

**TEC Calibration techniques:**

**Single-station estimation of arc offsets**

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Objective of the presentation

What is calibration

How it is traditionally performed

Why proposing the

**Single station, multi day, arc offset TEC calibration**

Effort will be spent in avoiding details, that will be developed in the last section.

## The observations

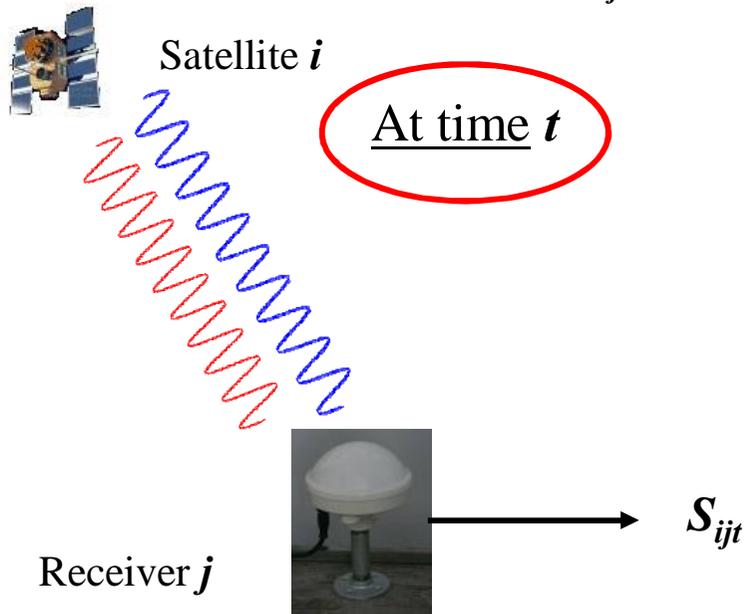
Properly processing GPS measurements

forming differential delays (dual frequency receiver)

combining them to obtain **‘leveled slants’**

one gets slant Total Electron Content (*TEC*) measurements affected by biasing terms  $\beta_i, \gamma_j, (\lambda_{Arc})$

$$S_{ijt} = TEC_{ijt} + \beta_i + \gamma_j + (\lambda_{Arc})$$



$i = 1, 2, \dots, 32$  available GPS satellites

$j = 1, \dots$ , available receivers

*Arc* = common to all continuous observations performed by receiver  $j$  on satellite  $i$  at times contiguous to  $t$

*Why bracketing  $\lambda_{Arc}$ ? Because this term is disregarded in the traditional approach but basic for the proposed “arc offset” solution.*

**Arc:**

a sub-set of continuous observations from one receiver to one satellite

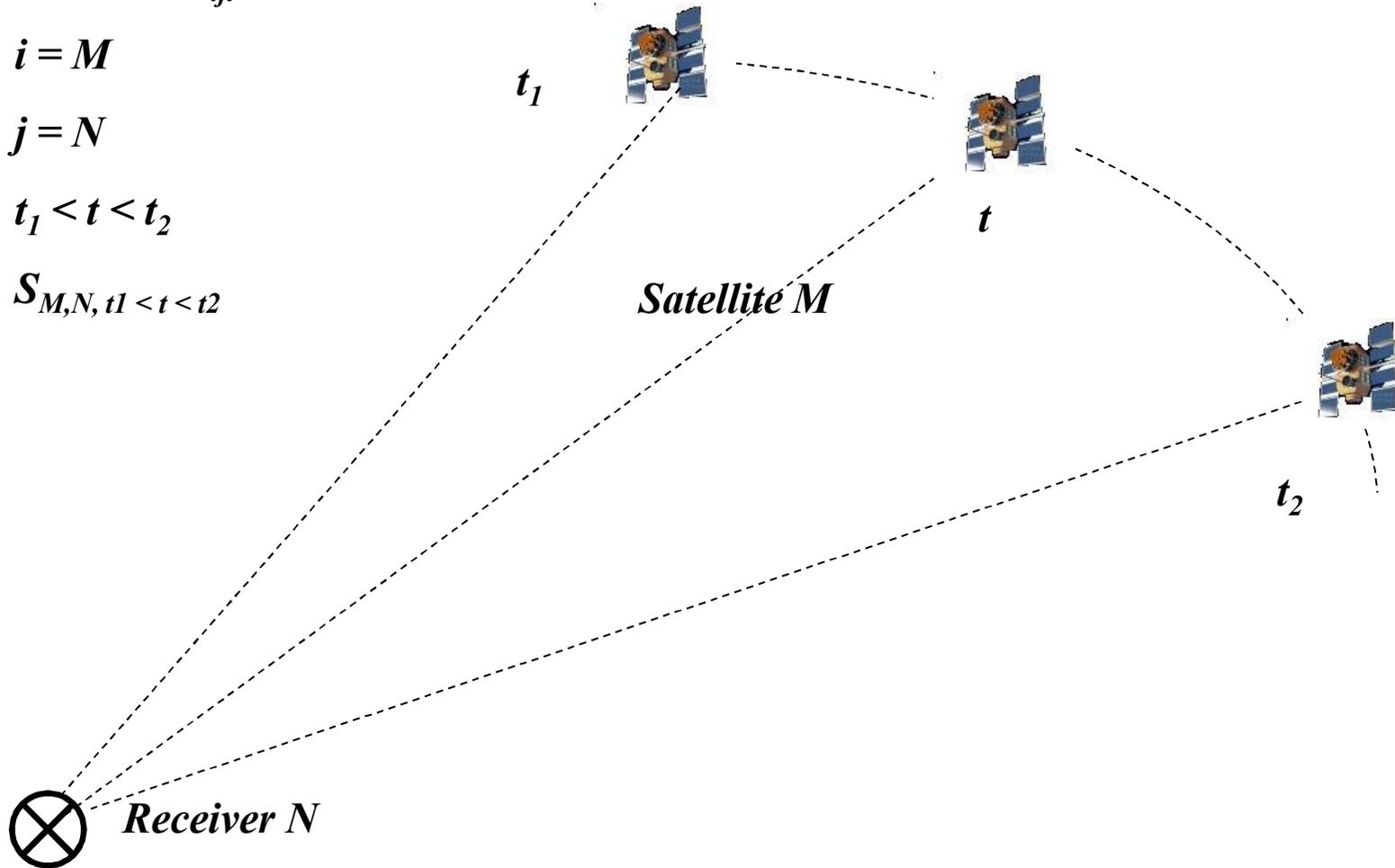
Subset of  $S_{ijt}$

$i = M$

$j = N$

$t_1 < t < t_2$

$S_{M,N,t_1 < t < t_2}$



## Description of the biasing terms

$$S_{ijt} = TEC_{ijt} + \beta_i + \gamma_j + (\lambda_{Arc})$$

$\beta$  differential hardware delays in satellite electronic circuitry

$\gamma$  the same for receiver circuitry

$\lambda$  the average contribution of differential multi-path along an arc

All biasing terms can be considered as constants

For ionospheric investigation and its applications (ionospheric corrections) an algorithm is needed able to estimate the biasing terms in order to have only *TEC*

$$TEC_{ijt} = S_{ijt} - \beta_i - \gamma_j - (\lambda_{Arc})$$

This algorithm is known as

## CALIBRATION or DE-BIASING

Red: unknowns

Blue: estimates

## The calibration or de-biasing of GPS leveled slants

The system of the equations of observation is linear in all unknown terms

$$S_{ijt} = TEC_{ijt} + \beta_i + \gamma_j + (\lambda_{Arc})$$

but contains more unknowns than equations.

*Number of unknowns = number of TECs plus number of unknown (constant) terms*

$$\beta_i, \gamma_j, (\lambda_{Arc})$$

How is it possible performing the calibration?

*TEC*'s are not actually uncorrelated: at some location, at some time they depend on the electron density distribution  $N_e$ .

Assume electron density  $N_e$  can be written as a function of position  $P$ , time  $t$  and a set of  $K$  parameters  $Z_1, Z_2, \dots$

$$TEC = \int N_e(P, Q, t, Z_1, Z_2, \dots) ds$$

Calibration is performed finding the values  $Z_1, Z_2, \dots, \beta_i, \gamma_j, (\lambda_{Arc})$  which minimize the sum of the square of the residuals

$$\varepsilon_{ijt} = S_{ijt} - TEC(P, t, Z_1, Z_2, \dots) - \beta_i - \gamma_j - (\lambda_{Arc})$$

$$\Sigma \varepsilon_{ijt}^2 \Rightarrow \text{Minimum}$$

Example: Ionospheric model *NeQuick* computes electron density  $N_e$  at given point  $P$ , at given time  $t$ , as a function of a Solar Flux equivalent parameter  $Az$ .

$$\varepsilon_{ijt} = S_{ijt} - TEC(P, t, Az) - \beta_i - \gamma_j - (\lambda_{Arc})$$

Find  $Az, \beta_i, \gamma_j, (\lambda_{Arc})$  such that  $\Sigma \varepsilon^2_{ijt} \Rightarrow \text{Minimum}$

Observations/Unknowns budget: very favorable

Problems

Non linear minimization methods needed / Dependence on parameters is not analytical but numerical

Models provide with excellent median values whereas calibration requires that the model describes very precisely the actual  $N_e$  distribution

But:

Excellent perspectives for the future

## Writing TEC

Better using formulations in which also actual gradients (not only median ones provided by the Ionospheric Models) can be taken into account, possibly linear in all unknowns.

$$S_{ijt} = TEC_{ijt} + \beta_i + \gamma_j + (\lambda_{Arc})$$

Writing TEC → Write the integral  $TEC = \int N_e(P, Q, t, Z_1, Z_2, \dots) ds$

Possible (linear) expansions of *TEC*

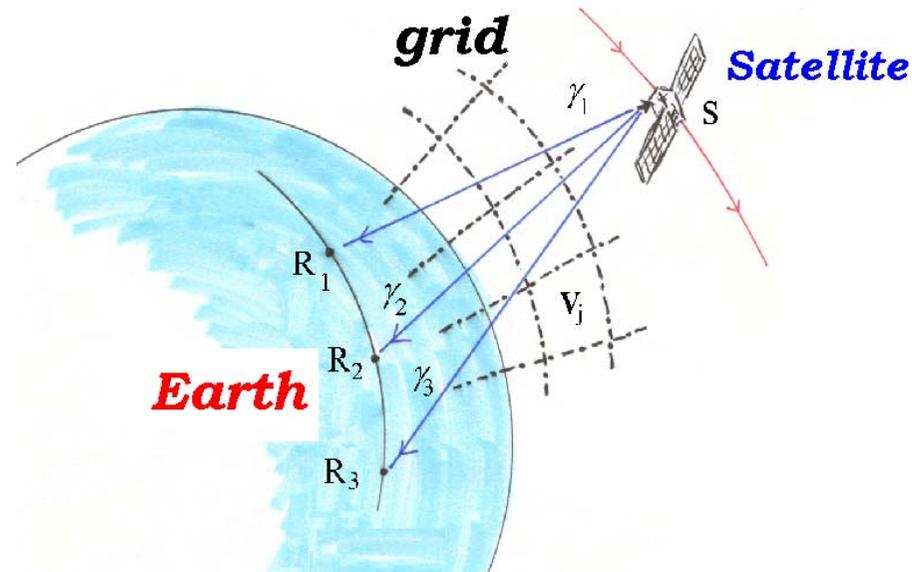
**3D (Tomography)**

**Multi shell**

**Thin shell**

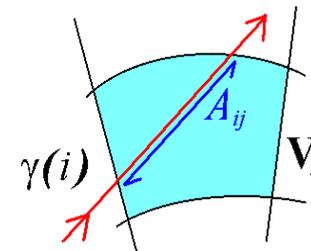
### 3D-4D approach (Tomography)

the ionosphere is divided in elements of volume (voxels) inside which  $N_e$  is constant.  $N_e$  of voxels are the unknowns. Evolution with time of  $N_e$  is considered to improve the budget unknowns/observations. Vertical behaviour of  $N_e$  is expanded in Empirical Orthogonal Functions (EOF)



