



*The Abdus Salam
International Centre for Theoretical Physics*



1944-1

**Joint ICTP-IAEA Workshop on Nuclear Reaction Data for Advanced
Reactor Technologies**

19 - 30 May 2008

**Gas-Cooled Reactors – International Reactor
Physics Experimental Benchmark Analysis.**

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USA*



IAEA-ICTP Workshop on Nuclear Reaction Data for Advanced Reactor Technologies

ICTP – Trieste, Italy, 18-30 May 2008

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Physics Experimental Benchmark Analysis**

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Benchmark Activities

IAEA-TECDOC-1249

- **PROTEUS (Pebble Bed) Critical Facility**
- **VHTRC (Prismatic Block) Critical Facility**

IAEA-TECDOC-1382

- **HTR-10 (Pebble Bed) Core Physics**
- **HTTR (Prismatic Block) Core Physics**

<http://www.iaea.org/inisnkm/nkm/aws/htgr/abstracts/index.html>

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HTGR Knowledge Base

Subject Index to Technical Documents

HTR Conferences

[Conference on High Temperature Reactors](#) (HTR-2004)

Proceedings of the Conference on High Temperature Reactors, Beijing, China, September, 22-24, 2004

[Conference on High Temperature Reactors](#) (HTR-2002)

Proceedings of the Conference on High Temperature Reactors, Petten, NL, April 22-24, 2002

Organized by HTR-TN in cooperation with the European Nuclear Society (ENS) and the IAEA

Reactor Design and General Technology

[Evaluation of high temperature gas cooled reactor performance: Benchmark analysis related to initial testing of the HTR and HTR-10](#) (IAEA-TECDOC--1382)[Current status and future development of modular high temperature gas cooled reactor technology](#) (IAEA-TECDOC--1198)

Overview of HTGR technology development as of 2001

[High temperature gas cooled reactor technology development.](#) (IAEA-TECDOC--988)

Technical committee meeting on high temperature gas cooled reactor technology development. Johannesburg (South Africa). 13-15 Nov 1996.

[Design and development of gas cooled reactors with closed cycle gas turbines.](#) (IAEA-TECDOC--899)

Technical committee meeting on design and development of gas cooled reactors with closed cycle gas turbines. Beijing (China). 30 Oct - 2 Nov 1995.

[Gas-cooled fast reactors.](#) (IAEA-TECDOC--154)

Proceedings of the IAEA study group meeting sponsored by the USSR State Committee on the Utilization of Atomic Energy, held at the Institute of Nuclear Energy of the Byelorussian Academy of Sciences Minsk, 24-28 July 1972.



see also:

Nuclear Power
Technology
Development Section

-- SMRs

-- LWRs and HWRs

-- Fast Reactors and
Hybrid Systems

-- HTGRs

-- Nuclear
Desalination

-- INPRO

-- Reactor Simulators

Power Reactor
Information System
(PRIS)

Technical committee meeting on design and development of gas cooled reactors with closed cycle gas turbines. Beijing (China). 30 Oct - 2 Nov 1995.

[Gas-cooled fast reactors](#). (IAEA-TECDOC--154)

Proceedings of the IAEA study group meeting sponsored by the USSR State Committee on the Utilization of Atomic Energy, held at the Institute of Nuclear Energy of the Byelorussian Academy of Sciences Minsk, 24-28 July 1972.

Component Technology

[Critical experiments and reactor physics calculations for low-enriched HTGRs](#) (IAEA-TECDOC--1249)

Results of an IAEA Co-ordinated Research Project in support of validation of reactor physics codes for modular HTGRs conducted 1990-1996

[Gas turbine power conversion systems for modular HTGRs](#) (IAEA-TECDOC--1238)

IAEA Technical Committee Meeting on "Gas Turbine Power Conversion Systems for Modular HTGRs", held from 14-16 November 2000 in Palo Alto, California

[Uncertainties in physics calculations for gas cooled reactor cores](#). (IWGGCR--24)

Uncertainties in physics calculations for gas cooled reactor cores. Proceedings of a specialist's meeting held in Villigen, Switzerland, 9-11 May 1990

[Seismic behaviour of gas cooled reactor components](#). (IWGGCR--22)

Seismic behaviour of gas cooled reactor components. Proceedings of a specialists' meeting held in Gif-sur-Yvette, France, 14-16 November 1989

[Gas-cooled reactor coolant circulator and blower technology](#) (IWGGCR--17)

Specialists' meeting on gas-cooled reactor coolant circulator and blower technology. San Diego, CA (USA). 30 Nov - 2 Dec 1987

[Technology of steam generators for gas-cooled reactors](#) (IWGGCR--15)

Specialists' meeting on technology of steam generators for gas-cooled reactors Winterthur (Switzerland) 9-12 Mar 1987

[Graphite component structural design](#) (IWGGCR--11)

Specialists' meeting on graphite component structural design, JAERI Tokai (Japan), September 8-11, 1986

[Heat exchanging components of gas-cooled reactors](#) (IWGGCR--9)

Specialists' meeting on heat exchanging components of gas-cooled reactors Duesseldorf (Germany) 16-19 Apr 1984

[Gas-cooled reactor fuel development and spent fuel treatment](#) (IWGGCR--8)

Specialists' meeting on gas-cooled reactor fuel development and spent fuel treatment Moscow (Russian Federation) 18-21 Oct 1983

Materials Technology

[Irradiation damage in graphite due to fast neutrons in fission and fusion systems](#) (IAEA-

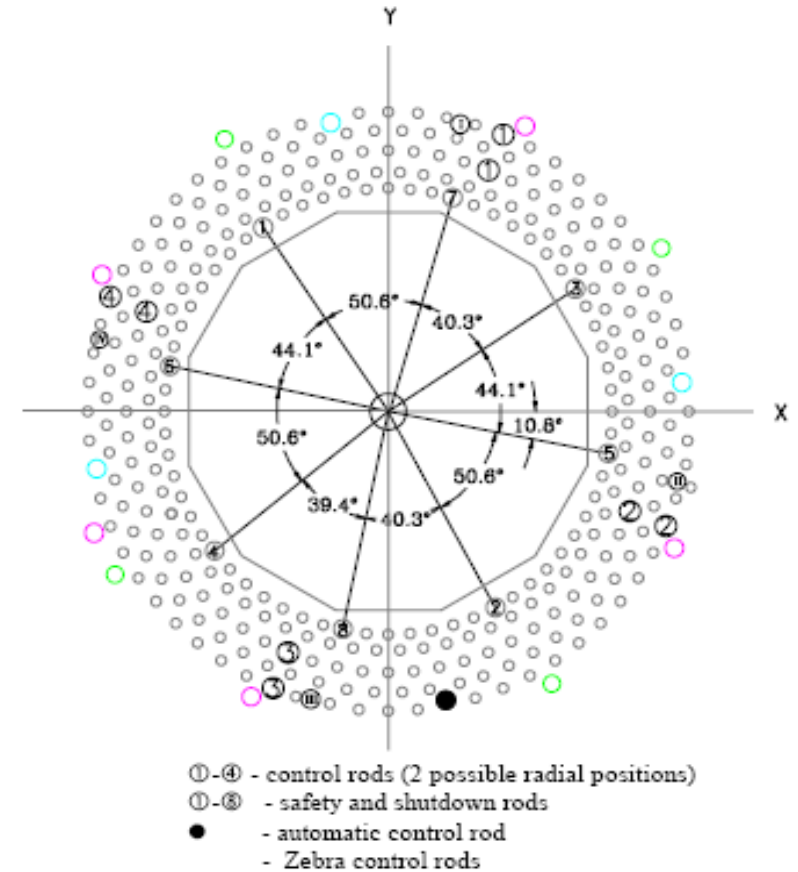
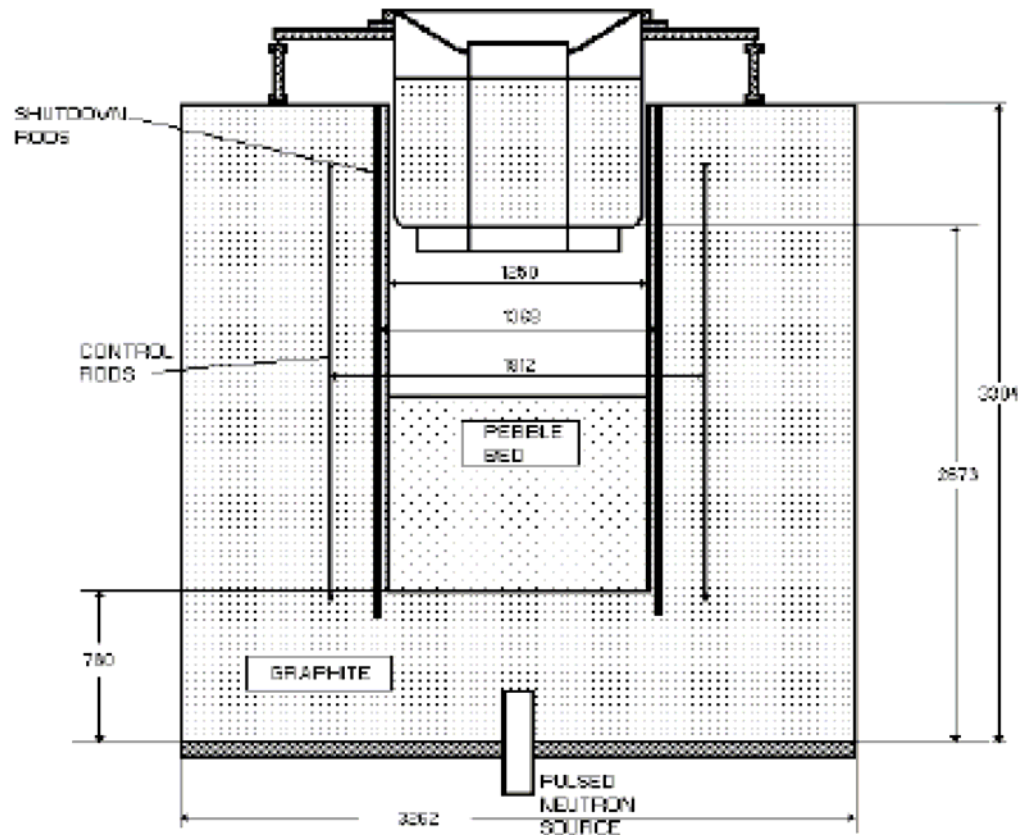


