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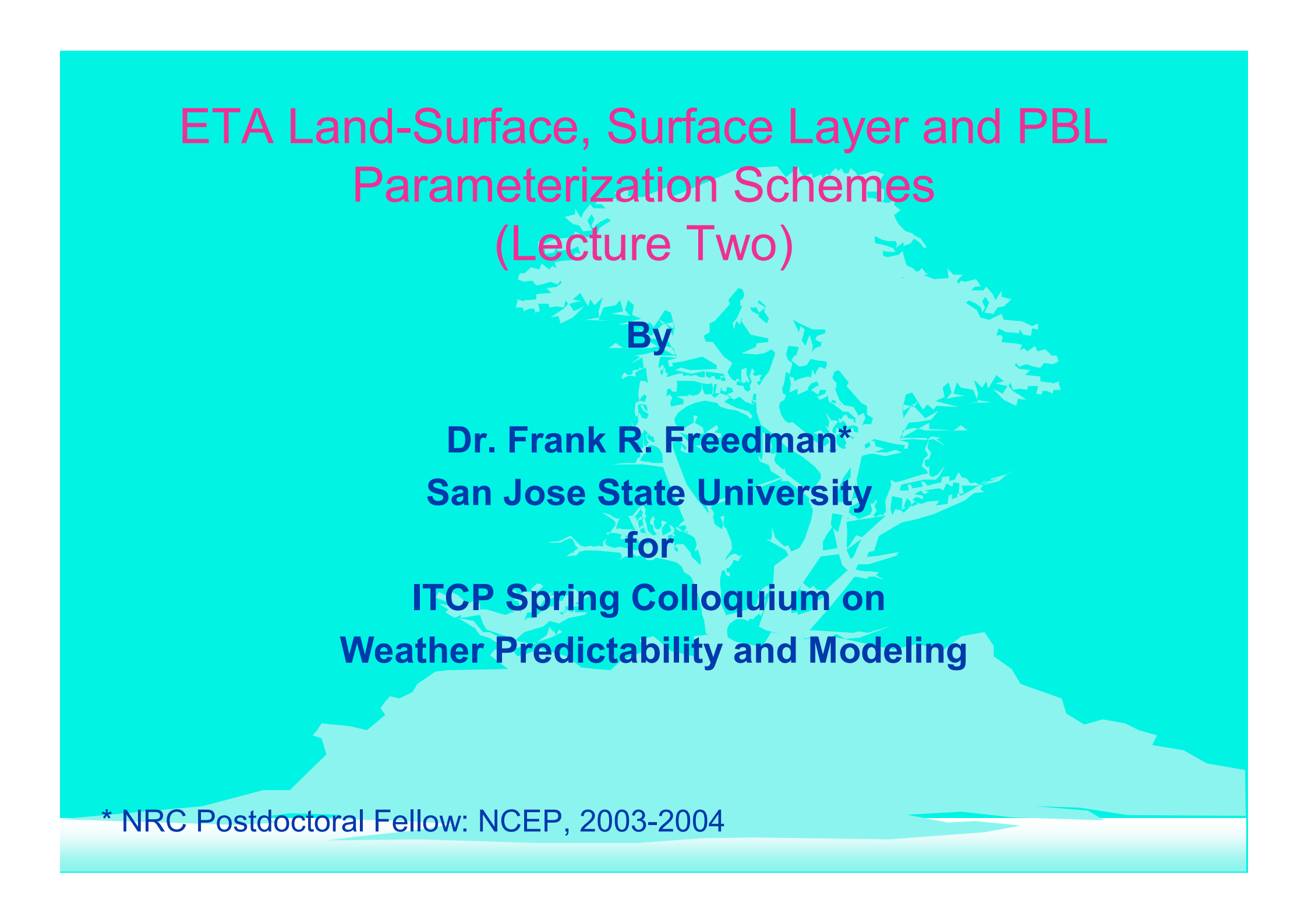
Spring Colloquium on
'Regional Weather Predictability and Modeling'
April 11 - 22, 2005

- 1) *Workshop on Design and Use of Regional Weather Prediction Models, April 11 - 19*
- 2) *Conference on Current Efforts Toward Advancing the Skill of Regional Weather Prediction. Challenges and Outlook, April 20 - 22*

301/1652-2

ETA Land-Surface, Surface Layer and
PBL Parameterization Schemes
Lecture II

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The background of the slide features a stylized, low-poly illustration of a large tree with a thick trunk and dense foliage, set against a backdrop of rolling mountains. The color palette is muted, consisting of various shades of blue, green, and brown, creating a naturalistic yet artistic atmosphere.

ETA Land-Surface, Surface Layer and PBL Parameterization Schemes (Lecture Two)

By

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for

**ITCP Spring Colloquium on
Weather Predictability and Modeling**

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Outline

- **Overview of schemes ...**
 - **Land Surface Model (LSM)**
 - **Surface Layer (SL)**
 - **Planetary Boundary Layer (PBL)**
 - **Noah LSM**
 - **Surface Layer**
 - **Planetary Boundary Layer**
-
- Lecture 1
- Lecture 2



Surface Layer & PBL Schemes

Purpose



- Surface layer
 - Exchange of heat, water vapor and momentum between atmosphere and land surface
 - Stability functions from Monin-Obukhov theory
- PBL
 - Vertical turbulent dispersion of heat, water vapor and momentum throughout the PBL.
 - Achieved through turbulent viscosity (K_m) and diffusivities (K_h)

Further Attributes: Surface Layer

- Limits on u_* , z/L , and other parameters to not allow turbulent mixing to diminish to zero in stable stratification (nighttime).
- Surface layer wind speed augmented in unstable conditions to account for downdrafts
- Roughness length for heat lower than that for momentum.

Further Attributes: PBL



- Mellor-Yamada Level 2.5 turbulence closure
- Local diffusion scheme, i.e. flux = $-K \times$ (mean vertical gradient)
- Limits on length scale, turbulent kinetic energy to avoid mathematical singularities in Level 2.5 solution space.

Surface Layer

- Sensible Heat Flux Calculation

$$H_s = \rho C_p C_h U_{SL} (\theta_s - \theta_a)$$

- Momentum Flux

$$\tau = \rho C_d U_{SL}^2$$

- $U_{SL}^2 =$ effective surface layer wind speed $= U_a^2 + U_{conv}^2$
where U_a is wind speed within first vertical layer
and U_{conv} is a “convective” velocity (to be defined)
- $\theta_s =$ “skin temperature”, from land-surface scheme
- $\theta_a =$ Air temperature within first eta layer
- $C_h, C_d =$ Exchange coefficients for heat and momentum

Surface Layer Equations

$$C_d = \frac{k^2}{[\ln(h / z_{0,m}) + \psi_m(h / L) - \psi_m(z_{0,m} / L)]^2}$$

$$C_h = \frac{k^2}{([\ln(h / z_{0,h}) + \psi_h(h / L) - \psi_h(z_{0,h} / L)] \bullet [\ln(h / z_{0,m}) + \psi_m(h / L) - \psi_m(z_{0,m} / L)])}$$

FROM
MONIN-
OBUKHOV
THEORY

where:

$\Psi_{m,h}$ - Stability functions for heat (h) and momentum (m)