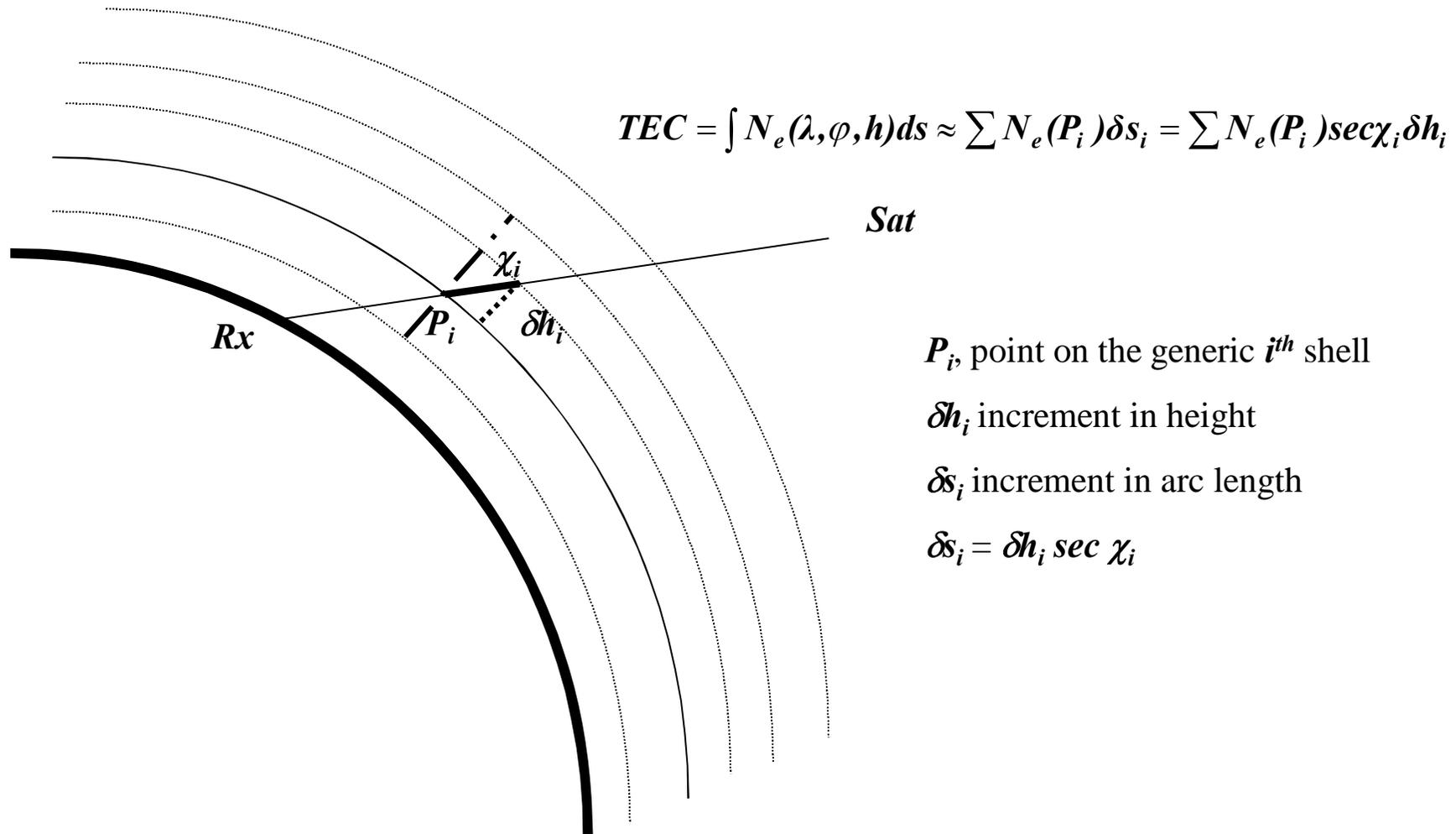
$$d_i = \int_{\gamma(i)} N(\mathbf{r}, t) ds = \sum_j x_j \int_{\gamma(i)} b_j(\mathbf{r}) ds \equiv \sum_j A_{ij} x_j$$

$$\underline{d} = \underline{A} \underline{x} \quad \Rightarrow \quad \underline{x} = \underline{A}_{SVD}^{-1} \underline{d}$$



### 3D: The multishell method

If many shells are used, this is exactly the method by which numerical integration is carried out. For each shell, a suitable 2D expansion in horizontal coordinates is assumed.



## The classical thin shell model

Reducing down the number of shells, *and in principle the expected accuracy,*

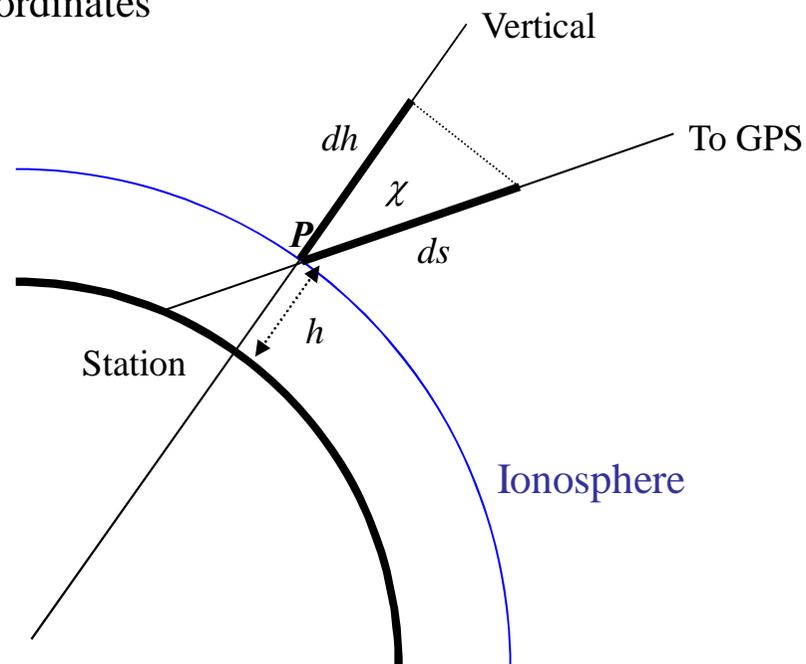
take only one (**thin**) shell at some reference height  $h$

$$TEC = V(P) \sec \chi$$

$V(P)$  is the *TEC* along the vertical of the ionospheric point  $P$

(Vertical Electron Content, *VEC*)

$V(P)$  is a **2D** function of horizontal coordinates



## Note

Thanks to its simplicity and despite its known limitations, the thin shell approach has been and is very widely used also in application in which integrity is a basic requirement, such as

### **Satellite Based Augmentation Systems (SBAS)**

In which *VEC* dependence on horizontal coordinates is implemented interpolating values of a grid of points covering the area of application

**Klobuchar model** uses this approach too

In the following, only the thin shell approach will be considered

## Calibration using the thin shell approximation

Given

The observations  $S_{ijt} = TEC_{ijt} + \beta_i + \gamma_j + (\lambda_{Arc})$

The thin shell assumption  $TEC_{ijt} = V(P_{ijt}) \sec \chi_{ijt}$

Write Vertical  $V(P_{ijt})$  as expansion in horizontal coordinates (geographic, geomagnetic or equivalent latitude  $\Phi$  and longitude  $\Lambda$ )

$$V(P_{ijt}) = \sum_n c_n^{(t)} \Psi_n(\Phi_{ijt}, \Lambda_{ijt})$$

$$\begin{aligned} S_{ijt} = TEC_{ijt} + \beta_i + \gamma_j + \lambda_{Arc} &= V(P_{ijt}) \sec \chi_{ijt} + \beta_i + \gamma_j + (\lambda_{Arc}) = \\ &= \sec \chi_{ijt} \sum_n c_n^{(t)} \Psi_n(\Phi_{ijt}, \Lambda_{ijt}) + \beta_i + \gamma_j + (\lambda_{Arc}) \end{aligned}$$

Representing the linear system of equations of observation to be solved in the unknowns

$$c_n^{(t)}, \beta_i, \gamma_j, (\lambda_{Arc})$$

Some simple example for *VEC* expansion

$$V(P_{ijt}) = \sum_n c_n^{(t)} \Psi_n(\Phi_{ijt}, \Lambda_{ijt})$$

Single-station: assume, at time  $t$ , that *VEC* is constant over the station horizon,  
 $VEC = V_0^{(t)}$ :

$$V(P_{ijt}) = V_0^{(t)}$$

Single-station : assume *VEC* varies linearly with latitude  $\Phi$  and longitude  $\Lambda$

$$V(P_{ijt}) = V_0^{(t)} + a^{(t)} (\Phi - \Phi_0) + b^{(t)} (\Lambda - \Lambda_0)$$

Which can be improved up to bi-linear, bi-polynomial expansion and the full spherical harmonics expansion for global solutions

Rewrite equations of observation

$$S_{ijt} = TEC_{ijt} + \beta_i + \gamma_j + \lambda_{Arc} = V(P_{ijt}) \sec \chi_{ijt} + \beta_i + \gamma_j + (\lambda_{Arc})$$

$$S_{ijt} = \sec \chi_{ijt} \sum_n c_n^{(t)} \Psi_n(\Phi_{ijt}, \Lambda_{ijt}) + \beta_i + \gamma_j + (\lambda_{Arc})$$

Symbolically written as

$$S = Ax$$

Unknowns  $x$  will be solved using Least Squares or equivalent (and more sophisticated) methods

$$x = (A^T A)^{-1} A^T S$$

Going back to the equations of observations, knowing solution  $x$  means knowing

The coefficients of the expansion of vertical TEC  $c_n^{(t)}$

The biasing terms  $\beta_i, \gamma_j, (\lambda_{Arc})$

## After the numerical solution

Having solved for  $c^{(t)}_n, \beta_i, \gamma_j, (\lambda_{Arc})$ , available products are

### The calibrated slants

Calibrated slants will be available as  $TEC_{ijt} = S_{ijt} - \beta_i - \gamma_j - (\lambda_{Arc})$

### The Vertical TEC

In addition, as a by-product of calibration, knowledge of the coefficients  $c^{(t)}_n$  of  $TEC$  expansion will enable to estimate slants along directions different from the ones of the actual observations.

$$TEC_{ijt} = sec \chi_{ijt} \sum_n c^{(t)}_n \Psi_n (\Phi_{ijt}, \Lambda_{ijt})$$

The most familiar is vertical  $TEC$  ( $VEC$ ), the Total Electron Content relative to the zenith of the station of coordinates  $\Phi^*_j, \Lambda^*_j$

$$VEC(j,t) = TEC_{jt} = \sum_n c^{(t)}_n \Psi_n (\Phi^*_j, \Lambda^*_j)$$

## Summary

All solutions for calibration follow the reported scheme

### **Extraction of un-calibrated slants from GPS observations**

### **Solution of the system in unknown *VEC* coefficients and biasing terms**

According to the geographical distribution of stations and the time span in which observations are available, several solutions are possible getting the possible combinations of one solution per line

Hourly / Single-day / Multi-day

Single-station / Regional /Global

## **Factors affecting the reliability of calibration**

### **Modelling of observations**

$$S = VEC \sec \chi + \beta + \gamma + (\lambda_{Arc})$$

Mapping function accuracy, constancy of biases, role of  $(\lambda_{Arc})$

### **Adequacy of the model used for the expansion of VEC**

$$VEC(P, t) = \sum c \Psi(P, t)$$

### **Conditioning of the resulting systems of equations**

Still under investigation: biasing terms and VEC strongly correlated

## **The traditional method: assumptions**

Accept the known limitations of the thin shell approach

Accept the constancy of biases

**Disregard the multi-path contribution**

Solve the system

$$S_{ijt} = \sec \chi_{ijt} \sum_n c_n^{(t)} \Psi_n(\Phi_{ijt}, \Lambda_{ijt}) + \beta_i + \gamma_j$$

In the unknowns  $c_n^{(t)}, \beta_i, \gamma_j$

## The traditional method: Advantages

$$S_{ijt} = \sec \chi_{ijt} \sum_n c_n^{(t)} \Psi_n(\Phi_{ijt}, \Lambda_{ijt}) + \beta_i + \gamma_j$$

### Excellent observations/unknowns budget

Coefficients of VEC expansion plus  
one  $\beta$  per satellite, one  $\gamma$  per receiver, both constant

### No need to perform calibration for every new set of data:

just compute the leveled slants and subtract an available set of pre-computed  $\beta_i, \gamma_j$

$$TEC_{ijt} = S_{ijt} - \beta_i - \gamma_j$$

Use pre-computed values during storm periods or at extreme latitudes (inadequacy of VEC expansion)

Use pre-computed values provided by others

## Use of pre-computed values

Slants to calibrate

**From a set of IGS stations (RINEX files)**

Work has been already done by IGS: monthly values biases for satellites and IGS stations are available at

<ftp://ftp.unibe.ch/aiub/CODE/>

**For user owning their own receiver**

Use CODE for satellite biases, set up a calibration algorithm to estimate the bias of the receiver  $\gamma$

