The Abdus Salam
International Centre for Theoretical Physics

United Nations
Educational, Scientific and
Cultural Organization

IAEA
International Atomic Energy Agency

2018-31

Winter College on Optics in Environmental Science

2 - 18 February 2009

Atmospheric Monitoring TDLS
- parts I and II -

Werle P.

Research Centre Karlsruhe
Germany

Forschungszentrum Karlsruhe
in der Helmholtz-Gemeinschaft

Institut für Meteorologie und Klimaforschung

INOA

KIT Karlsruhe Institute of Technology

Winter College on Optics in Environmental Science

February 2-13, 2009 - Trieste, Italy

Atmospheric Monitoring with Tunable Diode Lasers

Peter Werle

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National Institute for Applied Optics, CNR-INOA, Florence, Italy

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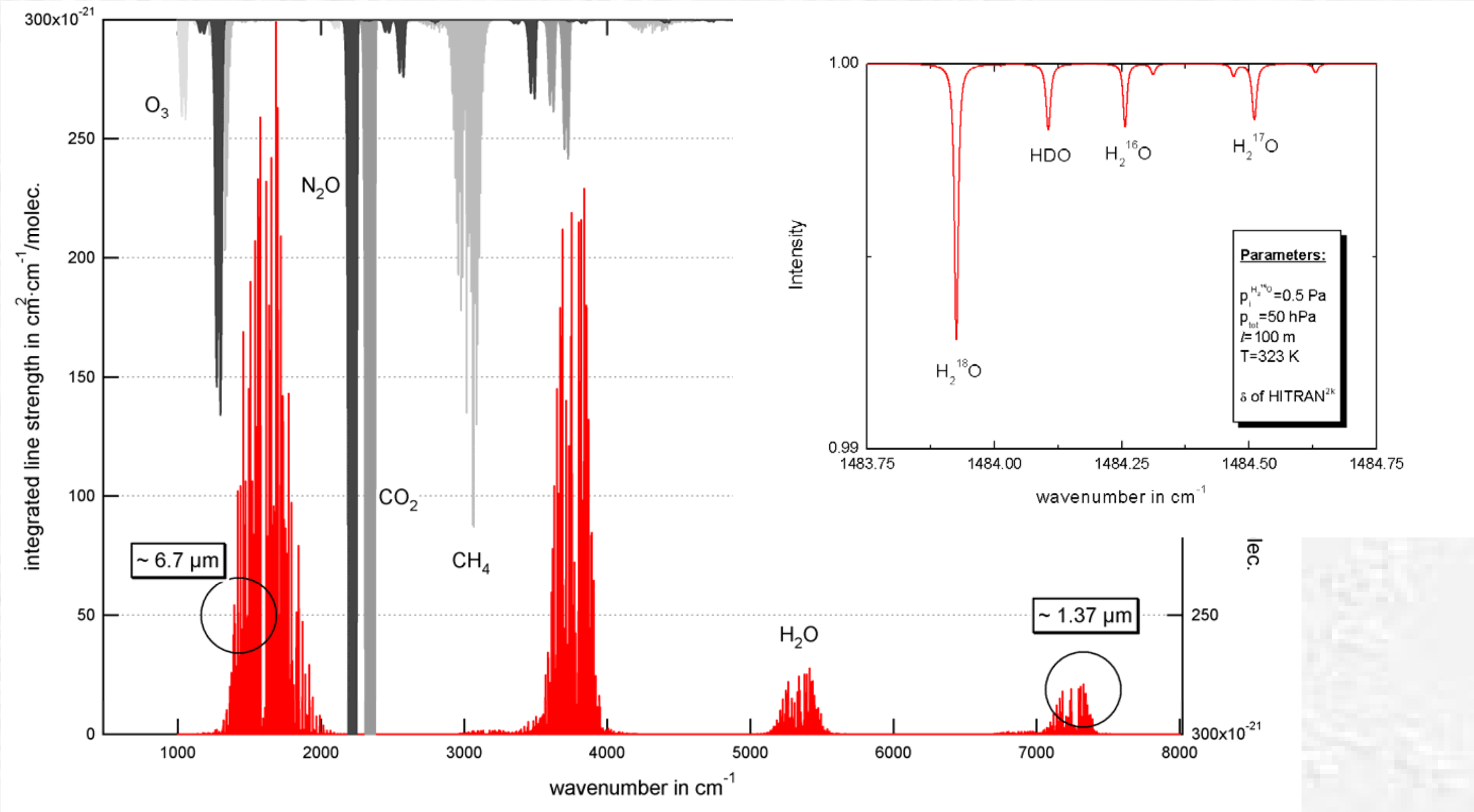
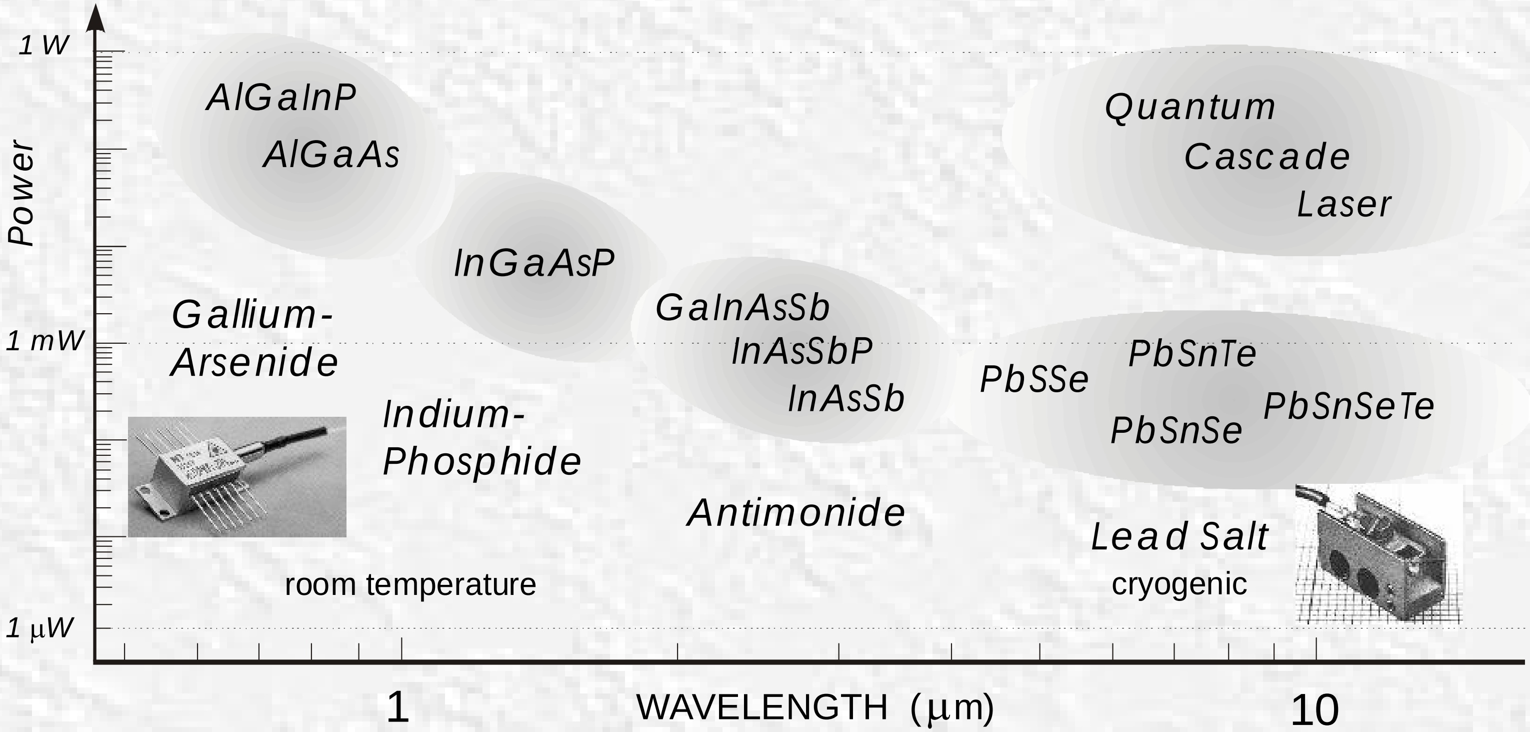
H_2O - Fingerprints

Spectral signatures in the near- and mid-infrared allow a unique quantitative identifikation of trace gases



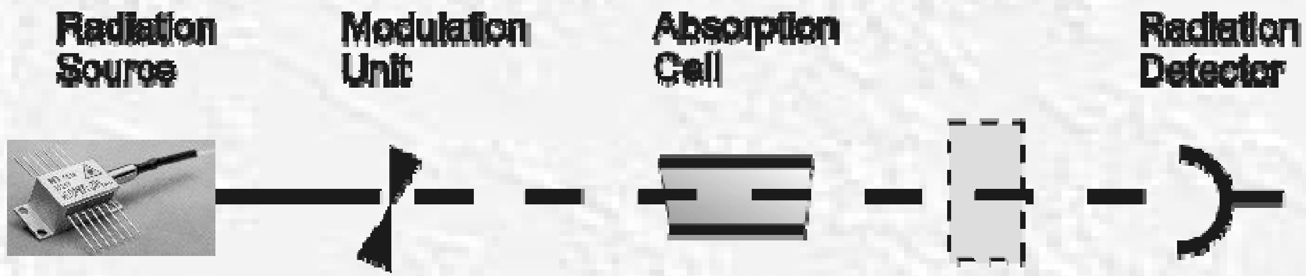
Semiconductor Lasers

Relevant Characteristics for Gas Sensing



- **Wavelength Range**
- **Output Power**
- **Noise Characteristics**
- **Far- Field / Beam Profile**
- **Impedance**
- **Temperature Range**

Optical Gas Analysis



Laser-Spectrometer

Gasfilter-Korrelator

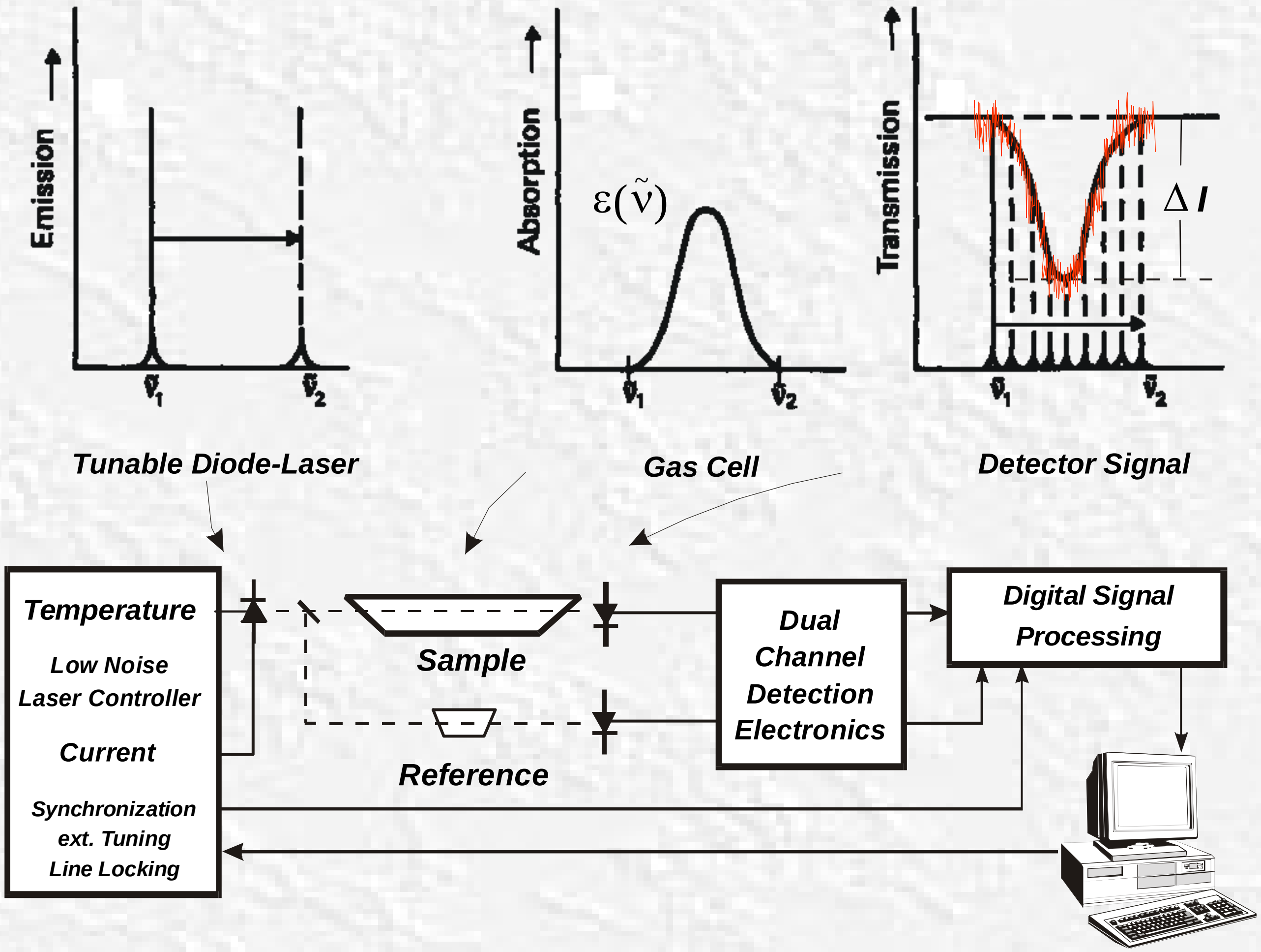
Monochromator
Interferometer
DOAS, FTIR

Opto-pneumatic
Detector NDIR
(Lehrer-Luft)

Specifity !

insert selective element

Laser Spectroscopy



Lambert-Beer´s Law

$$I(\nu) = I_0(\nu)\, e^{-\varepsilon(\nu)\, c\, l}$$

in the limit of low extinction : $\varepsilon(\nu)\, c\, l \ll 1$

$$c = \frac{1}{\varepsilon(\tilde{\nu})\;\; l} \left(\frac{\Delta I(\tilde{\nu})}{I_0(\tilde{\nu})} \right)$$

Apply sensitive measurement technique with sufficient detection limits
(e.g. 10^{-5} with **modulation schemes**)

*P. Werle, "**A review of recent advances in semiconductor laser based gas monitors**", Spectrochimica Acta A - Review 54, 197-236, (1998) (for paper click here)*

Select strong absorption line (e.g. from **HITRAN** Database) and check interferences !

Use long optical pathlength
(White/Herriott **multi-pass cells**, e.g. 100m)

A Cryogenically Operated Laser Diode (COLD)

S. Viciani, F. D'Amato, P. Mazzinghi, F. Castagnoli, G. Toci, P. Werle, Appl. Phys. B90, 581-592 (2008) View-PDF

Laser sources:

single mode FP lead salt TDL

λ = 5.8 µm for HNO_3 and H_2O

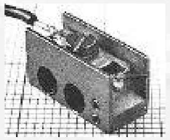
λ = 4.6 µm for N_2O and CO

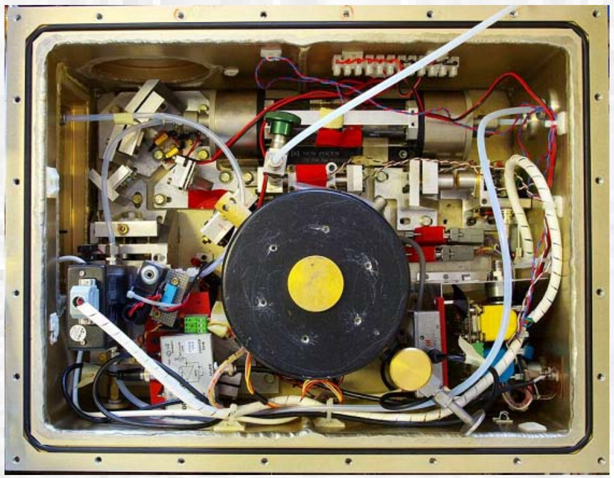
Multipass cell:

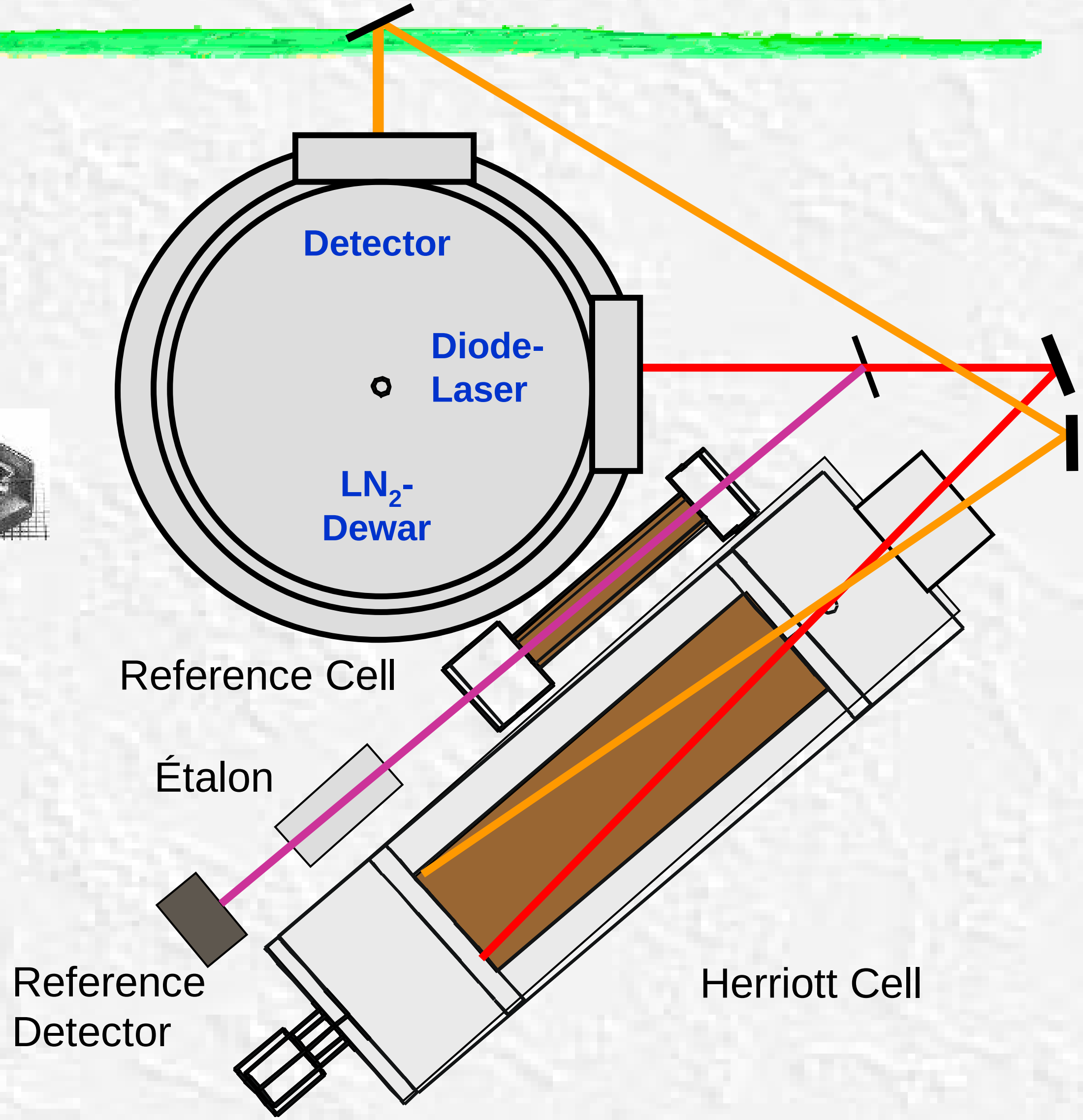
astigmatic Herriott cell

absorption path 36 m

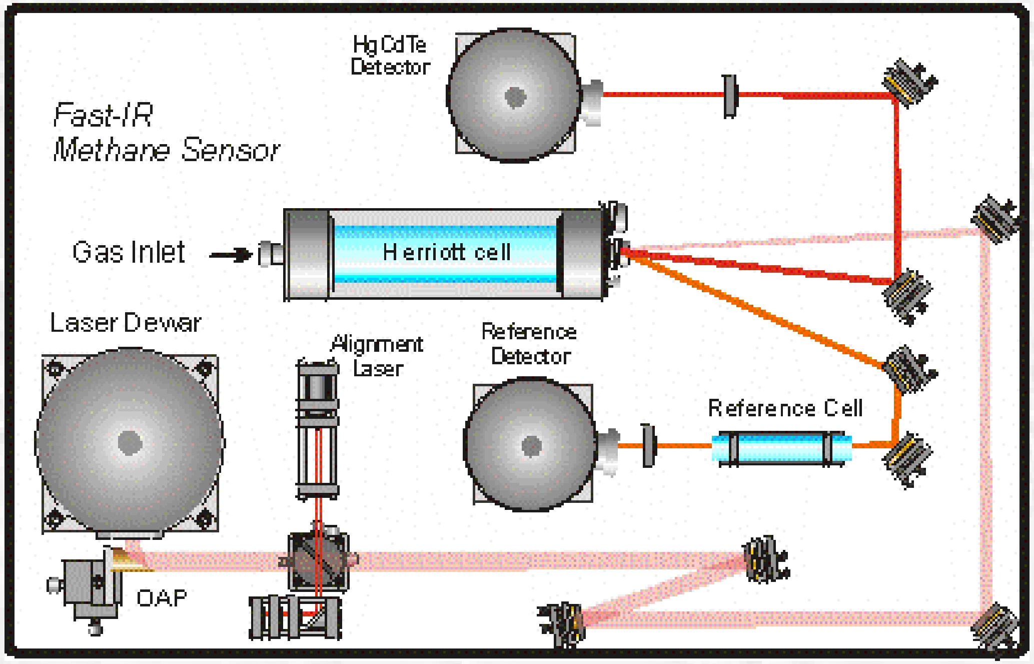
low volume (0.3 *l*)





