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"2nd Workshop on Earthquake Engineering for Nuclear Facilities: Uncertainties in Seismic Hazard"

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PSHA studies in Indian NPPs site

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2nd Workshop on Earthquake Engineering for Nuclear Facilities Uncertainties in Seismic Hazard Assessment Trieste - Italy, 14 - 25 February 2005

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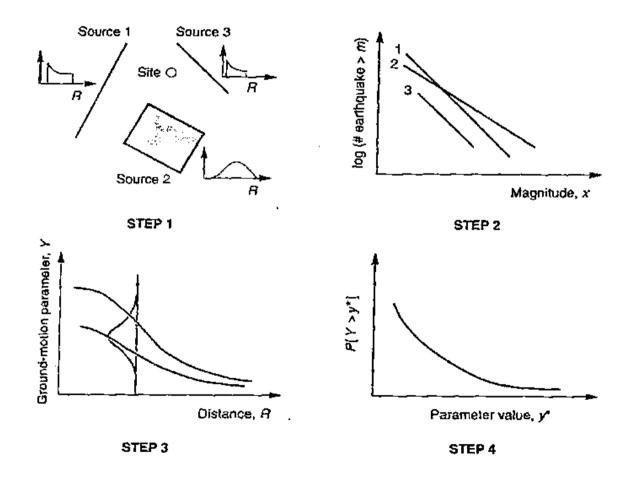
Outline of presentation

- Introduction
- PSHA of Indian NPPs site
- Examination of uncertainties
- Lessons learnt and conclusions
- Summary
- Reference and Glossary

Introduction

• The goal of probabilistic seismic hazard analysis (PSHA) is to calculate the rate (or probability) of exceedence of various groundmotion levels at a site (or a map of sites) given all possible earthquakes scenarios

• In contrast to the typical deterministic analysis, which make use of discrete, single valued events to arrive at the description of seismic hazard, probabilistic analysis allows the use of multi-valued or continuous events and models.



• Though the PSHA approach is more rational than deterministic method to evaluate ground motion parameters, the accuracy of PSHA becomes clouded with uncertainties due to inadequacy of data and lack of information.

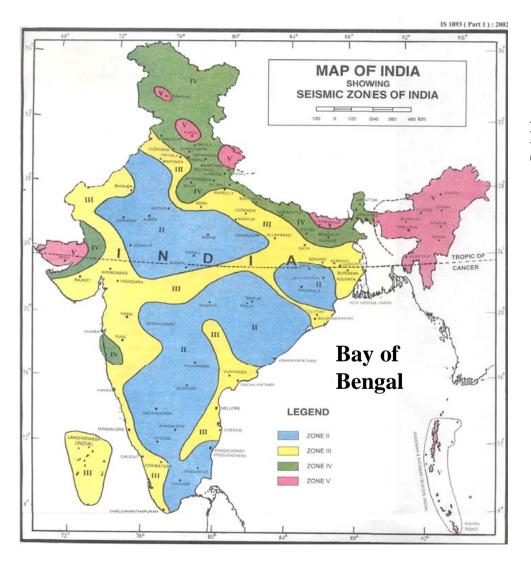
• This is particularly relevant for intra-plate regions like peninsular India.

• The problem of inadequacy of data and lack of knowledge can best be addressed, within the present - state of - knowledge, by examining the effects of uncertainties.

PSHA of Indian NPP site

- Work on PSHA of Indian NPPs site has been started in recent past. The work is in preliminary stage and would need more time for completion.
- Main emphasis is put on at present in the survey of uncertainties
- Work is presently confined to determination of PGA and not UHS
- Some of the results of PSHA (three analyses) carried out for an Indian NPP site is presented along with examination of uncertainties.
 - Analysis I : Approach
 - Analyses II & III : Examination of uncertainities

- Site is located on the coast of peninsular India
- As per Indian standard IS 1893 (2002), site falls in Mesozoic formation.
- Site falls in seismic zone III of IS 1893.



Seismic zone I II III IV V (as per IS1893)

Associated V VI VII VIII IX & above (MMI)

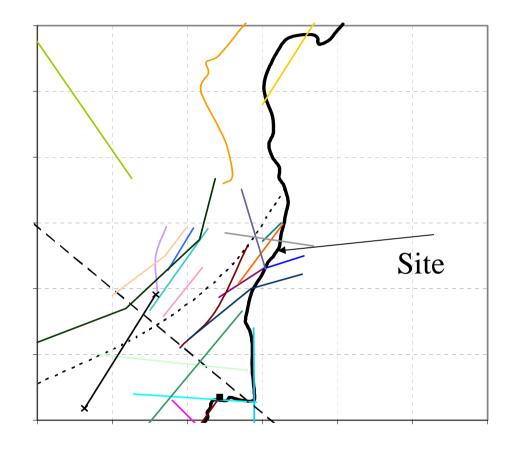
Magnitude 4 5 5-6 6-7 7-8

Seismic zoning map of India (IS 1893-2002).

