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1) Workshop on Design and Use of Regional Weather
Prediction Models, April 11 - 19

2) Conference on Current Efforts Toward Advancing the Skill of Regional Weather
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The Eta Model Numerical Design. **Vertical coordinate**

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The Eta Model Numerical Design. Vertical coordinate

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Spring Colloquium "Regional Weather Predictability and Modeling" Abdus Salam ICTP, Miramare, Trieste, 11-22 April 2005 Vertical coordinate issues:

The Earth has topography !

Domain and topography used for NCEP Reg. Reanalysis:

Vertical coordinate choices:

z, p: problems with coordinate surfaces intersecting topography; N. Phillips (1957) "sigma":

$$
\sigma = \frac{p}{p_S} \qquad \text{(Or, later,} \qquad \sigma = \frac{p - p_T}{p_S - p_T} \qquad \text{)}
$$

Isentropic:

attractive, but problems with topography not addressed;

Problems with sigma (PGF, and others, later), thus, Mesinger (1984) "eta":

$$
\eta = \frac{p - p_T}{p_S - p_T} \eta_S, \quad \eta_S = \frac{p_{rf}(z_S) - p_T}{p_{rf}(0) - p_T}
$$

Note: can be used as a switch, eta/ sigma

Step-topography discretization (Mesinger 1984):

FIG. 1. Schematic representation of a vertical cross section in the eta coordinate using step-like representation of mountains. Symbols u , T and p_s represent the u component of velocity, temperature and surface pressure, respectively. N is the maximum number of the eta layers. The step-mountains are indicated by shading.

Equations:

Generalization of Simmons, Burridge (1981); just as simple;

Moreover:

- Conservation of angular momentum (PGF), as done in Simmons, Burridge, doable;
- Conservation of energy in transformation between potential and kinetic (" $\omega\alpha\Box\Box$ ") doable as well

(Both, Mesinger 1984 in 2D,

energy: Dushka Zupanski, Appendix of Mesinger et al. 1988, 3D)

The very first result, 1984, using the switch eta/ sigma:

FIG. 6. 300 mb geopotential heights (upper panels) and temperatures (lower panels) obtained in 48 h simulations using the sigma system (left-hand panels) and the eta system (right-hand panels). Contour interval is 80 m for

In NCEP's "Eta Model", eta did extremely well:

tests during the early nineties using the eta/ sigma switch, on cases, and samples of forecasts,

very favorable for the eta, e.g.:

Fig. 3 Equitable precipitation threat scores for two versions of the Eta Model: Eta 80 km/38 lavers ("ETA"), and the same version of the Eta Model but run using sigma coordinate ("ETAY"), and for the NGM (RAFS), and the Avn/MRF ("global") Model; for a sample of 16 forecasts verifying 1200 UTC 21 September through 1200 UTC 29 September 1993. Eight forecasts are each verified once, for 12-36 h, and the remaining eight each twice, for 00-24 and for the 24-48 h accumulated precipitation.

However,

a 10-km Eta in 1998 did a poor job on a case of so-called Wasatch downslope windstorm, while a sigma system MM5 did well;

Eta: bad press ever since:

"ill suited for high resolution prediction models"

Schär et al., *Mon. Wea. Rev.,* 2002; Janjic, *Meteor. Atmos. Phys.,* 2003; Steppeler et al., *Meteor. Atmos. Phys*., 2003; Mass et al., *Bull. Amer. Meteor. Soc*., 2003; Zängl, *Mon. Wea. Rev.,* 2003; more ??

Is sigma a good way to go after all? Let us just look at what the sigma problem is, and at some recent results! PGF/resolution: in hydrostatic systems

$$
\phi = \phi_S - R_d \int_{p_S}^{R} T_v d \ln p \tag{1}
$$

Thus: PGF depends only on variables from the ground up to the considered p=const surface !