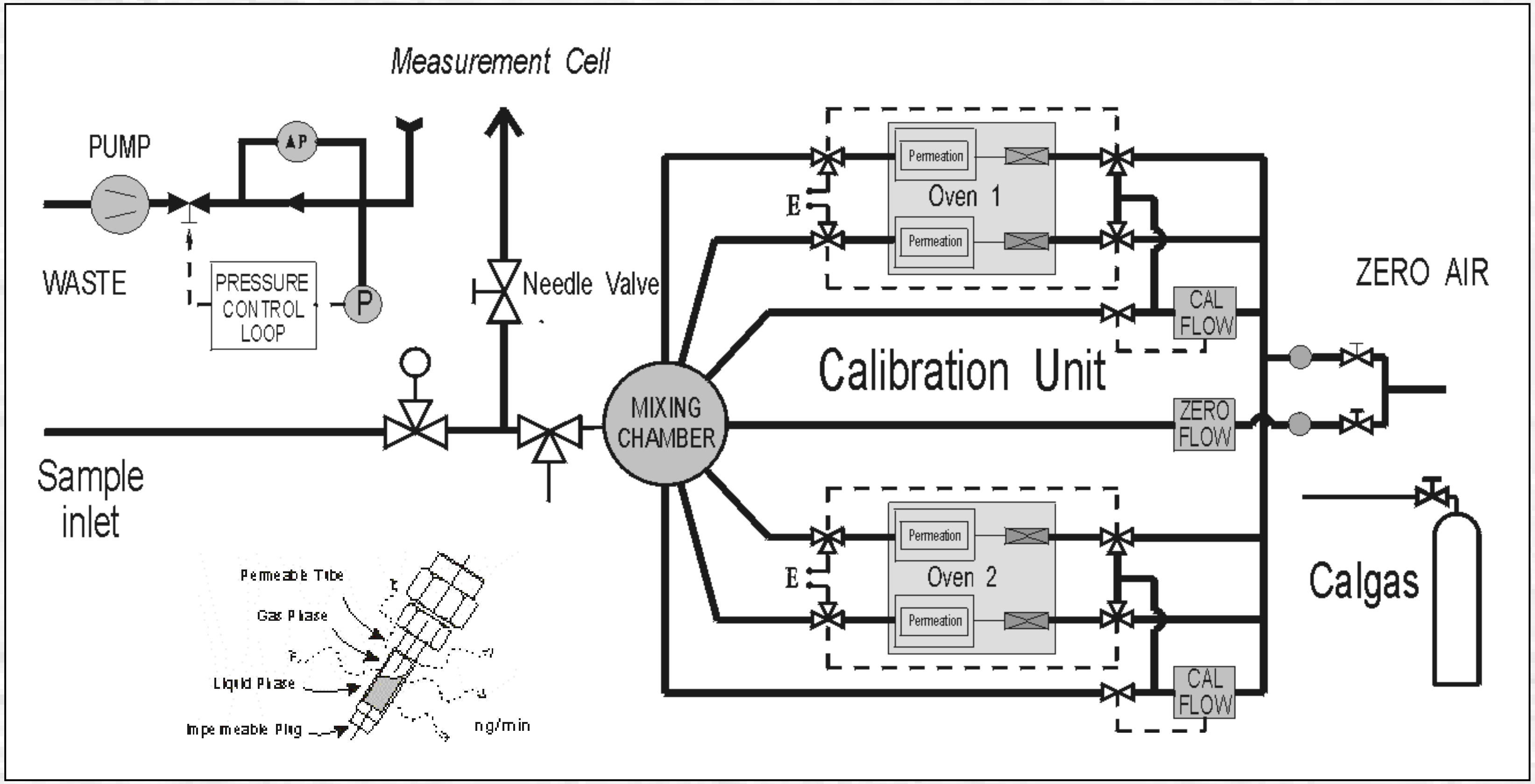


A „Field“ Diode Laser Spectrometer for Methane



P. Werle and R. Kormann, "A fast chemical sensor for eddy correlation measurements of Methane emissions from rice paddy fields“, Appl. Opt. 40, 846-858 (2001). View-PDF

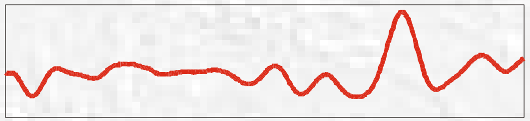
Dynamic Spectrometer Calibration is an issue



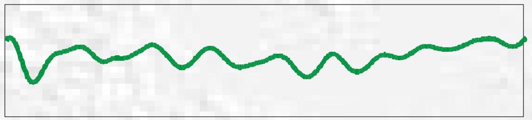
P. Werle, P. Mazzinghi, F. D´Amato, M. De Rosa, K. Maurer, F. Slemr, "Signal Processing and Calibration Procedures for in-situ Diode-Laser Absorption Spectroscopy", Spectrochimica Acta A - Review 60, 1685-1705 (2004) (for paper click here)

Signal Processing is an issue

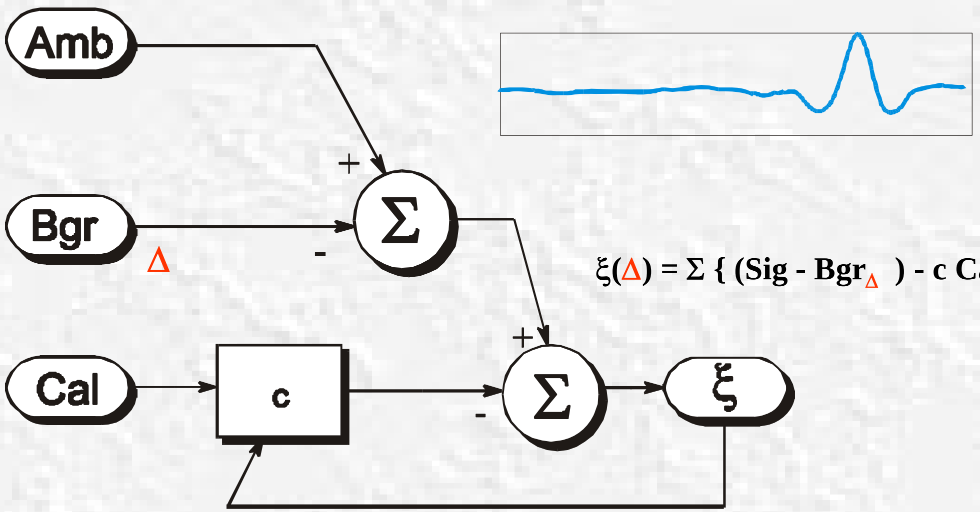
Measurement Signal (Amb)



Background Signal (Bgr)



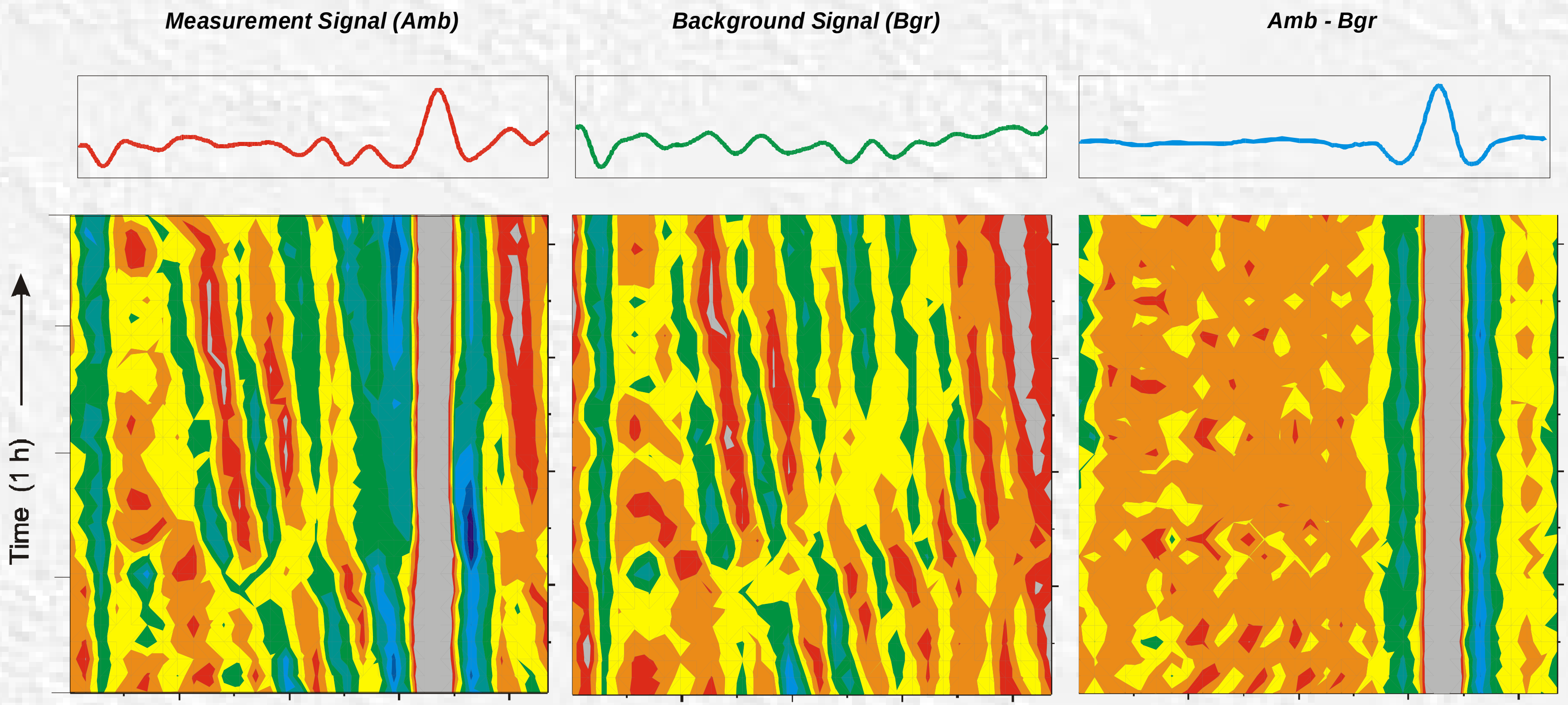
Amb - Bgr



$\xi(\Delta) = \Sigma \{ (Sig - Bgr_{\Delta}) - c\,Cal \}^2$

P. Werle, P. Mazzingh, F. D´Amato, M. De Rosa, K. Maurer, F. Slemr, “Signal Processing and Calibration Procedures for in-situ Diode-Laser Absorption Spectroscopy“, Spectrochimica Acta A - Review 60, 1685-1705 (2004) (for paper click here)

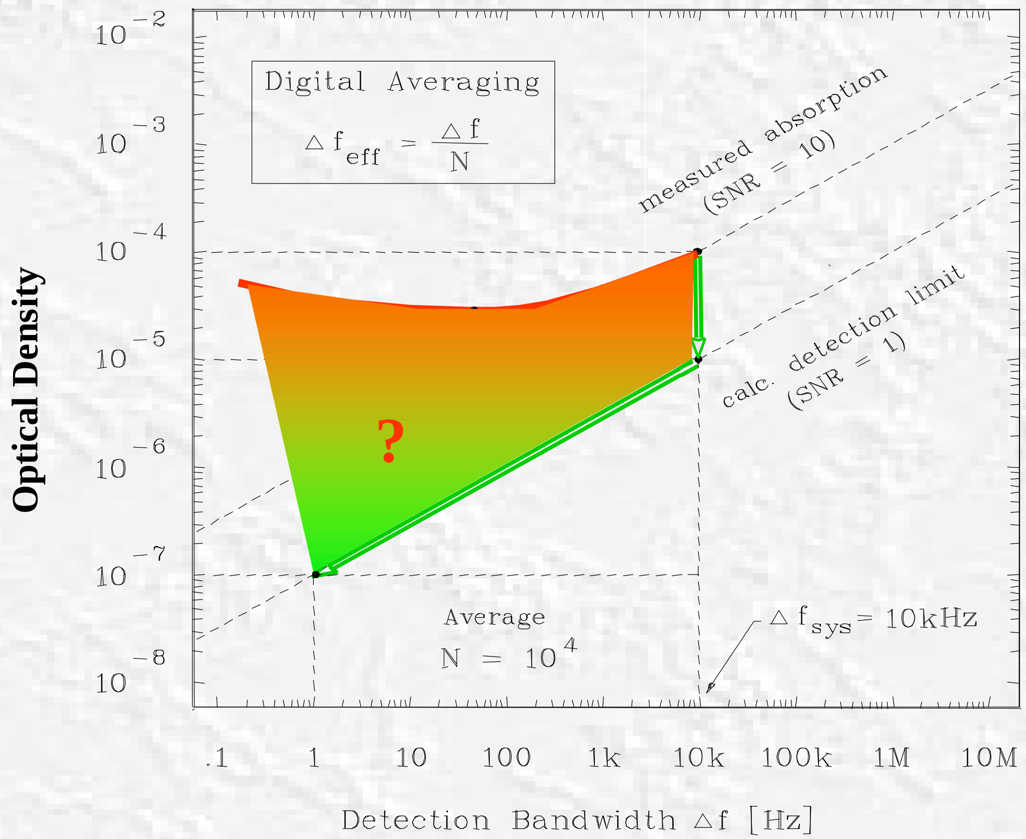
Background Drift



What are the Limits of Signal Averaging ?

What is the result of digital averaging of 10^4 spectra ?

Which curve does the detection limit follow ?



Sample Variance

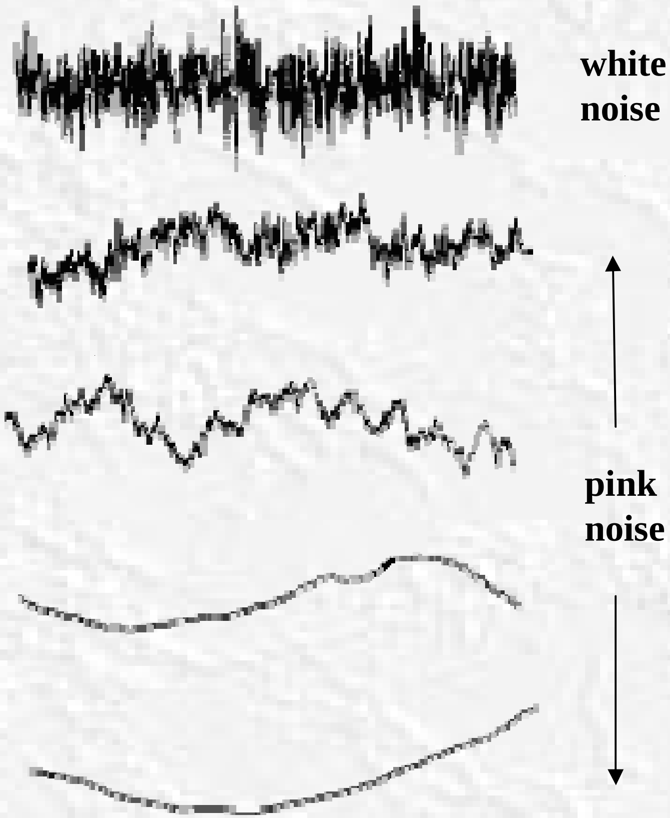
Typically, the sample variance is calculated from a data sample using the relation:

$$\sigma_{STD\ DEV\ y}(\tau) = \sqrt{\frac{1}{M-1}\sum_{i=1}^{M}\left(y_i - \bar{y}\right)^2}$$

Where it is implicitly assumed that the y_i,'s are random and uncorrelated (i.e., white) and where $\bar{y}$ is the sample mean calculated from the same data set.

What happens to the standard deviation …

… when a data set may be characterized by power law spectra which are more dispersive than classical white noise fluctuations ?



One can show that the standard deviation is a function of the number of data points in the set; it is also a function of the dead time and of the measurement system bandwidth. For example, using **flicker noise** as a model, as the number of data points increases, **the standard deviation monotonically increases without limit**.

Some statistical measures have been developed which do not depend upon the data length and which are readily usable for characterizing random fluctuations in precision oscillators.

IEEE subcommittee on frequency stability …

… has recommended what has come to be known as the "Allan variance" taken from the set of useful variances developed, and an experimental estimation of the square root of the Allan variance is

$$\sigma_y(\tau) = \sqrt{\frac{1}{2(M-1)} \sum_{i=1}^{M-1} \left(y_{i+1} - y_i\right)^2}$$

This equation is very easy to implement experimentally as one simply need **add up the squares of the differences between adjacent values of y_i divide by the number of them and by two, and take the square root**.

PROCEEDINGS OF THE IEEE VOL. 54, NO. 2 FEBRUARY, 1966

Statistics of Atomic Frequency Standards

DAVID W. ALLAN

Abstract—A theoretical development is presented which results in a relationship between the expectation value of the standard deviation of the frequency fluctuations for any finite number of data samples and the infinite time average value of the standard deviation, which provides an invariant measure of an important quality factor of a frequency standard. A practical and straightforward method of determining the power spectral density of the frequency fluctuations from the variance of the frequency fluctuations, the sampling time, the number of samples taken, and the dependence on system bandwidth is also developed. Additional insight is also given into some of the problems that arise from the presence of "flicker noise" (spectrum proportional to $|\omega|^{-1}$) modulation of the frequency of an oscillator.

The theory is applied in classifying the types of noise on the signals of frequency standards made available at NBS, Boulder Laboratories, such as: masers (both H and $N^{15}H_3$), the cesium beam frequency standard employed as the U. S. Frequency Standard, and rubidium gas cells.

"Flicker noise" frequency modulation was not observed on the signals of masers for sampling times ranging from 0.1 second to 4 hours. In a comparison between the NBS hydrogen maser and the NBS III cesium beam, uncorrelated random noise was observed on the frequency fluctuations for sampling times extending to 4 hours; the fractional standard deviations of the frequency fluctuations were as low as 5 parts in 10^{14}.

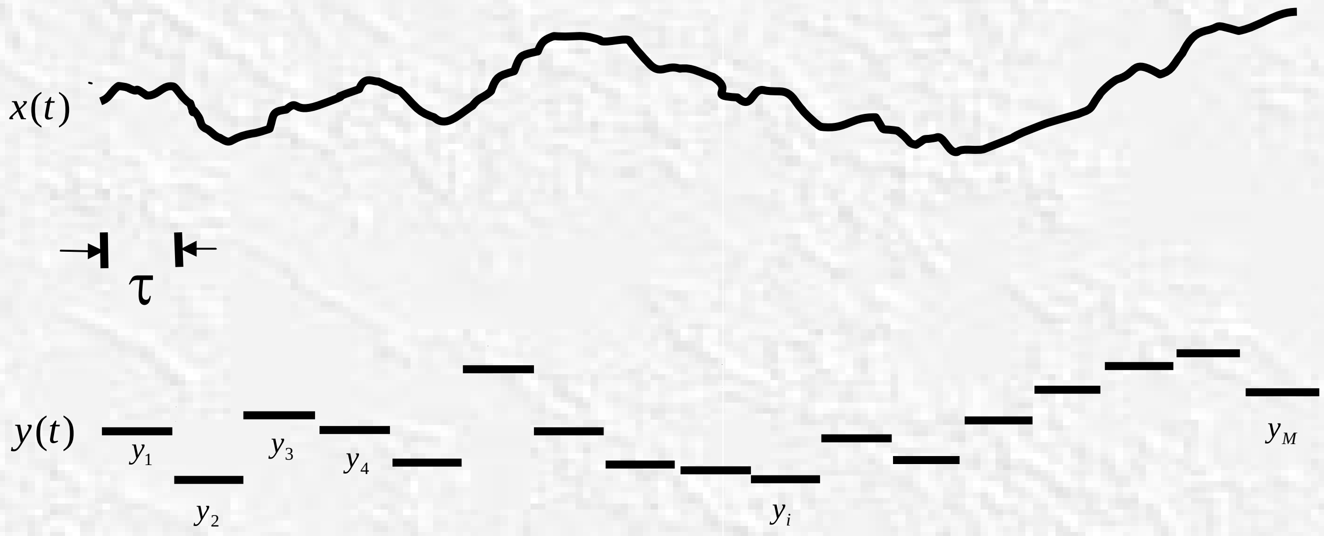
I. Introduction

As ATOMIC TIMEKEEPING has come of age, it has become increasingly important to identify quality in an atomic frequency standard. Some of the most important quality factors are directly related to the inherent noise of a quantum device and its associated electronics. For example, a … measure … a frequency standard is to compare two such standards by measuring the period of the beat frequency between the two standards. It is again the intent of the author to show a practical and easy way of classifying the statistics, i.e., of determining the power spectral density of the frequency fluctuations using this type of measuring system.