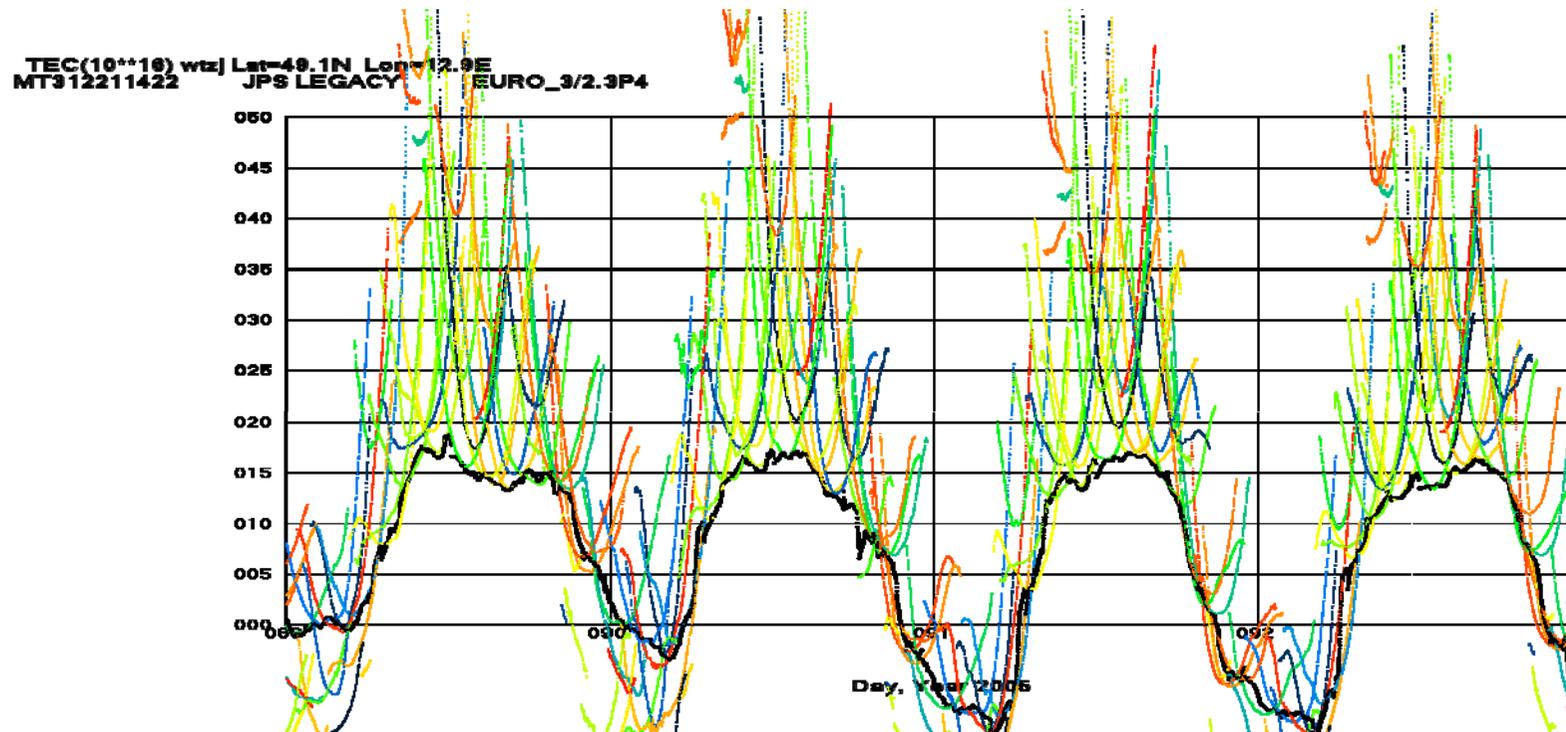
$$S_{ijt} - \beta_i = \sec \chi_{ijt} \sum_n c_n^{(t)} \Psi_n(\Phi_{ijt}, A_{ijt}) + \gamma$$

## Why proposing a different solution?

Reported gossips on the traditional solution:

Slants (to the same satellite) of co-located receivers are not the same

Possible occurrence of negative TECs



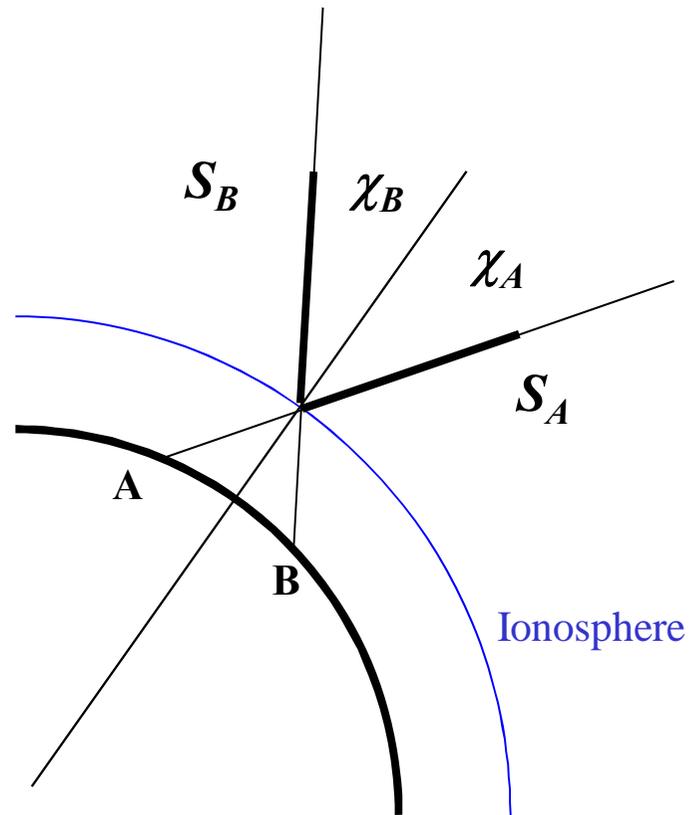
**Which of the reported limitations can produce this errors?**

Limitations of the thin shell assumption?

The thin shell assumption is self-evidently poor:

*TEC* is the same for rays passing through the same ionospheric point,  
**disregarding at all gradients**

If  $\chi_A = \chi_B$  then  $S_A = S_B$



But shall we discard the thin shell approach?

### A new interpretation

For a given ray, rearrange *TEC* definition using  $\sec \chi_{REF}$  at a given reference height

$$TEC = \int N_e ds = \int N_e \sec \chi dh = \sec \chi_{REF} \int N_e \frac{\sec \chi}{\sec \chi_{REF}} dh = \sec \chi_{REF} V_{eq}$$

$$V_{Eq} = \int N_e \frac{\sec \chi}{\sec \chi_{REF}} ds$$

$$TEC = \sec \chi_{REF} V_{eq}$$

The expression is formally identical to the mapping function approximation,

but it is **exact** provided  $V_{Eq}$ , a 2D Function (elevation/azimut or displacement of horizontal coordinates from the station) is not interpreted as the vertical *TEC*.

$V_{Eq}$  will change for stations in different locations, **so its use is limited to the calibration performed by the single station solution.**

Calibration requires a relationship correlating the various slants: for the single station solution the properly interpreted mapping function does not implies errors other than the capability to map  $V_{Eq}$  in satisfactory way.

Which of the reported limitations can produce this errors?

Disregarding the multi-path error  $\lambda_{Arc}$

The close stations experiment

*Station 1*

$$S1_{PRN} = TEC + \lambda1 + \beta_{PRN} + \gamma1$$

*TEC*

*Station 2*

$$S2_{PRN} = TEC + \lambda2 + \beta_{PRN} + \gamma2$$



< 100 m



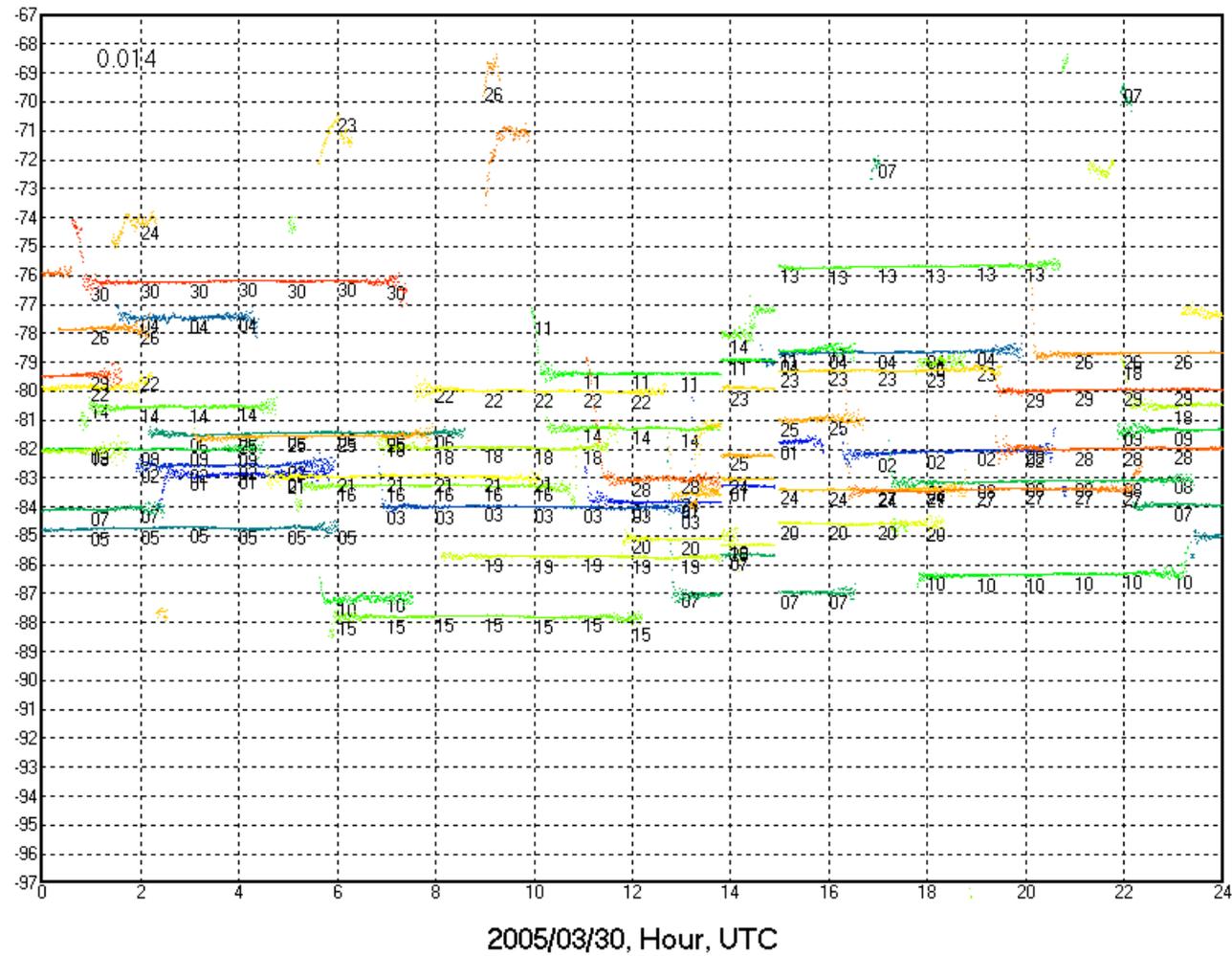
$\beta$

$$S1 - S2 = \gamma1 - \gamma2 + \lambda1 - \lambda2$$

Not dependent on PRN

# $S_{L1} - S_{L2}$ , all satellites

TEC(10\*\*16) zimm - zimj Lat=46.9N Lon=7.5E



How the  $\lambda_{Arc}$  contribution affects the observations?

$$S_{ijt} = TEC_{ijt} + \beta_i + \gamma_j + \lambda_{Arc}$$

This term results from the contribution of multi-path (and the way it is processed by the receiver) along any individual arc. For the same satellite, the same receiver, the overall contribution  $\beta_i + \gamma_j + \lambda_{Arc}$  will be different arc by arc.

