



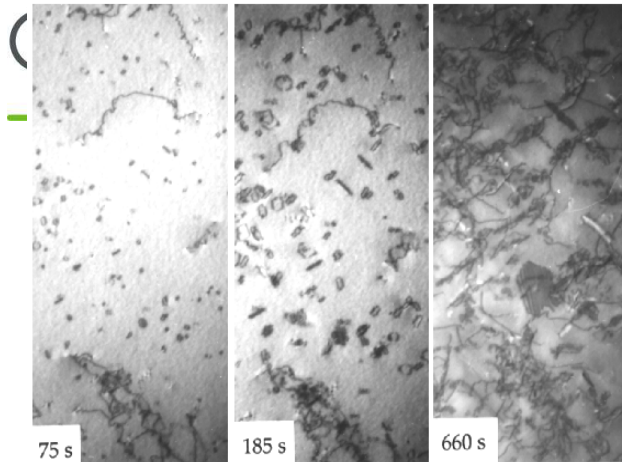
Rate theory – applications and comparison with experiments

(Barbu3)

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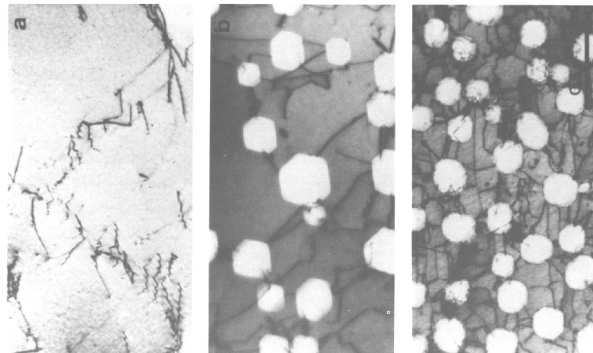
Microstructural evolution under irradiation

Point defects evolution



Dislocation network

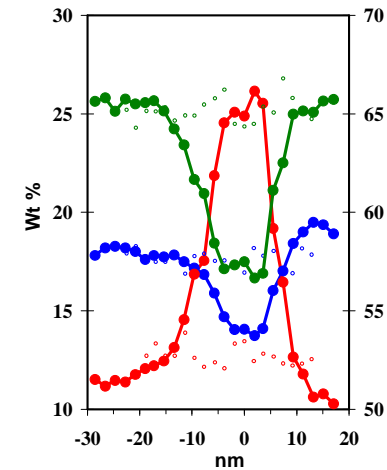
Nucleation and growth of dislocation loops
Dislocation climb



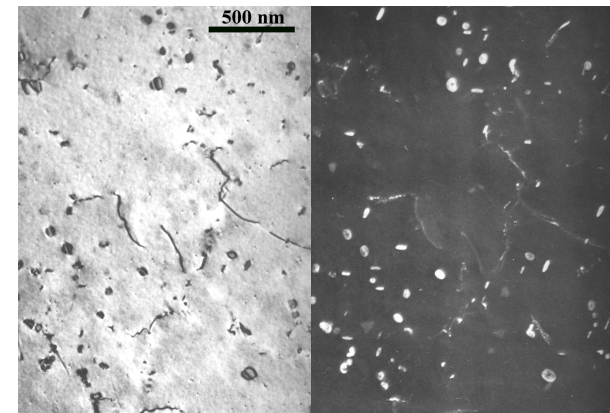
Nucleation and growth of voids

Microchemical evolution

Enhanced precipitation



Radiation induced segregation

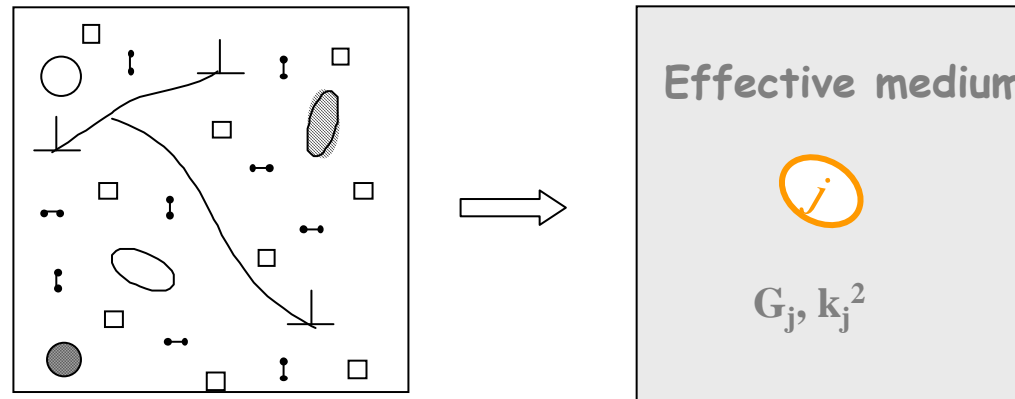


Radiation induced precipitation

Rate theory basis



- The actual material with its microstructure is replaced by an effective homogeneous medium.
- All processes occur continuously in space and time.
- The evolution of one object embedded in the effective medium is described by an ordinary differential equation (rate theory).
- The number density of objects must be low enough (dilute limit).



Object j embedded in the effective medium.

A simple case : only single point defects evolution



Constant microstructure assumption

elimination on sink of type p

creation recombination emission from sink of type p

$$\frac{\partial c_v}{\partial t} = G_v - R D_i c_i c_v - \sum_p k_{v,p}^2 D_v c_v + \sum_p k_{v,p}^2 D_v c_{v,p}^e$$
$$\frac{\partial c_i}{\partial t} = G_i - R D_i c_i c_v - \sum_p k_{i,p}^2 D_i c_i$$

The whole physics is contained in the rate coefficients G , D , k

Rate constant calculations



1. The point defect flux towards the considered sink is calculated by resolving the diffusion equation at stationary state with limit conditions properly chosen.
2. Integration over the « surface of the sink ».
3. Multiplication by the « number density » of the considered sinks.

Example: Cavity sink strength

Simplest method



Point defect captured by a voids made of n vacancies :

$\nabla^2 C_v = 0$

$C_v = C_{v,c}^e \quad \text{at} \quad r_{nv}^v$
 $C_v = C_v \quad \text{at} \quad R$

$I_{nv}^{0v} = 4\pi r_{nv}^v D_v (c_v - c_{v,c}^e) \quad r_{nv}^v \text{ capture radius}$

$I_{nv}^{0v} = I_{nv}^{0\beta v} - I_{nv}^{0\alpha v}$

$I_{nv}^{0\beta v} = 4\pi r_{nv}^v D_v c_v$
 $I_{nv}^{0\alpha v} = 4\pi r_{nv}^v D_v c_{v,c}^e$

absorption emission

Then: $k_{v,nv}^2 = 4\pi r_{nv}^v C_{nv}$

Where C_{nv} is the number density of cavities containing n vacancies.