An analysis has already been made of the noise present in passive atomic frequency standards [1], such as cesium beams, but a classification of the types of noise exhibited by the maser type of quantum-mechanical oscillator has not been made in the long term area, i.e., for low frequency fluctuations. Though this paper is far from exhaustive, the intent is to give additional information on the noise characteristics of masers. Because a maser's output frequency is more critically parameter dependent than a passive atomic device, it has been suggested [2] that the output frequency might appear to be "flicker noise" modulated, where "flicker noise" is defined as a type of power spectral density which is inversely proportional to the spectral frequency $\omega/2\pi$. It has been shown that if "flicker noise" frequency modulation is present on a signal from a standard, some significant problems arise, such as the logarithmic divergence of the standard deviation of the frequency fluctuations as the number of samples taken increases, and also the inability to define precisely the time average frequency. It thus becomes of special interest to … "flicker noise" … present on

D. W. Allan, "Statistics of atomic frequency standards," *Proc. IEEE*, vol. 54, pp. 221–230, Feb. 1966.

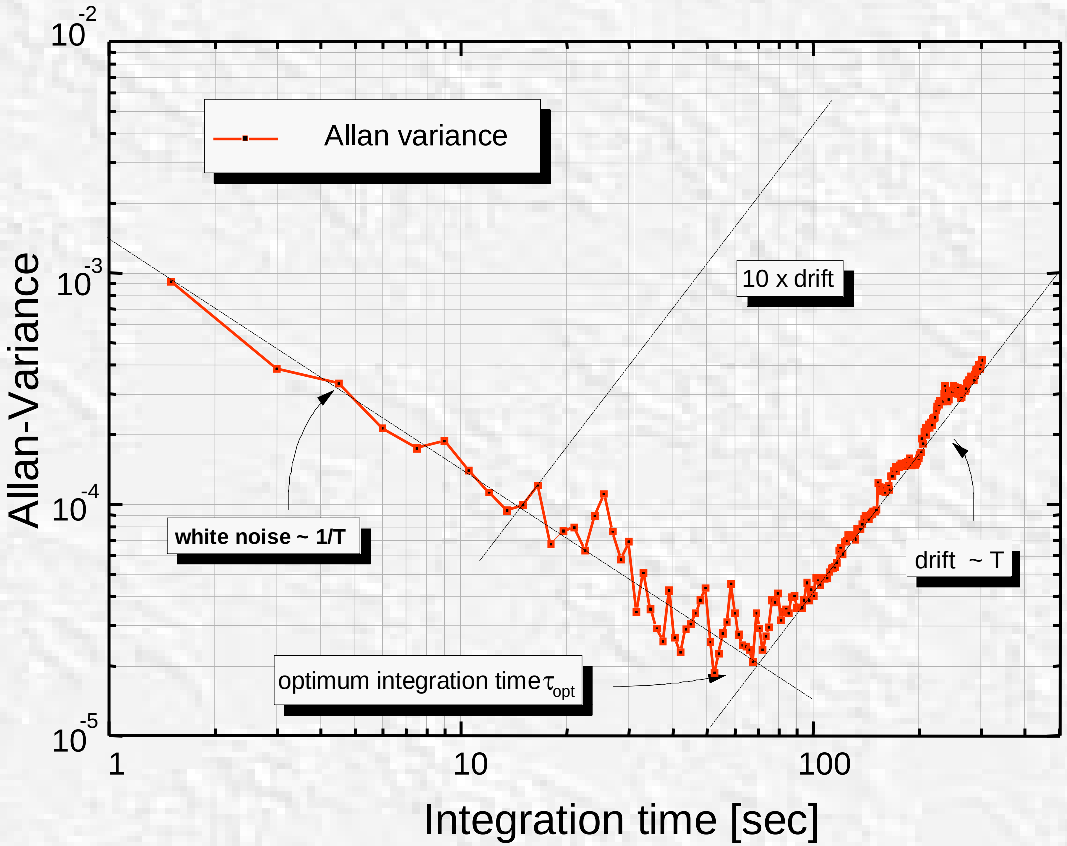
Sample Variance and Allan Variance



$$\sigma_{STD\ DEV\ y}(\tau) = \sqrt{\frac{1}{M-1}\sum_{i=1}^{M}\left(y_i - \bar{y}\right)^2} \qquad \sigma_y(\tau) = \sqrt{\frac{1}{2(M-1)}\sum_{i=1}^{M-1}\left(y_{i+1} - y_i\right)^2}$$

Time series x(t) with indicated sample time τ over which each y is measured. Equations are for standard deviation and for estimate of $\sigma_y(t)$ for a finite data set of M measurements.

Allan Plot



"Allan-Plot" for two different drift components. The rightmost trace corresponds to the "white noise and drift" data shown before.

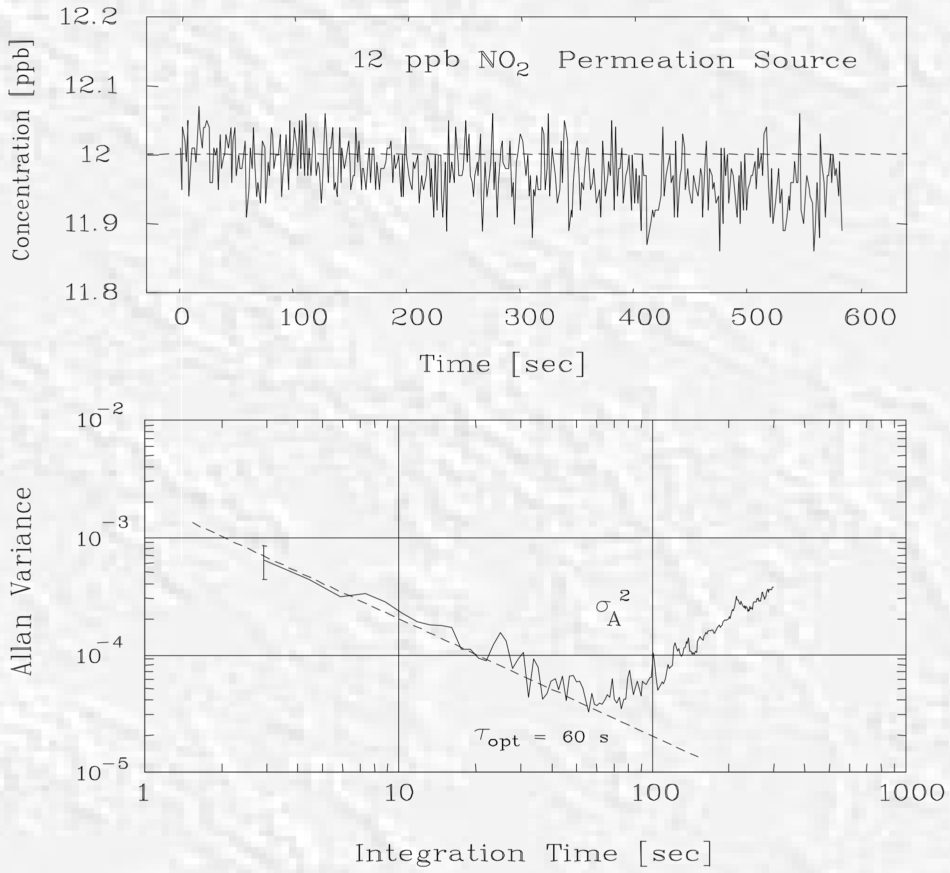
Minimum of Allan Plot defines maximum integration time (= detection limit !) for signal averaging

First application in trace gas analysis

The concept of the Allan Variance has been proposed and applied to characterize spectroscopic instrumentation

P. Werle, R. Muecke and F. Slemr, "The limits of signal averaging in atmospheric trace gas monitoring by tunable diode-laser absorption spectroscopy", Appl. Phys. B 57, 131-139 (1993). View-PDF

and has become a well established tool for researchers and instrument developers to describe the performance of laseroptical trace gas sensors.



Detection Limits

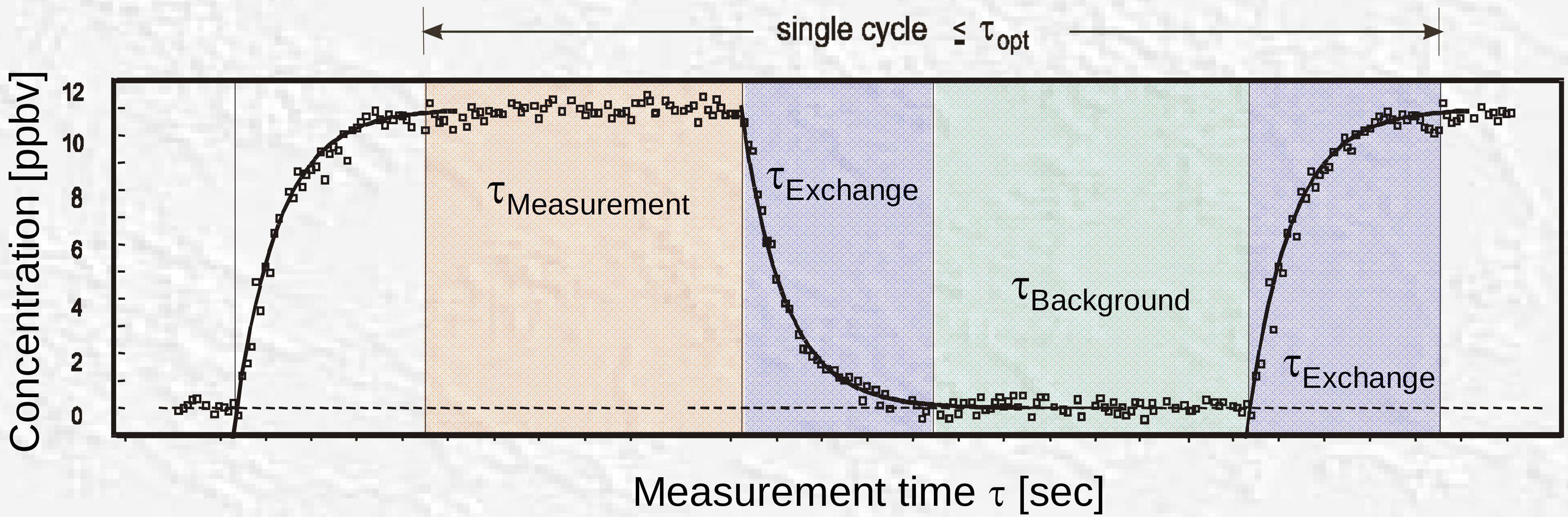
for atmospheric constituents for a sampling pressure of 30 mbar and T=296 K based upon a minimum detectable absorbance of 10^{-5} and 100 m optical path-length

Species	λ µm	ν cm^{-1}	S 10^{-19} cm/molec	γ_v 10^{-3} cm^{-1}	γ_v MHz	σ 10^{-17} cm^2/molec	DL pptv
N_2O	7.69	1301	1.56	2.77	83.1	1.92	70
CO	4.65	2151	1.89	3.85	115.5	1.85	73
CH_4	7.56	1322	0.53	3.25	97.5	0.60	225
NO	5.33	1876	0.34	3.26	97.8	0.39	350
SO_2	7.29	1372	0.49	3.86	115.8	0.41	330
NO_2	6.25	1600	2.18	2.90	87.0	2.70	50
NH_3	10.74	931	5.20	2.92	87.6	6.18	23
HNO_3	5.81	1722	0.72	3.75	112.5	0.25	218
HF	1.24	7856	0.76	12.09	362.7	0.27	500
HCl	3.40	2945	5.03	4.30	129.0	4.51	30
HBr	3.78	2649	0.45	2.90	87.0	0.57	240
ClO	11.6	860	0.08	2.73	81.9	0.09	1500
OCS	4.87	2053	10.30	3.55	106.5	10.00	13
HCHO	3.56	2781	1.19	5.17	155.1	0.84	160
CH_3Cl	3.29	3040	0.02	4.12	123.6	0.02	7800
H_2O_2	7.79	1284	0.45	3.52	105.6	0.43	320
H_2S	7.33	1365	0.01	4.89	146.7	0.007	20000
HCOOH	8.98	1113	0.44	3.32	99.6	0.44	310
HO_2	7.08	1411	0.12	3.63	108.9	0.11	1200

Current Limitations

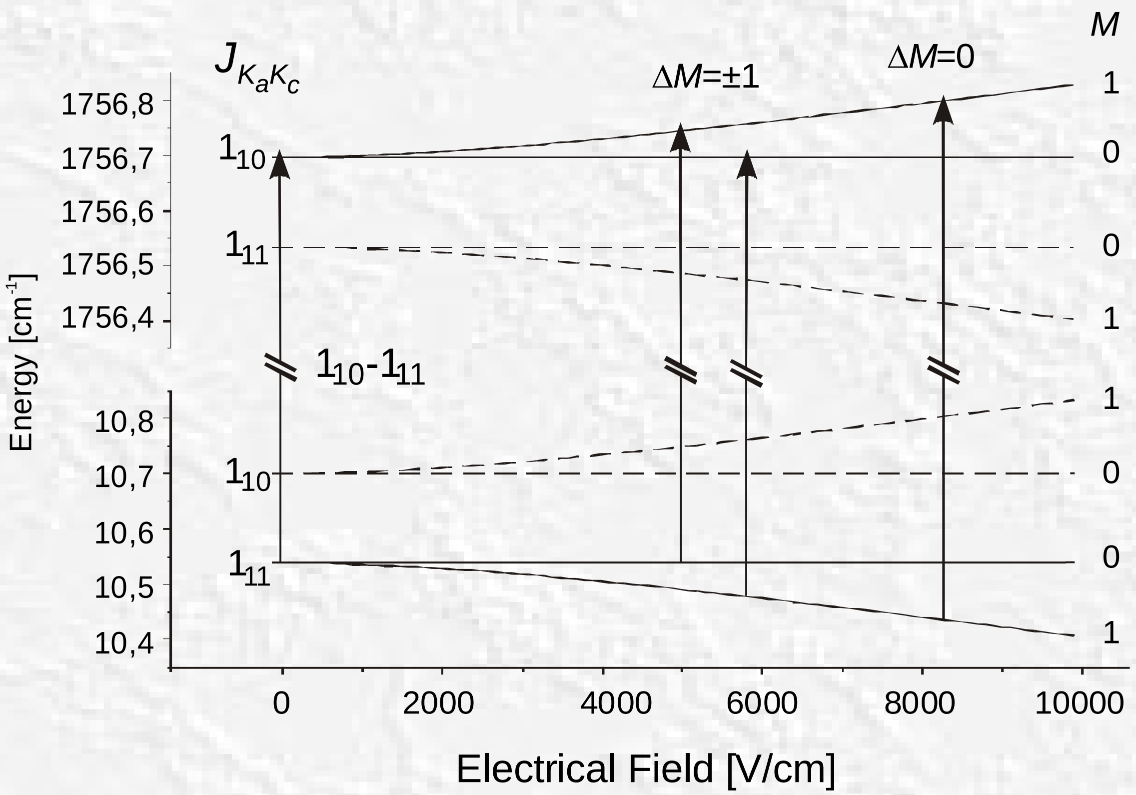
Problem: background is **time dependent**
Why: moves due to small temperature/pressure drifts

repeated background measurement necessary
duty cycle ~ 50% – 60%



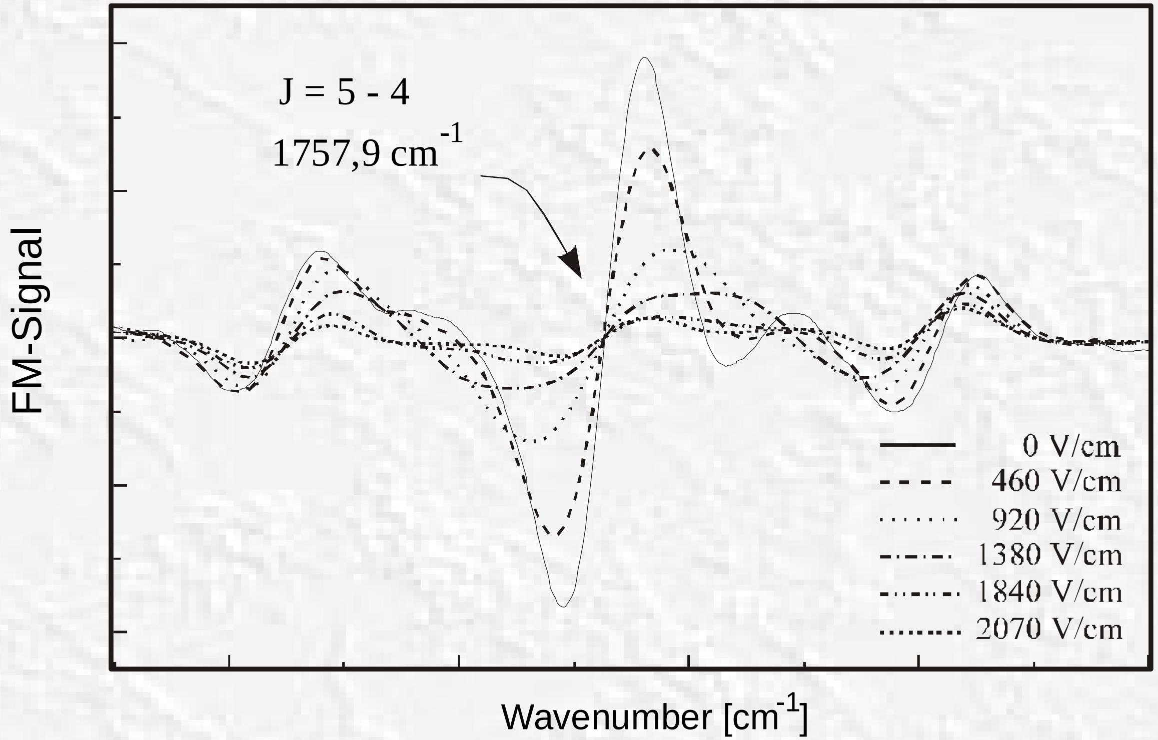
Concept : Sample Modulation - Stark Effekt

a periodic modulation of sample energy levels …

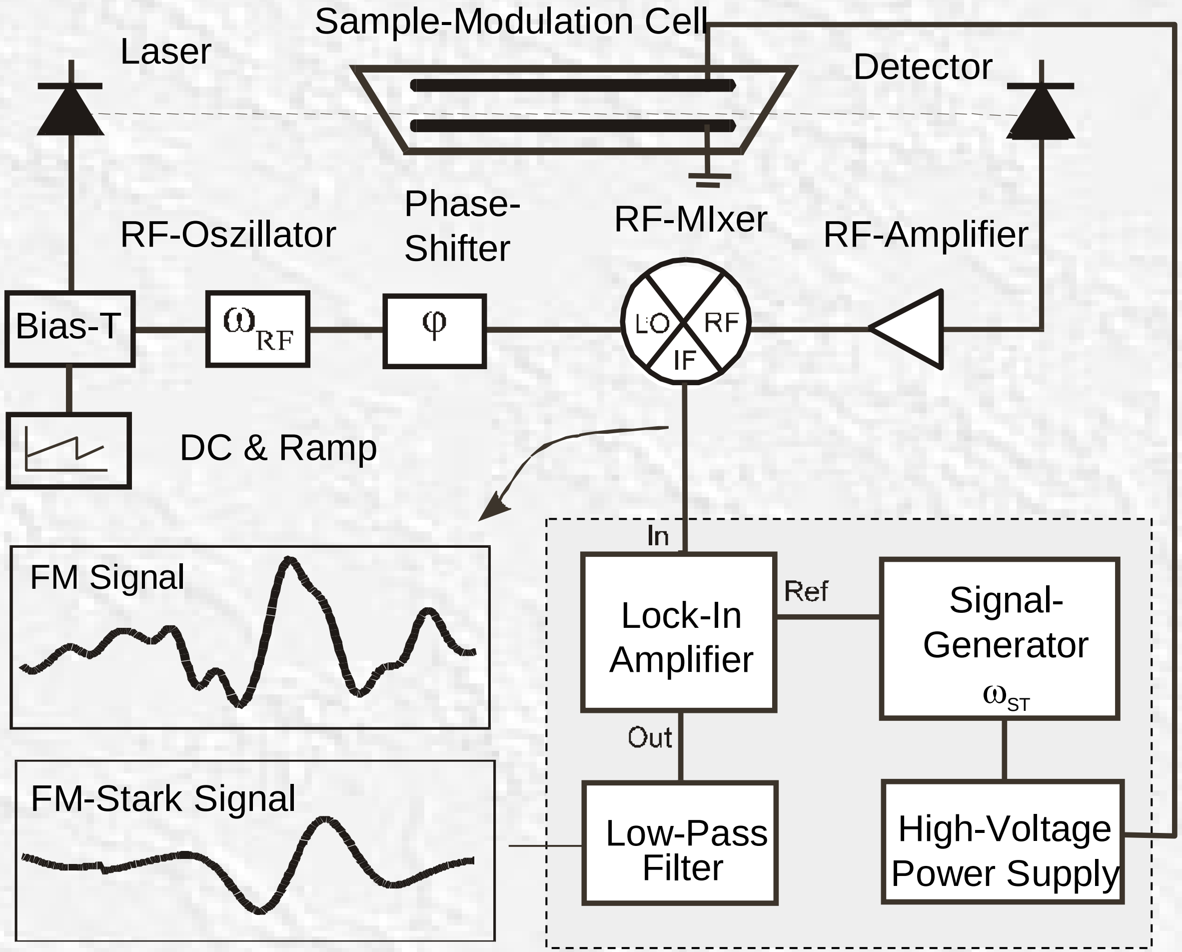


Background Suppression

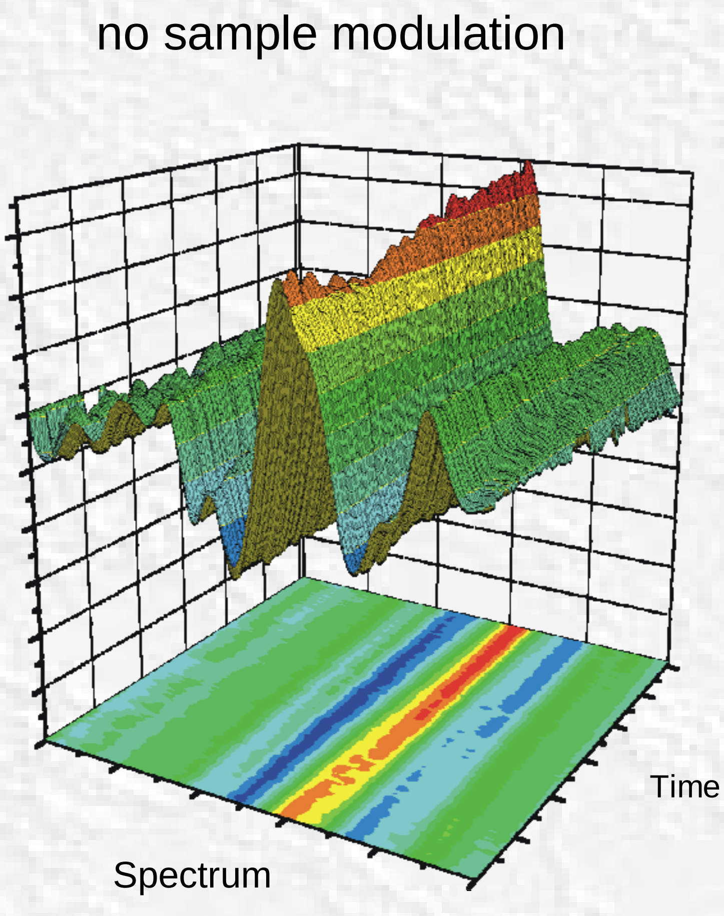
… influences signal from sample only – background is not affected

