



*The Abdus Salam  
International Centre for Theoretical Physics*



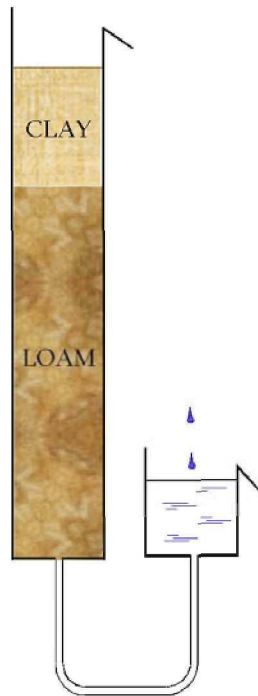
**1867-31**

**College of Soil Physics**

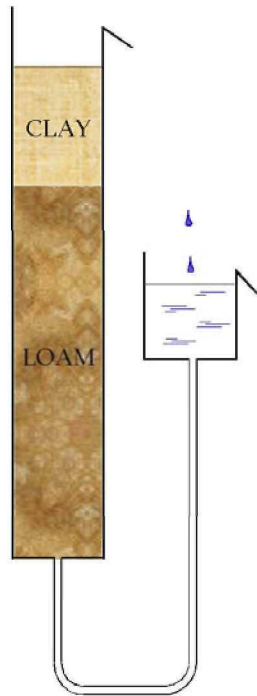
*22 October - 9 November, 2007*

**Soil water retention and water flow equations**

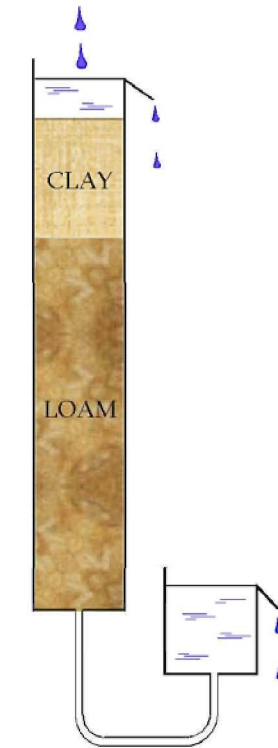
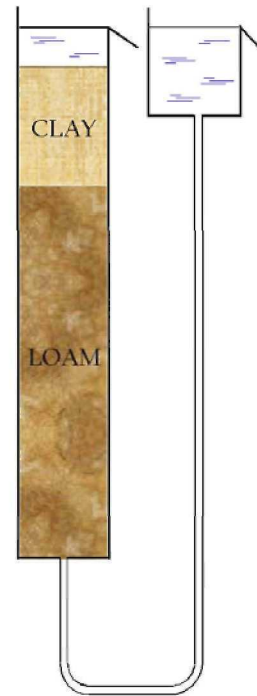
Donald Nielsen  
*University of California  
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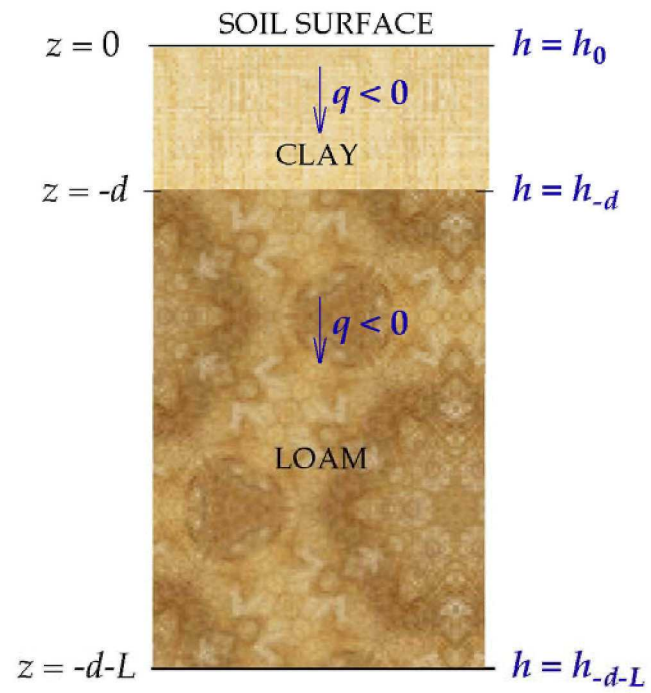
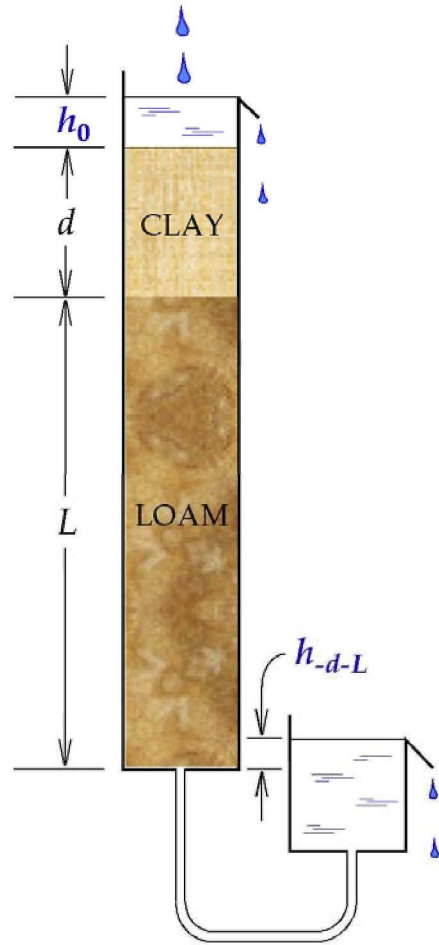
**FILLING FROM THE BOTTOM**  
Slowly Raising Water Supply



