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Soil salinization and sodification processes 4

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Soil Salinization and Sodification Processes

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Soil degradation and desertification , mainly by **erosion**, has affected more hilly sloping lands, but in valley bottoms where irrigation is being used for increasing productivity, **salinisation and sodification** have become a widespread form of soil degradation and desertification.

*There are evidences that **land degradation** processes leading to **desertification** by salinisation in the whole World is getting worse, because of different or mixed causes varying from one place to the other.*

**SALT AFFECTED SOILS
DEVELOPED UNDER
NON IRRIGATED
CONDITIONS**





Sahel (Senegal, Africa)







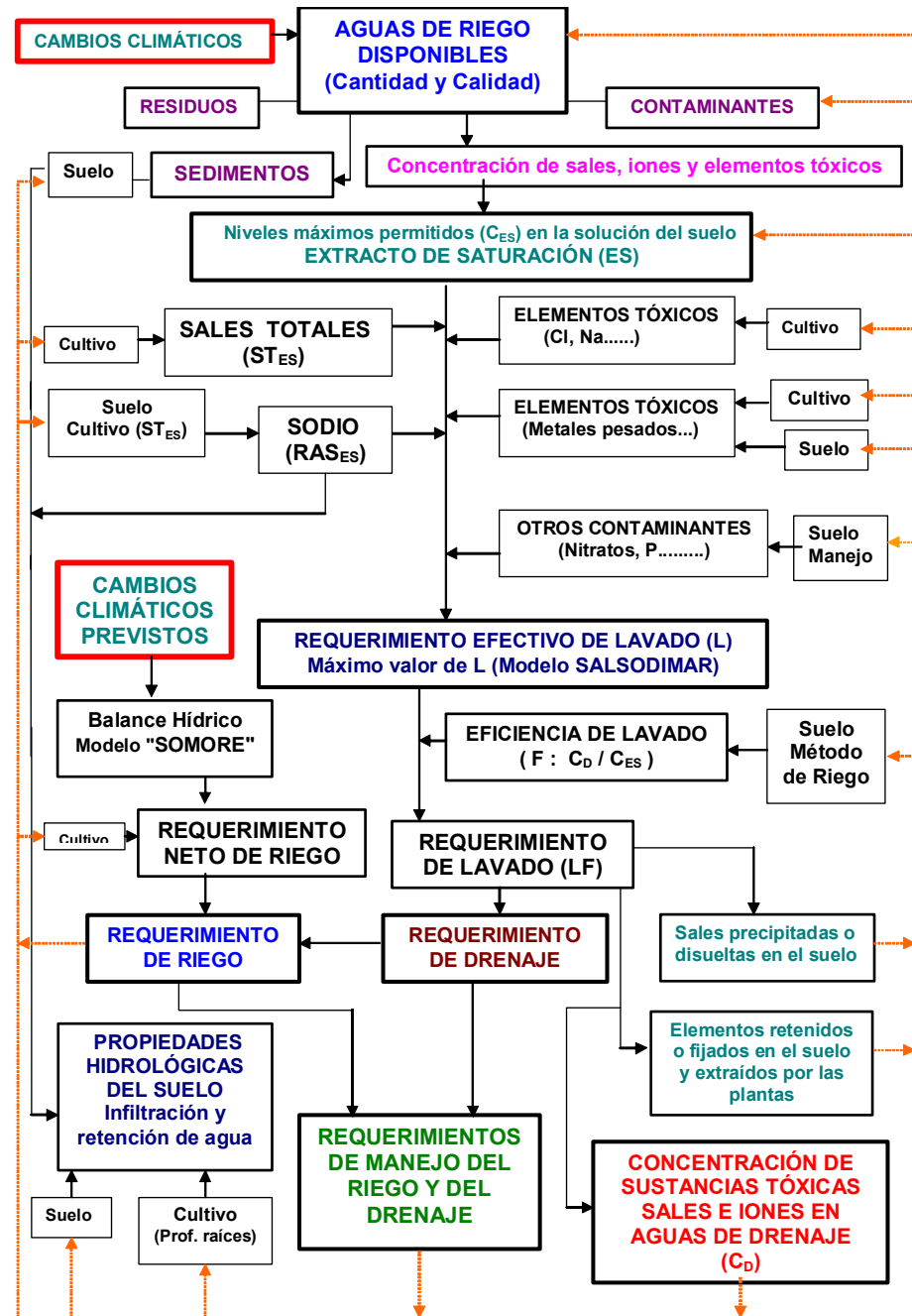


Figura 2.- Diagrama de flujo de un modelo conceptual de balance de sales y sustancias tóxicas en suelos bajo riego (RAS: Relación de Adsorción de Sodio) (Modelo SOMORE: Pla, 1997a; Modelo SALSODIMAR, Pla, 1996; 1997b). (-----> Posibles alternativas para resolver limitaciones)



Irrigation causes drastic changes in the regime and balance of water and solutes in the soil profile, which may result in soil salinisation, one of the processes of soil degradation leading to land desertification.

The salinity problems are a consequence of salt accumulation in zones and depths where the soil moisture regime is characterized by strong losses of water by evaporation and transpiration, and by reduced leaching of the remaining salts.

The salt accumulation may conduce to a partial or complete loss of soil capacity to provide the required amounts of water to plants, changing fertile lands to deserts.

The problems of secondary salinisation are a consequence of non adequate water mangement by irrigation and drainage, under a particular set of conditions, including:

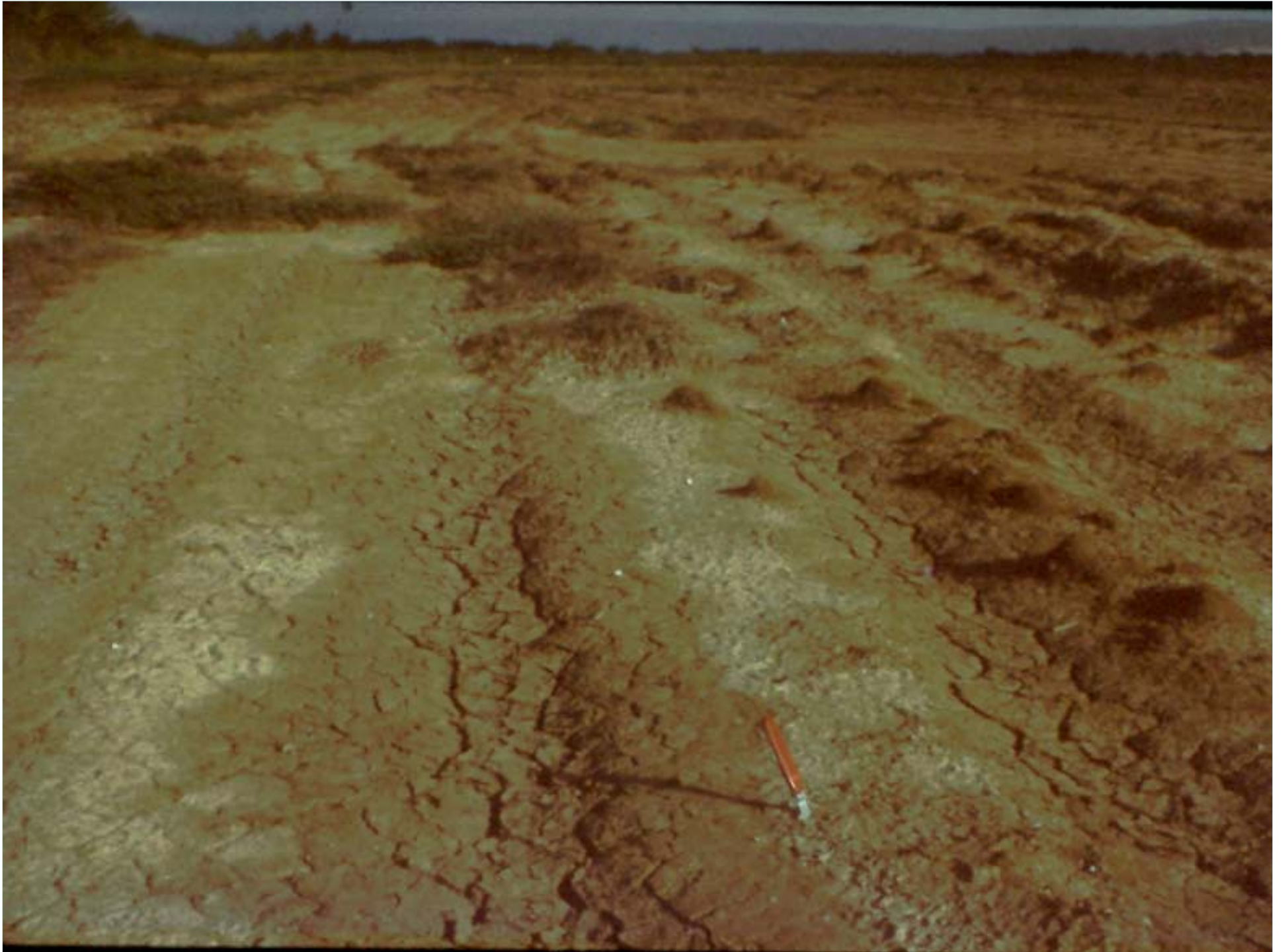
- Climate
- Crops
- Soils
- Fertilization
- Growndwater depth
- Water quality
- Irrigation system

















The salt affected soils, depending on their main effects on soils and plants, may be clasified as:

SALINE SOILS
SODIC SOILS

Tradicionalmente the **sodic soils** have been called **alcali soils**, **but** these only included the sodic soils with bicarbonates and carbonates of Na, and pH higher than 8.5-9.0, and often higher than 10.

There are other soils with properties of sodic soils with lower pH and Na levels lower than the so-called alcali soils.

Adicionally there are other specific types of salt-affected soils like the so-called **“saline-acid” soils**.

SALINE SOILS

“Saline soils” are the salt-affected soils where the content of salts and the osmotic pressure of the soil solution do not allow the absorption by the plant of a great part of the soil water, not affecting directly the soil physical properties. **The main consequence is a partial or complete reduction of the plant growth due to physiological deficit of water caused by the negative osmotic potential of the saline soil solution**

For practical purposes, **the salt concentration is expressed as the electrical conductivity (units of : ds (decisiemen)/m (meter) at 25°C) in soil saturated extract.** **One ds/m is approximately equivalent to a salt concentration in soil solution of 10 meq/l, and to an osmotic pressure of 36 kpa.**

The difficulty in plant water absorption from the soil is depending on the matric potential, which becomes more negative when the soil water content decreases, and on the osmotic potential, more negative when the salinity of the soil solution increases. The effect of both potentials is more or less additive.

















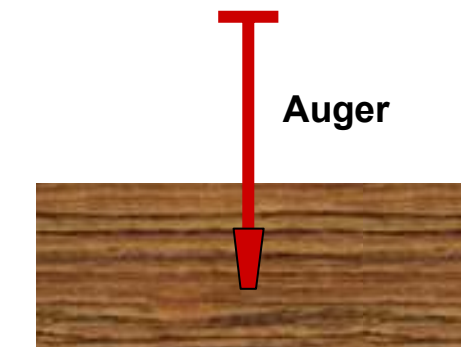




EVALUATION OF SOIL SALINITY IN THE FIELD

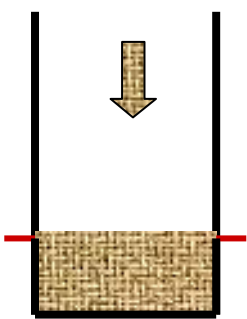


ELECTROMAGNETIC INDUCTION SENSORS

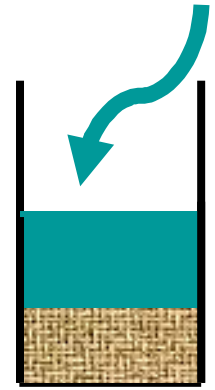


(I) Soil sampling

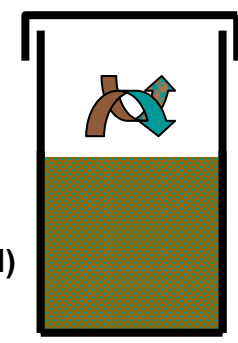
(2) Soil disaggregating and mixing. Put 100 g. of soil (aprox. by volumen) in a plastic flask



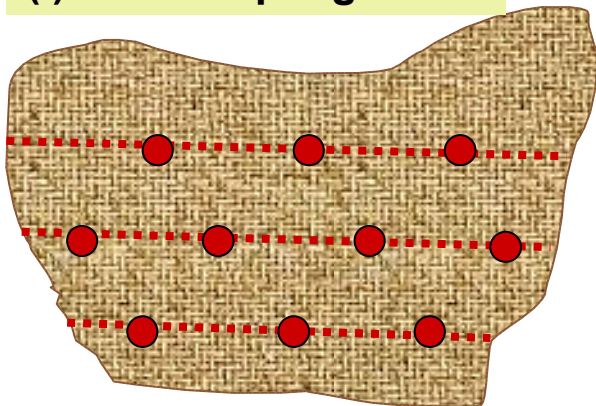
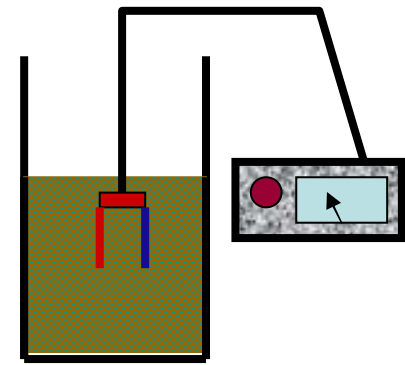
(3) Pour 100 cc. of low salinity or deionized water



(4) Close the flask and mix shaking vigorously



(5) Measure the EC of the 1:1 suspension with a portable EC meter



● Soil samples at different depths

$$EC_{SE} (dS/m) = f(d) \cdot EC_{(1:1)} (dS/m) \text{ (if there is no gypsum in the soil)}$$

$$EC_{SE} (dS/m) = f(d) \cdot (EC_{(1:1)} - 2) + 2(dS/m) \text{ (if gypsum in the soil)}$$

EC_{SE} : Electrical Conductivity in Saturation Extract

$EC_{(1:1)}$: Electrical Conductivity in suspension soil/water 1:1

$f(d)$: dilution factor (1.5; 2.0; 3.0 for sandy, loamy or clayey soils respectively)

EVALUATION OF SOIL SALINITY "IN SITU"

**SOILS WITH GYPSUM AND
CARBONATES OF Ca and Mg
of limited solubility**







RECLAMATION OF SALINE SOILS



































VALUABLE CROPS IN SALINE SOILS







SODIC SOILS

“Sodic soils” are the salt-affected soils where the accumulation of high levels of Na, sometimes accompanied of Mg, both in solution and as exchangeable cation, in relation to the levels of Ca + Mg and to the total salinity, conduces to **negative effects on the soil physical properties.**

The main consequence are drastic reductions both in the soil hydraulic conductivity and in the surface water infiltration rates.

