







SMR.1670 - 19

INTRODUCTION TO MICROFLUIDICS

8 - 26 August 2005

Wafer Bonding

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Wafer bonding

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There are only 3 basic concepts for making a micro/nanochannel: 1. drilling 2. carving and <u>sealing</u>

3. forming



1. surface micromachined



2. etched + waferbonded



3. grown carbon nanotube

Critical factors in wafer bonding



Wafer bonding (sealing at wafer scale)

Main concepts:

- 1. Direct (fusion, thermocompression)
- 2. Anodic (electrostatic, field-assisted thermal)
- 3. Intermediate layer



Let's do a bonding experiment

bonding starts here



Propagation of a "bonding wave" - takes seconds



Christiansen, MPI für Mikrostrukturphysik, Halle, D



Surface preparation



Schematic illustration of the adsorbate layers commonly expected on hydrophilic surfaces

Plössl e.a. Mat.Sci.Eng. R25, 1-88 (1999)

Surface cleaning procedures used before wafer bonding:

•RCA1 (NH₄OH/H₂O₂/H₂O 1 : 1 : 5) + RCA 2 (HCI/H₂O₂/H₂O 1 : 1 : 6)

•"Piranha" (H₂O₂/H₂SO₄)

•Conc. nitric acid







Bonding chemistry



Figure from: Christiansen, MPI für Mikrostrukturphysik, Halle, D





Gap closing theory for waviness



Waviness and (micro)roughness







Bonding interface after high temperature





Figure from: Christiansen, MPI für Mikrostrukturphysik, Halle, D

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Old school

Galileo Galilei, 1638

First hypothetical experiment and discussion on adhesion of solids with plane surfaces





IN LEIDA, Apprello gli Elfevinii. H. D. C. ZERVIII.

FRONTESPIZIO DEL DISCORSI E DIMOSTRAZIONI MATEMATICHE INTORNO A DLE NUOVE SCIENZE" "Fitenze, B. Biblioteca Nazumalei



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Bonding is about contact area and contact forces



Contact theory: Hertz



Hertz in 1880 investigated the deformation of polished glass lenses pressed together, in order to study the phenomenon of "Newton's rings"

His formulation forms the cornerstone of the theory of contact mechanics

Compression gives elastic deformation:

$$\frac{4a^3E}{3R(1-\nu^2)} = P$$

deformation:

$$\delta = \frac{a^2}{R}$$

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Contact theory: Derjaguin-Muller-Toporov

Include <u>surface adhesion energy</u> *w*:

$$\frac{4a^3E}{3R(1-v^2)} = P - 2\pi wR$$

with the adhesion energy given as:

$$w = \gamma_1 + \gamma_2 - \gamma_{12}$$



B.V. Derjaguin, V.M. Muller & Y.P. Toporov (DMT), J. Colloid Interface Sci. 53, 1975, p. 314 D. Maugis, J. Colloid Interface Sci. 150, 1991, p. 243





A stable bond is possible if:

Surface conditions allow a contact area large enough for a sufficient change in surface energy

Important parameters:

- * surface roughness
- * elasticity of materials
- * surface energy



Dimensional analysis of "bondability"

- "Soft" materials are easier to bond:
 - Bondability ~ 1/E [m³/J]
- Large interface energy leads to strong bond:
 - Bondability ~ w $[J/m^2]$
- Surface roughness of small height *h* or large wavelength λ is easy to deform:

– Bondability ~ λ/h [m/m]

since $\lambda \sim (R.h)^{1/2}$: Bondability $\sim (w/E).(R/h^3)^{1/2}$

=> Dimensionless parameter: (w/E).(λ /h²)





Contact between rough surface and rigid flat plane



Gaussian distribution of surface asperities

Mathematical treatment using Hertz-DMT theory leads to a characteristic parameter θ :

$$\theta = \frac{E^*}{w} \sqrt{\frac{\sigma^3}{R}}$$

with $\boldsymbol{\sigma}$ the standard deviation of the Gaussian curve

Gui e.a. J. Appl. Phys. 85, 7448-7454 (1999)



Bond area/energy vs. surface adhesion parameter



Bonding regime, θ <1 Non-bonding regime, θ >10 Adherence regime, 1< θ <10



Gui e.a. J. Appl. Phys. 85, 7448-7454 (1999)



Experimental results

Wafer	Surface modification	σ	R	η_{s}	$\sigma R\eta_s$
No.		[nm]	[µm]	[µm ²]	
6	CMP, Pad: IC 1000 / SUBA IV	1.2	10.9±4.6	6.25	0.08
	Slurry: Nalco2350/ DI HzO1: 30				
7	CMP, Pad: IC 1000 / SUBA IV	1.1	13.3±5.1	4.41	0.07
	Slurry: Semisperse25/DI HzO1: 2				
8	HF (1 %) etching, 60 sec.	1.0	1.8±0.5	38.4	0.07
	KOH (33 %) etching 30 sec.				
9	HF (1 %) etching, 60 sec.	0.9	2.0±0.8	33.6	0.06
	KOH (33 %) etching 10 sec.				
10	No	< 0.1	76.2 + 43	21.2	0.07



Experimental results cont^d.