- From this point of view, all PGF/ hydrostatic equation sigma system schemes, three groups:
- a. Those with hydrostatic eq. analog that relates geopotentials used for PGF to temperatures both below and above the considered level;
- b. "Level schemes": geopotentials used for PGF obtained by vertical integration of temperatures from the ground only up to the considered coordinate surface (e.g., straightforward isentropic coordinate schemes);
- c. "Layer schemes": using layer temperatures to define geopotential increments through layers (best from the point of view of (1))

Continuous case:PGF should depend on, and only on, variables from the ground up to the p=const surface

The best type of scheme:

*w*ill depend on $\mathcal{T}_{j+1/2,\,k+1}$, which \boldsymbol{it} should not; will *not* depend on *Tj-*1/2*,^k*-1, which *it should*. The problem aggravates with resolution !! Thus, PGF problem of terrain-following coordinates: Not one of "two large terms"

$$
-\nabla_p \phi \to -\nabla_\sigma \phi - RT \nabla \ln p_S
$$

(Easy to make them much smaller, subtract "reference" atmosphere" while having the error the same or about the same)

Not one of the "truncation error";

- The error is likely to **increase** with increased Taylor-series accuracy;
- It is likely to **increase** with increased resolution

Any signs of an impact?

One experiment: Eta (left), 22 km, switched to use sigma (center), 48 h position error of a major low increased from 215 to 315 km

Recent performance results

Three-model precipitation scores, on NMM ConUS domains ("East" ,…, "West"), available since Sep. 2002

• Operational Eta: 12 km, driven by 6 h old GFS forecasts;

• NMM: "Nonhydrostatic Mesoscale Model" nonhydrostatic, 8 km, most other features same or similar to Eta, but switched back to sigma, driven by the Eta;

• GFS (Global Forecasting System) as of the end of Oct. 2002 T254 (55 km) resolution, sigma

6 h old GFS LBCs ?

250 mb wind rms fits to raobs, m/s, Nov 2003-Apr 2004

Back to the three models:

NOAA-wide e-mail of 19 July 2002 announcing the operational implementation of the NMM, referring to the choice of the vertical coordinate:

"This choice will avoid the problems encountered at high resolution (10 km or finer) with the step-mountain coordinate

with strong downslope winds

and will improve

placement of precipitation in mountainous terrain".

Did this indeed happen?

However:

How can we tell how good is "placement of precipitation" ?

Are there any performance measures (precip scores) that tell us how good was specifically the placement of precipitation?

A 2 x 2 problem: forecast: yes, no event occurred: yes, no

Two kinds of correct forecasts: yes, yes, and no, no First papers: 1884! (Murphy, MWR 1996)

A very large number of performance measures !

However: are any of them "equitable", in the sense of Gandin and Murphy (MWR 1992)? (No reward for over- or underforecasting the event !)

Equitable threat score:

equitable with respect to random forecasting;

not in the sense of Gandin and Murphy :-(

Marzban (WF 1998):

looked at 14 measures and found none equitable !

Baldwin and Kain (WF 2005, in preparation): looked at 6 performance measures Of these, two: Odds ratio skill score; Heidke skill score; [1926; originally proposed by Doolittle (1988)] !

symmetric with respect to two types of correct forecast;

Equitable threat score, and Threat score emphasize correct forecasts of rain (yes, yes) more than correct forecasts of no rain (no, no)

But neither of them is equitable $-$

J12.617th Prob. Stat. Atmos. Sci.; 20th WAF/16th NWP

BIAS NORMALIZED PRECIPITATION SCORES

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Motivation

- **Equitable threat scores: commonly used to assess the** performance of model precipitation forecasts. Purpose (hoped for): access placement of precipitation
- However: sensitive to bias
- E.g.: Common wisdom has it that bias somewhat greater than 1 tends to benefit equitable threat score.
	- Thus: can we "normalize" the equitable threat score, to remove the impact of bias? (Also, standard threat score. Acknowledgment: Joe Schaefer).

Two Methods of Bias Normalization

- 1. dH/dF method: Assume the incremental change in hits per incremental change in bias is proportional to the "unhit" area, O-H
- 2. Odds Ratio method: Assume that the odds ratio remains unchanged as the hit and forecast areas are changed to satisfy the condition bias = 1

dH/dF Method

Assumption:
$$
\frac{dH}{dF} = a(O - H), \quad a = const.
$$
 (1)

Solve (1) to get
$$
H(F) = be^{-aF} + O, \quad b = const.
$$
 (2)

Since
$$
H=0
$$
 for $F=0$: $b = -O \to H(F) = O(1 - e^{-aF})$ (3)

Solve for a to get
$$
a = -\frac{1}{F} \ln \left(1 - \frac{H(F)}{O} \right)
$$
 (4)