- The site investigations carried out following AERB Safety Code, AERB/SC/S; and AERB Safety Guide AERB/SG/S-11
- Amongst others, site investigations carried out in particular are:
 - Photo-geological map .
 - Field checks.
 - Collection of seismic reflection survey data.
 - Geotechnical investigations
- Seismotectonic model of the region (having 300km radius) was developed.

- Geological setting
 - The bed rocks comprise of charnokolites and granite ferrous granite gniesses of Archean age intruded by dolerite dykes and covered by coastal sands.
 - The thickness of overburden (sand layer) varies between 6m to 9m, and total depth to top of fresh rock from the existing ground level varies between 10 to 15m.
- The site has been considered as rocky site as the average shear wave velocity $v_s > 1600 \text{m/s}$.

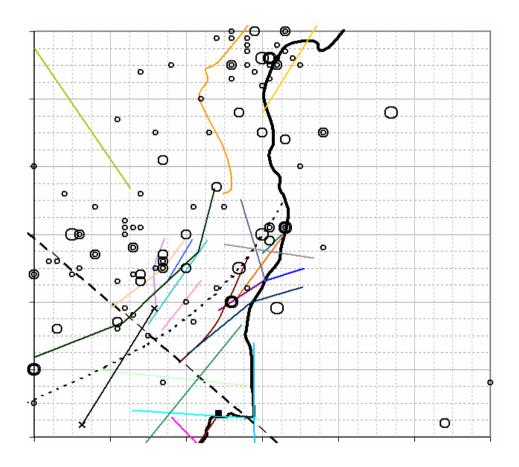
Square area is 6^0 x 6^0 i.e., ~ 660 x 660 km



Faults around the site

• The largest earthquake to have occurred within study area of peninsular India was the Coimbatore earthquake of February 8, 1900, having a magnitude of 6.0.

- Earthquake data for the site is available from 1807 to 2001.
- Approximately 100 records are available (m_o = 3.0)
- For historical data, magnitudes were calculated from observed epicentral intensities.



Earthquakes within 300 km radius of the site

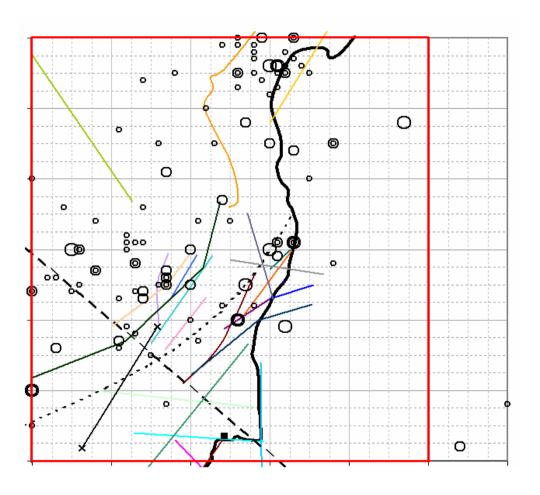
PSHA of Indian NPP Site... Analysis I

Step - 1

1. Definition of earthquake sources

- a) Geometry of the sources
- b) Maximum earthquake potential of the sources
- c) Calculation of the range of earthquake magnitudes and distances to be considered in the analysis

