School on Synchrotron Radiation

UHV - Technology

Oswald Gröbner

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- 1) Introduction and some basics
- 2) Building blocks of a vacuum system
- 3) How to get clean ultra high vacuum
- 4) Desorption phenomena
- 5) Practical examples

Oswald Gröbner, Retired from CERN Vacuum Group. Present Address: Schmiedgasse 5, Innsbruck, AT-6020, Austria e-mail: Oswald.Grobner@cern.ch, Oswald.Groebner@CHELLO.at

Literature

Books

The Physical Basis of Ultrahigh Vacuum, P.A. Redhead, J.P. Hobson, E.V. Kornelsen, American Vacuum Society Classics, American Institute of Physics, 1993 Foundations of Vacuum Science and Technology, Ed. J.M. Lafferty, John Wiley & Sons, 1998

Handbook of Accelerator Physics and Engineering, A. W. Chao, M. Tigner, World Scientific, 1998

CAS CERN Accelerator School : Vacuum Technology, Ed. : S. Turner. CERN 99-05, 19 August 1999

Handbuch Vakuumtechnik, M. Wutz et. al, Vieweg, Braunschweig/Wiesbaden, 2000

Journals:

VACUUM

Journal of Vacuum Science and Technology (A) Nuclear Instruments and Methods (Section A)

Accelerators at CERN

Historical map from 1996

Nearly all CERN accelerators require ultrahigh vacuum

Total length of vacuum systems over 60 km

LEP to be replaced by LHC (cryogenic vacuum system)

SPS: Super Proton Synchrotron **EPA: Electron Position Accurativity** AAC: Anipoton Accountace Complex LLL: Lap Injector Linux 150LDE: Incope Separator OrLine DEvice LINAC: LiBbar A Costantor PSE: Proton Synchrotron Eloop Inc. LEAR: Low Energy Antipoten Ring

Paduli Litri, Ki Liviaira, Citral, Subano

P2: Proton Synchrotron

Pressure and Molecular Density

Ideal gas law:
$$
P V = \frac{N}{No} R T
$$

\n P pressure, V volume, T temperature
\n N number of molecules
\n R gas constant = 8.31 kJ kmol⁻¹ K⁻¹,
\n $No = 6.02 10^{26}$ molecules kmol⁻¹
\n**Molecular density** $n = \frac{N}{V}$

Pressure :

 $P = n \; k \; T$ Boltzmann constant $k = 1.38 \; 10^{-25} \; J/K$

Note : $R = No \; k$

Note: In nearly all cases, it is the gas density rather than the pressure which matters.

Units :

Pressure : Pa (N/m^2) , mbar = 100 Pa, Torr = 133 Pa Gas load : Pa $m^3 = 7.5$ Torr l, mbar $l \sim 2.4$ 10¹⁹ molecules at RT Specific outgassing rate : Gas release from the walls Pa m $\mathrm{^{3}/s/m^{2}\,\sim 7.5\,\,10^{4}\,Torr}$ l/s/cm 2 <u>Leak rate</u>: Pa m³/s or W, mbar l/s or Torr l/s

Wall collisions

Frequency of wall collisions

 $v = \frac{1}{4}$ *4* $n \bar{v}$

proportional to the number density n and to the average molecular velocity \bar{v} .

Momentum transfer to the walls is $2m\bar{v}$, hence the pressure is proportional to $m v \bar{v}$

Distribution of Molecular Velocities

Maxwell-Boltzmann distribution of molecular velocities at the temperature T

$$
\frac{1}{N} \frac{dN}{dv} = \frac{4}{\sqrt{\pi}} \left(\frac{m}{2 k T}\right)^{\frac{3}{2}} v^2 e^{-\frac{m v^2}{2 k T}}
$$

The average velocity is given by (m = M m_o): $\overline{v} = \sqrt{\frac{8 k T}{\pi M m_o}}$, numerically ~146 $\sqrt{\frac{T}{M}}$ (m s⁻¹)

Molecular velocities for N_2 at 50, 100, 300 and 500K.