For practical purposes, the sodification levels of the soil are generally expressed as the **“Sodium Adsorption Ratio” (RAS)** in the soil saturation extract (ES) :

$$RAS_{ES} = Na_{ES} / (Ca_{ES} + Mg_{ES})^{1/2}$$

Where:

Na, Ca y Mg are the concentrations of those elements in the soil saturation extract (ES) in **milimols/liter**.







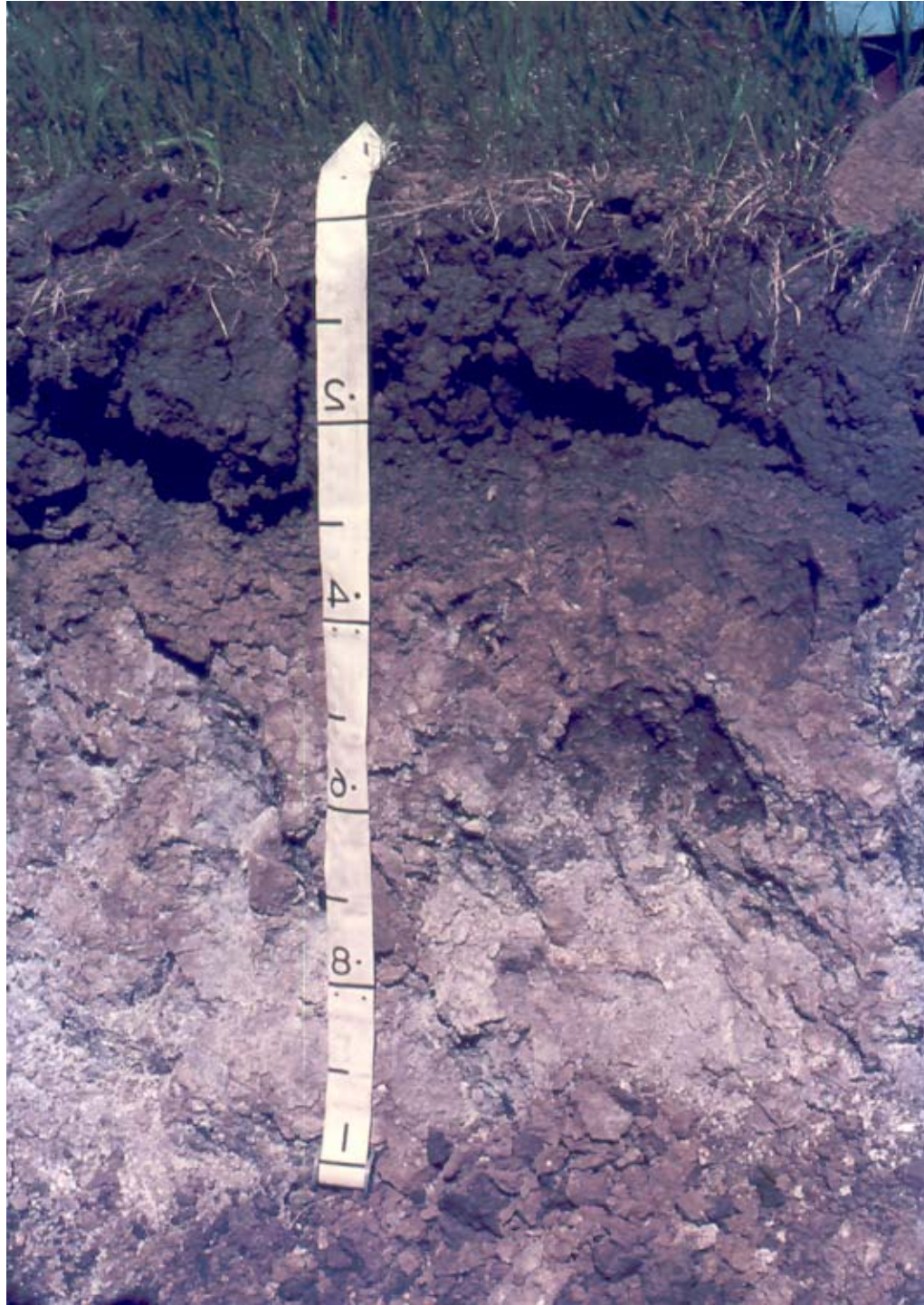








RECLAMATION OF SODIC SOILS

















**NUTRIENT DEFICIENCIES AND
TOXICITIES ASSOCIATED TO
SALINITY**



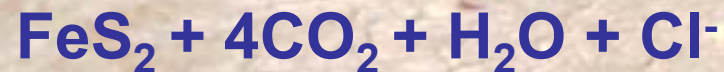




SALINE-ACID SOILS

Generally formed on clay fluvial sediments deposited on deltas (mainly in tropical regions) and submitted to periodical flooding with salty sea water, with the following steps:

Salts in solution (Cl^- y SO_4^-) + Iron reduced (Fe^{++}) + Organic Matter (4C) + Water (H_2O) > (anaerobic environment; reducing bacterias) >>>



Improvements in the drainage conditions and better aeration > Oxidation:



+ SALTS (Cl^- and SO_4^-)

SALINE-ACID SOIL























The reclamation of soils already affected by salinity cannot generally be justified by strictly economical reasons

It is more convenient to preestablish, using predictive indices and models, the best alternatives for the management of irrigation and drainage waters in order to prevent and to control salinization and sodification problems for each combination of climate, soil and available irrigation water

This is even more necessary when :

- . there is a high competence for the use of the available high quality water**
- . the quality of the available water is poor**
- . it is required to reduce the volume of effluents of salinized or contaminated drainage water**

Irrigation increases yields 100-400 %

World: 250 x 10⁶ ha irrigated lands. 10% degraded by salinisation. 0,5 x 10⁶ ha salinised yearly

World: 97,5% salt water; 2,5% fresh water

Cost of desalinisation (38 g/l > 0,5 g/l): 0,46 € /m³ (2,1 in 1970)

Freshwater withdrawn: Agriculture Domestic Industries

World	69%	10%	21%
W Europe	34%	15%	51%

(50% consumed by evapotranspiration in Agriculture)

(95% waste water in Industries)

(90% waste water in domestic use)

The quality of irrigation water is a relative term, and it is defined as the water characteristics determining its possibilities of being used for some specific purposes

In irrigation waters, the characteristics generally considered are the presence and content of:

- CHEMICAL contaminants: Salts, certain ions and other contaminants in solution**
- PHYSICAL contaminants: Sediments and temperature**
- BIOLOGICAL contaminants: Pathogens**

The qualification of irrigation waters would be determined by their potential to cause problems, more or less reversible, leading to:

- Diminishing yields and quality of crops and their products**
- Problems of contamination of crops, soils, groundwaters, and effluents**
- Requirements of special practices, equipments and structures for the management of irrigation and drainage water, of soils and of crops**

The qualification of waters in relation to potential problems of soil salinization and sodification is mainly based in the absolute and relative content of salts and certain ions

(HCO_3^- , Cl^- , $\text{SO}_4^{=}$, NO_3^- , Ca^{++} , Mg^{++} , Na^+ , K^+).

These contents are interpreted in relation to potential problems of **salinity** (limitations in the use of the soil water by plants), and of **sodicity** (deterioration of the soil physical properties) in relation to particular conditions of:

Soils

Climate

Crops

Limited available irrigation water

Difficulties in the management of irrigation and drainage

In the last decades there have been developed several systems for qualifying irrigation waters in relation to potential problems of **salinization and sodification**, including:

General schemes for average conditions, which cannot be applied to solve practical problems due to their qualitative nature and inability to be adjusted to specific situations

Empirical indices developed for very specific conditions of soils and crops in a specific area, which cannot be used or adapted to different conditions.

Among the general schemes the most known is the one proposed by the USSL-USDA (1954), which was developed for the predominant conditions in the SW of USA.

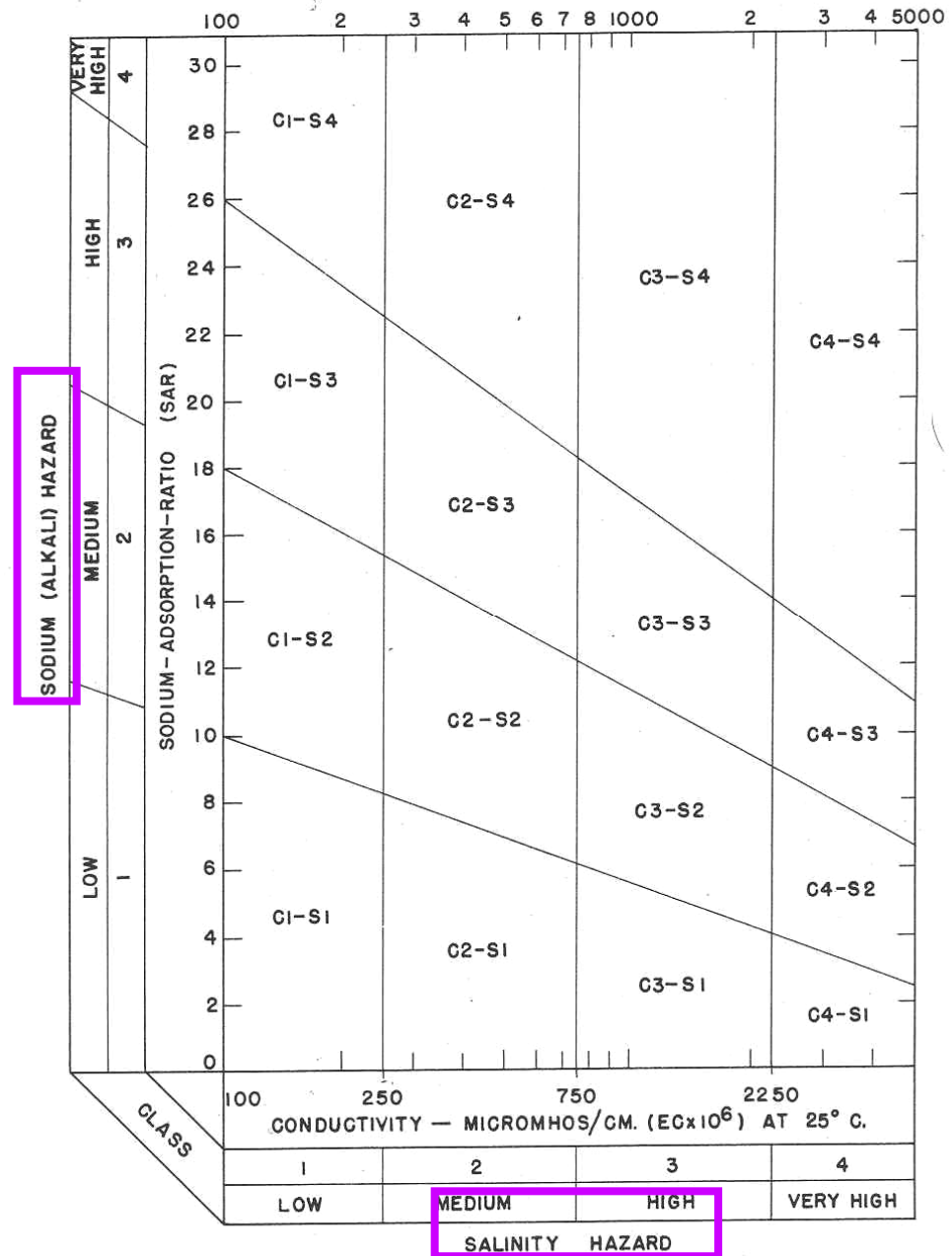
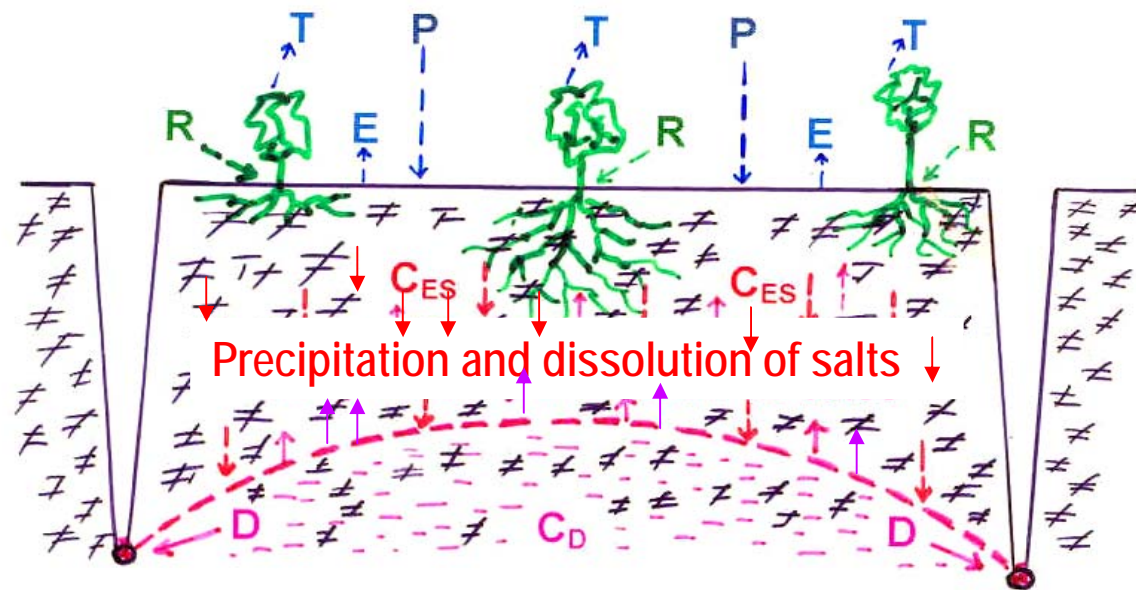