PROTEUS Benchmarks

- Critical Balances
- Reaction rate ratios and distributions
- Control rod worths
- Water ingress effects
- Reactivity of small samples
- Kinetic parameter (β/Λ)



PROTEUS Benchmarks





PROTEUS Benchmarks

CORE	DATES	F:M	PACKING	COMMENTS
G1	3/92-5/92	-	-	ONLY PNS MEASUREMENTS, NO FUEL IN CAVITY, WITH AND WITHOUT MODERATOR PEBBLES. ZEBRA RODS IN-SITU
1	7/92-6/93	2:1	HCP	ONLY CORE WITH ZEBRA RODS
1A	6/93-8/93, 2/94-3/94	2:1	HCP	CORE 1 WITH ZEBRA RODS REPLACED BY CONVENTIONAL CONTROL RODS
2	8/93-10/93	2:1	HCP	CORE 1A WITH FIVE FUELED LAYERS REPLACED BY MODERATOR PEBBLES - "CAVITY EFFECT"
G2	10/93	-	-	PNS MEASUREMENTS WITHOUT FUEL IN CAVITY. ZEBRA RODS COMPLETELY REMOVED
3	10/93-2/94	2:1	HCP	CORE 1A WITH SIMULATED WATER INGRESS - EVERY AVAILABLE VERTICAL CHANNEL CONTAINED A 9mm CH ₂ ROD
4(1,2,3)	3/94-6/94	1:1	RANDOM	THIS CONFIGURATION REPEATED THREE TIMES
5	7/94-4/95, 11/95-1/96	2:1	P-O-P	FIRST COLUMN HEX LOADING
6	4/95-5/95	2:1	P-O-P	CORE 5 WITH MAXIMUM CH ₂ LOADING, COMPENSATED WITH COPPER WIRE
7	5/95-10/95	2:1	P-O-P	CORE 5 WITH MAXIMUM CH ₂ LOADING, COMPENSATED BY REDUCING CORE HEIGHT
8	1/96-2/96	2:1	P-O-P	CORE 5 WITH EVERY VERTICAL CHANNEL CONTAINING A 15cm LONG TRIANGULAR CH ₂ ROD
9	2/96-5/96	1:1	P-O-P	CORE 5 REPEATED WITH F:M OF 1:1
10	5/96-6/96	1:1	P-O-P	CORE 9 WITH MAXIMUM CH ₂ LOADING, COMPENSATED BY REDUCING CORE HEIGHT

HCP = hexagonal close packed

P-O-P = point-on-point (column hexagonal),

F:M = fuel-to-moderator ratio

indicates simulated water ingress in this core



PROTEUS Benchmarks

METHOD CORE	CRITICAL LOADING	Σ_a	SUBCRIT CORE	SHUTDOWN RODS		CONTROL RODS		UPPER REFL.	β/Λ	MEAS. RODS	CENT. CONT. ROD	TEMP. COEFF	COM- PONENT WORTHS	MISC.
	PEBBLE COUNT	PNS	PNS	PNS	IK	SP	PNS	PNS (SP)	PNS	PNS	PNS	COMP	COMP	-
G1		✓												
1	✓		✓	✓	✓	✓	✓		✓	✓			✓	
1A	✓				✓	✓								
2	✓			✓	✓	✓	✓	✓	✓					
G2		✓												
3	✓		✓	✓	✓	✓	✓		✓					
1A	✓			✓		✓								
4(1)	✓					✓								
4(2)	✓			✓	✓	✓								
4(3)	✓			✓		✓								
5	✓			✓	✓	✓	✓	✓	✓	✓	✓	✓	✓	water/ CH ₂ CH ₂ in lower axial reflector
6	✓					✓								
7	✓			✓	✓	✓	✓	✓	✓	✓	✓	✓		water/ CH ₂ CH ₂ in lower axial reflector
8	✓						✓							
9	✓				✓	✓	✓	✓	✓	✓				
10	✓		✓		✓	✓	✓	✓	✓	✓				subcriticalit y with CH ₂ removed



PROTEUS Benchmarks

Methods - Critical Balances Including Streaming

At PSI:	The TWODANT [8.1] transport theory code with cross sections obtained from the MICROX-2 [8.2] cell calculation code, using JEF-1 based nuclear data, as well as the MCNP-4B [8.3] Monte Carlo code using an ENDF/B-V based continuous cross-section data library.
At IRI:	The DORT [8.4] transport theory and the BOLD-VENTURE [8.5] diffusion theory codes with inputs processed by the INAS code system (IRI-NJOY-AMPX-SCALE) [8.6] using JEF-2.2 basic nuclear data files, as well as the multigroup Monte Carlo code KENO-Va.
At JAERI:	The SRAC95 [8.7] code system with its library based on both ENDF/B-IV and JENDL-3.2.
At KFA:	The CITATION diffusion calculation code, part of the VSOP [8.8] code system using JEF-1 and ENDF/B-V based libraries.
At INET:	The VSOP computer code system.



PROTEUS Benchmarks

Experimental and Calculated Critical Balances Cores 1A, 2, 3 and 4.3

	Core 1A	Core 2	Core 3	Core 4.3
experimental	1.0147±0.0006	1.0106±0.0006	1.0033±0.0004	1.0132±0.001
VSOP (INET)	1.01299	1.00389	1.01333	1.00512
C/E	0.9983±0.0006	0.9934±0.0006	1.0100±0.0004	0.992±0.001
VSOP (KFA)	-	-	-	1.0246
C/E	-	-	-	1.011±0.001
SRAC-ENDF/B-IV (JAERI) *	1.0384	1.0376	-	-
C/E	1.0234±0.0006	1.0267±0.0006	-	-
SRAC-JENDL-3.2 (JAERI) *	1.0427	1.0412	-	-
C/E	1.0276±0.0006	1.0303±0.0006	-	-