### Proposed solution

Consider the observations affected by an unknown overall arc dependent bias

$$\Omega_{Arc} = \beta_i + \gamma_j + \lambda_{Arc}$$

Implement only single-station, possibly multi-day, solutions for calibration (getting in part rid of problems with the mapping function)

The system of observation equations becomes

$$S_{ijt} = sec \chi_{ijt} \sum_n c_n^{(t)} \Psi_n(\Phi_{ijt}, \Lambda_{ijt}) + \Omega_{Arc}$$

Expecting that from a numerical point of view the proposed solution will be less conditioned than the traditional one, but free from reported errors,

Notes:

having assumed the validity of the thin shell approximation in the single-station solution, in the observations

$$S_{ijt} = \sec \chi_{ijt} \sum_n c_n^{(t)} \Psi_n(\Phi_{ijt}, \Lambda_{ijt}) + \Omega_{Arc}$$

the expansion  $\sum_n c_n^{(t)} \Psi_n(\Phi_{ijt}, \Lambda_{ijt})$  represents the **Vertical Equivalent Content (VEq)** and not the actual **Vertical Electron Content (VEC)**

**VEq** takes automatically into account of plasmaspheric contribution.

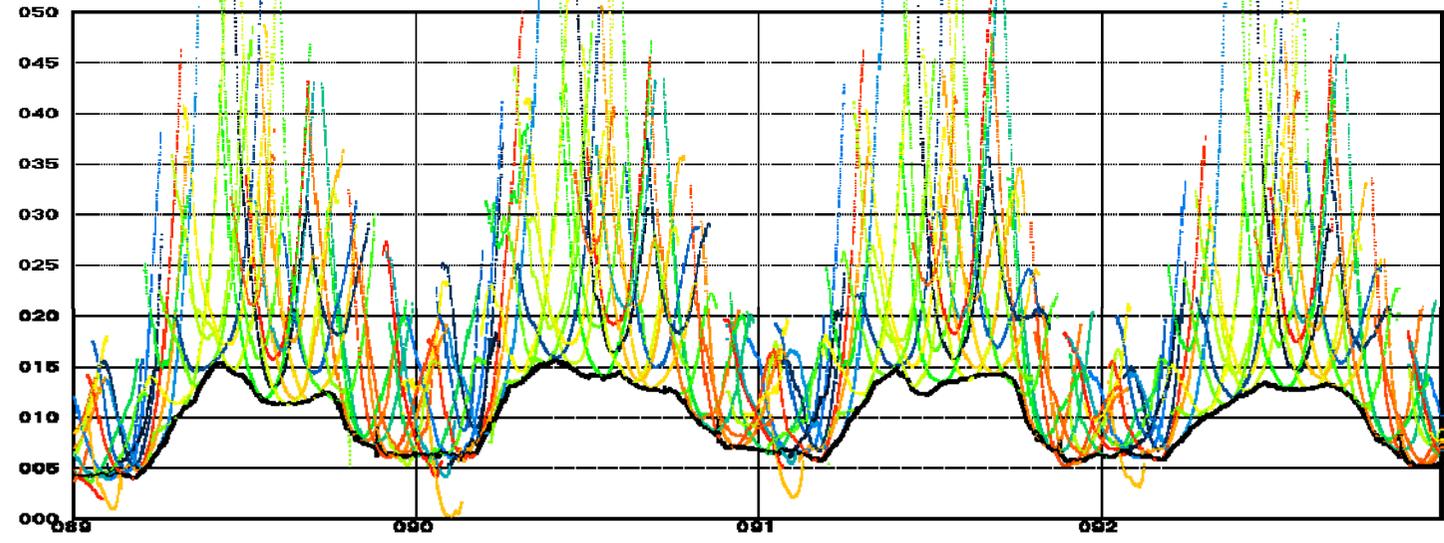
Considering Vertical **TEC** over the station, nothing will change as **VEC** and **VEq** coincide.

No possibility to use pre-computed biases

**But the solution for co-located receiver will look much more reliable**

TEC(10\*\*16) wizr Lat=49.1N Lon=12.9E  
T-317U AOA SNR-8000 ACT 3.3.32.5

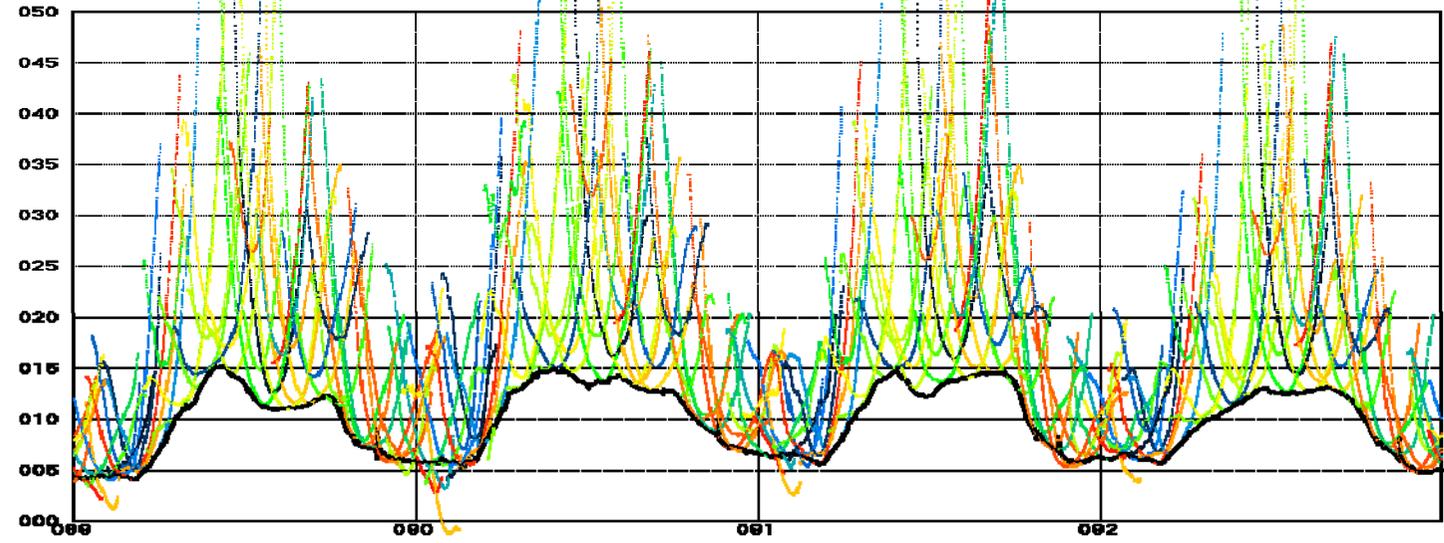
Proposed solution (Arc by arc)



Day, Year 2005

TEC(10\*\*16) wizr Lat=49.1N Lon=12.9E  
MT312211422 JPS LEGACY EURO\_3/2.3P4

Proposed solution (Arc by arc)



Day, Year 2005

## Summary of Proposed Solution characteristics

### Observations

Leveled slants or directly phase slants

### Assumptions

One thin shell at 400 km

Elevation mask: 10°

*TEC* expressed through  $V_{Eq}$  at the ionospheric point, by the mapping function *sec*  $\chi$

$V_{Eq}$  expressed as a proper expansion of horizontal coordinates  $l, f$  with one set of coefficients at each time  $V_{Eq}(l, f) = \sum_n c_n p_n(l, f)$

$$S_{ijt} = \sum_n c_n^{(t)} p_n(l_{ijt}, f_{ijt}) \sec \chi_{ijt} + \Omega_{Arc}$$

The unknowns are now the coefficients  $c_n^{(t)}$  and the offsets  $\Omega_{Arc}$

### *The adopted horizontal coordinates*

Using as horizontal coordinates *Modified Dip Angle* and *Local Time*, we can assume that for a set of adjacent epochs (up to  $\pm 15$  minutes), the coefficients  $c_n^{(t)}$  keep constant.

This allows also reducing computing resources during solution using commonly used standard methods for sparse systems.

After the solution of the system, we avail with :

Calibrated slants along the observed rays  $TEC_{ijt} = S_{ijt} - \Omega_{Arc}$

“Mapped slants” at given coordinates  $l_{ijt}, f_{ijt}$

Vertical *TEC* above the station (ionospheric point at the its zenith)

$$VTec(t) = \sum_n c_n^{(t)} p_n(l_{ijt}^{Zenith}, f_{ijt}^{Zenith}) \sec \chi_{ijt}$$

## Why multi-day solution

A multi-day solution is performed, avoiding day to day discontinuities in calibrated slants, except that at the beginning and the end of the solution.

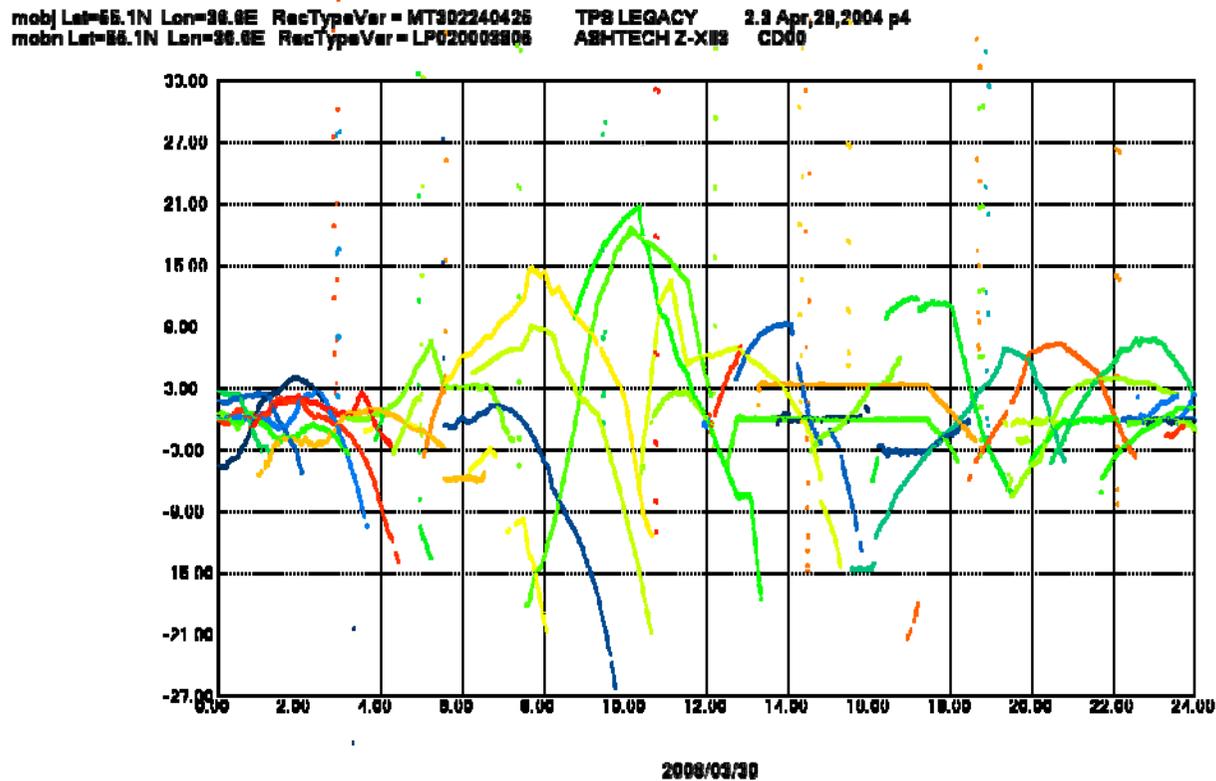
Still, at the beginning and the end of the set of data, broken arcs occur.

Broken arcs are generally shorter implying

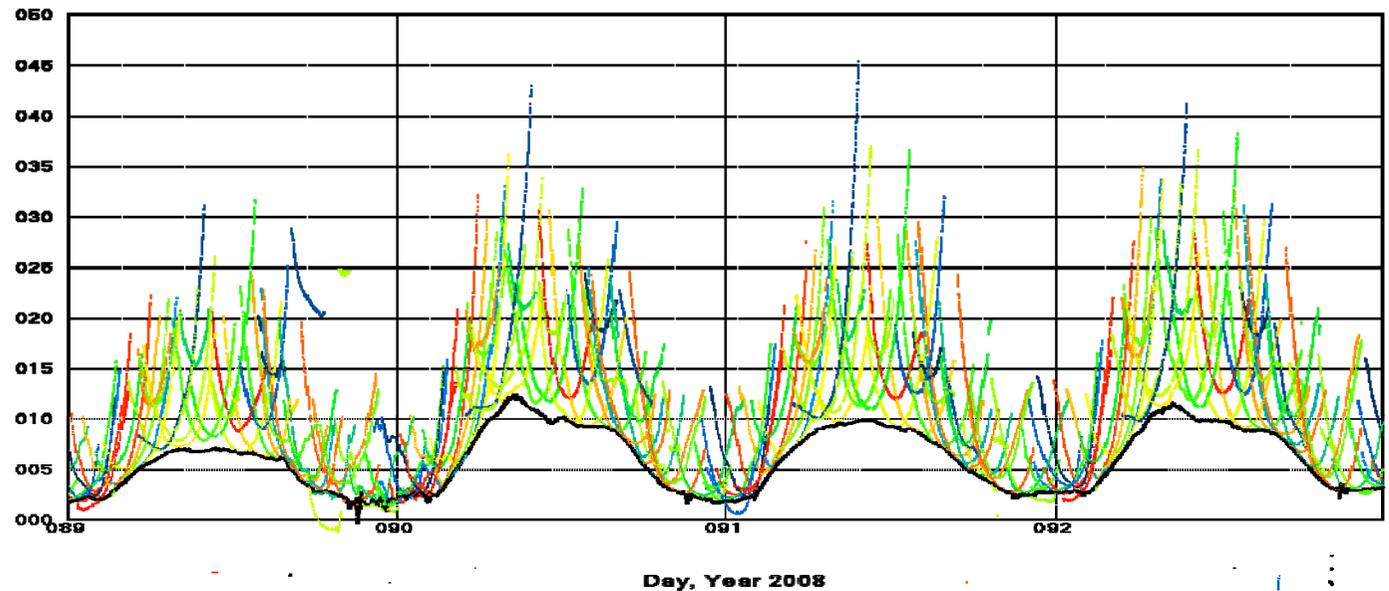
1. worse results during leveling
2. worse numerical conditioning for the solution

To reduce these problems, in order to calibrate  $N$  days,  $N+2$  days are actually processed: first and last day of the  $N+2$  set are discarded.