Cavity sink strength

Self consistent method (R. Bullough)



Cavity of radius r_{nv}^v now embedded in an effective medium in which vacancy are homogeneously created at a rate G_v and that contained sinks for vacancy of sink strength k_v^2 .

$$\nabla^2 C_v - D_v k_v^2 c_v + G_v = 0$$



$$k_{v,nv}^2 = 4\pi r_{nv}^v C_{nv} (1 + k_v r_{nv}^v)$$



Multi-sink correction

often negligible in actual conditions.

Bias coefficient



If interaction energy E_α between the point defect of α type and the object, capture coefficient solution of :

$$\nabla^2 C_\alpha + \frac{1}{kT} \nabla C_\alpha \nabla E_\alpha = 0$$

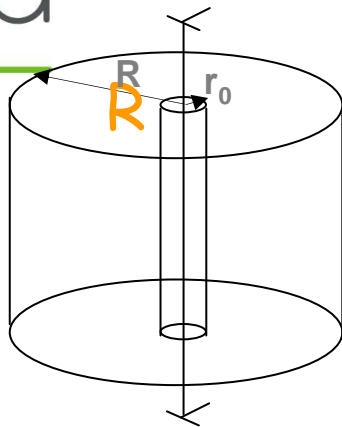
Instead of calculating the interaction energy the interaction very often treated phenomenologically by **multiplying the capture radius** by a **coefficient Z**

$$k_{\beta, n\alpha}^2 = 4\pi r_{n\alpha}^\beta Z_{n\alpha}^\beta C_{n\alpha}$$

$Z_{n\alpha}^\beta$ **bias coefficient of the object . $n\alpha$ for point defects of type β**

Dislocations sink strength

cea



$$k_{d,\alpha}^2 = Z_d^\alpha \rho_d, \quad \text{with } \rho_d \text{ dislocation density}$$

If no interaction between point defect α and dislocation:

$$Z_d^\alpha = \frac{2\pi\rho_d}{\ln(R/r_0)} \quad \text{with} \quad R \cong (\pi\rho_d)^{-1/2}$$

If significant interaction:

$$Z_d^\alpha = \frac{2\pi\rho_d}{\ln(R/r_d^\alpha)} \quad r_d^\alpha = \frac{\mu b(1+\nu)V_\alpha^r}{6(1-\nu)\pi kT} \quad \text{with } V_\alpha^r \text{ relaxation volume of the point defect of } \alpha \text{ type.}$$

- not only proportional to the sink density
- an additional term contains also the sink density = the multi-sink correction.

Often simplified: as the relaxation volume is considerably larger for interstitial than for vacancy $Z_d^v = 1$ and $Z_d^i = 1.1$ or 1.2

Grain boundary sink strength



For the point defects of α type

$$k_{gb,\alpha}^2 = \frac{6k_\alpha}{d}$$

With k_α the total sinks strength of the effective medium for the point defect α

The multi sink effect cannot be ignored for grain boundaries.

Properties of point defect: reminding

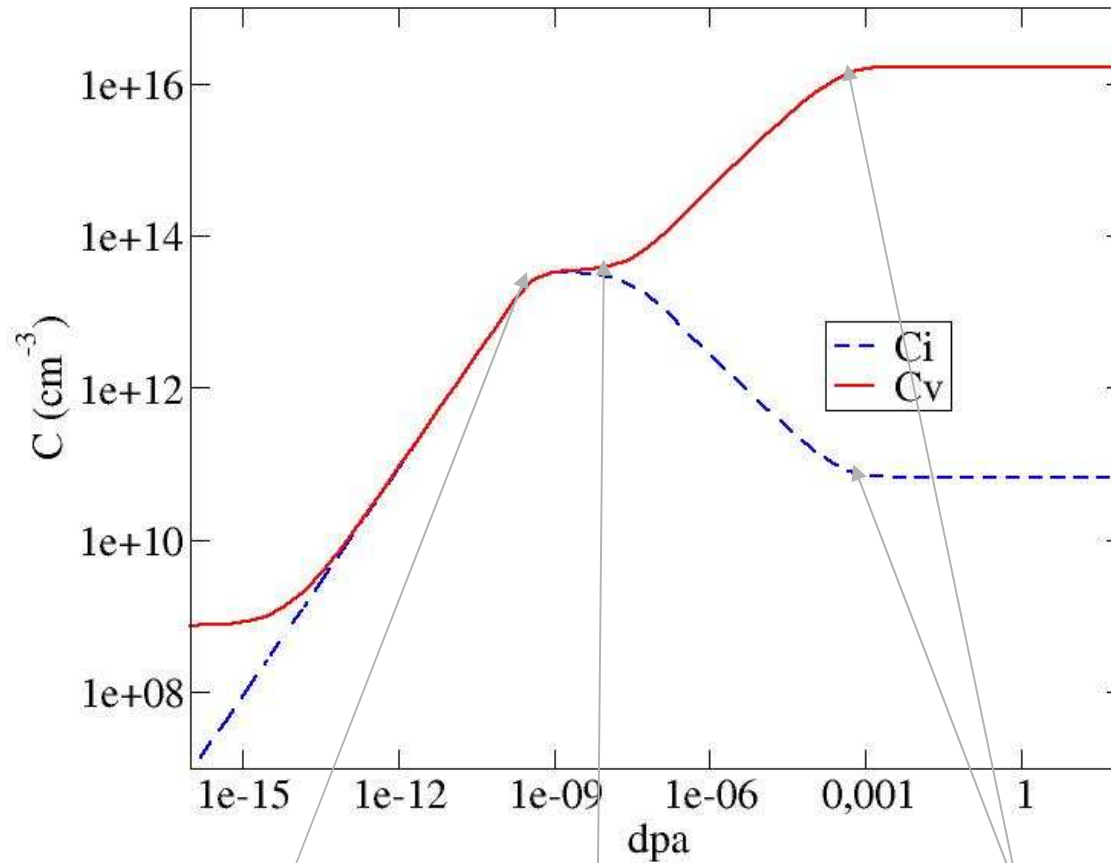


	H_v^f	H_v^m	V_v^r	H_i^f	H_i^m	V_i^r
Ni	1.6	1.1	-.20	≈ 4.0	0.15	1.8
Fe	1.6 (2.0)	1.3 (0.6)	-.20	≈ 4.0	0.3	1.1
Zr	>1.35	.7 ?	-.05	?	0.26	.6

Exemples de paramètres caractérisant les DP dans Ni, Fe et Zr.
(Laudolt-Börnstein, Wollenberger 1983 et Ehrhart et al 1986).