FIGURE 25.—Diagram for the classification of irrigation waters

The accumulation of salts in the soil occurs when the input of them with the irrigation water, required to replace the water losses by evaporation and transpiration, exceeds the losses by precipitation, leaching and internal drainage

Besides, the salt concentration in the soil solution increases in between of those additions by irrigation water, when the soil moisture decreases due to the temporal losses of water by evaporation and transpiration



The levels and composition of salts in the soil will be determined by the:

Composition of salts in the applied irrigation water

Possibilities of the different salts to reach determinate concentrations before they precipitate in the soil

Additionally, the composition of cations in the soil exchange phase is determined by the composition and relative concentration of the different cations in soil solution

Solid Phase

CaCO_3 , $\text{CaSO}_4 \cdot 2\text{H}_2\text{O}$, Na_2SO_4 , NaCl , KCl ,
 Na_2CO_3 , $\text{MgSO}_4 \cdot 7\text{H}_2\text{O}$, $\text{MgCl}_2 \cdot 6\text{H}_2\text{O}$,
 $\text{Na}_2\text{SO}_4 \cdot 10\text{H}_2\text{O}$, $\text{Na}_2\text{Mg}(\text{SO}_4)_2 \cdot 5\text{H}_2\text{O}$,
 $\text{CaMg}(\text{CO}_3)_2$, CaSO_4 , NaHCO_3

Mineral
Solubility



Solution Phase

Na^+ , Ca^{2+} , Mg^{2+} , K^+ ,
 Cl^- , SO_4^{2-} , HCO_3^- ,
 CO_3^{2-} , NO_3^- , H^+ , OH^-

Ion association

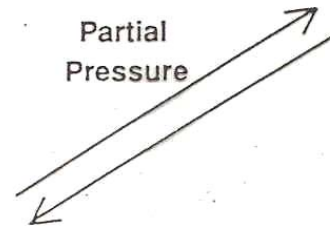


CaSO_4^0 , MgSO_4^0 , NaSO_4^- , KSO_4^-
 CaHCO_3^+ , CaCO_3^0 , MgHCO_3^+
 NaCO_3^- , KCO_3^- , NaHCO_3^0 , KHCO_3^0

Gas Phase

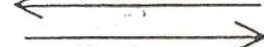
CO_2 , N_2 , N_2O , O_2

Partial
Pressure



Cation

Exchange

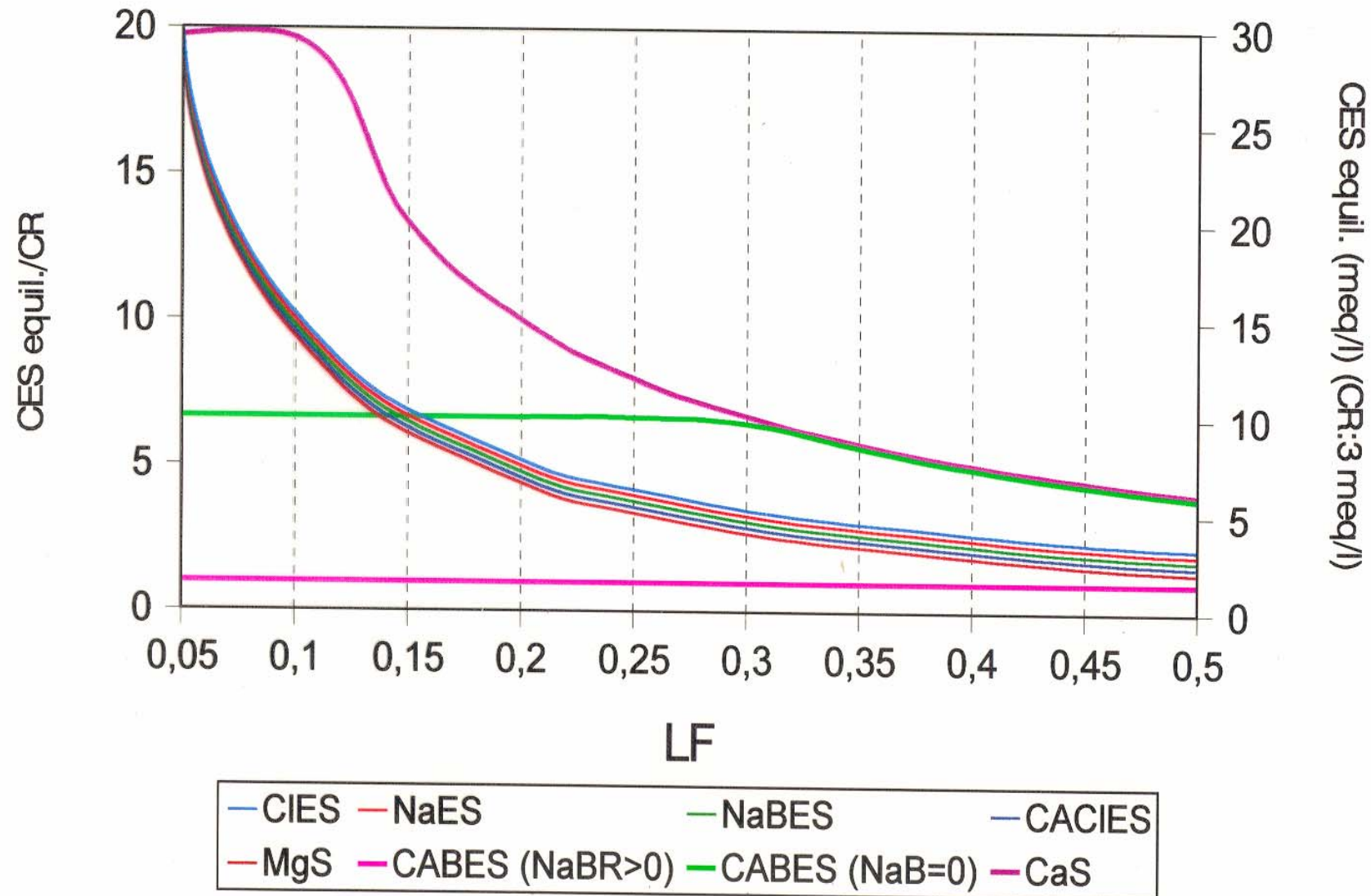


Na^+
 Ca^{2+}
 Mg^{2+}
 K^+

Exchange Phase

Equilibrium concentrations (CES equil.) of salts and ions in the soil solution vs effective leaching fraction (LF)

CES/CR: CIES, NaES, NaBES, CaCIES, MgS, CABES (NaB>0); CES (CR=3meq/l): CABES (NaB=0), CaS



In the soil salinisation process, the changes that may happen in the composition of the soil solution derived of the precipitation of some salts of limited solubility, like bicarbonates (carbonates) of Ca and Mg, and Ca sulfates, are very important.

Conditions leading to such precipitation, like:

Predominion of bicarbonates among the anions in the irrigation water, specially with the relation:

$$(\text{HCO}_3^- / (\text{Ca}^{++} + \text{Mg}^{++})) > 1$$

Losses of CO₂

Defficient drainage

would contribute to a relative enrichment of Na in the soil solution and at the same time in the exchange complex, and to a decrease in total salinity in the soil solution.

Conditions**IRRIGATION WATER**

Concentration:	(High)	(Medium)	(Low)	
EC:	>2 dS/m	1-2 dS/m	< 1 dS/m	
Composition:	Cl>S>B Na>=CA	S>=Cl>B CA>Na	B>=S>Cl CA>=Na	B>S>Cl (B>CA) Na>=CA
DRAINAGE	(Variable)	(Very restricted)	(Restricted)	
Soil Perm.(I):	1-50 mm/hour	< 1 mm/hour	< 5 mm/hour	
Groundwat.depth:#	< 1.5 m	< 0.5 m	< 1.0 m	
CLIMATE	(Ar.-DSAr.)	(Ar.-DSAr.)	(DSAr.-SH.)	(Ar.-HSAr.)
IMA (P/ETP):	< 0.5	< 0.5	0.5-1.0	< 0.8
LGP (P>(ETP/2)):	< 120 days	< 120 days	120-270 days	< 180 days

Resulting problem**SOIL SOLUTION**

Concentration (EC):	(Very saline)	(Mod. saline)	(Sligh. saline)	(Var. salin.)
Composition:	>8 dS/m	>4 dS/m	<4 dS/m	>2 dS/m
	Cl>>S>>B Na>CA	Cl>=S>>B Na>=CA	S>Cl>B Na>CA	(*S>=B>Cl Na>>CA
	(A)	(B)	(C)	(D)
	(E)			
pH	< 8.5	< 8.5	> 7.5	> 8.5
PRECIPIT. SALTS:	CAC + CaS	CAC + CaS	CAC	CAC
POTENTIAL KIND OF PROBLEM:	"SALINITY"			"SODICITY"

(*) Change of composition under anaerobic conditions ($2\text{Na}^+ + \text{SO}_4^{2-} + 2\text{C} + 2\text{H}_2\text{O} = \text{S}^{2-} + 2\text{NaHCO}_3$)







The plants do not take salts in the same proportion as they absorb soil water, and the losses of water by evaporation and transpiration leave the salts in solution behind.

Therefore, it is not possible to control salinity in irrigated soils without an adequate leaching of the salts and drainage of the leaching water, which requires a net flux of water below the soil root zone

This can be achieved applying an excess of irrigation water above the plant water requirements

When the original soil, before being irrigated, contains an excessive amount of salts in soil solution, there would also be necessary to apply an excess of water for leaching them.

In any case, the amount of excess water to apply will depend on the content and kind of salts present in the irrigation water, on the original content of salts in the soil solution, on the climate, and on the crops.

The excess of water required to leach salts from the soil, to reclaim or to prevent salinization, may cause other environmental problems derived of the disposal and further use of that water.

The problem is agravated because those leachates may contain not only natural salts, but also

-residues of fertilizers and pesticides - which are generally used in large amounts in intensive irrigated agriculture, and

-other polutants contained or derived from animal wastes and composted materials used as amendements, and from

-partially or non treated urban and industrial effluents used for irrigation





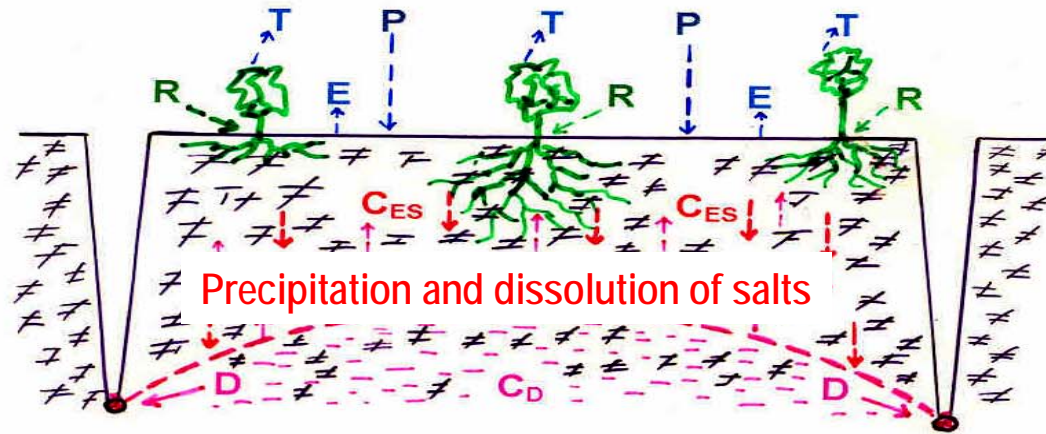












$$H_R = (H_{ET} - H_P) + H_D \quad H_R C_R = H_D C_D \quad (C_{ET} = 0; C_P \approx 0)$$

$$H_D/H_R = C_R/C_D = L \quad C_D/C_{ES} = F (\leq 1)$$

$$C_D = C_{ES} \times F \quad C_R/(C_{ES} \times F) = L$$

$$LF = C_R/C_{ES}$$

Potential precipitation of salts: $\text{CaCO}_3, \text{MgCO}_3, \text{CaSO}_4$

Potential dissolution of salts :

If there is precipitation of **Ca and Mg carbonates** and of **Ca sulfates** :

$$LF_{ST} = (Na + Mg + CaCl)/(ST_{ES} - 40)$$

$$LF_{Na} = \frac{[(RAS_{ES}^2 \times (Mg + CaCl)^2) + (320 Na^2)]}{80 RAS_{ES}} - \frac{(Mg + CaCl)}{80}$$

$$(Ca + Mg) C_p = B - 10 LF$$

$$CaS_p = CaS - 30 LF$$

The fraction of irrigation water applied in excess of the crop water requirements, and that infiltrates and finally is lost as drainage water after percolation through the soil rooting zone, is called leaching fraction (**L**)

L: Leaching fraction

$$L = HD / HR = CR / CD$$

HD: Drainage water in depth

HR: Irrigation water in depth

CR: Salt concentration in the irrigation water

CD: Salt concentration in the drainage water

The calculation of **L** has been changing through the years (Pla, 1968: 1983: 1988: 1996, 1997) (Rhoades, 1968, 1984), (Pla & Dappo, 1977), (FAO, 1976, 1986), and its use has been extended to the control of soil sodicity. **L**, integrating in a unique figure the present and required balances of water, salts and sodium in the soil, may be used as a basis for the **predictive indices and models for salinity and sodicity** in irrigated soils.