Mean molecular velocities at 20° C (m/s)

Pressure

$$
p = const \, m \, \overline{v} \, v
$$

m mass of a molecule \bar{v} average molecular velocity ν rate of wall collisions

A complete calculation gives *const* = $\frac{\pi}{2}$ Thus one finds

$$
p = \pi / 2 m \sqrt{\frac{8kT}{\pi m}} n \sqrt{\frac{kT}{2\pi m}}
$$

and the final result

Considering a molar quantity, $n =$ *N o Vo*

One finds again the familiar result with the gas constant *R*

$$
p = n kT
$$

$$
pV_O = N_O \ kT = RT
$$

Mean Kinetic Energy

The kinetic energy :
$$
E_{kin} = \frac{1}{2} m \overline{v}^2 = \frac{1}{2} M m_o \left(\frac{8kT}{\pi M m_o} \right) = \frac{4}{\pi} kT
$$

M molecular weight, $m_0 = 1.66 \, 10^{-27} \, \text{kg}$ does not depend on the molecular mass, M, but only on temperature T.

In thermal equilibrium heavy molecules move sufficiently slowly and light molecules move sufficiently fast to carry on average the same kinetic energy.

Total and Partial Pressures

For each gas component n_1 , n_2 , n_3 ,... the contribution to the total pressure : $P_i = n_i kT$ The total pressure is therefore the sum of the partial pressures: $P = \sum_{i} P_{i} = k T \sum_{i} n_{i}$

Mean Free Path

$$
l = \frac{1}{\sqrt{2} \pi D^2 n}
$$

D molecular diameter $({\sim}3 \ 10^{-8} \text{ m})$

Volume traversed by a molecule per second : $\pi D^2 \bar{\nu}$ Molecule collides with all other molecules contained within the cylinder of radius *D*. Number of collisions: $Z \approx \pi D^2 \bar{v} n$. The mean free path $l = \frac{\bar{v}}{Z} = \frac{l}{\sqrt{2} \pi D^2 n}$

It also follows that $n \mid \alpha \geq P \mid \alpha$ *const*.

Note: $\sqrt{2}$ accounts for the fact that molecules in the cylinder are not stationary. For air the product $n l \approx const$ is $\sim 2.5 10^{14}$ m⁻². For N₂ at 20 deg. C and at a pressure of 1 Pa \rightarrow *l* \sim 9 mm

Molecular Flow Conditions

Knudsen relation: gas flow $Q \propto \Delta P$ applies if the mean free path \gg relevant dimensions of system

Molecular flow conductance $c = \frac{4}{3} \frac{\overline{v}}{\int_{0}^{L} \frac{H}{A^2} dl}$ (m³/s)

L length of the element $(L \gg)$ transverse dimensions). H perimeter, A cross section of the element.

The conductance is proportional to the mean molecular velocity, i.e. to $\sqrt{\frac{T}{M}}$.

A cylindrical duct with uniform section and radius!r :

$$
c = \frac{4}{3} \overline{v} \left(\frac{r^3}{L} \right) \sim 306 \cdot \left(\frac{r^3}{L} \right) \sqrt{\frac{T}{M}}.
$$

An orifice (pumping orifice, $L<0$):

$$
c = \frac{1}{4} \overline{v} A \sim 36.5 \cdot A \sqrt{\frac{T}{M}}.
$$

Conductance of elements in series or in parallel add the same as for electric circuits Series : $\frac{1}{c} = \frac{1}{c_1} + \frac{1}{c_2}$ and parallel: $c = c_1 + c_2$

For complicated geometries it is often necessary to use Monte Carlo calculations for the molecular flow.

Molecular conductance of circular tubes

Fig. 2.1. Plots of conductance of cylindrical tubes for air at 20° C calculated according to equation 2.40.

Vacuum characteristics

Summary expressions:

 $n =$ *P* $\frac{1}{kT}$ $kT = 4.04 \; 10^{-21}$ Joule

 $\rho = M m_0 n$ $M m_O = 4.65 10⁻²⁶ kg$ $m_{\text{O}} = 1.66 \, 10^{-27} \, \text{kg}$

$$
v = \frac{1}{4} n \overline{v} \text{ and } \overline{v} = 146 \sqrt{\frac{T}{M}}
$$

$$
l = \frac{1}{\sqrt{2} \pi D^2 n}
$$

D (N₂) = 3.15 10⁻¹⁰ m

gas : Nitrogen, N_2 , 20°C, M = 28

Thermal transpiration

At high pressure, the pressures on both sides are equal.

