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Controlled Fusion by a Staged Z-pinch

H.U. Rahman

GTT International Inc. U.S.A. Controlled Fusion by a Staged Z-pinch

*H.U. RAHMAN*¹, P. Ney², F. J. Wessel, and N. Rostoker University of California, Irvine, USA

Phys. Rev Lett. **74**, 714(1995) Phys. Of Plasmas, **58**, 367(1997) Phys. Of Plasmas, **11**, 5595(2004)

1. GTT International Inc.

2. San Jacinto College

Outline

- Motivation from the experiments.
- 2D numerical simulation.
- Control and mitigation of RT-instability.
- Importance of high Z radiative liner.
- Possibility of breakeven in fusion energy.
- Experimental implementation.

PINCH INSTABILITIES







SAUSAGE m = 0

m = 0;

$$\gamma = \frac{C_A}{r_o} \frac{(kr_o)}{l'_m (kr_o)} ;$$

compressible, k -> 0;

$$\gamma = \frac{C_A}{r_o} \frac{(2 - \alpha^2)^{-1/2} kr_o}{\sim (50 \text{ ns})^{-1}}$$

RAYLEIGH TAYLOR



$$e^{2} = -kg + \frac{(\bar{k}\cdot\bar{B}_{o})^{2}}{4\pi\rho_{o}}^{2}$$
~ (10 ns)⁻¹

Staged Z-pinch



MAGNETO-INERTIAL FUSION

PINCH DYNAMICS

CURRENT DIFFUSES THROUGH HIGH Z LINER INNER LAYER OF LINER PEALS OFF PEALED OFF LAYER COMPRESSES TARGET UNSTABLE PART OF LINER STAYS BEHIND AT PEAK COMPRESSION, CURRENT TRANSFERS TO INNER STABLE LAYER.

BENEFITS

INERTIAL ENERGY TRANSFER TIMESCALES COMPRESSION IS RT STABLE BREAKEVEN FUSION IS PREDICTED

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STAGED Z-PINCH



Fusion Cross Sections



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STABILIZATION OF LINEAR PINCH

End-on Kerr cell photos

Stability of RT-instability

Unstable pinch



Pinch stabilized with B_z and B_{Θ} fields



D.J.Albares, N. A. Krall and C. L. Oxley, "Rayleigh Taylor Instability in a Stabilized Linear Pinch Tube," Phys. Fluids 4, 1031(1961).



Electrical Signals





Numerical Simulation

- 2&1/2 dimensional, time-dependent, single fluid, MHD simulation code.
- Used in Eulerian mode.
- External capacitor bank circuit is modeled.
- Tabular (SESAME) equations of state.
- Implicit MHD with components of **B** and **U**.
- Multi-species plasma.
- Flux-limited, single group, implicit radiation diffusion.

Equation used in the simulation

MACH2

Continuity Equation:

 $\frac{\partial \rho}{\partial t} = - \bigtriangledown \cdot (\rho \vec{u})$

Momentum Equation:

$$\begin{split} \rho \frac{\partial v^i}{\partial t} &= -\rho v^j \bigtriangledown_j v^i + \bigtriangledown_j [-(P+Q+\frac{1}{3}u_R)\delta^{ji} + \frac{1}{\mu_0}(B^jB^i - \frac{1}{2}B^2\delta^{ji}) + \\ \sigma^d_{ji}] \end{split}$$

Electron Specific Energy Equation:

$$\rho \frac{\partial \epsilon_e}{\partial t} = -\rho \vec{v} \cdot \nabla \epsilon_e - P_e \delta^{ji} \nabla_i v_j + \eta J^2 - \vec{J} \cdot \left(\frac{\nabla P_e}{en_e}\right) + \nabla \cdot \left(\kappa_e \nabla T_e\right) - ac\rho \chi_{planck} \left(T_e^4 - T_R^4\right) - \rho c_{v_e} \frac{\left(T_e - T_i\right)}{\tau_{ei}}$$