Calculation of the leaching requirements and of the concentration and composition of salts in the resulting soil solution (Pla, 1997)

$$C_D / C_{ES} = F (\leq 1)$$

$$LF = C_R / C_{ES}$$

C_D : Salt concentration in drainage water

C_{ES} : Salt concentration in saturation extract

F: Leaching efficiency

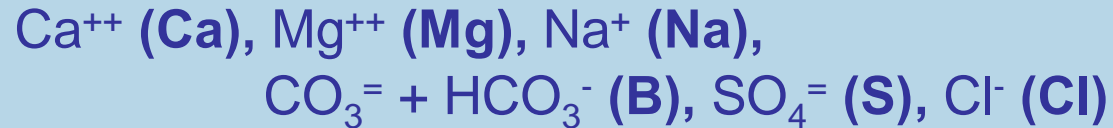
C_R : Salt concentration in irrigation water

LF: Leaching requirement

L : Effective leaching requirement

Required information

- **Cations and anions more common in irrigation waters (meq /liter) :**



- **Salts in irrigation water:**

$$\text{NaB} = \text{B} - \text{Ca} - \text{Mg} \quad \text{si } \text{NaB} \geq 0;$$
$$\text{MgB} = \text{B} - \text{Ca} - \text{NaB} \quad \text{si } \text{MgB} \geq 0;$$

$$\text{CaCl} = \text{Ca} - \text{B} - \text{S} \quad \text{si } \text{CaCl} \geq 0;$$
$$\text{CaS} = \text{Ca} - \text{B} - \text{CaCl} \quad \text{si } \text{CaS} \geq 0$$

- **Critical levels of total salts (STES), chlorides (CIES), sodium (NaES) and other toxic elements in the soil saturation extract (ES) for different crops.**

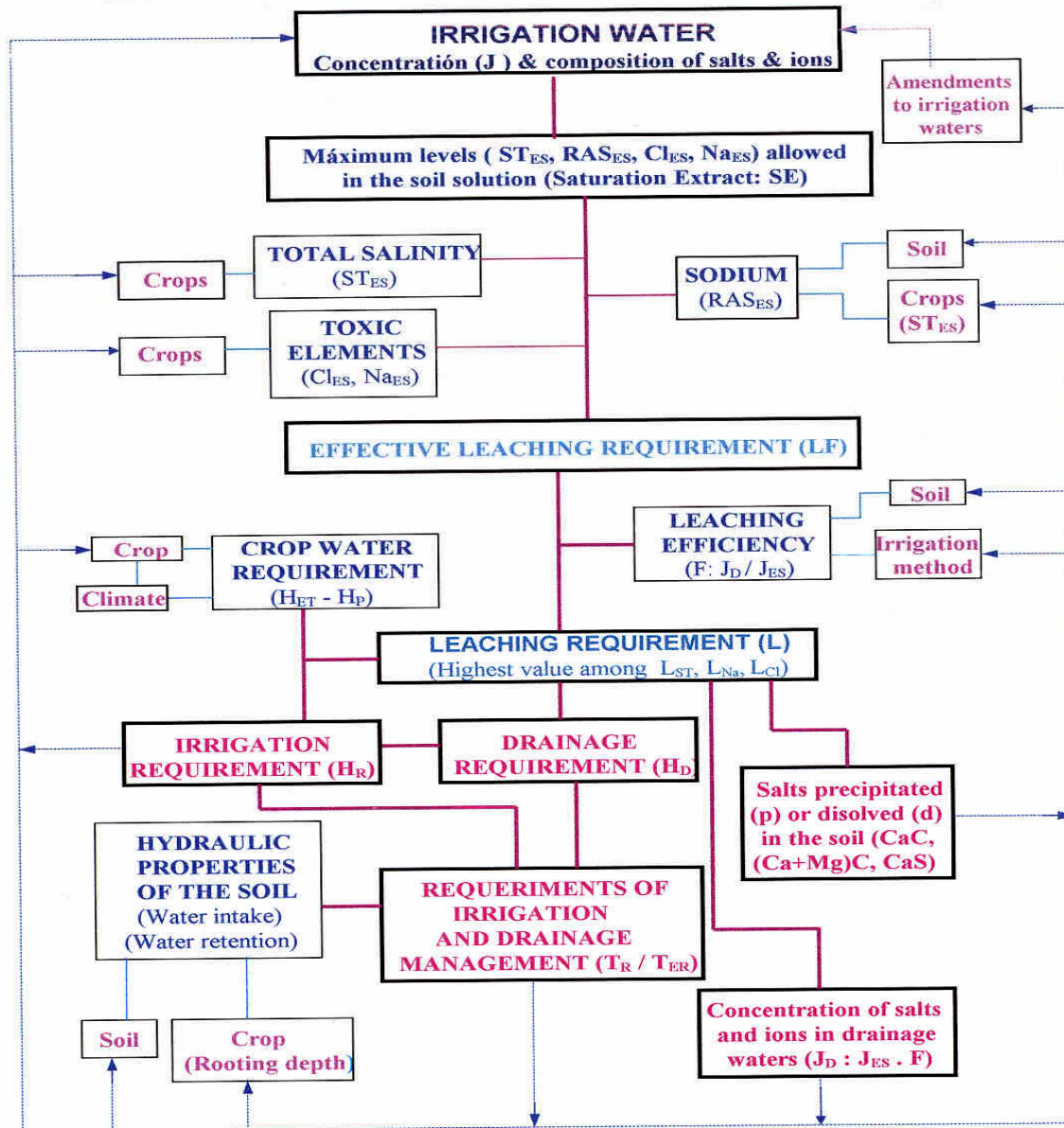
When the calculations show the possibility of precipitation of Ca carbonates and sulfates in the soil, the critical levels of STES may be increased by 20 meq/l.

Next figure shows the flow diagram which was the basis for the development of the model SALSODIMAR (Pla, 1996), which integrates the influence of climate, crops, soils, groundwater depth and composition, irrigation water quality, and irrigation and drainage management on the desertification by salinization, sodification and contamination of soils and groundwater.

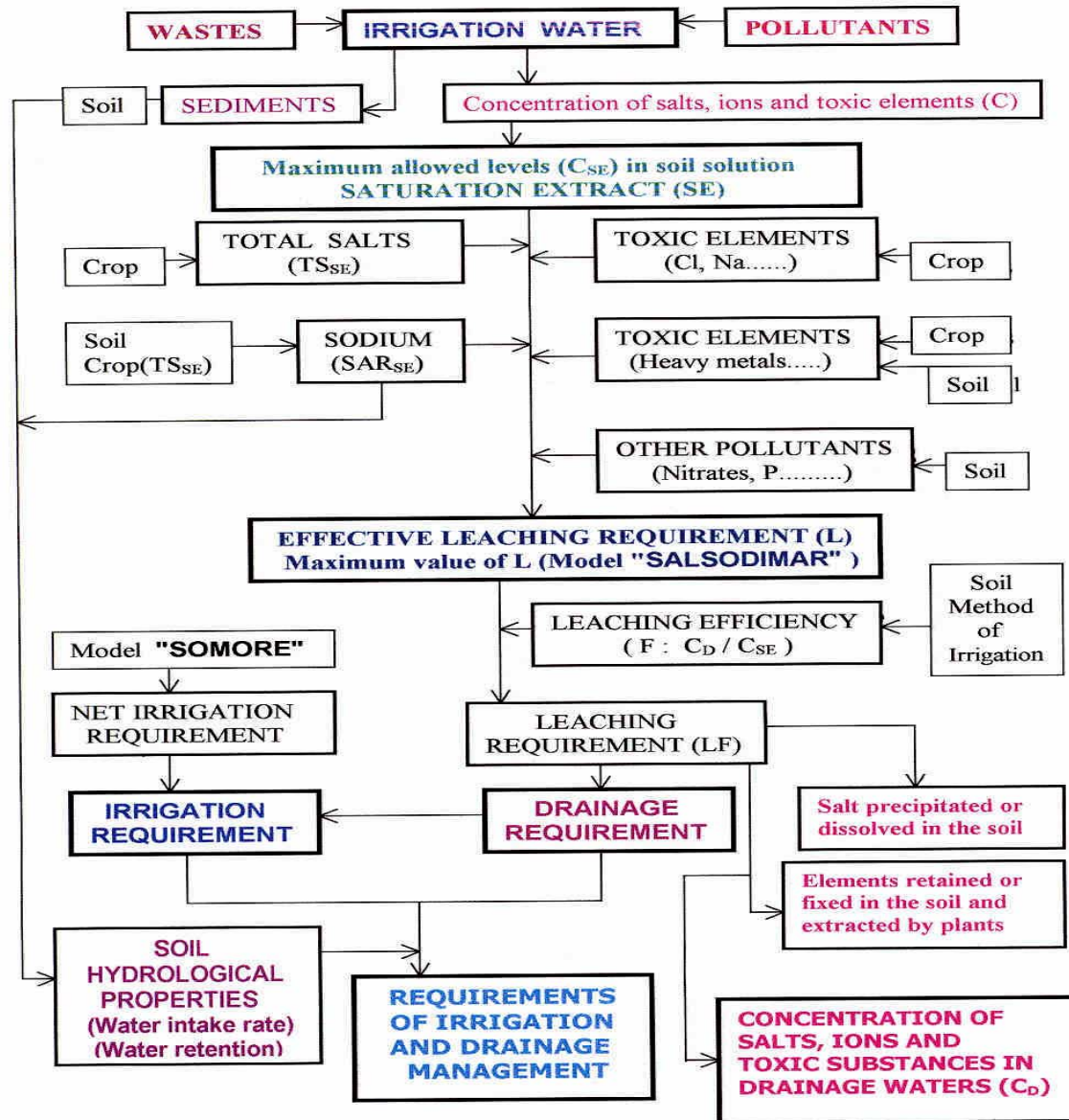
It may be useful, among other things, to preview the best alternatives for the use and management of the available soils and waters, preventing the process of desertification by secondary salinization.

It has proved to be reasonably good to predict salinization problems and to deduce the best alternative practices for irrigation and drainage to prevent salinization and sodification and other related environmental problems leading to desertification

FLOW DIAGRAM OF THE SIMULATION MODEL "SALSODIMAR"



→ Potential alternatives (crops, waters, soils ...) for limitations in irrigation, drainage, salts ..



Scheme 2. Flow diagram of a conceptual model of a balance of salts and toxic substances in irrigated soils (SAR: Sodium Adsorption Ratio) (Model "SOMORE": Pla, 1997a; Model "SALSODIMAR": Pla, 1997b)

Tolerance of different crops to total salinity (and to chlorides) in the soil saturation extract (STES and CIES)

TOLERANT CROPS

(ST_{ES} : 80-160 meq/l)

<i>Guayule</i>	<i>Cártamo</i>
<i>Cebada</i>	<i>Sorgo</i>
<i>Algodón</i>	<i>Dátil</i>
<i>Remolacha azucarera</i>	<i>Olivo</i>
<i>Pasto Bermuda</i>	<i>Higuera</i>
<i>Trigo</i>	

MODERATELY TOLERANT CROPS

(ST_{ES} : 40-80

meq/l)

<i>Soja</i>	<i>Alfalfa</i>
<i>Tomate</i>	<i>Caña de azúcar</i>
<i>Espinaca</i>	<i>Maíz</i>
<i>Girasol</i>	<i>Arroz</i>
<i>Pepino</i>	<i>Patata</i>
<i>Melón</i>	<i>Viña</i>

MODERATELY SENSIBLE CROPS

(ST_{ES} : 20-40

meq/l)

<i>Cebolla</i>	<i>Col</i>
<i>Pimiento</i>	<i>Cacahuete</i>
<i>Lechuga</i>	<i>Zanahoria (Cl < 10 meq/l)</i>

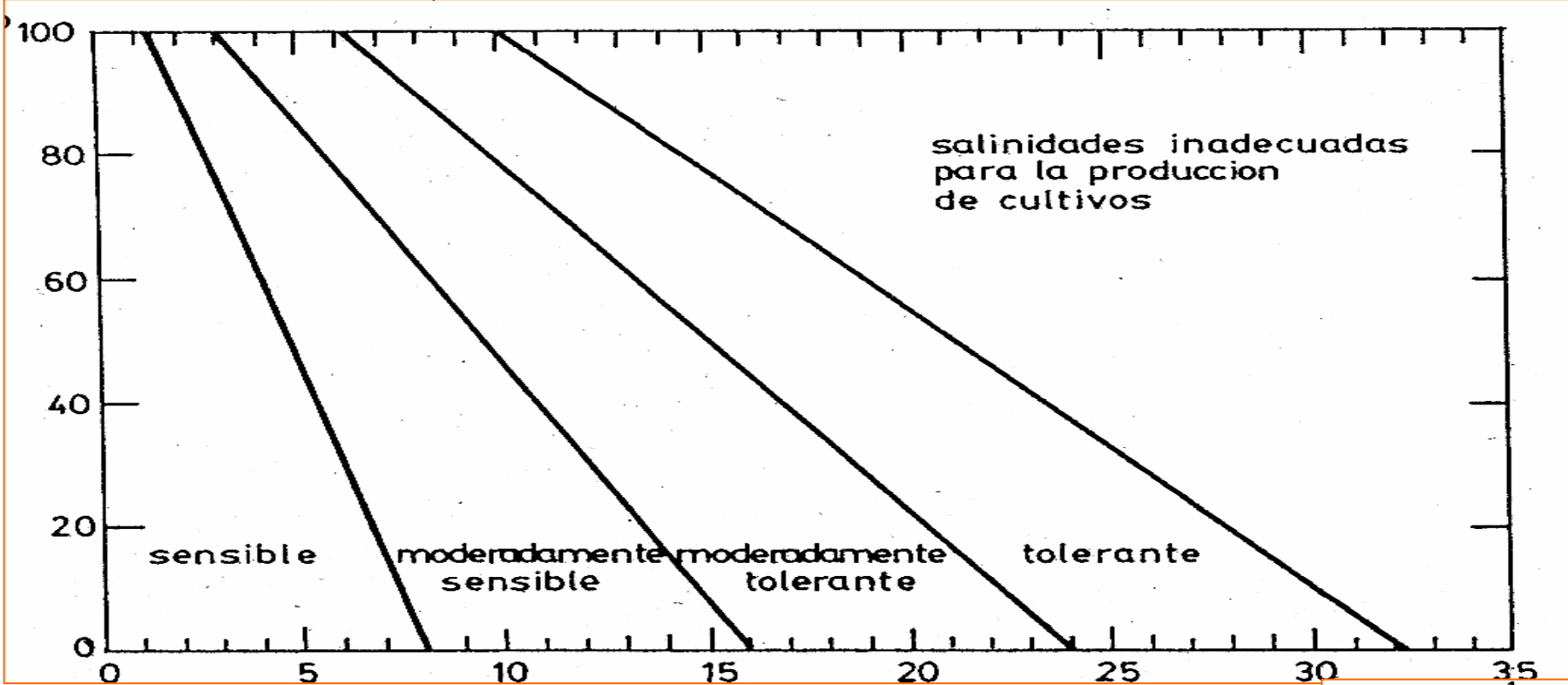
SENSIBLE CROPS

máx. ST_{es} : < 20 meq/l)