In molecular flow, the net number of molecules traversing the separating wall must be zero.

$$
v_I = v_2
$$

Since $v = \frac{I}{4}\overline{v}n$ and $\overline{v} = \sqrt{\frac{8kT}{\pi m}}$
 $n_I\sqrt{T_I} = n_2\sqrt{T_2}$ or $\frac{P_I}{\sqrt{T_I}} = \frac{P_2}{\sqrt{T_2}}$

Thermal Conductivity

Thermal conductivity of a gas is independent of the pressure when the pressure is well above the molecular flow regime.

In the transition regime, the heat transfer is proportional to the pressure and to the temperature difference. Principle of pressure measurement with a Pirani gauge.

Basic Vacuum System

V volume (m^3) , F surface (m^2) P pressure (Pa), S pumping speed (m^3/s) q specific outgassing rate (Pa $m^3/s/m^2$)

Stationary conditions (P is independent of volume) $P = \frac{q F}{g}$ *S*

Dynamic pressure

Solution (constant K depends on initial conditions) $P(t) = K e$ $-\frac{S}{V}$ *V* $\frac{d}{dx}$ + $\frac{qF}{g}$ *S*

The time constant of the pump down: *V S*

To obtain a low pressure :

 \sim $\frac{1}{\sqrt{2}}$ Low outgassing rate of the surface, No leaks!!

 $V \frac{\partial P}{\partial P}$

 $\frac{\partial f}{\partial t} = qF - SP$

Large pumping speed

Linear Vacuum System (Accelerators)

Gas flow: Q(x) [Pa m³ s⁻¹], specific outgassing rate: $q(x)$) [Pa m s⁻¹]

Specific surface area per unit length: A[m], molecular conductance per unit length: c $[m^4 s^{-1}]$

$$
\frac{dQ}{dx} = Aq \quad \text{and} \quad Q(x) = -c\frac{dP}{dx}
$$

$$
c\frac{d^2P}{dx^2} = -Aq
$$

Boundary conditions for this configuration:

By symmetry
$$
\begin{bmatrix} dP \\ dx \end{bmatrix}_{x=L} = 0
$$
 and the pressure at $x = 0$

$$
P(x = 0) = \frac{Q(x = 0)}{2S}
$$

$$
Q(0) = 2 A q L
$$

One obtains a parabolic pressure distribution: $P(x) = A q \left(\frac{2Lx - x^2}{2c} + \frac{L}{S} \right)$

The average pressure, relevant for the beam:

$$
P_{av} = \frac{1}{2L} \int_{0}^{2L} P(x) dx = A q \left(\frac{L^2}{3c} + \frac{L}{S} \right)
$$

Note: the pressure is limited by the molecular conductance of the system.

In spite of an increase of the pumping speed S , the average pressure is limited to the value!:

$$
P_{av\min} = \frac{AqL^2}{3c}
$$

Two important requirements :

Large diameter of the vacuum chamber

Close spacing of pumps

Time to form one monolayer

$$
t = \frac{\Theta}{\frac{1}{4}\overline{v} \, s \, n}
$$

Mono layer coverage: Θ (~ 3 10¹⁹ molecules m⁻²) Molecular velocity \overline{V} (m s⁻¹) Gas density n (molecules m^{-3}) Sticking probability s < 1

UHV becomes indispensable for surface analysis and for thin film technology -> Historically the main motivation to develop uhv techniques

Note: Area occupied per molecule *A* ~ *2 3r 2*

Beam Lifetime due to Vacuum

Beam loss by Bremsstrahlung : $-\frac{dE}{dx} = \frac{E}{X_O}$ Lifetime $\frac{1}{\tau} = -\frac{1}{N}$ $\frac{dN}{dt} = \frac{c\rho}{X_o}$ *W*

 X_0 radiation length, c speed of particles and $\rho = \frac{m_0 M}{kT} P$ is the density of the residual gas at the pressure P.

Here
$$
W = \log(E / \Delta E)
$$

Represents the probability per radiation length to emit a photon with an energy larger than the energy acceptance of the machine so that the particle will be lost. $\propto \frac{X_o}{P}$

The lifetime $\tau = \frac{X_o}{c_0 W}$

 $c\rho W$ *P* For nitrogen or CO one finds typically $\tau P = 3.410^{-8}$ (Torr hours)

Consequence : UHV is required for storage rings. Heavy molecules with short radiation length must be avoided.