L - Monin-Obukhov length

$z_{0,m}$, $z_{0,h}$ - roughness lengths for momentum and heat

k - Von Karman constant = 0.4

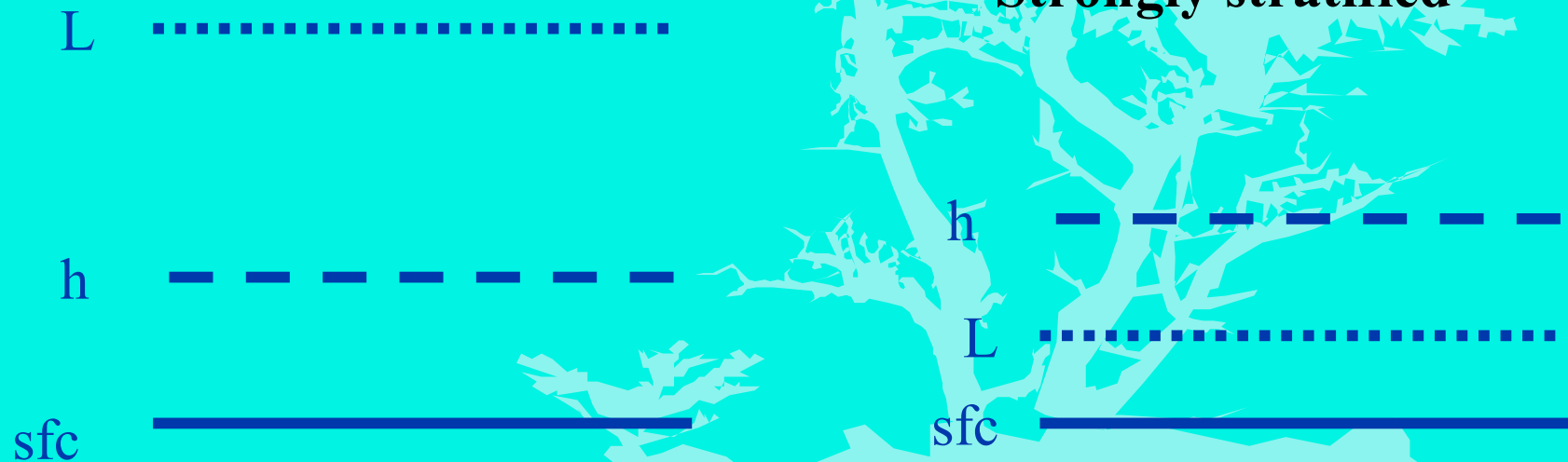
h - midpoint of lowest grid layer

Monin-Obukhov Length

$$L = -\frac{u_*^3}{k(g/\Theta_a)(H_s/\rho c_p)}$$

Weakly stratified

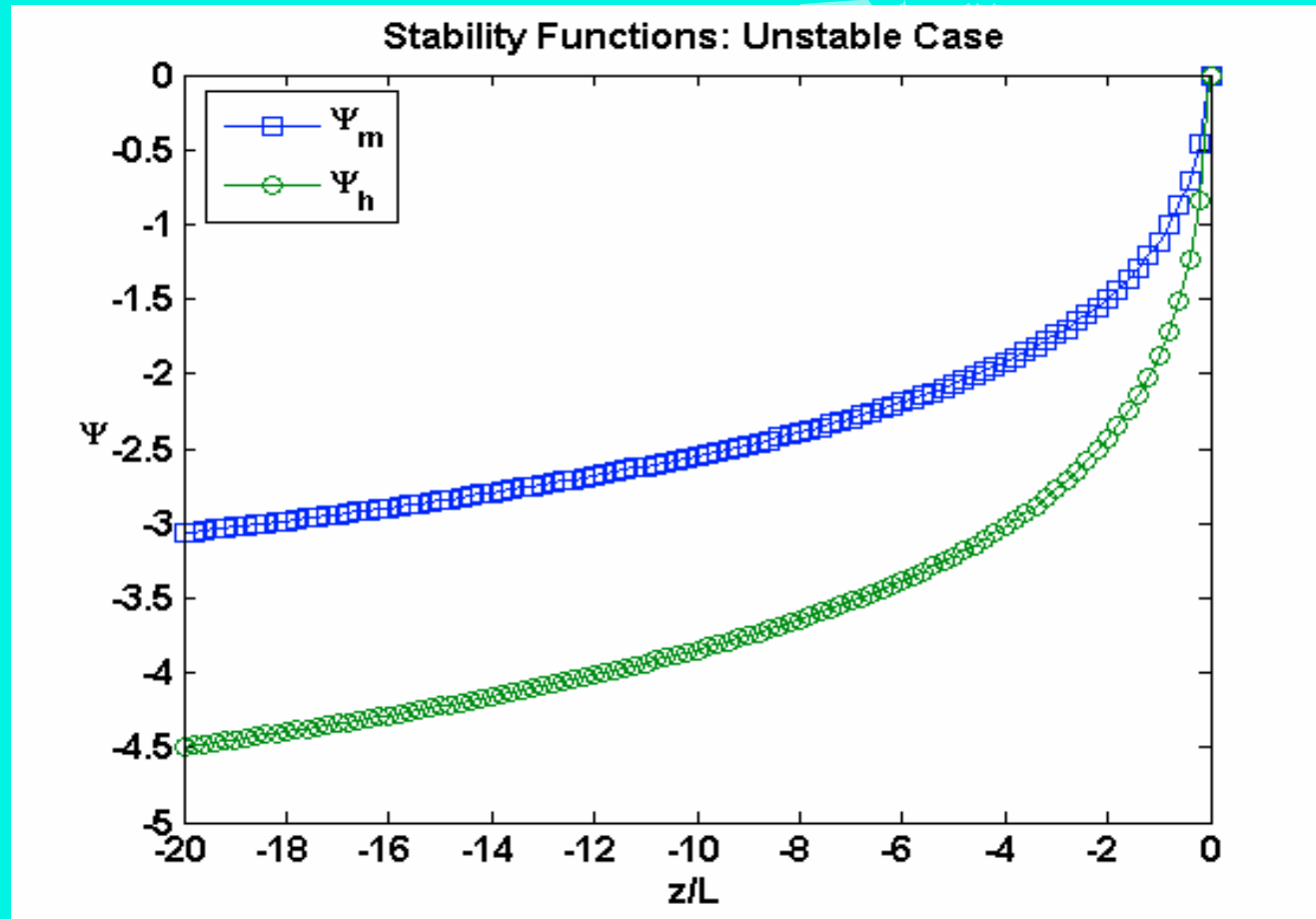
Strongly stratified



$h/|L| \ll 1 \sim$ quasi-neutral
Little effect of stratification
on fluxes

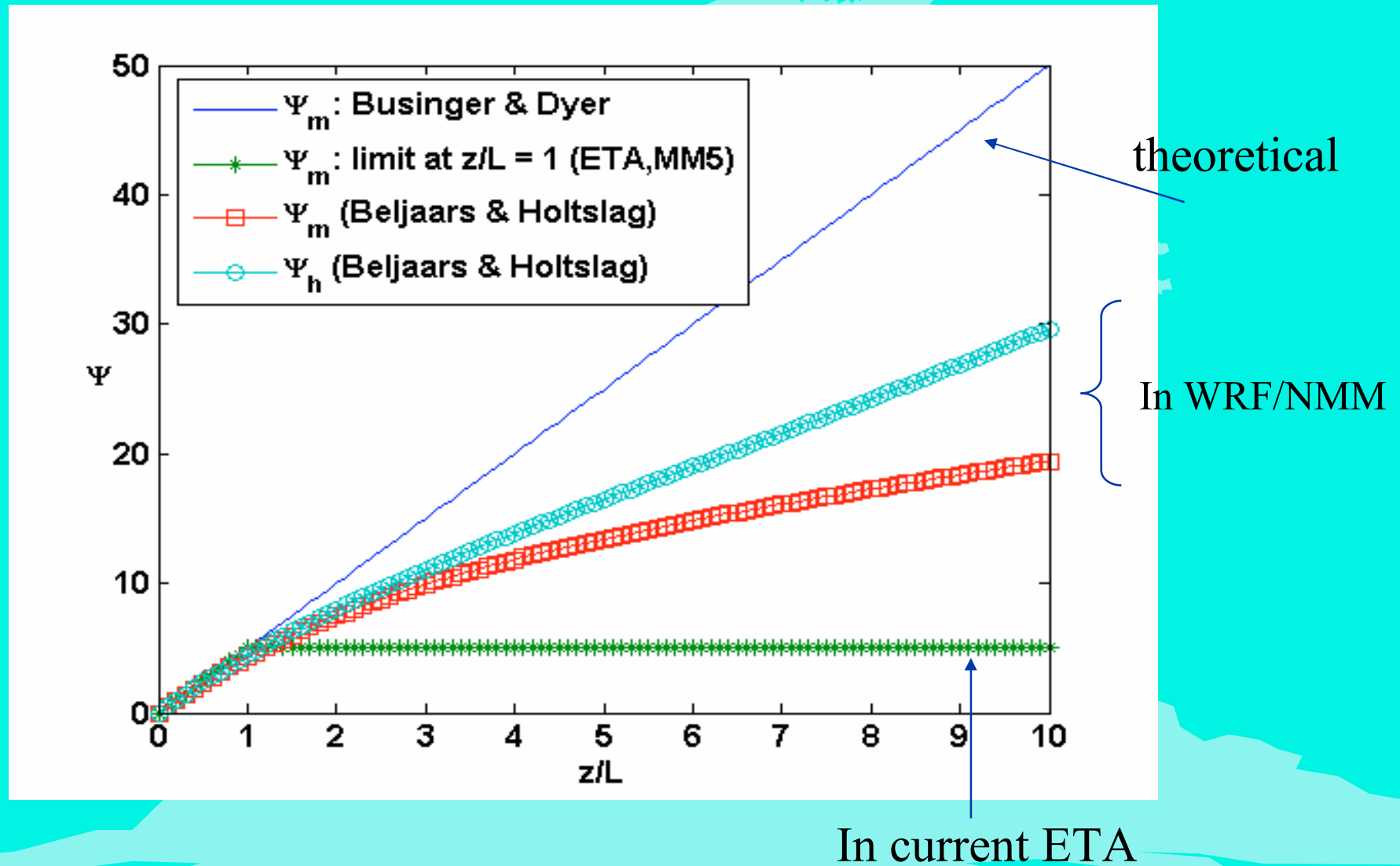
$h/|L| > 1$
Large effect of stratification
on fluxes