* Not corrected for streaming effect



PROTEUS Benchmarks

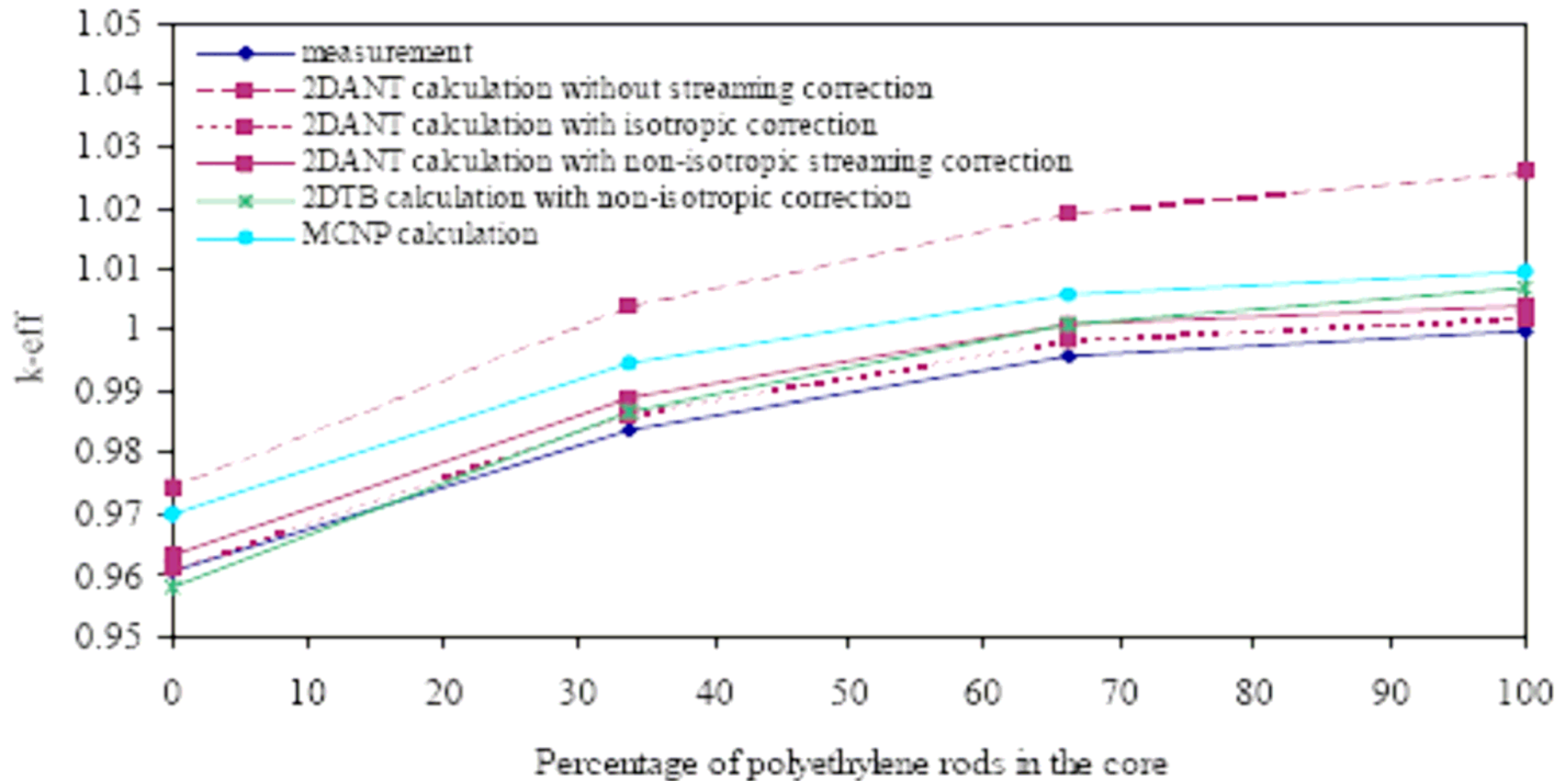
Experimental and Calculated Critical Balances Cores 5, 7, 9 and 10

	Core 5	Core 7	Core 9	Core 10
experimental	1.0112±0.0005	1.0067±0.0004	1.0142±0.0007	1.0075±0.0001
TWODANT (PSI)	1.0218	1.0384	1.0262	1.0330
C/E	1.0105±0.0005	1.00315±0.0004	1.0118±0.0007	1.0253±0.0001
DORT (IRI)	1.03126	1.03962	1.03017	1.03395
C/E	1.0198±0.0005	1.0327±0.0004	1.0157±0.0007	1.0263±0.0001
BOLD-VENTURE (IRI)	1.03147	1.03600	1.03018	1.03138
C/E	1.0200±0.0005	1.0291±0.0004	1.0158±0.0007	1.0237±0.0001
SRAC-ENDF/B-IV (JAERI)	1.0358	1.0515	-	-
C/E	1.0243±0.0005	1.0445±0.0004	-	-
SRAC-JENDL-3.2 (JAERI)	1.0394	1.0545	-	-
C/E	1.0289±0.0005	1.0475±0.0004	-	-
VSOP (KFA)	1.0379	1.0446	-	-
C/E	1.0264±0.0005	1.0376±0.0004	-	-
KENO (IRI)	1.03125±0.0007	1.03881±0.0006	1.02933±0.0005	1.03222±0.0005
C/E	1.0198±0.0009	1.0319±0.0007	1.0149±0.0009	1.0245±0.0005



