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**School on Physics, Technology and Applications of Accelerator Driven  
Systems (ADS)**

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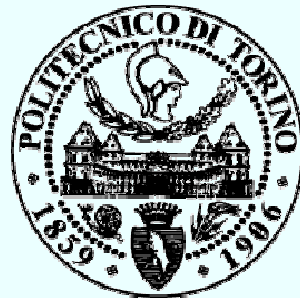
**ADS Dynamics  
"Accelerator-Driven System Dynamics  
Part I"**

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# Accelerator-driven system dynamics

## Part I

Politecnico di Torino  
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# Preface

Piero Ravetto:

- Professor of nuclear reactor physics
- Chair of the nuclear and energy engineering program

# Activities on reactor physics

Transport theory:

- Development of algorithms in  $P_N$  and  $S_N$  framework (FEM, BEM ...)
- Treatment of high anisotropy problems and reduction of ray-effects
- Propagation phenomena

# Activities on reactor physics

## Reactor dynamics:

- Development of algorithms and codes (quasi-static, multipoint...)
- ADS dynamics
- Interpretation of experiments

# Activities on reactor physics

Innovative reactor technology:

- Models and methods for fluid-fuel (molten-salt) systems
- Liquid-lead cooled reactors

# Standard tasks of reactor physics 1.

Describe basic phenomena of neutron  
motion in material systems:  
neutronic design of steady-state  
critical reactors



Provide multiplication parameters and  
flux distributions

# Standard tasks of reactor physics 2.

Short scale dynamic simulation

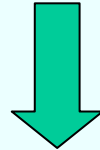


Provide information on transient  
behaviour in operational and accident  
conditions for stability and safety  
assessments



# Standard tasks of reactor physics 3.

Long scale dynamic simulation



Provide information on burn-up and  
nuclide evolution for fuel management

# A new challenge of reactor physics

Neutronic design of source-driven systems



New features in static and dynamic simulations

Need to develop specific models and algorithms

# Basics of transport theory for neutrons

The equation is of deterministic nature, the balance is based on statistical principles

The equation for neutrons can be derived from the original non-linear equation for particles in a force field removing the force term and assuming neutron collisions only with a fixed background of nuclei (equation becomes linear)

Transport (kinetic) theory plays a fundamental role for all the standard and advanced tasks of reactor physicists



Ludwig E. Boltzmann (1844 - 1906)

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# Basics of transport theory for neutrons

To write the particle balance probabilities per unit neutron path are needed: cross section  $\Sigma(\mathbf{r}, E)$

Emission function is also needed  $f(\mathbf{r}, E' \rightarrow E, \Omega' \cdot \Omega)$

**Note:** isotropic medium is supposed (does not imply isotropic emissions - important consideration for ADS !)

[J.J Duderstadt, W. Martin, *Transport Theory*]

# Basics of transport theory for neutrons

Neutron track length per unit volume, per unit energy, per unit solid angle, per unit time: **neutron flux** (velocity x density)

$$\varphi(\mathbf{r}, E, \Omega, t)$$

# Basics of transport theory for neutrons

Elementary **neutron current** vector,  
neutrons crossing the unit oriented area  
at one space point per unit time, per unit  
energy, per unit solid angle

$$\Omega\varphi(\mathbf{r}, E, \Omega, t)$$

# Integro-differential form (first order)

Local balance of particles

$$\begin{aligned} & \frac{1}{v(E)} \frac{\partial \varphi(\mathbf{r}, E, \Omega, t)}{\partial t} + \nabla \cdot \Omega \varphi(\mathbf{r}, E, \Omega, t) + \Sigma(\mathbf{r}, E) \varphi(\mathbf{r}, E, \Omega, t) \\ &= \int dE' \oint d\Omega' \Sigma(\mathbf{r}, E') \varphi(\mathbf{r}, E', \Omega', t) f(\mathbf{r}, E' \rightarrow E, \Omega' \cdot \Omega) + S(\mathbf{r}, E, \Omega, t) \end{aligned}$$

$$\varphi(\mathbf{r}, E, \Omega, t = 0) = \varphi_0(\mathbf{r}, E, \Omega) \quad \text{Initial conditions}$$

$$\varphi(\mathbf{r}_S, E, \Omega_{in}, t) = 0 \quad \text{Vacuum boundary conditions}$$



