



2023-18

Workshop on Topics in Quantum Turbulence

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Experiments on Vibrating Structures in 3He

BRADLEY David Ian

University of Lancaster Department of Physics LA1 4YB Lancaster UNITED KINGDOM Experiments on Turbulence with Vibrating Structures in Superfluid ³He

Ian Bradley



Plan of talk

- Basic superfluid ³He
 - Vortices
 - Andreev scattering
- Vibrating Wire experiments
- Vibrating Grid experiments
- Tuning Forks

³He Phase Diagram

Superfluid phases formed by Cooper pairs with S=1, L=1





At low temperatures, quasiparticle excitation number falls rapidly

 $n_{\rm ex} \propto \exp(-\Delta/k_B T)$

Mean free path virtually infinite – ballistic quasiparticles

Vibrating objects

at reasonable oscillation amplitudes are simple driven damped harmonic oscillators with motion governed by

$$m\ddot{x} + \mathcal{F}(\dot{x}) + kx = F_{drive}$$

with *m* a mass parameter, *k* a restoring force parameter, and $\mathcal{F}(v)$ describing the damping.

$$\mathcal{F}(v) \propto v$$
 for viscous drag
 $\mathcal{F}(v) \propto v^2$ for turbulent drag

Quickly look at the response for a vibrating wire

In ⁴He, there is a clear hysteretic transition from a low damping regime to a high turbulent damping regime







In ³He-B, life is more complicated. Again, results for a vibrating wire.



- critical velocity to pair breaking regime
- temperature dependent non-linear damping Andreev Scattering
- no clear sign of turbulence

If the liquid is in motion, then we see the dispersion curve in a moving frame of reference. Excitations approaching will have higher energies by $\sim p_{\rm F} v$ and those receding lower energies by the same amount





quasiparticles move with constant energy

• if one moves into a region where there is no available state it Andreev reflects

negligible change in momentum

Changes state from a quasiparticle to a quasihole (or vice versa)

- result is that as the wire moves faster, less quasiparticles are able to scatter off the wire resulting in a reduced damping
- wire moves even faster for a given driving force
- higher temperature, more thermally excited quasiparticles, therefore larger effect

Andreev scattering of quasiparticles by the turbulence flow field gives rise to the main turbulence detection technique

move object even quicker...

When the distortion in the dispersion curve, p_Fv , becomes as large as the gap Δ , the minimum in the dispersion curve goes to zero and thus quasiparticles can be freely created. Cooper pairs are broken and superfluidity begins to be destroyed at a velocity of Δ/p_F .



This makes analysis of the damping due to turbulence difficult as pair breaking and turbulence generation seem to occur together

Vibrating wires

Most commonly used wires made from multi-filamentary superconducting wire removing all but one of the filaments (typically 60 or so!)



Typical 4.5 μm vibrating wire with a 2.64 mm leg spacing prior to cleaning up the ends of the legs



Two filaments from the same multifilmentary wire



central filament in bundle



edge filament in bundle

Wires are not smooth or necessarily round!

Micro-fabricated wires have also been proposed for quantum turbulence studies



A silicon vibrating wire fabricated by reactive chemical etching with KOH.

The wire surface is smoother by chemical etching than by reactive ion etching.

The roughness of the surface is $\sim 1 \mu m$.

resonant frequency 8.7kHz, $Q \sim 10^5$

Hayashi, Nakagawa, Yano, Ishikawa and Hata, Physica B 329–333, 108, 2003



Prototype silicon vibrating goal post structures $10\mu m \times 20\mu m$ formed by a combination of chemical etching and reactive ion etching. "The poor straightness of the Silicon shape is due to the rather poor quality of the optical lithography."

resonant frequency 4.7kHz, $Q \sim 10^4$

(ULTIMA project)

Triqueneaux et al, Physica B 284, 2141, 2000Collin et al,JLTP 150, 739, 2008

Detection of turbulence by a moving wire



S.N. Fisher et al, PRL 86, 244, 2001











So, in one dimension both incoming quasiholes and quasiparticles must make <u>one</u> Andreev reflection process.

