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Ionospheric Data Processing and Analysis

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# **Ionospheric Data Processing and Analysis**

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## This talk is a tutorial on Total Electron Content (TEC) estimation using a GPS receiver

- Describe the GPS observables and the various linear combinations used to estimate TEC
- Demonstrate estimation and removal of the instrumental biases using several techniques
  - A simple technique (setting the minimum value of TEC at night)
  - A least squares approach (minimizing the variance of the vertical-equivalent TEC)
  - Kalman filter estimation of total TEC
- Discuss the influence of ionospheric structure on the GPS TEC
- Discuss the influence of the plasmasphere on the GPS TEC
  - A model for the plasmaspheric contribution to the total TEC
  - Kalman filter estimation of ionospheric and plasmaspheric TEC
- Concluding remarks





# The GPS Observables and TEC





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	$P_{1} = \rho + c \left( \Delta t_{r} - \Delta t_{s} \right) + I_{1} + T + b_{1r}^{P} + b_{1s}^{P} + m_{1}^{P} + \varepsilon_{1}^{P}$	For each signal broadcast:		
		1 – L1 (1575.42 x 10 <sup>6</sup> Hz)		
	$P_{2} = \rho + c(\Delta t_{r} - \Delta t_{s}) + I_{2} + T + b_{2r}^{P} + b_{2s}^{P} + m_{2}^{P} + \varepsilon_{2}^{P}$	2 – L2 (1227.6 x 10 <sup>6</sup> Hz)		
	Symbols:	$\Delta t_r$ – Receiver clock error (s)		
		$\Delta t_r = \text{Heceiver clock effor (3)}$		
	P – Pseudorange (m)	$\Delta t_s$ – Satellite clock error (s)		
	$\rho$ – Geometric range (m)	m <sup>P</sup> – Multipath (m)		

I – Ionospheric delay (m)

T – Tropospheric delay (m)

b – Instrumental bias for receiver and satellite

The Pseudorange Observation Equations:

 $\epsilon^{P}$  – thermal noise (m)

1 – L1 (1575.42 x 10<sup>6</sup> Hz)

2 – L2 (1227.6 x 10<sup>6</sup> Hz)

Forming the difference P2-P1 and neglecting multipath and thermal noise gives:

 $P_{2}-P_{1}=I_{2}-I_{1}+(b_{2r}^{P}-b_{1r}^{P})+(b_{2s}^{P}-b_{1s}^{P})$  $=I_{2}-I_{1}+b_{r}^{P}+b_{s}^{P}$ (The geometric range, clock error, & tropospheric delay cancel)





#### The Carrier-Phase Observation Equations:

$$\Phi_{1} = \rho + c \left( \Delta t_{r} - \Delta t_{s} \right) + I_{1} + T + b_{1r}^{\Phi} + b_{1s}^{\Phi} + \lambda_{1} N_{1} + m_{1}^{\Phi} + \varepsilon_{1}^{\Phi}$$

 $\Phi_{2} = \rho + c (\Delta t_{r} - \Delta t_{s}) + I_{2} + T + b_{2r}^{\Phi} + b_{2s}^{\Phi} + \lambda_{2} N_{2} + m_{2}^{\Phi} + \varepsilon_{2}^{\Phi}$ 

For each signal broadcast: 1 – L1 (1575.42 x 10<sup>6</sup> Hz) 2 – L2 (1227.6 x 10<sup>6</sup> Hz)

Symbols:	$\Delta t_r$ – Receiver clock error (s)
$\Phi$ – Carrier-phase (m)	$\Delta t_s$ – Satellite clock error (s)
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ρ – Geometric range (m)	$\lambda$ – Wavelength (m)
I – Ionospheric delay (m)	N – Phase cycle-ambiguity
T – Tropospheric delay (m)	$m^{\Phi}$ – Multipath (m)
b – Instrumental bias for receiver and satellite	$\epsilon^{\Phi}$ – thermal noise (m)