# Integro-differential form (second order, isotropic emissions)

even flux  $\psi(\mathbf{r}, E, \Omega, t) = \frac{1}{2} [\varphi(\mathbf{r}, E, \Omega, t) + \varphi(\mathbf{r}, E, -\Omega, t)]$

odd flux  $\chi(\mathbf{r}, E, \Omega, t) = \frac{1}{2} [\varphi(\mathbf{r}, E, \Omega, t) - \varphi(\mathbf{r}, E, -\Omega, t)]$

$$\left\{ \begin{array}{l} \frac{1}{v(E)} \frac{\partial \psi(\mathbf{r}, E, \Omega, t)}{\partial t} - \Omega \cdot \nabla \frac{1}{\Sigma(\mathbf{r}, E)} \Omega \cdot \nabla \psi(\mathbf{r}, E, \Omega, t) \\ + \Sigma(\mathbf{r}, E) \psi(\mathbf{r}, E, \Omega, t) = \frac{1}{4\pi} Q(\mathbf{r}, E, t) \\ \chi(\mathbf{r}, E, \Omega, t) = - \frac{1}{\Sigma(\mathbf{r}, E)} \Omega \cdot \nabla \psi(\mathbf{r}, E, \Omega, t) \end{array} \right.$$

Space second order term

# Integral form

## Global balance of particles

$$\varphi(\mathbf{r}, E, \Omega, t) =$$

$$= \int_0^{\text{Min}[s_0(\mathbf{r}, \Omega), vt]} ds \left[ \int dE' \oint d\Omega' \Sigma(\mathbf{r} - s\Omega, E') \varphi(\mathbf{r} - s\Omega, E', \Omega', t - \frac{s}{v}) f(\mathbf{r} - s\Omega, E' \rightarrow E, \Omega' \cdot \Omega) \right. \\ \left. + S(\mathbf{r} - s\Omega, E, \Omega, t - \frac{s}{v}) \right] \exp \left( - \int_0^s ds' \Sigma(\mathbf{r} - s'\Omega, E) \right)$$

# Integral form for isotropic emissions: Peierls equation

$$\Phi(\mathbf{r}, E, t) = \frac{1}{4\pi} \int d\mathbf{r}' \left[ \int dE' \oint d\Omega' \Sigma(\mathbf{r}', E') \Phi(\mathbf{r}', E', t - \frac{|\mathbf{r} - \mathbf{r}'|}{v}) f(\mathbf{r}', E' \rightarrow E) \right. \\ \left. + S(\mathbf{r}', E, t - \frac{|\mathbf{r} - \mathbf{r}'|}{v}) \right] \frac{\exp\left(-\int_0^{|\mathbf{r}-\mathbf{r}'|} ds' \Sigma(\mathbf{r} - s'\Omega, E)\right)}{|\mathbf{r} - \mathbf{r}'|^2}$$

# The Monte Carlo approach

The full statistical simulation retrieves information on the solution of the integral equation

The simulation is performed on the basis of elementary interaction probability laws

# The emission from fission

$$\begin{aligned} & \frac{1}{v(E)} \frac{\partial \varphi(\mathbf{r}, E, \Omega, t)}{\partial t} + \nabla \cdot \Omega \varphi(\mathbf{r}, E, \Omega, t) + \Sigma(\mathbf{r}, E) \varphi(\mathbf{r}, E, \Omega, t) \\ &= \int dE' \oint d\Omega' \Sigma_s(\mathbf{r}, E') \varphi(\mathbf{r}, E', \Omega', t) f_s(\mathbf{r}, E' \rightarrow E, \Omega' \cdot \Omega) \\ &+ \frac{\chi(\mathbf{r}, E)}{4\pi} \int dE' \Sigma_f(\mathbf{r}, E') \oint d\Omega' \varphi(\mathbf{r}, E', \Omega', t) + S(\mathbf{r}, E, \Omega, t) \end{aligned}$$