<i>Ciruelo</i>	<i>Peral</i>
<i>Limonero</i>	<i>Aguacate (Cl < 12 meq/l)</i>
<i>Naranja (Cl < 20 meq/l)</i>	<i>Melocotonero</i>
<i>Judía (Cl < 10 meq/l)</i>	<i>Berenjena</i>
<i>Manzano</i>	<i>Fresal (Cl < 10 meq/l)</i>

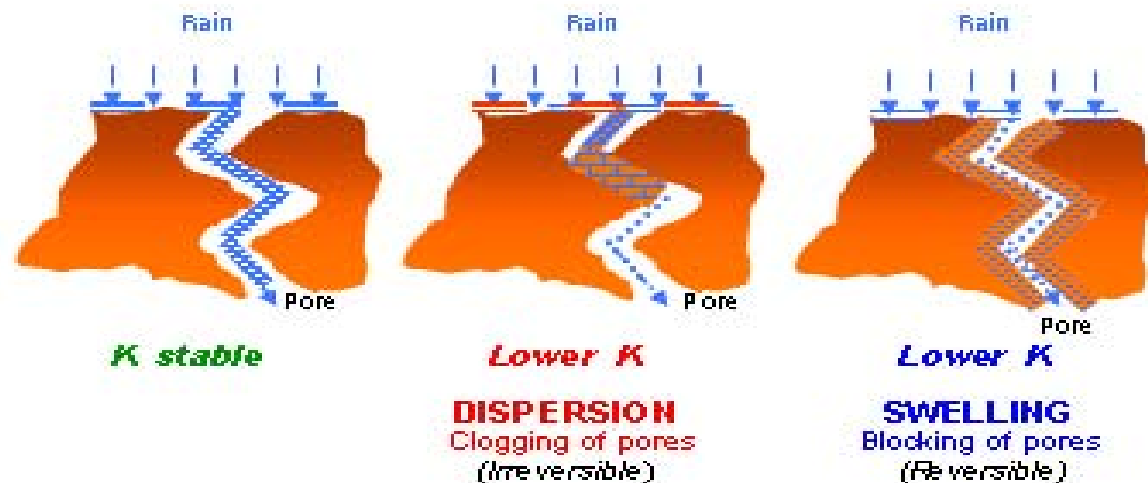
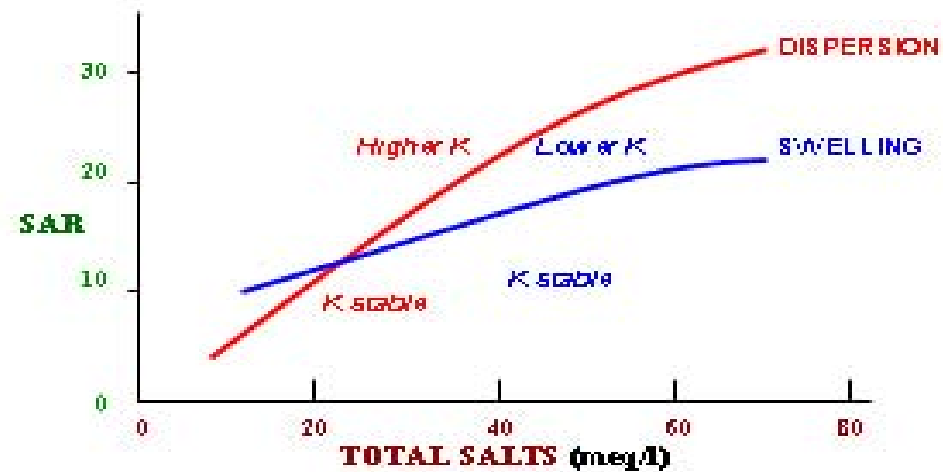
Crop salt tolerance

Relative yield Y%



Electrical conductivity
dS/m

EFFECTS OF SODIUM (SAR) AND TOTAL SALTS IN SOIL SOLUTION ON THE SATURATED HYDRAULIC CONDUCTIVITY (K) OF THE SOIL



REQUIREMENTS OF IRRIGATION AND DRAINAGE MANAGEMENT

Departing from and adequate evaluation of the **leaching requirements**, taking into consideration the previewed salt precipitation or dissolution in the soil profile, and the possibilities of **sodification** besides **salinization** it is possible a more precise calculation of the irrigation and drainage requirements: $L = LF / F$

$$H_R = (H_{ET} - H_P) / (1 - L)$$

$$H_D = (L (H_{ET} - H_P)) / (1 - L)$$

$$T_R / T_{ER} = (H_{ET} - H_P) / (720 I (1-L))$$
$$T_{ER} \leq T_{ER} (\text{máx.})$$

$$T_{ER} (\text{máx.}) = (15 \times DA \times P \times CC) / (H_{ET} - H_P)$$

Irrigation requirements (HR) and drainage requirements (HD) in mm/month, mm/day...., in order to satisfy the crop water requirements and to control at the same time the levels of salts, chlorides, sodium in the soil solution and drainage waters under the pre selected critical levels

Requirements for the irrigation management (TR /TER) in order to be able to fill the irrigation and drainage requirements (HR, HD), derived from the relation between the duration of irrigation (TR: time in hours or days required for the infiltration in the soil of the irrigation water) and the maximum interval in hours or days among irrigations (TER) for each soil (P, DA, CC and I).

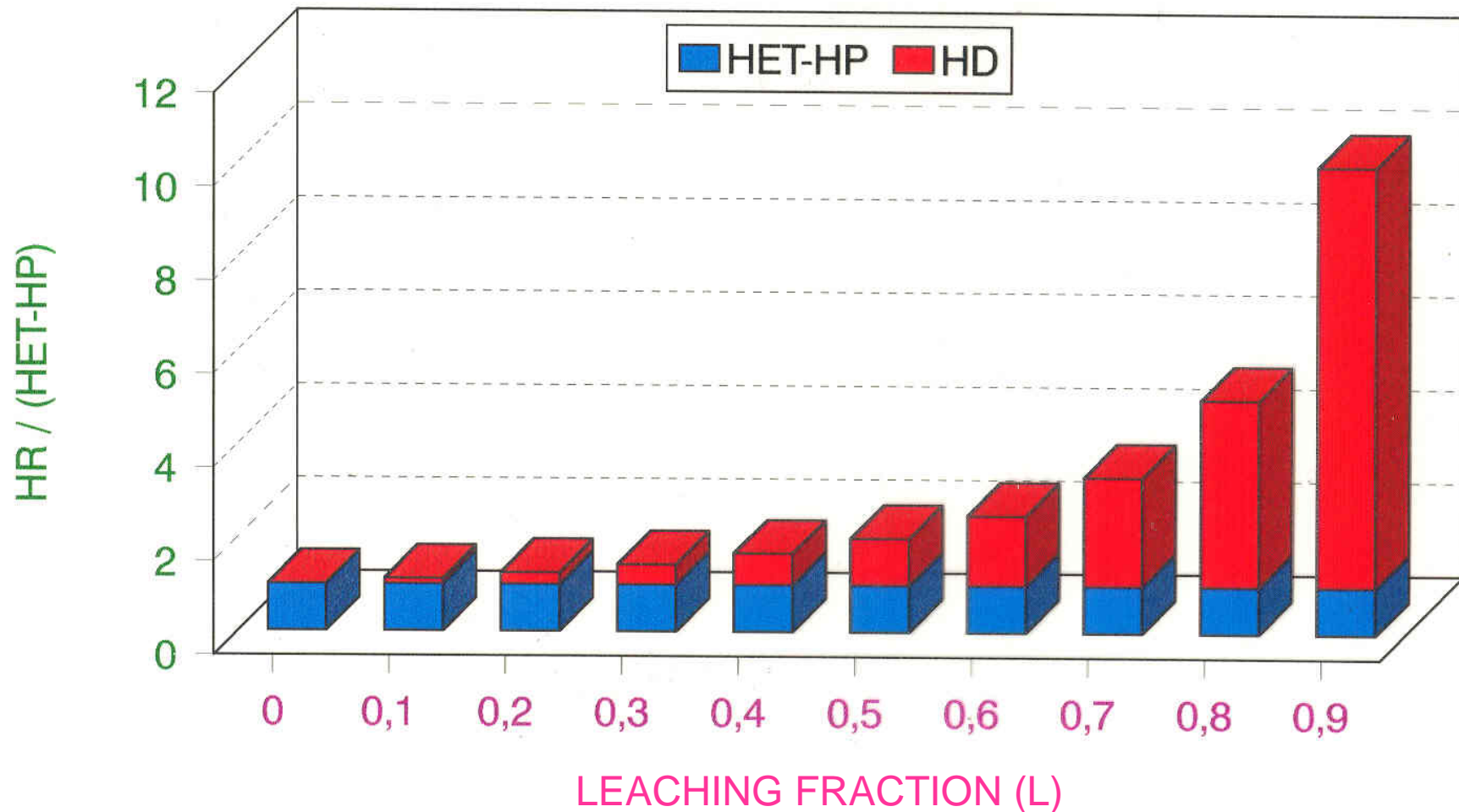
The requirements for irrigation and drainage management are the basis for precisising the best possible alternatives for irrigation and drainage management.

The final selection of a determinate alternative will depend on practical, economical and environmental limitations, such as

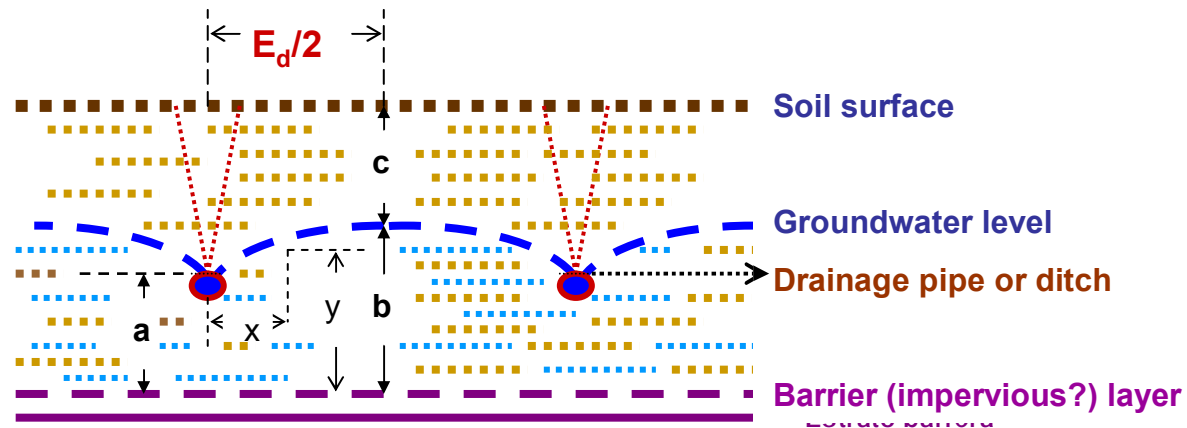
- availability and cost of the irrigation water,**
- soil hydrological properties,**
- groundwater depth,**
- natural drainage capacity and requirements of artificial drainage,**
- costs of the irrigation system,**
- limitations in the volume and salinity of the effluent drainage waters, etc.**

Irrigation water requirements (HR) in relation to the net irrigation water requirements (HET-HP) for different leaching fractions (L)

(HET: evapo-transpiracion; HP: precipitacion efectiva; HD: requerimiento de drenaje)
(HET: evapo-transpiracion; HP: precipitacion efectiva; HD: requerimiento de drenaje)



DONNAN DRAINAGE FORMULA



E_d : Distance between the drainage lines (m)

a: Vertical distance from the depth of the drainage line to the barrier layer

b: Vertical distance from the groundwater level at the middle point between the drainage lines to the barrier layer

c: Minimum depth of the groundwater level (m)

If $c+b$ (depth of the barrier layer) $> 3m$, we take $c+b = 3m$

$$E_d = (4K (b^2 - a^2)/h_d)^{1/2}$$

K: Saturated hydraulic conductivity (m/day)

h_d : Water depth to be drained (m/day)

$$Q_x = (c) (E_d/2 - x). \text{ When } x = 0 : Q_x = Q/2 \quad y \quad c = Q/E_d$$

$$Q_x = Q / E_d (E_d/2 - x)$$

$$i = dy/dx ; A = (y) (1 \text{ m section}); Q = A i K$$

$$Q_x = Q / E_d (E_d/2 - x) = K \cdot y \cdot dy/dx \cdot 1\text{m}$$

$$Q/2KE_d \cdot 1\text{m} \int (E_d - 2x)dx = \int y dy$$

Integrating between the limits: $x = E_d/2 ; x = 0 ; y = b ; y = a$

$$Q / 2K.E_d \cdot 1\text{m} (E_d x - x^2) \Big|_0^{E_d/2} = y^2/2 \Big|_a^b$$

$$(Q / 2K.E_d \cdot 1\text{m}) \cdot (E_d^2/2 - E_d^2/4) = (b^2 - a^2)/2 ; Q E_d/4K = b^2 - a^2$$

$$E_d = 4K (b^2 - a^2) / Q$$

$$h_d = Q / E_d ; Q = h_d \cdot E_d ; E_d^2 = 4K (b^2 - a^2) / h_d$$

$$E_d = (4K (b^2 - a^2)/h_d)^{1/2}$$

Q: Volume in m³/day discharged from a drainage line per m of line

K: Saturated hydraulic conductivity (m/day); i: hydraulic gradient

A: Area of the section (m²) through which the water flows to the drainage line (y.1m)

h_d: Water depth (m/day) to be drained = m³/(m².day)

It is assumed:

-That all the flux in the drainage line is due to the water removal from a soil section 1 m thick extending to a distance of E_d/2 at each side of the drainage line. -That the horizontal flux Q_x, at any distance x, is proportional to the distance from the middle point between the drainage lines, where the flux is zero.