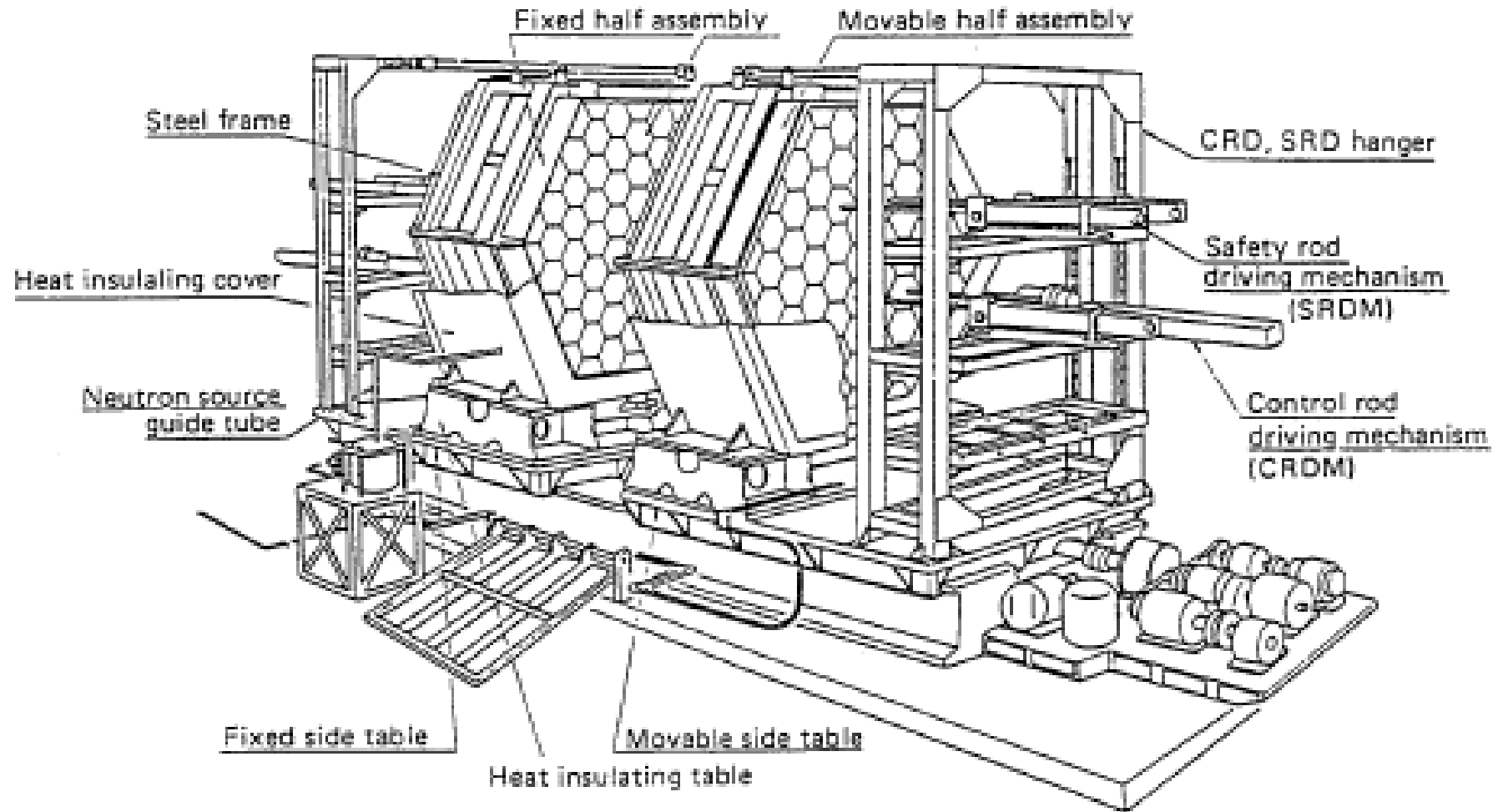
PROTEUS Benchmarks

Reactivity vs. Percentage of Polyethylene Rods in Core 10



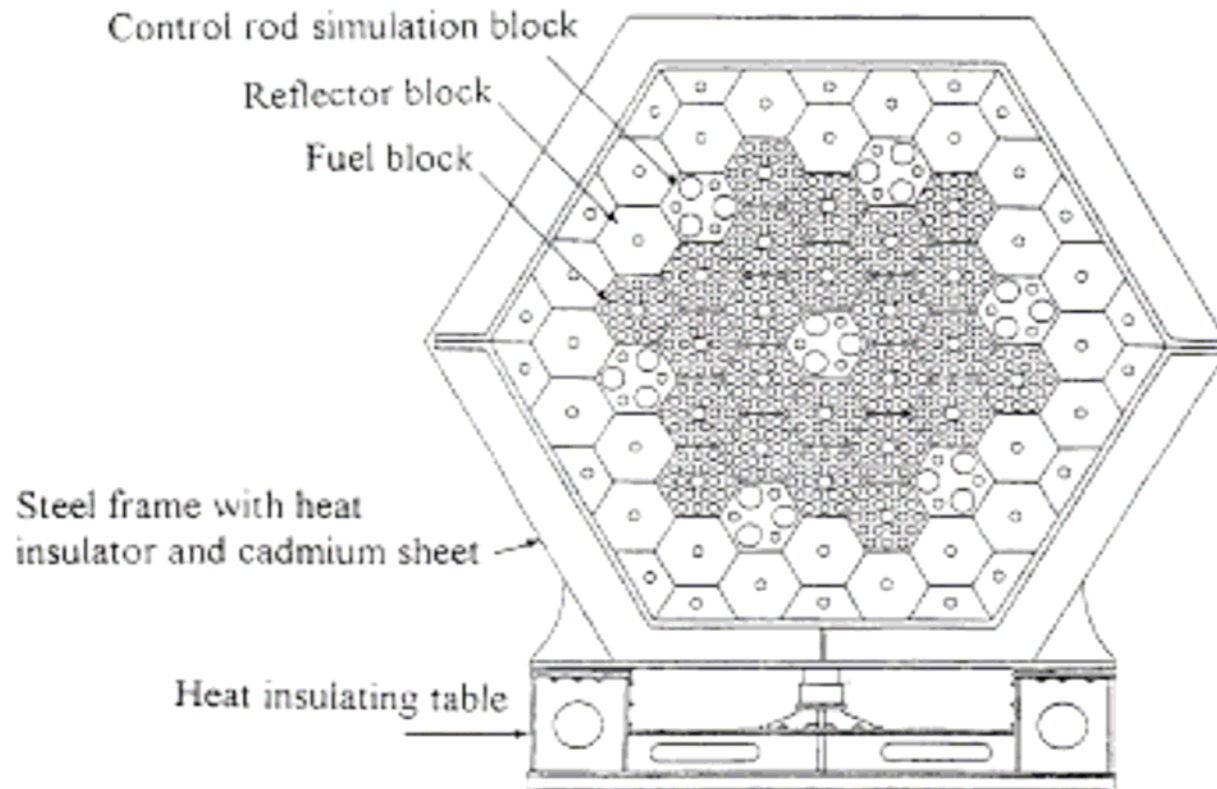


VHTRC Benchmark





VHTRC Benchmark

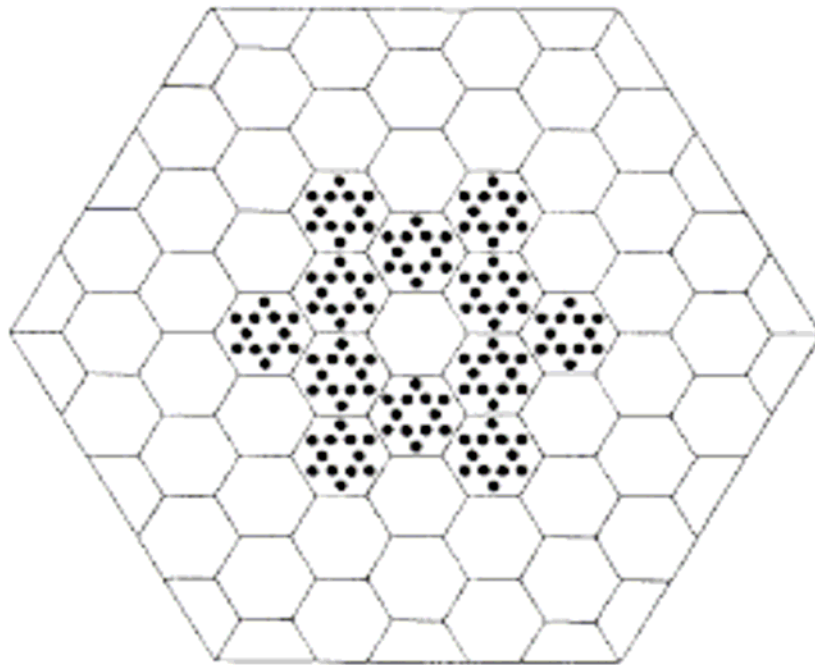


Circles in core and reflector indicate graphite rods. The rods in core can be replaced with fuel rods, while those in reflector can be replaced with heater rods.