# The emission from fission: delayed neutrons

$$\begin{aligned}
 & \frac{1}{v(E)} \frac{\partial \varphi(\mathbf{r}, E, \Omega, t)}{\partial t} + \nabla \cdot \Omega \varphi(\mathbf{r}, E, \Omega, t) + \Sigma(\mathbf{r}, E) \varphi(\mathbf{r}, E, \Omega, t) \\
 &= \int dE' \oint d\Omega' \Sigma_s(\mathbf{r}, E') \varphi(\mathbf{r}, E', \Omega', t) f_s(\mathbf{r}, E' \rightarrow E, \Omega' \cdot \Omega) \\
 &+ \frac{\chi(\mathbf{r}, E)}{4\pi} (1 - \beta) \int dE' \Sigma_f(\mathbf{r}, E') \oint d\Omega' \varphi(\mathbf{r}, E', \Omega', t) \\
 &+ \sum_{i=1}^R \lambda_i G_i(\mathbf{r}, t) \frac{\chi_i(\mathbf{r}, E)}{4\pi} + S(\mathbf{r}, E, \Omega, t)
 \end{aligned}$$

# The emission from fission: delayed neutrons

Additional equations are needed for delayed precursors  
For solid fuel:

$$\frac{\partial C_i(\mathbf{r}, t)}{\partial t} = \beta_i \int dE' \nu \Sigma_f(\mathbf{r}, E') \oint d\Omega' \varphi(\mathbf{r}, E', \Omega', t) - \lambda_i C_i(\mathbf{r}, t)$$

For fluid fuel:

$$\frac{\partial C_i(\mathbf{r}, t)}{\partial t} = \beta_i \int dE' \nu \Sigma_f(\mathbf{r}, E') \oint d\Omega' \varphi(\mathbf{r}, E', \Omega', t) - \lambda_i C_i(\mathbf{r}, t) - \nabla \cdot [\mathbf{V}(\mathbf{r}, t) C_i(\mathbf{r}, t)]$$

 A boundary condition for  $C_i$  is needed !

# "Simple" transport models

Steady-state monokinetic equation in plane geometry, isotropic emissions

Integro-Differential 
$$\mu \frac{\partial \varphi(x, \mu)}{\partial x} + \Sigma \varphi(x, \mu) = \frac{\Sigma_s}{2} \int_{-1}^1 d\mu' \varphi(x, \mu') + \frac{1}{2} S(x)$$

Integral 
$$\Phi(x) = \frac{1}{2} \int dx' E_1(\Sigma |x - x'|) [\Sigma_s \Phi(x') + S(x')]$$



However "simple" ...  
it constitutes a tremendous  
physico-mathematical task ...

# The source-free steady-state problem and the eigenvalue

$$\begin{aligned} & \frac{1}{v(E)} \frac{\partial \varphi(\mathbf{r}, E, \Omega, t)}{\partial t} + \nabla \cdot \Omega \varphi(\mathbf{r}, E, \Omega, t) + \Sigma(\mathbf{r}, E) \varphi(\mathbf{r}, E, \Omega, t) \\ &= \int dE' \oint d\Omega' \Sigma(\mathbf{r}, E') \varphi(\mathbf{r}, E', \Omega', t) f(\mathbf{r}, E' \rightarrow E, \Omega' \cdot \Omega) + S(\mathbf{r}, E, \Omega, t) \end{aligned}$$

# The source-free steady-state problem and the eigenvalue

$$\begin{aligned} & \nabla \cdot \Omega \varphi(\mathbf{r}, E, \Omega) + \Sigma(\mathbf{r}, E) \varphi(\mathbf{r}, E, \Omega) \\ &= \int dE' \oint d\Omega' \Sigma_s(\mathbf{r}, E') \varphi(\mathbf{r}, E', \Omega') f_s(\mathbf{r}, E' \rightarrow E, \Omega' \cdot \Omega) \\ &+ \frac{\chi(\mathbf{r}, E)}{4\pi} \int dE' \nu \Sigma_f(\mathbf{r}, E') \oint d\Omega' \varphi(\mathbf{r}, E', \Omega') + S(\mathbf{r}, E, \Omega) \end{aligned}$$