- That when x=0, the flux towards the drainage is 1/2 of the total flux in the drainage line (Q/2). Therefore, Q_x, at any point perpendicular to the drainage line will be: Q_x = (c) (E_d/2 - x)

	meq/litro									
	<u>Na</u>	<u>Ca</u>	<u>Mg</u>	<u>Cl</u>	<u>S</u>	<u>B</u>	<u>NaB</u>	<u>MgB</u>	<u>CaCl</u>	<u>CaS</u>
I	11,5	5,6	3,9	9,7	4,5	6,7	0	1,1	0	0
II	2,1	9,0	3,1	1,4	10,3	2,3	0	0	0	6,7
III	2,0	1,0	1,0	1,0	0,5	2,5	0,5	1,0	0	0
III(E)	2,0	1,5	1,0	1,0	1,0	2,5	0	1,0	0	0

(III(E) es el agua III más una enmienda de yeso de 0,5 meq/litro o 43 g/m³)

Cuadro 2. Concentración y composición iónica de las sales presentes en aguas de riego seleccionadas

Figura 6. Requerimientos de riego (HR = HET-P+HD) y de drenaje (HD) para cultivos sensibles (STES: 40 meq/l) (HD40) y tolerantes (STES: 120 meq/l) (HD120) en un clima árido tropical

AGUA I (LFST40 = 0,48; LFST120 = 0,13; F = 0,6)

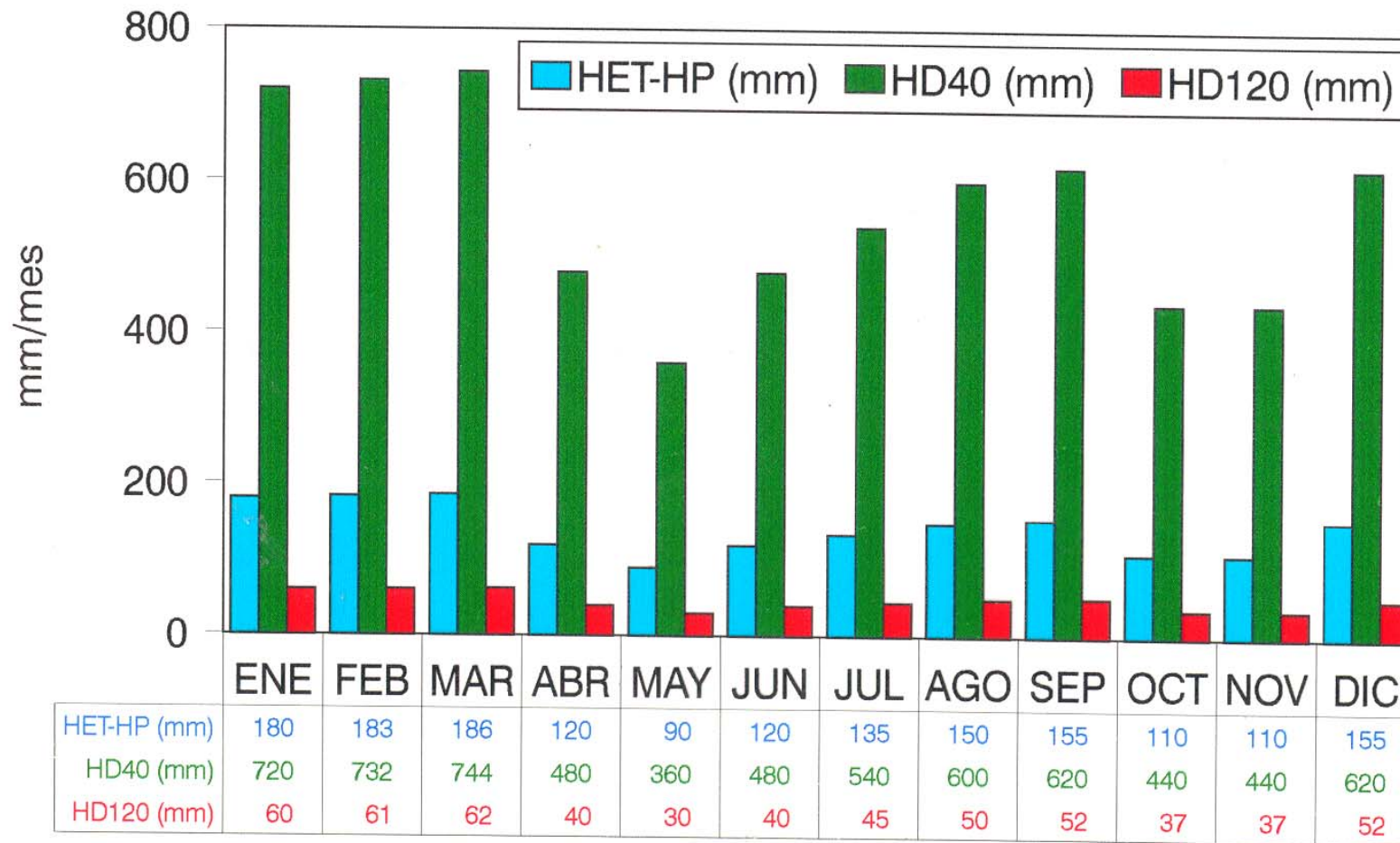


Figura 6. Requerimientos de riego (HR = HET-P+HD) y de drenaje (HD) para cultivos sensibles (STES: 40 meq/l) (HD40) y tolerantes (STES: 120 meq/l) (HD120) en un clima mediterráneo semiárido

AGUA I (LFST40 = 0,48; LFST120 = 0,13; F = 0,6)

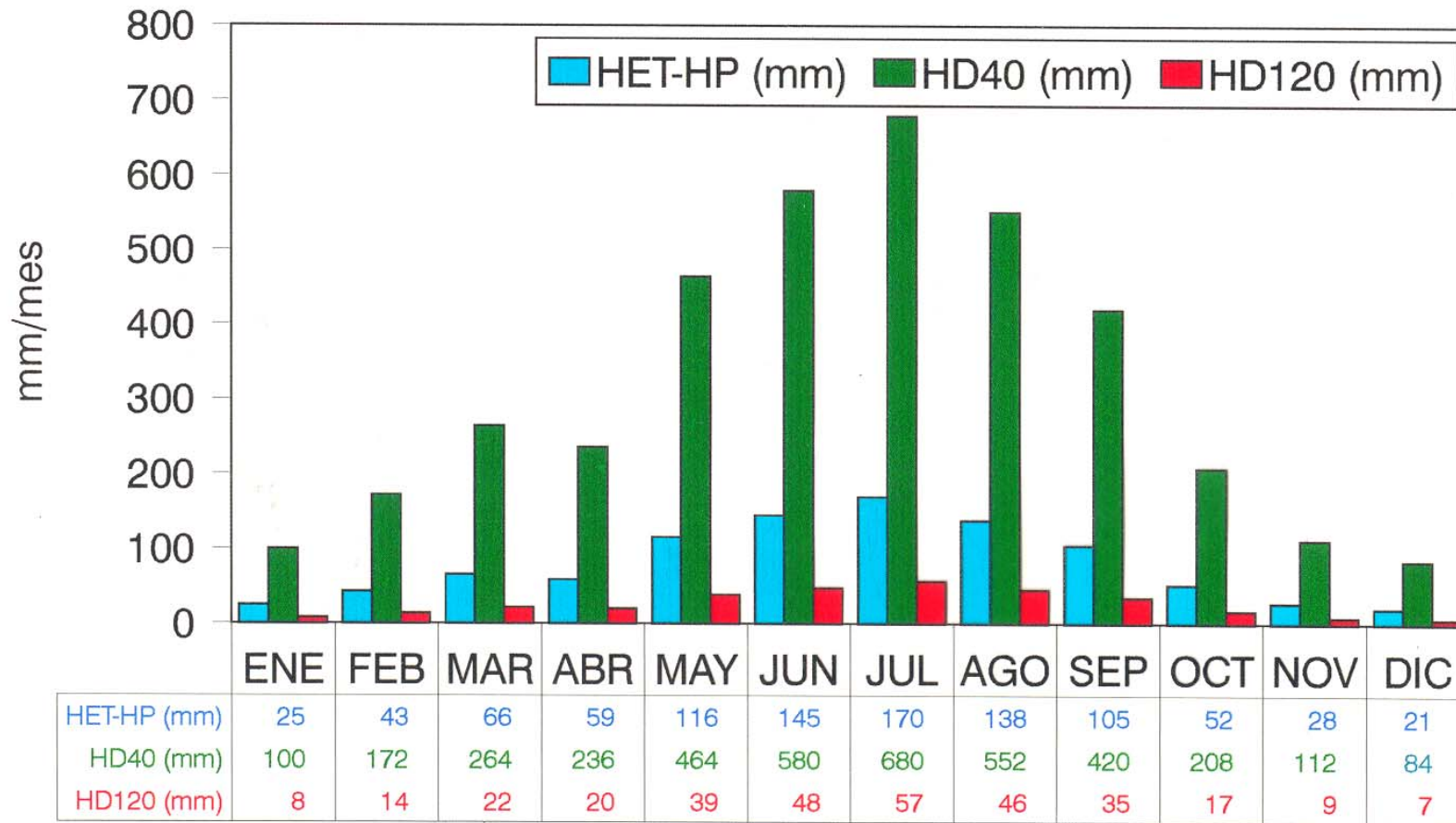


Figura 7. Requerimientos de riego (HR = HET-P+HD) y de drenaje (HD) para cultivos sensibles (STES: 40 meq/l) (HD40) y tolerantes (STES: 120 meq/l) (HD120) en un clima árido tropical

AGUA II (LFST40 = 0,36; LFST120 = 0,07; F = 0,6)

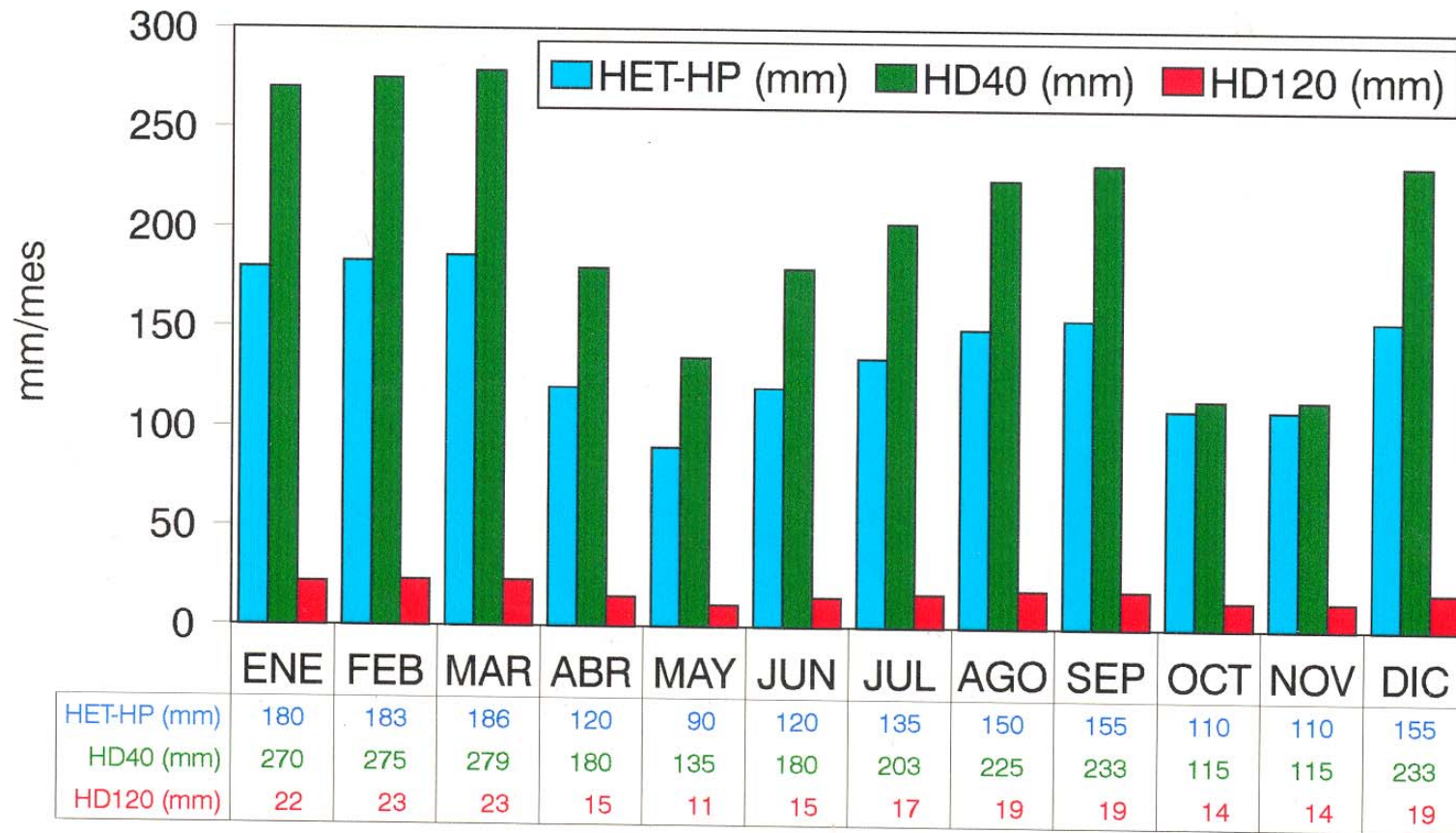


Figura 7. Requerimientos de riego (HR = HET-P+HD) y de drenaje (HD) para cultivos sensibles (STES: 40 meq/l) (HD40) y tolerantes (STES: 120 meq/l) (HD120) en un clima mediterráneo semiárido

AGUA II (LFST40 = 0,36; LFST120 = 0,07; F = 0,6)