Ion Specific Energy Equation:

$$\begin{split} \rho \frac{\partial \epsilon_i}{\partial t} &= -\rho \vec{v} \cdot \bigtriangledown \epsilon_i + [-(P_i + Q)\delta^{ji} + \sigma^d_{ji}] \bigtriangledown_i v_j + \bigtriangledown \cdot (\kappa_i \bigtriangledown T_i) + \\ \rho c_{v_e} \frac{(T_e - T_i)}{\tau_{ei}} \end{split}$$

Radiation Energy Density:

$$\frac{\partial u_R}{\partial t} = -\rho \vec{v} \cdot \bigtriangledown u_R - \frac{4}{3} u_R \bigtriangledown \cdot \vec{v} + \bigtriangledown \cdot (\rho \chi_{ros} \bigtriangledown u_R) + ac\rho \chi_{planck} (T_e^4 - T_R^4)$$

Magnetic Induction:

$$\frac{\partial \vec{B}}{\partial t} = \bigtriangledown \times (\vec{v} \times \vec{B}) - \bigtriangledown \times (\eta \vec{J}) - \bigtriangledown \times (\frac{\vec{J} \times \vec{B}}{en_e}) + \bigtriangledown \times (\frac{\bigtriangledown P_e}{en_e})$$

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Elastic Stress:

$$\frac{\partial \sigma_{ji}^d}{\partial t} = 2\mu d_{ji}^d - v^k \bigtriangledown_k \sigma_{ji}^d$$

Fusion Neutron Production Rate and Energy Gain:

$$P_{DT} = 5.6 \times 10^{-13} \ n_D n_T (\bar{\sigma \nu})_{DT}$$
$$P_{DD} = 3.3 \times 10^{-13} \ n_D n_D (\bar{\sigma \nu})_{DD}$$

 $(\sigma \bar{\nu})_{DT}$ and $(\sigma \bar{\nu})_{DD}$ are determined from a table look up.

Elastic Stress:

$$\frac{\partial \sigma_{ji}^d}{\partial t} = 2\mu d_{ji}^d - v^k \bigtriangledown_k \sigma_{ji}^d$$

Fusion Neutron Production Rate and Energy Gain:

$$\begin{split} P_{DT} &= 5.6 \times 10^{-13} \ n_D n_T (\bar{\sigma\nu})_{DT} \\ P_{DD} &= 3.3 \times 10^{-13} \ n_D n_D (\bar{\sigma\nu})_{DD} \\ (\bar{\sigma\nu})_{DT} \text{ and } (\bar{\sigma\nu})_{DD} \text{are determined from a table look up.} \end{split}$$

Initial configuration for UCI Pinch



Ion density During run-in phase



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Current Density During run in phase



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Initial Configuration For Z-Facility



Dynamics of pinch During run-in Phase

Density

Ionization Charge state

Axial current density



ION DENSITY

Rayleigh-Taylor Instability



Growth of perturbations depend upon the radius of the pinch

Energy coupling

$$W = \int_{R_0}^{R} \frac{B_{\theta}^2}{8\pi} \bullet 2\pi R \bullet h dR$$

$$B_{\theta} = \frac{2I}{cR}$$

$$=h\left(\frac{I}{c}\right)^2\ln\left(\frac{R_0}{R}\right)$$

Final energy of the pinch depends weakly on the compression ratio!

ION DENSITY (Four initial radii)





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Ionization charge state (four initial radii)



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Profiles of charge state



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Axial current (four initial radii)



Profiles of axial currents



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Large Energy Production

- Xe liner is used
- Both the masses of the liner and the target are optimized
- Optimized parameters of the Z-facility are used
- Initial radius of 0.7cm is used
- Perturbation level of 0.1% is used
- 12 MJ of Energy is produced with a stored energy of 2 MJ.
- Real breakeven is possible with existing technology

Breakeven



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Energies



Ion Density (full run)





Ion Density (near peak)



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Magnetic Field (Full run)



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Magnetic field (near peak)



Axial current (full run)



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Axial current (near peak)



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Plasma ion temperature (full run)



Plasma ion temperature (Near peak)



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Conclusions

- R-T instability can be controlled.
- Pinch current is amplified.
- Current rise time is reduced.
- Breakeven fusion (i.e., nuclear energy larger than stored energy) is possible.
- Reactor design is not yet considered.