Calculated single point defect evolution in iron

Iron, $2 \cdot 10^{-8}$ dpa/s, 300°C, low dislocation density..



Recombination beginning

SIA reach the sinks

vacancies reach the sinks

Point defect: stationary state



If $c_{v,p}^e \ll c_v \quad \forall p$

Stationary state satisfies $D_v c_v \sum_p k_{v,p}^2 = D_i c_i \sum_p k_{i,p}^2$

Point defect stationary concentrations

-

- Sink dominant regime :

-

$$c_v = \frac{G}{D_v \sum_p k_{v,p}^2} \quad c_i = \frac{G}{D_i \sum_p k_{i,p}^2}$$

- Recombination dominant regime :

$$c_v = \left(\frac{G \sum_p k_{i,p}^2}{RD_v \sum_p k_{v,p}^2} \right)^{1/2} \quad c_i = \left(\frac{GD_v \sum_p k_{v,p}^2}{RD_i^2 \sum_p k_{i,p}^2} \right)^{1/2}$$

-

Growth velocity of point defect clusters at point defect at stationary state



If dislocations are the dominant sinks

Stationary state

$$Z_d^v D_v c_v = Z_d^i D_i c_i$$

Growth velocity of a void of radius r_c

$$\frac{dr_c}{dt} = \frac{\Omega}{r_c} \{Z_c^v D_v c_v - Z_c^i D_i c_i\}$$



$$\frac{dr_c}{dt} = \frac{\Omega}{r_c} \frac{Z_d^i - Z_d^v}{Z_d^i} D_v c_v$$

as for void $Z_c^v \approx Z_c^i = 1$

If the mean bias of the medium is the same as bias coefficient for voids (the object we are here interested by):

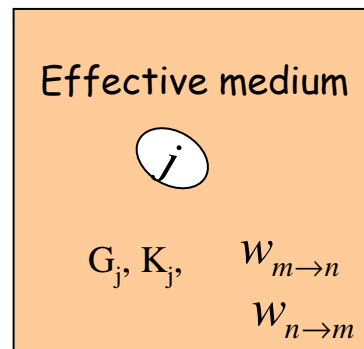
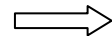
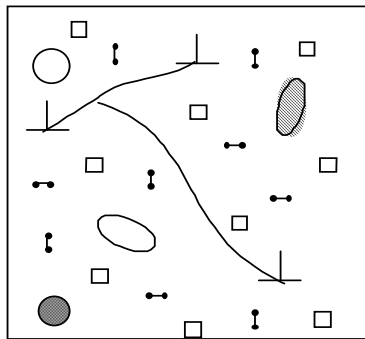
$$\frac{dr_c}{dt} = 0$$

Rate theory for the clustering of point defects : cluster dynamics



- Based on rate theory
- Gas of clusters embedded in an effective homogeneous medium → Only applicable to diluted object
- Positions of the objects are not considered: (Price to pay to reach large fluences considering a representative volume of materials).

Evolution of the number density of a cluster of j kind



Object j embedded in the effective medium.
(j = nature, size, composition, etc. of the clusters)

$$\frac{dC_n}{dt} = \sum_m J_{m \rightarrow n} - \sum_q J_{n \rightarrow q} + G_n - K_n C_n$$

In principle able to treat nucleation, growth and coarsening of point defect clusters or precipitates (homogeneous precipitation)

Basic master equation



$$J_{m \rightarrow n} = \sum_m w_{m \rightarrow n} C_m$$



$$\frac{dC_n}{dt} = G_n + \sum_m w_{m \rightarrow n} C_m - \sum_q w_{n \rightarrow q} C_n - K_n C_n$$

All the physics is contained in the coefficients $G(j)$, $w(k,j)$, K_j

In principle as many equations as kind of cluster j (size, nature)

But N_{\max} (cluster sizes) = number of differential equations limited by the ability of computer and by the CPU time.

Treatment of large clusters

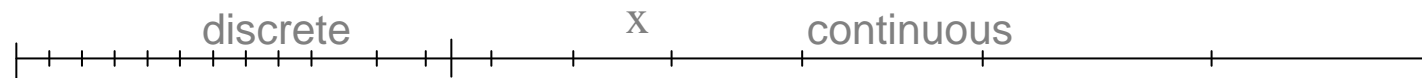
To reach large cluster sizes (>2nm), two methods:



- Transformation of the discrete general equation into a continuous Fokker-Planck type equation:

$$\frac{\partial C(x)}{\partial t} = \frac{\partial}{\partial x} [f(x)C(x)] + \frac{\partial^2}{\partial x^2} [d(x)C(x)]$$

To solve the continuous equation: Discretized with Δx increasing with x



New numerical scheme always stable © V. Duwig et al.

Grouping method: a group represented by one element. Golubov (2001)

Distribution characterize only by:

- The first moment of the distribution (conservation of the cluster number)
- The second moment of the distribution (matter conservation)

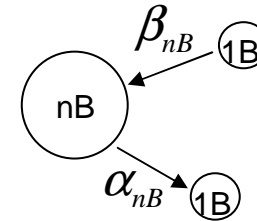
Two times more equations.