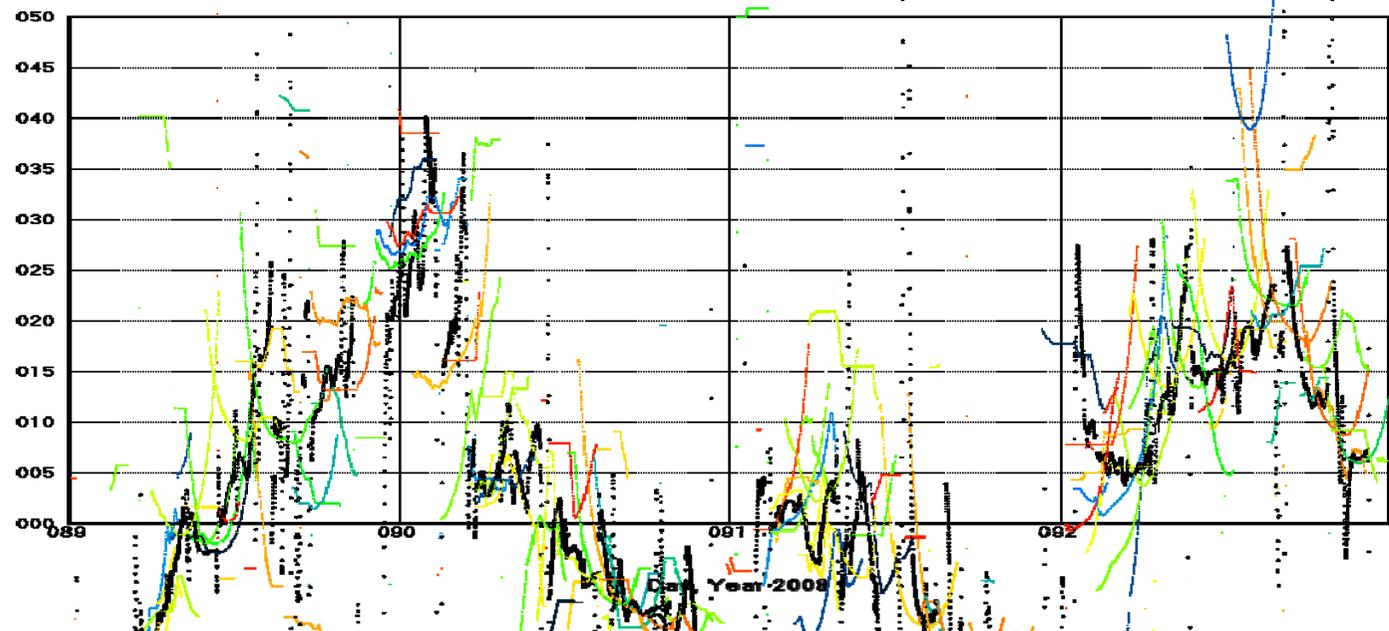
Will it work everytime? Yes, provided phase slants  $S_p$  are reliable. For some pair of stations (namely  $S_p [mobj] - S_p [mobn]$ ), the situation looks like here, showing that, for at least one of them, observations are not reliable. Still, no a priori way exists to know what is going wrong. For the present sample, the solutions of individual stations (next slide) show that the problem arises with “*mobj*”.



TEC(10\*\*16) mobn Lat=66.1N Lon=36.6E  
LP020003606 ASHTECH Z-XIII CD00



TEC(10\*\*16) mobj Lat=66.1N Lon=36.6E  
MT302240425 TPS LEGACY 2.3 Apr,28,2004 p4



## **Conclusions for the single-station, multi-day, arc-offset solution**

Is it better than the traditional solutions?

A direct answer is *not* possible because reliable truth data to perform comparison are not available.

Models of the electron density can provide with “artificial data” to check the performance of the technique used for the calibration,

**but they will not “simulate” the problems of the observations (multi-path)**

Some positive aspects:

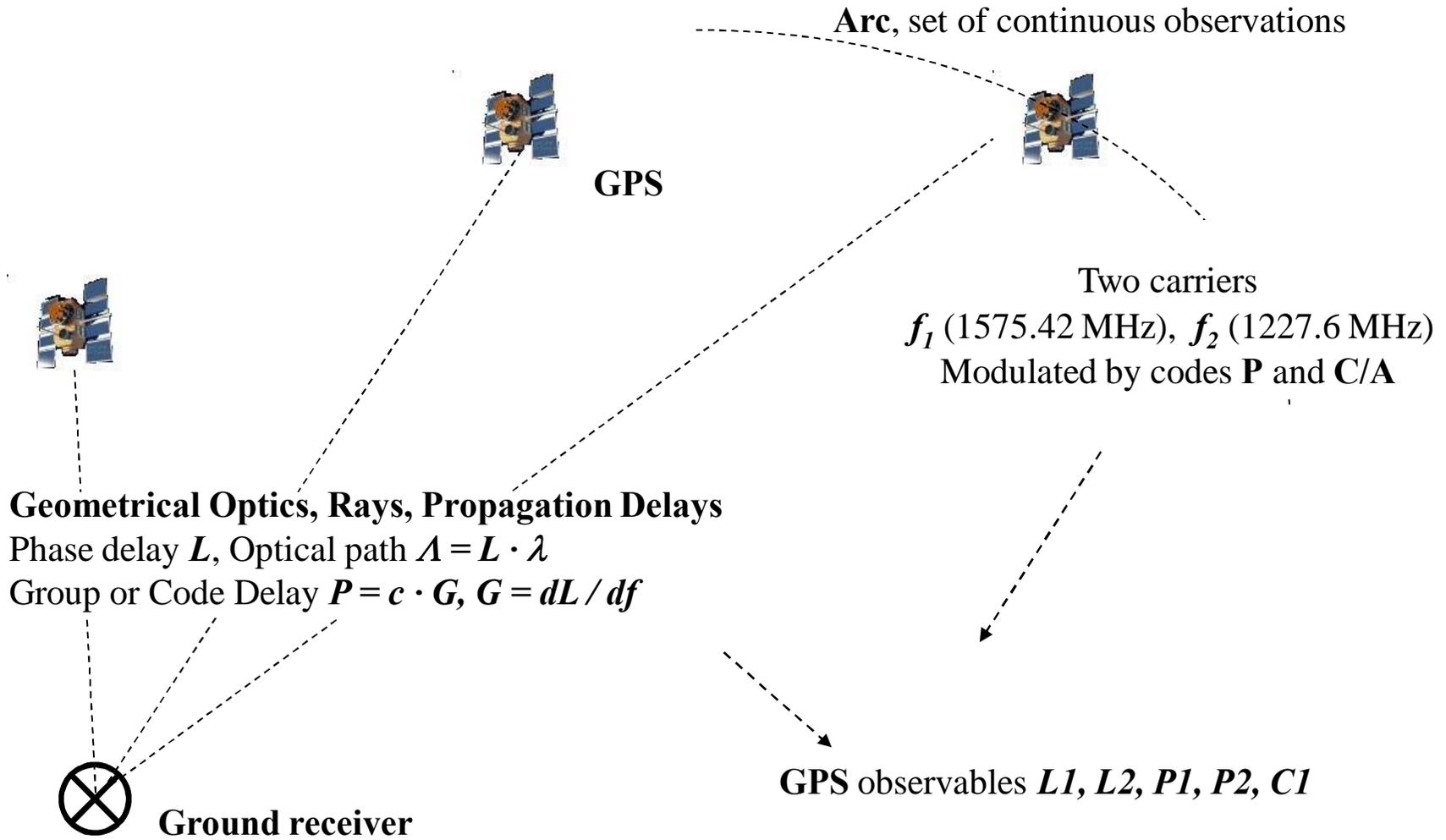
*TEC*'s from two co-located receivers is the same

In the following, “details” and use of “artificial data” will be briefly discussed

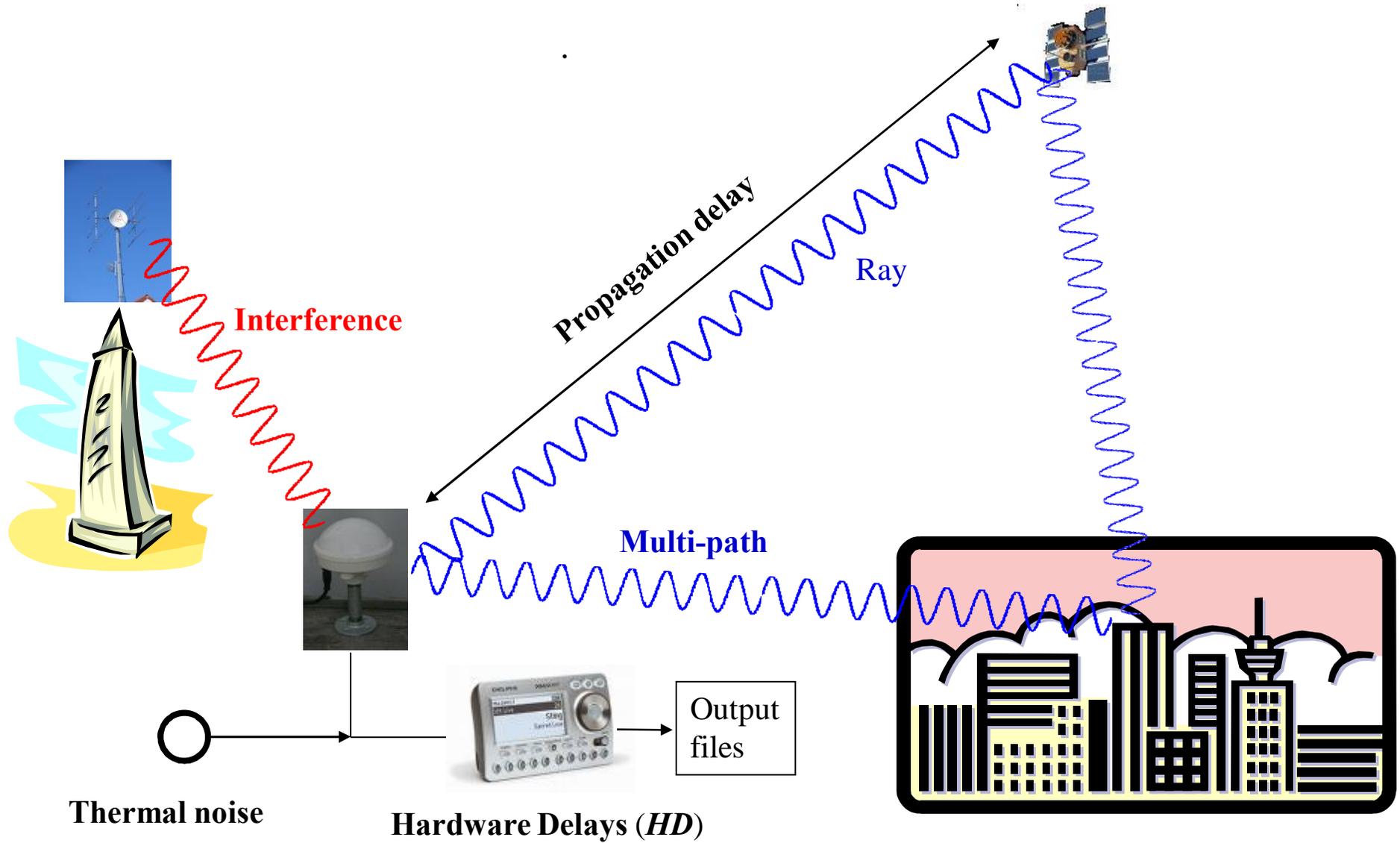
End of the description of calibration:

Some detail

# GPS scenario



# Propagation delays, Disturbances, Hardware Delays, Multi-Path



## Propagation Delays

Propagation and Atmospheric contributions to optical path  $L$ :

**Geometric (D)istance), T**ropospheric, **I**onospheric

$$L = D + T + I$$

Equivalent Group Path  $P =$  Group delay  $G \times$  speed of light

$$P = G \cdot c = D + T - I$$

Refractivity  $R = n - 1$ ,  $n$  Index of Refraction

$$T = \int R_{atm}(s) ds \quad I = \int R_{Iono}(s) ds \quad R_{Iono} = -\frac{40.3 \cdot N_e}{f^2},$$

$$TEC = \int N_e(s) ds, \quad I = -\frac{40.3 \cdot TEC}{f^2}$$

$$L = \frac{D + T + I}{\lambda} = \frac{f}{c}(D + T) - \frac{40.3 TEC}{cf}$$

$$G = \frac{dL}{df} = \frac{D + T}{c} + \frac{40.3 TEC}{cf^2}$$

Measurements introduce additional "delays"