Stability Functions (Unstable Stratification, $L < 0$)



Equations from Paulson (1970)

Stability Functions (Stable Stratification, $L > 0$)



Elaborations & Limits

1) $z_{0h} < z_{0m}$

from Zilitinkevich (1995) ...

$$z_{0h} = z_{0m} \exp\left(-k C \sqrt{\text{Re}^*}\right)$$

$$\text{Re}^* = \frac{u_* z_{0m}}{\nu}$$

- Heat roughness can be orders of magnitude less than for momentum
- C – constant determined by numerical experimentation
- $C = 0.1$ chosen for ETA after substantial experimentation
- Affects surface fluxes and skin temperature during daytime conditions
- Positive impact of summer precipitation forecast scores

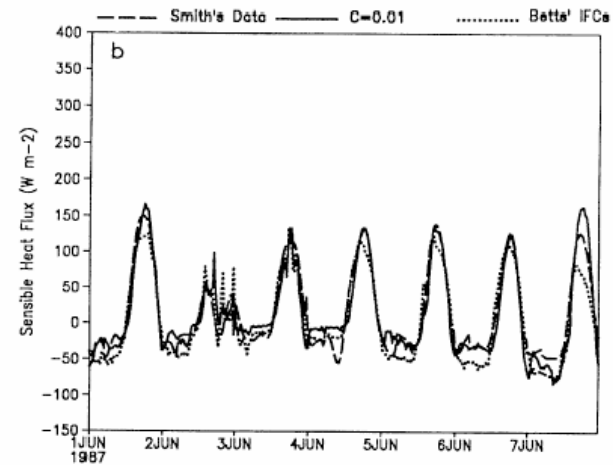
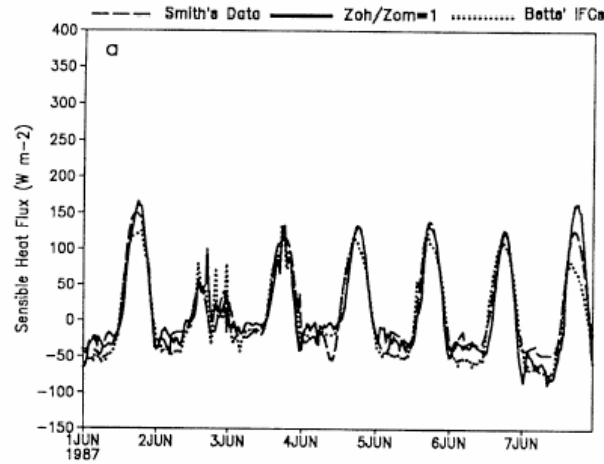
Details: Chen, Jancic & Mitchell (1997, BLM)

Effect on surface heat flux

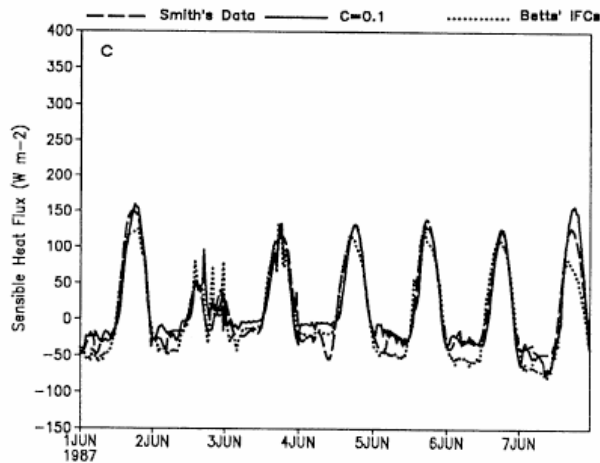
Offline testing: Predictions (solid), FIFE observations (others)

Source: Chen, Jancic & Mitchell (1997, BLM)

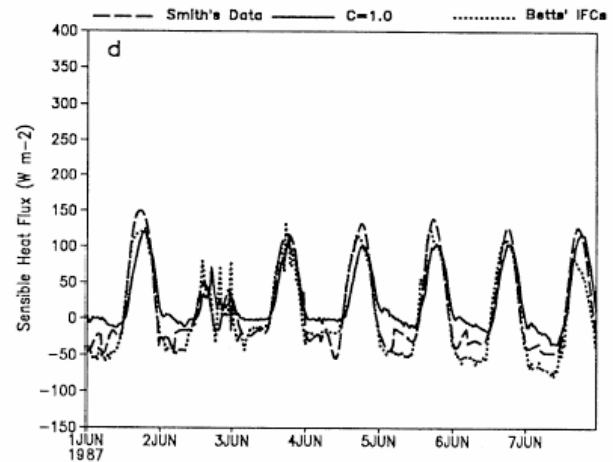
$Z_{0m} = Z_{0h}$



$C = 0.01$



$C = 0.1$



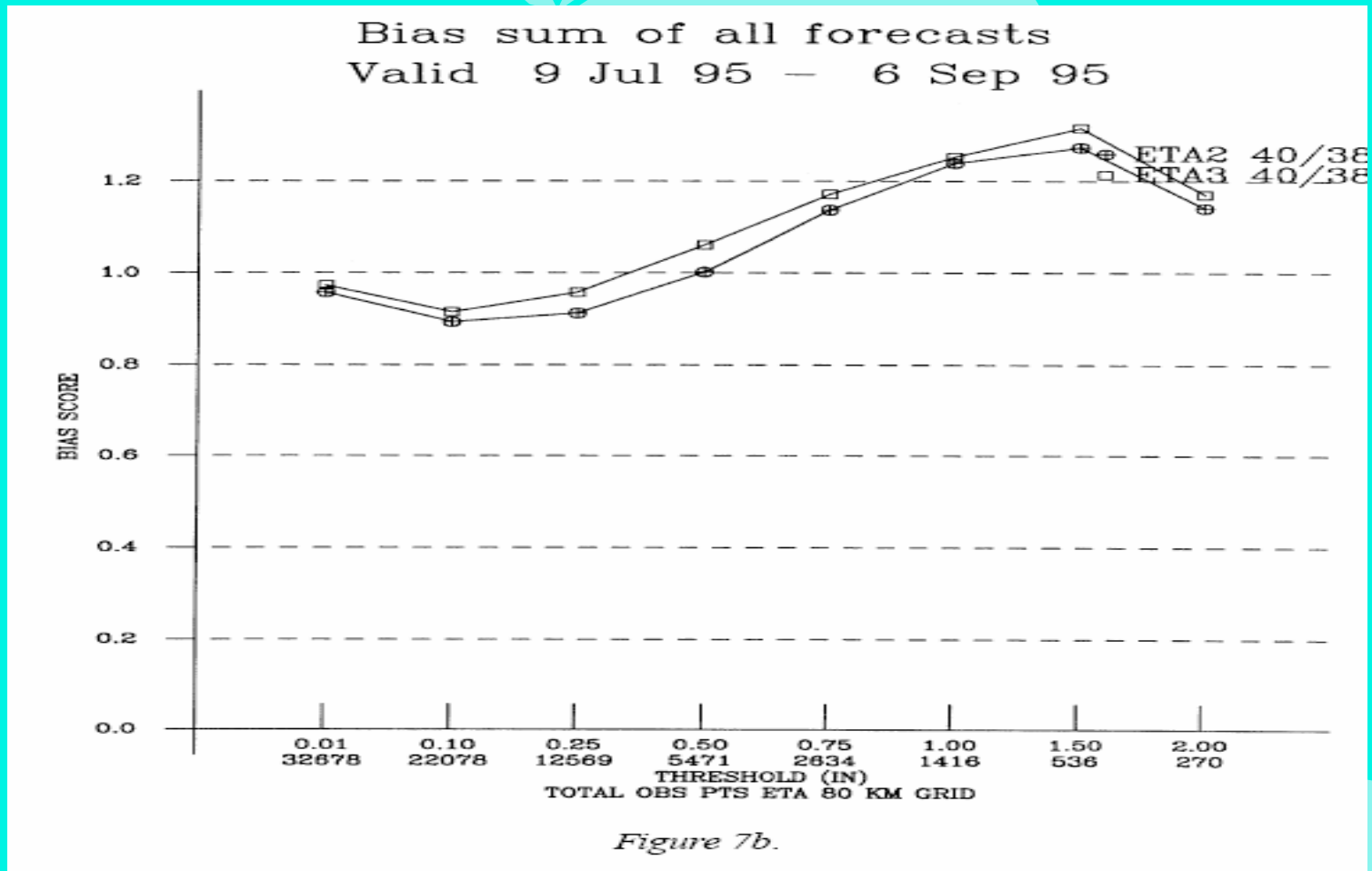
$C = 1$

Effect on summer precipitation

ETA2: $z_{0h} = z_{0m}$

ETA3: $z_{0h} = 0.1z_{0m}$

BIAS



THRESHOLD

Source: Chen, Jancic & Mitchell (1997, BLM)