If H_b and F_b are known values of *H* and *F* with *O* given,

$$
a = -\frac{1}{F_b} \ln \left(1 - \frac{H_b}{O} \right) \tag{5}
$$

Insert (5) into (3) to get
$$
H(F) = O\left[1 - \left(\frac{O - H_b}{O}\right)^{\frac{F}{F_b}}\right]
$$
 (6)

Bias = 1 implies $F = O$, and adjusted *H, H_a* is given by $H_a = O$

$$
H_a = O\left[1 - \left(\frac{O - H}{O}\right)^{\frac{O}{F}}\right] \qquad (7)
$$

Note that the subscript *b* has been dropped from (7) as the distinction is no longer needed as it is in (6).

What has happened since ? "Odds ratio method": declared not to have a valid basis

(Manuscript on only one method about to be submitted/ in internal review)

Eta vs NMM:

East, no major topography: 12-km Eta about the same as the 8-km NMM, even a tiny bit better; West, complex topography: 12-km Eta much better than the 8-km (sigma system) NMM !!

GFS vs Eta:

East: GFS (when corrected for bias) uniformly better; West: Eta *much* better (overcoming handicaps of the 6 h lateral boundary error, and less successful data assimilation) !

Thus, summary of performance results:

Very strong indication that the eta works extremely well !

But what about its downslope windstorm problem ?

The Eta Problem:

Flow separation on the lee side (à la Gallus and Klemp 2000)

Suggested explanation

Flow from left: from the box 1 the flow enters box 2 to the right of it. When conditioned to move downward, it will move downward via the interface between boxes 2 and 5. Some of the air that entered box 2 will continue to move horizontally into box 3.

Missing: the flow directly from box 1 into 5 ! (It would have existed had the discretization accounted for the terrain slope !) As a result: some of the air which should have moved slantwise from box 1 directly into 5 gets deflected horizontally into box 3.

Refined (sloping steps) eta

(Mesinger and Jovi ć)

Discretization accounting for slopes. Continuity equation ($\;$ at $\dot{\eta}$ $\;$ pøints not zero): \dot{q} poig

$$
\frac{\partial p_S}{\partial t} = -\int_0^{\eta_S} \nabla \cdot \left(\mathbf{v} \frac{\partial p}{\partial \eta} \right) d\eta - \left(\dot{\eta} \frac{\partial p}{\partial \eta} \right)_S \tag{3}
$$

Approach:

Define slopes at **v** points, based on four surrounding *h* points. Slopes discrete, valid on halves of the sides of *h* points, and halves of the eta layers. Slantwise transports calculated within the 1st term on the right of (3), and in other equations as appropriate.

Other possibilities available. However: keep the eta feature of having cells in horizontal of about equal volume (difference compared to Adcroft et al. 1997, shaved cells) ! This makes Arakawa-type conservation schemes, used in the Eta, very nearly finite-volume schemes. Also, robust in the CFL sense.

The sloping steps, vertical grid

The central **v** box exchanges momentum, on its right side, with **v** boxes of two layers:

Horizontal treatment, 3D

Example #1: topography of box 1 is higher than those of 2, 3, and 4; "Slope 1"

Inside the central **v** box, topography descends from the center of T1 box down by one layer thickness, linearly, to the centers of T2, T3 and T4

Slantwise advection of mass, momentum, and temperature, and " $\omega \alpha$ ":

Velocity at the ground immediately behind the mountain increased from between 1 and 2, to between 4 and 5 m/s. "lee-slope separation" removed. Zig-zag features in isentropes at the upslope side removed.

Conclusions (re eta)

12-km Eta: excellent QPF performance over complex topography ! Better than the sigma system 8-km NMM, and better than the GFS;

The Eta downslope windstorm problem: correctible/ corrected, while keeping favorable Eta features: quasi horizontal coordinates (PGF !); very nearly finite-volume; robustness in the CFL sense.

Some of the references made

Baldwin, M. E., and J. S. Kain, 2005: Sensitivity of several performance measures to displacement error, bias, and event frequency. *Wea.*

Simmons, A. J., and D. M. Burridge, 1981: An energy and angular-momentum conserving vertical finitedifference scheme and hybrid vertical coordinates. *Mon. Wea. Rev*., **109**, 758-766.