Hardware electronic delays originating

in satellite and receiver,  $\beta, \gamma$

Offset (delay, ambiguity) for phase  $\Omega$

Noise  $n$

Multipath  $m$

User clock offset  $\tau$

Code delay affected by user clock offset is *pseudorange*

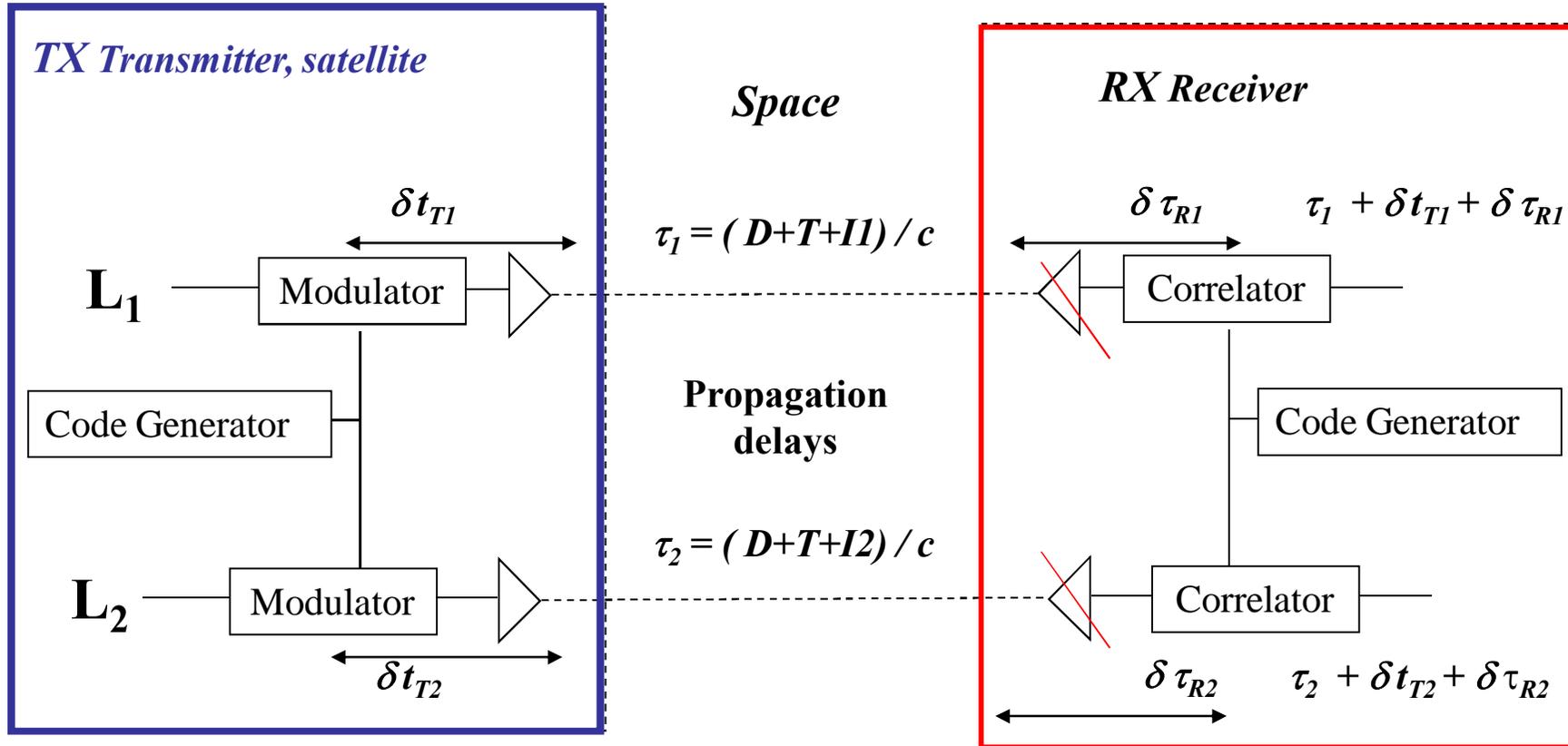
$$P = D + T - I + \beta + \gamma + n + m + \tau$$

For following discussion, noise and multipath can be neglected for phase delays.

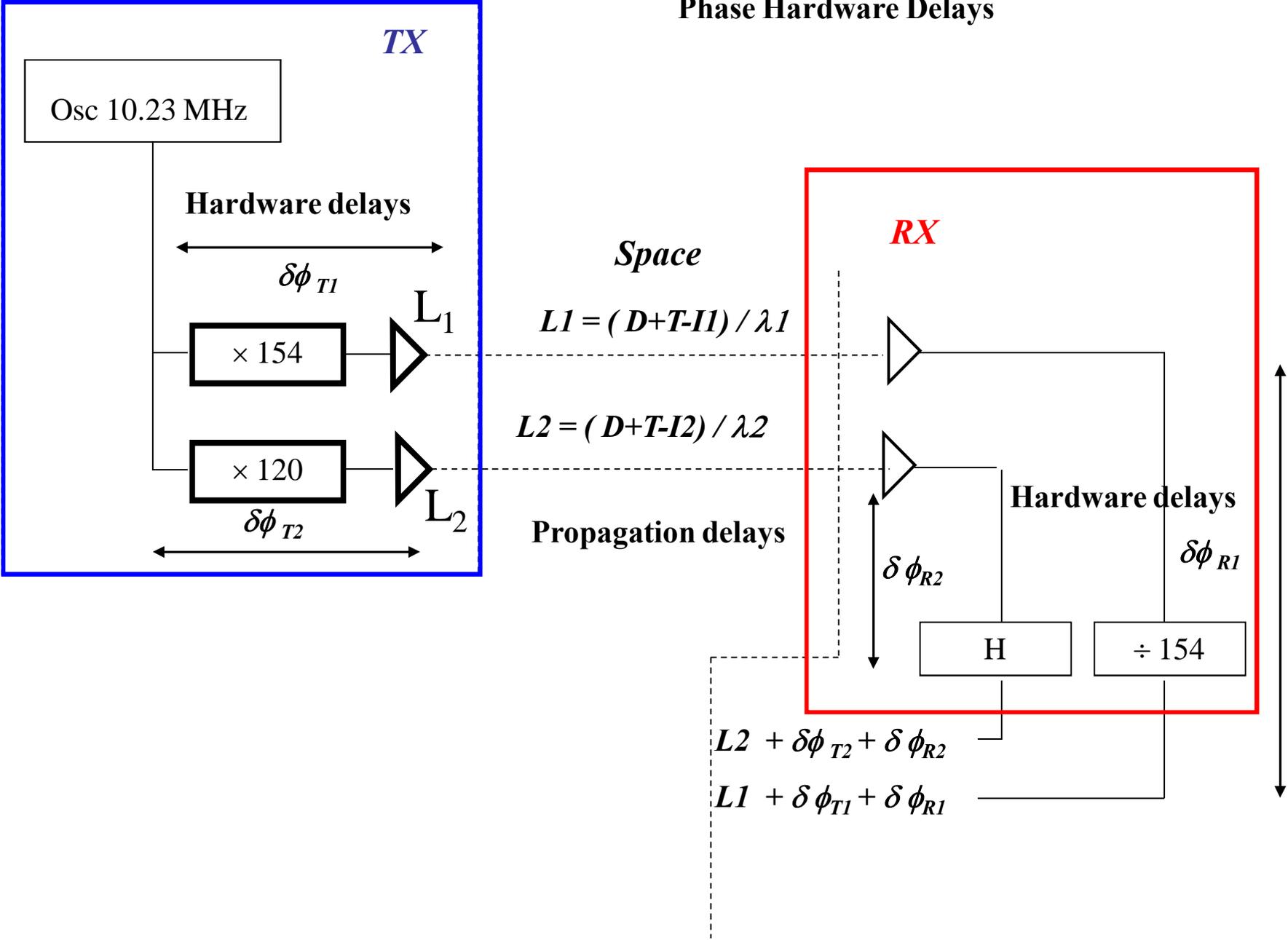
Hardware delays for phase are included in  $\Omega$

$$A = D + T + I + \Omega$$

### Code hardware delays



**Phase Hardware Delays**



Availing GPS delays *P1, P2, L1, L2, C1*

Users aiming to determine their position, will get rid of ionospheric contribution taking proper combinations of them.

Users aiming to investigate ionosphere, will simply compute differential delays

Differential pseudorange

$$P2 - P1$$

Differential phase path

$$\Lambda1 - \Lambda2 = L1 \cdot \lambda1 - L2 \cdot \lambda2$$

Both differential delays are in meters.

Following steps:

Show dependence on *TEC*

Transform to *TEC units* ( $10^{16}$  electrons/m<sup>2</sup>), *TECu*

## The differential Delays

For the carrier  $i$  ( $i = 1,2$ ), contributions with no index do not depend on frequency and cancel out forming differential delays

$$P_i = G_i \cdot c = D + T - I_i + \beta_i + \gamma_i + n_i + m_i + \tau,$$

$$\underline{\Delta P = P_2 - P_1 = I_1 - I_2 + \Delta\beta + \Delta\gamma + \Delta n + \Delta m}$$

$$A_i = D + T + I_i + \Omega_i$$

$$\underline{\Delta A = A_1 - A_2 = I_1 - I_2 + \Delta\Omega}$$

$$I_2 - I_1 = k \cdot TEC \quad k = 40.3 TEC \left( \frac{1}{f_2^2} - \frac{1}{f_1^2} \right)$$

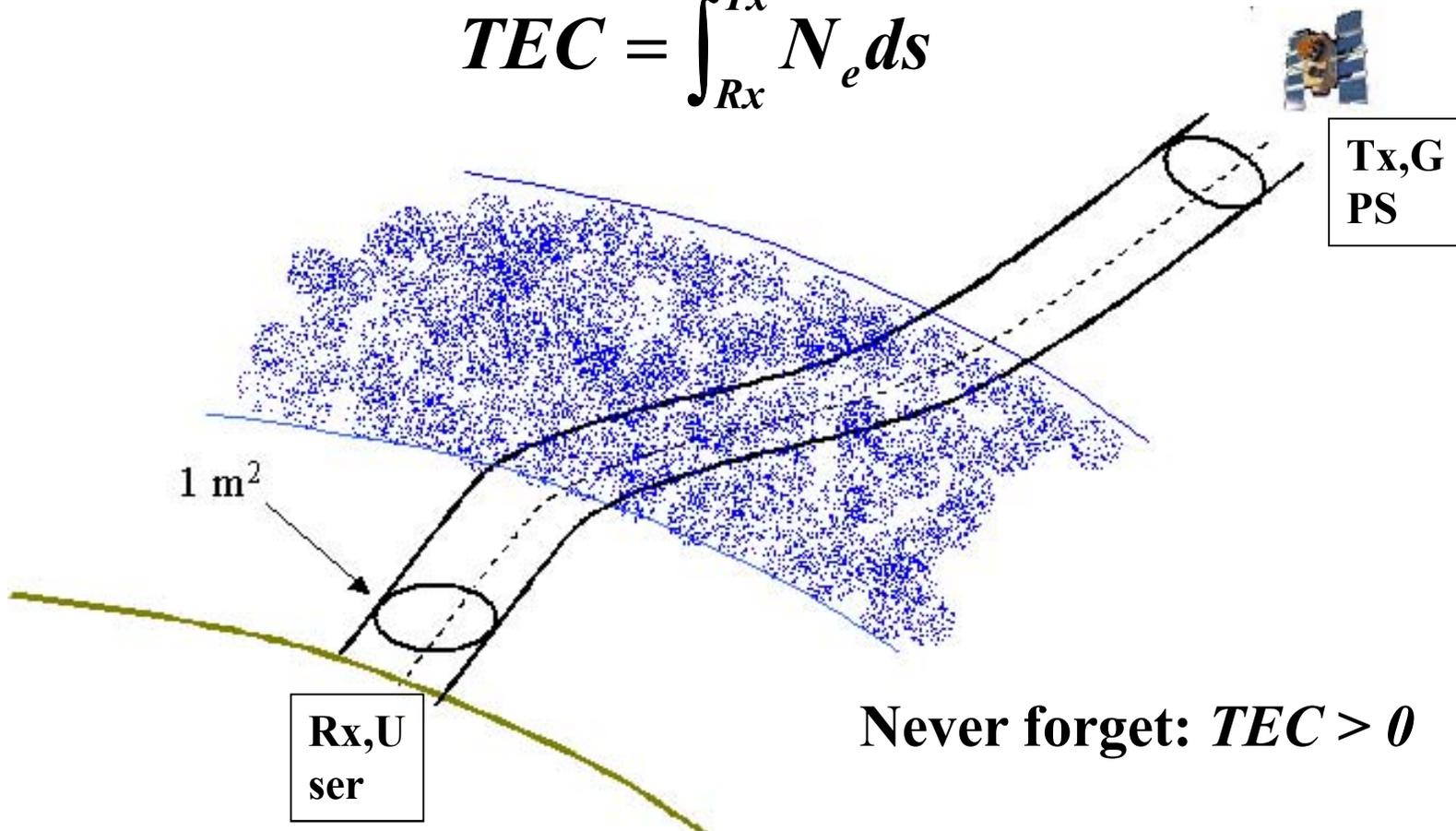
Divide by  $k \cdot 10^{-16}$ , drop out the  $\Delta$  symbol to obtain the *phase slants*  $S_p$  and *group or code slants*  $S_c$  in  $TECu$ , 1  $TECu = 10^{16}$  electrons/m<sup>2</sup>, disregard radio noise  $n$

$$S_p = \frac{1}{k} \cdot (A_1 - A_2) = TEC + \Omega$$

$$S_c = \frac{1}{k} \cdot (P_2 - P_1) = TEC + m + \beta + \gamma$$

The classical interpretation of *TEC* as the **numbers of electrons** contained in a column of unitary base along the ray

$$TEC = \int_{R_x}^{T_x} N_e ds$$



Note for the following: expressions for observations like

$$S = TEC + b$$

denote the set of all available observations used for performing some specific task.