A simple case : precipitation in dilute solid solution



- only single B atoms are mobile
- only single B atoms can be emitted from a precipitate
- spherical precipitates of n solute atoms

$$J_{m_B \rightarrow n_B} = \beta_{n_B} C_{1_B} C_{n_B} - \alpha_{n_B+1} C_{n_B+1}$$



$$\beta_{n_B} = 4\pi r_{n_B} D_{1_B}$$

$$\alpha_{n_B} = 4\pi r_{n_B-1} \frac{D_1}{\Omega} \exp\left[\frac{(G_{n_B} - G_{n_B-1} - G_1)}{kT}\right]$$

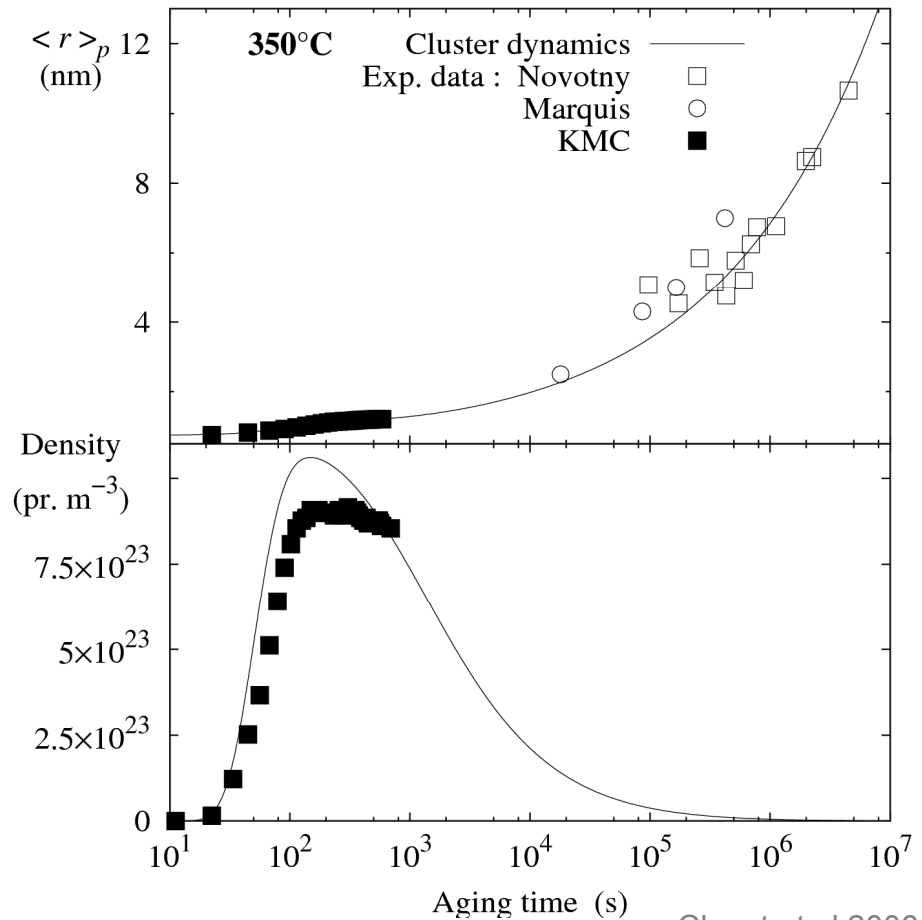
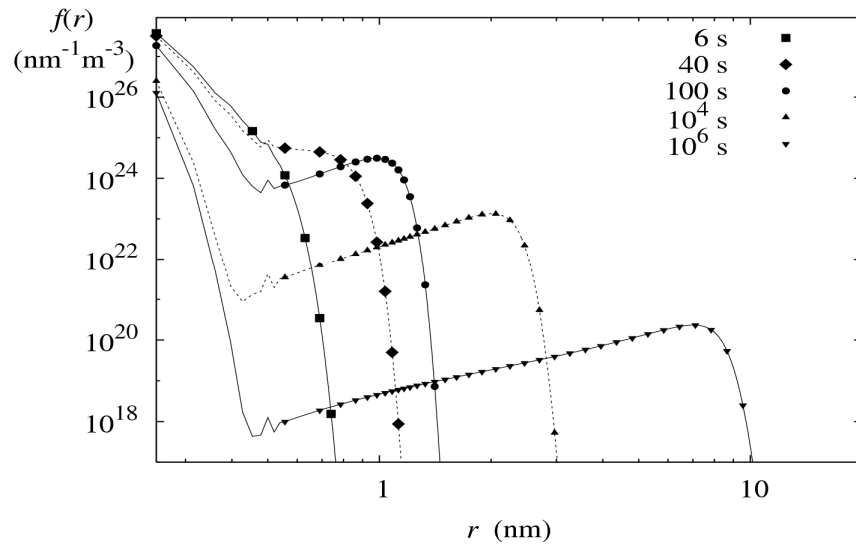
Capillary model

$$G_{n_B} = 2n_B \mu(C_B^0) + \frac{n_B}{C_p} \Delta G^{nuc}(C_B^0) + (576\pi\Omega^2)^{2/3} n_B^{2/3} \sigma_{n_B}$$

$$\alpha_{n_B} = 4\pi r_{n_B-1} \frac{D_1}{\Omega} \exp\left[\frac{(576\pi\Omega^2)^{1/3} \{n_B^{2/3} \sigma_{n_B} - (n_B - 1)\sigma_{n_B-1} - \sigma_{1_B}\}}{kT}\right]$$

α_{n_B} independent of ΔG^{nuc}

Al₃Sc precipitation in AlSc0.18at% solid solution



Clouet et al 2006

Point defect clustering under irradiation.

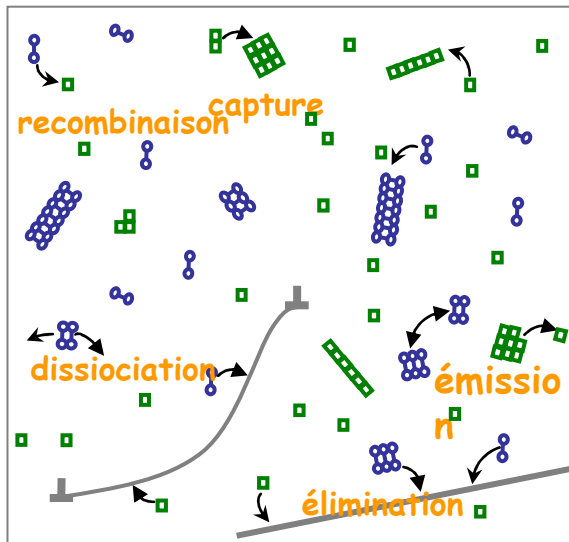
Point defects are not conservative : creation and elimination