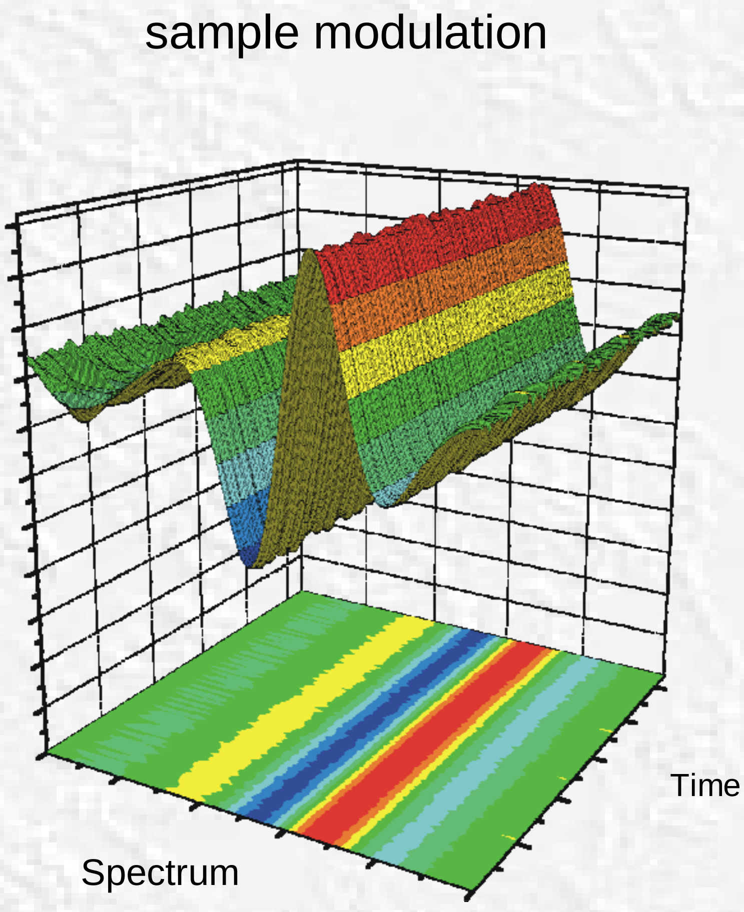


A Laser – Sample Double Modulation Setup



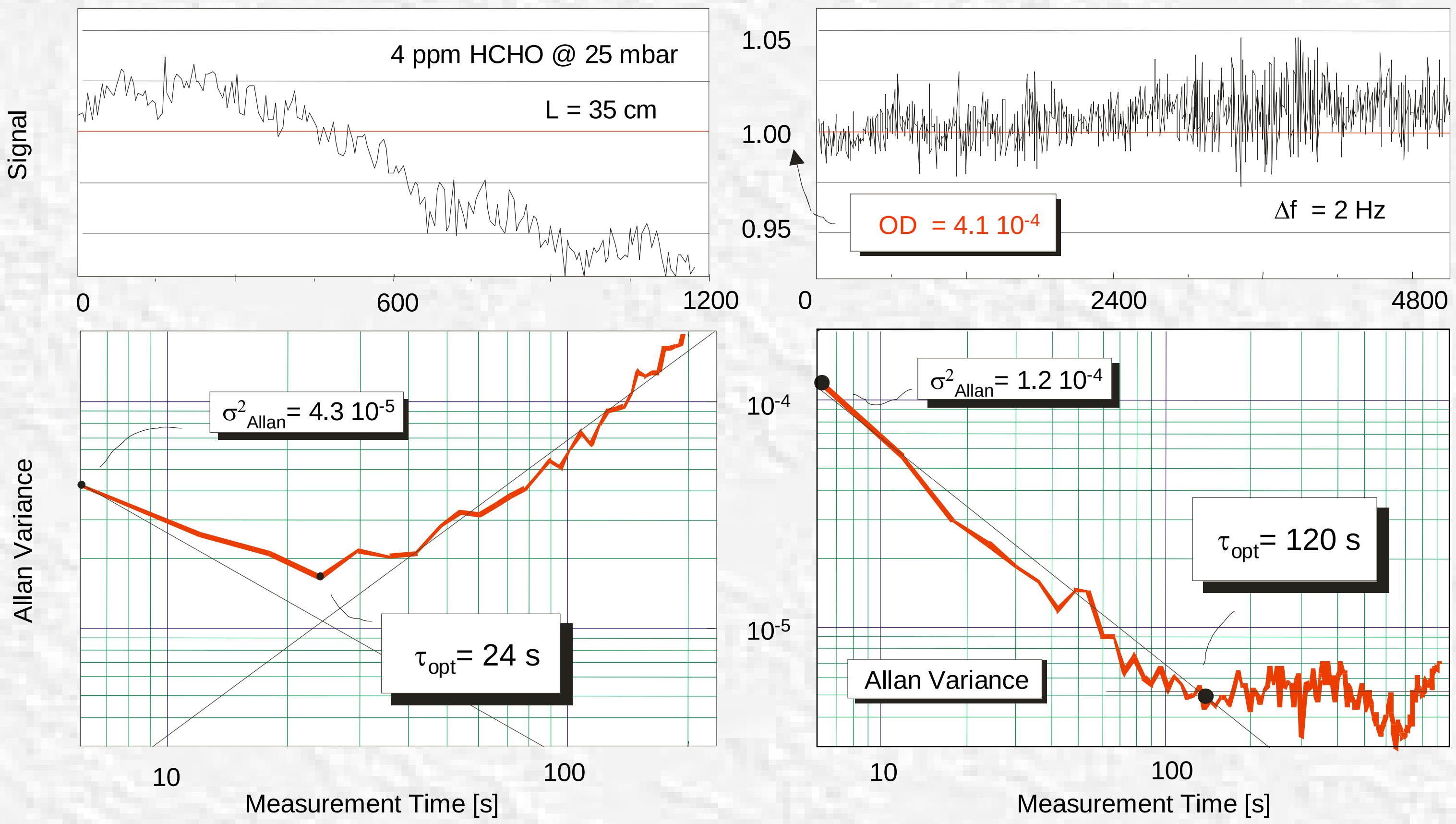
Signal comparison





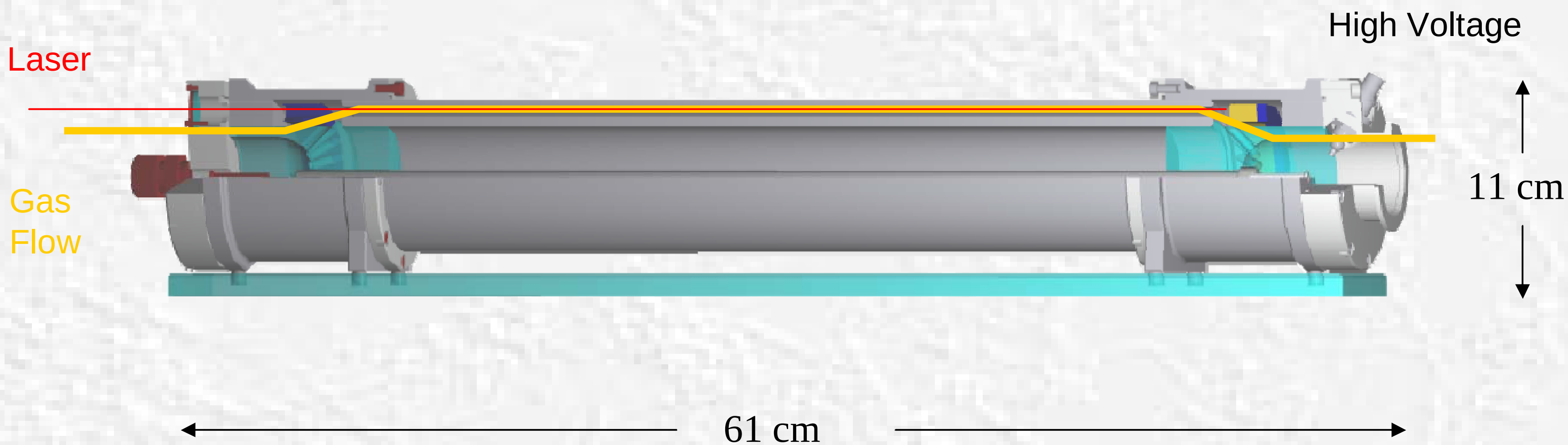
a promising approach ...

no sample modulation | sample modulation



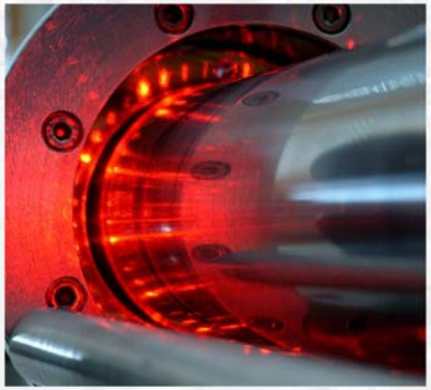
... the next step

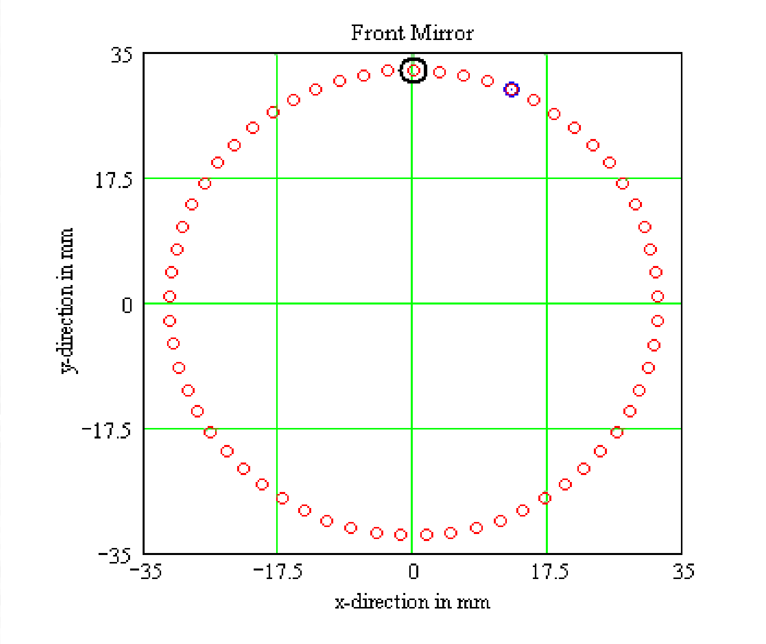
a multi-pass cell with small volume of 0.5 Liter for a fast gas exchange and a laminar gas flow to avoid turbulence

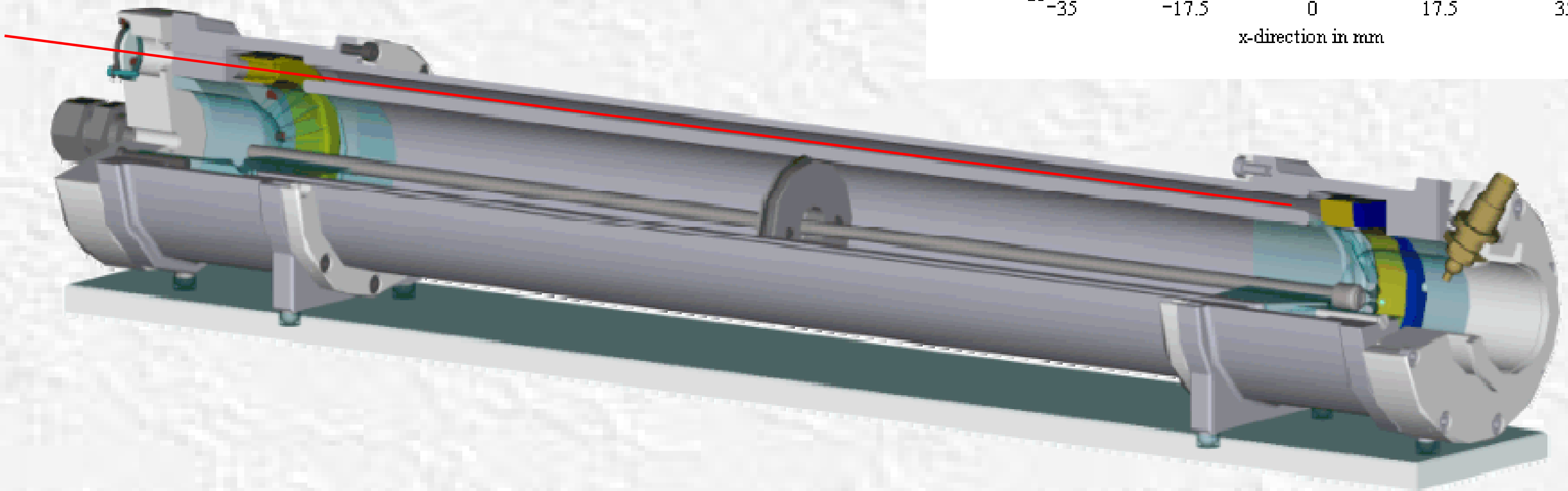


Stark Multipass Cell Design

ring mirror
11 m radius
61 spots
122 passes
46 cm baselength
0,9 l Volume

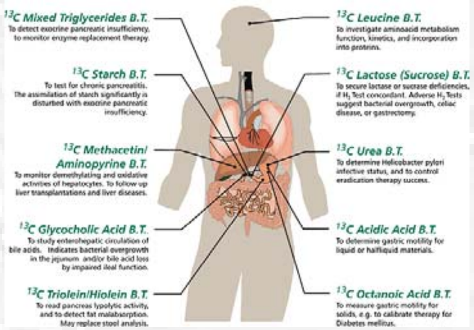






Let´s move from the laboratory to …

Industrial Process Control & Emission Monitoring
High Purity Gases (Semiconductor Industry)
Plasma Diagnostics, Combustion Diagnostics,
Lifescience & Agriculture & Medicine
..



Environmental Research


from the **upper Troposphere**

and **lower Stratosphere**

to **Biosphere - Atmosphere**

exchange over complex terrain


The state of the art

FLAIR - Industry Session

http://www.inoa.it/flair/industry.htm

… an assessment of the present status

Industrial Analytical Systems based on Tunable Diode-Lasers

LASER COMPONENTS

VERTILAS

Nanosystems and Technologies GmbH nanoplus

Ekips

Alpes Lasers

TOPTICA PHOTONICS

Scienza Industria Tecnologia

ACULIGHT

Sacher Lasertechnik Group

Vescent Photonics

CASCADE TECHNOLOGIES

LGR

AERODYNE RESEARCH

UNISEARCH ASSOCIATES INC.

Norsk Elektro Optikk AS

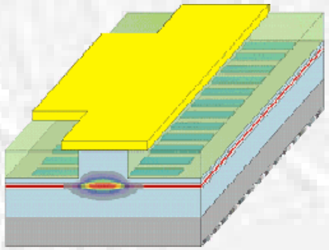
SIEMENS

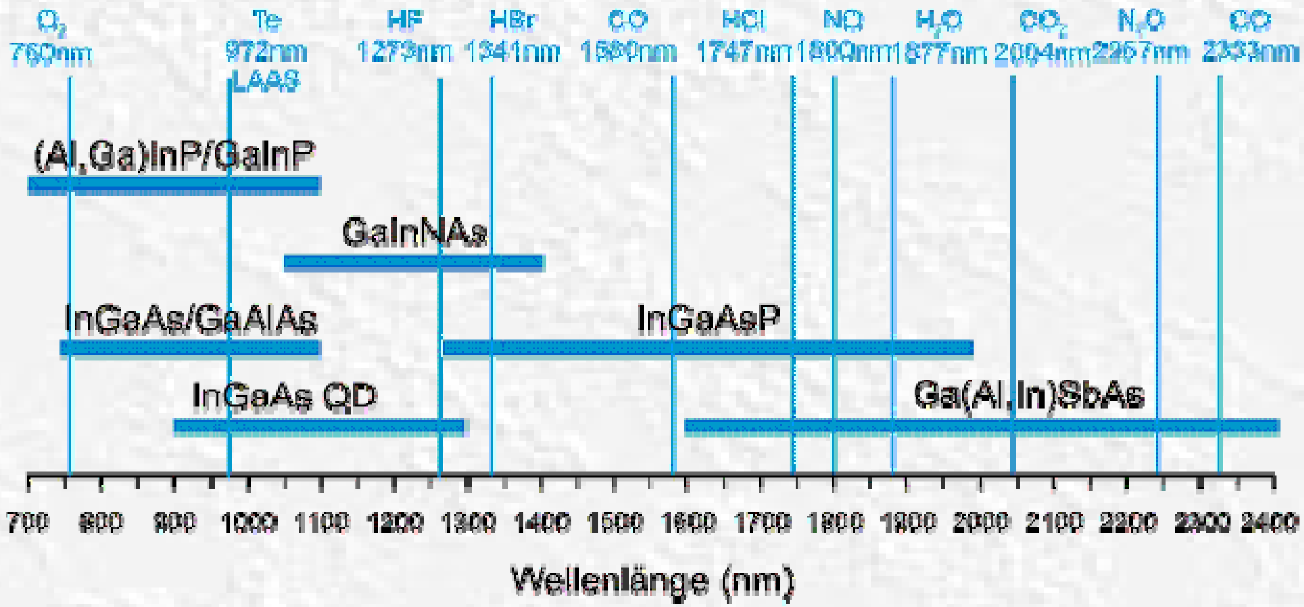
DFB Diode Lasers

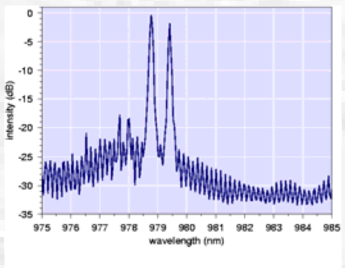
Nanosystems and Technologies GmbH
nanoplus

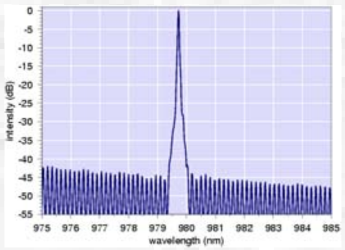
avialable wavelengths

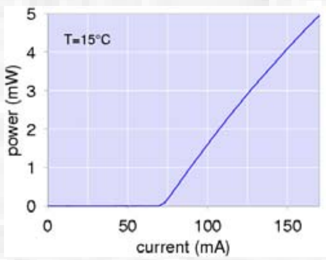
laterally coupled
DFB laser diode

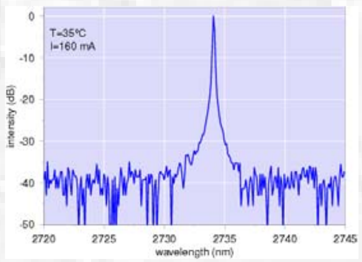








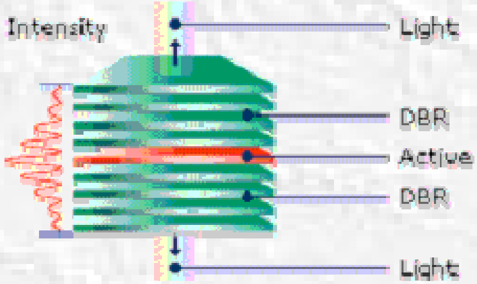


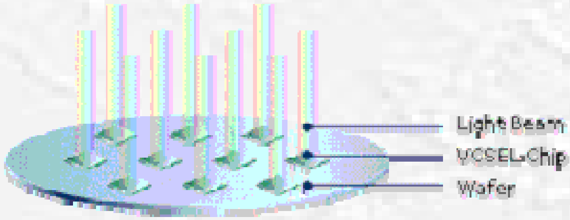


2735 nm
DFB laser diode
for H_2O absorption

www.nanoplus.com

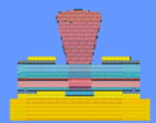
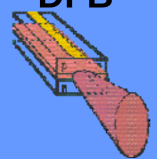
VCSEL