# The source-free steady-state problem and the eigenvalue

$$\begin{aligned} & \nabla \cdot \Omega \varphi(\mathbf{r}, E, \Omega) + \Sigma(\mathbf{r}, E) \varphi(\mathbf{r}, E, \Omega) \\ &= \int dE' \oint d\Omega' \Sigma_s(\mathbf{r}, E') \varphi(\mathbf{r}, E', \Omega') f_s(\mathbf{r}, E' \rightarrow E, \Omega' \cdot \Omega) \\ &+ \frac{\chi(\mathbf{r}, E)}{4\pi} \int dE' \nu \Sigma_f(\mathbf{r}, E') \oint d\Omega' \varphi(\mathbf{r}, E', \Omega') \end{aligned}$$

# The source-free steady-state problem and the eigenvalue

$$\begin{aligned} & \nabla \cdot \Omega \varphi(\mathbf{r}, E, \Omega) + \Sigma(\mathbf{r}, E) \varphi(\mathbf{r}, E, \Omega) \\ &= \int dE' \oint d\Omega' \Sigma_s(\mathbf{r}, E') \varphi(\mathbf{r}, E', \Omega') f_s(\mathbf{r}, E' \rightarrow E, \Omega' \cdot \Omega) \\ &+ \left[ \frac{1}{k} \right] \frac{\chi(\mathbf{r}, E)}{4\pi} \int dE' \nu \Sigma_f(\mathbf{r}, E') \oint d\Omega' \varphi(\mathbf{r}, E', \Omega') \end{aligned}$$

# The source-free steady-state problem and the eigenvalue

$$\begin{aligned} & \nabla \cdot \Omega \varphi(\mathbf{r}, E, \Omega) + \Sigma(\mathbf{r}, E) \varphi(\mathbf{r}, E, \Omega) \\ &= \begin{bmatrix} 1 \\ - \\ \gamma \end{bmatrix} \left[ \int dE' \oint d\Omega' \Sigma_s(\mathbf{r}, E') \varphi(\mathbf{r}, E', \Omega') f_s(\mathbf{r}, E' \rightarrow E, \Omega' \cdot \Omega) \right. \\ & \left. + \frac{\lambda(\mathbf{r}, E)}{4\pi} \int dE' \nu \Sigma_f(\mathbf{r}, E') \oint d\Omega' \varphi(\mathbf{r}, E', \Omega') \right] \end{aligned}$$

# The source-free steady-state problem and the eigenvalue

$$\begin{aligned} & \nabla \cdot \Omega \varphi(\mathbf{r}, E, \Omega) + \left[ \Sigma(\mathbf{r}, E) - \frac{\alpha}{v} \right] \varphi(\mathbf{r}, E, \Omega) \\ &= \int dE' \oint d\Omega' \Sigma_s(\mathbf{r}, E') \varphi(\mathbf{r}, E', \Omega') f_s(\mathbf{r}, E' \rightarrow E, \Omega' \cdot \Omega) \\ &+ \frac{\chi(\mathbf{r}, E)}{4\pi} \int dE' \nu \Sigma_f(\mathbf{r}, E') \oint d\Omega' \varphi(\mathbf{r}, E', \Omega') \end{aligned}$$

# The source-free steady-state problem and the eigenvalue

$$\begin{aligned} & \nabla \cdot \Omega \varphi(\mathbf{r}, E, \Omega) \\ &= \left[ \begin{array}{c} 1 \\ \delta \end{array} \right] \left[ \int dE' \oint d\Omega' \Sigma_s(\mathbf{r}, E') \varphi(\mathbf{r}, E', \Omega') f_s(\mathbf{r}, E' \rightarrow E, \Omega' \cdot \Omega) \right. \\ & \quad \left. + \frac{\lambda(\mathbf{r}, E)}{4\pi} \int dE' \nu \Sigma_f(\mathbf{r}, E') \oint d\Omega' \varphi(\mathbf{r}, E', \Omega') - \Sigma(\mathbf{r}, E) \varphi(\mathbf{r}, E, \Omega) \right] \end{aligned}$$