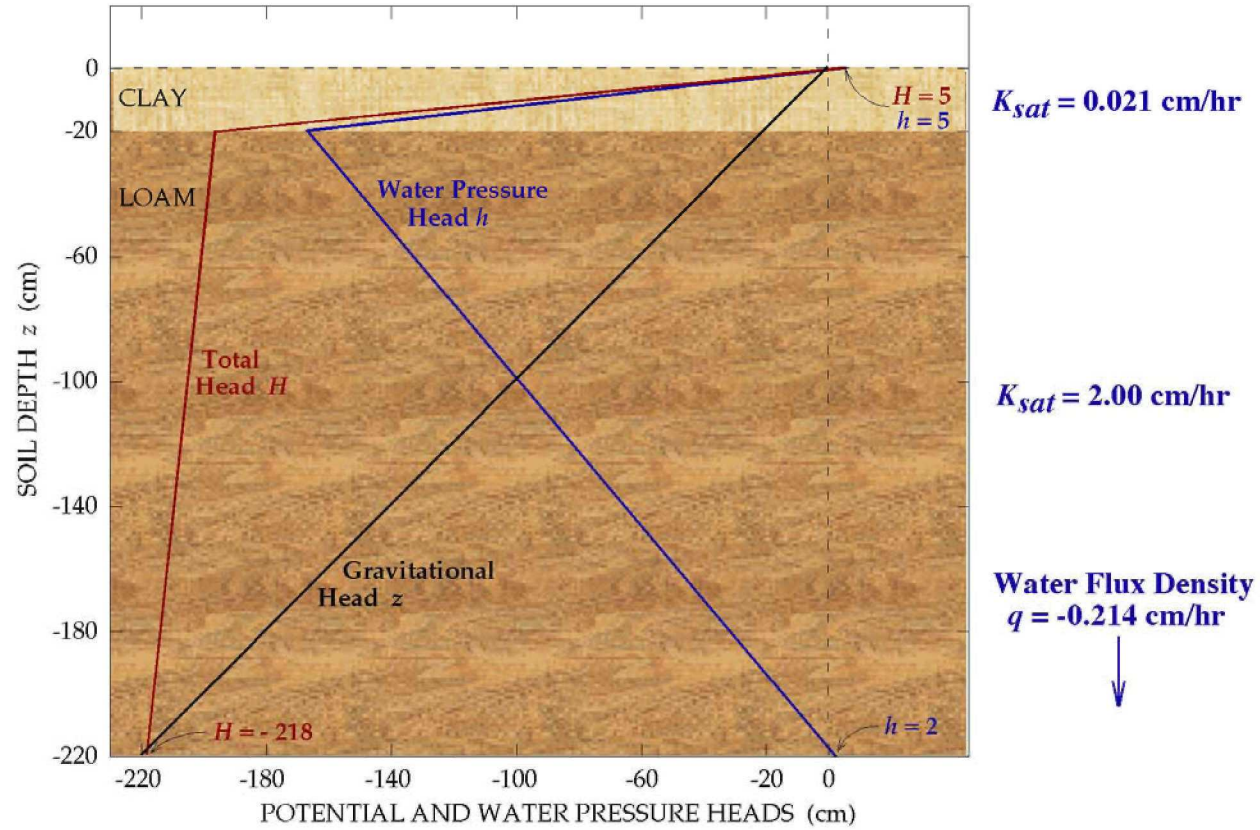
**WATER-FILLED SOIL**  
Water Not Flowing