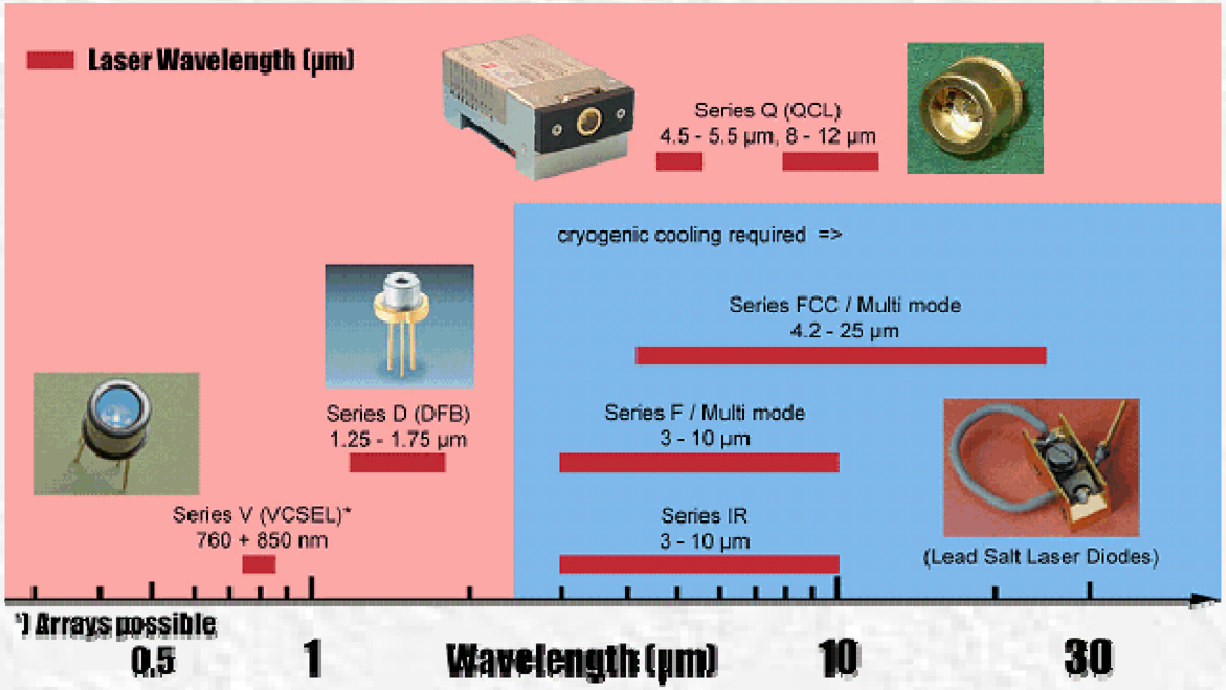


- Longitudinal single mode
- Circular and low divergence output beam
- High fiber coupling efficiency
- Small power consumption
- One and two dimensional arrays
- Simplified manufacturing, testing & packaging
- Low-cost potential

www.vertilas.com

Laser type	Threshold current	Output power	Current tuning rate	Current tuning range	Temperature tuning rate	Maximum modulation
VCSEL 	0.5–2 mA	0.4-3 mW	0.7 nm/mA	3-5 nm	~0.11 nm/°C	> 1 MHz
DFB 	20 mA	5 mW	<0.01 nm/mA	< 1 nm	~0.11 nm/°C	< 100 kHz

Lead Salt Diode Lasers



Lead-salt diode-laser

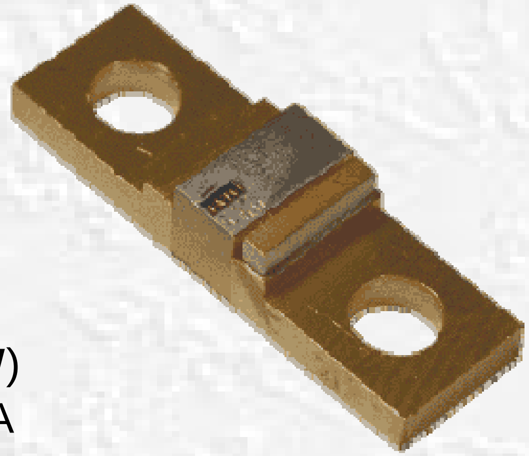
- Spectral Positions: 400 – 3250 cm^{-1}
- Spectral Resolution: 10^{-4} cm^{-1}
- min. power 0.1 mW up to typ. 1 mW
- CW and pulsed to MHz

- Current: 50 to 2,000 mA
- Temperature: 25 to 120 K
- Delivery time 6-8 weeks

www.lasercomponents.com

Alpes Lasers

Quantum Cascade Laser

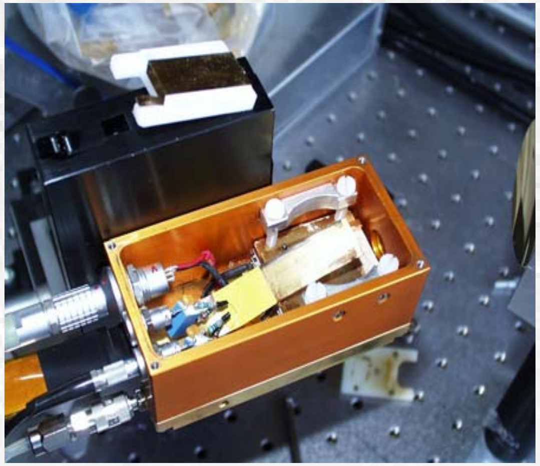


LN_2 and RT continuous-wave DFB

Available wavelengths off-the-shelf: 4.2 to 10.4 μm

Characteristics:

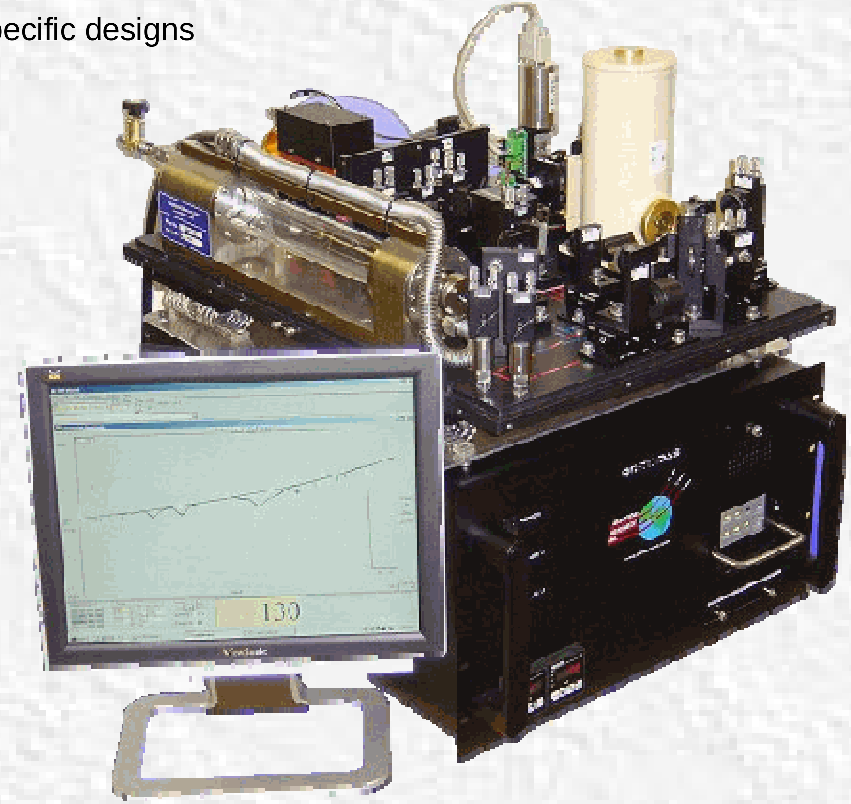
Power typical 2 mW (max up to **100 mW**)
Operating current: 0.3 - 2 A, typical 0.8 A
Operating voltage: 8-10 V
Tuning range: **> 0.4%**
Spectral linewidth **~ 3 MHz**



www.alpeslasers.com

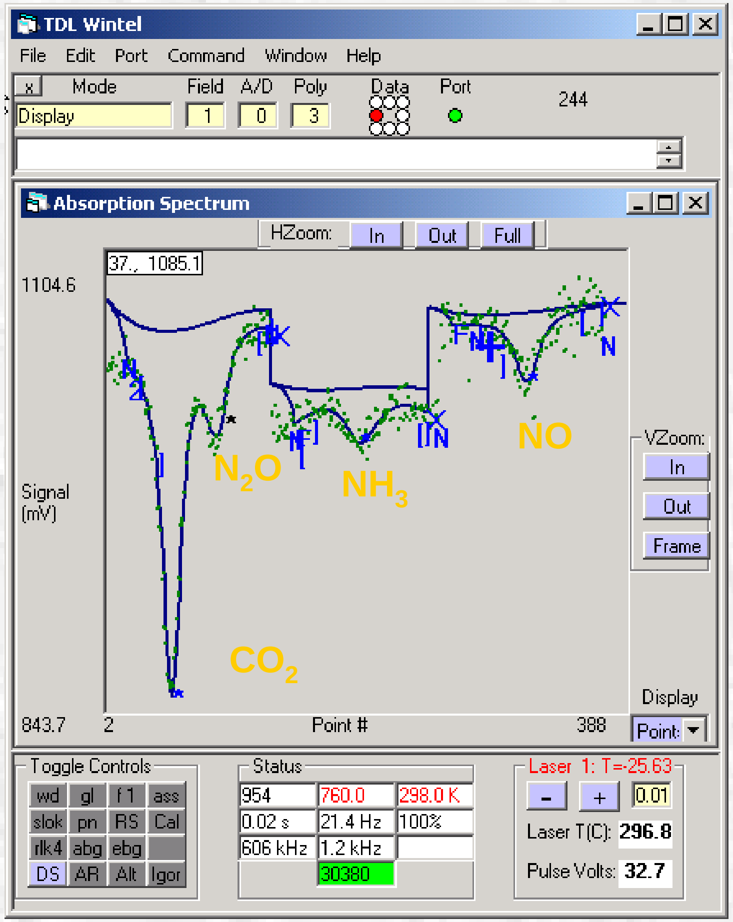
QCL Spectrometers

Customer
specific designs



Optical Module with QC lasers and
76 m astigmatic Herriott cell

www.aerodyne.com



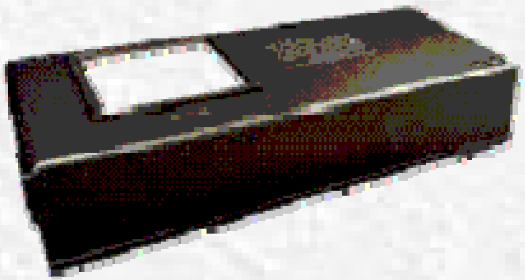
TDL Wintel Data Sample: 3 lasers, 4 gases, 20 ms

TDL & Cavity ring down instruments for Field Application

- Mirror-Reflectivity Measurements
- Thin-Film Absorption Measurements
- Substrate-Absorption Measurements
- Process Control and Validation
- Quality Control
- Testing of Optical Coatings
- Total Insertion-Loss Measurements
- Material Research
- Atmospheric Monitoring
- Industrial-Process Monitoring and Control
- Homeland Security
- Trace-Gas Sensing
- Optimization of Singlet-Oxygen Generators
- Chemical Oxygen-Iodine Laser Studies
- Fundamental Physical Sciences

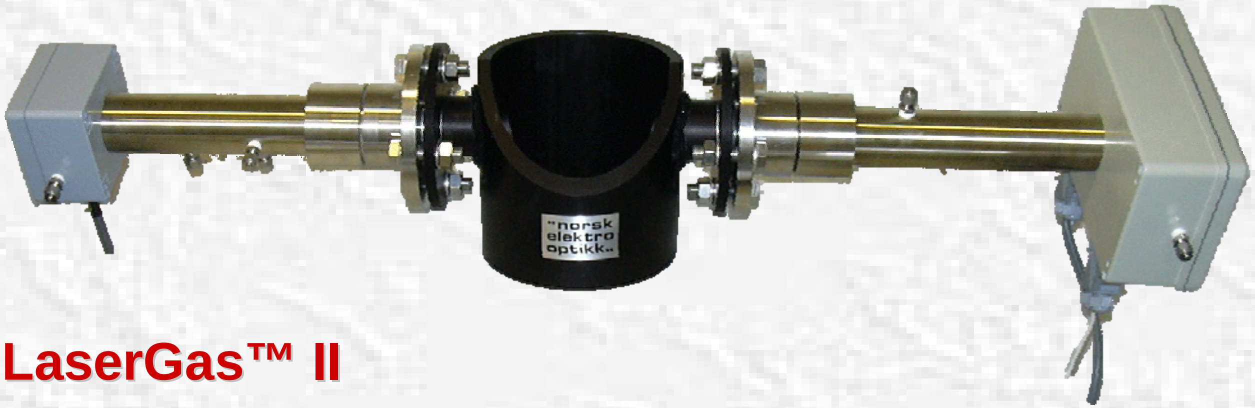
- Plasma Decontamination
- Carbon Sequestration in Ocean Waters
- Eddy-Correlation Flux Measurements
- Chamber-Flux Measurements
- Combustion Diagnostics
- Trace-Gas Monitoring
- Leak Detection from Natural-Gas Pipelines
- Hydrological Applications
- Methane-Hydrate Studies
- Hydrotherrmal-Vent-Effluent Analysis
- Analytical Applications
- Biological-Science Applications
- Atmospheric Sciences
- Methanogenic-Bacteria Studies

www.lgrinc.com



LaserGas Monitor

Norsk Elektro Optikk AS



available as

Single Path Monitor

Dual Path Monitor

Multipass Monitor

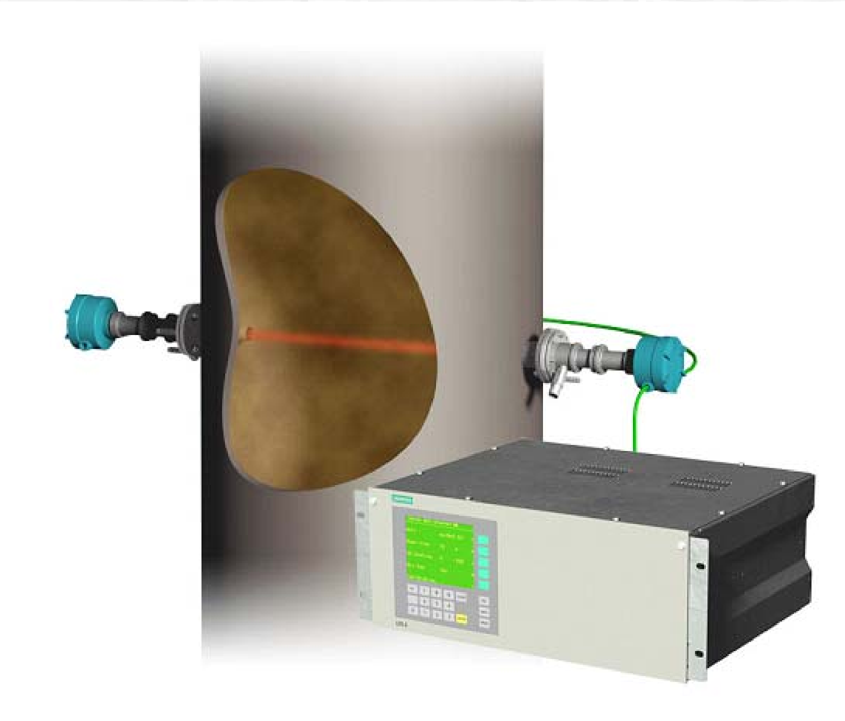
LaserGas™ II

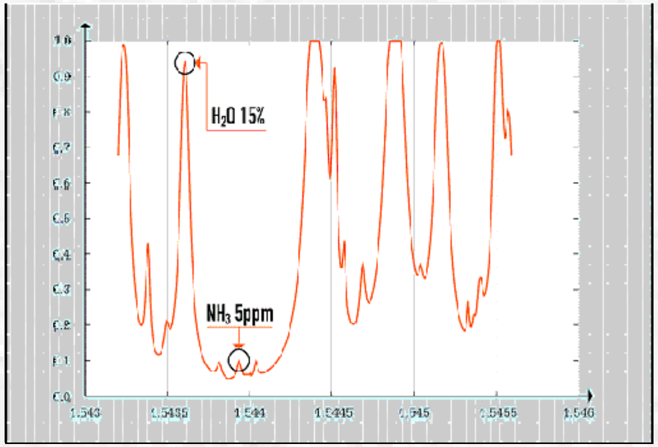
Compact design (transmitter and receiver only)
”Plug and play”
Ethernet connection
Modular design
Optional Ex-p solution

www.neo.no

Process Analytics

SIEMENS





LDS 6

all **fibre coupling**, protection class IP 67
$-30 < T_{ambient} < +70°C$
sub-ppm resolution, 1 sec. response time

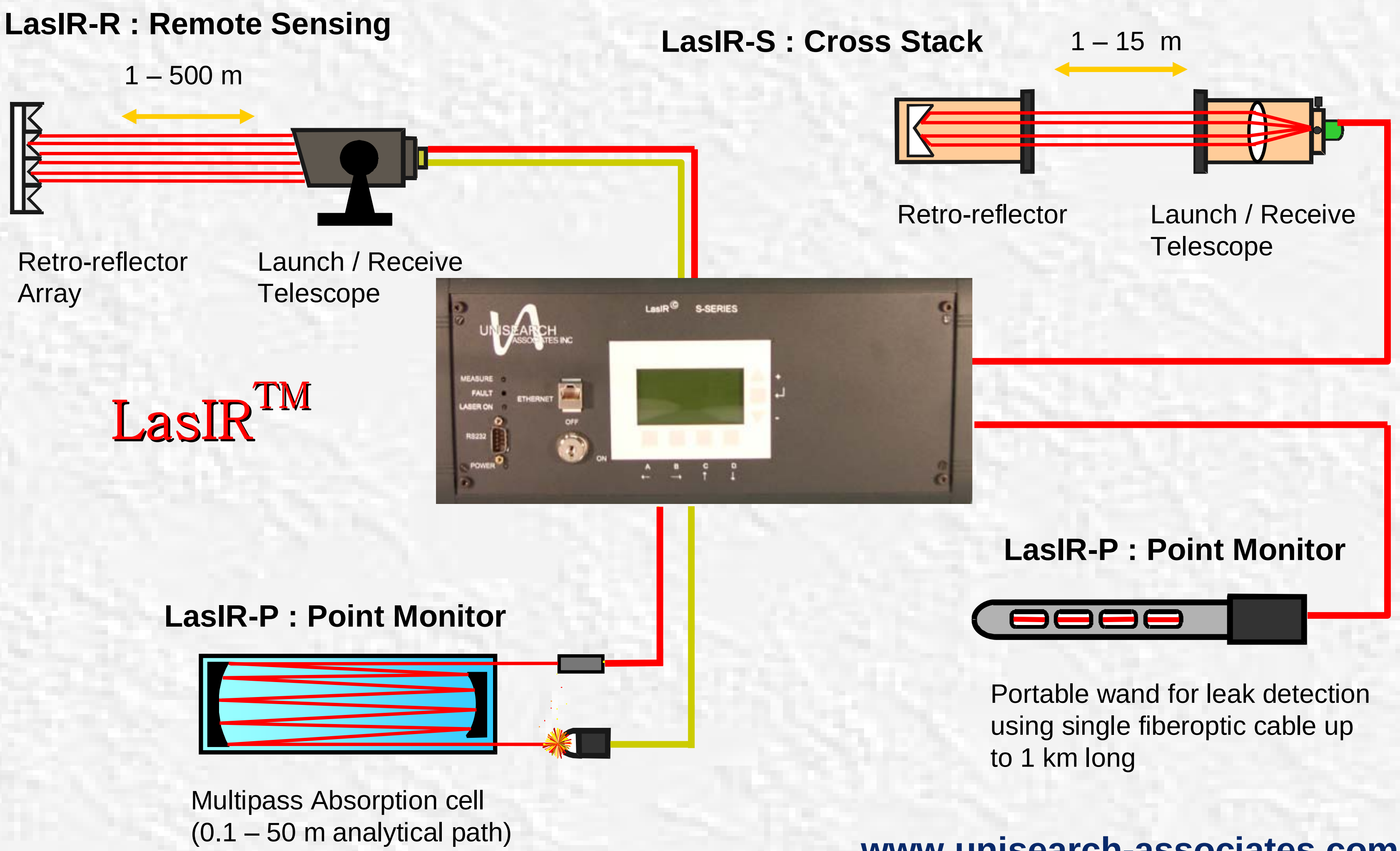
auto-calibration, no drifts

automatic compensation of changing temperature, pressure,gas matrix, dust load

Sensors EEx ia, EEx n

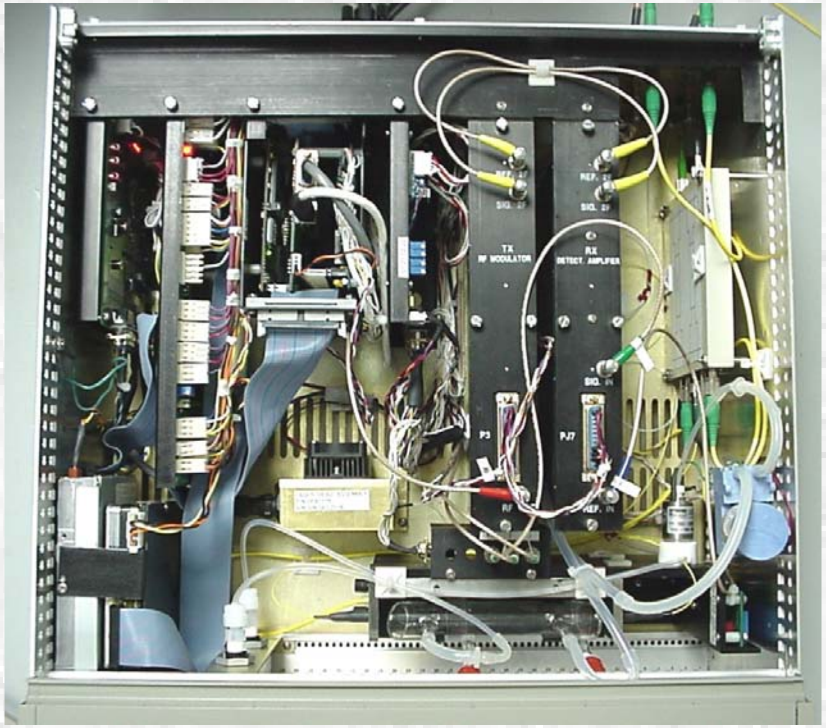
www.siemens.com/processanalytics

Versatile Instrumentation



www.unisearch-associates.com

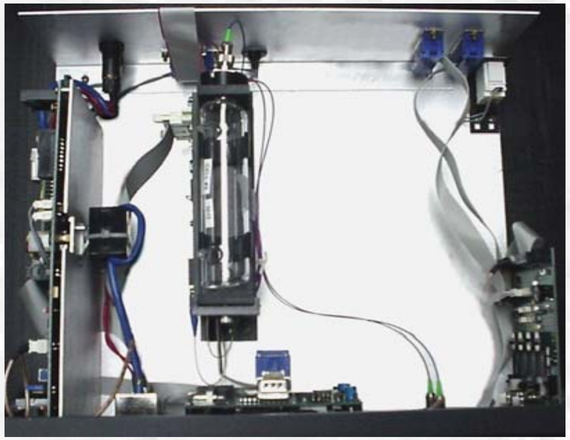
Progress …



2-channel Analyzer (older model)