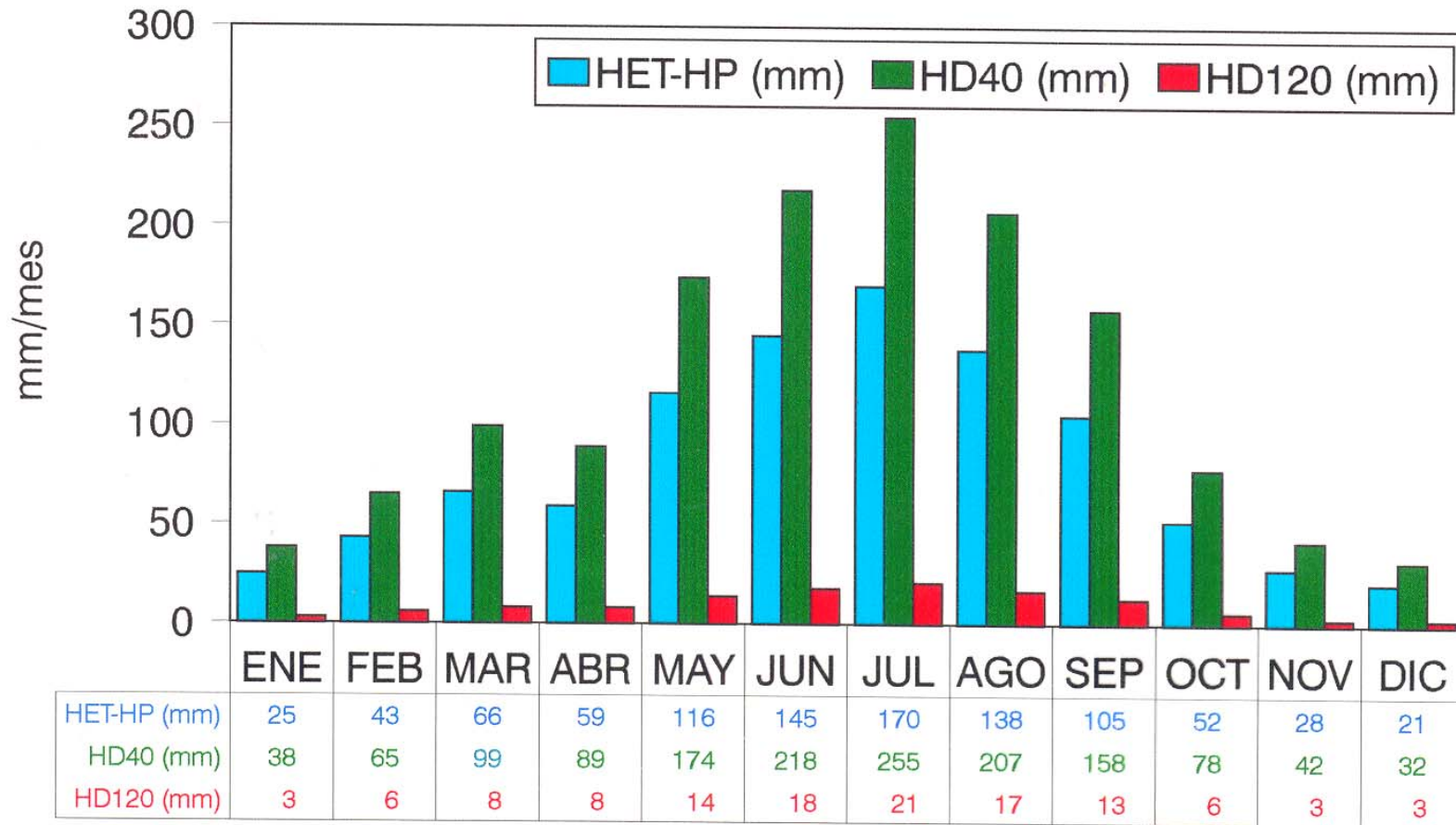


Figura 8. Requerimientos de riego (HR = HET-P+HD) y de drenaje (HD) para valores límites de RASES: 10 (HD10) y de RASES: 20 (HD20) en clima árido tropical

AGUA III (LFNa10 = 0,20; LFNa20 = 0,10; F = 0,6)

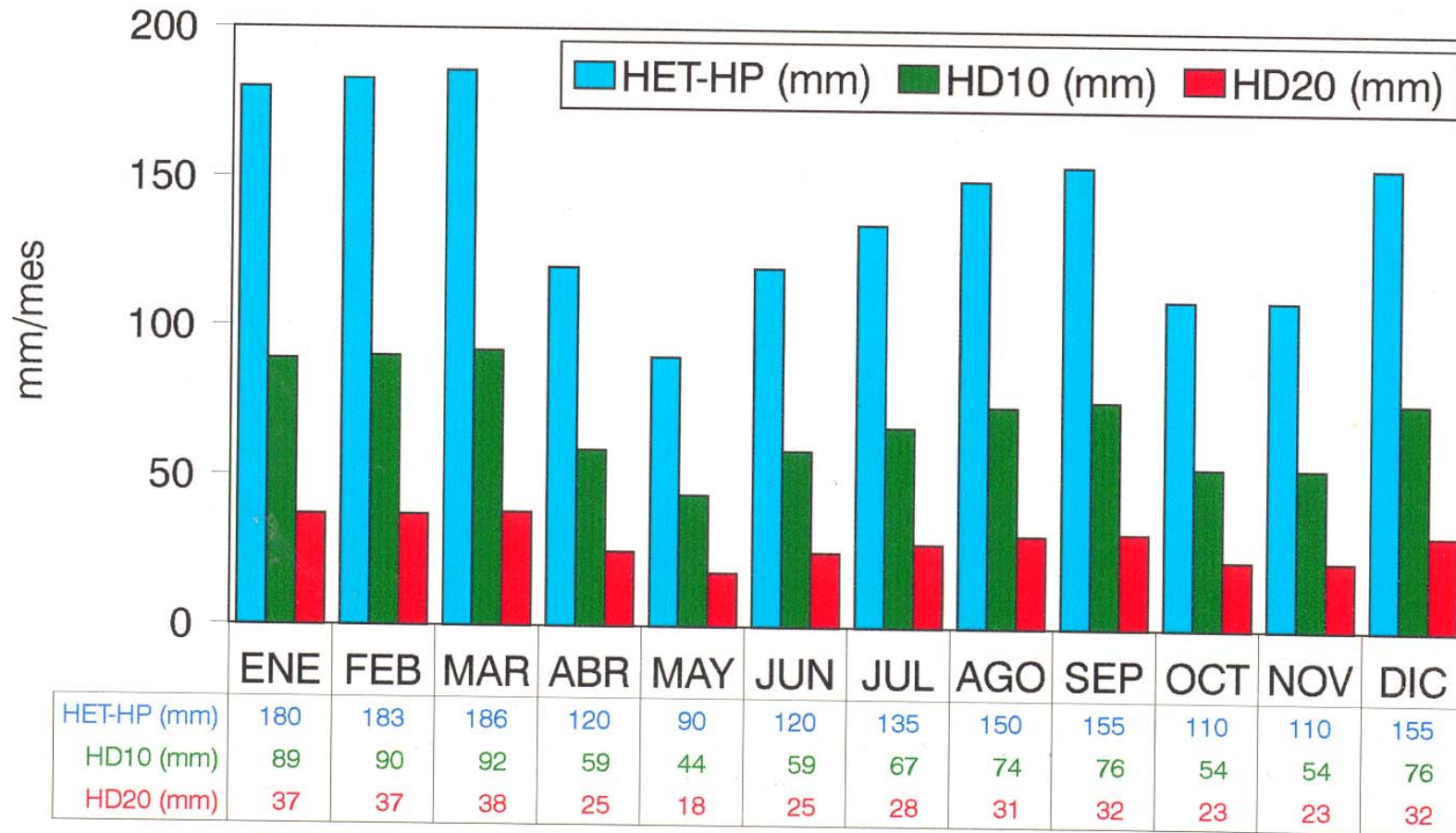


Figura 8. Requerimientos de riego (HR = HET-P+HD) y de drenaje (HD) para valores límites de RASES: 10 (HD10) y de RASES: 20 (HD20) en clima mediterráneo semiárido

AGUA III (LFNa10 = 0,20; LFNa20 = 0,10; F = 0,6)

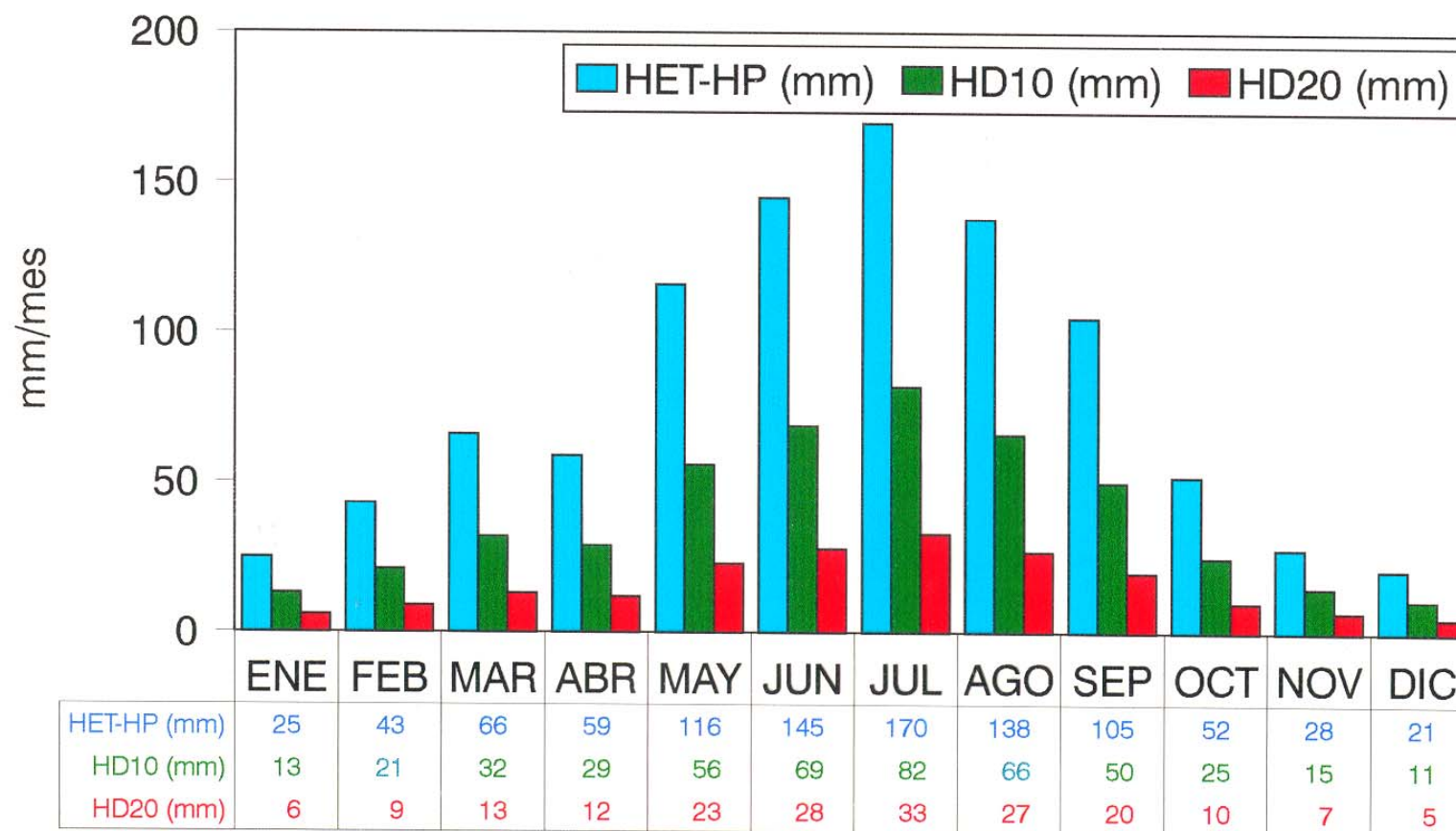


Figura 9. Requerimientos de riego (HR = HET-P+HD) y de drenaje (HD) para valores límites de RASES: 10 (HD10) y de RASES: 20 (HD20) en clima árido tropical

AGUA III(E) (LFNa10 = 0,09; LFNa20 = 0,05; F = 0,6)