Forming the difference P2-P1 and neglecting multipath and thermal noise gives:

$$\Phi_{1}-\Phi_{2}=I_{1}-I_{2}+(b_{1r}^{\Phi}-b_{2r}^{\Phi})+(b_{1s}^{\Phi}-b_{2s}^{\Phi})+(\lambda_{1}N_{1}-\lambda_{2}N_{2})$$
  
=  $I_{1}-I_{2}+b_{r}^{\Phi}+b_{s}^{\Phi}+(\lambda_{1}N_{1}-\lambda_{2}N_{2})$ 

(The geometric range, clock error, & tropospheric delay cancel)





lonospheric delay:

$$I_f = \frac{40.30}{f^2} TEC$$

f – Signal frequency (Hz)

 $I_f$  – lonospheric delay (m)

TEC – total electron content (e<sup>-</sup>/m<sup>2</sup>)

Substituting ionospheric delay into the pseudorange observation equation gives:

$$P_2 - P_1 = I_2 - I_1 + b_r^p + b_s^p = 40.30 \left(\frac{1}{f_2^2} - \frac{1}{f_1^2}\right) TEC + b_r^p + b_s^p$$

Solving this for the TEC yields:

$$TEC = \frac{1}{40.30} \left[ \frac{f_1^2 f_2^2}{f_1^2 - f_2^2} \right] \left[ \left( P_2 - P_1 \right) - \left( b_r^P + b_s^P \right) \right] = 9.52 \times 10^{16} \left[ \left( P_2 - P_1 \right) - \left( b_r^P + b_s^P \right) \right]$$

We define the pseudorange TEC without the bias terms in units of TECU:

$$TEC_P = 9.52(P_2 - P_1)$$
 where 1 TECU = 10<sup>16</sup> e<sup>-</sup>/m<sup>2</sup>

unambiguous but noisy and therefore an imprecise observable





lonospheric phase advance:

$$I_f = \frac{40.30}{f^2} TEC$$

*f* – Signal frequency (Hz)

 $I_f$  – lonospheric delay (m)

TEC – total electron content (e<sup>-</sup>/m<sup>2</sup>)

Substituting phase advance into the carrier-phase observation equation gives:

$$\Phi_1 - \Phi_2 = I_1 - I_2 + 40.30 \left(\frac{1}{f_2^2} - \frac{1}{f_1^2}\right) TEC + b_r^{\Phi} + b_s^{\Phi} + \left(\lambda_1 N_1 - \lambda_2 N_2\right)$$

Solving this for the TEC yields:

$$TEC = \frac{1}{40.30} \left[ \frac{f_1^2 f_2^2}{f_1^2 - f_2^2} \right] \left[ (\Phi_1 - \Phi_2) - (b_r^{\Phi} + b_s^{\Phi}) - (\lambda_1 N_1 - \lambda_2 N_2) \right]$$
$$= 9.52 \times 10^{16} \left[ (\Phi_1 - \Phi_2) - (b_r^{\Phi} + b_s^{\Phi}) - (\lambda_1 N_1 - \lambda_2 N_2) \right]$$

We define the carrier phase TEC in units of TECU:

 $TEC_{\Phi} = 9.52(\Phi_1 - \Phi_2)$  where 1 TECU = 10<sup>16</sup> e<sup>-</sup>/m<sup>2</sup>

Precise but ambiguous observable. Biases and ambiguities will be estimated using pseudoranges











Approximate  $\text{TEC}_{\Phi}$  as a superposition of a quadratic polynomial and a Heaviside step function at the slip location

$$\sum_{j} V_{ij} t_{j} = TEC_{\Phi}^{j}$$

Basis vectors:

 $V_1(t)=1$   $V_3(t)=t^2$  $V_2(t)=t$   $V_4(t)=H_{ts}(t)$ 

Find solution to this over-determined system via least squares:

 $(\mathbf{V}^{\mathsf{T}}\mathbf{V})\mathbf{T} = \mathbf{V}^{\mathsf{T}}\mathbf{\Phi}$ 

Solve via singular-value decomposition

Coefficient of the Heaviside step function  $(V_4)$  is the size of the slip



Slip not corrected if  $\chi^2 > 1$  TECU

Advantage over predictor methods – uses data on both sides of slip, can de-weight (or omit) data immediately surrounding the slip, if noisy











Relative TEC (leveled phases):

$$TEC_{R} = TEC_{\Phi} + \left\langle \underbrace{TEC_{P} - TEC_{\Phi}}_{Offset} \right\rangle_{arc}$$

Take difference between pseudorange TEC and phase TEC

$$x_{i} = TEC_{P}^{i} - TEC_{\Phi}^{i}$$

Weighted average of x gives the offset:

$$Offset = \frac{\sum_{i} W_{i} X_{i}}{\sum_{i} W_{i}}$$

Summation is taken over all samples (*i*) in the same phase connected arc with  $\varepsilon_i > 20^\circ$ 

Weighted standard deviation,  $\sigma$ , provides estimate of the leveling error:

Weighting chosen is usually the sine of the satellite elevation,  $\epsilon$ :

$$\sigma^{2} = \frac{\left|\sum_{i} w_{i} x_{i}^{2}\right| \sum_{i} w_{i} - \left|\sum_{i} w_{i} x_{i}\right|^{2}}{\left|\sum_{i} w_{i}\right|^{2} - \sum_{i} w_{i}^{2}}$$

 $w_i = \sin(\varepsilon_i)$ 

Quality control: entire phase connected arc is discarded if  $\sigma > 5$  TECU











Once the instrumental biases are known, they can be subtracted from relative TEC measurements to give the calibrated (unbiased) slant TEC







# Estimation and Removal of the GPS Instrumental Biases





To estimate the instrumental biases from the measurements themselves, we must make assumptions about the (real) TEC we are trying to measure:

## **TEC** must be non-negative

- and -

## The structure of the TEC is assumed to satisfy one or more of these ...

- -We assume a value for the TEC attained at night
- Spatial gradients in TEC assumed negligible (at night)
- TEC well approximated by a polynomial of order N (higher order derivatives assumed negligible)
- TEC in the ionosphere well approximated by a polynomial and TEC in the plasmasphere by a model (generally structured according to dipole field-lines)

These techniques work by exploiting the fact that slant TEC depends on elevation (since the path length through ionized region is longer) while the biases do not



## A Useful Tool for Bias Estimation and Visualization: Computing the Vertical-Equivalent TEC





Application of mapping function to slant TEC gives the vertical-equivalent TEC:

 $TEC_{v} = TEC_{s}/M(\varepsilon)$ 

The standard geometric mapping function, *M*, is the projection of slant distance onto zenith distance at the IPP:

$$M \equiv s / d = \sec(\eta)$$

The zenith angle at the IPP,  $\eta$ , can be expressed in terms of shell height, h, and Earth radius R:

d

$$(R_{e} + h)\sin(\eta) = R_{e}\sin(90^{\circ} + \varepsilon) = R_{e}\cos(\varepsilon)$$

This gives the mapping function in terms of the satellite elevation,  $\epsilon$ :

$$M(\varepsilon) = \sec\left[\sin^{-1}\left(\frac{R_{e}}{R_{e} + h}\cos(\varepsilon)\right)\right]$$







#### **Characteristics of well-calibrated TEC:**

- TEC is non-negative
- TEC curves collapse well (especially at night and during post-sunrise ramp up)

There are noteworthy Exceptions to this rule!





The technique used by the receiver to measure TEC<sub>P</sub> dictates the type of satellite instrumental biases that must be removed.