LasIR™

2-channel Analyzer (new model)



www.unisearch-associates.com

Airborne in-situ measurements ...

are a useful tool for calibration and validation of remote sensing instruments for atmospheric research

the fast response of TDLS allows detection of fine structures also when operating at the cruise speed of jet aircrafts

achieved scientific results indicates further area to be investigated by the next generation of airborne or satellite remote sensors

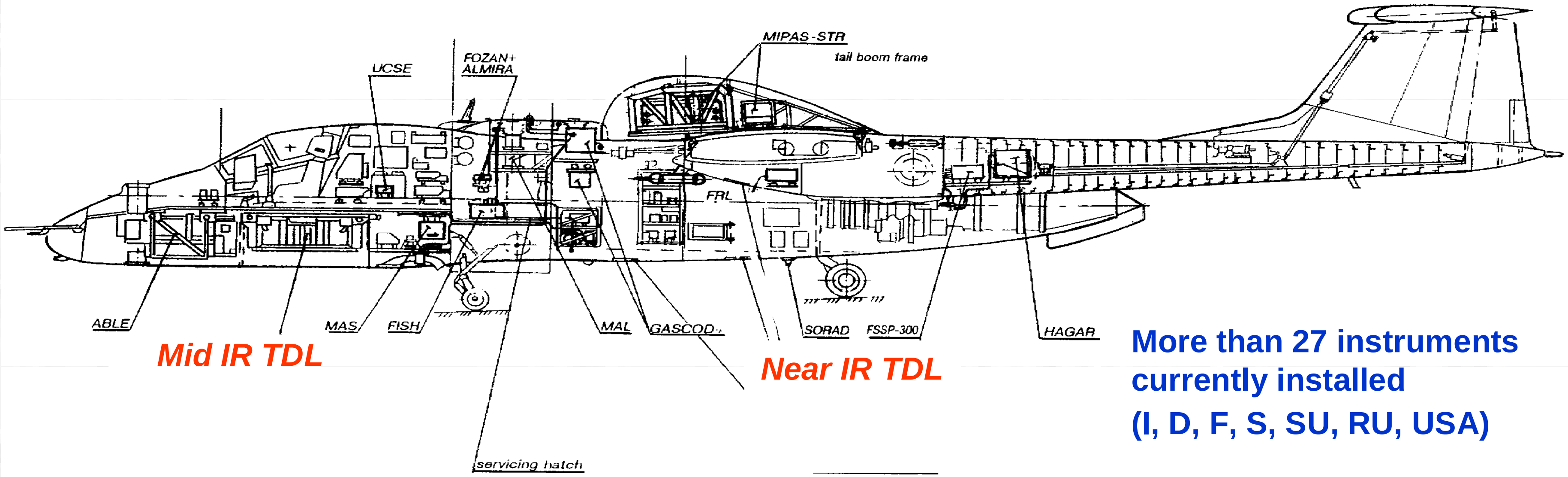
- study of ultra-thin clouds (UTTC, PSC)
- small scale effects leading to mixing phenomena very important in homogeneous and heterogeneous chemistry (tropical convection, polar vortex filaments)

Stratospheric Research Aircraft

Aircraft	**WB-57**	**ER-2**	**M-55**	**Proteus**
Make	EEC	Lockheed	Myasishchev	Scaled Composites
Operated by	NASA	NASA	Geophysica EEIG	Angel Technol. Corp.
Birth	1944 (B57)	1955 (U2)	1988	1998
Flight parameters				
Altitude (m)	18000	21300	21830	18600 (22000 design)
Range (km)	4600	4100	4500	5500
Cruise Speed (m/s)	210	210	210	120
Payload (kg)	2700	1000	1500	3200
Duration (h)	6 h 30’	6 h 30’	5 h 40’	20

Instruments on M55 Geophysica



More than 27 instruments currently installed (I, D, F, S, SU, RU, USA)

INOA instruments :

Mid-Infrared TDL for HNO_3/H_2O or N_2O/CO

Near-Infrared TDL for CH_4 and CO_2

The TDLS on the Geophysica are part of a complete payload system including *in situ* and remote sensing instruments, particle analysis etc...

⇒ **This is necessary to achieve valuable scientific results**

Location of TDLs on M55 Geophysica

A Cryogenically Operated Laser Diode (COLD)

S. Viciani, F. D'Amato, P. Mazzinghi, F. Castagnoli, G. Toci, P. Werle, Appl. Phys. B90, 581-592 (2008) View-PDF

Laser sources:

single mode FP lead salt TDL

λ = 5.8 μm for HNO_3 and H_2O

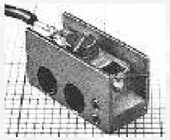
λ = 4.6 μm for N_2O and CO

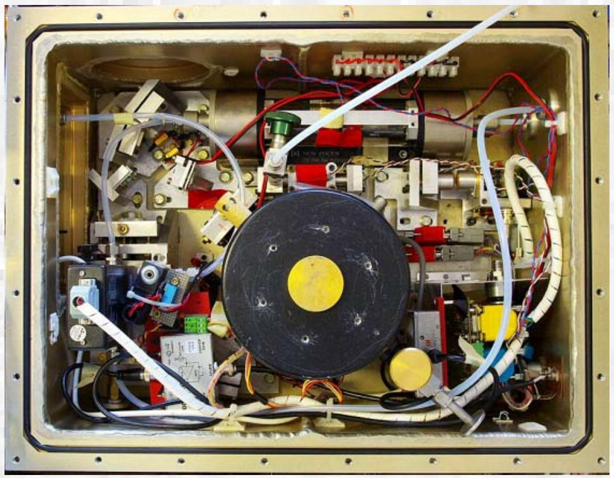
Multipass cell:

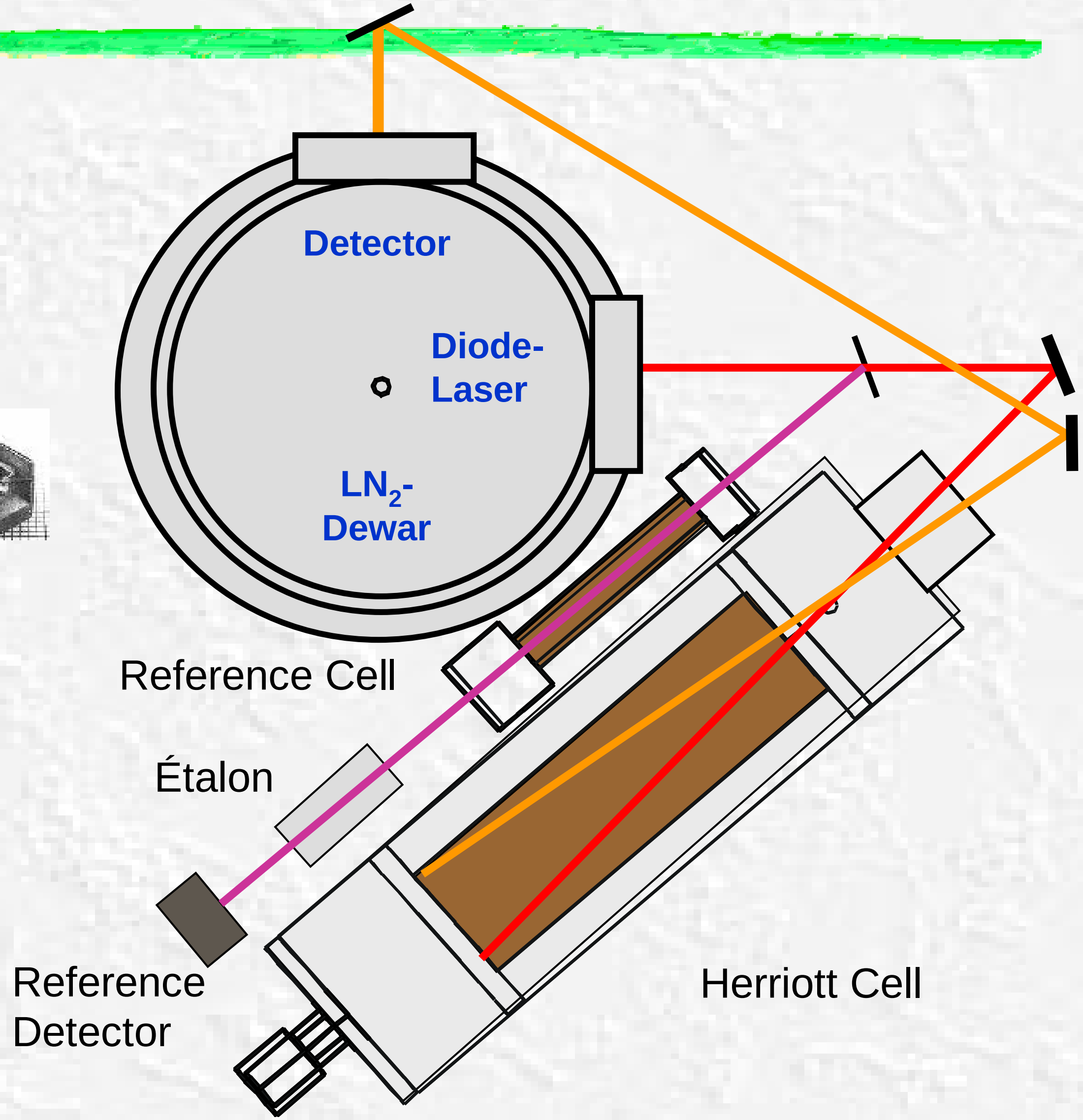
astigmatic Herriott cell

absorption path 36 m

low volume (0.3 *l*)







COLD – Data Processing

Acquisition

- direct absorption with fast sweep integration
- sample rate 5 MS/s @ 12 bit resolution
- 1000 points spectra acquired @ 2 kHz
- up to 64,000 averaged scans
- equivalent resolution up to 28 bit (2.6 10^8)
- interleaved acquisition of reference spectra

Data processing

- FFT filtering and/or fringe subtraction
- lineshape fitting of the averaged spectra
- number density retrieved from HITRAN
- concentration calculated as f(T, P)

Achieved performance

Absorption sensitivity

$< 10^{-5}$ in laboratory tests

$\approx 10^{-4}$ during flights

Ultimate sensitivity is due to fringes, not to detection technique

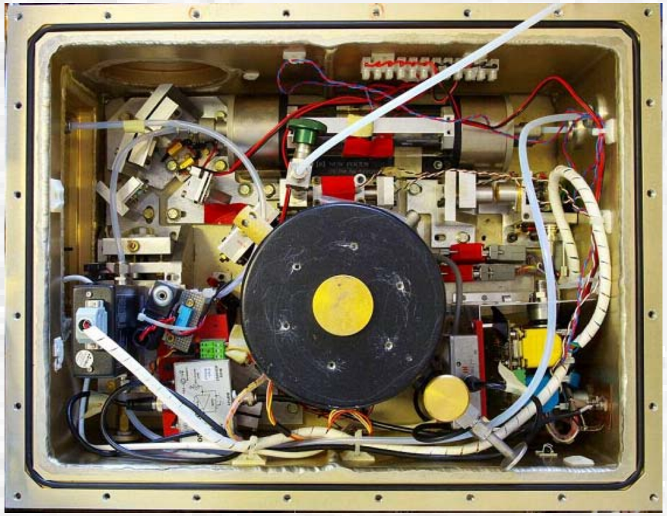
COLD after several campaigns

Learned from campaigns

Liquid nitrogen is not a problem
Actually sometimes it is an advantage

in case of power failure
⇒ the laser remains cool

in case of high humidity on ground
⇒ keeps the whole optics dry
⇒ used for flushing the cell



Reliability was found quite high

⇒ No laser failures during campaigns, just replacements for different targets
⇒ The same set of mirrors still in use after 6 years and 5 campaigns!
⇒ Alignment found very stable (no realignment required in campaigns).

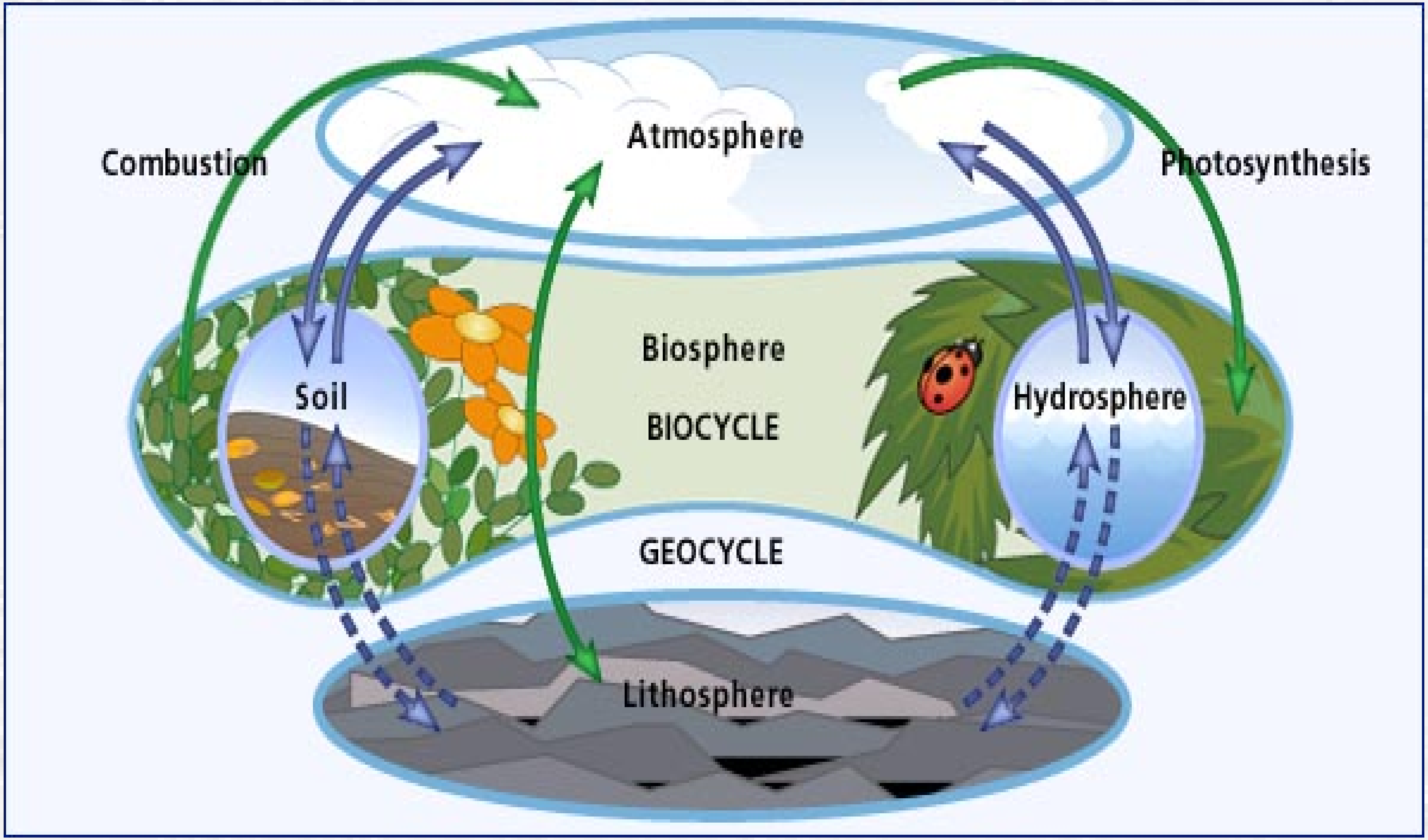
Main problems were:
multimode emission from some lasers
communication failure with the laser controller

Future developments

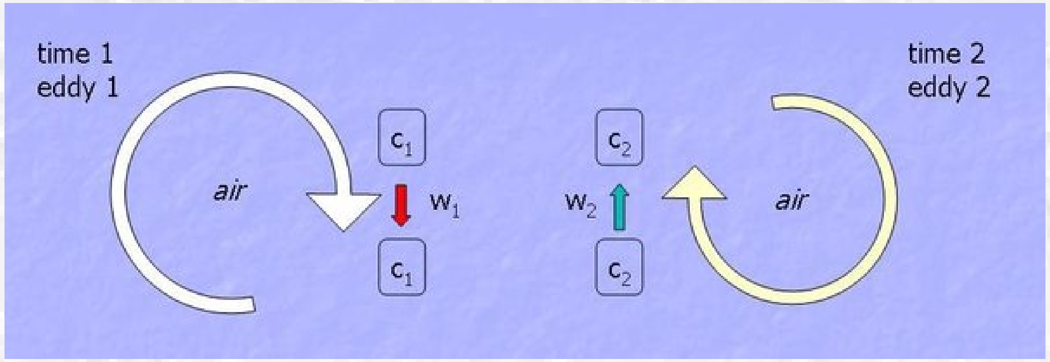
- **Increasingly-sophisticated scientific questions addressed by *in situ* payloads (aircraft, balloon) has increased demand for higher precision, higher accuracy measurements of tracers and water**
- **Aircraft platforms need duplication with differing techniques for continuous intercomparison (TDL, QCL, CRD, DFG, ...)**

- **fast systems for airborne eddy correlation measurements**
- **in-situ measurements of reactive species in open multipass cells**
- **airborne measurements of water isotopes ...**

Biogeochemical cycles - Turbulent Fluxes



Air Flow and Turbulent Vortices



Air flow can be imagined as a horizontal flow of numerous rotating eddies, a turbulent vortices of various sizes, with each eddy having 3D components, including vertical components as well. The situation looks chaotic, but vertical movement of the components can be measured from the tower.

Reynolds Decomposition and Eddy Covariance I

In turbulent flow, vertical flux can be presented as:
($s=\rho_c/\rho_a$ is a mixing ratio of substance '*c*' in the air)

$$F = \overline{\rho_a w s}$$

Reynolds decomposition is used then to break into means and deviations:

$$F = \overline{(\overline{\rho_a} + \rho'_a)(\overline{w} + w')(\overline{s} + s')}$$

Open parenthesis:

$$F = \overline{(\overline{\rho_a}\,\overline{w}\,\overline{s} + \overline{\rho_a}\,\overline{w}\,s' + \overline{\rho_a}\,w'\,\overline{s} + \overline{\rho_a}\,w's' + \rho'_a\,\overline{w}\,\overline{s} + \rho'_a\,\overline{w}\,s' + \rho'_a\,w'\,\overline{s} + \rho'_a\,w's')}$$

Averaged deviation from the average is zero

Equation is simplified: $F = (\overline{\rho_a}\,\overline{w}\,\overline{s} + \overline{\rho_a}\,\overline{w's'} + \overline{w}\,\overline{\rho'_a s'} + \overline{s}\,\overline{\rho'_a w'} + \overline{\rho'_a w' s'})$

Reynolds Decomposition and Eddy Covariance II

Then important assumption is made (for conventional Eddy Covariance) – density fluctuations are assumed negligible:

$$F = (\overline{\rho_a}\,\overline{w}\,\overline{s} + \overline{\rho_a}\,\overline{w's'} + \cancel{\overline{w}\,\overline{\rho'_a s'}} + \cancel{\overline{s}\,\overline{\rho'_a w'}} + \cancel{\overline{\rho'_a w' s'}}) = \cancel{\overline{\rho_a}\,\overline{w}\,\overline{s}} + \overline{\rho_a}\,\overline{w's'}$$

Then another important assumption is made – mean vertical flow is assumed negligible for horizontal homogeneous terrain (no divergence/convergence):

$$F \approx \overline{\rho_a}\,\overline{w's'}$$

'Eddy flux'