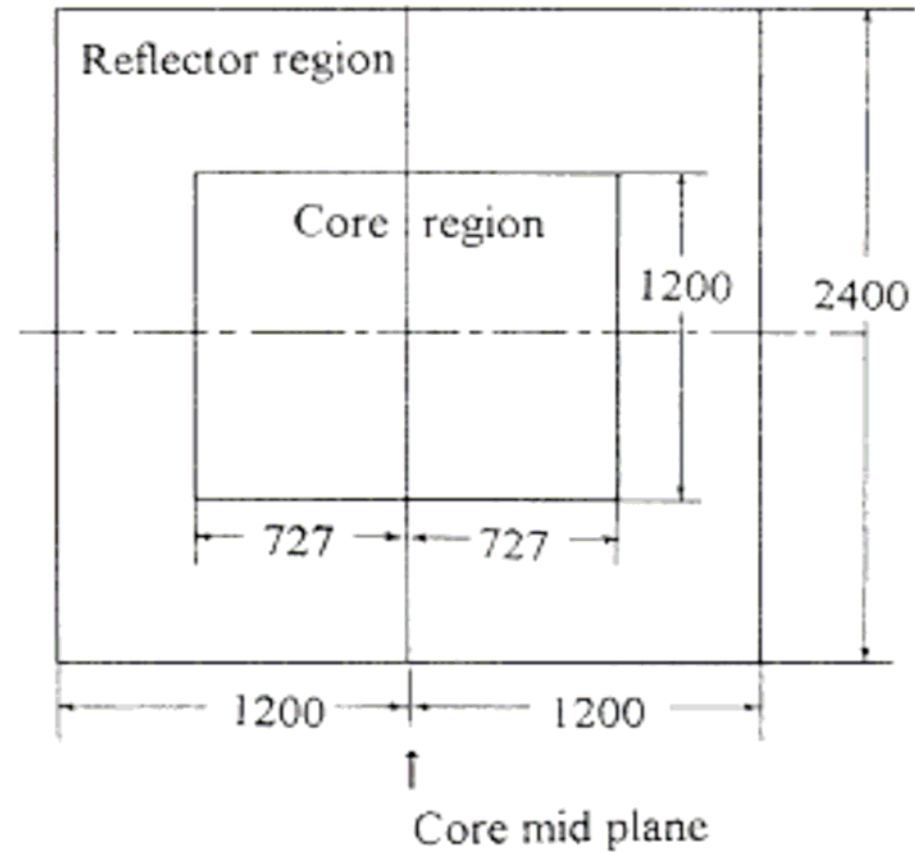


VHTRC Benchmark

Unit : mm



• B-4 fuel rod





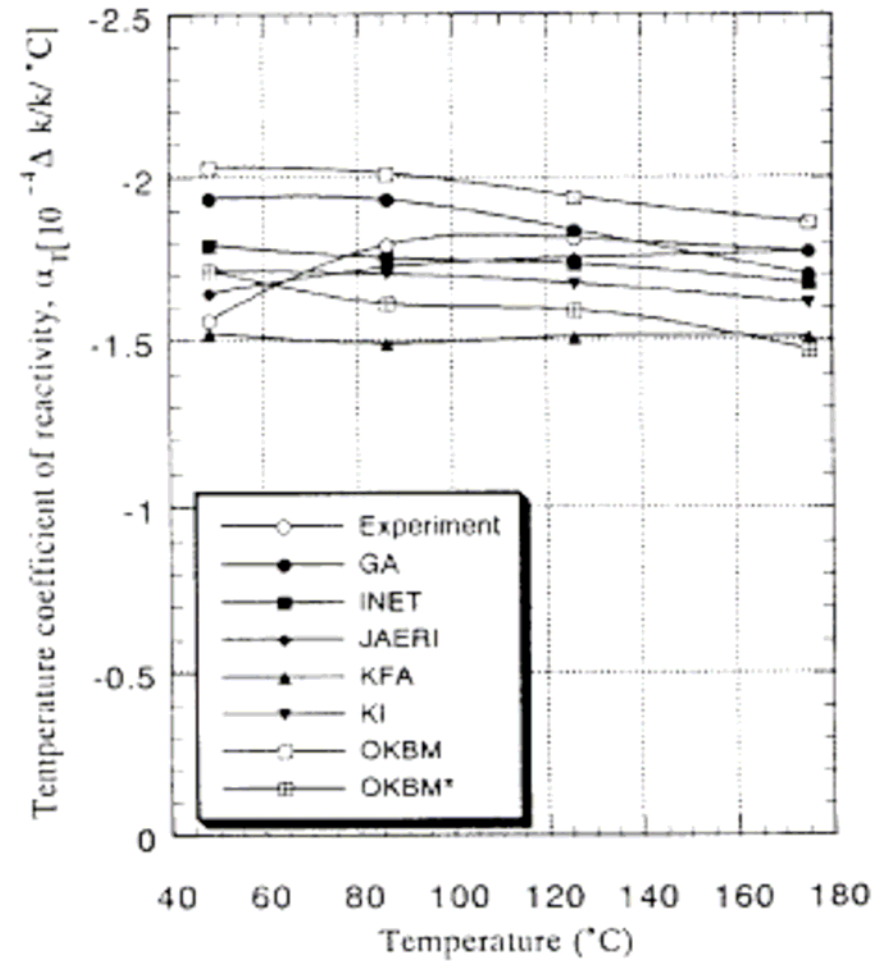
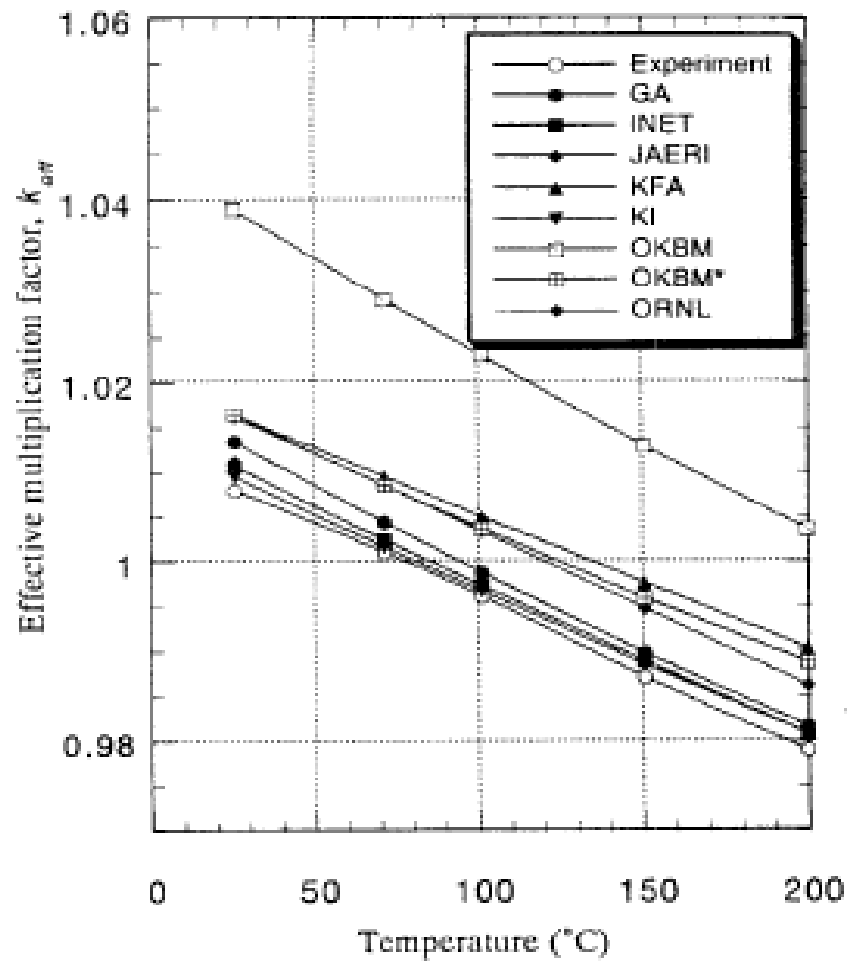
VHTRC Benchmark

Institute	Nuclear data	Resonance calculation		Cell calculation			Whole reactor calculation		
		Code	Group	Code	Group	Geometry	Code	Group	Geometry
GA	ENDF / B-V	GAR	9k-15k	GAM GATHER MICROX	92 101 92+101	Coaxial cylinders	DIF3D	9	3D(T-Z)
INET	ENDF / B-IV	ZUT		GAM THERMOS		Cylinder	CITATION	4	2D(R-Z)
JAERI	ENDF / B-IV ENDF / B-III	PEACO	4.6k	[SRAC] PIJ	21+41	Hexagonal cylinder	[SRAC] CITATION	25	3D(T-Z)
KFA	ENDF / B-V JEF-1	ZUT-DGL		[VSOP] GAM THERMOS		Cylinder	[VSOP] CITATION	5	2D(R-Z)
KI	Domestic	Experiment correlated		FLY	26+77	Cylinder	CONSUL (Diffusion)	4	3D(T-Z)
OKBM	Domestic UKNDL	NEKTAR (plane)		WIMS-D4 THERMOS	67	Cylinder	JAR (Diffusion)	2	3D
ORNL	ENDF/B-V	[MCNP] V 4.X	Conti.	[MCNP] V 4.X	Cont.	Hexagonal cylinder	[MCNP] V 4.X	Cont.	3D(xyz)

Cont. : Continuous energy



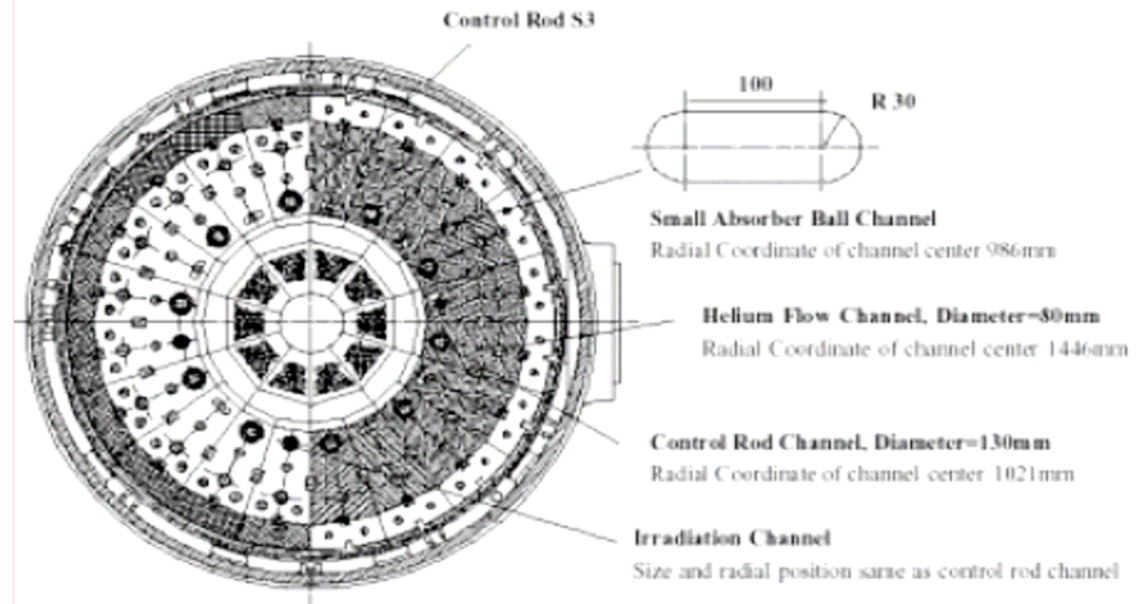
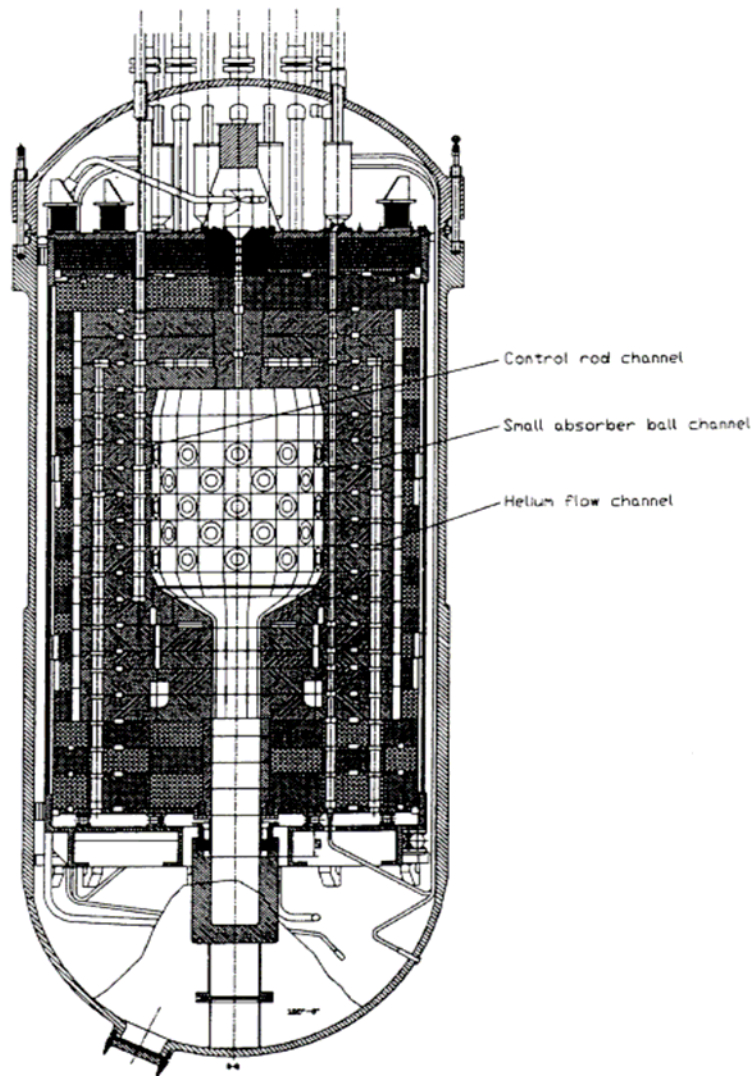
VHTRC Benchmark