Receiver Model	Method used to measure the DPR	Type of Satellite Bias to Remove
Ashtech Z-12	L2(P2) - L1(P1)	P1P2 bias
Ashtech µZ-CGRS	L2(P2) - L1(P1)	P1P2 bias
NovAtel GSV 4004B	L2(P2) - L1(CA)	P1P2 bias minus the P1C1 bias

Files containing monthly estimates for the P1P2 and P1C1 biases can be downloaded from http://www.aiub.unibe.ch/download/CODE/.

These satellite differential codes bias are not absolute timing biases, instead they average to zero. The unknown offset is immaterial in that it will be lumped together and removed along with the receiver bias.





#### **Procedure:**

- Assume the minimum TEC (generally attained during nighttime) is known, e.g. zero
- Download estimates of the satellite biases from CODE. Multiply the biases by -2.85 TECU/ns to convert the reported biases from units of nanoseconds to TECU.
- Select the receiver bias to enforce that min(TECS) = TEC\*:

 $b_R = min(TEC_R) + b_S - TEC^*$ 

Compute the calibrated slant TEC:

 $TEC_S = TEC_R - b_S - b_R$ 







#### Procedure:

- If ionosphere is uniformly distributed in a thin slab (no spatial gradients) then the vertical-equivalent TEC estimates should the same for all satellites.
- Download estimates of the satellite biases from CODE. Multiply the biases by -2.85 TECU/ns to convert the reported biases from units of nanoseconds to TECU.
- Manually change the assumed value of the receiver bias until the vertical-equivalent curves collapse most closely together (at least during nighttime hours)















































<u>Assumption:</u> In absence of spatio-temporal density gradients, the verticalized calibrated TEC measured by all satellites should be the same.

Given the satellite biases and h, TEC<sub>V</sub> can be expressed as a function of  $b_R$ :

$$\begin{aligned} \mathsf{TEC}_{\mathsf{V}}(\mathsf{b}_{\mathsf{R}}) &= [\mathsf{TEC}_{\mathsf{R}} - \mathsf{b}_{\mathsf{R}} + \mathsf{b}_{\mathsf{S}}] / \mathsf{M}(\varepsilon, h) \\ & \uparrow \\ \\ & \mathsf{Single layer mapping function} \end{aligned}$$



We calculate the  $b_R$  that minimizes Var(TEC<sub>V</sub>) late at night when gradients are smallest





Final calibrated TEC result, using estimated value of 22.3 TECU for receiver bias









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Largest deviations from trend occur when TEC is structured late at night

These nights often correlate with the occurrence of scintillation

#### A closer look at two outliers:



Late-night structure in TEC







This station (Kwajalein) experienced weaker GPS scintillations than Antofagasta in 2005

Deviations in the receiver bias from the trend are correspondingly smaller



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Less structure at night generally means more accurate TEC calibration





# Kalman Filter Estimation of Total TEC





Observation equation (for the *i*<sup>th</sup> GPS receiver-satellite pair):



- $\epsilon$  Elevation
- $\alpha$  Azimuth
- $d\lambda$  Difference between MLT at ionospheric penetration point and station
- $d\varphi$  Difference between MLAT at ionospheric penetration point and station
- $b_{R}$ ,  $b_{S}$  Receiver and satellite instrumental biases

Thin shell mapping function

$$M(\varepsilon) = \sec\left[ \arcsin\left(\frac{R_e}{R_e + h}\right) \cos(\varepsilon) \right]$$











## Kalman Filter Estimation of TEC in both the lonosphere and Plasmasphere




- Gradients from the plasmasphere cause an apparent "spread" in the vertical-equivalent TEC which violates our assumption that spatial gradients are small.
- Moreover, the thin-shell approximation commonly used for the ionosphere is not a suitable representation for the plasmaspheric contribution to the TEC
- This effect is most evident during periods of very low solar activity such the one we are currently experiencing.









Plasmaspheric contribution to the TEC depends on location, azimuth, and elevation.