# Eigenvalue: various formulations

Multiplication  $k$

Collision  $\gamma$

Time  $\alpha$

Density  $\delta$

# Eigenvalue

The time eigenvalue can be defined to include delayed neutron information ( $\omega$ -modes)

$$\begin{aligned} & \nabla \cdot \Omega \varphi(\mathbf{r}, E, \Omega) + \left[ \Sigma(\mathbf{r}, E) + \frac{\alpha}{v} \right] \varphi(\mathbf{r}, E, \Omega) \\ &= \int dE' \oint d\Omega' \Sigma_s(\mathbf{r}, E') \varphi(\mathbf{r}, E', \Omega') f_s(\mathbf{r}, E' \rightarrow E, \Omega' \cdot \Omega) \\ &+ \frac{1}{4\pi} \left[ (1 - \beta) \chi_p(\mathbf{r}, E) + \sum_{i=1}^R \frac{\beta_i}{\alpha + \lambda_i} \chi_i(\mathbf{r}, E) \right] \int dE' \nu \Sigma_f(\mathbf{r}, E') \oint d\Omega' \varphi(\mathbf{r}, E', \Omega') \end{aligned}$$

# What is a **critical** system?

A system for which a non-zero solution exists in the absence of any external source !

Hence:  $k=1$

$\alpha=0$

# What is a **subcritical** system?

A system for which fission production **cannot compensate** losses due to streaming (leakage through the boundary) and net removal through collisions; only by a source a steady-state can be established!

Hence:  $k < 1$

$\alpha < 0$

# What is a **supercritical** system?

A system for which fission production is **larger** than losses due to streaming (leakage through the boundary) and net removal through collisions; no steady-state can be established !

Hence:  $k > 1$

$\alpha > 0$

# A digression on analytical methods

## Why analytical methods?

- To grasp the mathematical nature of the problem
- To get full insight into physics
- To obtain reference solutions

# The analysis of the transport problem in the Fourier-transformed space

[Case, DeHoffmann, Placzek, *Introduction to the Theory of Neutron Diffusion*]

$$\tilde{\Phi} = \frac{\frac{1}{B} \arctan \frac{B}{\Sigma}}{1 - c\Sigma \frac{1}{B} \arctan \frac{B}{\Sigma}} \tilde{S}(B) \equiv \Gamma(B) \tilde{S}(B)$$

Frequency analysis of the problem

# The analysis of the transport problem in the Fourier-transformed space

All approximations to the transport model amount to a suitable approximation of the transport kernel

$$S_N \quad \Gamma(B) \simeq \frac{\frac{1}{2} \sum_{n=1}^N \frac{w_n}{iB\mu_n + \Sigma}}{1 - \frac{c\Sigma}{2} \sum_{n=1}^N \frac{w_n}{iB\mu_n + \Sigma}} = \frac{\sum_{n=1}^{N/2} \frac{w_n \Sigma}{B^2 \mu_n^2 + \Sigma^2}}{1 - c\Sigma \sum_{n=1}^{N/2} \frac{w_n \Sigma}{B^2 \mu_n^2 + \Sigma^2}}$$

diffusion

$$\Gamma(B) \simeq \frac{1}{\frac{\tilde{\mu}^2}{\Sigma} B^2 + \Sigma(1-c)} \left[ = \frac{1}{\frac{1}{3\Sigma} B^2 + \Sigma_a} \right]$$



# The analysis of the transport problem in the Fourier-transformed space

Space  
discretization

$$\Gamma(B) \simeq \frac{\frac{1}{\xi(B)} \arctan \frac{\xi(B)}{\Sigma}}{1 - c\Sigma \frac{1}{\xi(B)} \arctan \frac{\xi(B)}{\Sigma}}$$

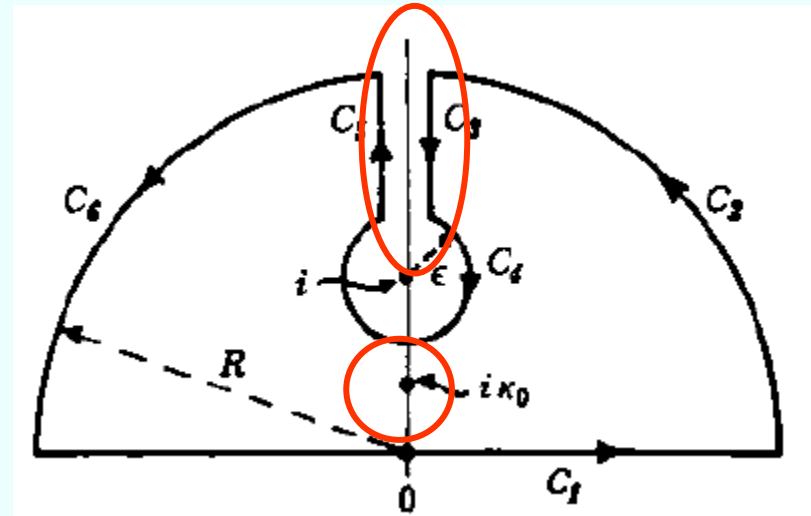
$$\xi(B) = \frac{\sin\left(B \frac{\Delta x}{2}\right)}{\frac{\Delta x}{2}}$$