Therefore an incoming quasihole goes out as a quasiparticle and an incoming quasiparticle goes out as a quasihole.

In both cases, no momentum is exchanged with the wire.

How does this affect the damping?



Look at the response of the "detector wire" as we drive the source wire at just above the critical velocity



While we drive the source wire beyond the critical velocity the quasiparticle wind increases the damping on the second wire simply because there are more excitations to provide damping.



If try higher velocities.



- clear fall in damping while source wire is driven
- noisy signal
- effectively a rather blurry one pixel camera looking at the shadows cast by the local turbulence



Conclusion

We detect the presence of turbulence as a fall in the damping by incoming thermal excitations on the detector wire because of the shadowing effect of the turbulence

Production of turbulence by a moving wire





- clear turbulence onset at pair breaking critical velocity
- VWR to the side sees no shielding, similarly a VWR above array sees nothing
- conclude turbulence along direction of quasiparticle beam
- turbulence extent falls roughly exponentially over length scale ~2mm

Bradley et al, *Physica* B 329, 104, 2003



a vibrating wire thermometer
 a vibrating wire heater

o a small hole

heat box to produce a quasiparticle beam

turn on generator wire to produce turbulence

measure the additional power reflected into the box by Andreev reflection of quasiparticles from the beam by the turbulence

relate fraction reflected to the vortex line density



B lack body radiator contains

Know how to relate the reflected fraction to the line density from previous work (Bradley et al, *Physica* B 329, 104, 2003)

result is that *L* proportional to the reflected fraction *f* and the extent of the turbulence *x*

$$L = f \frac{2m_3 k_B T}{p_F \hbar x}$$



Although, as we heard on Tuesday, more sophisticated calculations suggest that the reflected fraction for complex systems is less than simply the sum of the fraction expected from single vortices...

So our *L* is a lower limit!



[•] inset is the temperature dependence at $v/v_c = 1.5$

• suggests reaching the low temperature limit

PRL 93, 235302 (2004)

Turbulence only generated once the wire exceeds the pair breaking velocity

➢ is this true?

turbulence generation starts



Drive level (force)

The dependence of velocity on drive: the ideal case

The Dependence of Velocity on Drive: the Reality





PRL 84, 1252 (2000).





Osaka City group – two VWR's at 183Hz and 47Hz used one as turbulence generator and one as detector

observed pair breaking and turbulence production in both



Is this a manifestation of the suggested frequency dependence of some critical velocity?

The Vibrating Grid Resonator



Grid response as a function of driving force for several temperature ranges additional warming due to heating at high drives





Ratio the two signals gives the damping suppression by turbulence. Investigate build up and recovery of turbulence signal





Vortex rings

Ballistic emission of vortex rings

The turbulence is measured at a distance of 1 mm from the grid.

For such a short time constant of ~0.1 sec, the rings must travel at ~10 mm s⁻¹



self-induced motion of vortex ring.

ring propagation speed: $u \cong \kappa/2\pi d$

 $u \sim 10 \text{ mm s}^{-1} \Rightarrow d \sim 5 \text{ }\mu\text{m}$



Grid frequency is 1250 Hz

First Kelvin wave resonance for loops of order ~5 µm

and generates $\sim 5 \ \mu m rings$

Grid thus produces a cloud of similar sized rings

Vortex rings shrink due to mutual friction

estimated range for vortex ring size R is $x \sim R / q$ (Donnelly)

The mutual friction parameter q is strongly temperature and pressure dependent

Extrapolating the published higher temperature data experimental data (Bevan et al JLTP 109, 423, 1997) allows estimates of the temperatures at which the rings can just reach the nearest detector wire for different pressures...

so we measure the signal size as a function of temperature...



Data consistent with the range estimates



At low grid velocities, independent loops are created which travel fast (~10 mm/s) and disperse rapidly.

Above a critical grid velocity, the ring density becomes high enough for a cascade of reconnection to occur, rapidly creating fully-developed turbulence which disperses only slowly.