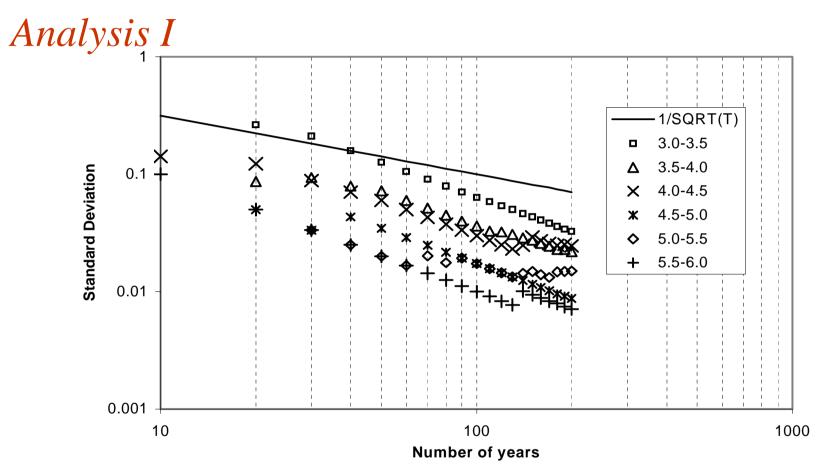
Analysis I



Source model SM₁: site with a single source

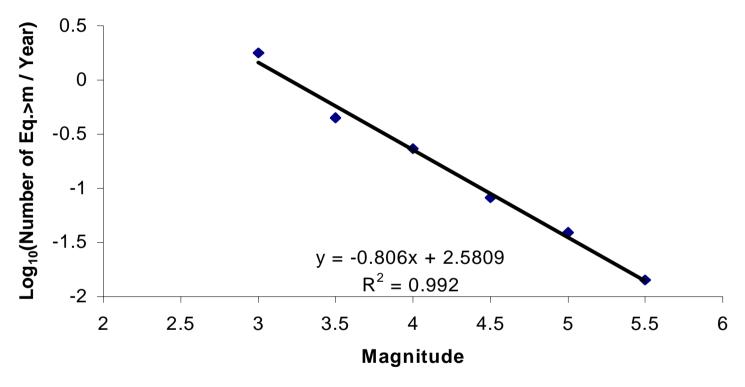
Analysis I Step – 2

- Calculation of recurrence relationships for each source
 - Completeness checking of the earthquake catalogue (by Stepp's method)
 - Derivation of 'a' and 'b' values
 - The exceedance rates corresponding to each magnitude are plotted in semi-log scale and the parameters (a & b) corresponding to best fit straight line is derived.



Checking the completeness of catalogue by Stepp's method ((10 year increment in data bins and 0.5 increase in magnitude bins)

Analysis I

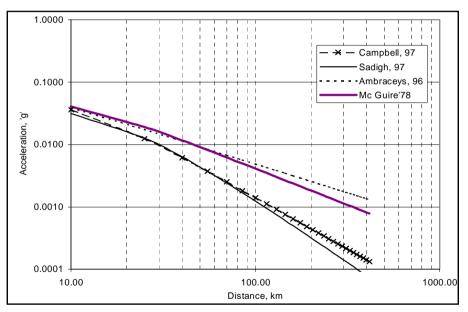


Gutenberg-Richter relationship

(Option-3: 10 year as data bins and 0.5 as magnitude bins used for completeness test)

Step - 3

- •Attenuation model ($\ln y = C1 + C2m + C3 \ln R$) has been used.
- •Particular attenuation relation adopted for the work was Mc Guire'78



Comparison of some attenuation relationships

Analysis I

$$Step - 3$$

• The expected value of the annual probability of exceedence of PGA, 'z'

$$E(z) = \sum_{i=1}^{N} \alpha_{i} \int_{m_{0}}^{m_{u}} \int_{r=0}^{r=\infty} f_{i}(m) f_{i}(r) P(Z > z | m, r) dr dm$$

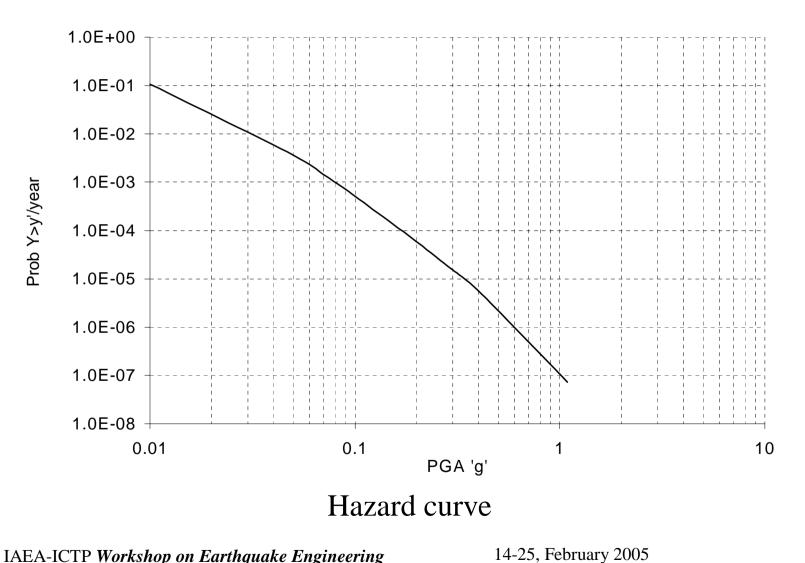


 Software 'EQRISK' was used to estimate E(z)

Analysis I

The following considerations are made in calculating E(z)

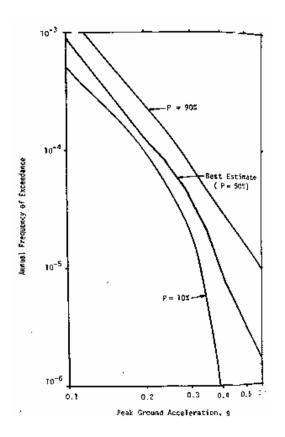
- Minimum magnitude, m_0 was taken as 3.0
- Upper cutoff magnitude (m₁₁) was decided based on the maximum observed magnitude in that source
 - $m_u = m_{observed} + 0.7$ (1 intensity equivalent)
- No de-aggregation of seismic hazard has been performed.