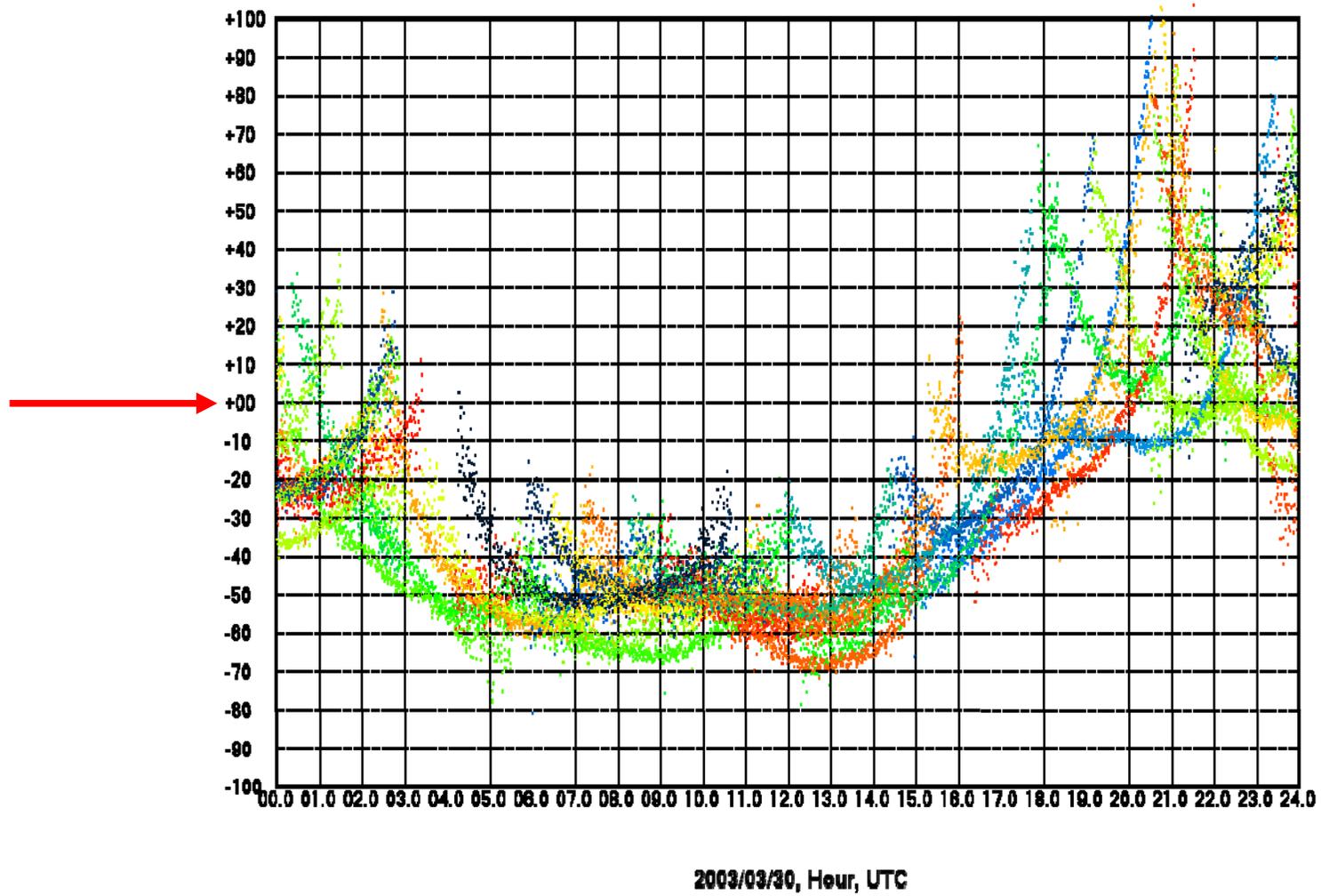
Actually observations should be indexed as  $S_{ijt}$  meaning that the individual observed quantity, the “slant”, refers to  $i^{th}$  satellite,  $j^{th}$  station,  $t^{th}$  time.

Biasing terms can still be indexed according to satellite and station (not time as assumed to be constant), but also according to the specific observed arc.

When needed for clarity, indexing will be explicitly adopted.

# Plot of $S_C$ arcs for one day

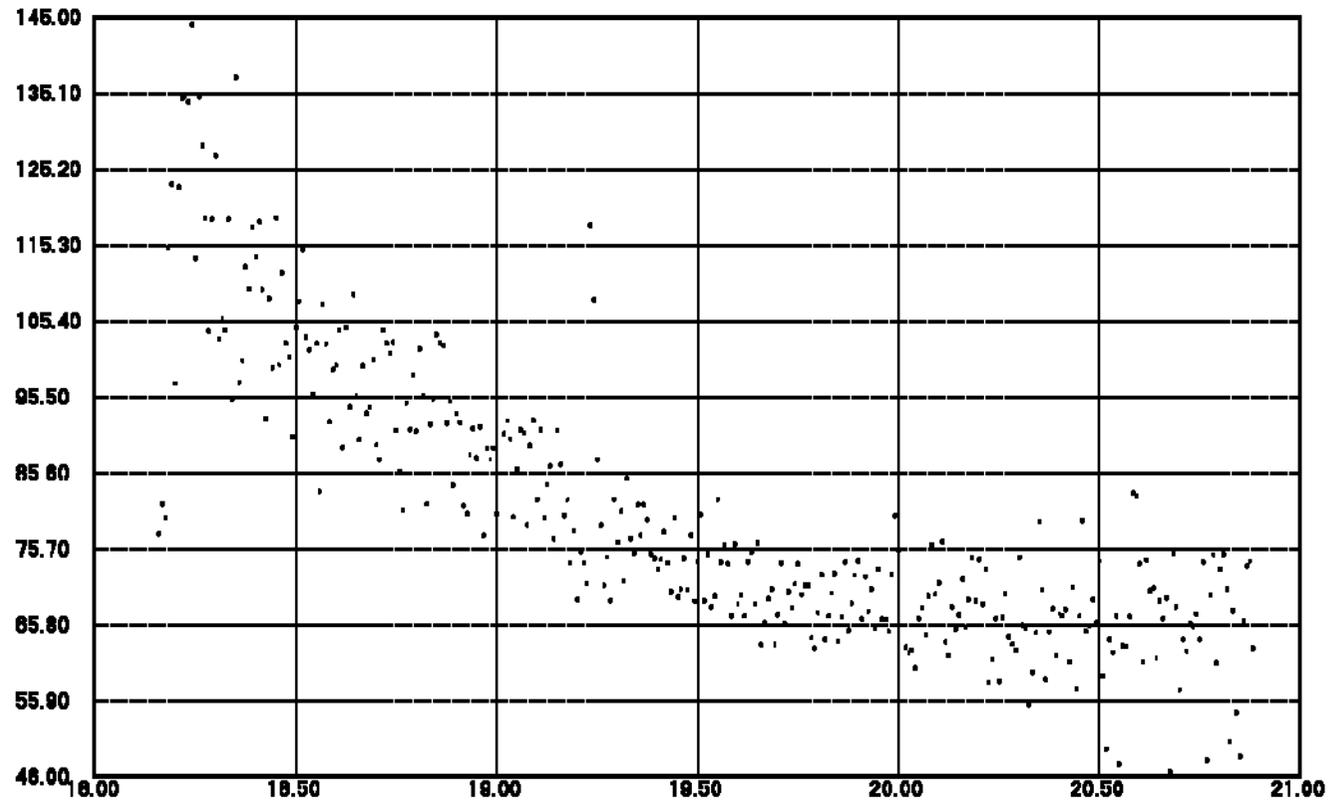
TEC( $10^{16}$ ) albh Lat=48.4N Lon=-123.5E  
2025 AOA BENCHMARK ACT 3.3.32.2N lk 99/07/2



**\* Evidence that calibration is needed: TEC is a positive quantity**

# Sample $S_C$ , one arc: the common situation

Code Slant (TECu), PRN#=25 meta Lat=40.6N Lon=16.7E RecTypeVer = 21580 TRIMBLE 4000SSI NAV 7.29 SIG 3.07

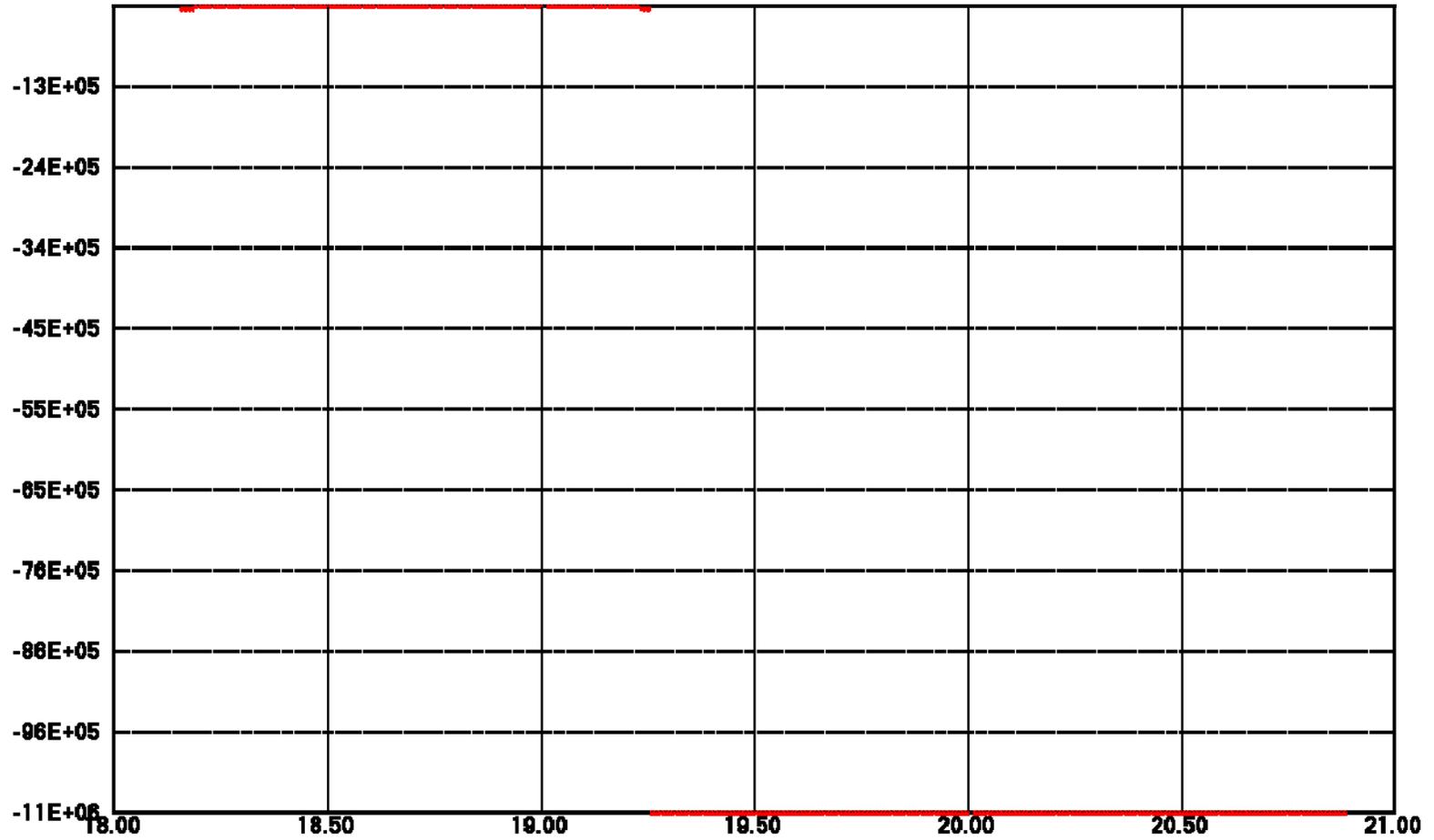


2000/03/30, Hour, UTC

Sample  $S_p$ , one arc: the common situation (phase jumps)