Measurement of Turbulent Fluxes

Sonic Anemometer

- measures transit time of ultrasonic pulse $\rightarrow$ depends on air velocity
- three velocity components
- at $\geq$ 10 Hz: resolves most fluctuations in turbulence

$$w = \bar{w} + w'$$

Laser Sensor

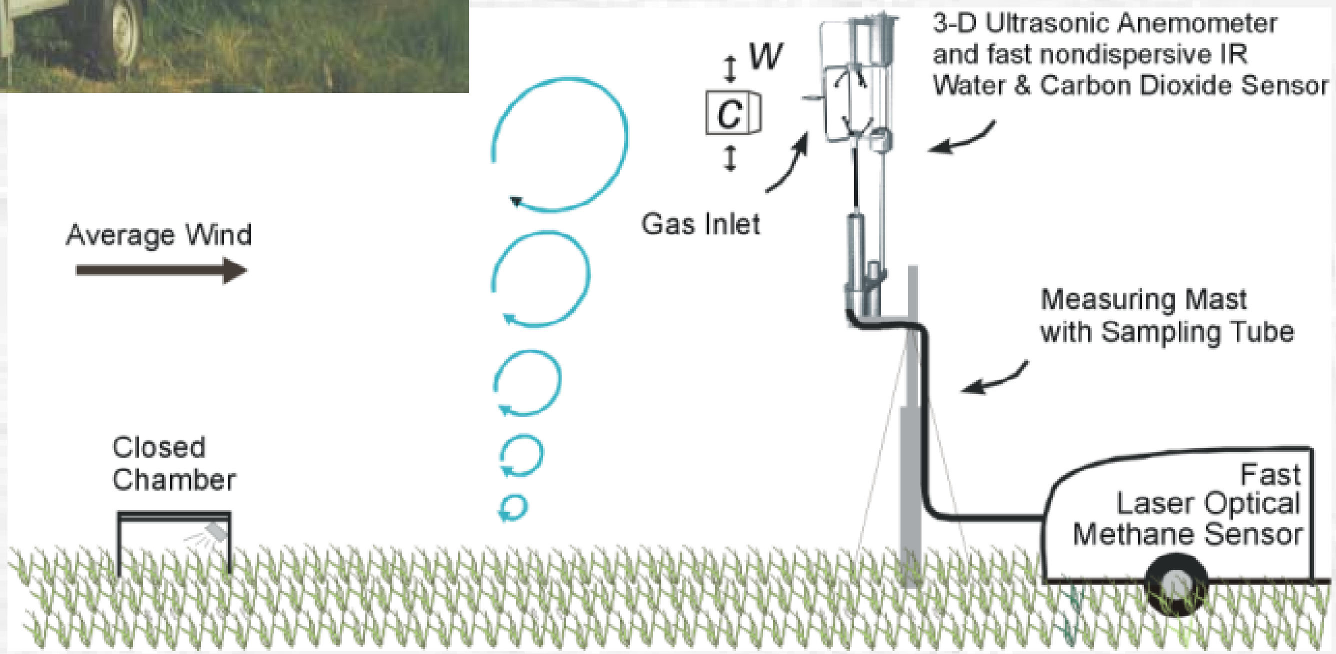
- Time-lag analysis with sonic signals

$$C = \bar{C} + C'$$

The fast diode-laser trace gas sensor

TO DO :

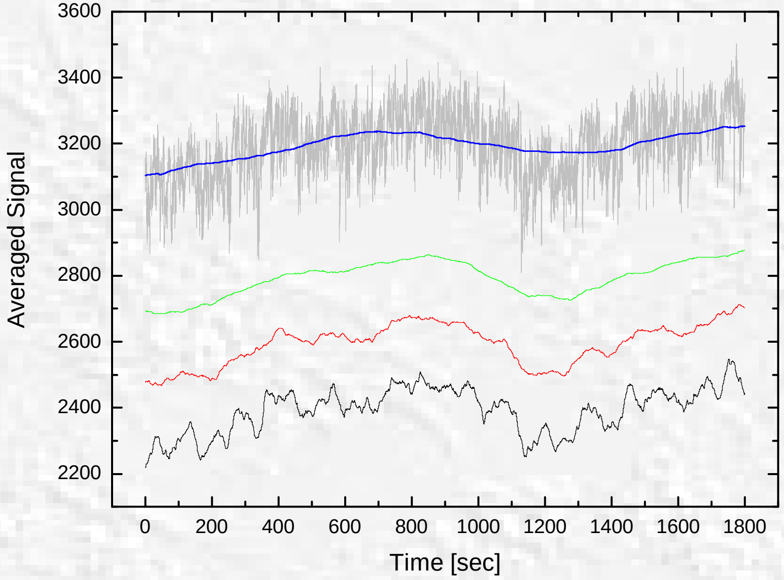
- **detrending**
- **frequency spectra**
- **covariance and cospectrum**
- **time lag**
-



Detrending of time series data

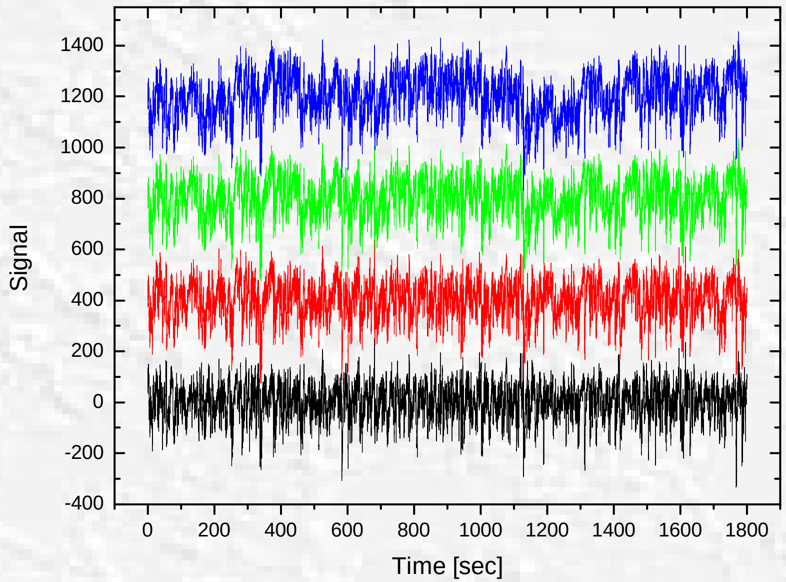
Smoothing effect of the moving average filter with different time constants

Low pass filtered



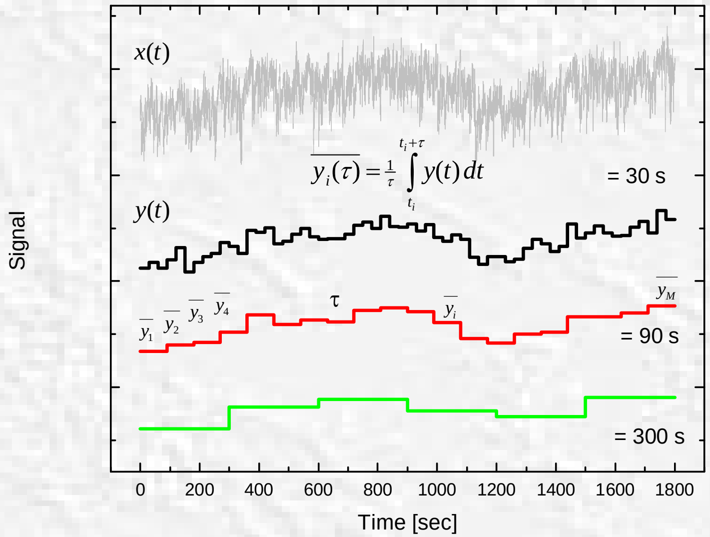
$$y[i] = \sum_{j=-(M-1)/2}^{(M-1)/2} \frac{1}{M} \cdot x[i-j]$$

High pass filtered

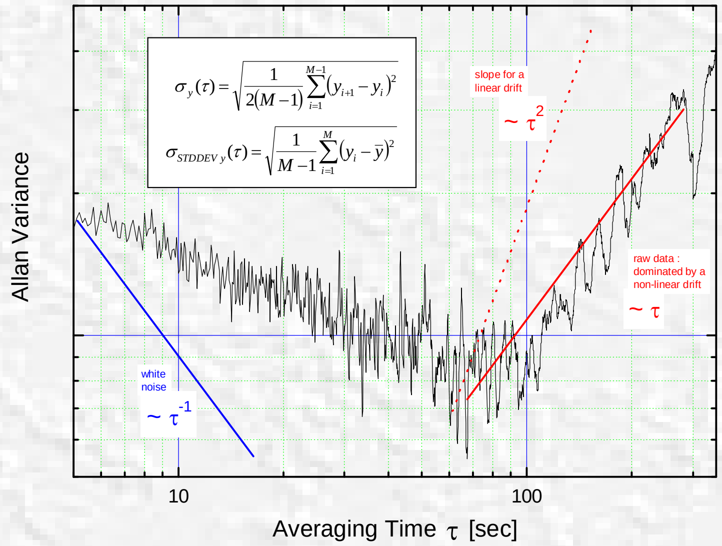


$$y(t) = [\delta(t) - h(t)] * x(t)$$

Detrending : What is the optimum time constant ?

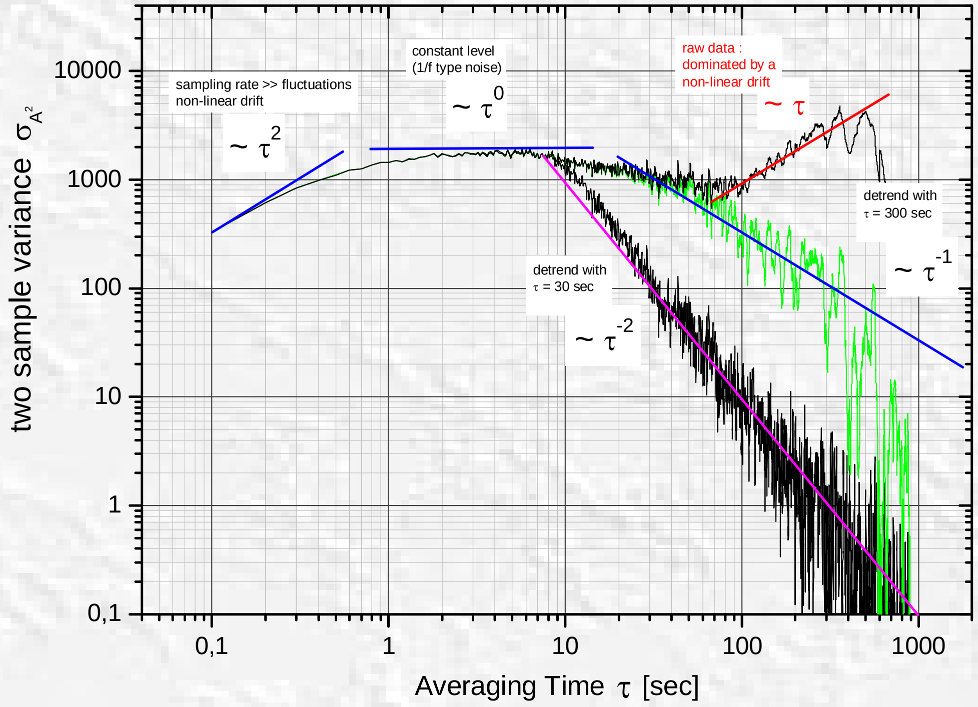


10 Hz time series data together with selected plots for subensemble averages with bin-sizes of 30s, 90s and 300s.



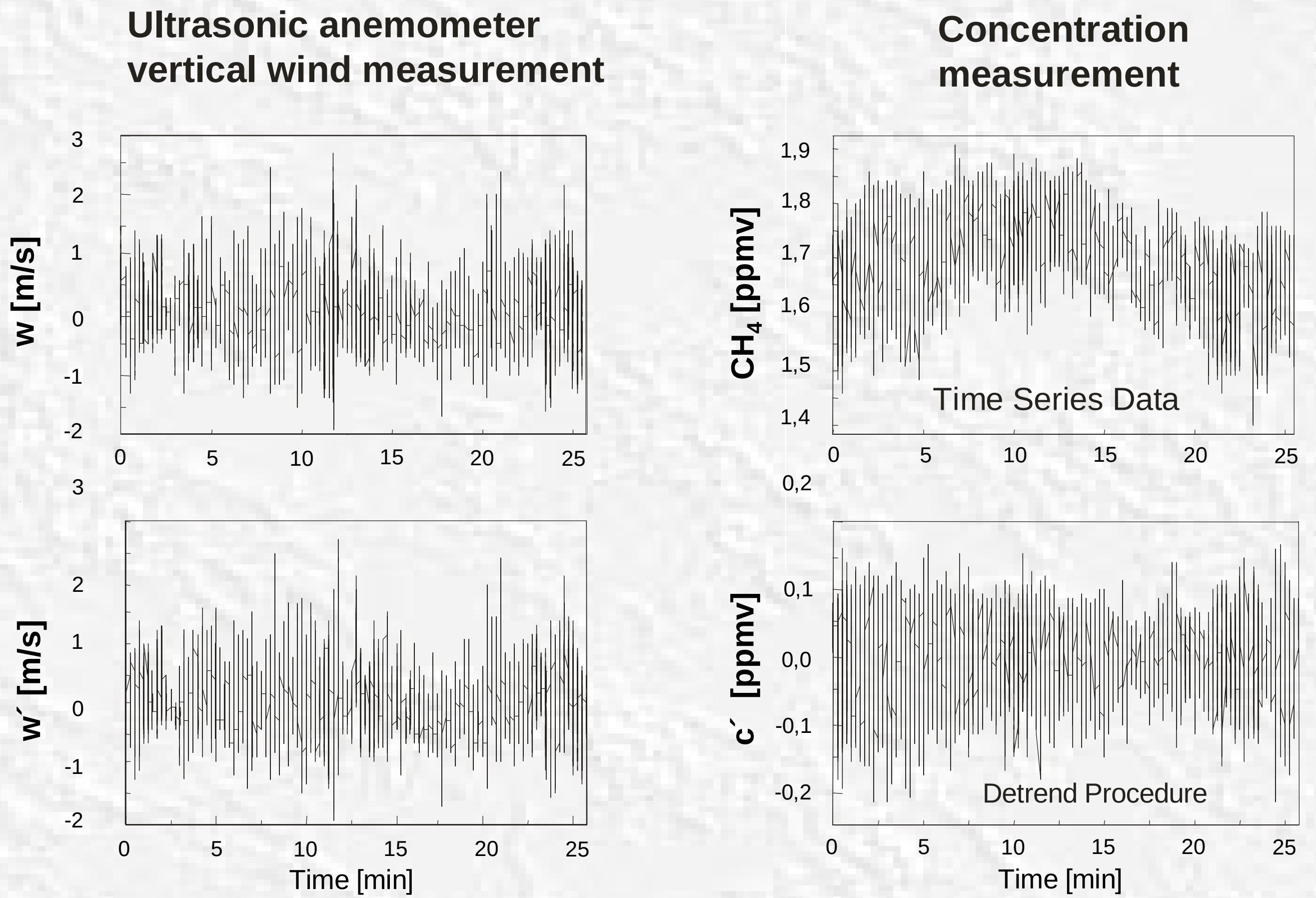
Plot of the two sample variance as a function of the subensemble averaging time t. The line following t-1 indicates the expected behaviour for a “white noise” dominated system.

Stability Analysis vs Filter Time Constant



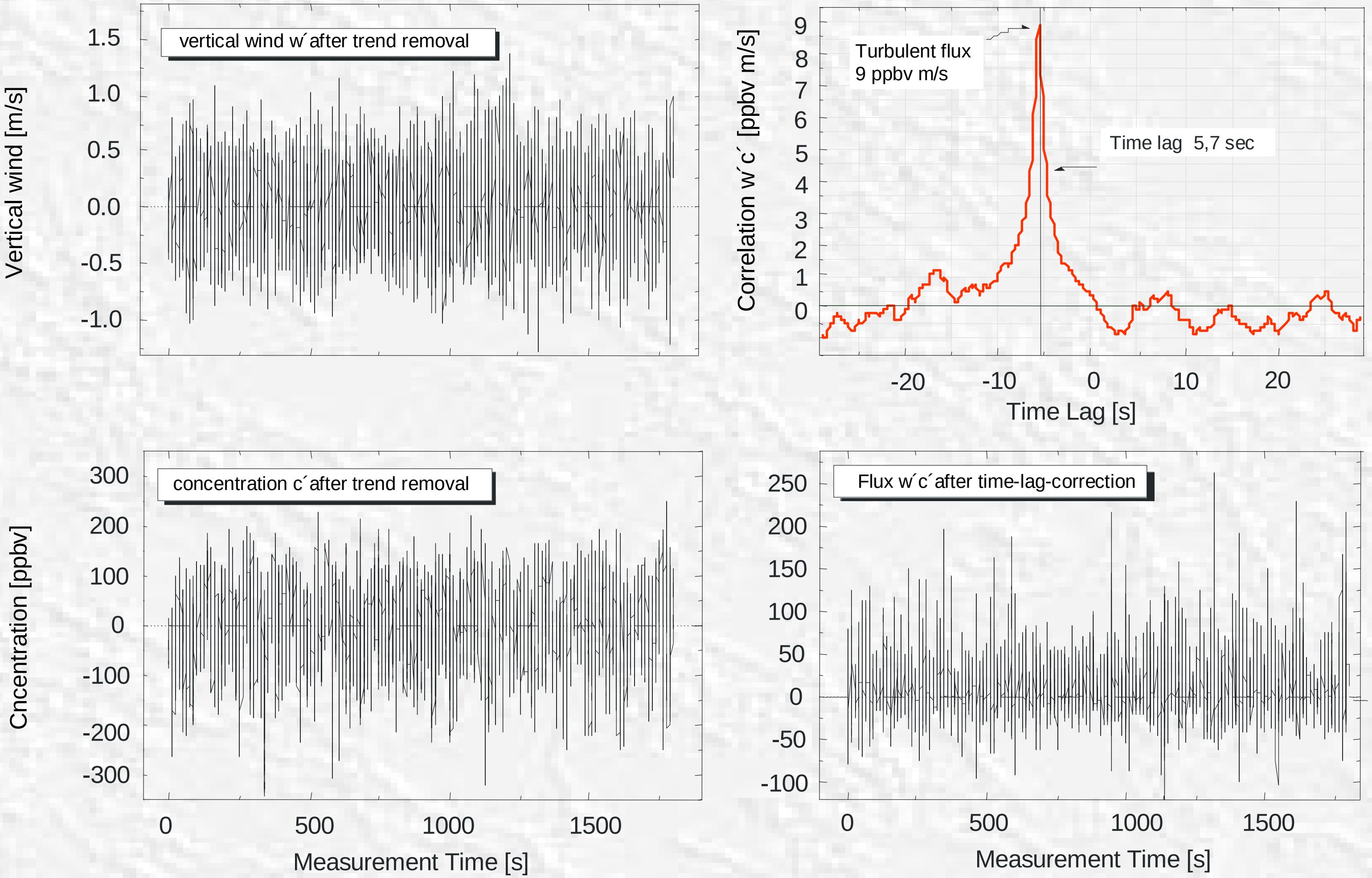
Two sample variance characterization of a trace gas concentration time series in the time domain. For averaging intervals below 1 s atmospheric turbulence is well resolved and appears as a ´non-linear drift´, while in the range between 1s to 10s ´flicker noise´ dominates. The upper right part is the drift dominated behaviour of the raw data. The middle trace can be considered as ideal and corresponds to the application of a 300 s moving average filter for detrending. The lower trace belongs to the 30 sec time constant.

Detrended time series data to get the fluctuations



„running means“ or „high-pass filtering“ : Allan Variance and be used to determine the high pass constant

Turbulent flux after time lag correction

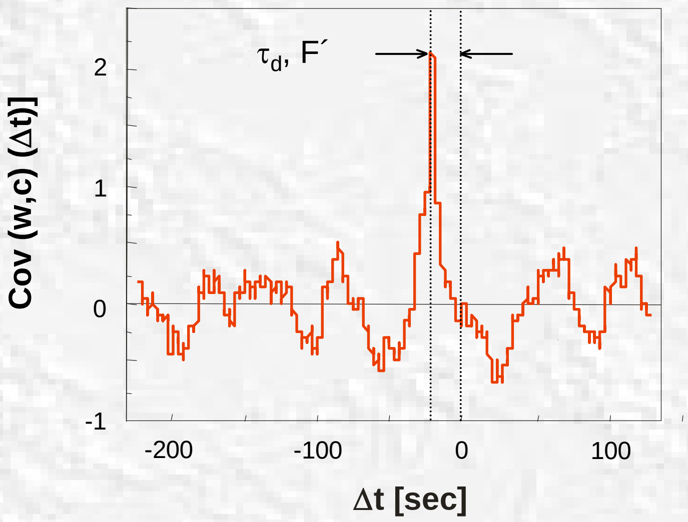


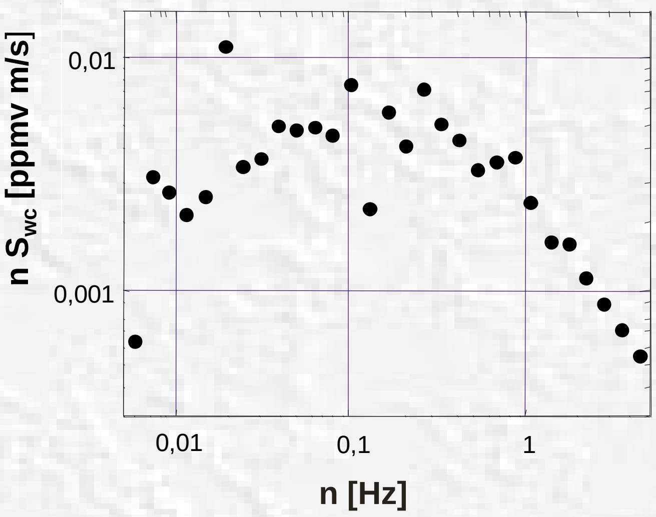
Covariance & Cospectrum

$$Cov[w,c](\Delta t) \propto \int w'(t+\Delta t)\cdot c'(t)\cdot dt \qquad C_{w'c'}(n) \propto \mathrm{Re}\left[W(n)\cdot C^{*}(n)\cdot e^{2\pi i n \tau_d}\right]$$

