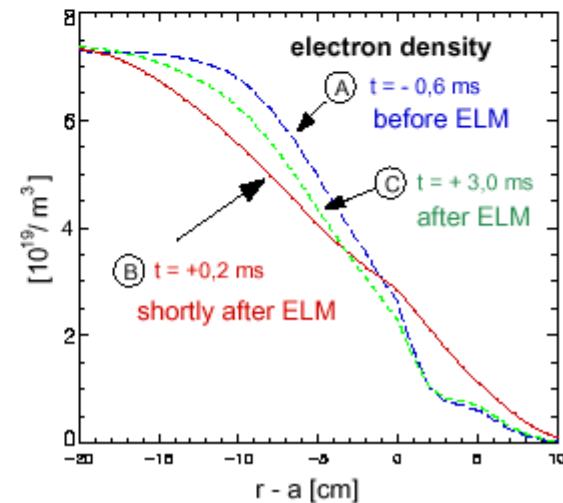
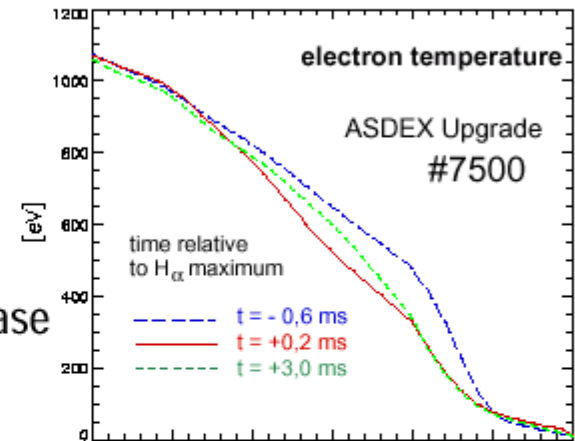
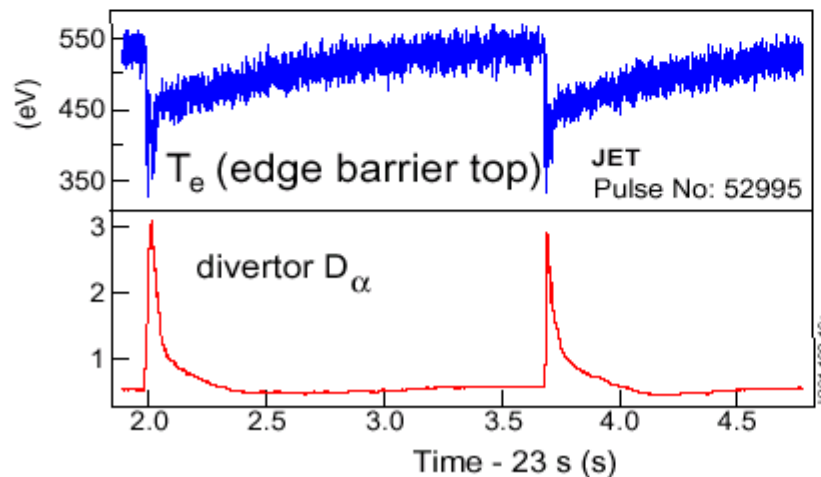


## Edge Localised Modes (ELMs)

ELM oscillations:

- A. Critical  $\nabla p$  in H-mode barrier region reached  
Short unstable phase (ELM event)
- B. Energy and particle loss has lead to reduced gradients
- C. Gradients build up during reheant/refuelling phase

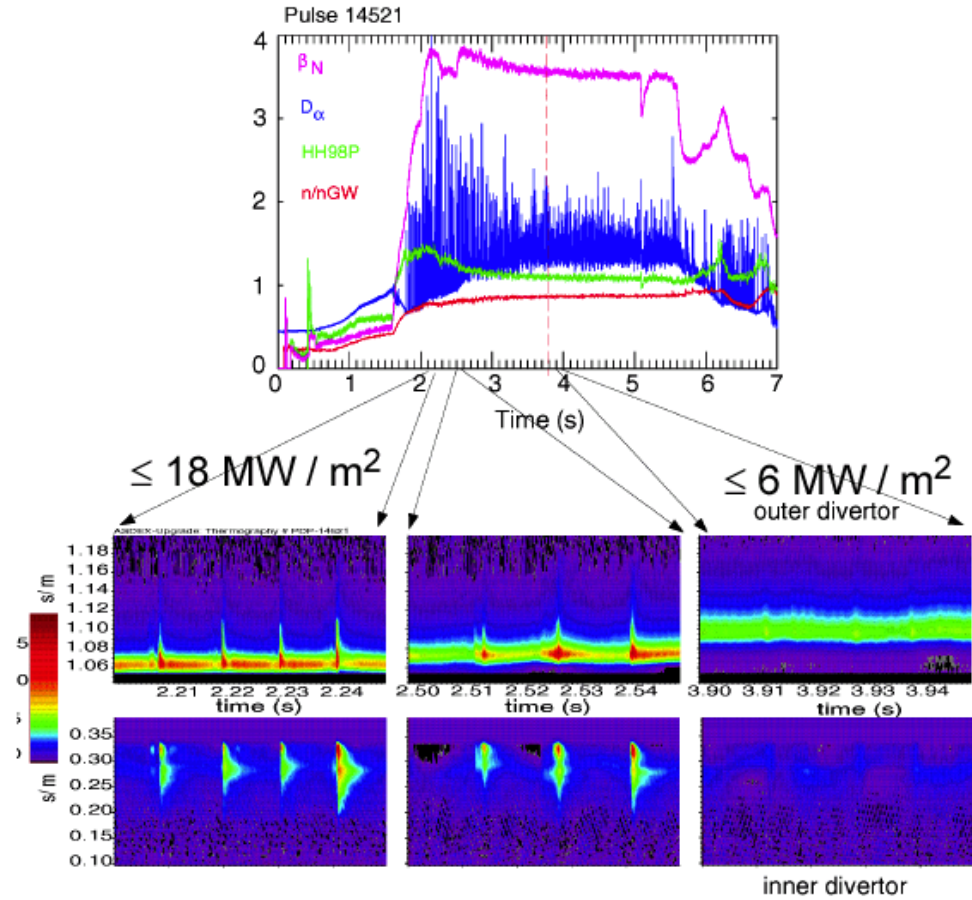
B      C      A





# Q =10: divertor issues

- **divertor & plasma wall interaction issues (ELM tolerance, tritium):**
  - determine pulses: how long & how often
  - has to be solved for any kind of fusion reactor
  - focussed effort starts bearing fruit
    - type 2 ELMs
    - control of C erosion & tritium co-deposition by surface temperature control
    - viability of W-solution
    - Be-experiments on Pisces

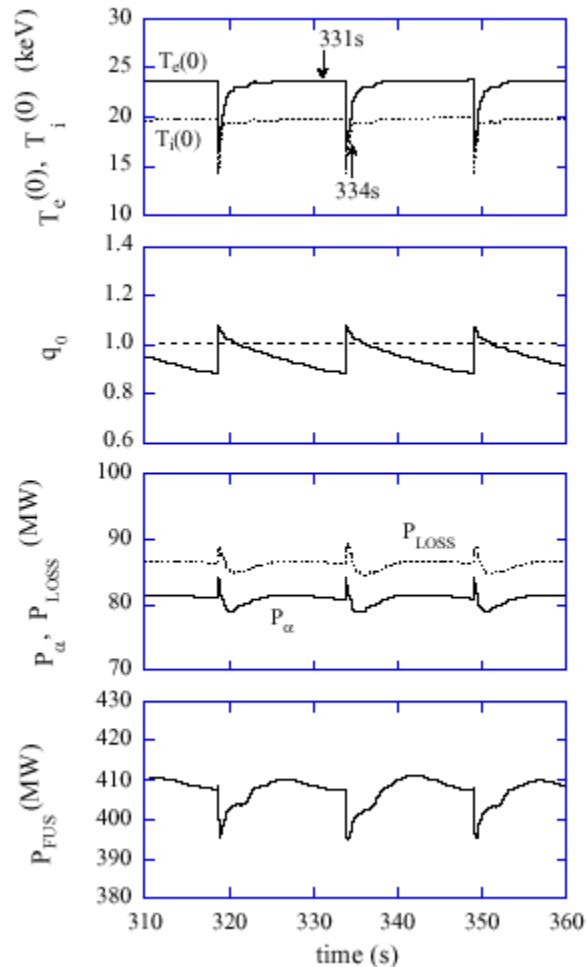


# Q =10: $\alpha$ -particle effects



## $\alpha$ -particle confinement:

- **classical confinement good** (ripple reduction through ferromagnetic inserts)
- AE-modes: for „nominal“ (monotonic) q-profiles (PENN,Mishka):
  - linearly stable or
  - weak redistribution of  $\alpha$ -particles
- fishbones: (marginally) unstable for nominal parameters

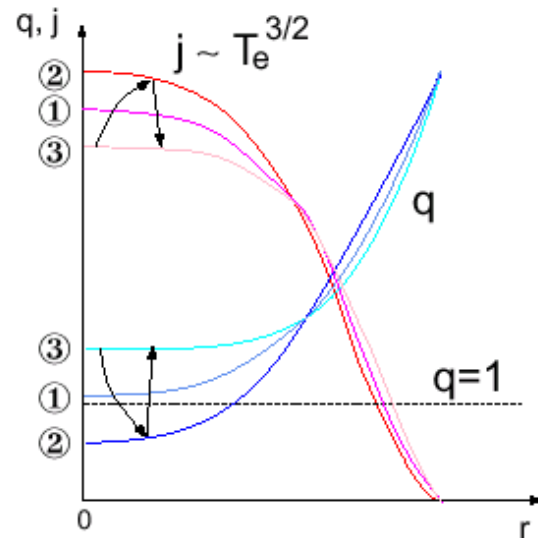


## sawteeth:

- period extended by  $\alpha$ -particle stabilisation
- 30% central T-excursion
- small effect on heat flux

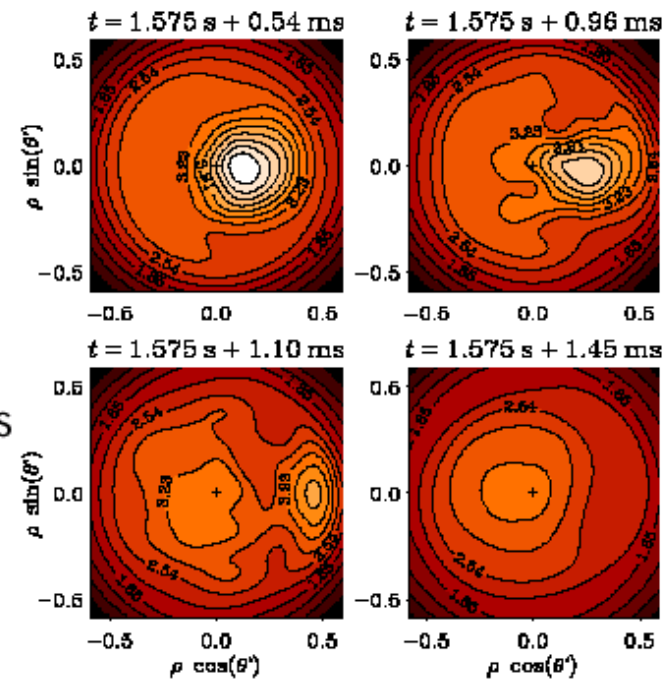
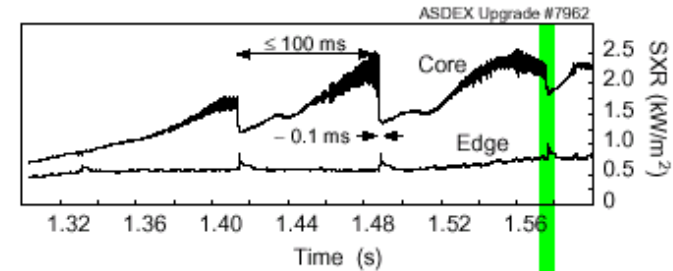
# Sawtooth oscillations

Central profiles:

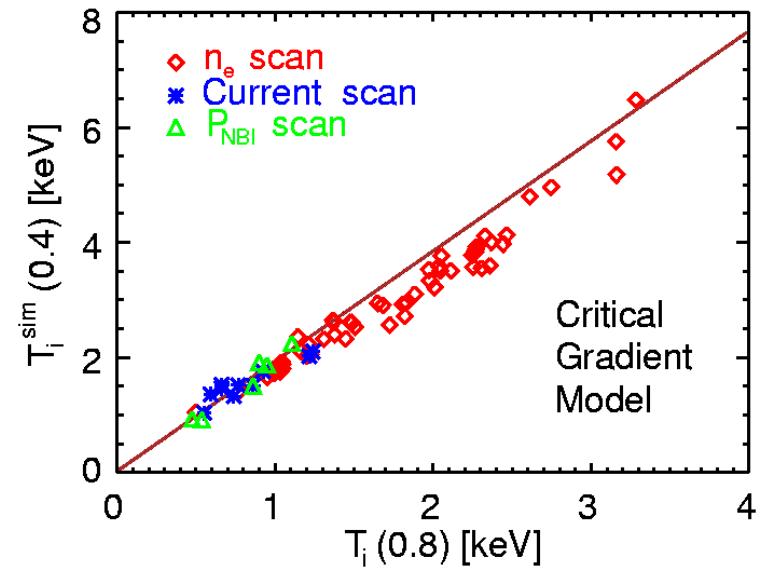
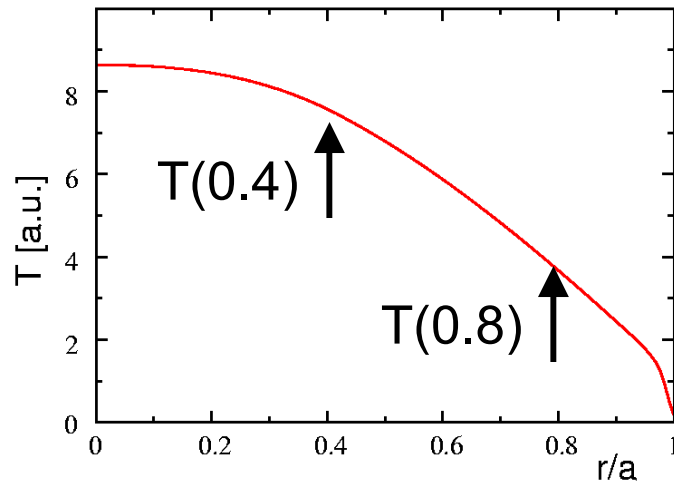


- ①  $T(0)$  and  $j(0) \propto T^{3/2}$  rise
- ②  $q(0)$  falls below 1  $\rightarrow$  kink instability grows
- ③ Fast reconnection event:

$T, n$  flattened inside  $q=1$  surface  
 $q(0)$  rises slightly above 1, kink stable