OKBM* - Macroscopic cross sections by WIMS-D4/UKNDL

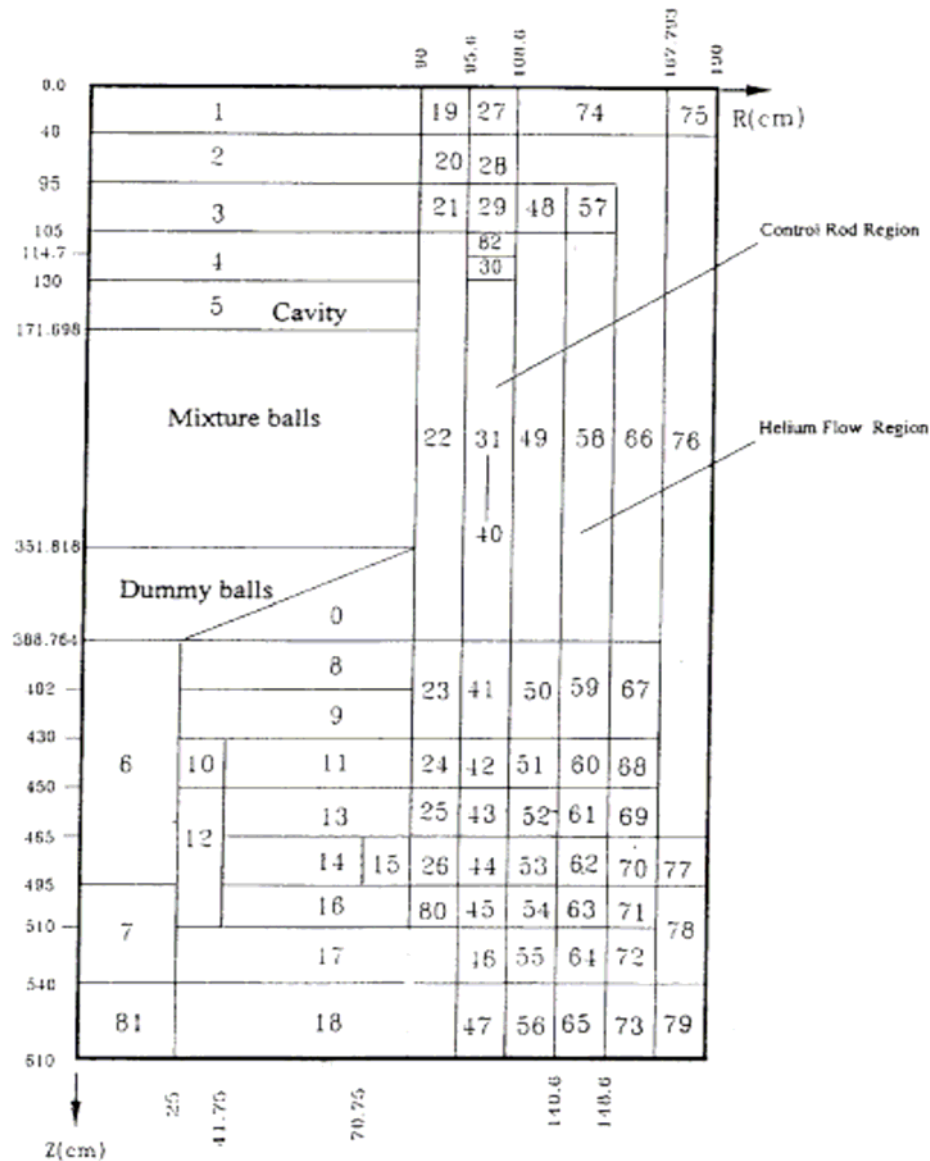


HTR-10 Benchmarks





HTR-10 Benchmarks



Core physics calculation
Geometric model



HTR-10 Benchmarks

HTR-10 Benchmark Problems		
B1	Initial Criticality	Pebble loading height for $k_{\text{eff}} = 1.0$ with no control rods inserted
B2	Temperature Coefficient	k_{eff} of the full core (5 m^3) at 20°C (B21), 120°C (B22), and 250°C (B23) with no control rods inserted
B3	Control Rod Worth, Full Core	Δk_{eff} for ten (B31) and one (B32) fully inserted control rods, with other rods in withdrawn position, full core (5 m^3) at 20°C
B4	Control Rod Worth, Initial Core	Δk_{eff} for ten (B31) and one (B32) fully inserted control rods, with other rods in withdrawn position, core loading height of 126 cm at 20°C
All cases to assume helium atmosphere		

Post-Test Adjustment to Benchmark Problem Assumptions/Conditions

- Density of dummy balls: $1.73 \rightarrow 1.84 \text{ g/cm}^3$
- Boron equivalent of impurities in dummy balls: $1.3 \rightarrow 0.125 \text{ ppm}$
- Core atmosphere: Helium $\rightarrow$ Air
- Temperature: $20^\circ\text{C} \rightarrow 15^\circ\text{C}$



HTR-10 Benchmarks

Example Results – Initial Criticality (B1)

	Original Benchmark Problems		Revised (Deviated) Benchmark Problems	
	Diffusion/Transport	Monte Carlo	Diffusion/Transport	Monte Carlo
China	125.8	126.1	122.558	122.874
France ¹	-	-	-	115.36 117.37
Germany ²	124.2 126.8	-	121.0 123.3	-
Indonesia ³	107 120	-	-	-
Japan	113	-	-	-
Netherlands	125.3	-	122.1	-
Russia	136	137.3	-	-
South Africa	-	-	122.537	-
Turkey ⁴	119.27	129.7 135.3	-	-
USA ⁵	-	127.5 128	-	-

Experimental result of critical loading height: 123.06cm. It is noted that the experimental conditions are those conditions for the revised (deviated) benchmarks except the temperature is 15°C instead of 20°C (or 27°C).

1. The first row of data is obtained with simplified PB modeling, and the second row of data with improved PB modeling.
2. The first row of data is obtained with 2-dimensional VSOP, and the second row of data with 3-dimensional VSOP.
3. The first row of data is obtained with the DELIGHT code, and the second row of data with SRAC code.
4. The first row of data in the Monte Carlo approach is obtained with the ENDF/B-IV nuclear data set, and the second row of data with ENDF/B-V nuclear data set.
5. The first row of data is obtained with the UTXS nuclear data set, and the second row of data with ENDF/B-VI nuclear data set.