The white points are taken from Akira's calculation.



Estimated vortex line density from the shielding compared to ⁴He data and Komolgorov-like $t^{-3/2}$ decay ⁴He parameter fit of an effective kinematic viscosity of v'=0.5v fails for ³He Vinen' suggestion of effective kinematic viscosity of v' $\propto \kappa$ fits both



- turbulent signals appear noisy due to fluctuations in the line density
- dominant fluctuations on time scales of the order of a few seconds or more

Turbulent fluctuations on detector wire from grid, 5.8 mm/s



look for correlations in the fluctuations between detector wires

Define the instantaneous fluctuation in the line density $\delta L(t)$ as the deviation from the time averaged value $\langle L \rangle$

$$\delta L(t) = L(t) - \left\langle L \right\rangle$$

Then the correlation between the two detector wires as a function of the delay time Δt

$$R_{1,2} = \frac{\left\langle \delta L_1(t) \, \delta L_2(t - \Delta t) \right\rangle}{\sqrt{\left\langle \delta L_1^2 \right\rangle} \, \sqrt{\left\langle \delta L_2^2 \right\rangle}}$$

(detector 1 is nearest the grid)

0.6 0.4 0.2 0.0 -10 -8 -6 -4 -2 0 2 4 6 8 10 time, s

01, 065302, 2008

delay ~2 secs between the wires 1 mm apart

Cross correlation

- delay ~4 secs between the two wires 2 mm apart
- implies turbulence is long-lived on scale of a few seconds
- mean flow of turbulence away from the grid of ~0.5 mm s⁻¹



- delay ~2 secs between the wires 1 mm apart
- delay ~4 secs between the two wires 2 mm apart
- implies turbulence is long-lived on scale of a few seconds
- mean flow of turbulence away from the grid of ~0.5 mm s⁻¹

Power spectrum of fluctuations on detector wire 1mm from grid



- above 3 mms⁻¹ grid velocity (developed turbulence) power law $f^{-5/3}$ above 0.1Hz
- below 3 mms⁻¹ grid velocity (ballistic rings) power law f⁻¹
- use mean flow 0.5 mms⁻¹ to estimate turbulence length scales ($\lambda \sim v/f$)
 - > a few millimetres at start of $f^{-5/3}$ power law behaviour
 - $> \sim 0.1$ mm where $f^{-5/3}$ power law merges with noise

Quartz Tuning Forks

Small, cheap, reliable First proposed for LT work by the Nottingham group Clubb et al *JLTP 136, 1, 2004*

Developed further by Helsinki, Kosice/Prague & Lancaster groups

To date, used to detect quantum turbulence in ³He only in a qualitative manner

e.g. Blažková et al, JLTP 150, 525, 2008

but little quantitative although this is developing

Excite tuning fork and measure the current. Key point current ∞ velocity





- similar pair breaking velocities
- tuning fork sees non-linear damping expected for oscillating object in ³He-B
- tuning fork damping ~x12 greater than that of wire
- VWR more sensitive than this particular fork

Fork 1.5 mm away from grid VWR's 1, 2 and 3 mm away from grid



Fractional screening seen by tuning fork much less than that seen by VWR's Do we need smaller forks?

active region

Our wires have typical dimensions and active regions covering several mms.

few mm



What about a real digital vortex video camera – say with 9 pixels?

We start with a black-body radiator emitting a beam of excitations.





Conclusions

• Turbulence easily generated by vibrating wires and grids

• vortex line densities Wire $L \sim \text{few } \times 10^7 \text{ m}^{-2}$ Grid $L \sim \text{few } \times 10^8 \text{ m}^{-2}$

• grid initially produce rings which at high production rates reconnect to form developed static turbulence

• Fluctuation correlations between detectors and power spectrum analysis suggests Richardson cascade and Komogorov-like energy spectrum

• Tuning forks can detect the shielding of quasiparticles by turbulence but currently, sensitivity is relatively small