# The Fourier transform can be inverted

- Fundamental work by Case-DeHoffmann-Placzek
- It is possible to obtain the exact Green function of the problem
- The Fourier transform is characterized by a polar singularity and a branch-cut (discrete and continuous spectra)
- The residue in the pole yields a diffusion-like contribution
- The integral along the branch-cut yields the "typical" transport behaviour

# Singularities

$$1 - \frac{c\Sigma}{B} \arctan \frac{B}{\Sigma} = 0$$



The poles characterize the spatial relaxation length of the asymptotic portion of the solution, the branch cut describes the “transient” behaviour

# The Fourier transform can be inverted

Fully analytical solution:

$$\begin{aligned}\Phi_{exact}(r) &= K \frac{e^{-r/L}}{r} + \frac{1}{r} \int_{\Sigma}^{+\infty} dy F(y) e^{-ry} \\ &\equiv \Phi_{diffusion}(r) + \Phi_{transport}(r) \equiv \Phi_{pole}(r) + \Phi_{branch-cut}(r) \\ &\equiv \Phi_{asymptotic}(r) + \Phi_{transient}(r)\end{aligned}$$

# Case method

[K.M. Case, P.F. Zweifel, *Linear Transport Theory*]

Method of **singular** eigenfunctions:

The solution to the transport equation is "expanded" as a sum of a term containing the discrete eigenfunctions and an integral term (!), containing the superposition of continuous eigenfunctions

# Case method

$$\Phi_{exact}(x, \mu) = A_+ \psi_0^+(\mu) e^{-x/\nu_0} + A_- \psi_0^-(\mu) e^{x/\nu_0} + \int_{-1}^1 d\nu A(\nu) \psi_\nu(\mu) e^{-x/\nu}$$

Asymptotic solution



"Transport" solution



# Solution of the transport problem for realistic configurations

The usual "engineering" procedure for too complicated deterministic physico-mathematical problems:

1. Approximate the model (physics is distorted), e.g. transport  $\rightarrow$  diffusion
2. Solve equations of approximate model by algorithms (numerically induced effects are introduced ... discretizations, truncations ... further distortions of physics)

# Solution of the transport problem for realistic configurations

The Monte Carlo method avoids physical  
distortions of 1. and 2.

however

Statistical uncertainties are introduced



# Basics of reactor calculations

Split the full problem (too complicate)  
into a succession of problems trying  
to separate specific aspects and  
treat them separately (multi-scale)  
Well-known technique in engineering

# Basics of reactor calculations: dynamics

Handle numerical stiffness

Reduce the complication of the full  
problem

# The solution of the transport equation: the direction variable

1. Spherical harmonics [B. Davison, *Transport Theory*]

Idea:

To expand angular dependence as a truncated series of spherical harmonics functions

# The solution of the transport equation: the direction variable

## 1. Spherical harmonics

Solve a space-energy integro-differential system for the expansion coefficients (angular moments)

# The solution of the transport equation: the direction variable

## 1. Spherical harmonics

### Advantages

- no angular distortion
- coupling of nearest moments only
- good mathematical and physical properties of the method
- low-order: diffusion

# The solution of the transport equation: the direction

## 1. Spherical harmonics

Example: plane geometry with  
anisotropic scattering

$$\Phi(x, \mu, t) = \sum_{n=0}^{\infty} \frac{2n+1}{2} \Phi_n(x, t) P_n(\mu)$$

$$S(x, \mu, t) = \sum_{n=0}^{\infty} \frac{2n+1}{2} S_n(x, t) P_n(\mu)$$

# The solution of the transport equation: the direction variable

## 1. Spherical harmonics

### Physical meaning of first moments

$$\Phi(x, t) = \int_{-1}^1 d\mu \Phi(x, \mu, t) = \Phi_0(x, t) \quad \text{Total flux}$$

$$J(x, t) = \int_{-1}^1 d\mu \mu \Phi(x, \mu, t) = \Phi_1(x, t) \quad \text{Total current}$$