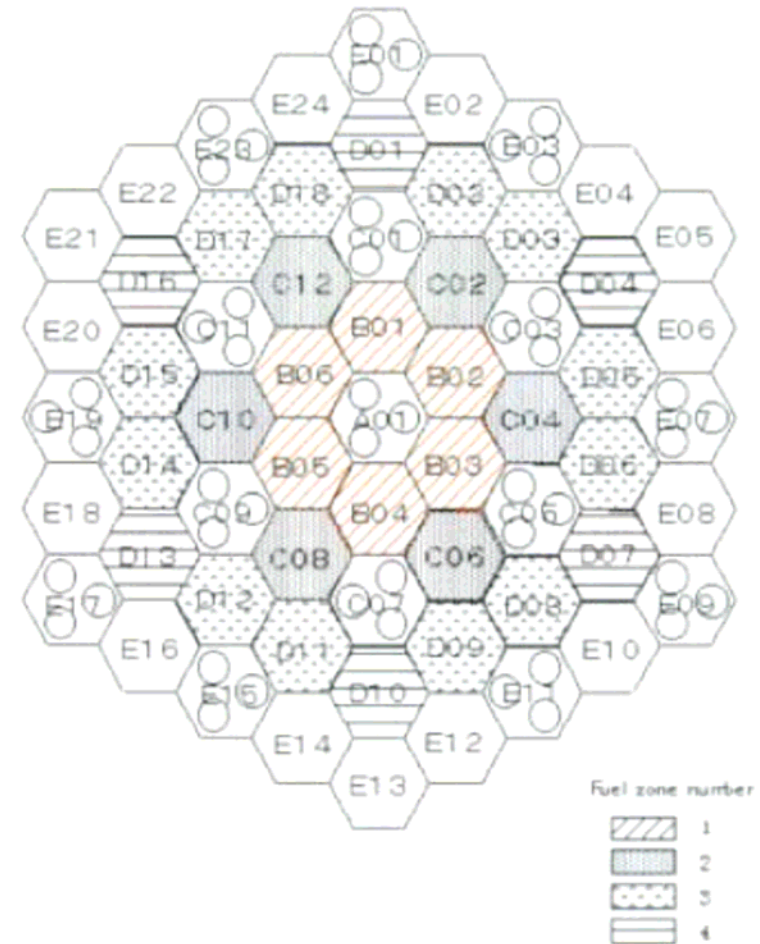
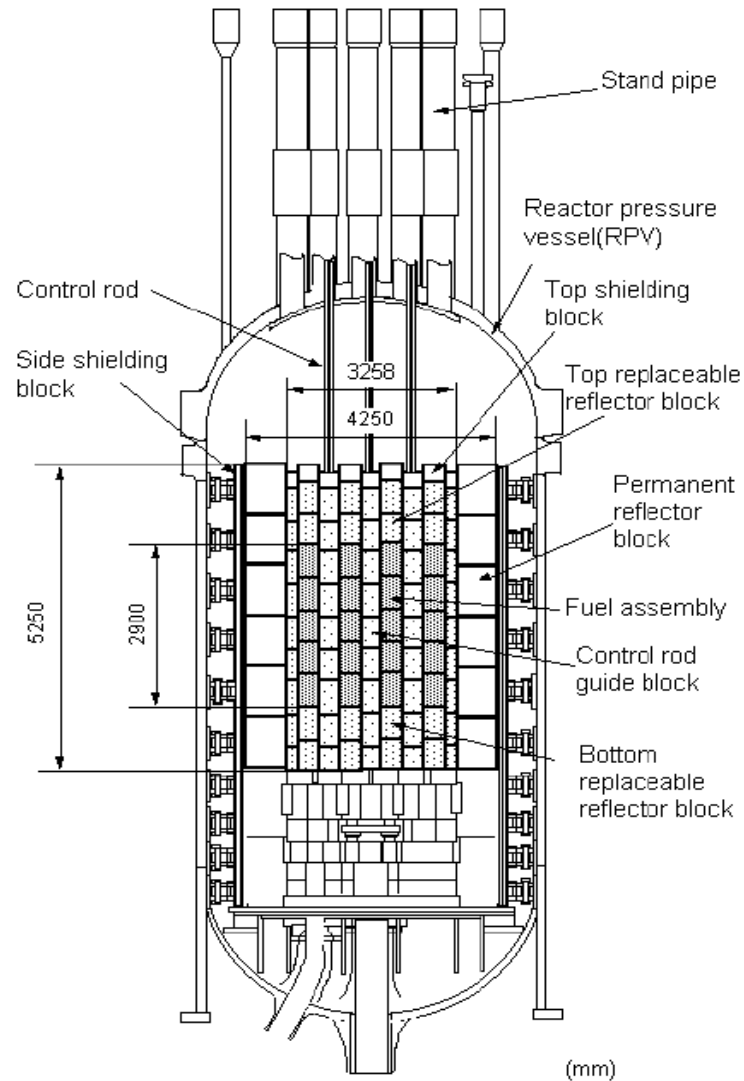
HTR-10 Benchmarks

Reasons for Differences in Results

- Some control rod cross section cell calculations more appropriate for rod array than single rod worth evaluations
- Uncertainty in the modeling of neutron streaming
- Choice of selected cross section library (JEFF, ENDF, JENDL, etc.)
- Water content of graphite pores
- Library dependent cross-sections for temperature coefficients
- Effective fuel homogenization methods
- Modeling of fuel with Monte Carlo Calculations
 - Explicit geometry (particle distribution in pebble, pebble distribution in core)
 - Modeling of fuel/dummy ball ratio