Bonded wafer pairs θ		Bond speed	Specific effective	Voids
			bonding energy [J/m ²]	
Nos. 1 and 6	9.5	With pressure, slow	0.05	a few
Nos. 2 and 7	7.7	slow	0.07	a few
Nos. 3 and 8	16.	Not bondable	-	-
	8			
Nos. 4 and 9	13.	Not bondable	-	-
	8			
Nos.5 and 10	0.1	Spontaneously	0.10	No

Results of direct wafer bonding at room temperature

I	2	Δ	+
	0	A	_

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Intermezzo:

Reducing surface roughness by CMP

Surface roughness after machining





Source: Machinery's Handbook, 24th ed., Industrial Press, 1992

CMP vs Mechanical Polishing





Micro-reaction Zone

as'

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Chemical mechanical polishing, CMP





 $R_{r} = K * P * V$

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CMP and bonding of Si-based materials



DWB between SCS and SCS after KOH etching and CMP





DWB between P^{++} Si and LPCVD Si_{3+x}N₄ after CMP









DWB between SiO₂ and LPCVD Polysilicon after CMP





DWB between SCS and PECVD SiO₂ after CMP





Effects of CMP

- Reduction of roughness •
- Surface (chemical) conditioning •
- Planarisation •



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before and after planarisation by CMP



Planarisation of PECVD silicon oxide





Selective direct bonding



Selective bonding for NC-valve





Layer transfer by direct bonding



Smart cut process



Figure from: Christiansen, MPI für Mikrostrukturphysik, Halle, D



For details see: Tong e.a. Adv.Mat. 11, 1409-1425 (1999)



Smart cut process: surface before polishing







Layer transfer by waferbonding



Thick buried oxide

Multiple buried layer stack



Figure from: Aspar, TraciT Technologies, Grenoble, F



Pattern transfer by waferbonding





SOI devices transfered onto 200 mm fused silica wafers



Silicon on plastic





Maleville e.a. Solid-State Electr. 48, 1055-1063 (2004)



Layer transfer onto etched wafer



6-7 µm SOI layer





InfraRed microscopy: Newton rings



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Multiple layer stacks with patterns



micro gas turbine, 6 or 7 Si wafer stack, deep RIE features, direct bonding, <0.5 µm alignment accuracy



Pressure fed microrocket, chamber pressures to 125 Atm (60 achieved), 6 layer stack, direct bonding. Glass frit and anodic bonding used in packaging



- Direct Glass-to-Glass Bonding



Several glass types (BF33, AF45, fused silica, Pyrex) Glass thickness: 1.1 mm (standard), 175 μm (conf. micr.)



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Microfabricated reactors "piled up"



Fig. 3 A photograph of the ten-layer, pile-up microreactor.







Hydrogen Fluoride bonding





Nakanishi e.a. Sens.Act.A 79, 237-244 (2000)

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HF bonding for UV flow cell







Direct polymer bonding



- a. before bonding
- b. after direct bonding

c. after annealing above the glass transition temperature of the polymer



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b.

c.







Intermezzo:

Plasma activation

Theories why plasma activation helps

•Cracks and removes hydrocarbons

• Modifies surface chemistry (terminates surface with O and OH species)

• Increases porosity of surface oxide

• Increases surface hydrophilicity



Result:

• high bond energy after lower temperature anneal

• faster bonding kinetics



Pictures from: Gabriel, Süss MicroTec, D





Plasma over complete wafer - EVG, AU

Local plasma + scanning - Süss MicroTec, D





Anodic bonding



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0.02

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a) b)

30 **↑**



Electrostatic attractive force

Depleted

Depleted

Si-O bond

zone

Bonding time [sec]

States described in

c) <= the corresponding subfigures

zone

Conditions

For 0.5 mm Pyrex glass to silicon: T = 400-450 °C, V = 500V

Glass types containing ions like sodium that become mobile at higher temperature, work best



A point electrode is prefered to avoid multiple bonding starting locations and improve uniformity