# missing understanding: scaling of pedestal?

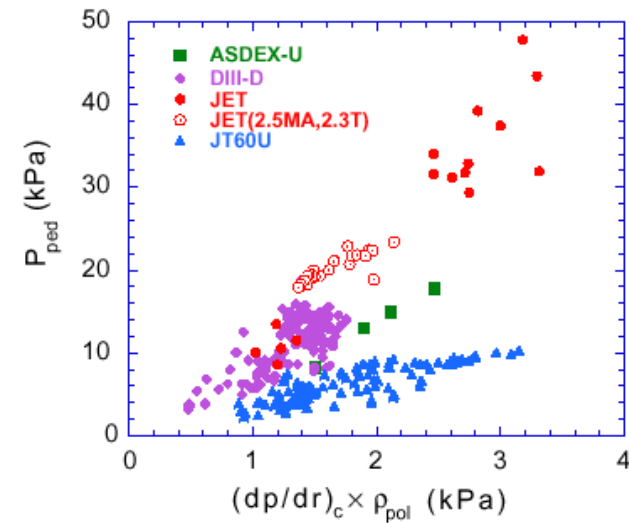
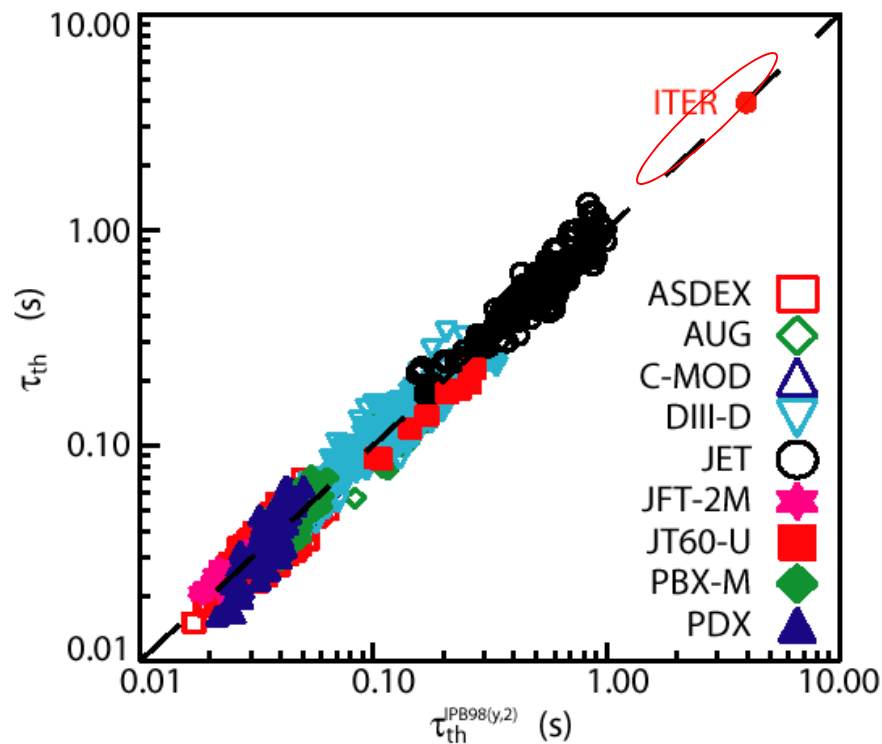


in simulations: pedestal parameters assumed input

# Extend scaling and verify theory: confinement

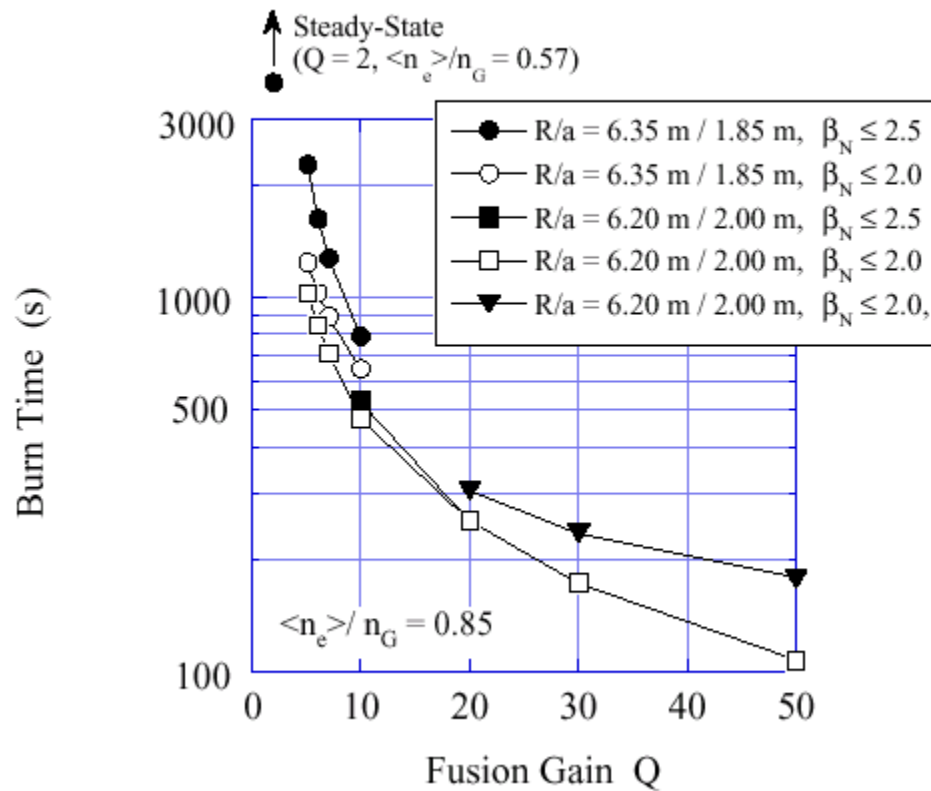
- pedestal scaling
  - pressure gradient limited
  - spatial scale?

$$R^\alpha \rho^{1-\alpha}$$



- profile stiffness
  - agreement with codes
  - role of self-generated shear-flows
  - electron transport
- role of  $n/n_{GR}$  vs  $v^*$

# hybrid scenario: conservative scenario for technology testing



	Scenario 3
	Hybrid #1
R (m)/a (m)	6.2/2.0
$\kappa_{95} / \delta_{95}$	1.7/0.33
$V_P$ (m <sup>3</sup> )	831
$B_T$ (T)	5.3
$I_P$ (MA)	13.8
$q_{95}$	3.3
$\langle n_e \rangle$ (10 <sup>19</sup> m <sup>-3</sup> )	9.3
$\langle n_e \rangle / n_G$	0.85
$\langle T_i \rangle$ (keV)	8.4
$\langle T_e \rangle$ (keV)	9.6
$\beta_N$	1.9
$P_{FUS}$ (MW)	400
$P_{NB}$ (MW)	33
$P_{RF}$ (MW)	40
$Q = P_{FUS} / (P_{NB} + P_{RF})$	5.4
$I_{CD} / I_P$ (%)	25
$I_{BS} / I_P$ (%)	17
$\gamma_{20}^{NB}$ (10 <sup>20</sup> AW <sup>-1</sup> m <sup>-2</sup> )	0.24
$\gamma_{20}^{RF}$ (10 <sup>20</sup> AW <sup>-1</sup> m <sup>-2</sup> )	0.30
$\gamma_{20}^{TOT}$ (10 <sup>20</sup> AW <sup>-1</sup> m <sup>-2</sup> )	0.27
$\tau_{He^+} / \tau_E$	5
$H_{H98(v,2)}$	1.0
$V_{loop}$ (mV)	56
Burn flux (Vs)	60
Burn time (s) <sup>*1</sup>	1070

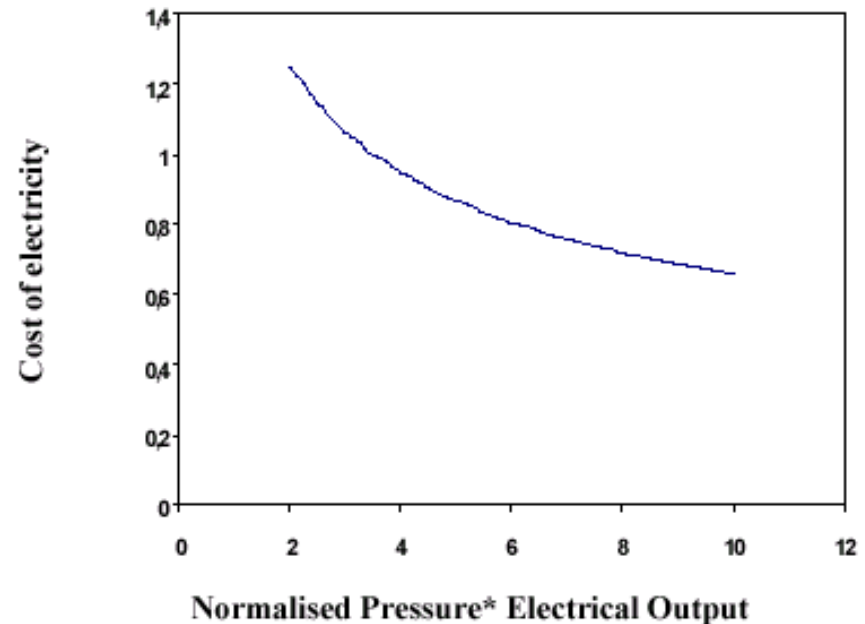


# advanced tokamak operation on ITER



- satisfy „steady-state“ objective
- prepare DEMO ( i.e. characteristics of a commercially viable reactor)
  - blue ribbon „fast track“ panel
  - fusion industry committee

- **associated physics issues match ITER capabilities**
  - $\alpha$ -physics compatibility
  - long pulse aspects
    - current profile
    - plasma surface interaction
  - heating power > current drive power
    - controllability



	ITER-baseline	ITER-steady	1 <sup>st</sup> generation reactor designs	“advanced” reactor designs
$\beta_n$	1.8	3.1	3.5 - 4	> 4
$\langle \beta \rangle$ [%]	2.5	2.9	2.2 - 3	3 - 5

# steady state („advanced“) scenarios:



- development needed
- spectrum of scenarios
- scenarios illustrative

	Scenario 4		Scenario 6	Scenario 7	
	WNS	WNS	SNS	WPS	Low-Q
R/a (m)	6.35/1.85	6.35/1.85	6.35/1.85	6.35/1.85	6.35/1.85
B <sub>T</sub> (T)	5.18	5.18	5.18	5.18	5.18
I <sub>p</sub> (MA)	9.0	9.5	9.0	9.0	11.0
K <sub>95</sub> /δ <sub>95</sub>	1.85/0.40	1.87/0.44	1.86/0.41	1.86/0.41	1.84/0.43
<n <sub>e</sub> > (10 <sup>19</sup> m <sup>-3</sup> )	6.7	7.1	6.5	6.7	5.7
n/n <sub>G</sub>	0.82	0.81	0.78	0.82	0.57
<T <sub>i</sub> > (keV)	12.5	11.6	12.1	12.5	9.3
<T <sub>e</sub> > (keV)	12.3	12.6	13.3	12.1	12.1
β <sub>T</sub> (%)	2.77	2.67	2.76	2.75	2.2
β <sub>N</sub>	2.95	2.69	2.93	2.92	1.9
β <sub>p</sub>	1.49	1.25	1.48	1.47	0.77
P <sub>fus</sub> (MW)	356	338	340	352	174
P <sub>RF</sub> + P <sub>NB</sub> (MW)	29 + 30 <sup>*1</sup>	35 + 28 <sup>*1</sup>	40 + 20 <sup>*2</sup>	29 + 28 <sup>*3</sup>	36 + 50
Q = P <sub>fus</sub> /P <sub>add</sub>	6.0	5.36	5.7	6.2	2.0
W <sub>th</sub> (MJ)	287	292	287	284	212
P <sub>loss</sub> /P <sub>L-H</sub>	2.59	2.74	2.63	2.6	3.0
τ <sub>E</sub> (s)	3.1	2.92	3.13	3.07	2.15
f <sub>Hc</sub> (%)	4.1	4.0	4.0	4.0	3.0
f <sub>Bc</sub> (%)	2	2.0	2	2	2
f <sub>Ar</sub> (%)	0.26	0.16	0.2	0.23	0.19
Z <sub>eff</sub>	2.07	1.87	1.89	1.99	1.86
P <sub>rad</sub> (MW)	37.6	30.6	36.2	34.6	22
P <sub>loss</sub> (MW)	92.5	100.0	91.6	92.7	99
l <sub>i</sub> (3)	0.72	0.43	0.6	0.69	0.58
I <sub>CD</sub> /I <sub>p</sub> (%)	51.9	49.7	53.7	50.2	73.6
I <sub>bs</sub> /I <sub>p</sub> (%)	48.1	50.3	46.3	49.8	26.4
I <sub>OH</sub> /I <sub>p</sub> (%)	0	0	0	0	0
q <sub>95</sub> /q <sub>0</sub> /q <sub>min</sub>	5.3/3.5/2.2	5.0/3.8/2.7	5.4/5.9/2.3	5.3/ 2.7/2.1	4.1/ 1.5/1.3
H <sub>H98(y,2)</sub>	1.57	1.46	1.61	1.56	1.0
τ <sub>Hc</sub> <sup>*</sup> /τ <sub>E</sub>	5.0	5.0	5.0	5.0	5.0



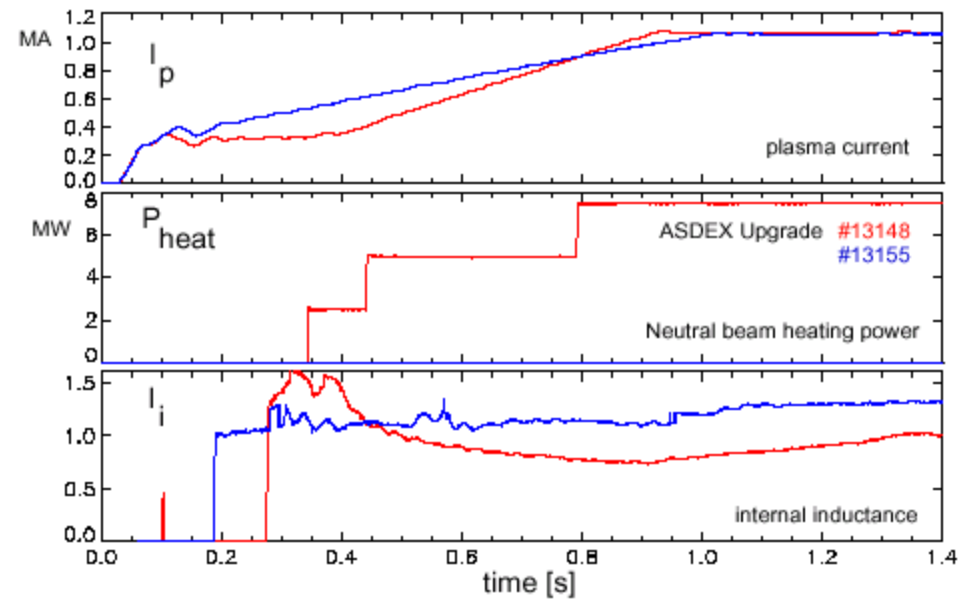
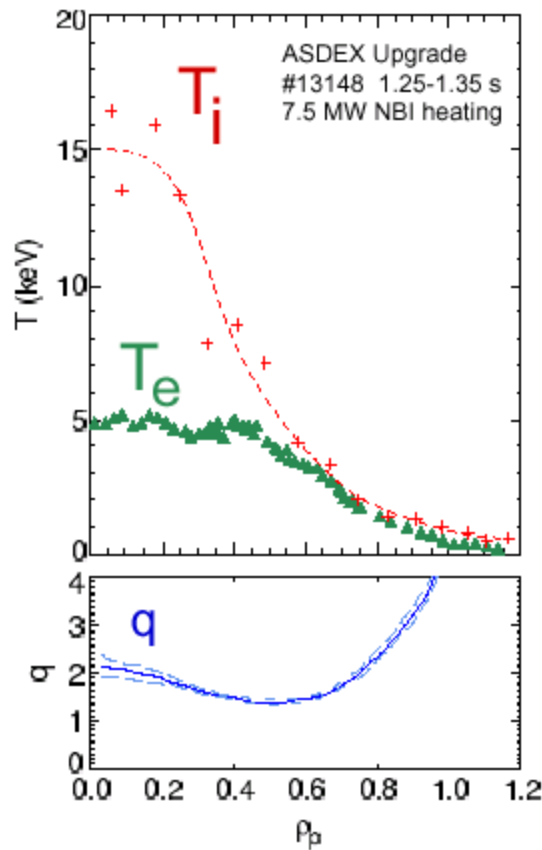