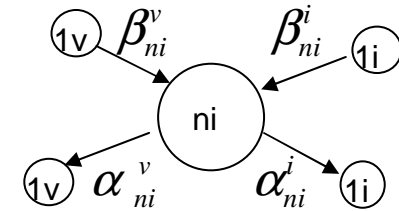
OBJECTS

SIA clusters = dislocation loops

Vacancy clusters = dislocation loops, voids, stacking fault tetrahedra



Typical ODE in a simple case: only SIA's and vacancies are 3D mobile

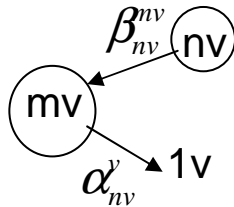


$$\frac{dC_{ni}}{dt} = G_{ni} + (\beta_{(n-1)i}^i C_{1i}) C_{(n-1)i} + (\beta_{(n+1)i}^v C_{1v} + \alpha_{(n+1)i}^i) C_{(n+1)i} - (\alpha_{ni}^i + \beta_{ni}^v C_{1v} + \beta_{ni}^i C_{1i}) C_{ni}$$

$$\frac{dC_{1i}}{dt} = G_{1i} + \beta_{2i}^v C_{1v} C_{2i} - C_{1i} \sum_{m=1} \beta_{mi}^i C_{mi} - \beta_{1i}^i C_{1i}^2 - C_{1i} \sum_{m=1} \beta_{mv}^i C_{mv} - \beta_{1i}^v C_{1i} C_{1v} + \sum_{m=2} \alpha_{mi}^i C_{mi} + \alpha_{2i}^i C_{2i} + \sum_{m=2} \alpha_{mv}^i C_{mv} - K_i C_{1i}$$

If cluster are 3D mobile, equations simply more complicate

Kinetic coefficient for 3D mobile objects



Capture and emission by point defect clusters

$$\beta_{nv}^{mv} = 4\pi r_{nv}^{mv} (D_{nv} + D_{mv})$$

$$\alpha_{nv}^v = 4\pi r_{(n-1)v}^v D_v \exp(-E_{nv}^B / kT)$$

r_{nv}^{mv} = reaction radius \neq of the actual radius of the objects

If elastic interaction between reacting objects (bias coefficient) in r_{nv}^{mv}

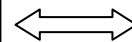
Important parameters

External: T, G_n

Material:

Mobility: $D_n = D_{n0} \exp(-E_n^m / kT)$

Formation energy of clusters: E_n^f

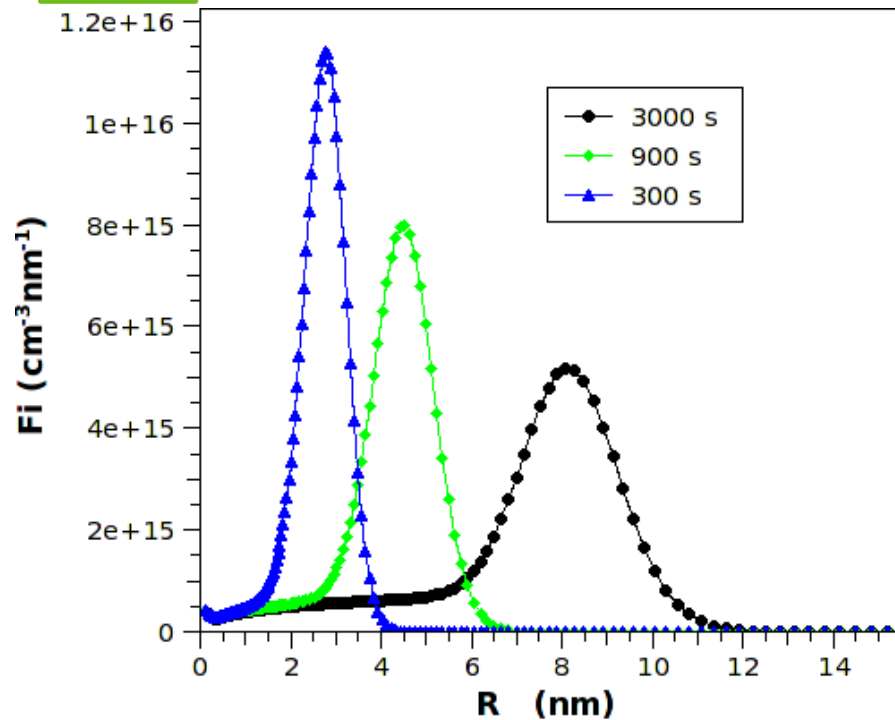


Further approximation to reduce the number of parameters

$$E_n^f = \frac{E^f - E_2^B}{2^{2/3} - 1} n^{2/3}$$

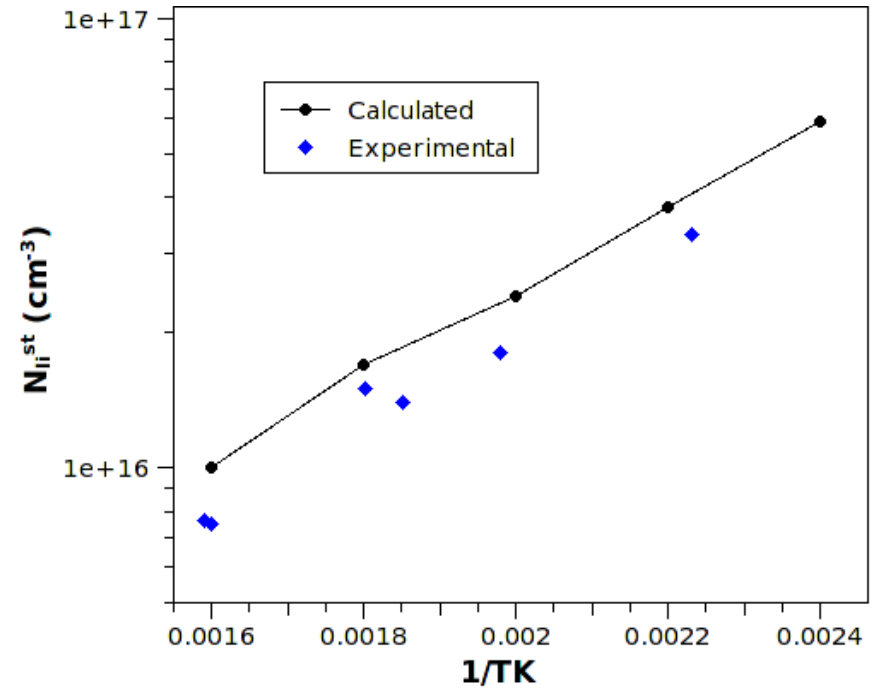
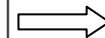
Continuous isothermal irradiation.

Point defect clusters in the FeCu 0.1 at% continuously irradiated with 1 MeV electrons.