2) Augmented SL wind speed (daytime, $H_s > 0$)

$$U_{SL}^2 = U_h^2 + U_{conv}^2$$

Added term

where

$$U_{conv} = \alpha w_*$$

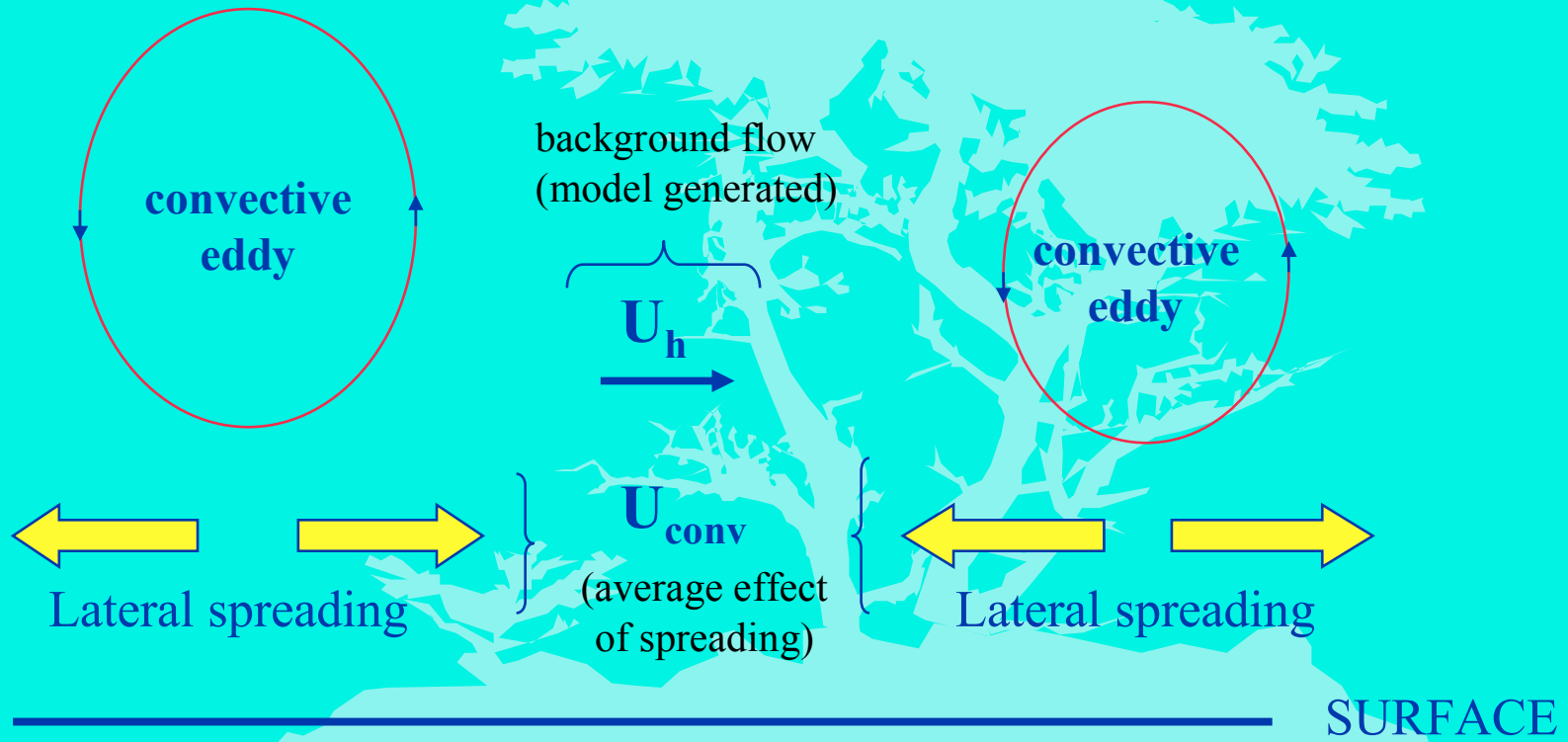
$$w_* = \left[\underbrace{(g/\Theta_a)(H_s/\rho c_p)}_{\text{Buoyancy flux}} \underbrace{h_{PBL}}_{\text{PBL depth}} \right]^{1/3}$$

FREE CONVECTIVE
VELOCITY SCALE

α ranges from 1-2
(1.2 in ETA)

Description ...

(lowest ~ 100 m)



3) Limits during stable, nighttime conditions ...

- Maximum value of $z/L = 1$
- Minimum value of $u_* = 0.07 \text{ ms}^{-1}$
- First imposition limits correction term in C_d , C_h calculation so that these do not become too small.
- Physically: maintenance of a “background level” of turbulent mixing in stable conditions.
- Helps keep near-surface temperatures from becoming too cold at night.
- Active area of research
 - assess origin of such turbulence
 - how to best parameterize from a fundamental basis.

PBL

COMPUTE VERTICAL TURBULENT MIXING AT EACH LEVEL ABOVE SURFACE

FOR EXAMPLE ...

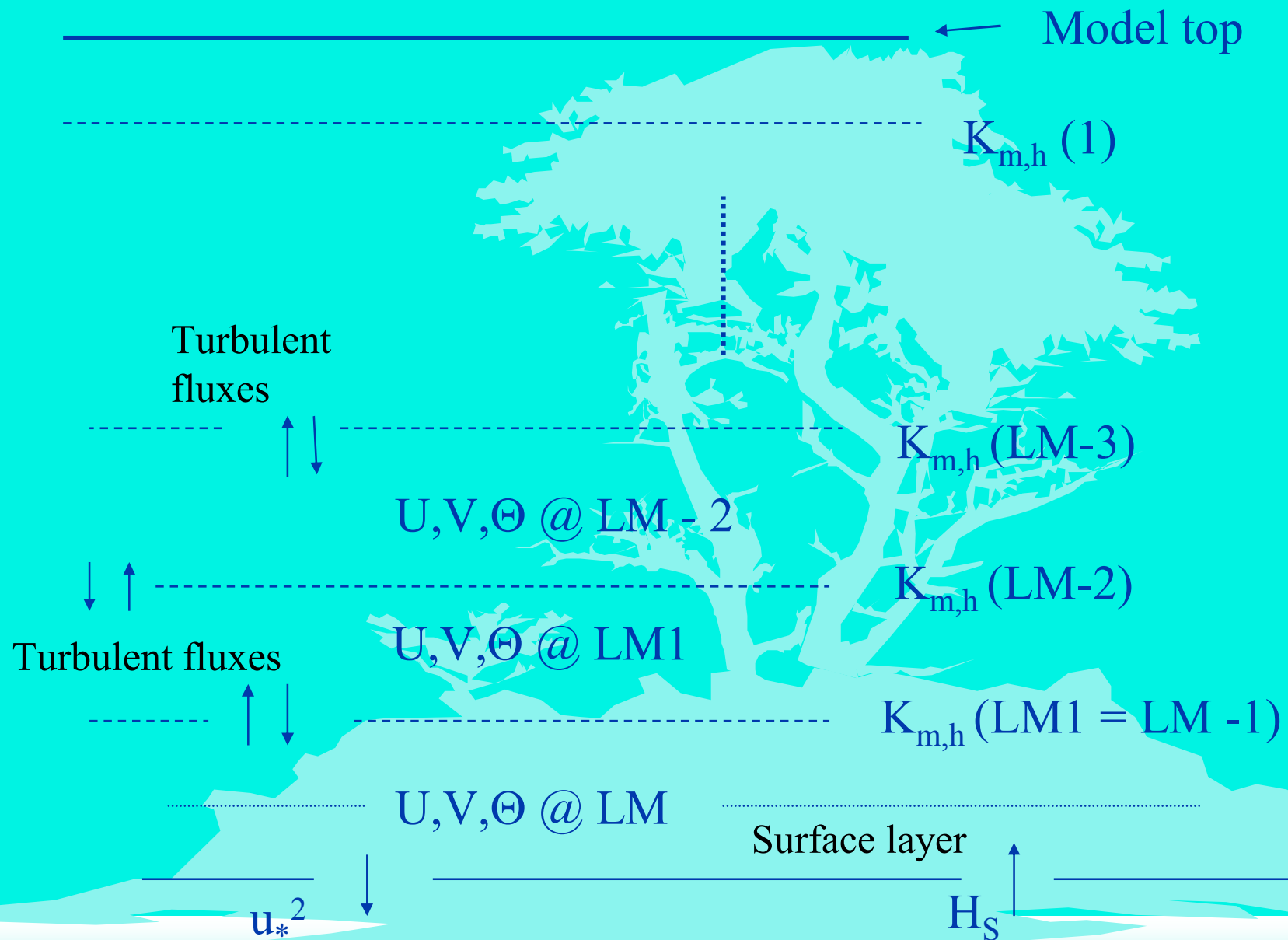
$$-\overline{w' u'} = K_M \frac{\partial U}{\partial z}$$

