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Simulations on Vibrating Structures and a Simple Model for the Critical Velocity

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Simulations on Vibrating Sphere and Tilted Rotating Cylinder

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Outline

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- Introduction
- Numerical simulations with vortex filament model
- What is the steady state like?

2 Tilted rotating cylinder: steady state turbulence?

- Background and motivation
- Motion of ideal fluid
- Vortex configurations and steady states
- Summary



Vibrating structures in helium superfluids

Many different structures:

- grids
- wires
- forks
- spheres
 - most simple case numerically



- M. Niemetz and W. Schoepe, J. Low Temp. Phys. 135, 447 (2004).
- J. Jäger, B. Schuderer, and W. Schoepe, Physica B 210, 201 (1995).
- J. Jäger, B. Schuderer, and W. Schoepe, Phys. Rev. Lett. 74, 566 (1995).
- W. Schoepe, Phys. Rev. Lett. 92, 095301 (2004).

Vibrating Sphere

Oscillating flow around sphere, $v > v_c$

⁴He-II, R = 0.1 mm, v = 150 mm/s, f = 200Hz, T=0:





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Vibrating Sphere

Oscillating flow around sphere, $v > v_c$

⁴He-II, R = 0.1 mm, v = 200 mm/s, f = 200Hz, T=1.5K (Stokes flow for v_n):





Oscillating flow around sphere, $v > v_c$

⁴He-II, R = 0.1 mm, v = 120 mm/s, f = 200Hz, T=1.5K (Stokes flow for v_n):





Vibrating Sphere

Oscillating flow around sphere

⁴He-II, R = 0.1 mm, f = 200Hz:



Vortex number, T=0.

Critical velocity $v_c \approx 100 \text{ mm/s}$.



Vortex number T=1.5K. (Stokes for v_n .)



Numerical problems/chalenges

- difficult to reach a steady state
- limited range of length scales
- hard to estimate the numerical dissipation at low temperatures
- rouch surfaces may alter results
- what is the normal component doing at finite temperatures?
- calculation of the damping force is a complicated task
- no clear evidence for $v_c \propto \sqrt{\kappa \omega}$



What is the steady state like?

"Large" structures (spheres, grids, forks, thick wires):

- large number of vortices, vortex avalanche?
- mimicing normal flow? (no such indication in simulations with sphere of R=100 μ m)
- "Small" structures (thin wires)
 - simulations do not indicate a vortex avalanche (sphere of R=10µm, numerical problem?)
 - can a single (or few) vortex cause the observed damping for small structures?

Consider Osaka measurements for thin wires at low temperatures: H. Yano *et al.* PRB **75**, 012502 (2007).

Vibrating Sphere

Tilted rotating cylinder

Effect of single vortex

Extra return force due to vortex tension:

$$T_{\rm v} = \rho_{\rm s} \kappa^2 \ln(\ell/a)/2\pi$$

direction depends on the vortex orientation.

■ simulations $\rightarrow \eta \approx 90^{o}$ when oscillation amplitude, x, is close to sphere radius, R, therefore sin $\eta \approx x/\sqrt{x^2 + R^2}$.

All this results that $\omega^2 = \omega_0^2 + T_v/(RM)$, where M is the mass of the wire.

Osaka parameters: $R=1.25\mu$ m, $R_{loop}{=}1$ mm ightarrow $Mpprox 10^{-10}$ kg.

$$\Delta \omega \approx 0.25 \text{Hz}$$



Vibrating Sphere

Tilted rotating cylinder

Tilt of the cylinder axis



Perfect alignment

Small misalignment



Previous results

Result by Mathieu et al., PRB 1984:

- Using continuous model for vorticity
- Rectangular cavity with infinite lenght along y-direction
- Assumed that $\omega \parallel \Omega$ deep in the cavity



Motion of ideal fluid:

Consider a situation (at some particular time) where $\mathbf{\Omega} = \mathbf{\Omega} \hat{\mathbf{Z}}$ and the cylinder axis is along $\hat{\mathbf{z}} = \cos \eta \hat{\mathbf{Z}} + \sin \eta \hat{\mathbf{X}}$. Cartesian(X, Y, Z) and cylindrical (ρ, ϕ, z) coordinates are related by

$$X = \rho \cos \phi \cos \eta + z \sin \eta$$

$$Y = \rho \sin \phi$$

$$Z = -\rho \cos \phi \sin \eta + z \cos \eta.$$



In cylindrical coordinates Ω and r are given by

$$\begin{aligned} \mathbf{\Omega} &= & \Omega \left[-\sin\eta \cos\phi \hat{\boldsymbol{\rho}} + \sin\eta \sin\phi \hat{\boldsymbol{\phi}} + \cos\eta \hat{\mathbf{z}} \right] \\ \mathbf{r} &= & \rho \hat{\boldsymbol{\rho}} + z \hat{\mathbf{z}} \end{aligned}$$