Recent discovery (~1990s): transport barriers in the plasma core

Weak or negative central magnetic shear  $S = (r/q) dq/dr$

Transport barrier (ions and/or electrons) can develop

Technique: Fast current ramp with heating  
 → skin effect raises edge  $j$



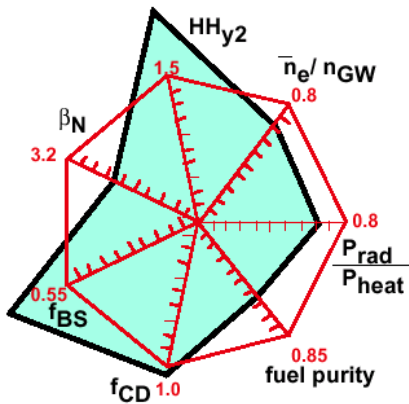
# extrapolation and extension of regime

approach to ITER s.s.-targets in dimensionless *performance* parameters:  
the 7-fold way\*)

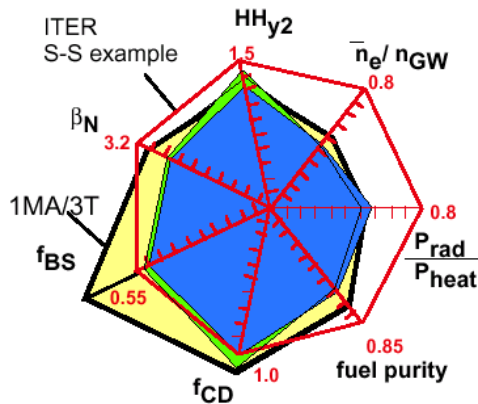
\*) + pulse length: -> only full CD,ELMy H-mode cases shown

smaller q (implied by high  $f_{BS}$ , low  $\beta_N$ )

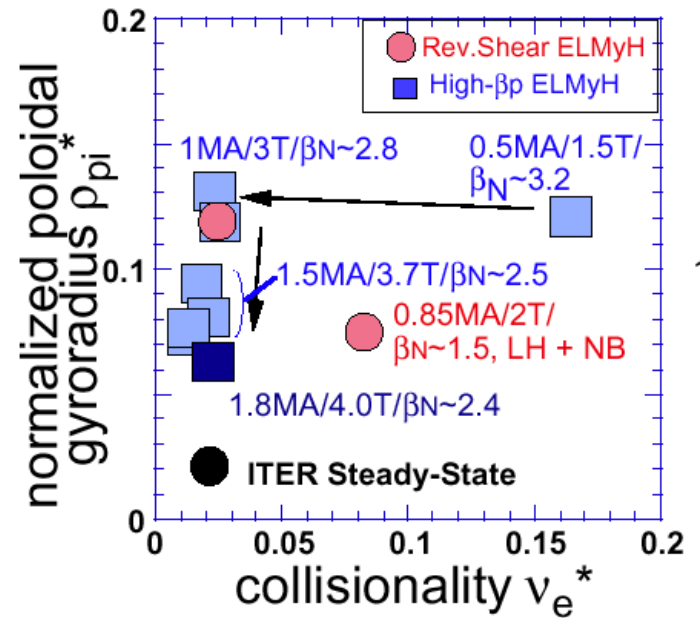
JT-60U RS



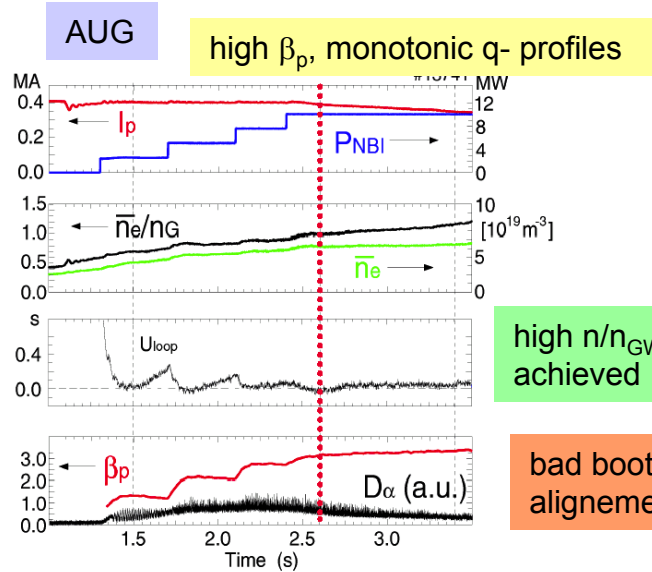
JT-60U high  $\beta_p$



ITER & Power Plant:  
higher  $n/n_{GW}$  but lower  $v_e^*$  !



self-consistency of parameters and profiles: a range of „advanced“ regimes exist



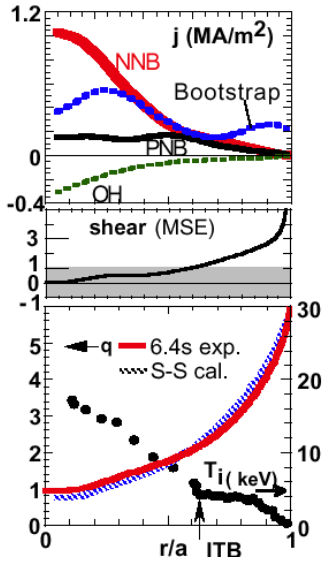
high  $n/n_{GW}$  achieved

bad bootstrap alignment

good bootstrap alignment

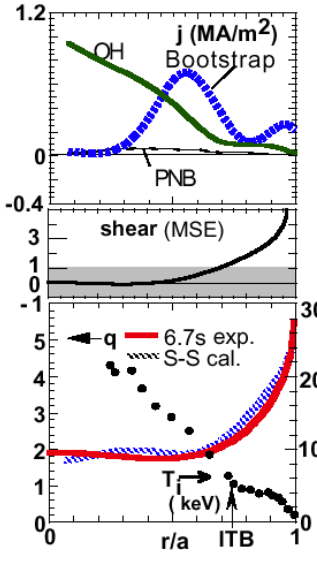
difficult  $\alpha$ -particle confinement

**central CD+ bootstrap**  
 $q_{95}=4.8, \beta_N=2.5, HH_{y2}=1.4$

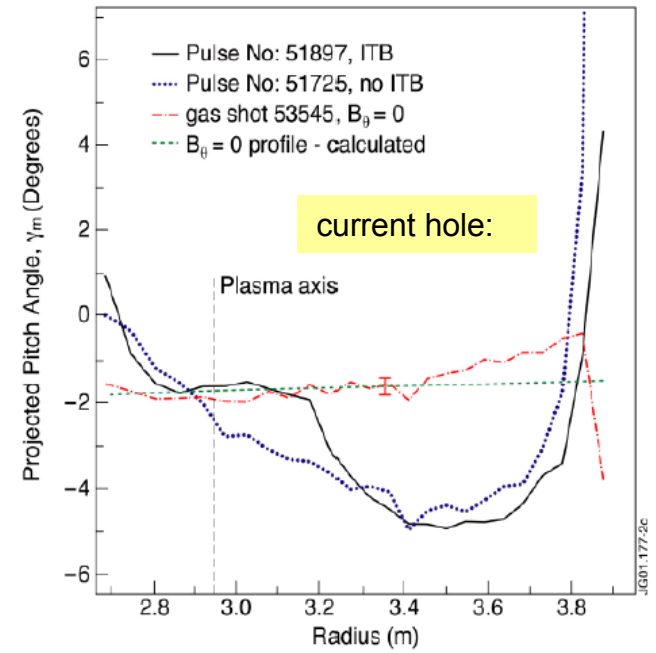
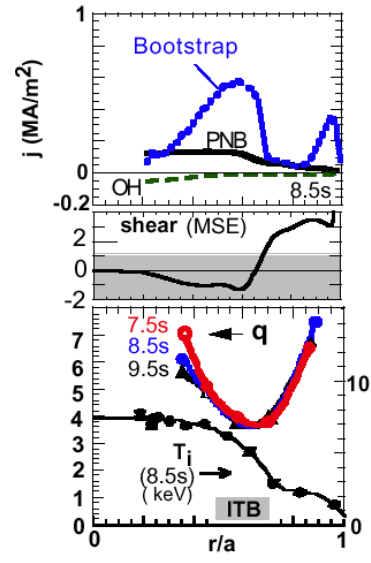


JT60-U

**bootstrap**  
 $\beta_N=2.8, HH_{y2}=1.5$

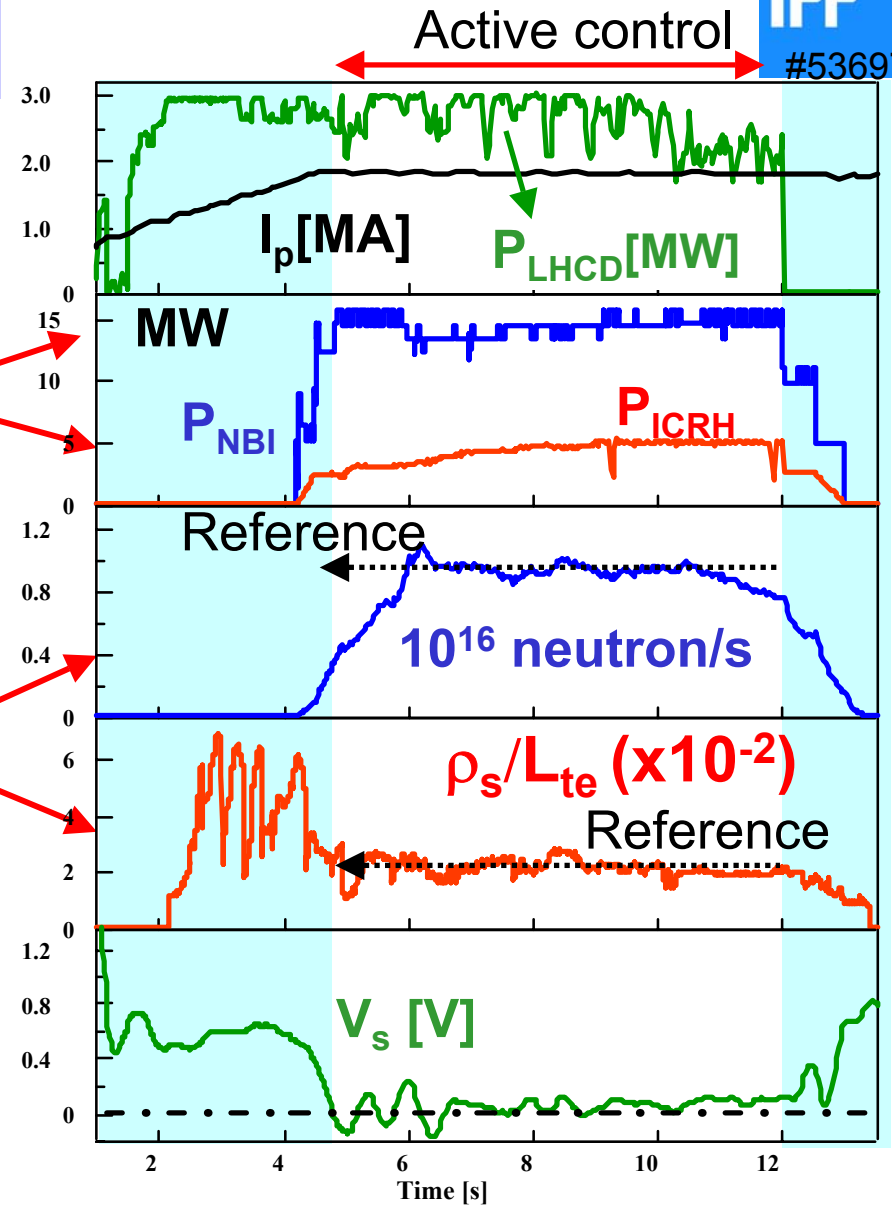


**broad CD + high bootstrap**  
 $q_{95}=9.3, \beta_N=2.2, HH_{y2}=2.2$



JET: LHCD

# „advanced scenarios“ control



High non-inductive current fraction  
reducing current profile development

ITB existence criterium and control  
parameter  $\rho_T^* = \rho_s / L_T > \rho_{ITB}^*$

long pulse feedback control of  
JET ITB discharges

# $\alpha$ -particle physics and self-heating in advanced scenarios



significantly more problematic than in standard scenarios

to allow study of instability effects: improve „classical confinement“ – ferritic inserts

	Inductive		Weak RS (#4)		Strong RS	
	No FI	With FI	No FI	With FI	No FI	With FI
Total particle loss fraction (%)	2.15	negligible	6.5	0.08	21	0.75
Total power loss fraction (%)	0.65	negligible	2.5	0.04	9.3	0.13
Peak FW heat load (MWm <sup>-2</sup> )	< 0.1	negligible	0.23	0.005	0.8	0.025
Plasma current (MA)	15		10		10	

Parameter	NBI	ICRH	$\alpha$ 's (TFTR)	$\alpha$ 's (JET)	$\alpha$ 's (1998)	$\alpha$ 's (FEAT)
$P_f(0)$ [MWm <sup>-3</sup> ]	3	1-3	0.3	0.16	0.3	0.44
$\delta_f/a$	0.05	0.3	0.3	0.34	0.05	0.08
$n_f(0)/n_e(0)$ [%]	13	1-10	0.3	0.17	0.3	0.8
$\beta_f(0)$ [%]	0.9	1-3	0.26	0.3	0.7	1.1
$\langle \beta_f \rangle$ [%]	<b>0.4</b>	<b>0.5</b>	<b>0.03</b>	<b>0.04</b>	<b>0.2</b>	<b>0.16</b>
$\max  R \cdot \nabla \beta_f $	<b>0.04</b>	$\approx 0.1$	<b>0.02</b>	<b>0.016</b>	<b>0.06</b>	<b>0.08</b>
$v_f/v_A(0)$	0.35	$\approx 1-2$	1.6	1.4	1.9	1.8

relevant for D –KAE:

$$\frac{\omega^*}{\omega_{TAE}} \cong 2nq^2 \rho^{*2} (R\omega_{pi}/c)$$

„synergies“ between AE core losses and ripple edge losses?