**Vertical turbulent flux
of u-momentum**

$$-\overline{w' \theta_v'} = K_H \frac{\partial \theta_v}{\partial z}$$

**Vertical turbulent flux
of virtual potential temperature**

ARCHITECTURE



PBL

- Based on prognostic “turbulent kinetic energy” (TKE):

$$q^2 = 2 \times \text{TKE} = (u')^2 + (v')^2 + (w')^2$$

- Level 2.5 Scheme:

$$K_M = lqS_M (G_M) \quad K_H = lqS_H(G_H)$$

l – mixing length, prescribed function of height and TKE

q^2 - solved from prognostic equation

$S_{m,h}$: stability functions of shear (G_m) and stability (G_h)

SUBROUTINES: MIXLEN, PRODQ2, DIFCOF, VDIFQ

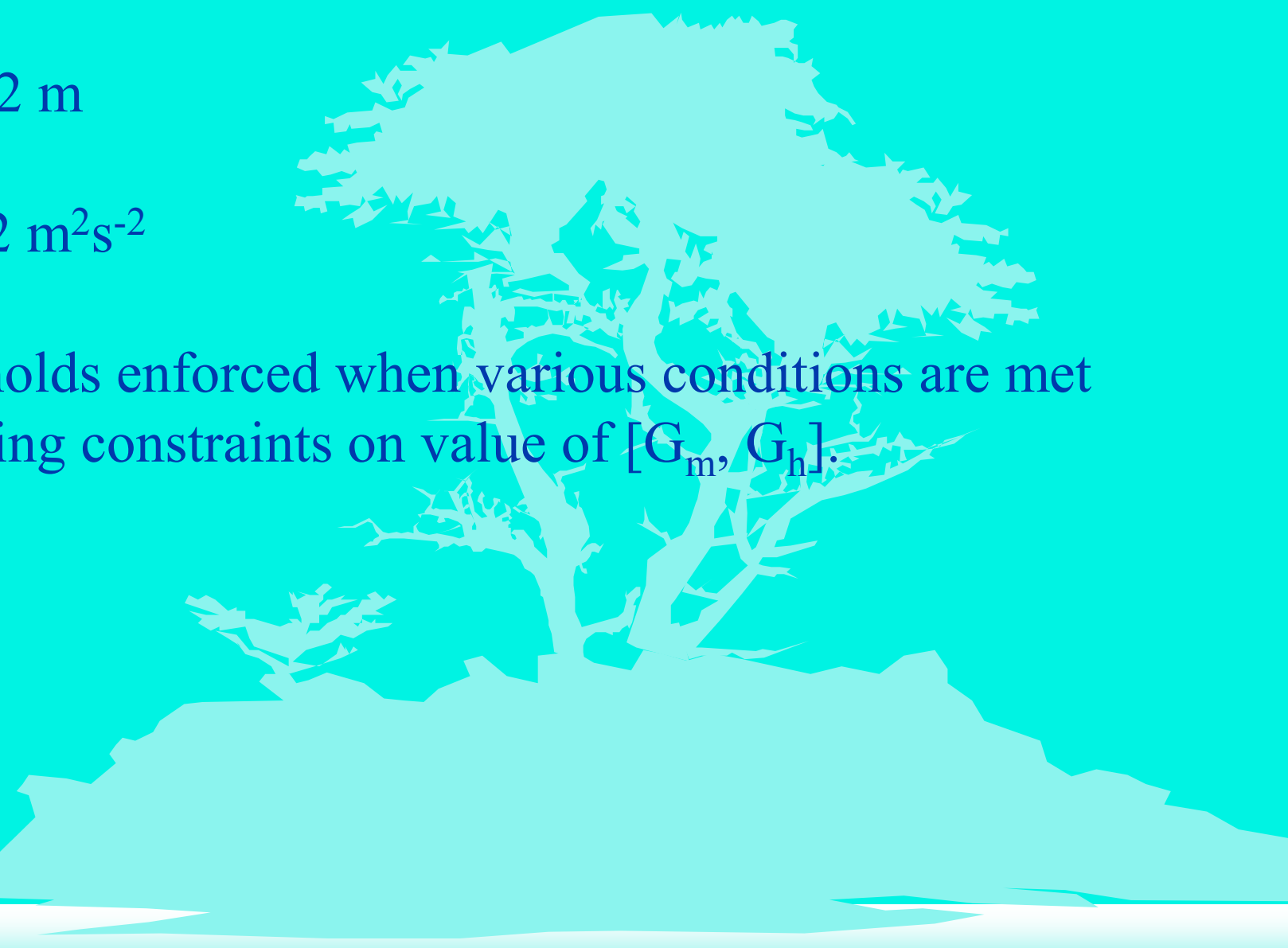
Details given by Dr. B. Rajkovic

LOWER LIMITS IN PBL SCHEME ...

1) $l = 0.32 \text{ m}$

2) $q^2 = 0.2 \text{ m}^2\text{s}^{-2}$

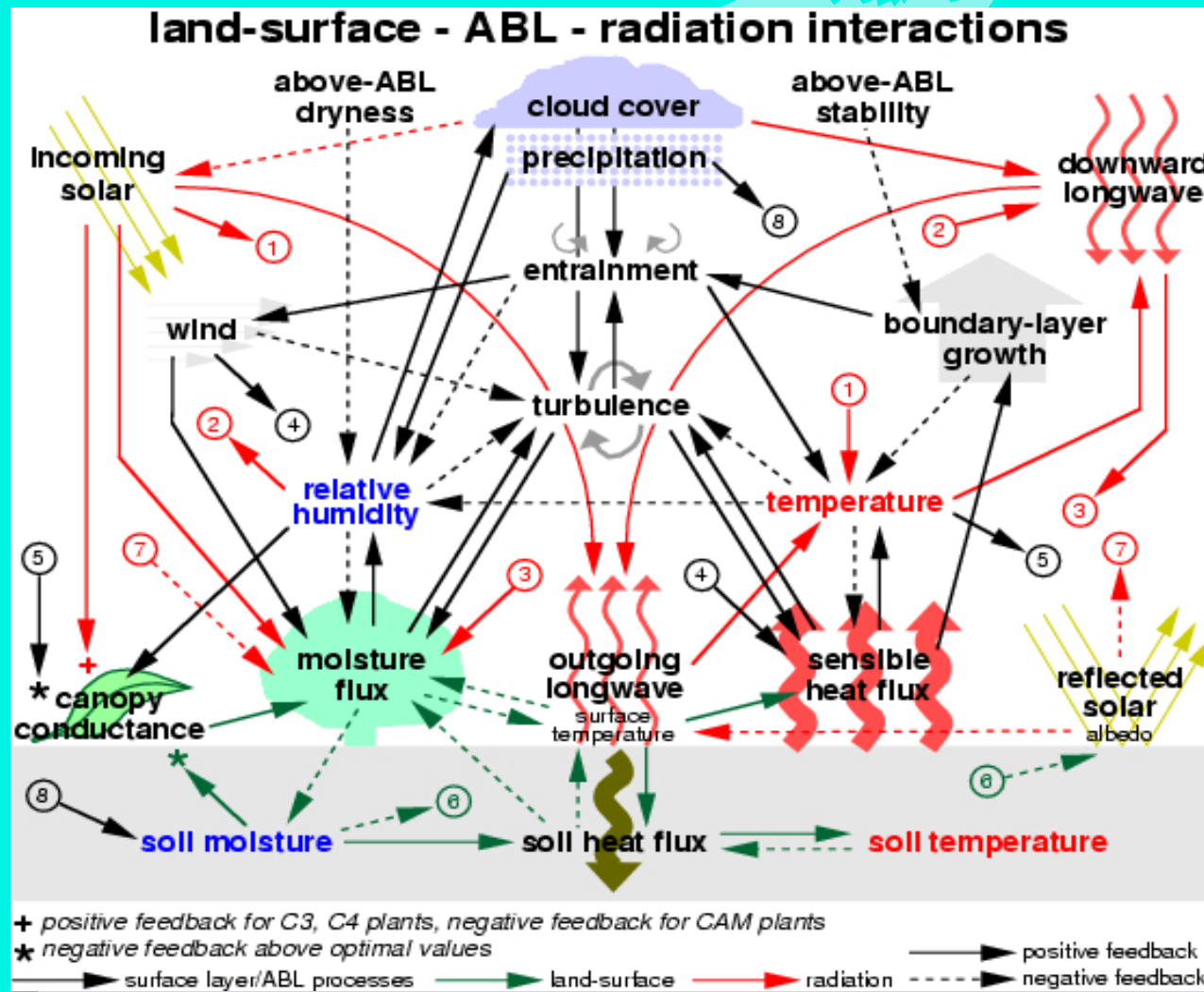
3) Thresholds enforced when various conditions are met involving constraints on value of $[G_m, G_h]$.