Interstitial loop distributions

Only single SIA and single-vacancies mobile.



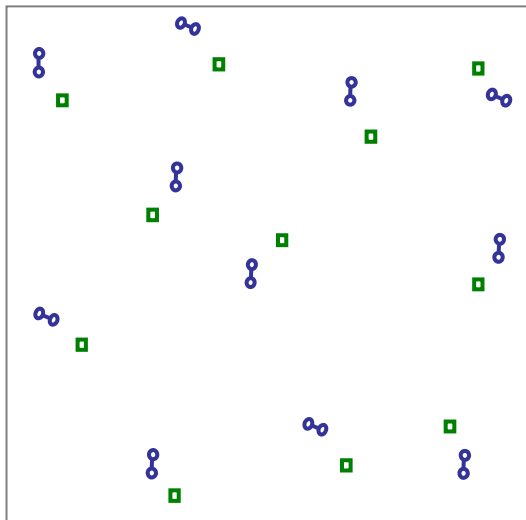
Emi (eV)	EB2i (eV)	Emv (eV)
0.3	1.2	1.36

Effect of spatial correlations

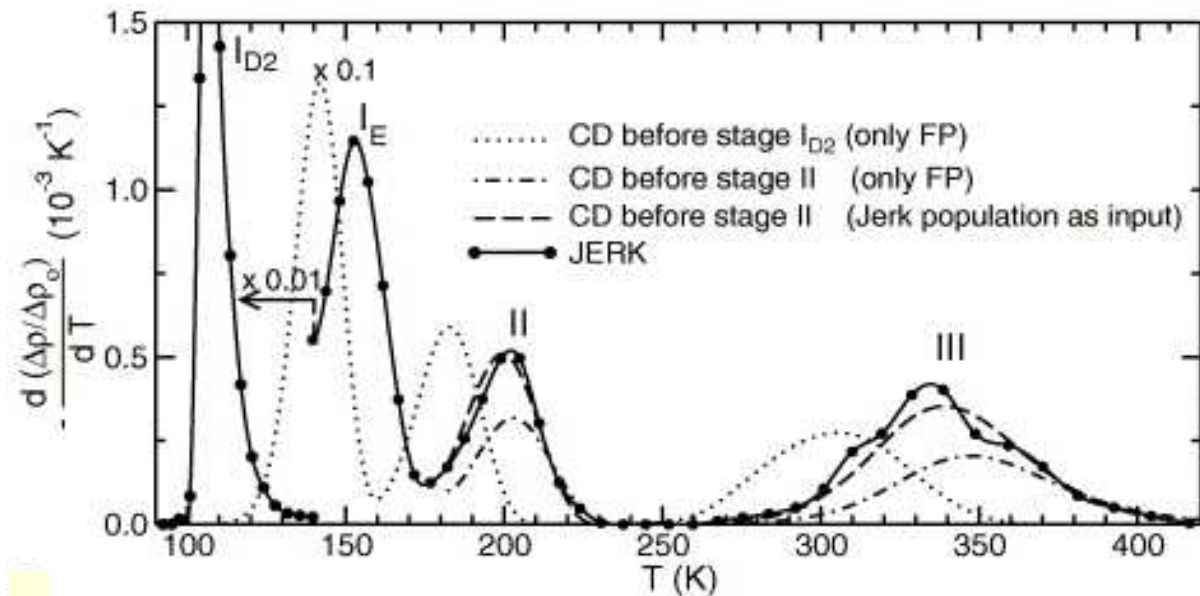
— A full multi-scale modeling: isochronal recovery of ultra pure Fe electron irradiated at 4K.



Comparison between CD, KMC.



Correlations between vacancies and SIA even under electron irradiation

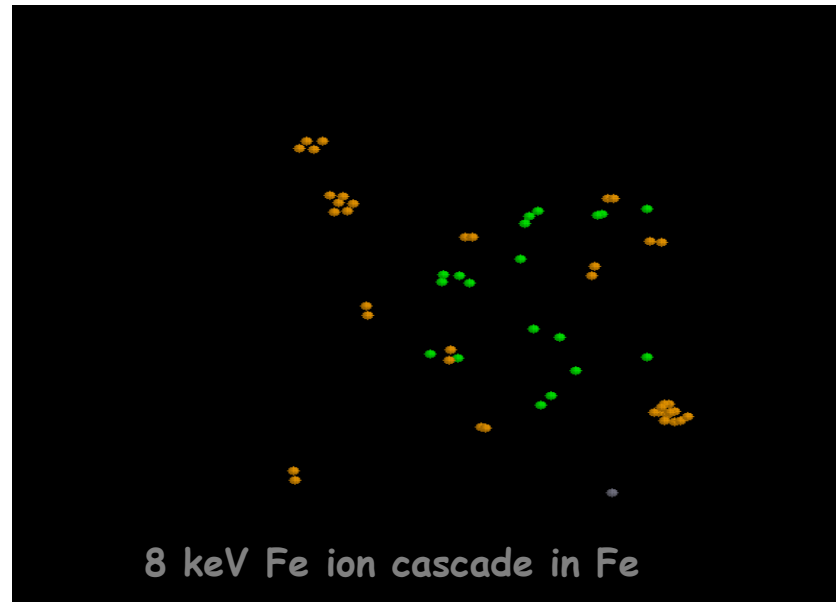


CD given good results only if a short KMC annealing at stage I is performed to erase correlations.

Displacement cascade correlations



Strong correlations in displacement cascades
(neutron and ion irradiations)