Without vortices $\mathbf{v} = \nabla \Phi \Rightarrow \nabla^2 \Phi = 0$.

$$\frac{1}{\rho}\frac{\partial}{\partial\rho}\left(\rho\frac{\partial\Phi}{\partial\rho}\right) + \frac{1}{\rho^2}\frac{\partial^2\Phi}{\partial\phi^2} + \frac{\partial^2\Phi}{\partial z^2} = 0$$

Boundary condition: $\frac{\partial \Phi}{\partial n} = \hat{\mathbf{n}} \cdot (\mathbf{\Omega} \times \mathbf{r})$ implies:

$$\frac{\partial \Phi}{\partial \rho}_{\mid_{\rho=R}} = \Omega z \sin \eta \sin \phi, \qquad \frac{\partial \Phi}{\partial z}_{\mid_{z=\pm L/2}} = -\Omega \rho \sin \eta \sin \phi$$

These are in lab. frame. In rotating frame:

$$\mathbf{v}=\nabla\Phi-\mathbf{\Omega}\times\mathbf{r}$$



Т

Tilted rotating cylinder

Trial
$$\Phi(\rho, \phi, z) = \Omega(\rho z + g(\rho, z)) \sin \phi \sin \eta$$
:
 $\frac{1}{\rho} \frac{\partial}{\partial \rho} \left(\rho \frac{\partial g}{\partial \rho} \right) + \frac{\partial^2 g}{\partial z^2} - \frac{1}{\rho^2} g = 0$
 $\frac{\partial g}{\partial \rho}\Big|_{\rho=R} = 0 \qquad \frac{\partial g}{\partial z}\Big|_{z=\pm L/2} = -2\rho.$

Velocity components in the rotating frame are then given by

$$\begin{aligned} v_{\rho} &= \Omega \sin \phi \sin \eta \frac{\partial g}{\partial \rho} \\ v_{\phi} &= \Omega \cos \phi \sin \eta \frac{g}{\rho} - \Omega \rho \cos \eta \\ v_{z} &= \Omega \sin \phi \sin \eta (2\rho + \frac{\partial g}{\partial z}) \end{aligned}$$

Now one can do vortex filament calculations in rotating frame with $\mathbf{v}_n = 0$ and $\mathbf{v}_s = \mathbf{v} + \mathbf{v}_{\omega} + \mathbf{v}_{b}$, where \mathbf{v} is due to rotation.





Single vortex inside rotating tilted cylinder





Configuration for Singe Vortex, $\Omega = 0.5 \text{rad/s}$



Here $\eta = 0, 10, 20, ...,$ and 90 degrees. Vortex is practically on the xz-plane (defined by rotation and cylinder axis). (*Left*) L = R = 3mm, (*Middle*) L = 4R = 12mm, and (*Right*) L = 20R = 60mm (only upper half is plotted)

Vortex array in infinitely long cylinder (g=0)

$$v_{
ho} = 0$$
 $v_{\phi} = -\Omega
ho \cos \eta$ $v_z = 2\Omega
ho \sin \phi \sin \eta$

Vortex density due to reduced azimuthal counterflow is

$$n_{\rm v} = 2\Omega \cos \eta / \kappa \tag{1}$$

Axial velocity affects the vortex configuration only when it is above the Glaberson critical value. Since $v_{z,max} = 2\rho\Omega \sin \eta$, the vortices suffer the instability if $(\nu = \kappa \ln(1/ka_0)/(4\pi) \approx \kappa)$

$$N > N_{\rm c} = 2\pi \frac{\nu}{\kappa} \cot^2 \eta \approx 2\pi \cot^2 \eta.$$
 (2)

Numerically^{(*} with $\eta = 30^{\circ}$ ($N_c \approx 19$) a vortex cluster with N=22 is stable and N=25 Kelvin waves appear.

* with L = 30 mm (periodic b.c.), R = 6 mm, $\Omega = 100$ mrad/s and $T = 0.5T_c$

Finite cylinder, small tilt or Ω

L = 10R = 30mm, $\Omega = 50$ mrad/s, $\eta = 15^{\circ}$, static steady state:





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Finite cylinder, large tilt or Ω

L = 6R = 18mm, $\Omega = 0.25$ rad/s, $T = 0.4T_c$, $\eta = 30^{\circ}$, dynamic steady state:





Finite cylinder, large tilt or Ω

L = 5mm, R = 3mm, $\Omega = 0.25$ rad/s, T = 0, $\eta = 30^{\circ}$:







Finite cylinder, large tilt or Ω

L = 5mm, R = 3mm, $\Omega = 0.25$ rad/s, high T ($\alpha = 10, \alpha' = 0.1$), $\eta = 30^{\circ}$:





- with large enough tilt vortices become unstable
- unexpected configuration for single vortex
- possible to obtain dynamic steady state and polarized turbulence



Thank You Very Much for Your Attention!