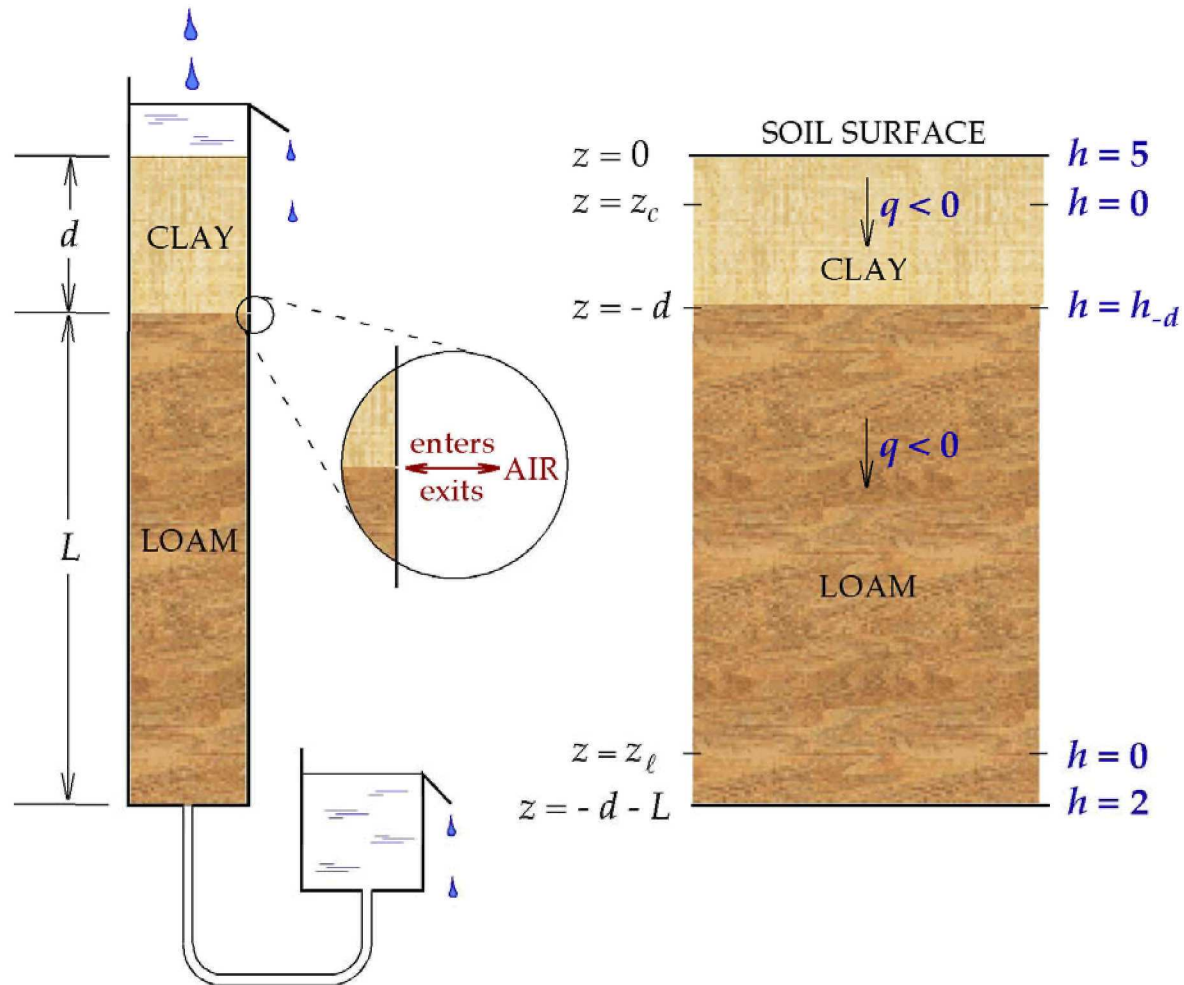


**WATER FLOWING**  
Downwards

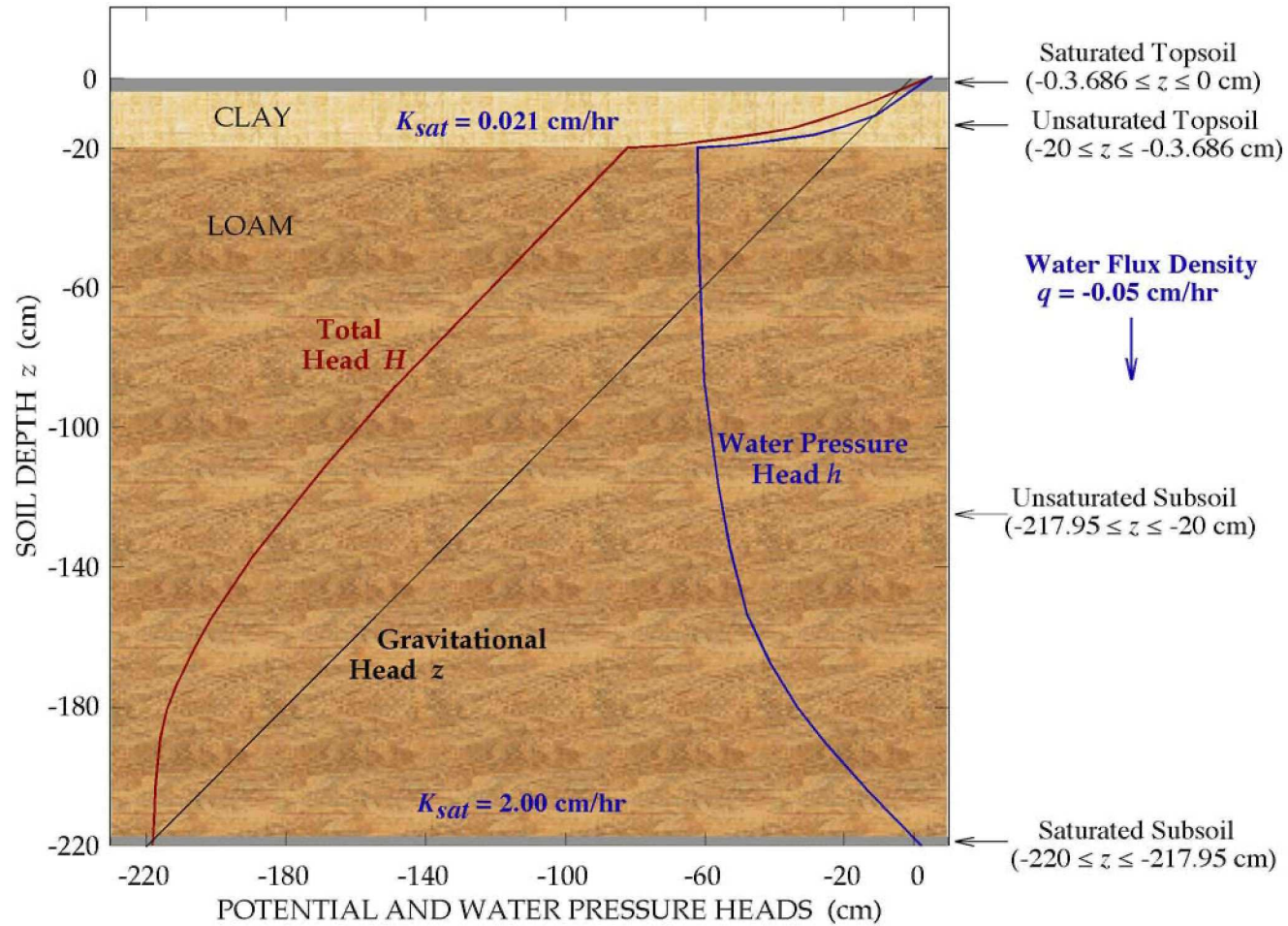


### "CLOSED" SYSTEM





# "OPEN" SYSTEM



## TWO EQUATIONS, TWO UNKNOWNNS

$$q = -K_{c_{sat}} \left( \frac{h_0 - h_{-d} + d}{d} \right) \quad \text{TOPSOIL}$$

$$q = -K_{\ell_{sat}} \left( \frac{h_{-d} - h_{-d-L} + L}{L} \right) \quad \text{SUBSOIL}$$

$$h_{-d} = \frac{d \cdot K_{\ell_{sat}} (h_{-d-L} - L) + L \cdot K_{c_{sat}} (h_0 + d)}{d \cdot K_{\ell_{sat}} + L \cdot K_{c_{sat}}}$$

## TWO UNKNOWN IN TOPSOIL

SATURATED  
TOPSOIL

$$\int_{z_c}^0 dz = - \int_0^5 \frac{dh}{q/K_{c\text{sat}} + 1}$$