# pulse length & duty cycle

Moreau: simulation of ITER-FDR \*) feedback control with fuelling, FWCD & LHCD



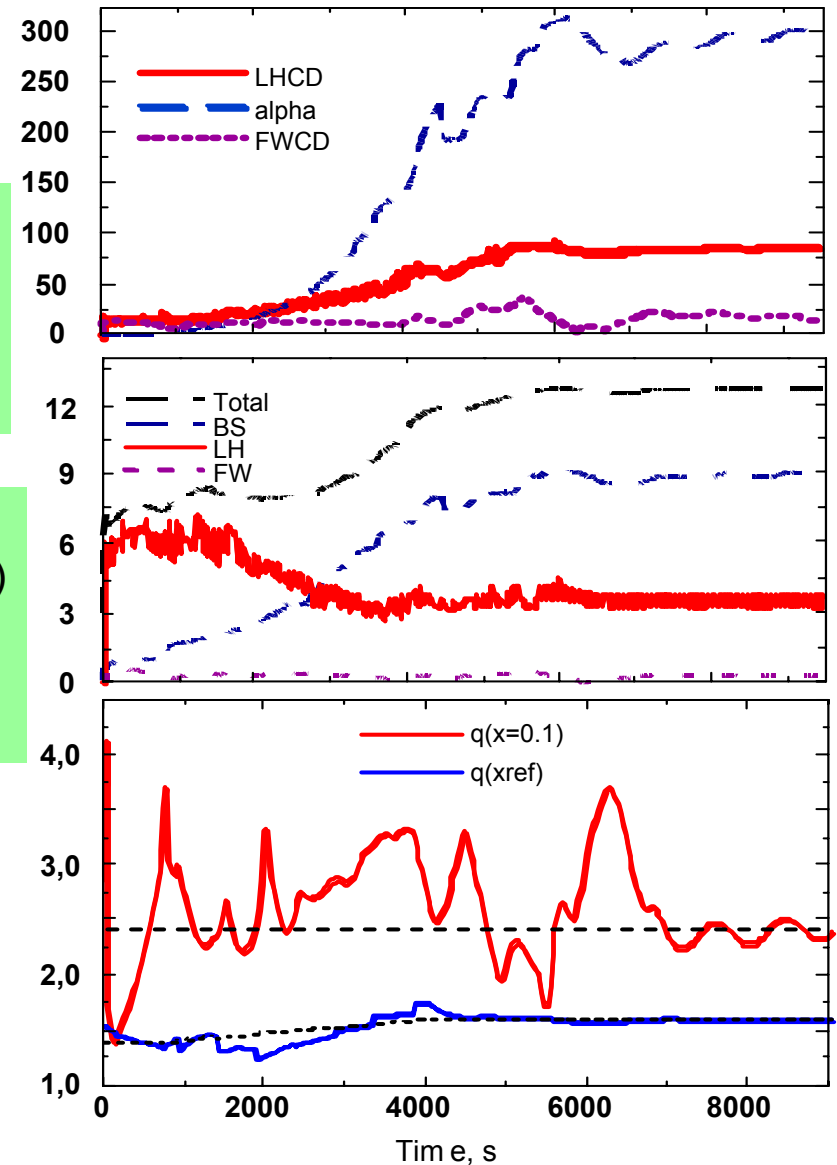
scenario	burn time*) [sec]
inductive, (reference)	500
hybrid	1000
steady-state	3000* *)

• high availability:  
 → ample time & opportunity for experiments

• (although observation of current diffusion on  $\tau \sim \tau_{skin}$ )  
 execution of control:  
 →  $\tau \gg \tau_{skin}$

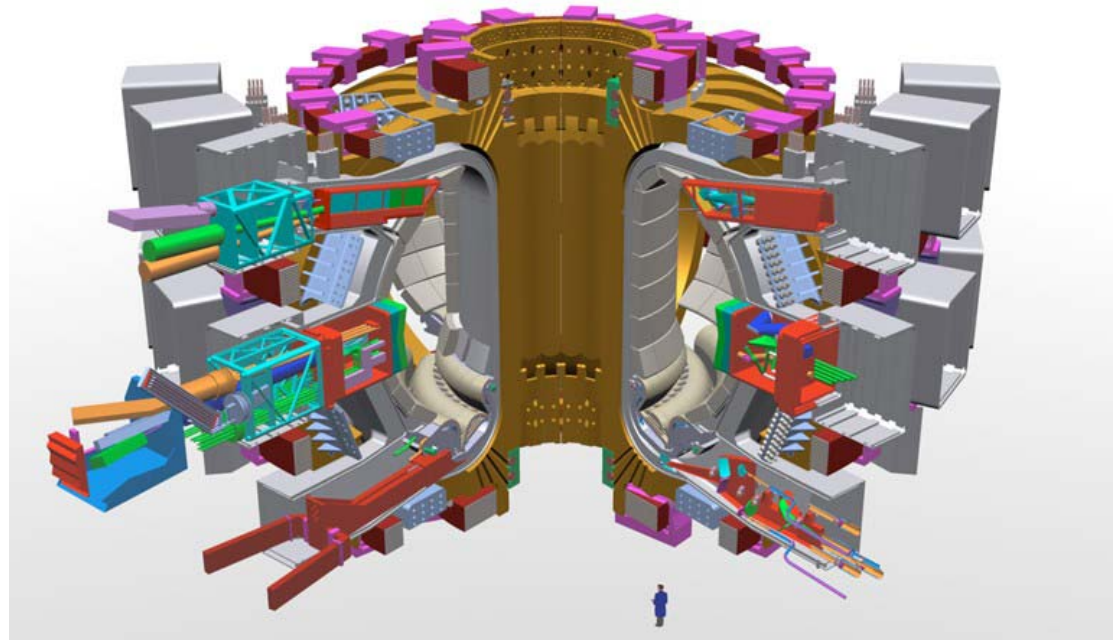
\*) repetition time = 4 x burn time

\*\*) (at present) limited by external cooling capacity



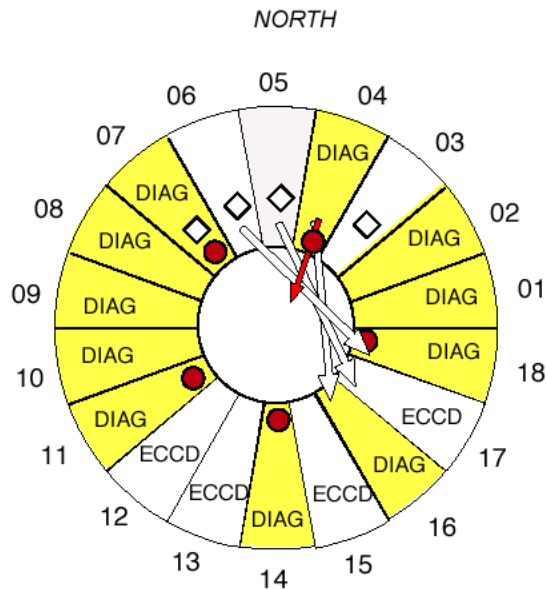
\*) reduce times by factor of 2 for ITER-FEAT

# diagnostic access & facilities



## ITER

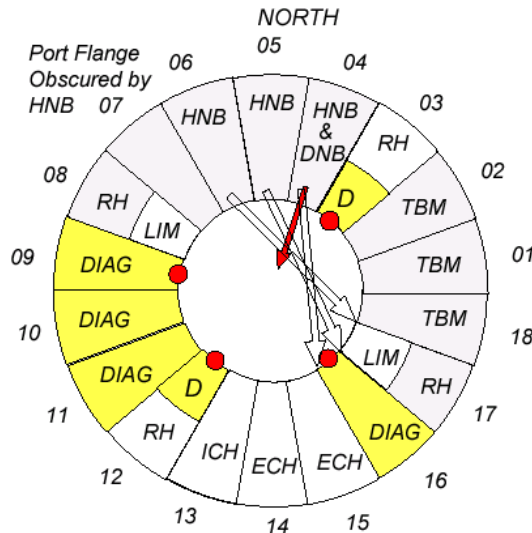
### UPPER PORT



- |   |  |
|---|--|
| 1 Active Spectr (MSE)<br>Neutron Act syst ( $^{16}\text{N}$ )       | 9 H-alpha/Vis. spec (upper edge)                           |
| 2 H-alpha /Misspec(inner edge)<br>Main plasma reflect.              | 10 VUV,<br>X-ray Crys Array<br>Neutron Act syst (foil)     |
| 3 Neutron Camera $\diamond$   | 11 Edge Thomson scattering<br>Wide angle viewing/IR        |
| 4 CXRS(pol rotn - DNB)<br>Wide angle viewing/IR                     | 14 Wide angle viewing/IR<br>Position Reflectometry         |
| 5 Neutron Camera $\diamond$<br>Neutron Act syst ( $^{16}\text{N}$ ) | 16 Bolometry<br>Soft X-Ray<br>Divertor Impurity (div16)    |
| 6 Neutron Camera $\diamond$<br>Neutron Act syst (foil)              | 18 Wide angle viewing/IR<br>H-alpha/Vis. spec (outer edge) |
| 7 Neutron camera $\diamond$<br>Wide angle viewing/IR                |  |
| 8 Bolometry<br>Position Reflectometry                               | all In-vessel diagnostic wiring                            |

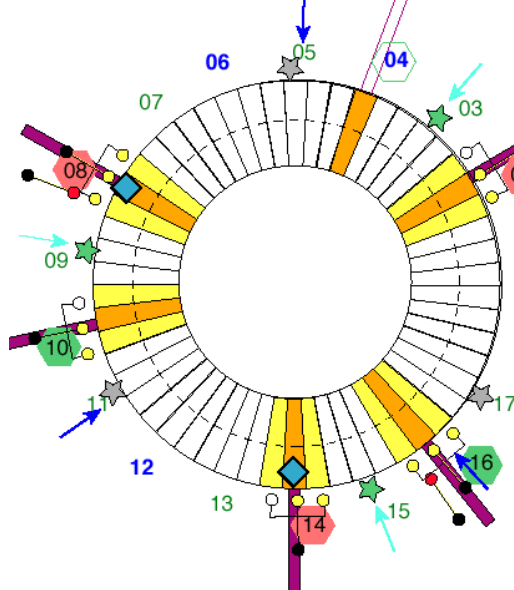
diagnostic  
access  
&  
facilities

**EQUATORIAL PORT**



- 3 Wide angle viewing/IR CXRS (with DNB) MSE (with heating NB) H-alpha/Vis spect (Div).
- 4 DNB
- 7 Obscured port
- 8 RH plus Limiter Neutron flux monitor
- 9 Wide angle viewing/IR Tor./Interfer. polarimeter ECE Fast Wave Reflectometry (possibly) MSE
- 10 LIDAR Thomson Scattering Polarimeter
- 11 X-ray Cryst spec NPA VUV (main & div.) Reflectometry
- 12 Wide angle viewing/IR H- $\alpha$  /Vis. spec (upper edge) Vis. continuum array
- 16 Wide angle viewing/IR Radial Neutron Camera Bolometry Soft x-ray array Divertor Impurity (div 16)
- 17 RH plus Limiter Neutron flux monitor Neutron Act syst (foil &  $^{16}\text{N}$ )
- Unassigned: Collective scattering

**DIVERTOR**



- 2 VUV Impurity Monitor (g) IR Thermography (c) Langmuir Probes Magnetics Thermocouples
  - 4 CXRS(c) Dust measurement(g), Magnetics
  - 8 Reflectometry/Interferometry(g) LIF (c) Bolometry , Magnetics Pressure Gauges
  - 10 X-point LIDAR (c) Div Thomson Scattering (g) Bolometry, Magnetics Langmuir Probes Pressure Gauges,
  - 14 Reflectometry/Interferometry (g) Plate Erosion (c) Magnetics, Thermocouples Langmuir Probes
  - 16 Visible Div Impurity Monitor (c,g) Bolometry, Magnetics Pressure Gauges, Thermocouples
- Port
- Red hexagon: Div. RH large ports
  - Green hexagon: RH-like diag. ports
  - Green star: GDC & IVV (L) plugs
  - Grey star: IVV (L)
  - Cyan arrow: Gas (GIS) & Pellet (PIS) (tubes)

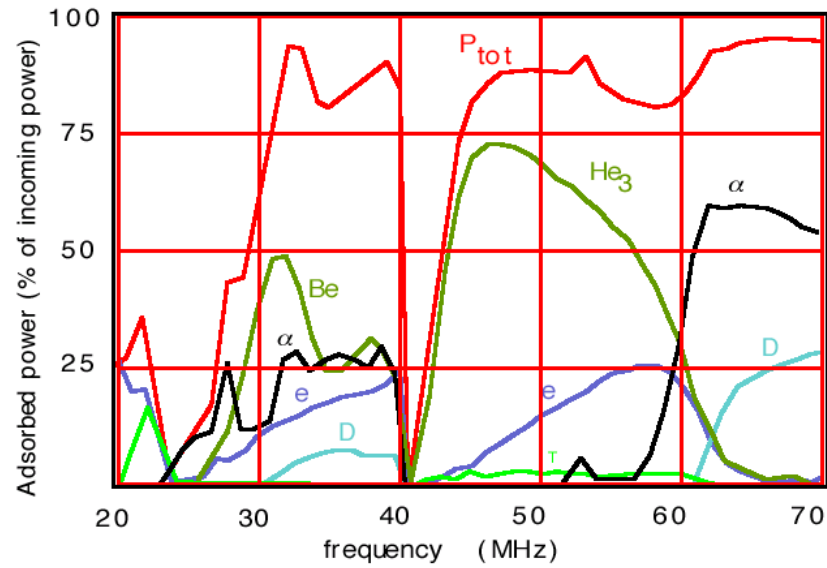




# heating & current drive systems



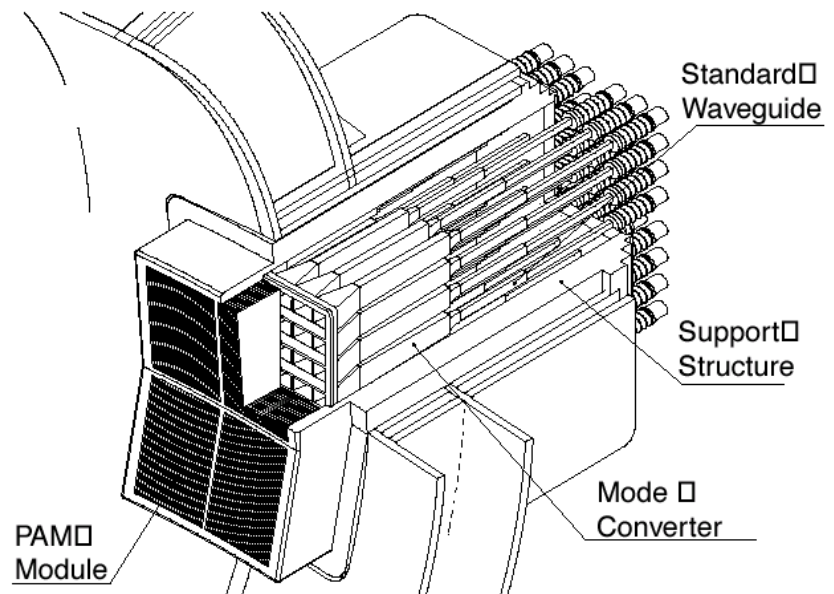
ITER- $\omega$  range



IC power absorption by species

heating system	stage I	possible upgrade by	remarks
NBI (1MeV negative ion)	33	16.5*	vertically steerable (z at $R_{tan}$ : -0.42m to +0.16m)
ECR H&CD (170 GHz) (+2MW 120 GHz for start-up)	20	20	equatorial port & upper port launcher; steerable
ICR H&CD (40 – 60 MHz)	20		$2\Omega_T$ (50% power to ions), $\Omega_{3He}$ (70% to ions); FWCD
LH H&CD (5GHz)		20	$1.8 < n_{  } < 2.2$
<b>total</b>	73	130 (110 simultan.)	upgrade in different RF combinations possible
ECRH start-up system (120 GHz)	2		
Diagnostic Beam (100 keV H, neg. ion?)	>2		

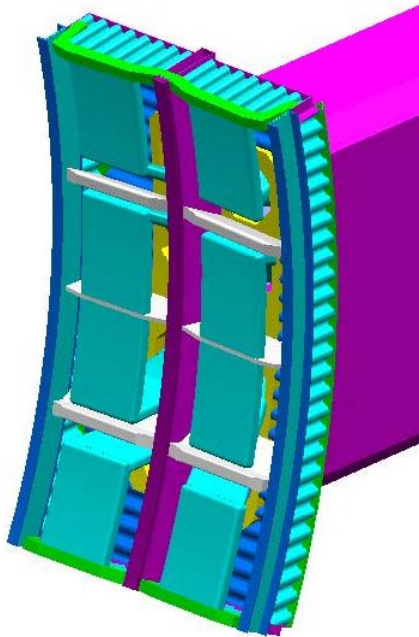
LH-launcher; based on Passive-Active Multi-junction principle\*)  
 \*) to be tested on FTU, Tore-S.