- Randomness in PSHA arises out of the following:
 - Aleatory variability
 - Epistemic uncertainty
- Aleatory variability is due to primary randomness of the physical system, and is taken care in the equation for hazard computation.
- Epistemic uncertainty is of secondary type and is due to data inadequacy, lack of information, deficiency in modeling, etc.

- Major contributors to the epistemic uncertainties are:
 - a) model of seismic sources
 - b) specification of activity of the seismic sources
 - c) estimation of earthquake magnitude from records based on intensity and maximum magnitude m_u
 - d) attenuation relationship
 - e) proportioning of activity into different sources

Two approaches for addressing the epistemic uncertainties



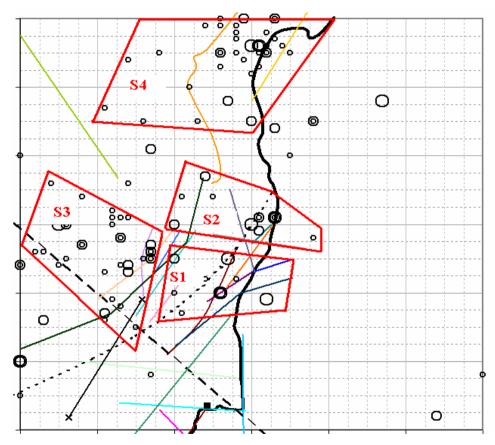
Area Source

Uncertainty bands

Logic trees

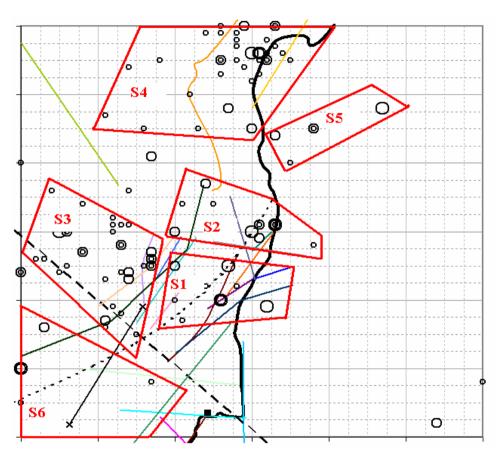
- Analysis II covers the examination of uncertainties conducted for the following
 - modeling of source gometry
 - 'a' & 'b' values, and
 - attenuation relationship

Analysis II



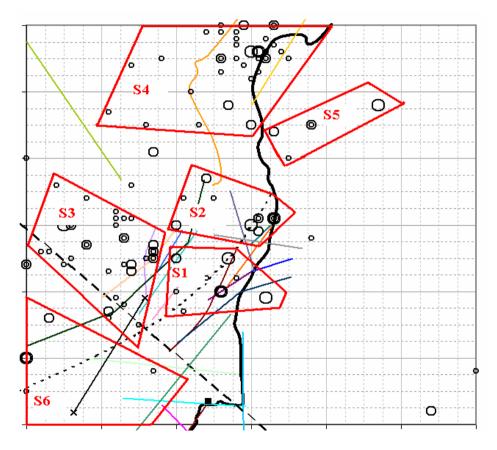
Source geometry model SM₂: site with four sources and remaining seismicity assigned to background activity

Analysis II

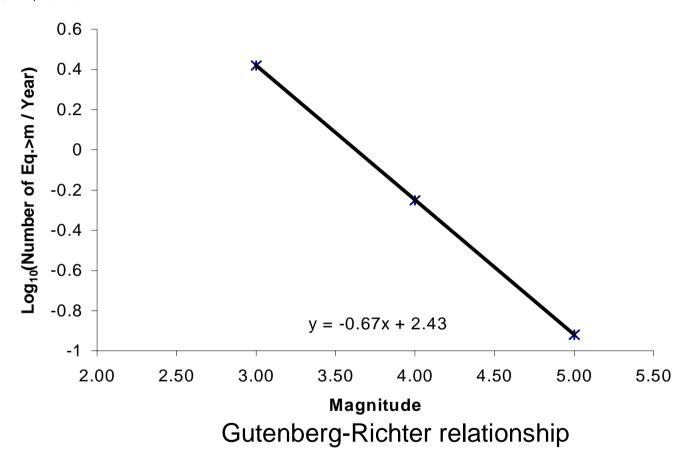


Source geometry model SM₃: site with six sources and remaining seismicity assigned to background activity