OFFLINE TESTING



PHYSICS “WHEEL OF PAIN”



OFFLINE TEST: SURFACE LAYER

- TWO-METER TEMPERATURE, Θ_{2m}
- CAN BE SHOWN (MO THEORY) ...

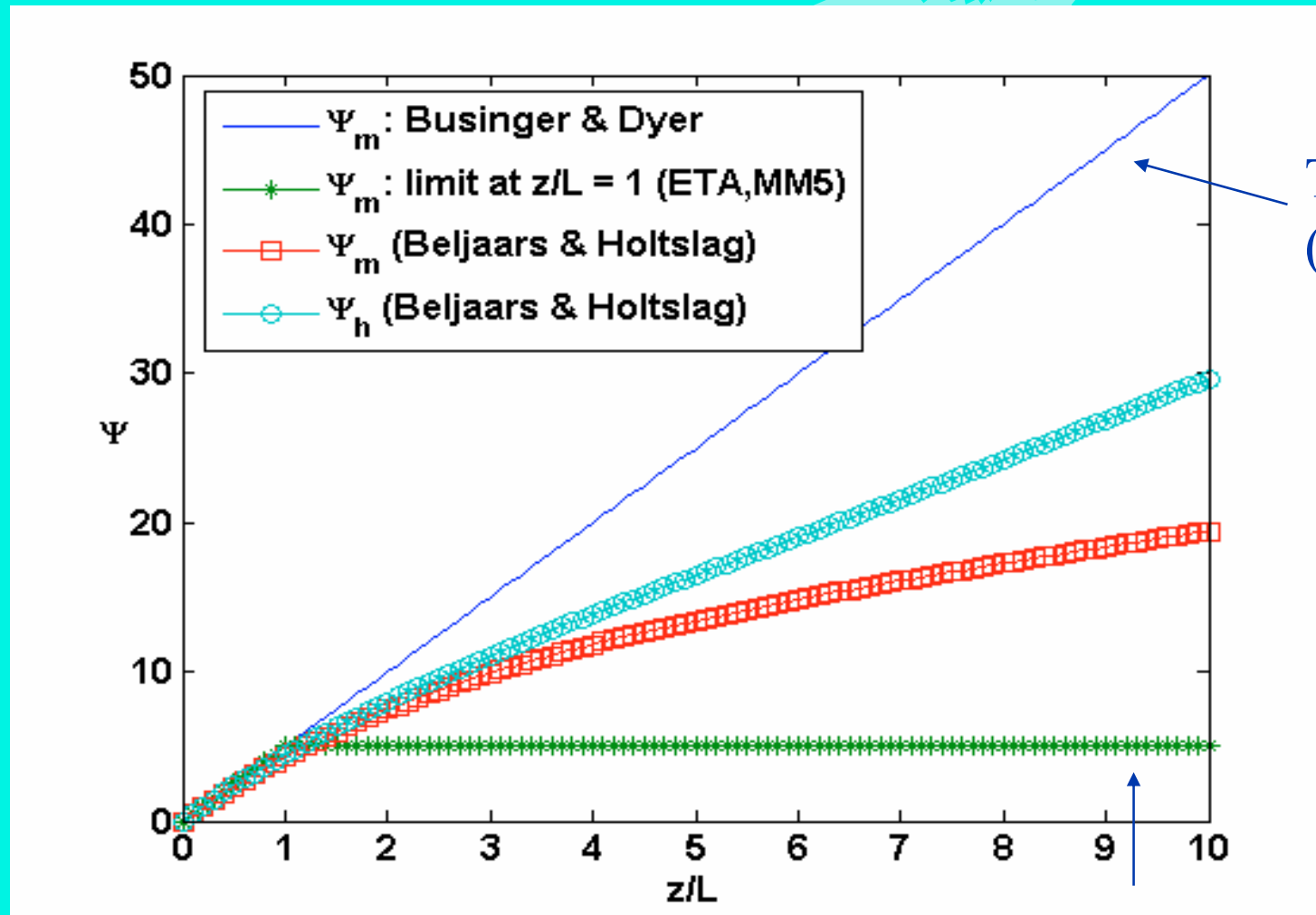
$$\Theta_{2m} = \chi \Theta_h + (1 - \chi) \Theta_0$$

WHERE

$$\chi = \frac{\ln(2/z_{0h}) - \psi_h(2/L)}{\ln(h/z_{0h}) - \psi_h(h/L)}$$

- PLUG IN OBSERVED Θ_0 , Θ_h and U_h
- COMPARE PREDICTIONS FROM WITH OBS.
- CASES99 DATA (STABLE ABL, KANSAS, 10/2002)
- NIGHTS 18, 19, 21, 22 (10-minute avg. data)
- 288 TOTAL DATA POINTS

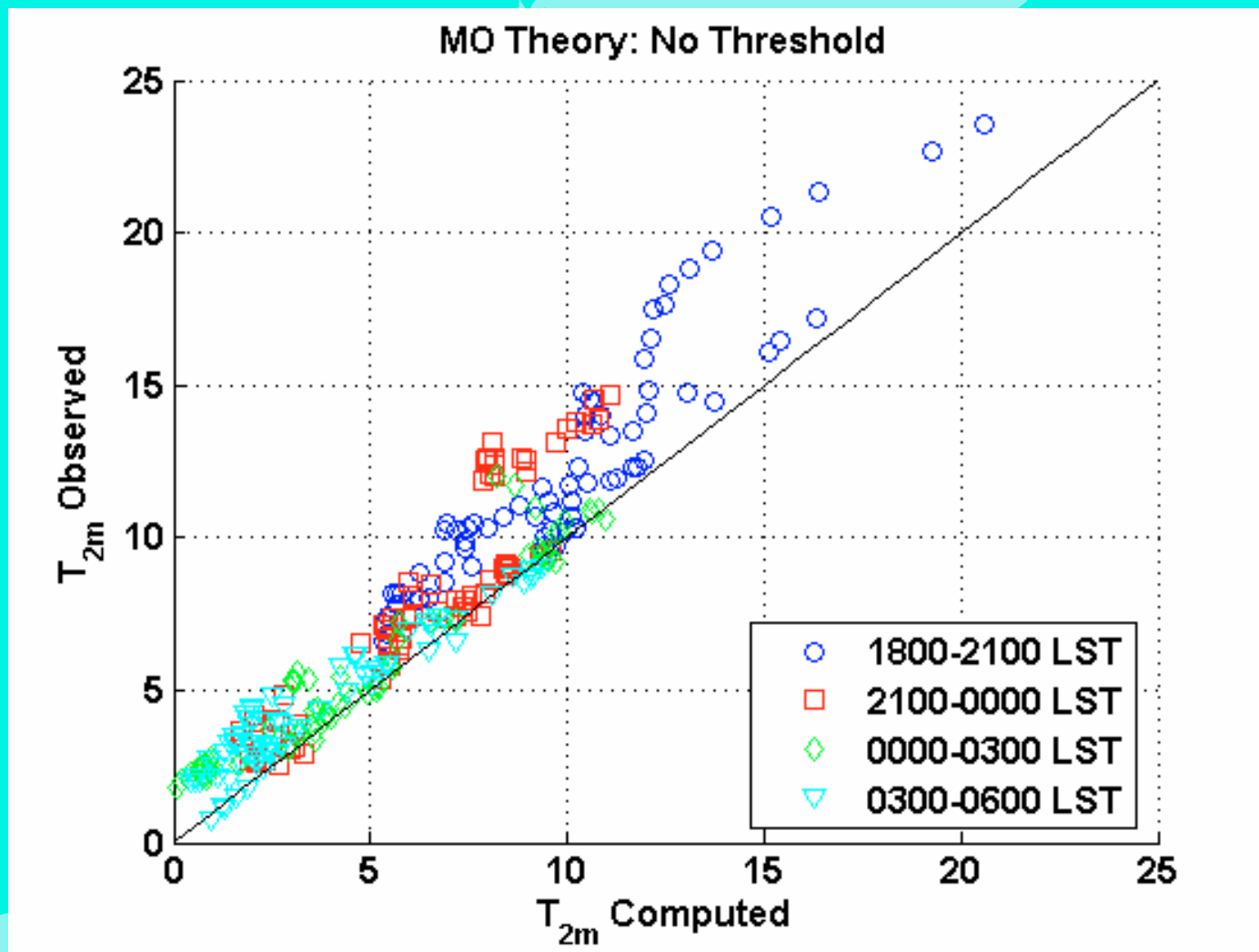
Stability Functions (Stable Stratification, $L > 0$)