# preparatory physics R&D for ITER heating in JET

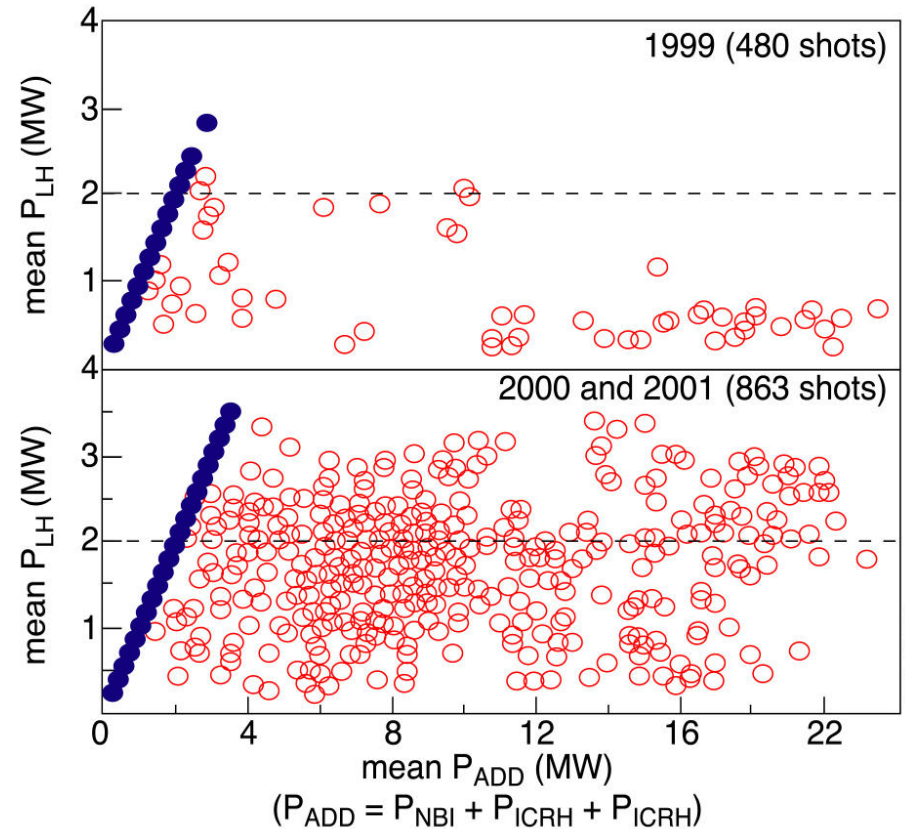
## the JET ICRH ITER-like antenna (2005)

- 7.5 MW at ITER relevant coupling (2-4 W/m)
- High coupling efficiency (90%) in range  $30 < f < 55$  MHz
- ELM resilient

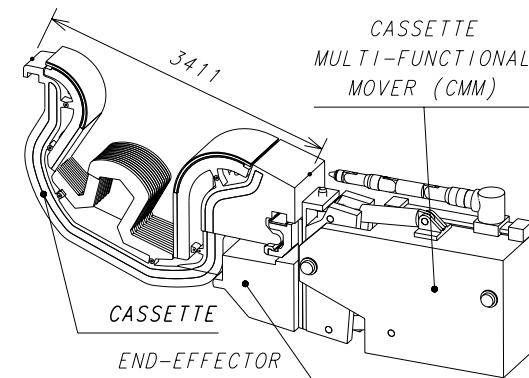
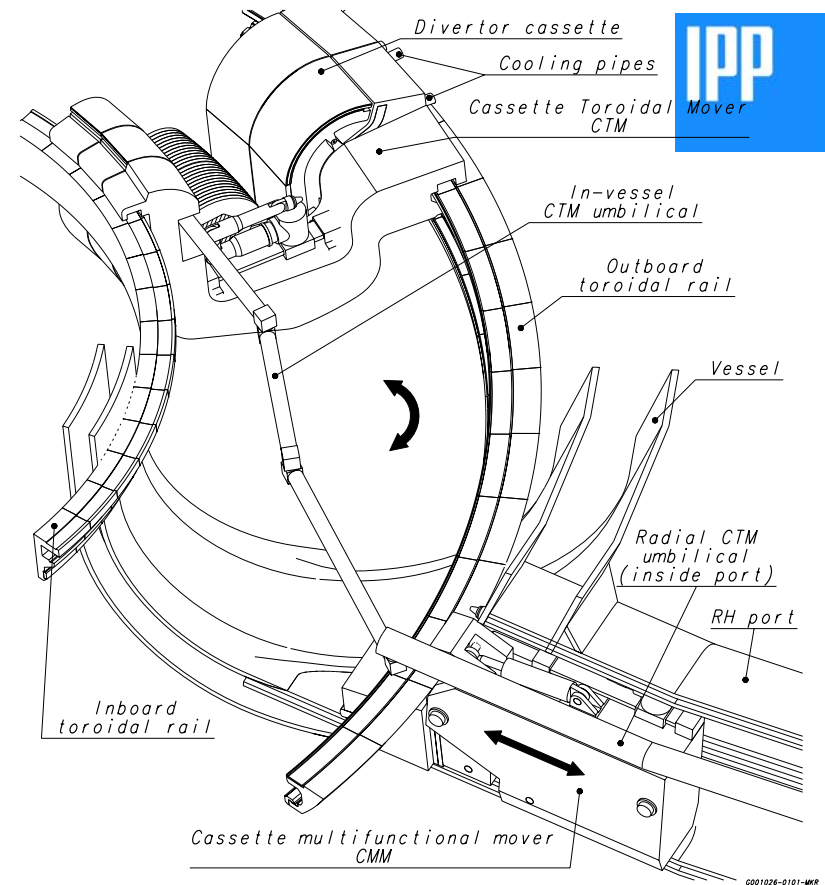
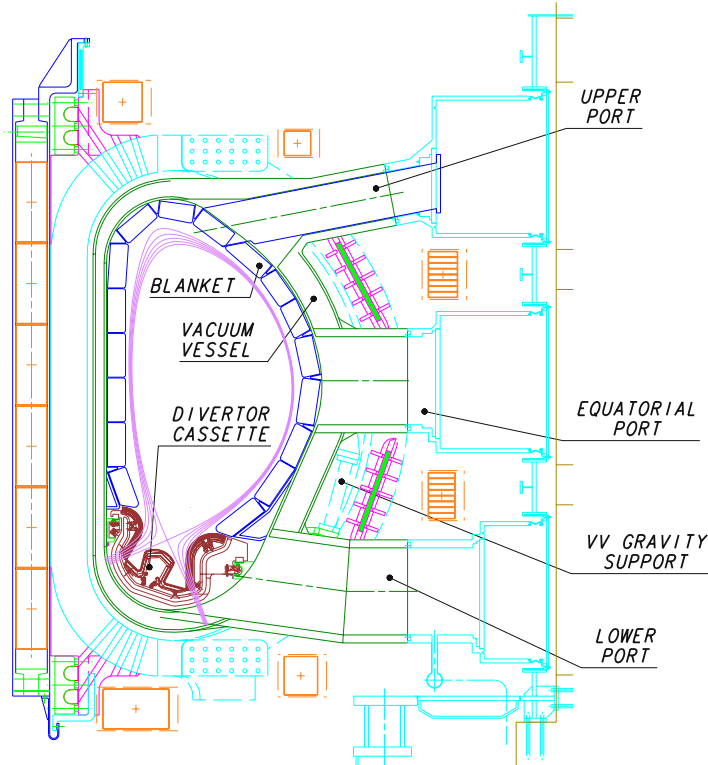


strong effort to increase LH availability *in combination with other heating systems*

- Plasma with LHCD + ICRH + NBI
- Plasma with LHCD only



# flexibility through divertor maintenance and exchange capability



for refurbishment and design-improvements  
divertor cassette system allows  
replacement of divertor within 6 months:

# high field side pellet launch



type	number of injectors	repetition frequency	size	velocity	pulse length capability
high field side; centrifuge	2 (3)	7 – 50 Hz	3 - 6 mm	< 0.5 km/s	3000 s

inward shift of mass deposition with respect to ablation

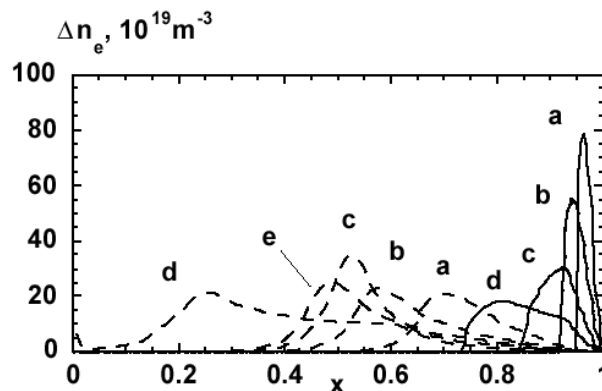
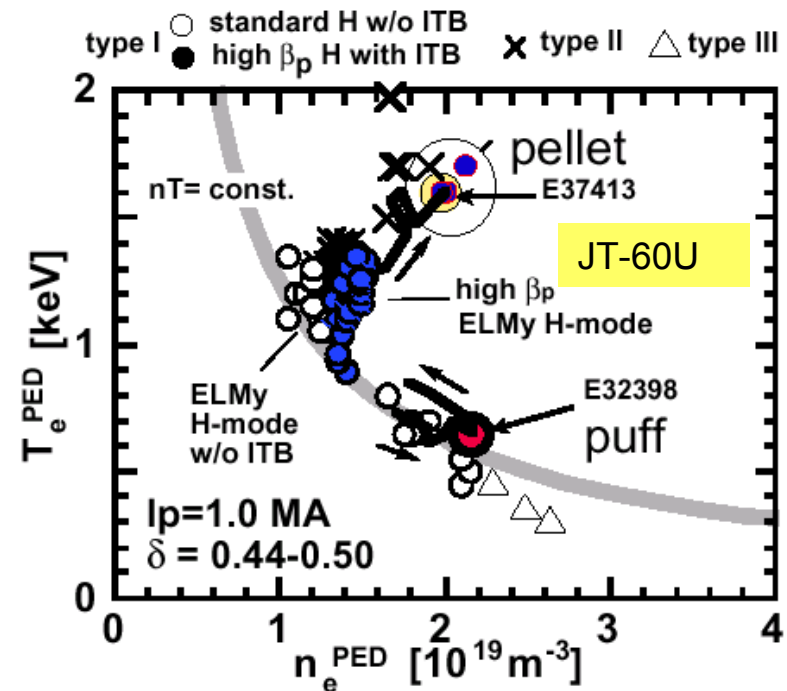


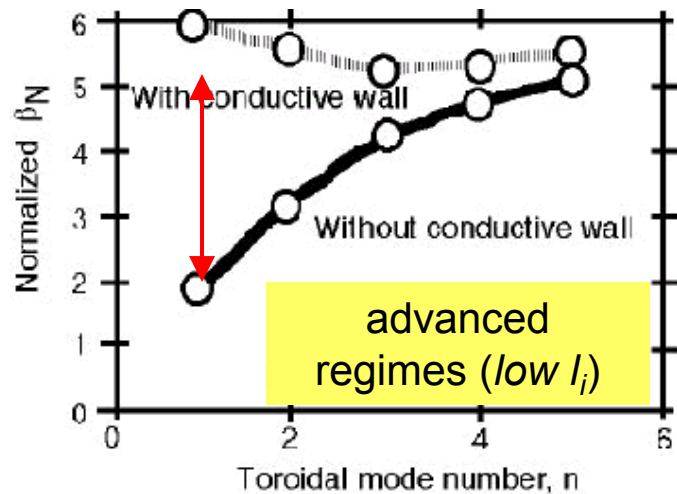
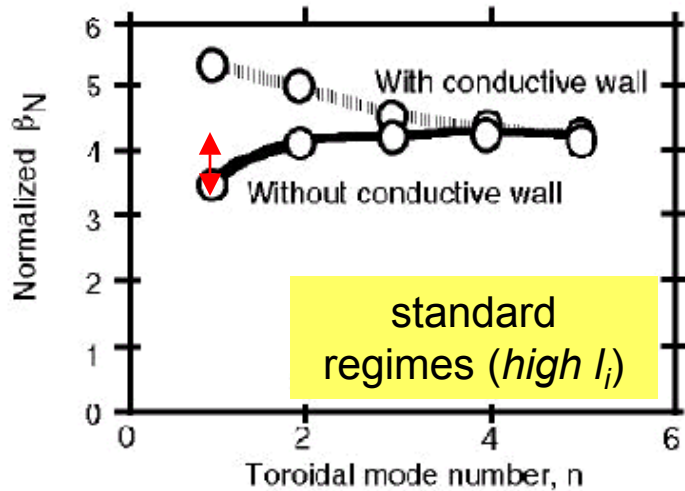
Figure 4.5-2 Model Predictions for the HFS Injection in ITER  
Solid lines correspond to pellet ablation, dashed lines for the ablated mass deposition

benefit for high-β<sub>p</sub> ELMy H-mode

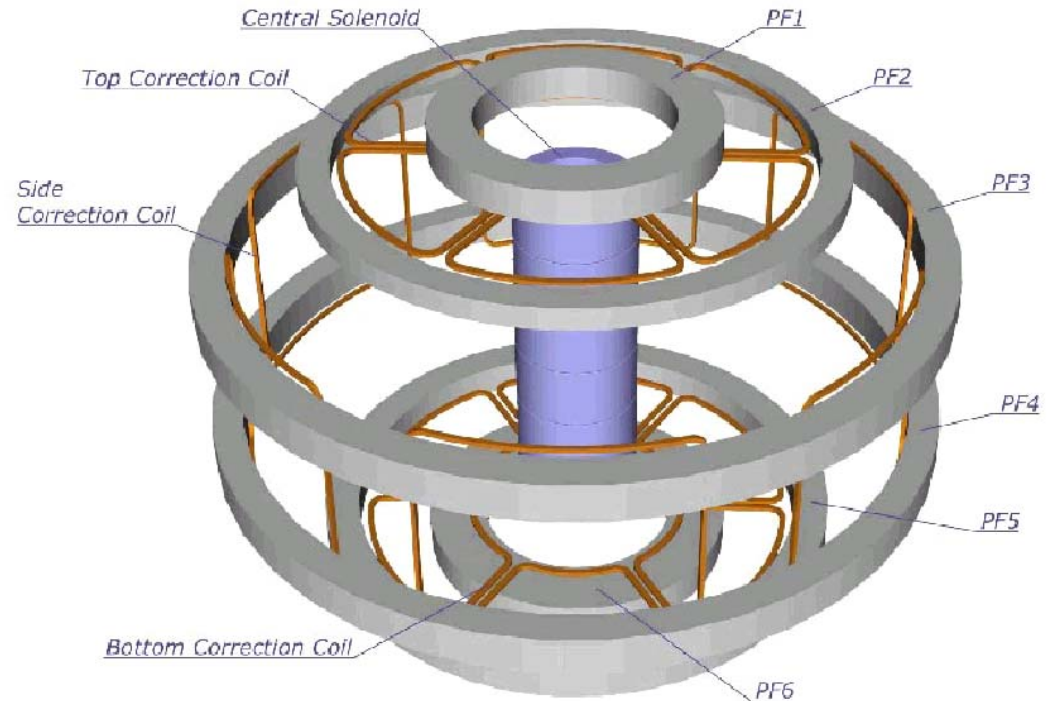


benefit of pellet injection on reverse shear modes: still to be explored

# advanced scenarios at high $\beta_n$ require RW feedback stabilisation



↑↓ potential gain by low- $n$  RWM feedback



ITER error field correction and RWM control coils

relevant & attractive range of plasma shapes covered:

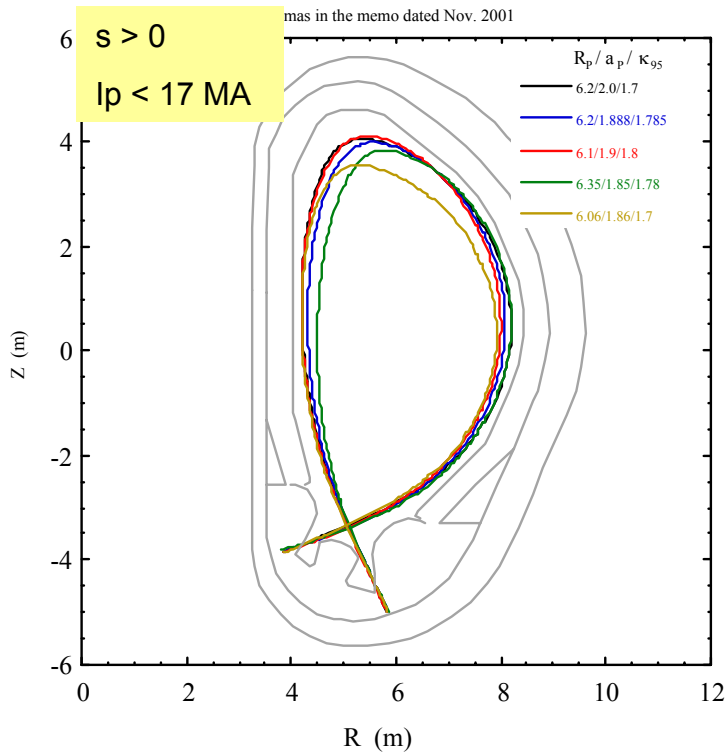
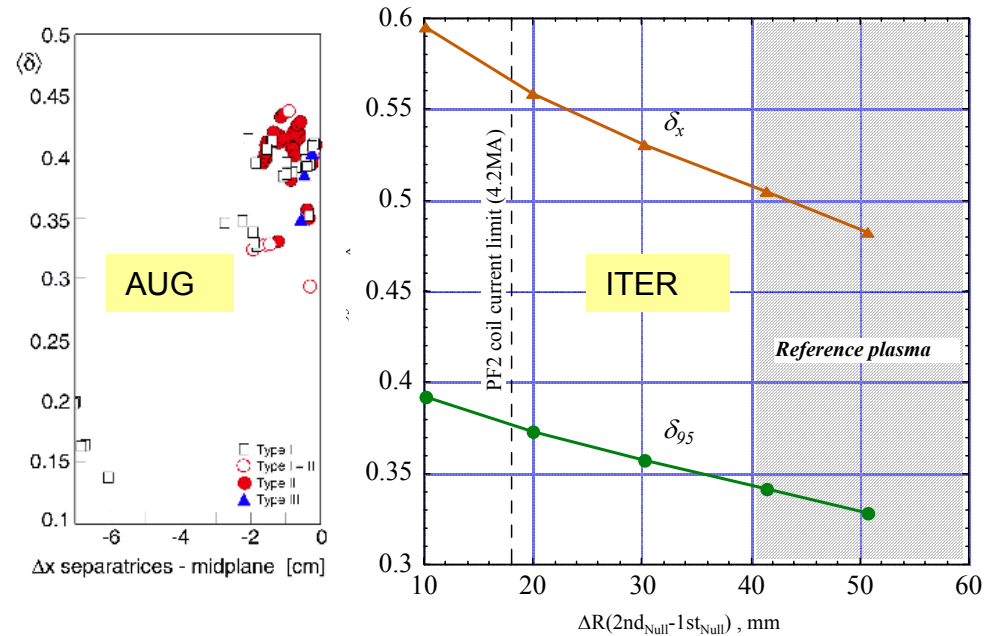


Double-Null proximity (+triangularity) for access to type II ELMs

enhanced shaping viz. ITER-FDR

	FDR	FEAT
$\kappa_{95}/\kappa_x$	1.6 / 1.76	1.7 / 1.86
$\delta_{95}/\delta_x$	0.24 / 0.31	0.35 / 0.5

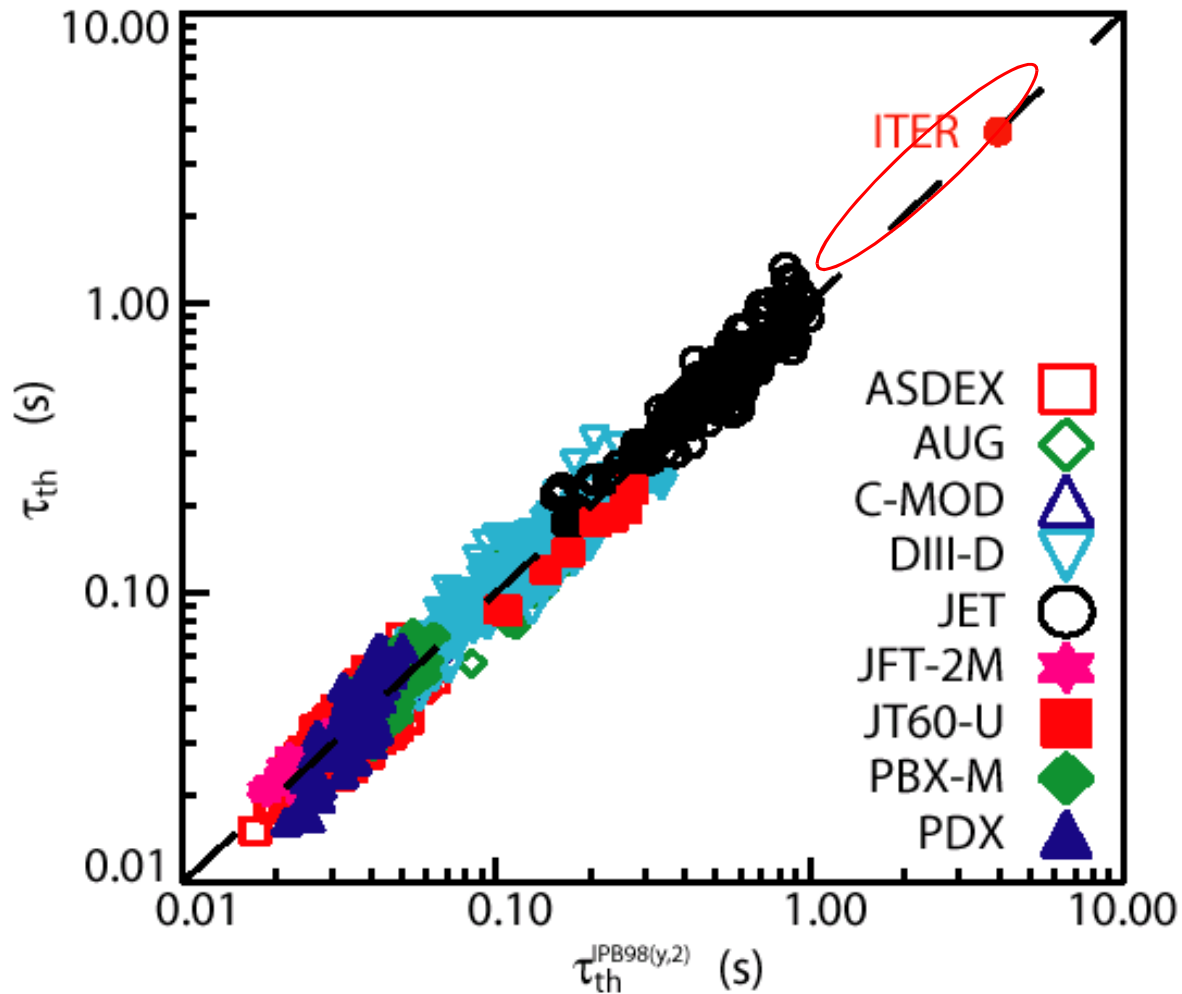
can be further pushed to accommodate important observations



advanced scenarios -> stronger shaping possible ( $I_p = 9 \text{ MA}$ )

$I_i$	0.6	0.4
$k_{95, ma}$	<2	<2.

# ITER's mission: physics of reactor grade (size) plasmas



ITER is **not one** experiment, but a facility on which we will run a broad range of experiments (like on other devices)

on ITER: **no conflict to be expected between**

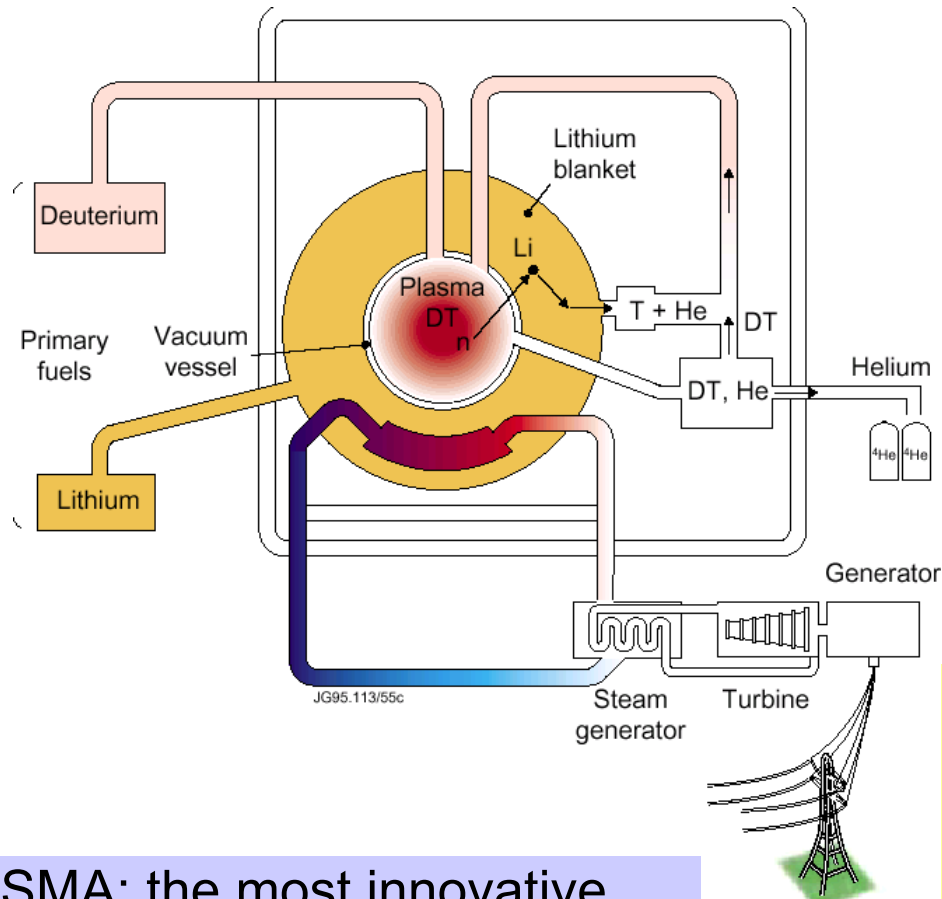
- exciting burning plasma physics
- reactor oriented performance maximization

only high performance plasmas will burn

ITER sufficiently close to reactor that regimes transferrable



Fusion Power Plant: fusion core integrated into a „conventional“ requirement

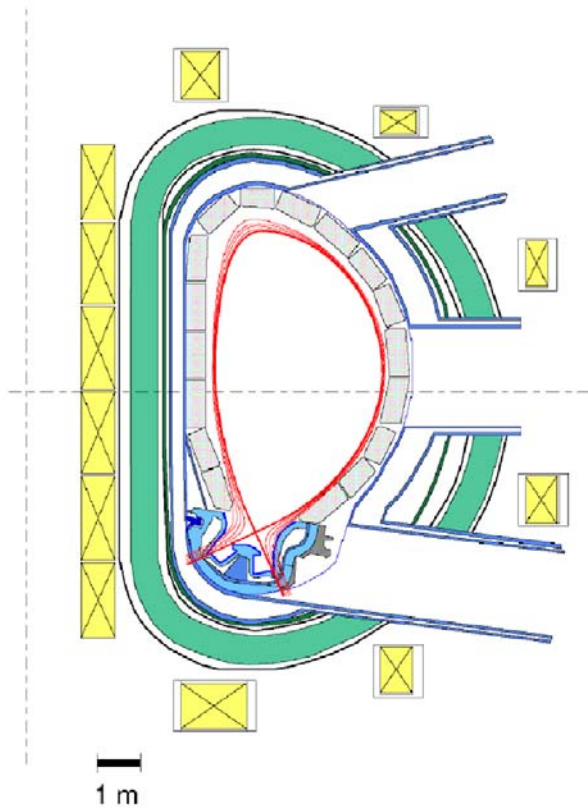


The PLASMA: the most innovative subsystem of a Fusion Power Plant

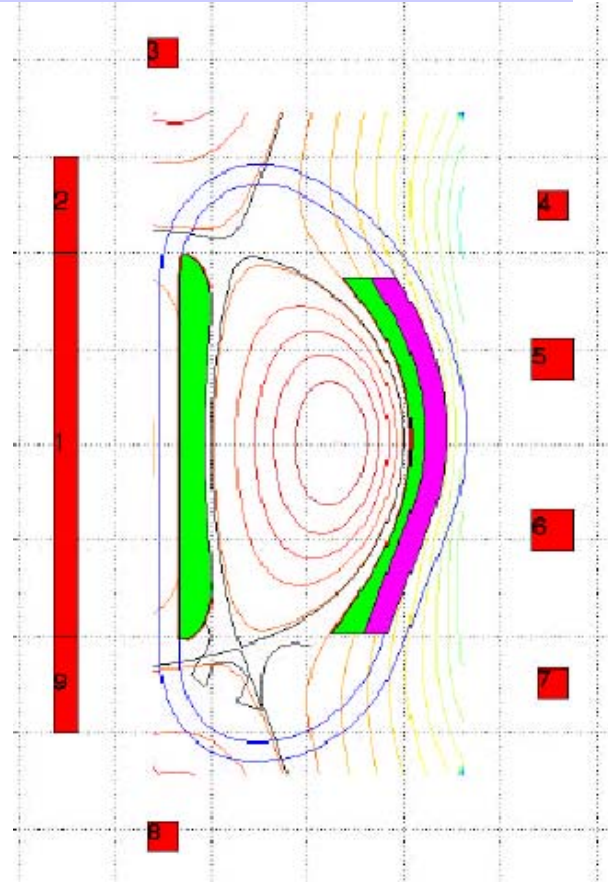
optimization and control of fusion plasmas  
 task of ITER and an accompanying physics program