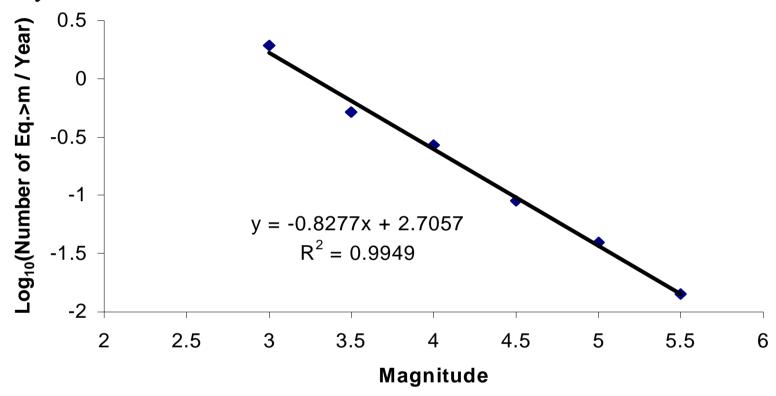
Analysis II



Source geometry model SM₄: site with a six sources (modified S1 and S2) and remaining seismicity assigned to background activity

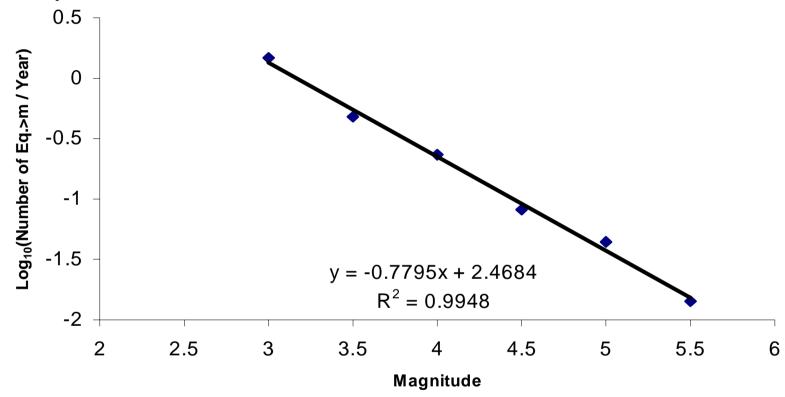


(Option 1: for the full data available for the site, no completeness check)



Gutenberg-Richter relationship

(Option 2: 5 year as data bins and 0.5 as magnitude bins used for completeness test)



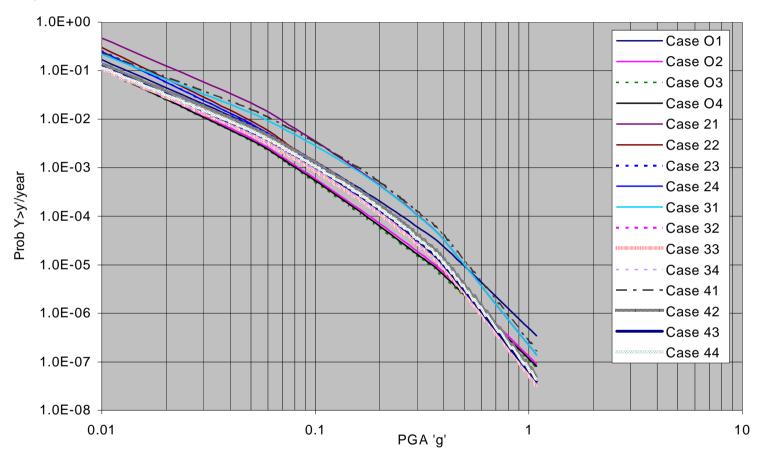
Gutenberg-Richter relationship

(Option 4: 20 year as data bins and 0.5 as magnitude bins used for completeness test)

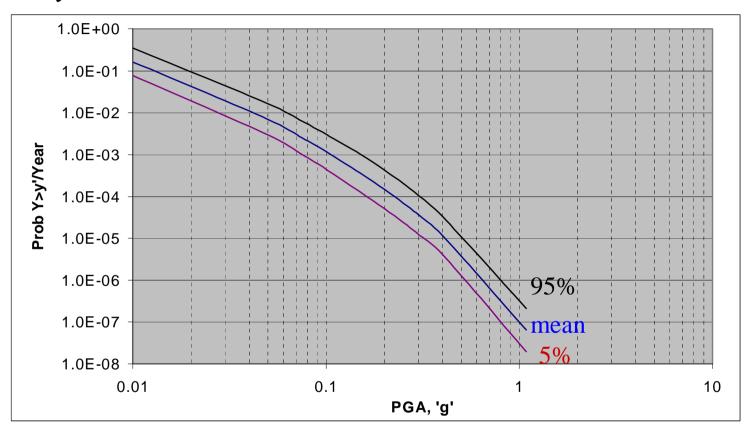
Analysis II

Different Cases

	$a_1 = 2.43,$	$a_2 = 2.71$,	$a_3 = 2.58,$	$a_4 = 2.47$,
Source model	$b_1 = -0.67$	$b_2 = -0.82$	$b_3 = -0.81$	$b_4 = -0.78$
SM ₁ : Single Source	Case 01	Case 02	Case 03	Case 04
SM ₂ : Four Source	Case 21	Case 22	Case 23	Case 24
SM ₃ : Six Source	Case 31	Case 32	Case 33	Case 34
SM ₄ : Six Source (Modified)	Case 41	Case 42	Case 43	Case 44