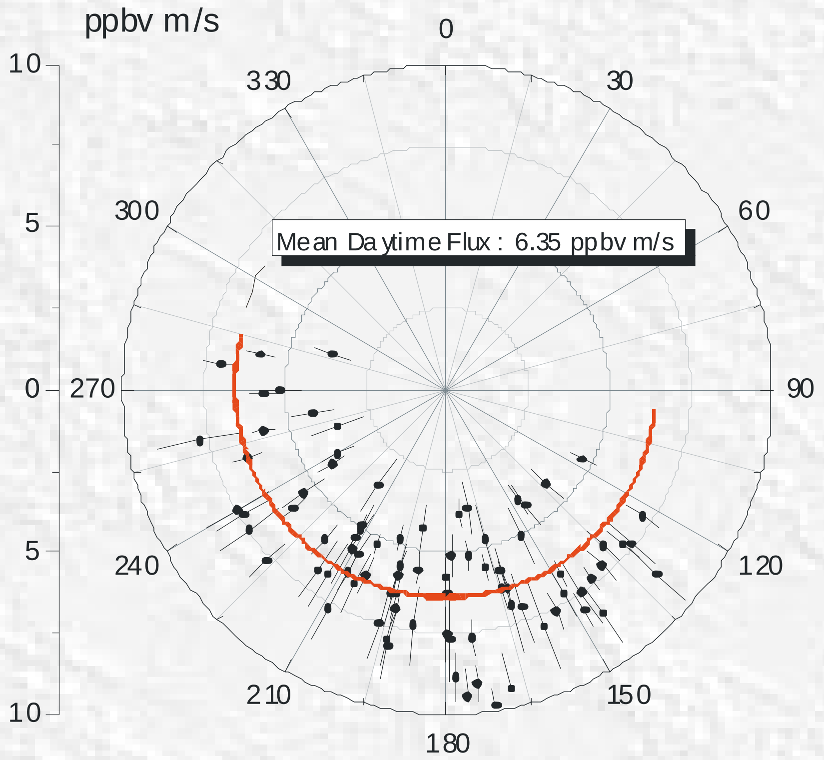
Turbulent Flux $F' = Cov\,[w,c]\,(\tau_d)$

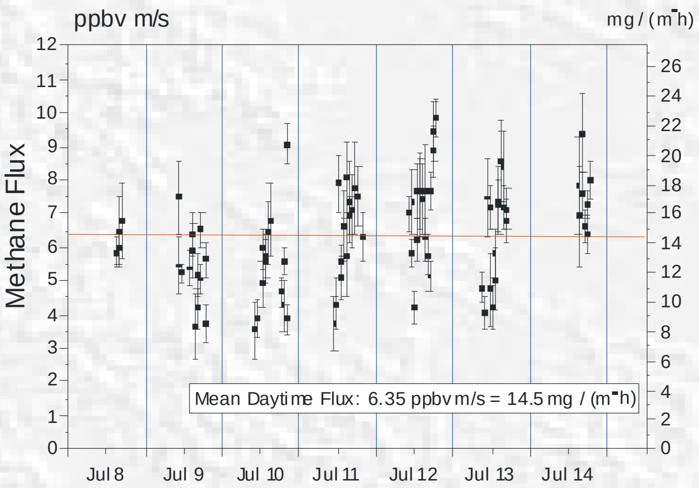
Time Lag —— τ_d ⟶





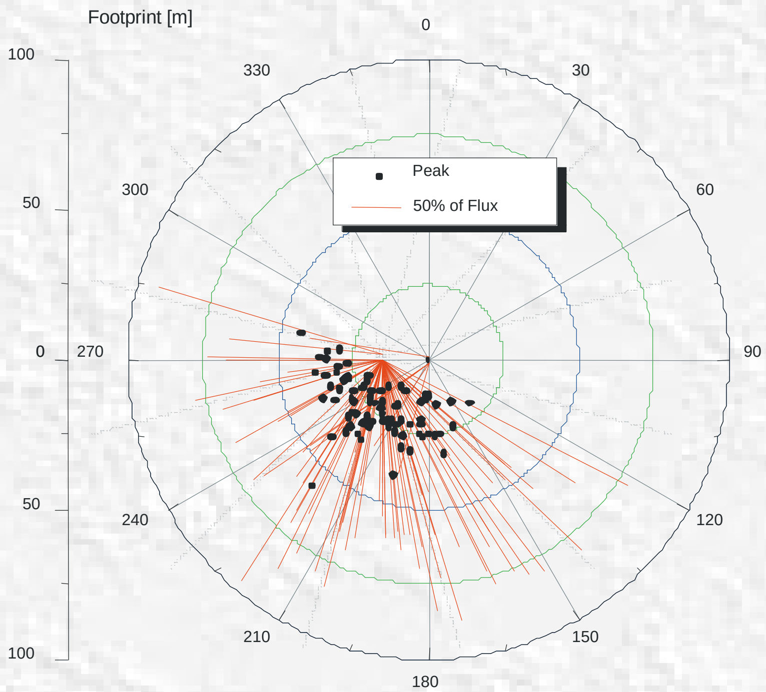
Mean daytime flux vs wind direction

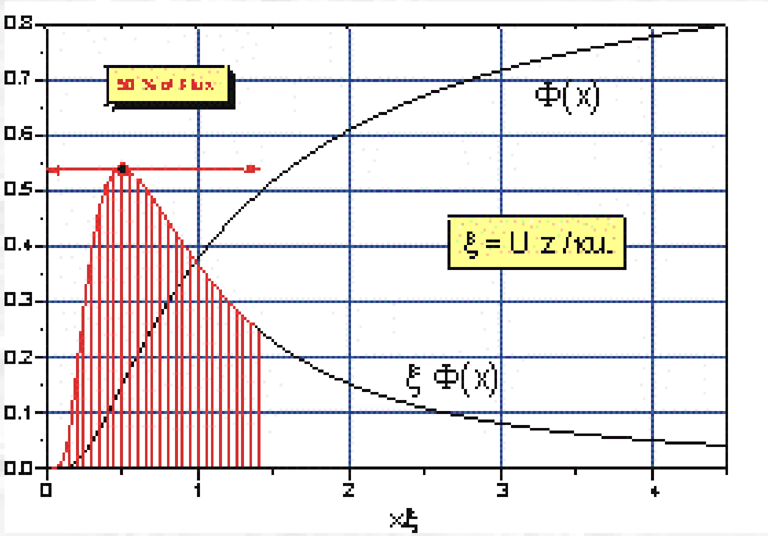




Mean daytime flux : 6,35 ppbv m/s

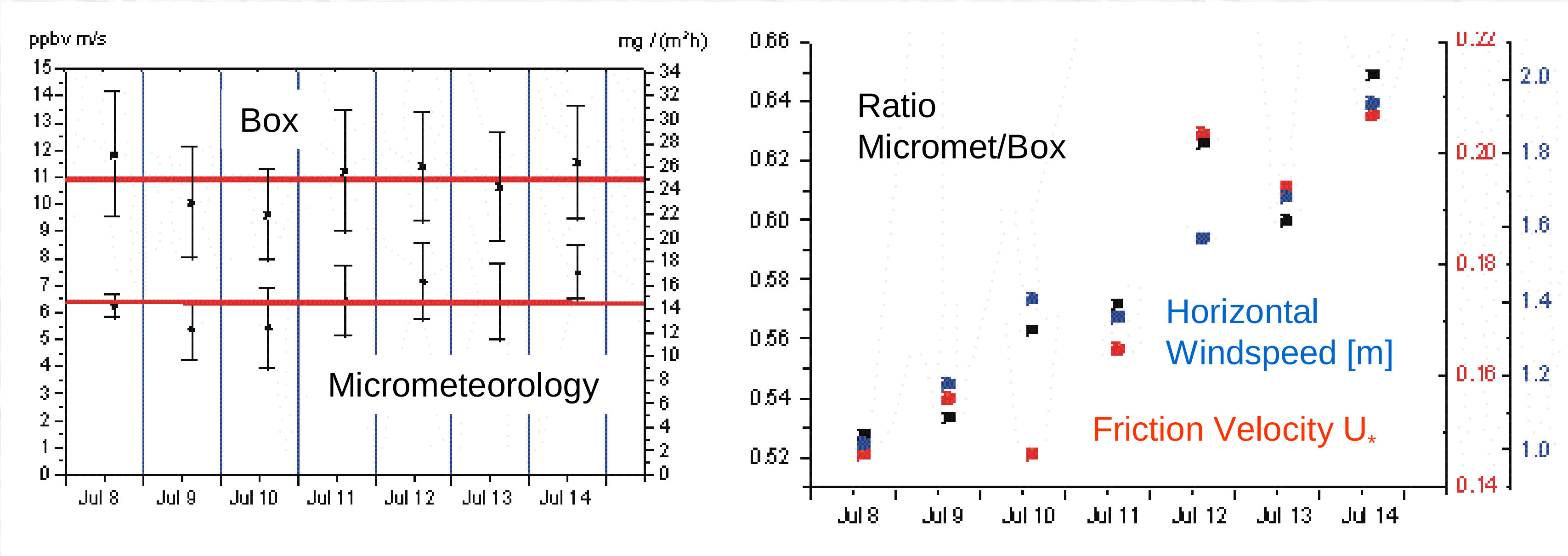
Footprint estimation





Schuepp et. al., Bound.-Lay. Met 50, 355 (1990)

Results .....



The closed chamber measurements reported to about **70%** higher CH_4 fluxes than the eddy corrrelation instruments (3 independent systems).

Closed chamber measurements may overestimate methane fluxes from rice paddy fields.

Werle, P., Kormann, R., 2001. A fast chemical sensor for eddy correlation measurements of Methane emissions from rice paddy fields. Appl. Opt. 40, 846-858.

Denmead, O.T., 2008. Approaches to measuring fluxes of methane and nitrous oxide between landscapes and the atmosphere. Plant Soil 309, 5–24.

Problems that challenge EC measurements at night

high frequency motions / small scale turbulence not captured

stationarity criteria not fulfilled / similarity relations not valid

footprint problems

failure of EC method under low turbulence conditions

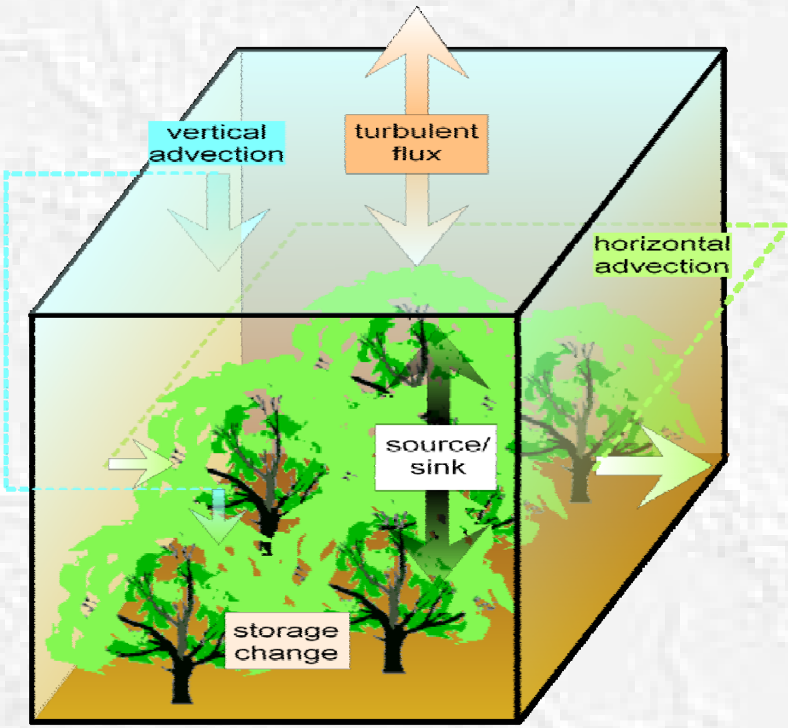
reference measurement level decoupled from surface processes

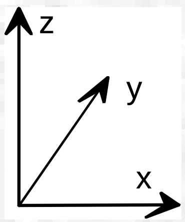
horizontal transports ignored

non turbulent (low frequency) fluxes not captured
(averaging interval, advection, storage)

Carbon Balance Equation

$$\int_0^{z_r} S(t,z)dz = NEE = \int_0^{z_r} \frac{\partial \bar{c}(z)}{\partial t} dz + \overline{w'c'}(z_r) + \int_0^{z_r} \bar{w}(z)\frac{\partial \bar{c}(z)}{\partial z}dz + \int_0^{z_r}\left(\bar{u}(z)\frac{\partial \bar{c}(z)}{\partial x} + \bar{v}(z)\frac{\partial \bar{c}(z)}{\partial y}\right)dz$$





I source/sink of *c*

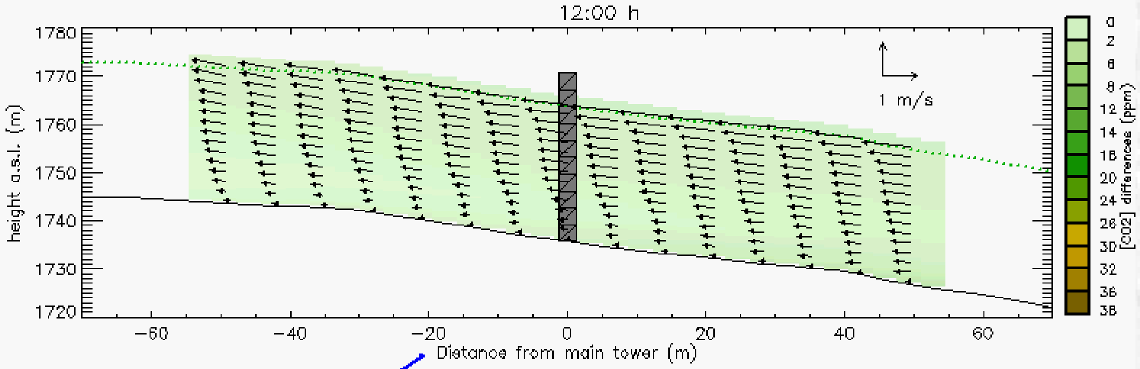
II storage change
(Finnigan, 2006; Yang et al., 2007)

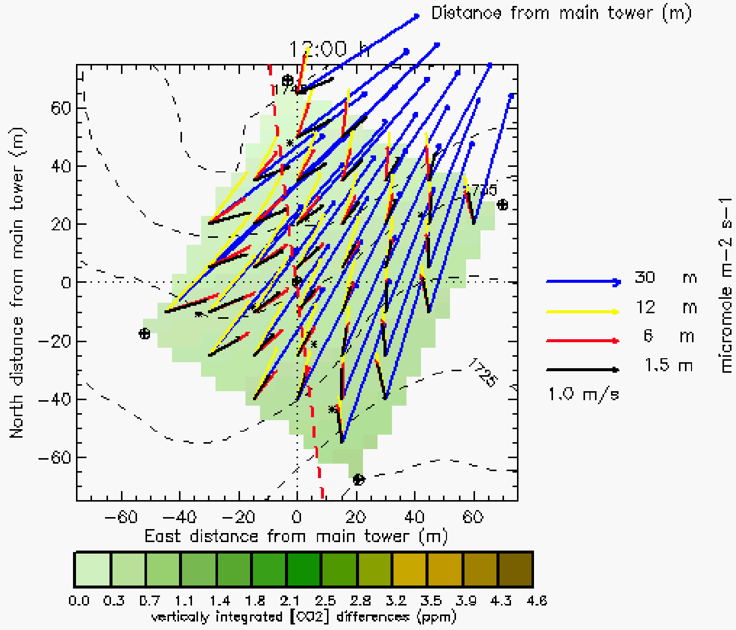
III turbulent flux
(EUROFLUX, Aubinet et al., 2000; FLUXNET, AFM Vol. 113, 2002; Loescher et al., 2006; FLUXNET Canada, AFM Vol. 136, 2006)

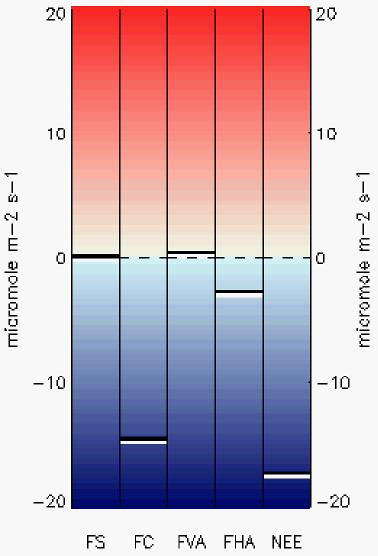
IV vertical advection
(Lee, 1998; Finnigan, 1999; Baldocchi, 2000; Paw U, 2000, Vickers and Mahrt, 2006; Sun et al., 2007; Heinesch et al., 2007)

V horizontal advection
(Aubinet et al., 2003; Staebler and Fitz-jarrald, 2004; Feigenwinter et al., 2004; Marcolla et al., 2005; Moderow et al., 2007; Feigenwinter et al., 2008; Sun et al., 2007; Heinesch et al., in press; Yi et al., in press)

The winds are changing …



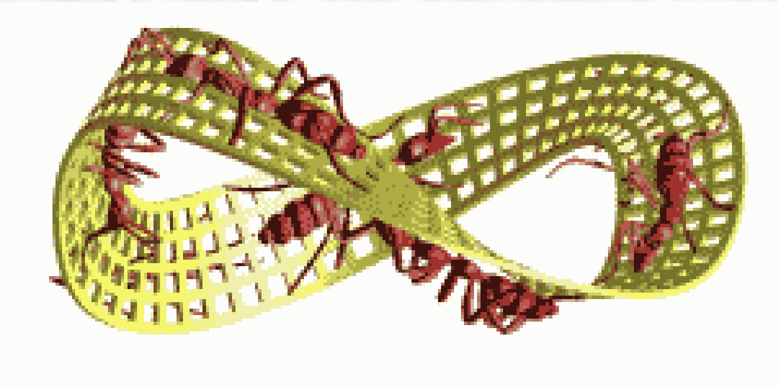




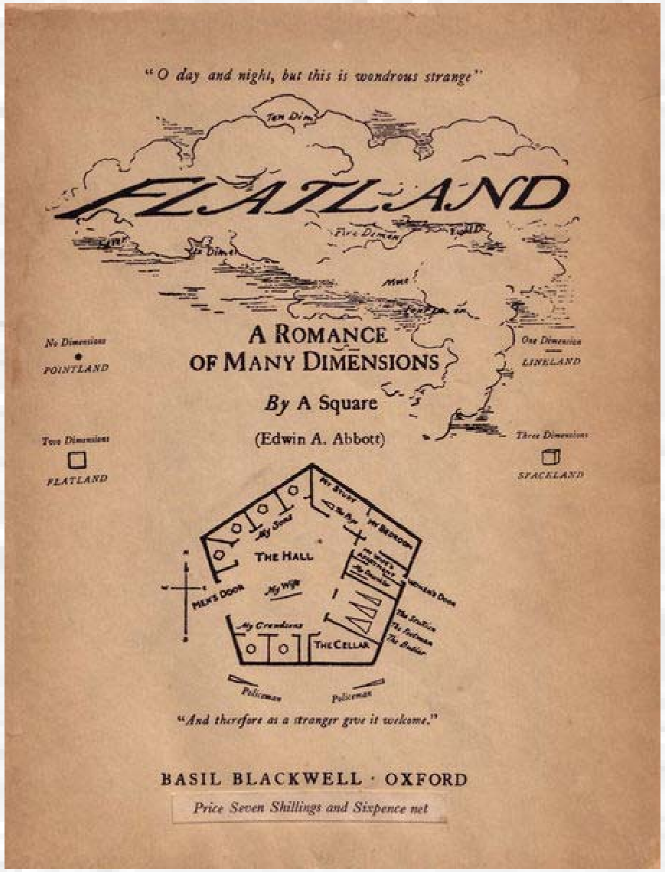
Renon slope wind system

„Houston we have Advection“

What do we know about the „3rd dimension“ ?



In the book, the three-dimensional Sphere has the ability to stand inches away from a Flatlander and observe them without being seen, can remove Flatland objects from closed containers and teleport them via the third dimension without traversing the space in between, and is capable of seeing and touching the inside and outside of everything in the two-dimensional universe



Flatland: A Romance of Many Dimensions
1884 science fiction n novella by Edwin A. Abbott

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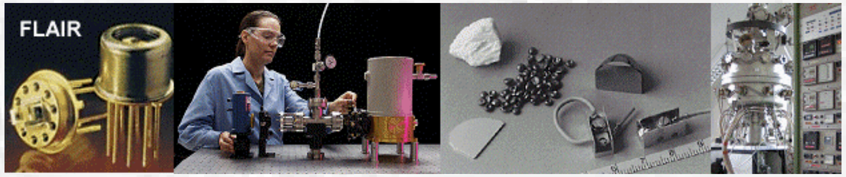

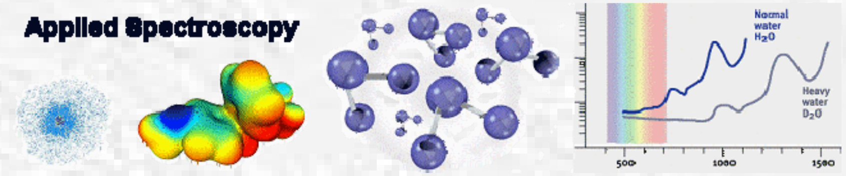

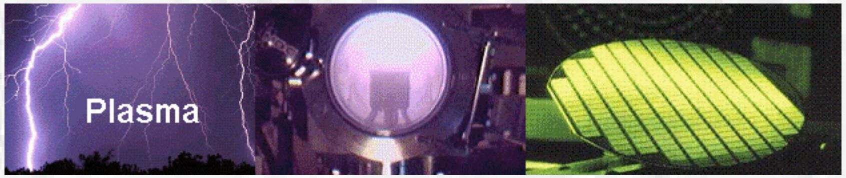

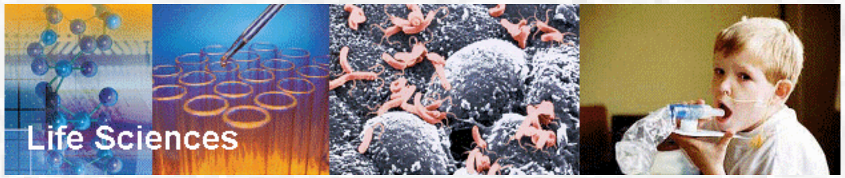

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