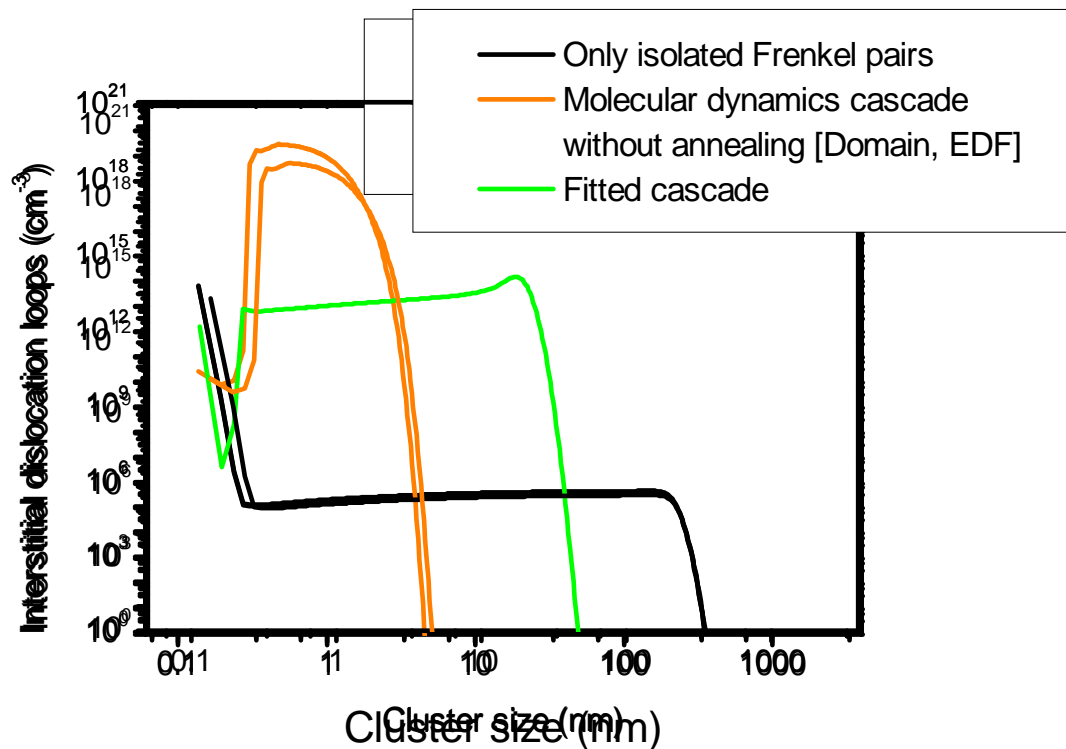
The point defect cluster distribution cannot be directly taken as the point defect sources in RT equations.

Necessity to carried out a KMC pre-annealing of the cascade to minimize the correlations.

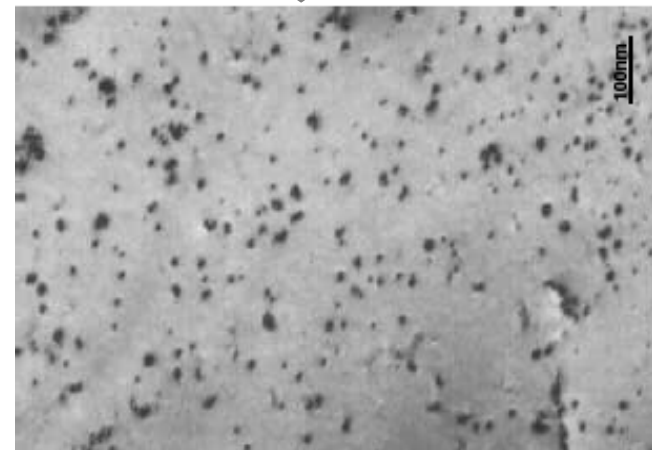
Example: point defect clusters in neutron irradiated iron



Parameters for small point defect clusters from ab initio calculations.

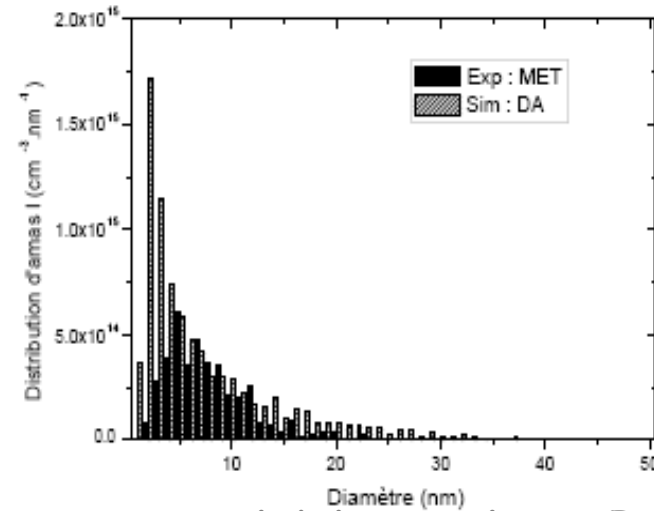
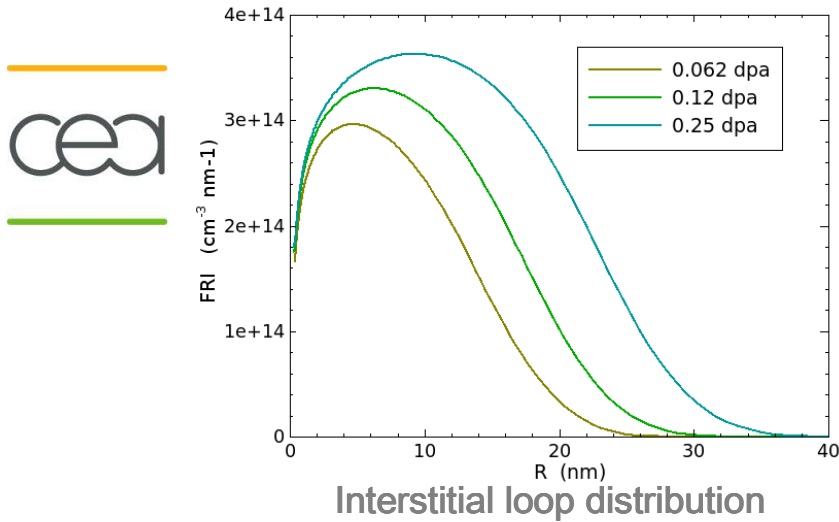


- Only Frenkel pairs
- Molecular dynamics cascades
- Fitted source term on experiments (Kr 2 MeV ions and BR2 neutrons)