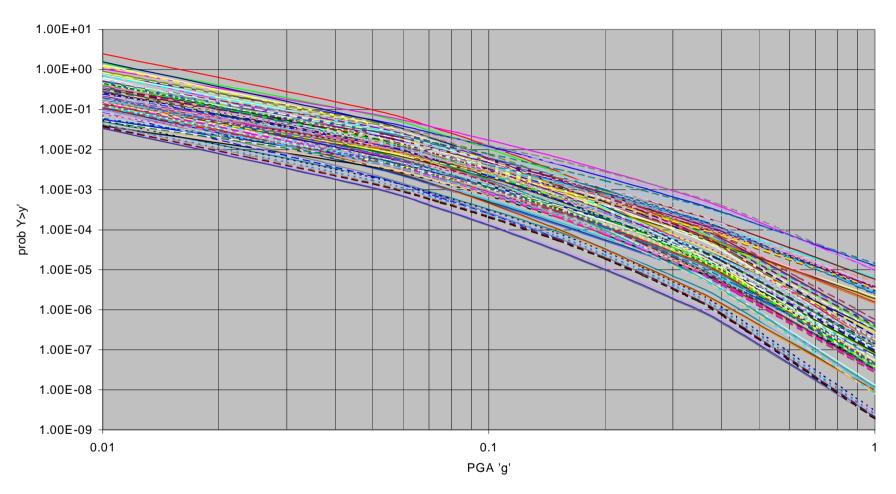


Hazard curves obtained for different combinations of source models and 'a' & 'b' values.



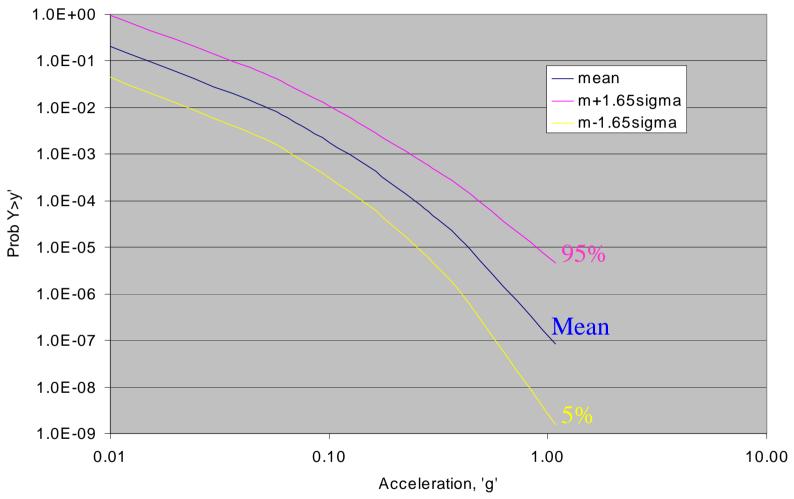
Hazard band - I (4 source geometry models SM1, SM2, SM3 & SM4 and 4 combinations of a & b values, a_1b_1 , a_2b_2 , a_3b_3 , & a_4b_4)

- Analysis III covers the examination of uncertainties on account of attenuation relationship was examined considering the following:
 - Mc Guire '78,
 - Boore'97,
 - Tento '92,
 - Dahle'90,
 - Ambraseys'96,
 - Atkinson '97,
 - Sadigh'97,
 - Campbell'97



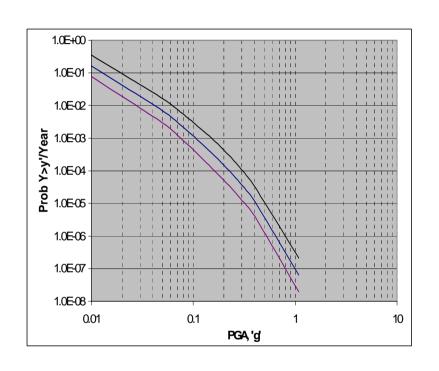
Hazard band (128 combinations 4 source geometry models, 4 combinations of a-b values and 8 attenuation relations)

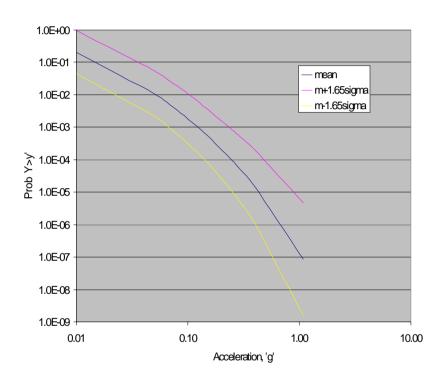
Examination of Uncertainties...Analysis II