Thermal expansion matching





Channel collapse during anodic bonding



Bonding parameters: 1027 V, 450 °C, 30 min. Microchannel depth: 168 nm in (a), 207 nm in (b)

Collapse can be avoided if:

$$\frac{\varepsilon_{air}V^2a}{E_{eff}d^3} < 1$$

with E_{eff} characterising the stifness of the materials, *a* the half with of the channel, *d* channel depth



Shih e.a. J.Appl.Phys. 95, 2800-2808 (2004)







Case study: peristaltic micropump with low-dead-volume pumping chambers



Peristaltic micropump







Veenstra e.a J. Electrochem. Soc. 148, G68-G72 (2001)

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Peristaltic micropump



425°C

Selective anodic bonding





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Cr works, Al does not



Anodic bonding with intermediate film

- Silicon-to-silicon with sputtered Pyrex layer; e.g. Berenschot e.a. Sens.Act.A 41/41, 338-343 (1994)
- Glass-to-glass with sputtered Si layer; e.g. Kutchoukov e.a. Proc. Transducers'03, (Boston, June 8-12, 2003) 1327-1330; shows 50 nm deep channels



Anodic bonding with intermediate PECVD films



Glass-to-glass bonding results for different intermediate layers (+, strong bonding; -, no strong bonding obtained)

Layer no. 2	Layer no. 1						
	(a) None	(b) Polysilicon	(c) Nitride	(d) Oxide	(e) α-Silicon	(f) Carbide	
(1) None	-	-	-	-	-	-	
(2) Polysilicon	+	-	-	+	-	-	
(3) Nitride	+	-	-	+	-	-	
(4) Oxide	-	-	-	-	-	-	
(5) α – Silicon	+	-	-	+	-	-	
(6) α – Silicon/nitride	+	-	-	+	-	-	
(7) Carbide	+	-	-	+	-	-	
(8) Nitride/oxide	+	-	-	+	-	-	
(9) α – Silicon/oxide	+	-	-	+	-	-	



Berthold e.a. Sens.Act.A 82, 224-228 (2000)







Bonding with intermediate layers



Low melting point bonding films, e.g.:

- spin-on sodium silicate, 90 °C; Wang e.a. Sens.Act. B 45, 199-207 (1997)
- Si-Au eutectic alloying, 365 °C; Wolffenbuttel e.a. Sens.Act. A. 43, 223-229 (1994)
- In-Sn solder, 160 °C; Lee e.a. Sens.Avt. A 85, 330-334 (2000)











Photoresists as bonding layers

Polymer	Film thickness (µm)
SU-8	20-30
BCB	15–25
JSR-137N	20-30
AZ-4620	10-20
SP-341	15–20

Range of film thickness of the photosensitive used



Pan e.a. Microel.Reliab. 45, 657-663 (2005)





Example: SU-8 on SU-8





Silicon





Solvent bonding for polymer microfluidics



In (B) the assembly is heated, and liquid paraffin wax fills the microchannels; in (C) the device is cooled to solidify the wax, PDMS slab is removed and placed on the opposite side of PMMA to protect device exterior; patterned side of PMMA is coated with acetonitrile (black). In (D) a second PMMA piece is pressed against first PMMA for 2 min to effect bonding. In (E) the device is heated to melt the wax, which is removed by combination of vacuum and dissolution in cyclohexane.



Kelly e.a., Anal. Chem. 77, 3536-3541 (2005)





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Case study Field-effect flow control

μTICs microchannels in glass

EOF control by radial voltage



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Electrical model





Fabrication of µTICs*



<u>µTIC devices</u>





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EOF as a function of Vg



Field-effect flow control devices on glass





Fabrication technology



Device ok, but low yield



Main problem: dielectric breakdown of insulator film (PECVD SiO_2) May be caused by high bonding temperature (600-650 °C)



Anodic bonding with intermediate silicon nitride layer



200 nm PECVD Si-nitride

400 °C, 1000 V, 1 hour

result: plates can be separated by knife

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Voids



water / air bubbles ?out gassing particles ?



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Combination of glass chip with electrodes and PDMS microchannels



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Influence gate potential on local zeta potential





<u>Velocity profiles under gate electrode for</u> <u>different zeta potentials</u>



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Gate DC voltage on-off

Gate AC voltage





Recommended reading

Q.-Y. Tong and U. Gösele Semiconductor wafer bonding: Science and Technology VCH-Wiley, New York, 1999

Proceedings Electrochemical Society Meetings, held regularly, mainly under the title "Semiconductor Wafer Bonding"