# Further Steps to a Power Plant:

physics and materials: the key issues for a fusion power plant



**ITER**



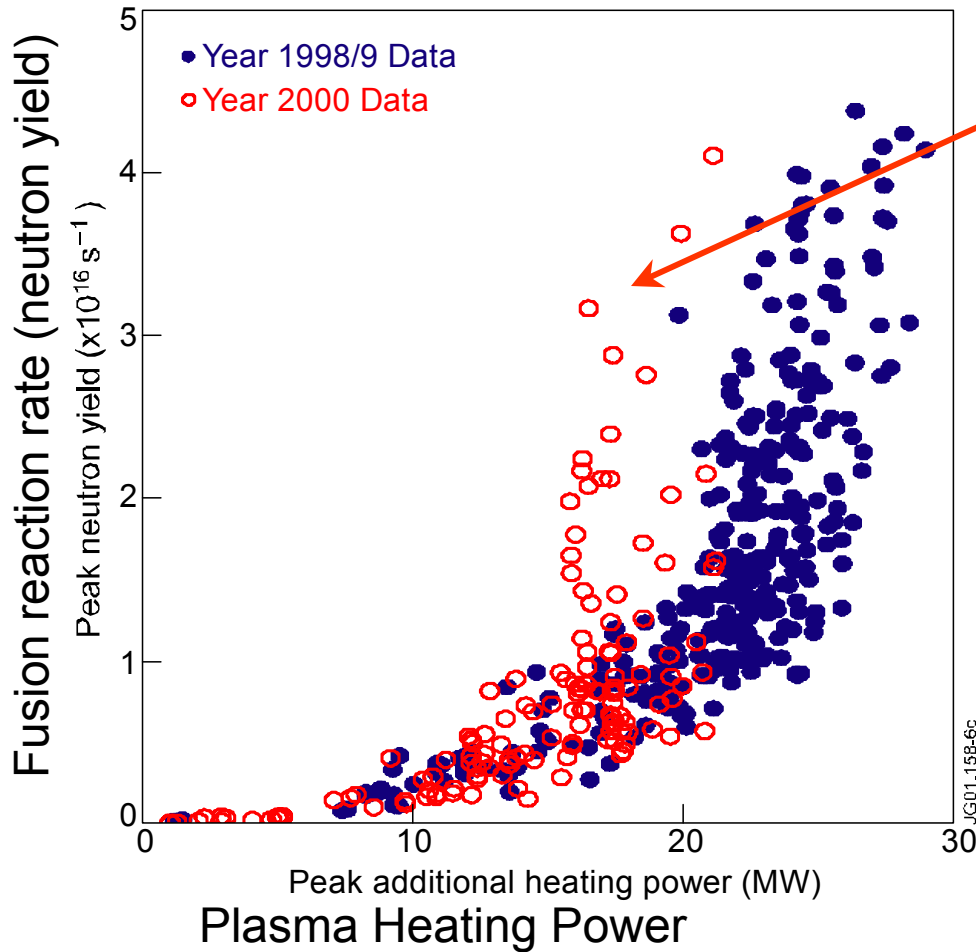
**PPCCS-D**  
(a conceptual power plant)

size and shape of a power plant could be quite close to ITER  
(stellarator - sharing most of the physics and technology with a tokamak - might be advantageous for easier steady-state operation)

Further Steps to a Power Plant:  
***Power Plant Conceptual Design Studies:***  
 reactor requirements beyond basic ITER

	ITER	ITER-RS	PPCD - C	PPCD - D
Ro [m]	6,20	6,20	7,5	6,1
Ip[MA]	15,00	9,00	20,1	14,1
fBS	0,15	0,46	0,69	0,76
$\beta$ N	1,80	2,90	4,0	4,5
H98y	1,00	1,60	1,3	1,2
Pfus [GW]	0,40	0,34	3,4	2,5
Q	10,00	5,70	30	35
Pel, net[GW]	n.a.	n.a.	1,5	1,5
structural materials	SS	SS	Eurofer+SiCSiC inserts;Eurofer ODS for first wall	SiC/SiC
blanket coolant	H <sub>2</sub> O	H <sub>2</sub> O	He+PbLi	PbLi
breeding blanket design	n.a.	n.a.	PbLi	PbLi
divertor load [MW/m <sup>2</sup> ]	10	10	10	5
thermal power cycle efficiency	n.a.	n.a.	~43%	~59%
<neutron wall load> [MW/m <sup>2</sup> ]	0,5	0,4	2,2	2,4

# Further Steps to a Power Plant: plasma performance beyond ITER nominal requirements



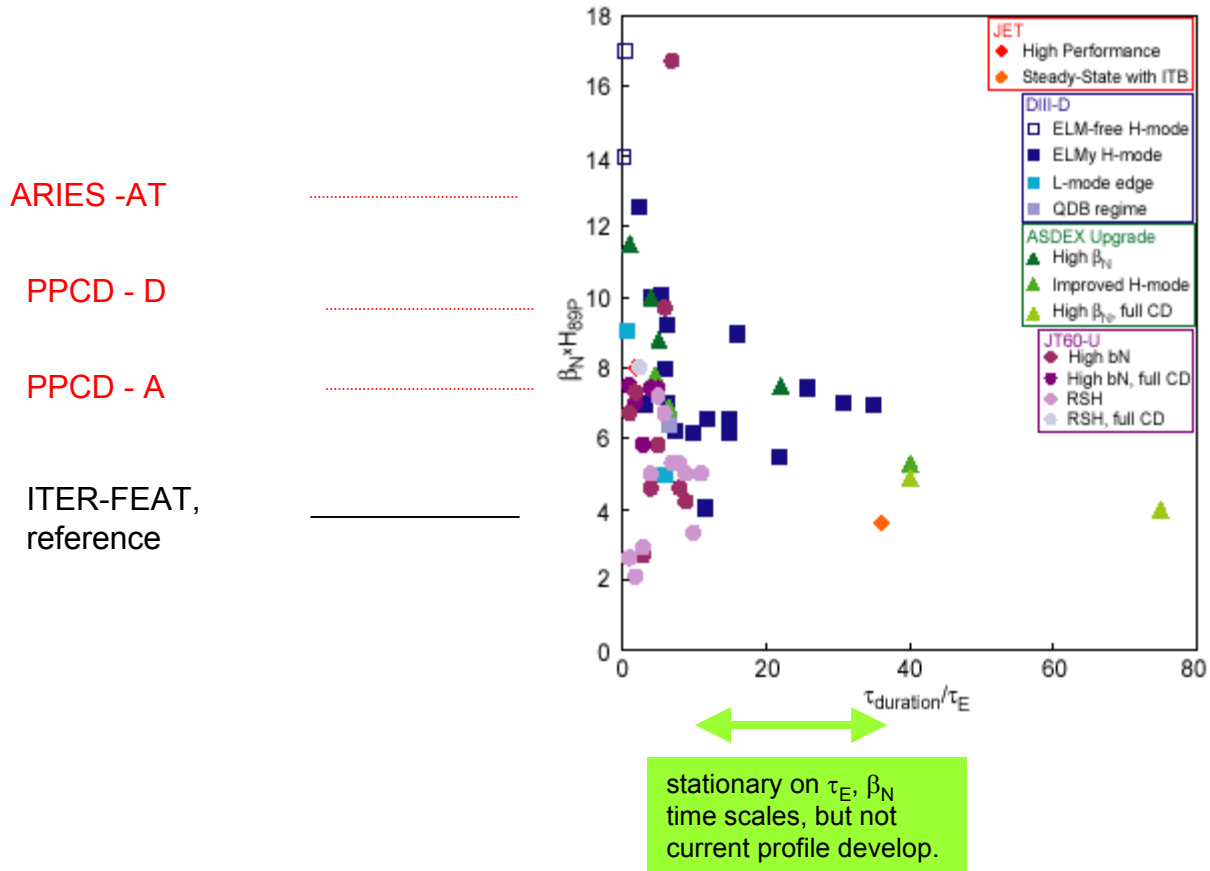
improved  
efficiency modes

fusion performance  
(neutrons in DD-  
operation) improves with

- heating power
- advanced mode operation

# Further Steps to a Power Plant: plasma performance: steady state at high $\beta_N$

## long-pulse control of advanced (high $\beta_N$ , $H$ ) regimes



attractive reactor regimes so far only attained transiently (in contrast to ITER Q = 10 regime)

stationary profile control strongly dependent on heating characteristics  
 ⇒ experiments on ITER critical

## Alternatives to tokamak: stellarator ..&..?

up to early 80ies stellarator had no consistent theoretical foundation:

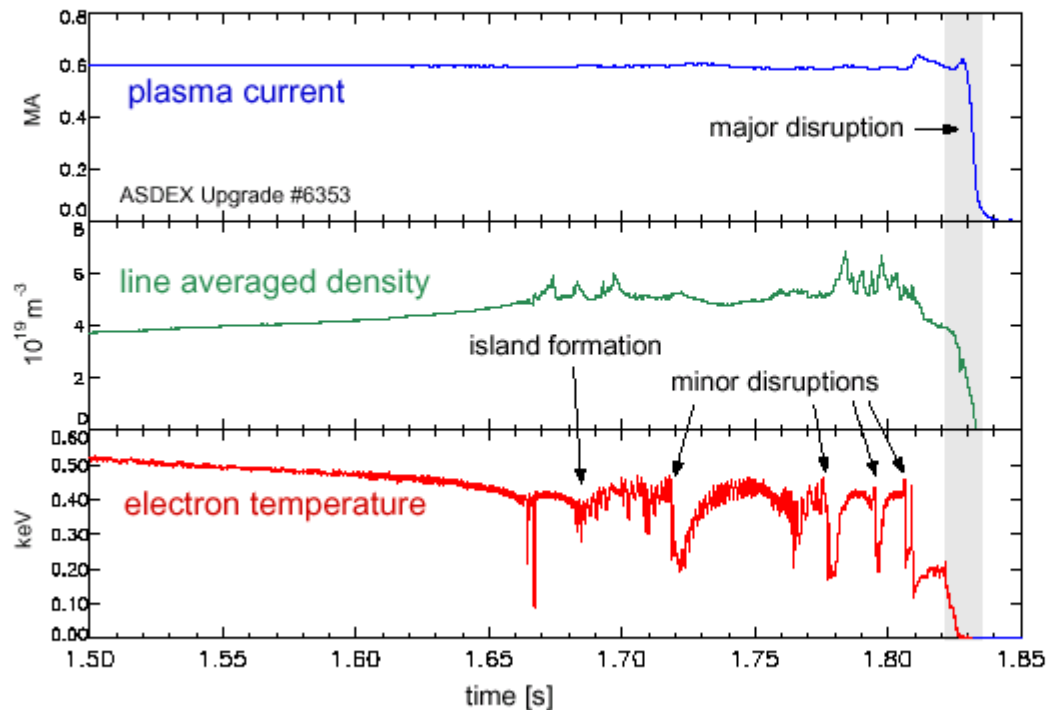
**tokamak:** axisymmetry ensures a constant of motion -> confined orbits; small neoclassical losses

**stellarator:** discovery of quasisymmetry (Boozer&Nührenberg) configurations exist with constants of motion *in drift approximation*

# Alternatives to tokamak: why?

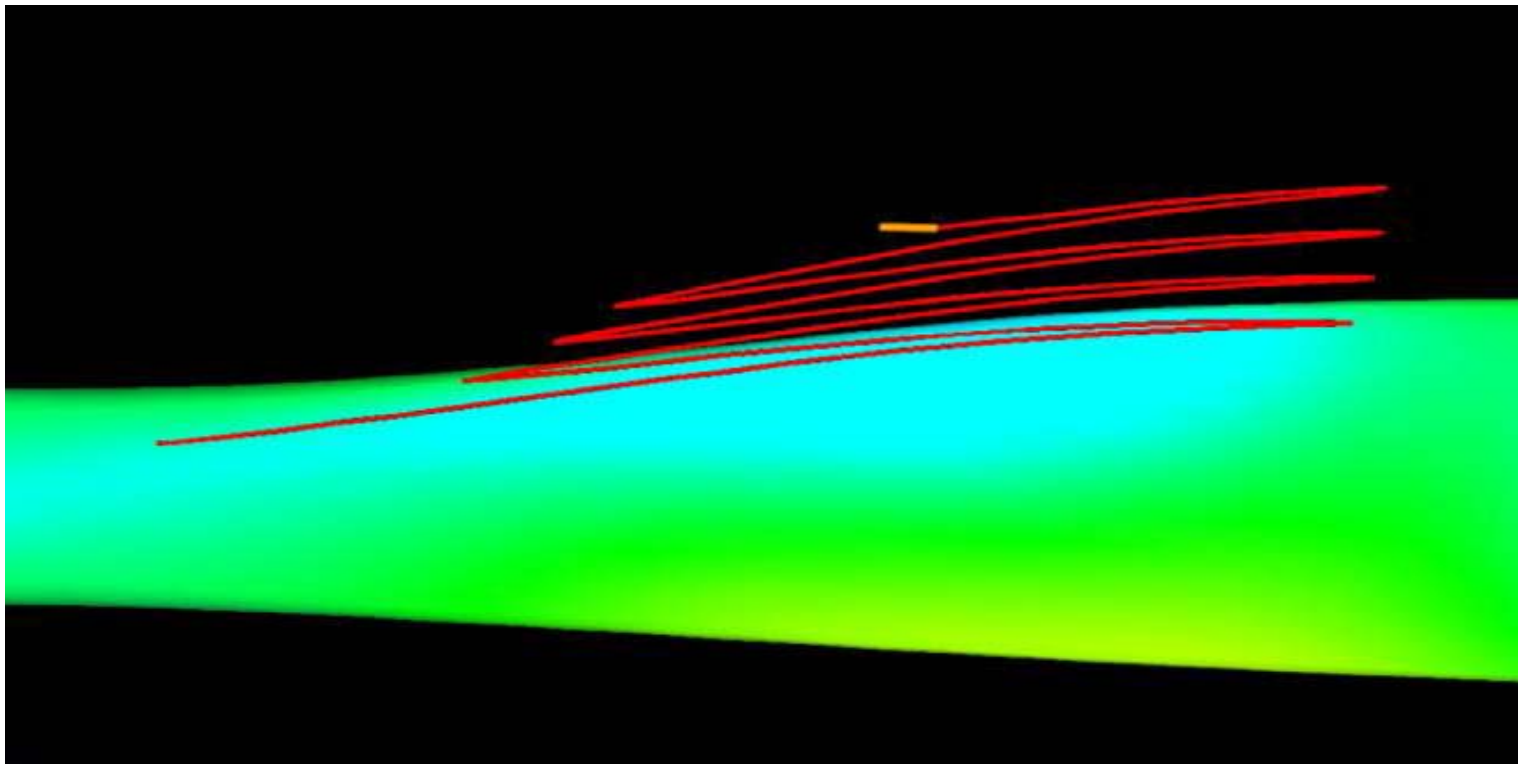
- (1) intrinsic steady state capability
- (2) possibility of current disruptions

Time history of a (provoked) density limit disruption:

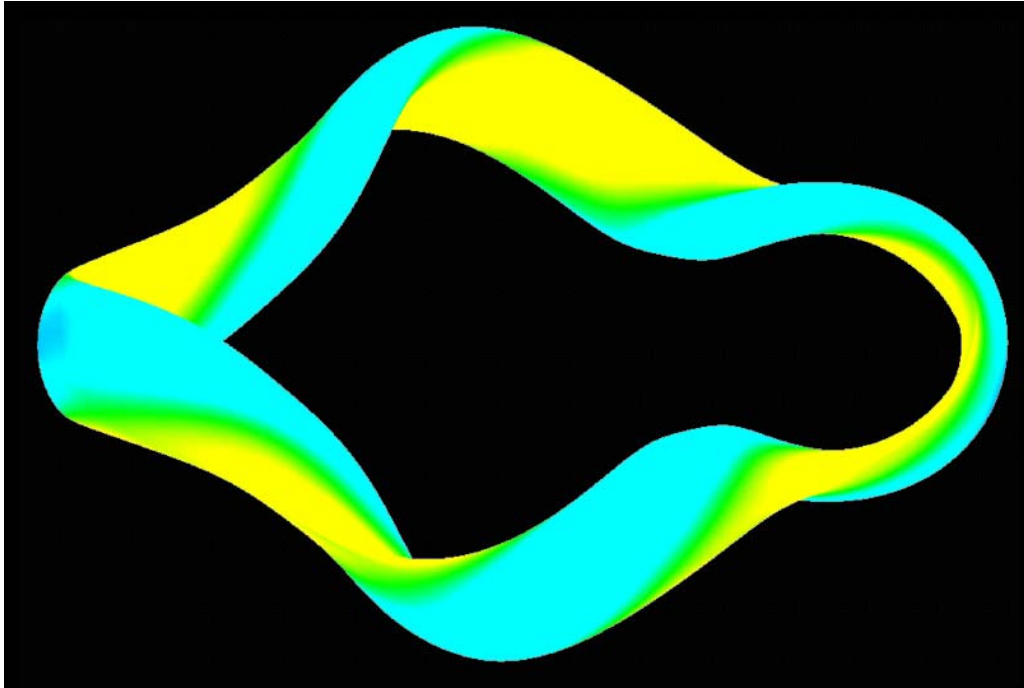


1. Radiation instability  
plasma edge cooled
2. Resistive MHD:  
tearing modes  
magnetic islands
3. "Minor" disruptions  
loss of confinement
4. "Major" disruption:  
plasma current quench

problem of classical stellarator  
confinement of fast particles



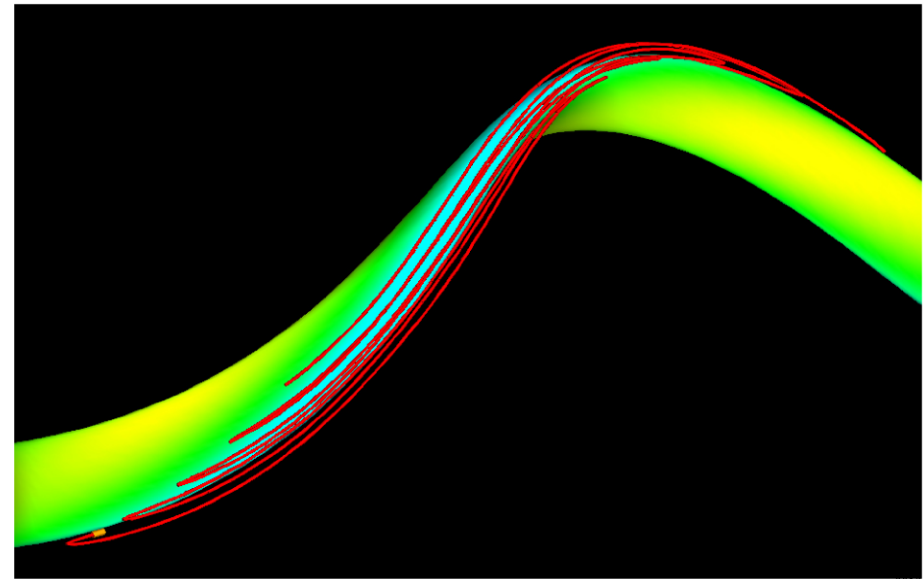




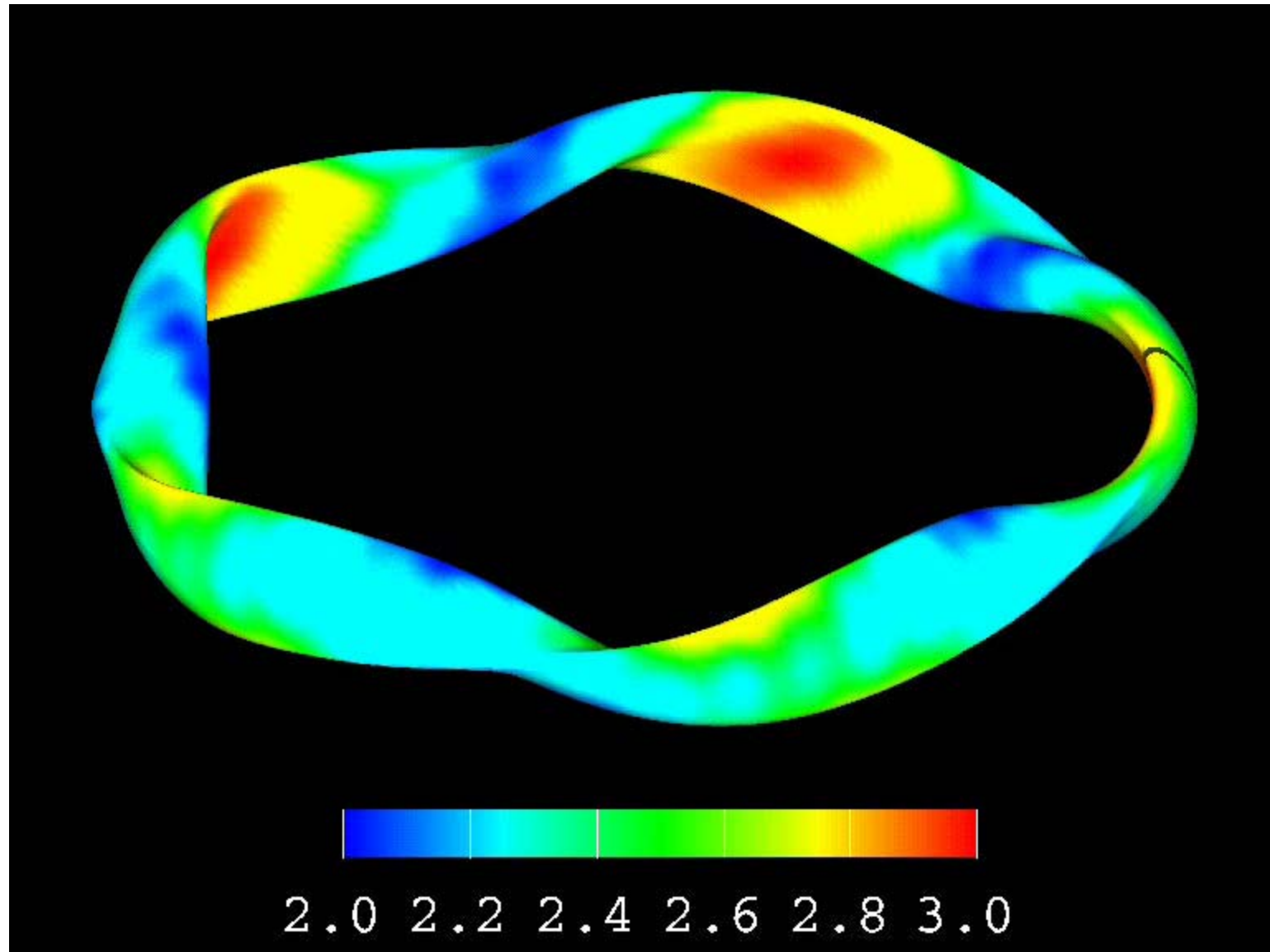
## Quasihelikale Symmetrie

$$B = B(s, \theta - \varphi)$$

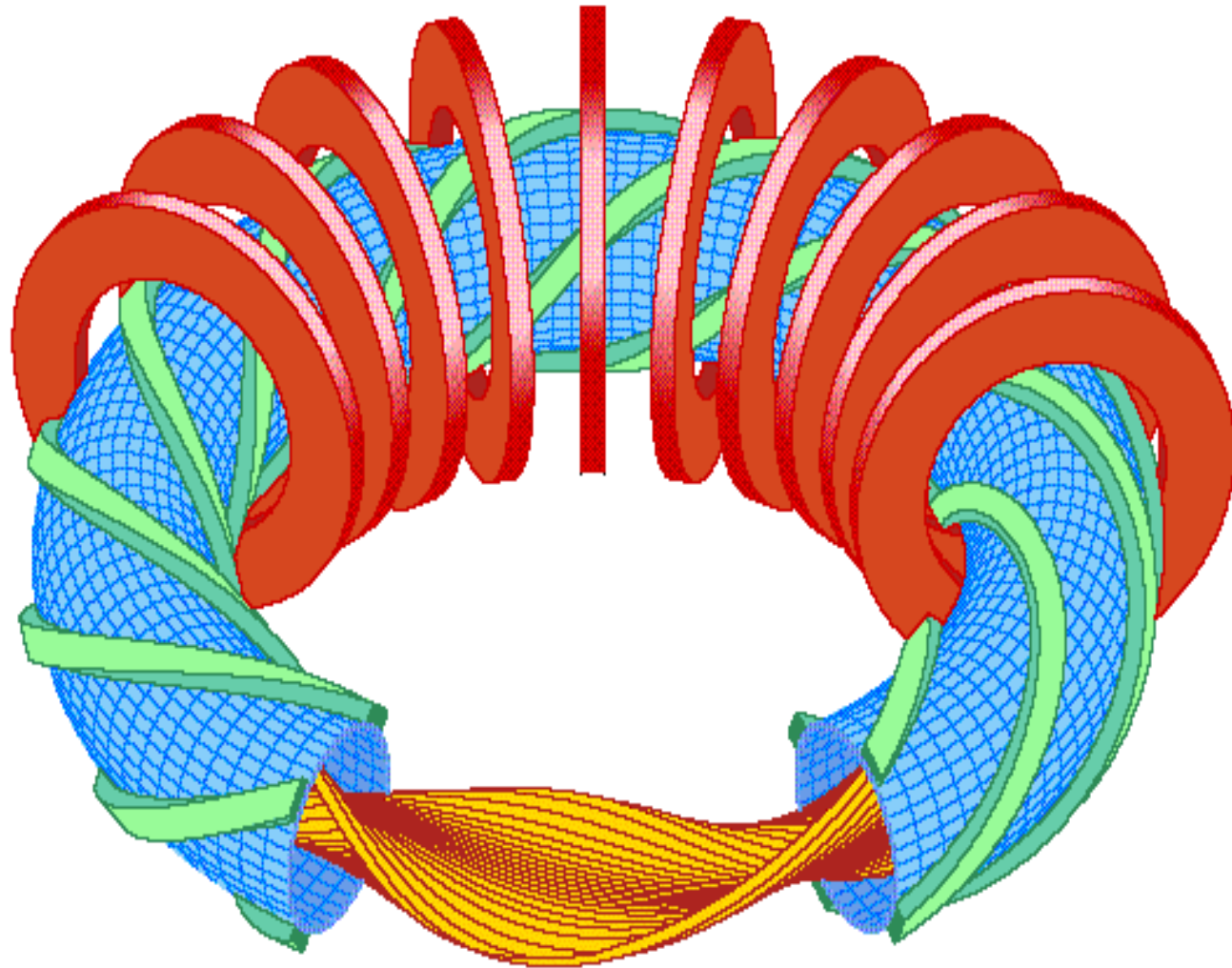
gyrocenters rest on  
closed surfaces



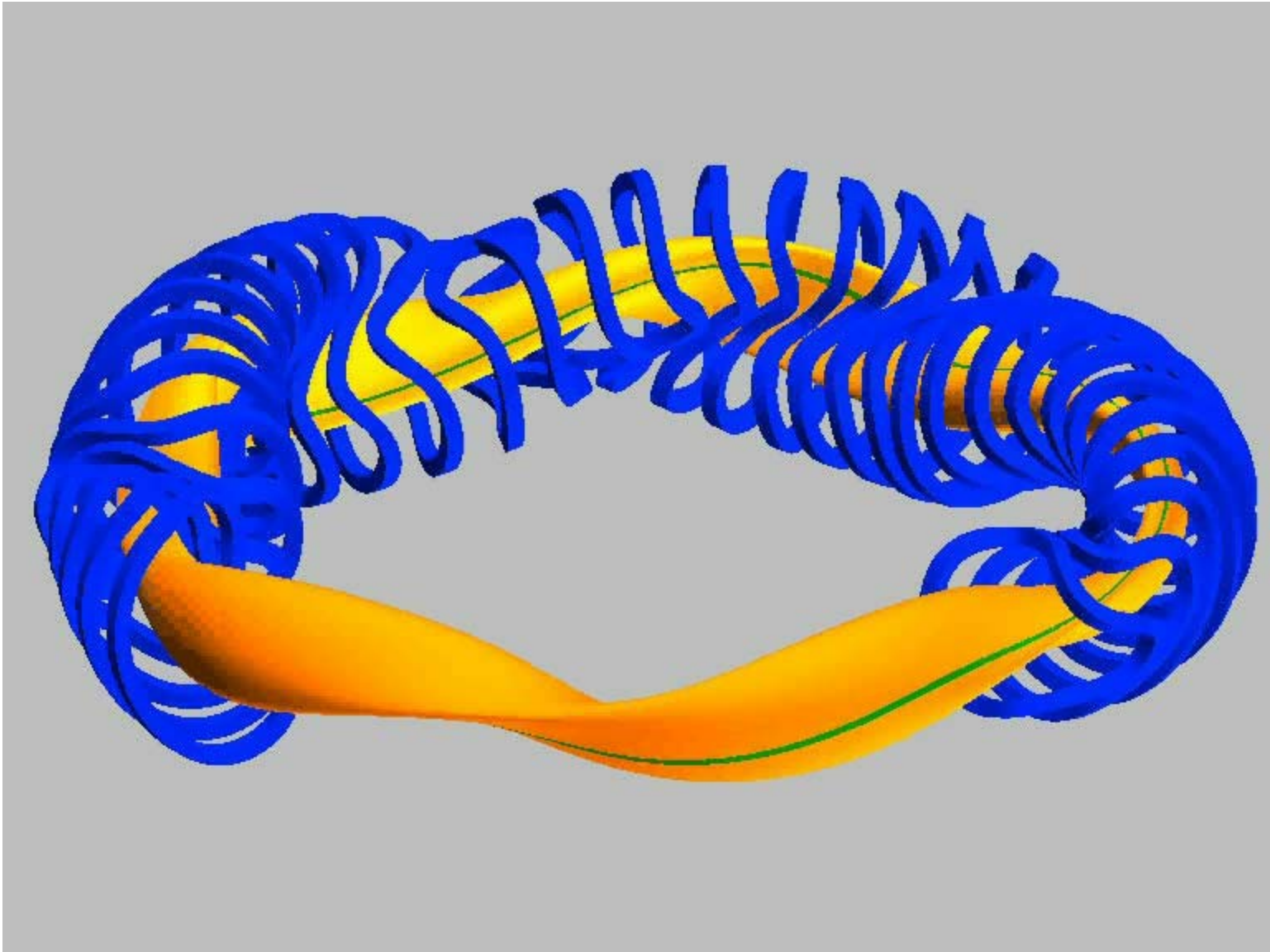
# W7-X: confinement of fast particles



## W7-X: modular coils



## W7-X: modular coils



# W7-X aim: close performance gap to tokamaks