$$z_c = \frac{5}{q/a_c(b_c + a_c/q)}$$


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UNSATURATED  
TOPSOIL

$$\int_{-d}^{z_c} dz = - \int_{h-d}^0 \frac{a_c dh}{q(b_c + a_c/q + h^2)}$$

$$z_c = -d + \frac{a_c}{q(b_c + a_c/q)^{1/2}} \tan^{-1} \left( \frac{h_{-d}}{(b_c + a_c/q)^{1/2}} \right)$$


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$$\frac{5 + d + db_c q / a_c}{(b_c + a_c / q)^{1/2}} = \tan^{-1} \left( \frac{h_{-d}}{(b_c + a_c / q)^{1/2}} \right)$$



## TWO UNKNOWN IN SUBSOIL

SATURATED  
SUBSOIL

$$\int_{-220}^{z_\ell} dz = - \int_2^0 \frac{dh}{(q/K_\ell + 1)}$$

$$z_\ell = -220 + \frac{2}{q/a_\ell(b_\ell + a_\ell/q)}$$


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UNSATURATED  
SUBSOIL

$$\int_{z_\ell}^{-d} dz = - \frac{a_\ell}{q} \int_0^{h-d} \frac{dh}{[(b_\ell + a_\ell/q)^{1/2}]^2 + h^2}$$

$$z_\ell = -d - \frac{a_\ell}{q} \frac{1}{2(b_\ell + a_\ell/q)^{1/2}} \ln \left( \frac{(b_\ell + a_\ell/q)^{1/2} + h-d}{(b_\ell + a_\ell/q)^{1/2} - h-d} \right)$$


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$$\frac{[(-440 + 2d)(b_\ell q/a_\ell + 1) + 4]}{(b_\ell + a_\ell/q)^{1/2}} = \ln \left( \frac{(b_\ell + a_\ell/q)^{1/2} + h-d}{(b_\ell + a_\ell/q)^{1/2} - h-d} \right)$$