Plasmapause location has strong influence on PTEC encountered at high to mid latitudes.





• Carpenter and Anderson [1992] model for the electron density in the inner plasmasphere:

$$\log n_{e}^{i} = -0.3145L + 3.9043 + \left[ 0.15\cos\frac{2\pi(d+9)}{365} - 0.075\cos\frac{4\pi(d+9)}{365} + 0.00127\overline{R} - 0.0635 \right] e^{\frac{(L-2)}{1.5}}$$

• Location of the plasmapause:

$$L_p = 5.6 - 0.46 K p,_{max}$$

• Width of the plasmapause (Gallagher et al. [2000]), neglecting local time dependence:

 $L_{w} = 0.14$ 

• Electron density in the trough (Sheeley et al. [2001]) neglecting local time dependence:

 $n_{e}^{t} = 124(3/L)^{4}$ 

- Regions spliced together using tanh step function
- Integration of electron density from 700 km to 20,200 km along signal path gives  $P(\alpha, \varepsilon)$
- Model very simple, but Kalman filter will scale the results to best fit the measurements





### Assume ionosphere is an idealized thin slab



# Add slant TEC through model plasmasphere



### Construct slant TEC via thin-shell mapping fn











### Vertical TEC NCA 11/17/2007 Vertical TEC NCA 11/17/2007 UT (hours) UT (hours) 20 70 10 30 40 50 60 10 20 30 40 60 70 50 15 S 52.5 52.5 51.3 51.3 10 10 50.1 TECU TECU 45.4 2 ß 44.2 43.0 43.0 41.8 41.8 40.7 MLAT MLAT 0 0 10 20 70 0 30 40 50 60 10 0 20 30 40 50 60 70 MLT (hours) MLT (hours)

# **TEC When Neglecting Plasmasphere**

### Idealized Ionosphere and Plasmasphere





Observation equation (for the  $i^{th}$  GPS receiver-satellite pair):



- $\epsilon$  Elevation
- $\alpha$  Azimuth
- $d\lambda$  Difference between MLT at ionospheric penetration point and station
- $d\varphi$  Difference between MLAT at ionospheric penetration point and station
- $P(\alpha, \varepsilon)$  PTEC from Carpenter-Anderson et. al [1992] (scaled to fit observations)
- $b_{R}$ ,  $b_{S}$  Receiver and satellite instrumental biases

Thin shell mapping function (for the ionosphere only)

$$M(\varepsilon) = \sec\left[ \arcsin\left(\frac{R_e}{R_e + h}\right) \cos(\varepsilon) \right]$$



















Neglecting the plasmasphere tends to cause overestimation of the total TEC at middle latitudes and underestimation at equatorial latitudes.



# Why the Estimated TEC Can Be Negative and What to Do About It





When this happens, we fall back on the simple approach: choose the bias to enforce that  $min(TECS) = TEC^*$ 

Now, however, we can make a more informed selection of TEC\*. A reasonable value to use is the (zenith) plasmaspheric contribution according to the Carpenter-Anderson model.







Simulation conditions: 13 month average solar flux = 7.9; Kp=1; Day of year = 1







- When estimating the GPS instrumental biases from the measurements we must make various assumptions about the structure of the ionized regions traversed by the signals
- Inaccuracies in estimation of the biases can be expected when these assumptions are violated. Phenomena that cause difficulty in estimating the biases include:
  - Ionospheric structure and scintillation
  - The contribution to the GPS TEC from the plasmasphere
- Neglecting the plasmasphere tends to cause overestimation of the total TEC at middle latitudes and underestimation at equatorial latitudes.
- Software to perform the calibrations using the Kalman filter approach (with and without the plasmasphere term) is available upon request. We will demonstrate this software during Wednesday's TEC calibration laboratory.
- A manuscript (draft) recently submitted to Radio Science describing the technique is also available upon request