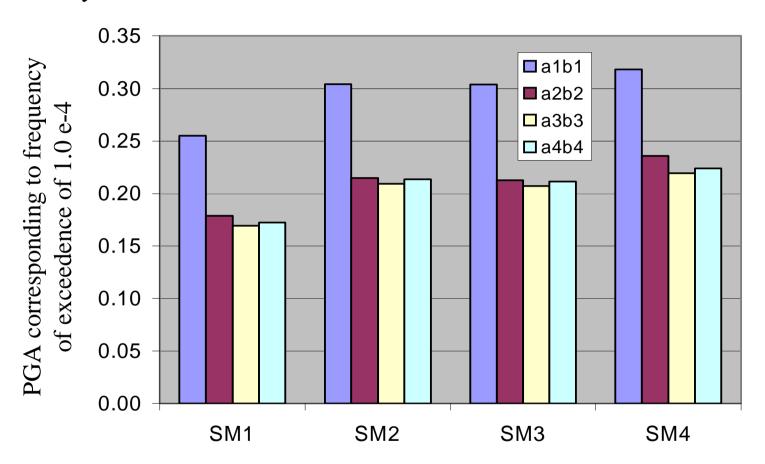
Hazard bands II (4 source geometry models, 4 combinations of a-b values and 8 attenuation relations)

Examination of Uncertainties...Analysis II



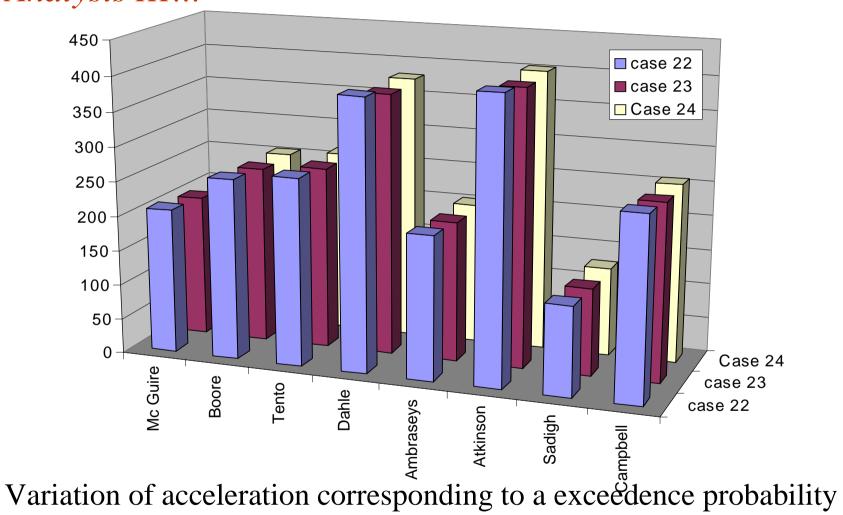


Hazard bands I & II



PGA corresponding to annual frequency of exceedence of 1x10⁻⁴ (4 sources geometry and 4- combinations of a & b values)

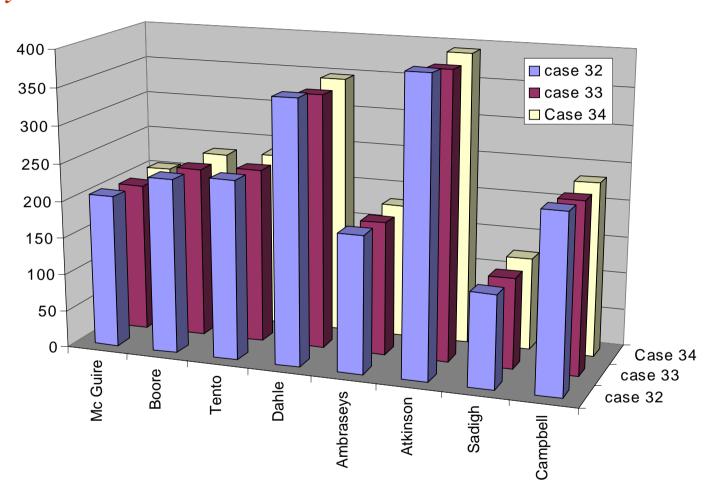
Analysis III...