## SOLVING FOR THE TWO UNKNOWN

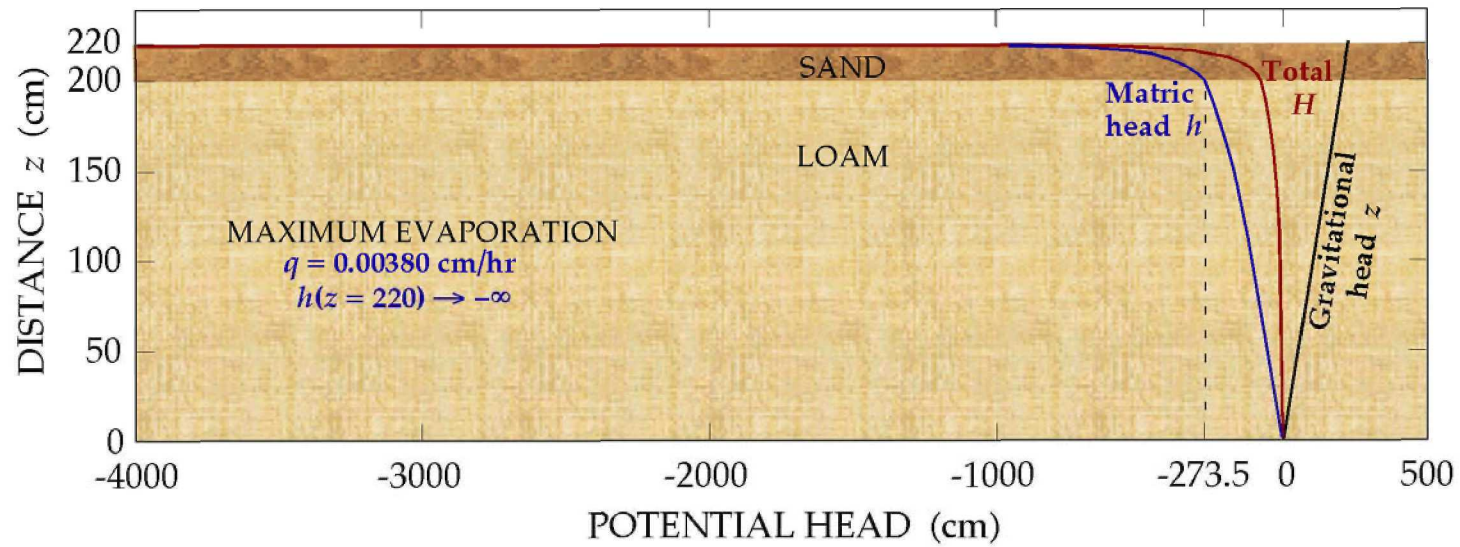
$$\text{TOPSOIL} \quad \frac{5 + d + db_c q / a_c}{(b_c + a_c / q)^{1/2}} = \tan^{-1} \left( \frac{h_{-d}}{(b_c + a_c / q)^{1/2}} \right)$$

$$\text{SUBSOIL} \quad \frac{[(-440 + 2d)(b_\ell q / a_\ell + 1) + 4]}{(-b_\ell - a_\ell / q)^{1/2}} = \ln \left( \frac{(-b_\ell - a_\ell / q)^{1/2} + h_{-d}}{(-b_\ell - a_\ell / q)^{1/2} - h_{-d}} \right)$$