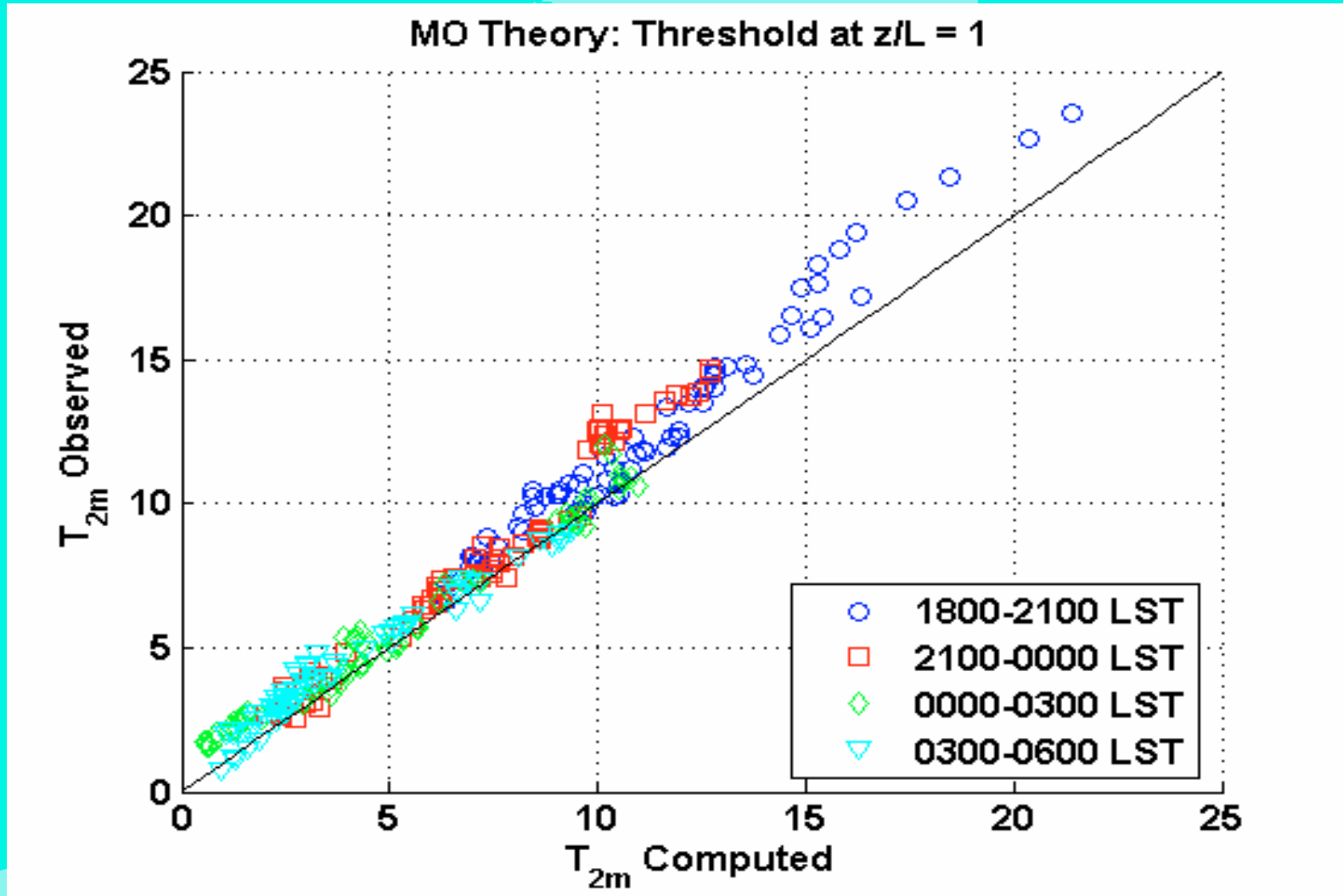
Theoretical
(test this)

Current ETA (test this)

STABILITY FUNCTIONS VIA MO THEORY: NO LOWER THRESHOLD ON Z/L (THEORETICAL)



STABILITY FUNCTIONS VIA MO THEORY: LOWER THRESHOLD AT $Z/L = 1$ (CURRENT ETA IMPLEMENTATION)



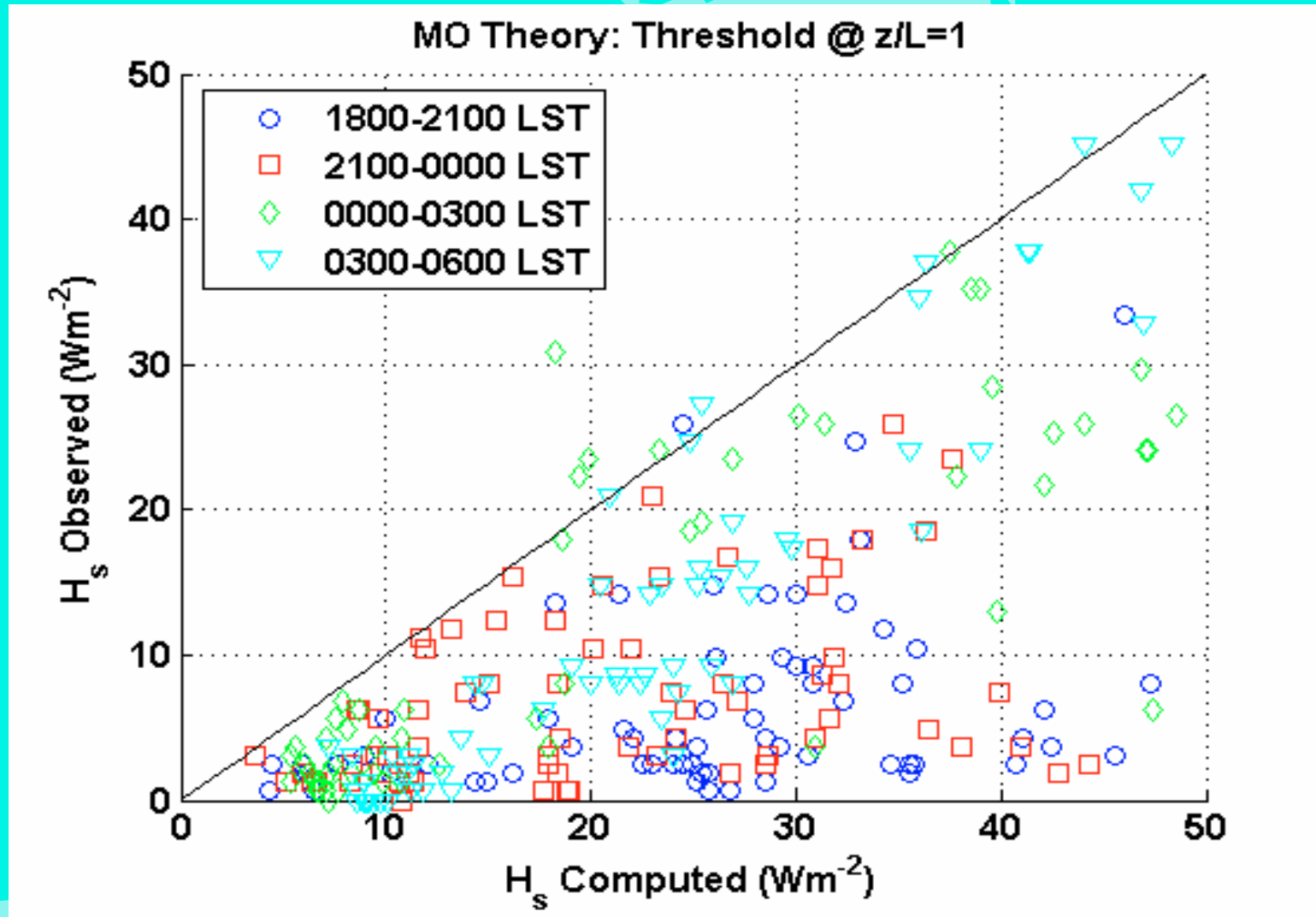
PERFORM TEST ON SURFACE HEAT FLUX ...