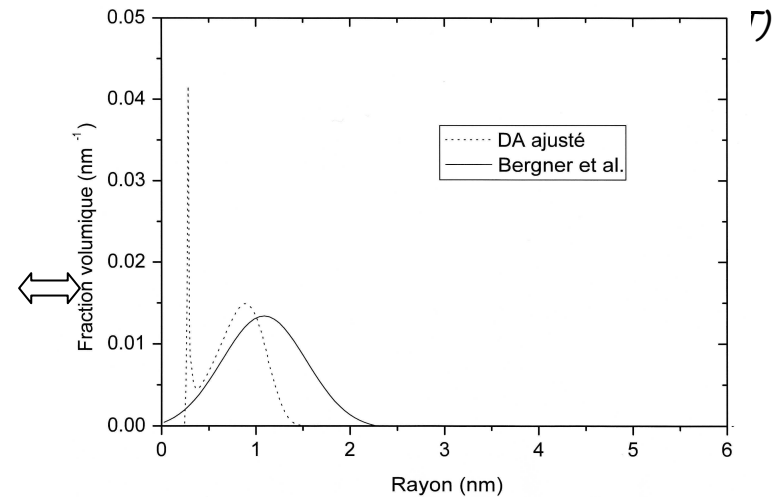
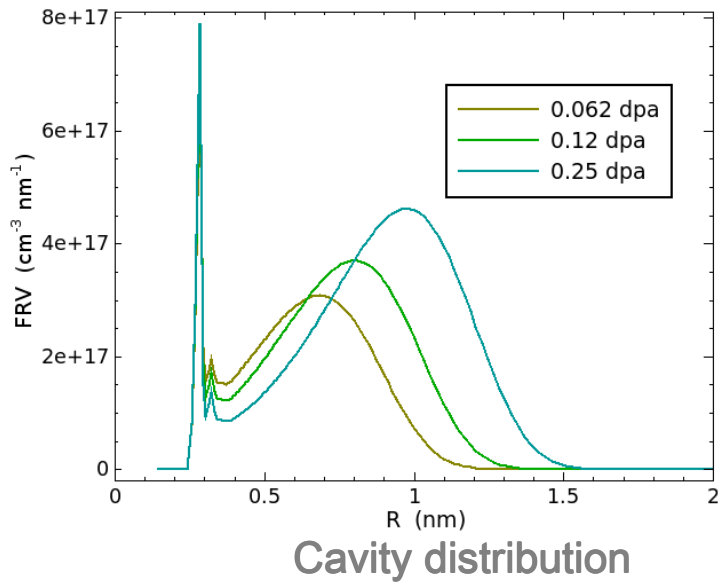


Interstitial dislocation loops, Fe, 300°C, BR2
(M. Hernandez CIEMAT)

Neutron irradiated iron (2)



Interstitial dislocation loops. Fe. 300°C, BR2



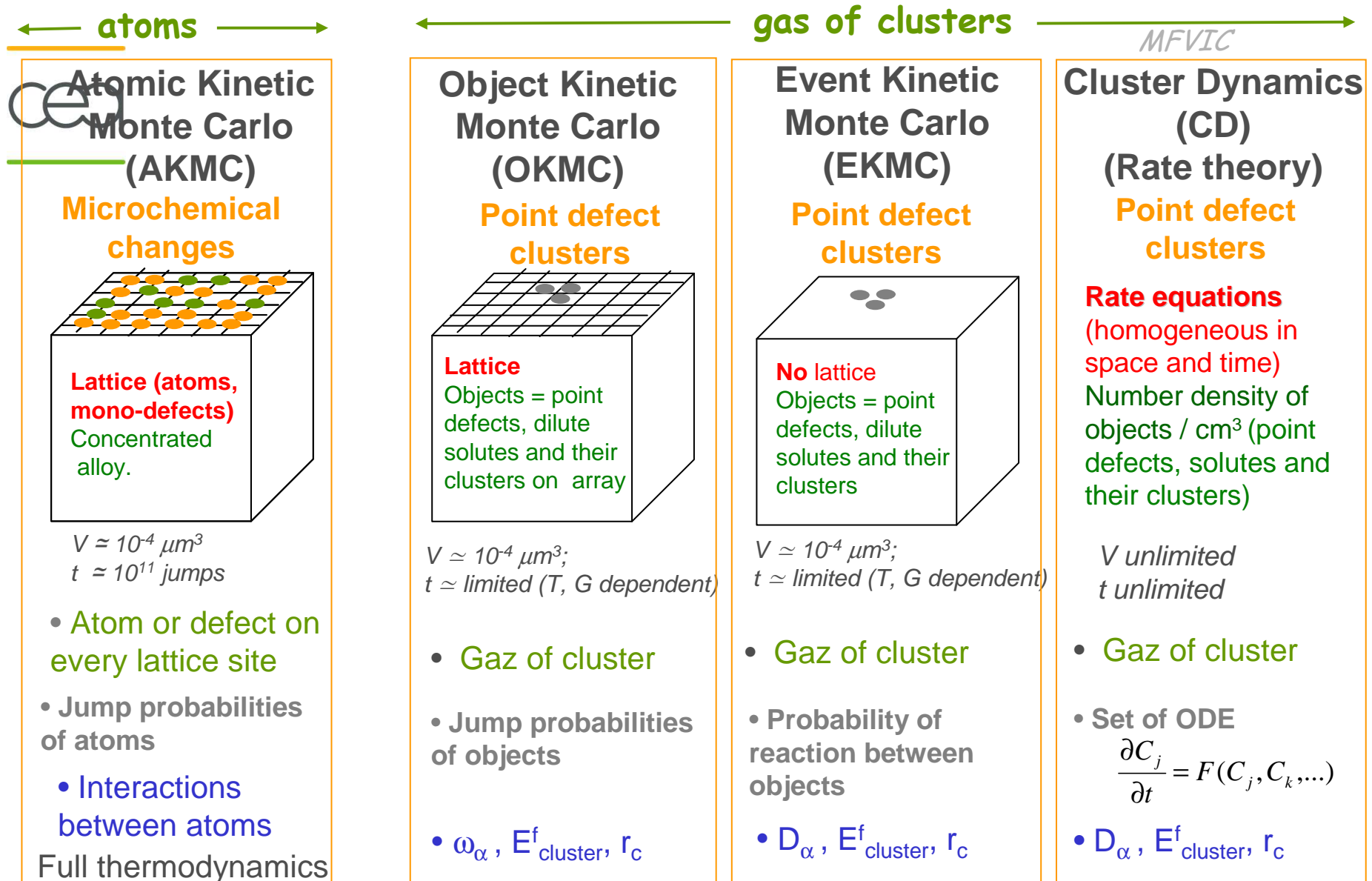
Comparison with experimental (SANS) vacancy distribution

Conclusion



- **Cluster dynamics (based on rate equations) modeling remains a very interesting method to simulate the long term evolution of materials.**
- **Low computational cost compared to OKMC**
- **Allows very long time evolution of a representative volume of materials impossible to obtain with KMC.**
- **Being based on an homogenization procedure, care must be taken when spatial correlations are important.**

Long term evolution modeling of clusters



Long term evolution modeling: precipitation, segregation