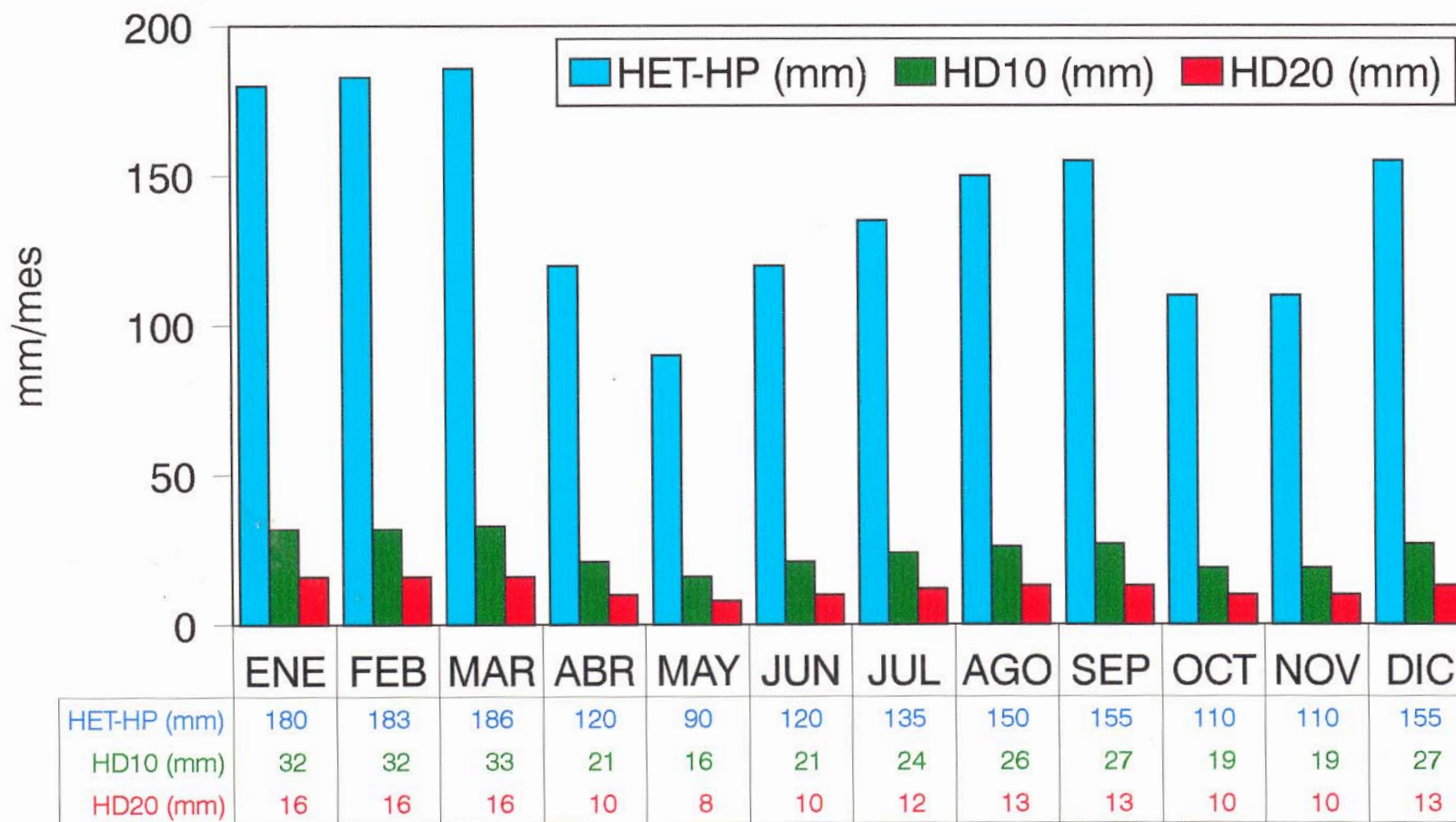
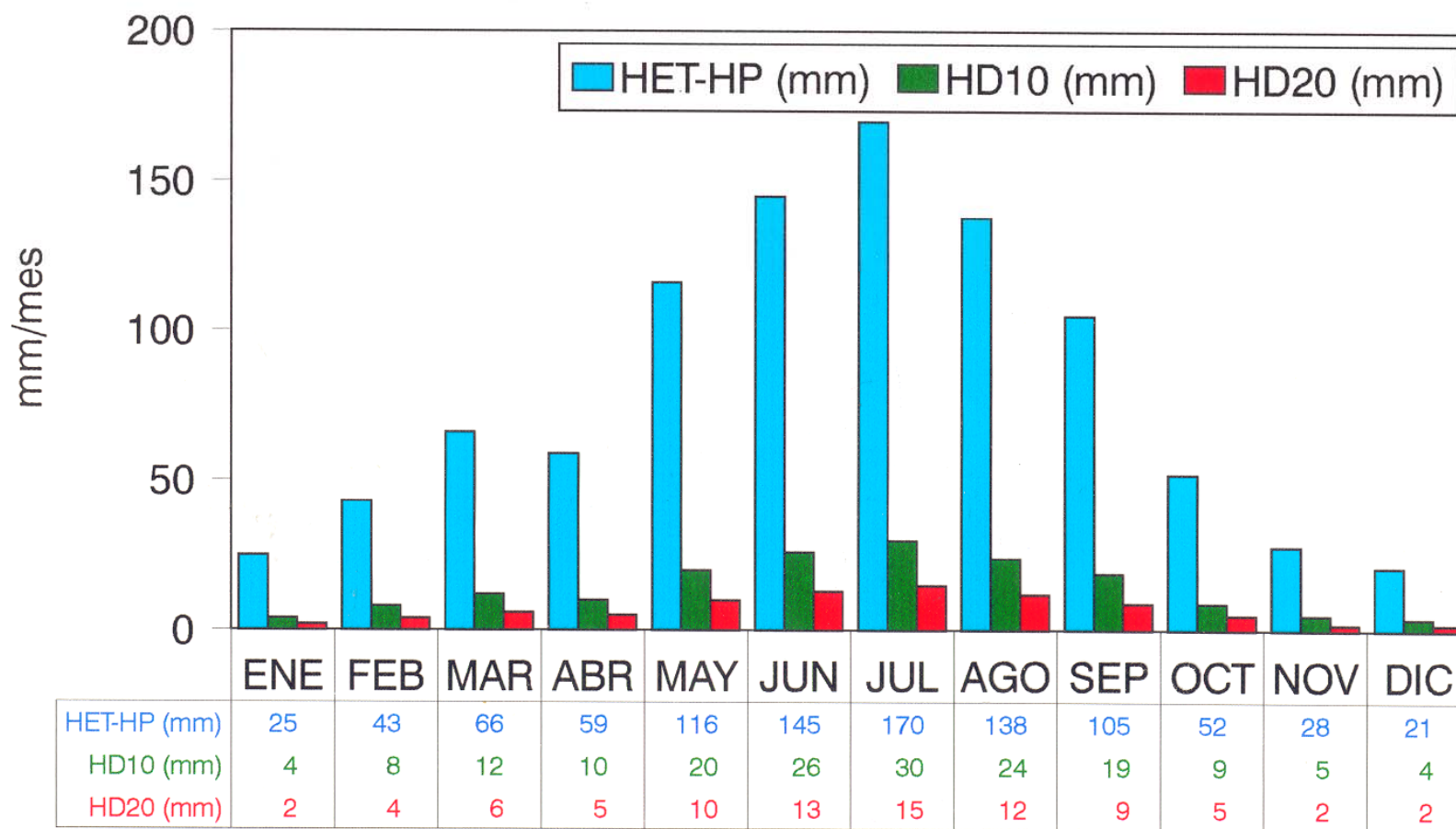
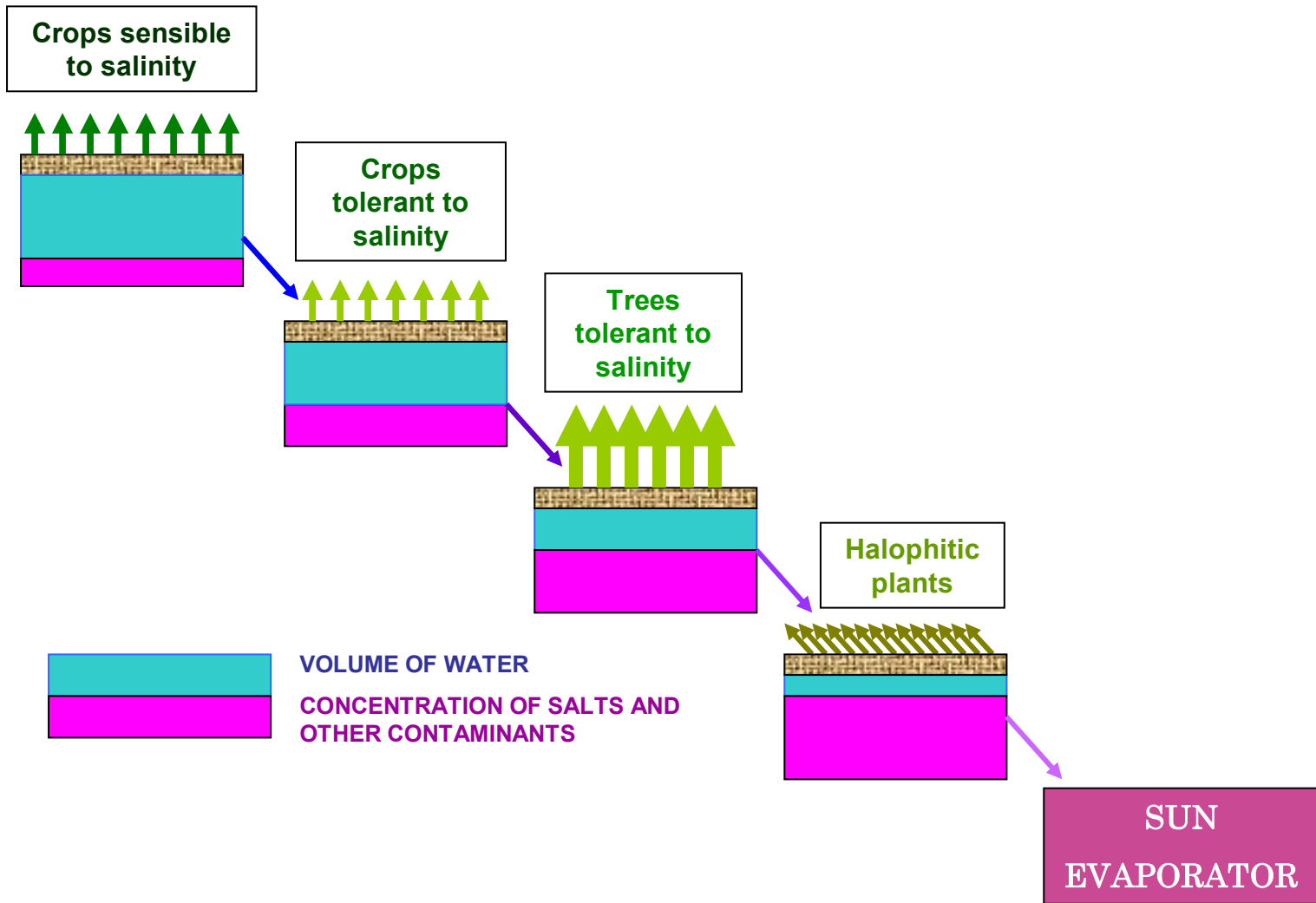


Figura 9. Requerimientos de riego (HR = HET-P+HD) y de drenaje (HD) para valores límites de RASES: 10 (HD10) y de RASES: 20 (HD20) en clima mediterráneo semiárido

AGUA III(E) (LFNa10 = 0,09; LFNa20 = 0,05; F = 0,6)





REUTILIZATION AND DISPOSAL OF DRAINAGE WATERS OF INCREASING SALINITY AND CONTAMINATION

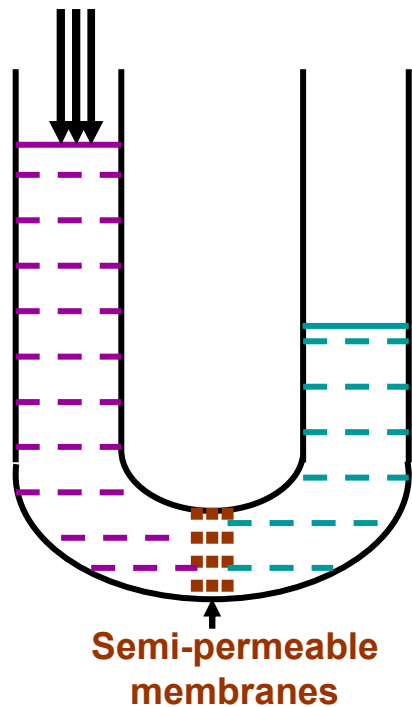
DESALINISATION OF SEA WATER

PROCESS OF DESALINISATION OF SEA WATER BY INVERSE OSMOSIS

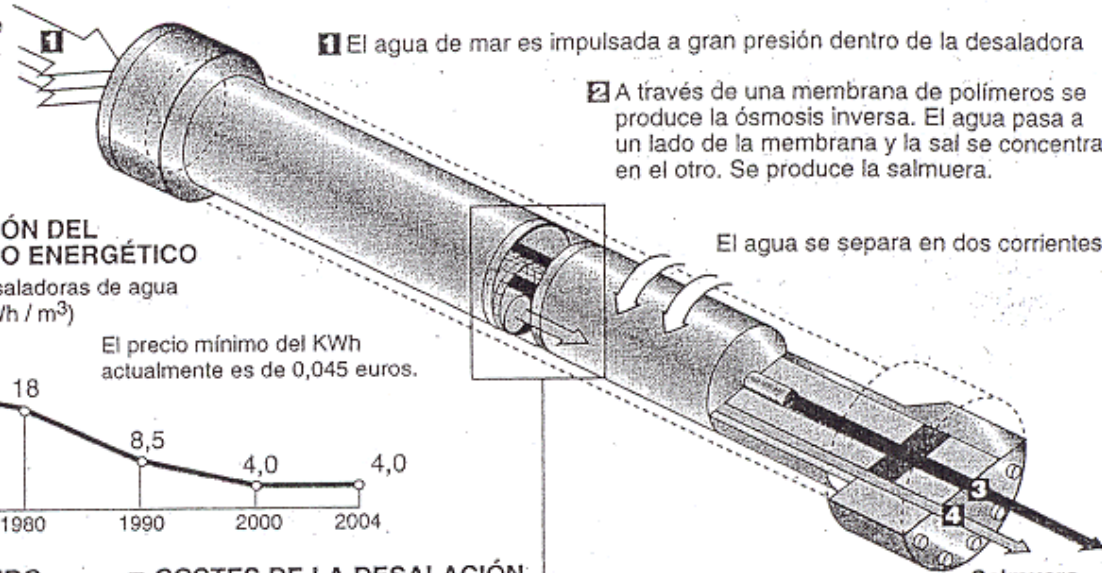
 Pure water

 Salty water

Pressure

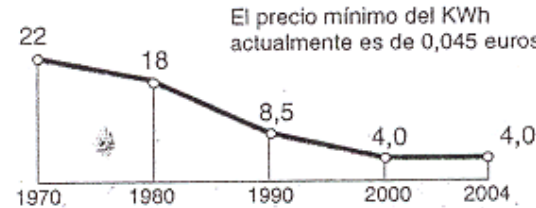


Corriente de agua



EVOLUCIÓN DEL CONSUMO ENERGÉTICO

Plantas desaladoras de agua de mar (KWh / m³)



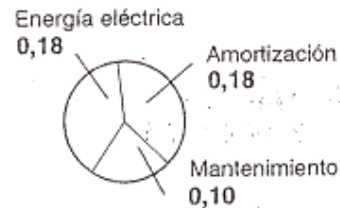
CONTENIDO DE SAL

Gramos por litro

- 37-38 Agua marina (Mediterráneo)
- 6-7 Agua salobre
- 0,5 Agua potable (máx.)

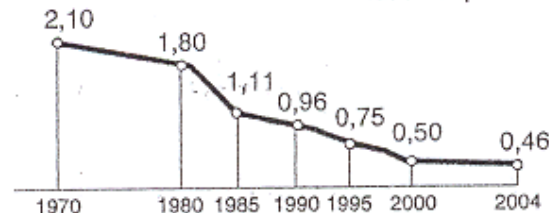
COSTES DE LA DESALACIÓN

Para una planta de 50.000 m³ / día
 Coste de inversión: 31 millones de euros (620 euros m³ / día)
 Coste del m³: 0,46 euros



COSTE DEL AGUA DE MAR DESALADA

En euros por m³



2 A través de una membrana de polímeros se produce la ósmosis inversa. El agua pasa a un lado de la membrana y la sal se concentra en el otro. Se produce la salmuera.

El agua se separa en dos corrientes

3 El agua de mar es bombeada hacia la red.

La membrana retiene la salmuera.

4 La salmuera es devuelta al mar. Como la sal está muy concentrada puede dañar la pradera de algas Posidonia que hay en muchos puntos del litoral. Existen sistemas de difusión que la diluyen en el agua circundante.



I. Pla
1964

L. A. RICHARDS
US Salinity Lab (Riverside, USA)

1964

RICHARDS EQUATION(1931)

$$\frac{\partial \theta}{\partial t} = \frac{\partial}{\partial z} (K(\Phi_m) \cdot \frac{\partial(\Phi_m)}{\partial z}) + \frac{\partial K(\Phi_m)}{\partial z}$$

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