$$H_s = -\rho c_p C_h U_h (\Theta_h - \Theta_0)$$

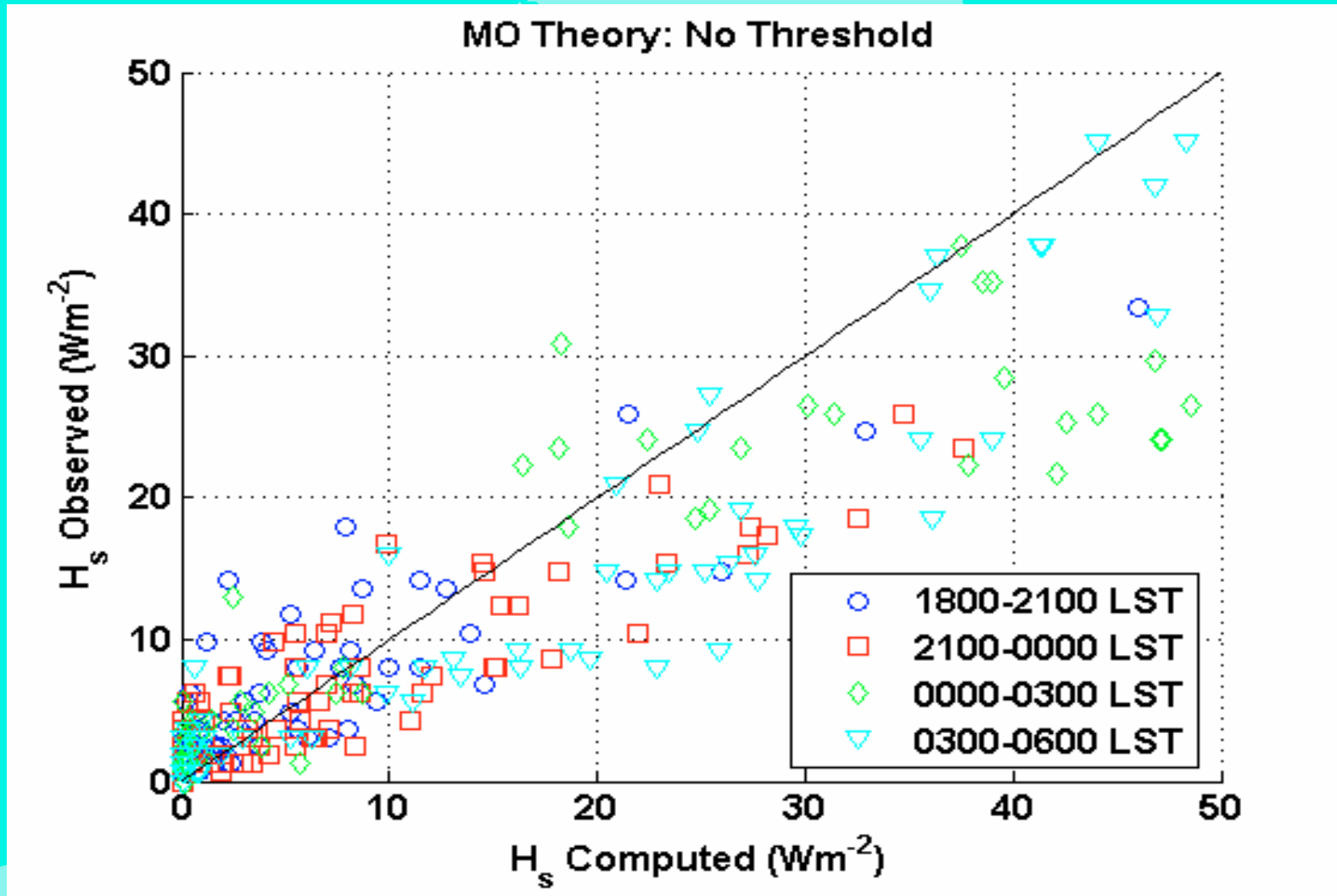
$$C_h = \frac{k^2}{([\ln(h / z_{0,h}) + \psi_h (h / L) - \psi_h (z_{0,h} / L)] \bullet [\ln(h / z_{0,m}) + \psi_m (h / L) - \psi_m (z_{0,m} / L)]]}$$

SAME PROCEDURE AS FOR
TWO-METER TEMPERATURE ...

STABILITY FUNCTIONS VIA MO THEORY: LOWER THRESHOLD AT $Z/L = 1$ (CURRENT ETA IMPLEMENTATION)



STABILITY FUNCTIONS VIA MO THEORY: NO LOWER THRESHOLD ON Z/L (STANDARD THEORY)



SUMMARY OF RESULTS

- LOWER THRESHOLD ON Z/L KEEPS 2-M TEMPERATURES WARMER THAN THEY WOULD BE OTHERWISE
- HELPS ALLEVIATE NIGHTTIME COLD BIAS IN ETA (ALTHOUGH IT STILL EXISTS ...)
- TEST SUGGESTS THAT IT DOES SO BY CREATING ARTIFICIAL” DOWNWARD HEAT FLUX
- MUST UNDERSTAND PHYSICS BETTER TO ARRIVE AT MORE FUNDAMENTAL CORRECTION

SUGGESTED EXERCISES I

- C factor in Zilitinkevich thermal roughness equation
 - Subroutine REDPRM (in SFLX.F, change CZIL_DATA in PARAMETER statement from 0.2 to other values between 0 & 1).
 - Subroutine SFCDIF (SFCDIF.F, make identical change to CZIL in PARAMETER statement)
 - Check differences in **daytime** 2-meter temperature, surface fluxes & precipitation patterns

SUGGESTED EXERCISES II

- α factor for surface layer velocity enhancement term
 - Subroutine SFCDIF (make change to WWST in PARAMETER statement from 1.2 to other value in range 1-2)
 - Check differences in **daytime** 2-meter temperature, surface fluxes & precipitation patterns

SUGGESTED EXERCISES III

- Sensitivity to surface layer threshold values (SFCDIF)
 - Change ZTMAX (maximum z/L) in PARAMETER statement from 1 to other values. Large value (~ 100) effectively shuts off threshold since model calculations would not normally exceed this.
 - Change EPSUST (minimum u_*) in PARAMETER statement from 0.07 ms^{-1} to lower value (< 0.01 effectively shuts off threshold)
 - Check **nighttime** two-meter temperature, 10-meter winds, surface fluxes, mean profiles for sensitivity

SUGGESTED EXERCISES IV

- Different stability functions for stable conditions.
- Lines 64 and 66 in SFCDIF
 - Current: $\text{PSPMS}(YY) = 5*YY$ & $\text{PSPHS}(YY) = 5*YY$. This is the $\psi_m = \psi_h = 5z/L$, the theoretical relationship plotted in the above figure for stable stability functions ($yy = z/L$).
 - Change:
 - $\text{PSPMS}(YY) = 0.7*yy + 0.75*yy*(6.-0.35*yy)*\exp(-0.35*yy)$
 - $\text{PSPHS}(YY) = 0.7*yy + 0.75*yy*(6.-0.35*yy)*\exp(-0.35*yy)$
 - Similar to Beljaars & Holtslag functions in stability function plot.
 - Set $ZTMAX = 100$ (or other large number) to not allow lower threshold to act. See previous slide.
 - Check **nighttime** two-meter temperature, 10-meter winds, surface fluxes, mean profiles for sensitivity