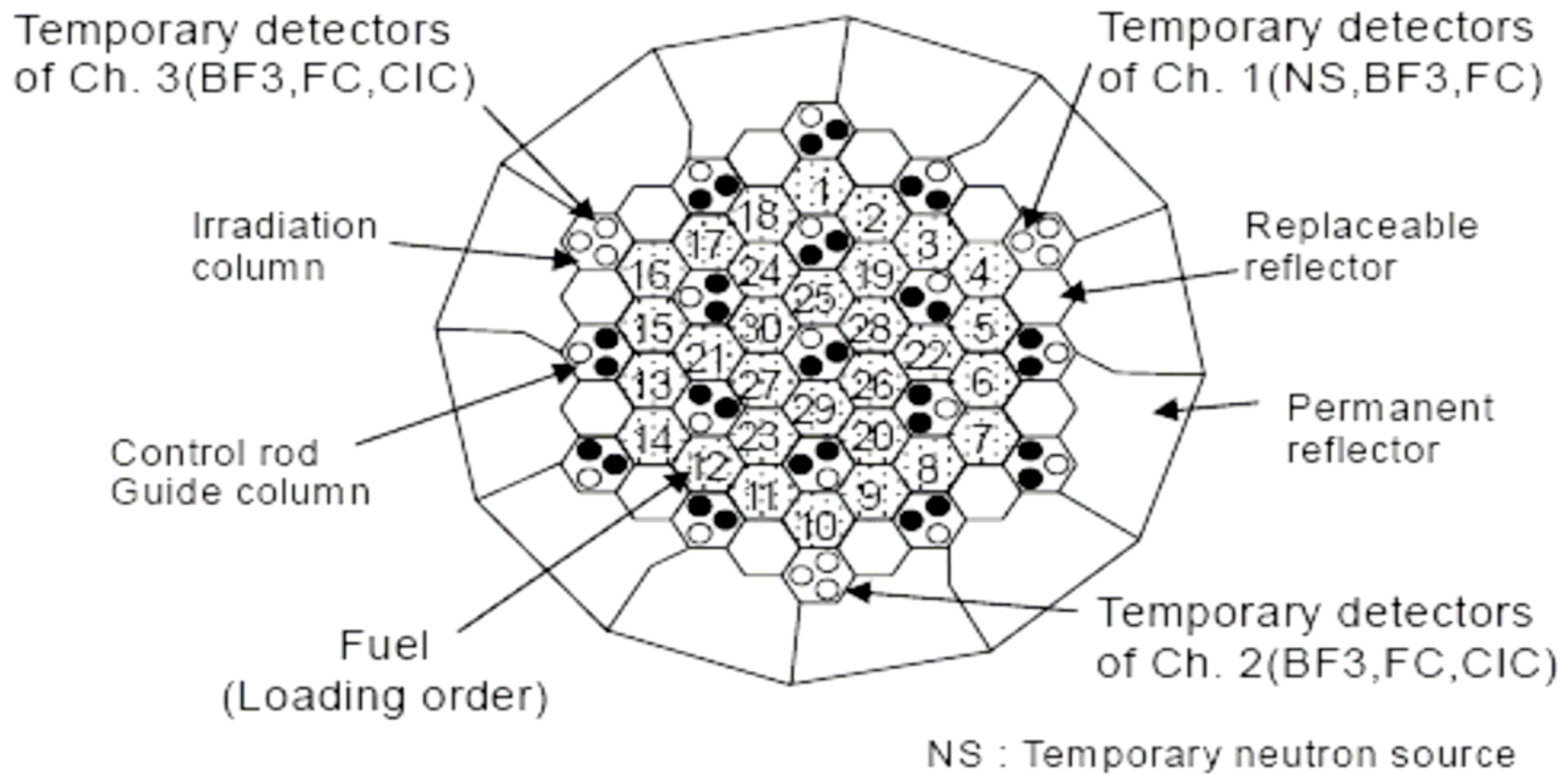
HTTR Benchmarks





HTTR Benchmarks

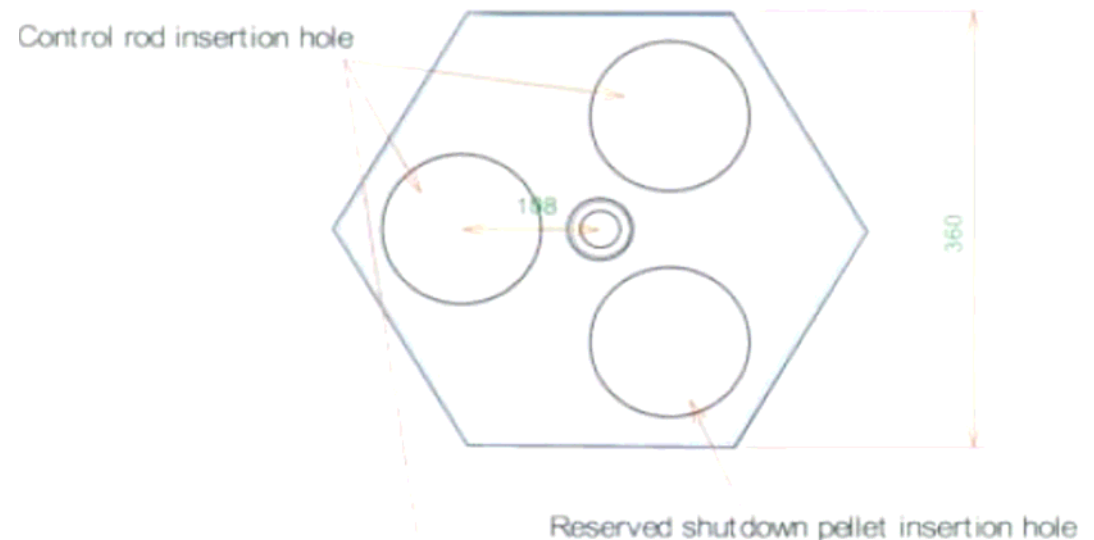
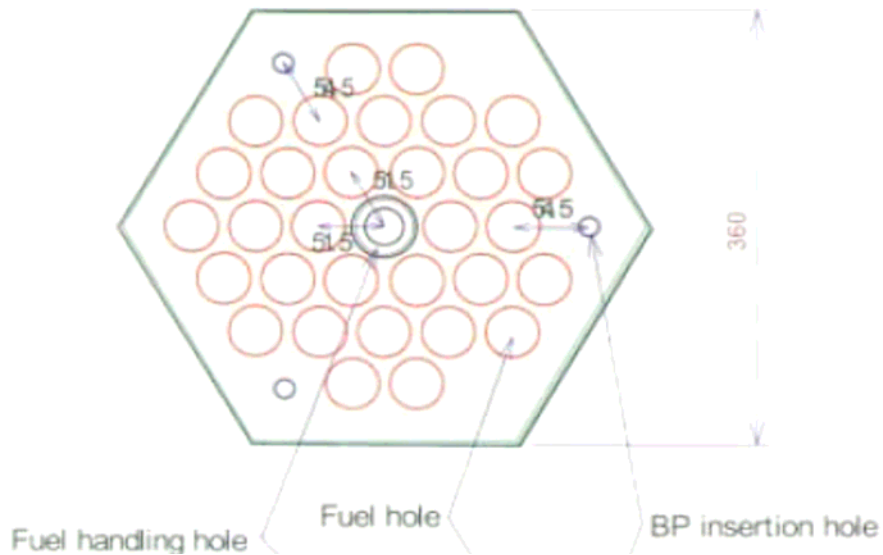
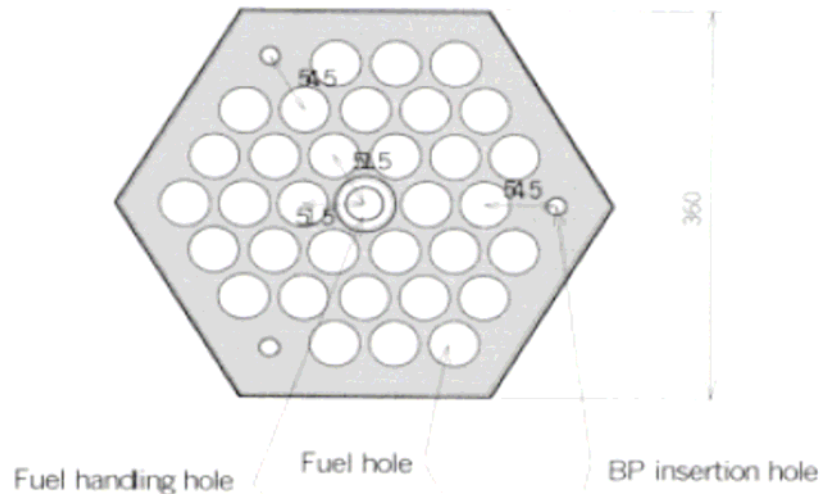
Core Cross Section with Fuel Block Loading Order





HTTR Benchmarks

Core Region Block Configurations





Fuel Compacts & Burnable Poison Pellets



HTTR Benchmarks

Analysis Methods – Diffusion Calculations

Items	Germany	Russia	Japan	Netherlands	
	FZJ	OKBM	HTTR	NRG	IRI
Nuc. Data File	JEF-2.2	ENDF/B6	ENDF/B-4	JEF2.2	JEF2.2
Fuel Cell Code	TOTMOS	WIMS-D/4	DELIGHT	WIMS	SCALE4
Theory	Col.	S4	Col.	Col.	Transport
Model	Cyl.	Cyl.	Cyl.	Cyl.	Cyl.
No. of Groups	123	69	40	69	172
BP Cell Code	TOTMOS DORT	WIMS-D/4	TWOTRAN	WIMS	SCALE4
Theory	Transport	S4	Transport	Col.	Transport
Model	Cyl.	Cyl.	Cyl.	Hex.	Cyl.
No. of Groups	123	69	6	16	172
Core Cal. Code	CITATION	JAR-3D	CITATION-1000VP	PANTHER	BOLD-VENTURE
Model	Tri. (24mesh)	Tri. (6 mesh)	Tri. (24mesh)	Hex.	
No. of Groups (Fast + Thermal)	26	1 + 1	6 (3+3)	2	13
Cut-off Energy (eV)	1.86	0.625	2.38	2.1	2.1

Col. = Collision Probability

Cyl. = Cylindrical



HTTR Benchmarks

Analysis Methods – Monte Carlo Calculations

Items	Russia		Japan	Netherlands	
	RRC KI	IBRAE	HTTR	NRG	IRI
Nuc. Data File	DLC/MCUDAT-1.0	ENDF/B6	JENDL-3.2	--	JEF2.2
Energy Struct.	Continuous	Continuous	Continuous		Group
Code	MCU	MCNP 4A	MVP	--	KENO V.a
History	200	2000 (up to 16000)	20000		10000
Batches	5000	1000	150		200
Skipped-Batches	1	10	5		1



HTTR Benchmarks

HTTR Benchmark Problems		
FC	Initial Criticality	Number of fuel blocks in sequenced loading
CR	Control Rod Position at Criticality	Control rod insertion depth at criticality for 18, 24 and 30 column core
EX	Excess Reactivity	Excess reactivity for an unrodded 18, 24 and 30 core
SC	Scram Reactivity	Scram reactivity for 1) all reflector CRs, 2) all CRs in reflector and core (30 column core)
TC	Isothermal Temperature Coefficient	Isothermal temperature coefficients at 290, 320, 360, 400, 440 and 470°C for 30 column core with control rod position for criticality at 480°C



HTTR Benchmarks

FC - Initial Criticality

Diffusion Calculations

Member state	Number of fuel columns	Keff	Excess(%dk/k)
Japan	17	1.0005	0.05
France	17	1.0061	0.61
Germany	18	1.008	0.79
Indonesia	18	1.0058	0.577
Russia (OKBM)	16	1.005	0.498
Experimental results	19		

Monte Carlo Calculations

Member state	Number of fuel columns	Keff	Excess(%dk/k)
Japan	18	1.0061	0.61
France	18	1.0085	0.85
Netherlands(IRI)	17	1.0062	0.62
Russia(IBRAE)	16	1.006	0.596
Russia(RRCKI)	17	1.004	0.398
Turkey	15	1.005	0.50
Experimental results	19		



HTTR Benchmarks

Reasons for Differences in Results

- Uncertainties in levels of impurities in dummy blocks, and in water and air or nitrogen in graphite pores
- Monte Carlo model geometry representation
- Choice of selected cross section data library and version (JEF, ENDF, JENDL, etc.)
- Uncertainties in modeling neutron streaming with diffusion methods
- Difficulties in modeling harmonics in thin annular cores with diffusion methods