$$q = -0.05 \text{ cm/hr}$$

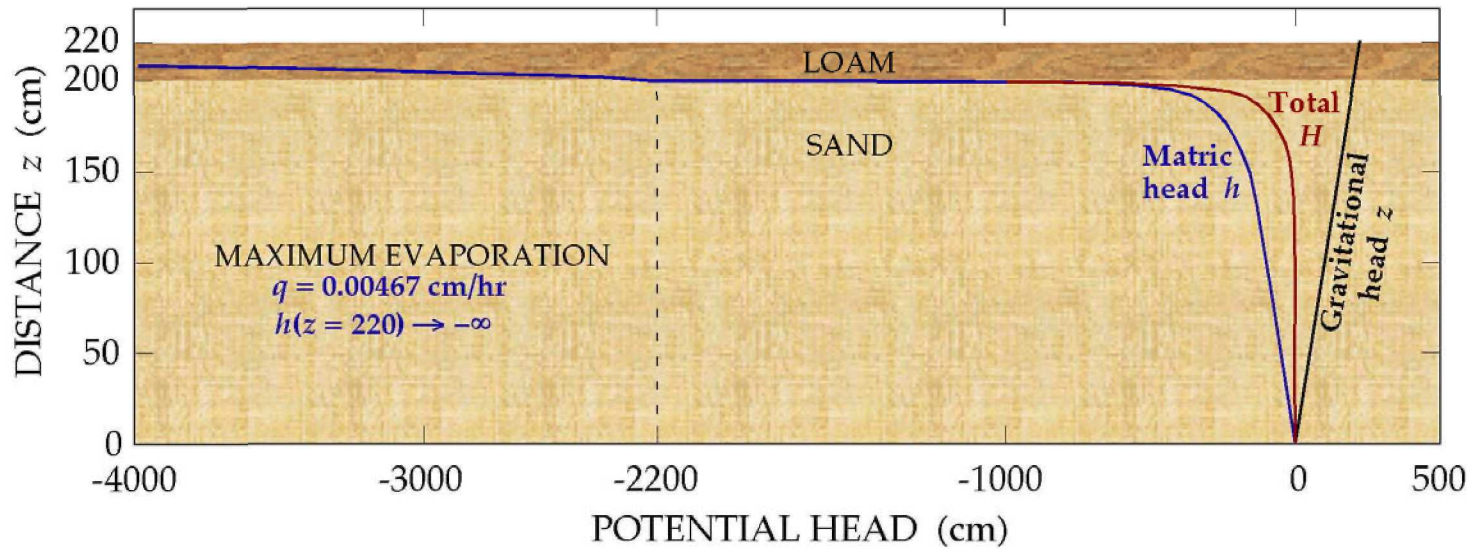
$$h_{-d} = -62.21 \text{ cm}$$

## MAXIMUM STEADY STATE EVAPORATION



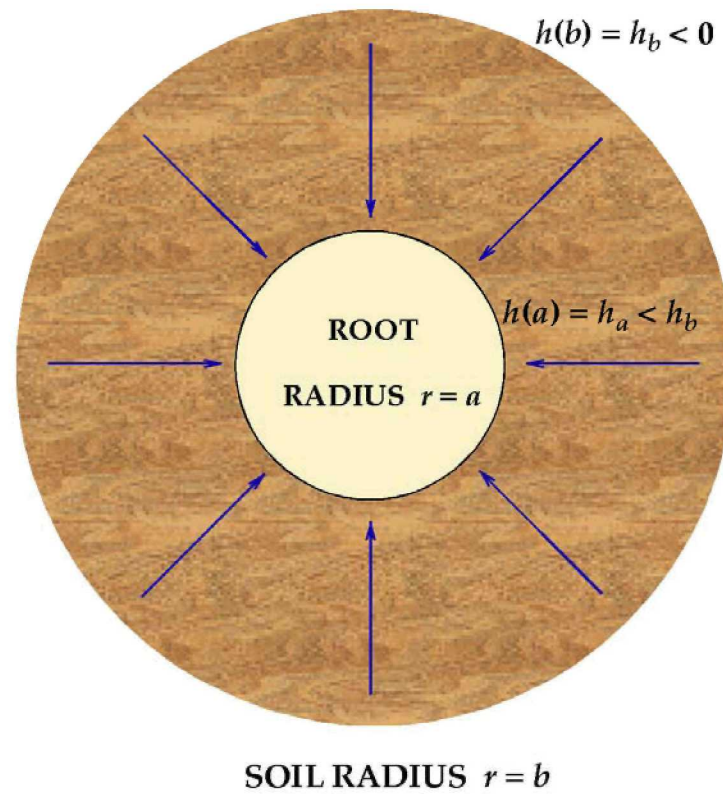
IF SOIL ENTIRELY A SAND,  $q_{max} = 0.00323$  cm/hr