# The solution of the transport equation: the direction variable

## 1. Spherical harmonics

Expansion of scattering cross section:

$$\oint d\Omega' \sum_{n=0}^{\infty} \frac{2n+1}{2} \Sigma_n(x) P_n(\Omega \cdot \Omega') \Phi(x, \mu', t) = \sum_{n=0}^{\infty} \frac{2n+1}{2} \Sigma_n(x) \Phi_n(x, t) P_n(\mu)$$

General equation:

$$\begin{aligned} -\frac{1}{v} \frac{\partial \Phi_n(x, t)}{\partial t} - \Sigma \Phi_n(x, t) + \Sigma_n \Phi_n(x, t) + S_n(x, t) \\ = \frac{n+1}{2n+1} \frac{\partial \Phi_{n+1}(x, t)}{\partial t} + \frac{n}{2n+1} \frac{\partial \Phi_{n-1}(x, t)}{\partial t} \end{aligned}$$



# The solution of the transport equation: the direction variable

## 1. Spherical harmonics

### Disadvantages

- complication and large number of equations in multi-D
- complicate numerical methods are needed for space discretization of first-order operators

# The solution of the transport equation: the direction variable

2. Discrete ordinates [based on method of  
**Wick** Chandrasekhar]

Idea:

To discretize the direction unit vector  
and to use a proper integration formula  
for collision terms

# The solution of the transport equation: the direction variable

## 2. Discrete ordinates

Solve a space energy system for  
direction fluxes

# The solution of the transport equation: the direction variable

## 2. Discrete ordinates

Example: plane geometry with anisotropic scattering

$$\frac{1}{v} \frac{\partial \Phi(x, \mu_i, t)}{\partial t} + \mu_i \frac{\partial \Phi(x, \mu_i, t)}{\partial \mu} - \Sigma \Phi(x, \mu_i, t) = \sum_{j=0}^N \Sigma_{ij} \Phi(x, \mu_j, t) + S(x, \mu_i, t)$$

Angular transfer cross-section:

$$\Sigma_{ij} = \sum_{n=0}^L \frac{2n+1}{2} \Sigma_n w_j P_n(\mu_i) P_n(\mu_j)$$

# The solution of the transport equation: the direction variable

## 2. Discrete ordinates

### Advantages

- simple derivation of the method
- unknowns retain physical meaning

# The solution of the transport equation: the direction variable

## 2. Discrete ordinates

### Disadvantages

- full coupling of unknowns
- balance equations are not sufficient to close the equations; need of transmission relations
- complications in multi-D
- ray effect distortions for time dependent and multi-D problems

# The solution of the transport equation: the direction variable

## 3. Collision probabilities

### Idea:

Subdivide the spatial domain into subdomains and use the integral equation to generate a system describing the integral balance through spatial coupling among subdomains

# The solution of the transport equation: the direction variable

## 2. Collision probabilities

### Advantages

- simple derivation and numerical stability
- physically meaningful
- no ray effect



# The solution of the transport equation: the direction variable

## 2. Collision probabilities

### Disadvantages

- limitation to isotropic or linearly-anisotropic scattering
- complicate calculation of spatial integrals in multi-D

# The solution of the transport equation: New challenges

Use better angular descriptions (angular finite elements, characteristics, boundary elements)

1. Remove ray effects (e.g., source-driven problems)
2. Treat complicated configurations
3. Treat high streaming systems (e.g., fusion blankets)

Hope: not to change the physico-mathematical structure of the problem ...)

# The solution of the transport equation: New challenges

Improve the representation of scattering

1. High anisotropy scattering problems  
(high energy source problems)
2. Shortcoming of Legendre representation  
of scattering function (either unphysical  
behaviour or high order expansion)
3. Radiative transfer problems

# The solution of the transport equation: tools to meet new challenges

1. Method of characteristics
2. Simplified spherical harmonics and  $A_N$
3. Second-order and angular finite elements
4. Nodal and response matrix formulation
5. Boundary element techniques
6. Domain decomposition, coupling of statistical and deterministic techniques
7. Stochastic transport