of 1x10⁻⁴, source type SM2

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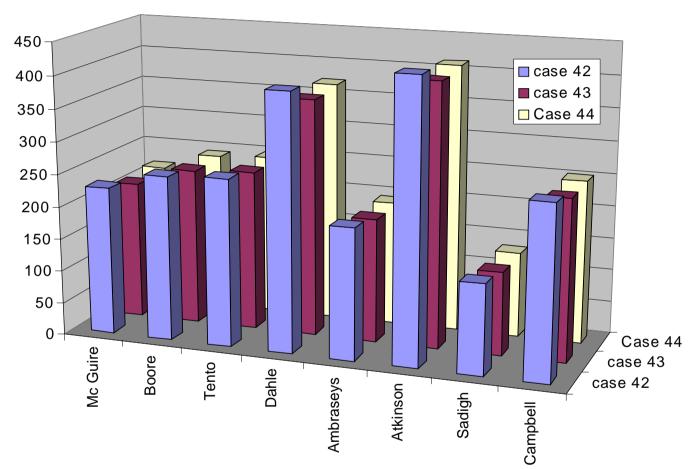
Examination of Uncertainties... Analysis III...



Variation of acceleration corresponding to a exceedence probability

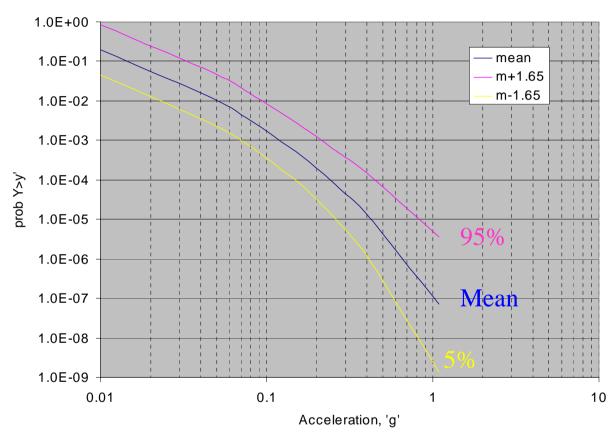
of $1x10^{-4}$, source type SM3 IAEA-ICTP Workshop on Earthquake Engineering 14-25, February 2005

Examination of Uncertainties... *Analysis III*...



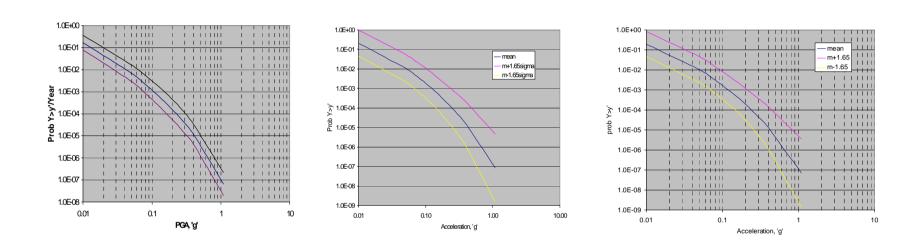
Variation of acceleration corresponding to a exceedence probability of $1x10^{-4}$, source type SM4

Examination of Uncertainties... *Analysis III*...



Hazard band III (3 source geometry models, SM2, SM3 & SM4; 3 combinations of a & b values, a_2b_2 , a_3b_3 , & a_4b_4 ; and 8 attenuation equations)

Examination of Uncertainties...Analysis II



Hazard bands I, II & III

Lessons learnt

- Construction of hazard band is a convenient approach to tackle epistemic uncertainties in PSHA.
- Single source geometry is not suitable
- For stable continental region like peninsular India, m_{min} may be taken as 3.0
- Attenuation relations is a large contributor to uncertainties
- Suitable attenuation relationship for stable continental region?
- Available attenuation relationships do not, in general, handle near field earthquakes

Lessons learnt...

- Appropriate guidelines are required to reduce the subjective ness in
 - Assigning m_u of a source
 - Apportioning activities among different sources, when a common database is used to derive the 'a' & 'b' value.

Summary

- Work on PSHA for Indian NPPs has been started
- Further work will be carried out with
 - Extensive checking of catalogues
 - Refining estimation of 'a' and 'b' values
 - Appropriate attenuation relationships
 - Use of alternative source area models
 - Considering alternative approaches for proportioning of activities

References

- IS 1893 (2002), Criteria for Earthquake Resistant Design of Structures, BIS, New Delhi
- AERB/SC/S, Code of Practice on Safety in Nuclear Power Plant Siting
- AERB/SG/S-11
- IAEA TECDOC 724
- Users manual, EQRISK

- E(z) is the expected number of exceedences of ground motion level z during a specified time period t (usually taken as one year),
- α is the mean rate of occurrence of earthquakes between the lower and upper bound magnitudes (m₀ & m_u) considered for the ith source (=N(m₀))
- $f_1(m)$ is the probability distribution of magnitude (i.e., recurrence relationship) for the i^{th} source,
- f(r) is the probability distribution of the distance to the source for the various locations within the source i, and
- P(Z>z|m,r) is the probability that a given earthquake of magnitude m and epicentral distance r will exceed the ground motion level z.

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