## MAXIMUM STEADY STATE EVAPORATION



IF SOIL ENTIRELY A LOAM,  $q_{max} = 0.0101$  cm/hr

## SOIL WATER FLOW TO PLANT ROOTS



## SOIL WATER FLOW TO PLANT ROOTS

### RICHARDS EQUATION IN CYLINDRICAL COORDINATES

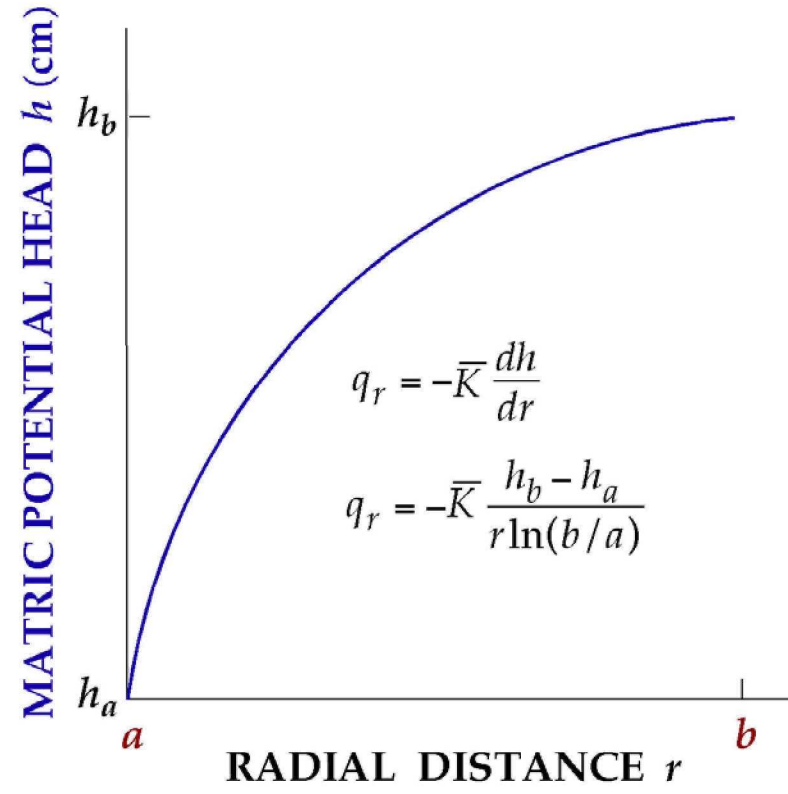
$$\frac{\partial \theta}{\partial t} = \frac{1}{r} \frac{\partial}{\partial r} \left( r K \frac{\partial H}{\partial r} \right) + \frac{1}{r} \frac{\partial}{\partial \theta} \left( K \frac{1}{r} \frac{\partial H}{\partial \theta} \right) + \frac{\partial}{\partial z} \left( K \frac{\partial H}{\partial z} \right)$$

### STEADY-STATE RADIAL FLOW ONLY

$$\frac{d}{dr} \left( r K \frac{dh}{dr} \right) = 0 \quad \bar{K} = \frac{1}{h_a - h_b} \int_{h_a}^{h_b} K(h) dh$$

$$\frac{d}{dr} \left( r \frac{dh}{dr} \right) = 0 \quad h = A \ln r + B$$

$$\frac{h - h_a}{h_b - h_a} = \frac{\ln(r/a)}{\ln(b/a)}$$



$$\frac{J_r}{(2\pi r \cdot 1)} = -\bar{K} \frac{(h_b - h_a)}{r \ln(b/a)} \quad J_r = -\frac{2\pi\bar{K}(h_b - h_a)}{\ln(b/a)}$$

## **ABSORPTION OF SOIL WATER BY PLANT ROOTS**

### **AN ABUNDANT NUMBER OF ROOTS**

Wheat: 5 to 40 (km root length)/(m<sup>2</sup> soil surface)

### **HUGE AREA FOR ABSORBING WATER**

Tens of m<sup>2</sup> of root surface area

### **WATER MOVES VERY SHORT DISTANCES IN SOIL**

Only a few mm's