Phase Slant (TECu), PRN#=26 mate Lat=40.6N Lon=16.7E RecTypeVer = 21580

TRIMBLE 4000SSI NAV 7.29 SIG 3.07

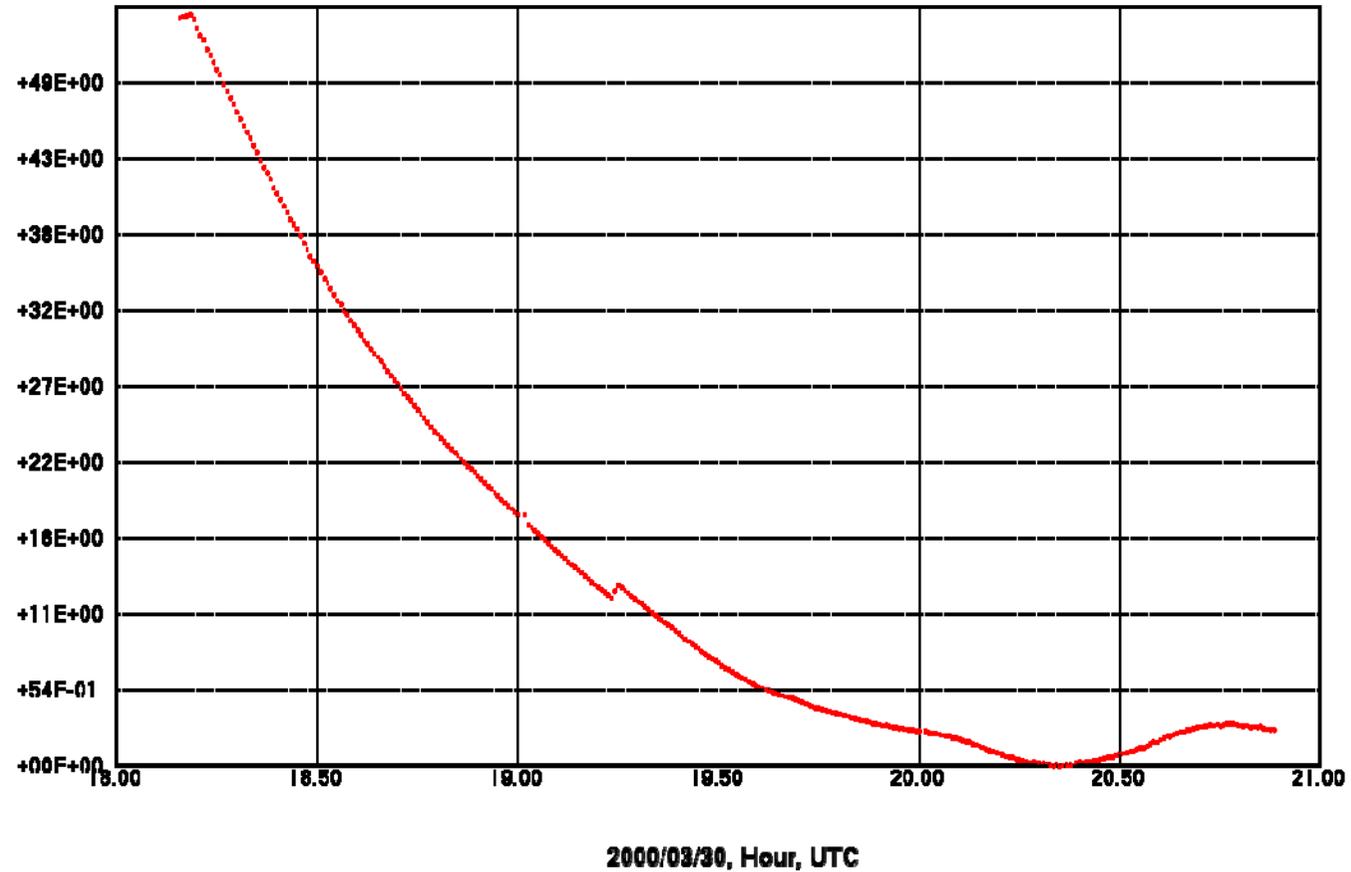


2000/03/30, Hour, UTC

Sample  $S_p$ , one arc, : after removing jumps, fixing the minimum to zero

Phase Slant (TECu), PRNF=25 mete Lat=40.6N Lon=16.7E RecTypeVer = 21580

TRIMBLE 4000SSI NAV 7.29 SIG 3.07



Offset  $\Omega$  is an arbitrary quantity: can we set it in some useful way?

**A new set of observables: Phase slants leveled to Code**

Operator  $\langle \cdot \rangle$  is a properly selected weighted (possibly robust) average

Build, arc by arc, the leveled slants  $S_L$

$$S_L = S_P - \langle S_P - S_C \rangle$$

$$\langle S_P - S_C \rangle = \Omega - \langle m \rangle - \beta - \gamma$$

$$S_L = TEC + \langle m \rangle + \beta + \gamma$$

Properties of  $S_L$

Noise is the same (neglected) of phase slants

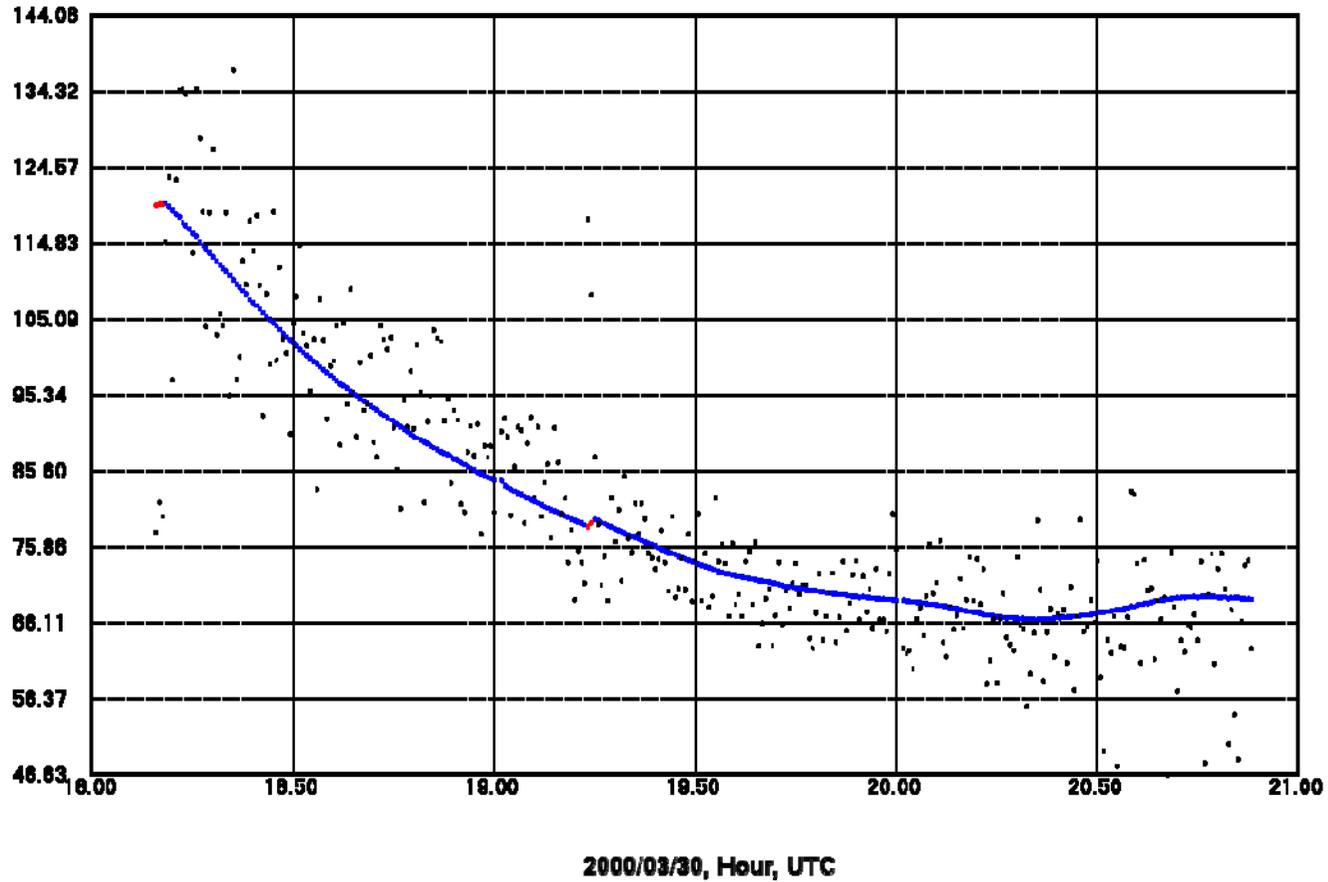
Biased exactly as code slants

**But:** an arc dependent constant leveling error  $\lambda = \langle n \rangle + \langle m \rangle$  appears

Sample  $S_C$  and  $S_P$  with properly selected phase offset  $\Omega = S_L$

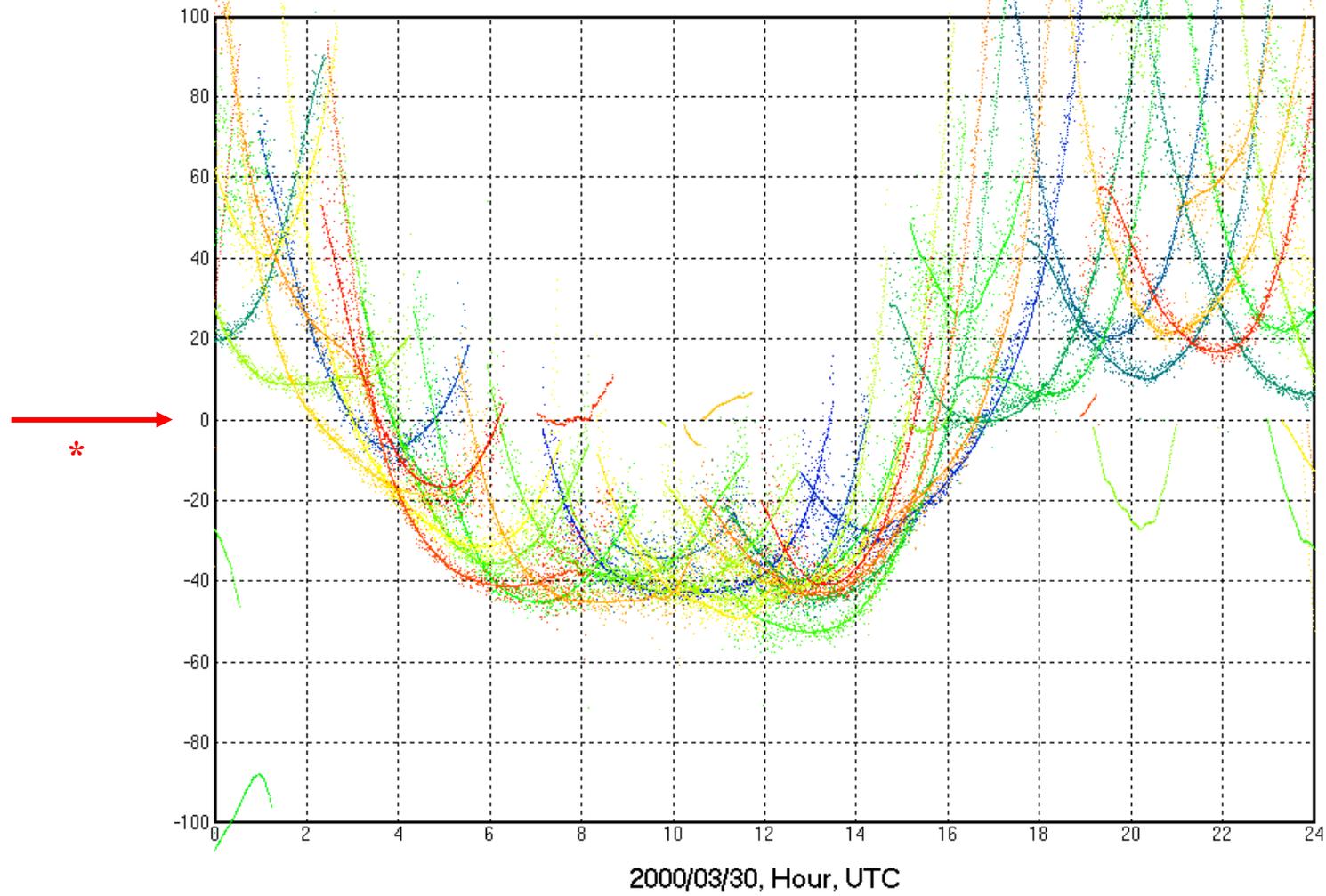
mate Lat=40.6N Lon=16.7E RecTypeVer = 21580

TRIMBLE 4000SSI NAV 7.28 SIG 3.07



# One day, $S_C$ and $S_L$ arcs

TEC( $10^{16}$ ) albh Lat=48.4N Lon=123.5W



**\* Evidence that calibration is needed: TEC is a positive quantity**

How do traditional and proposed solution compare?

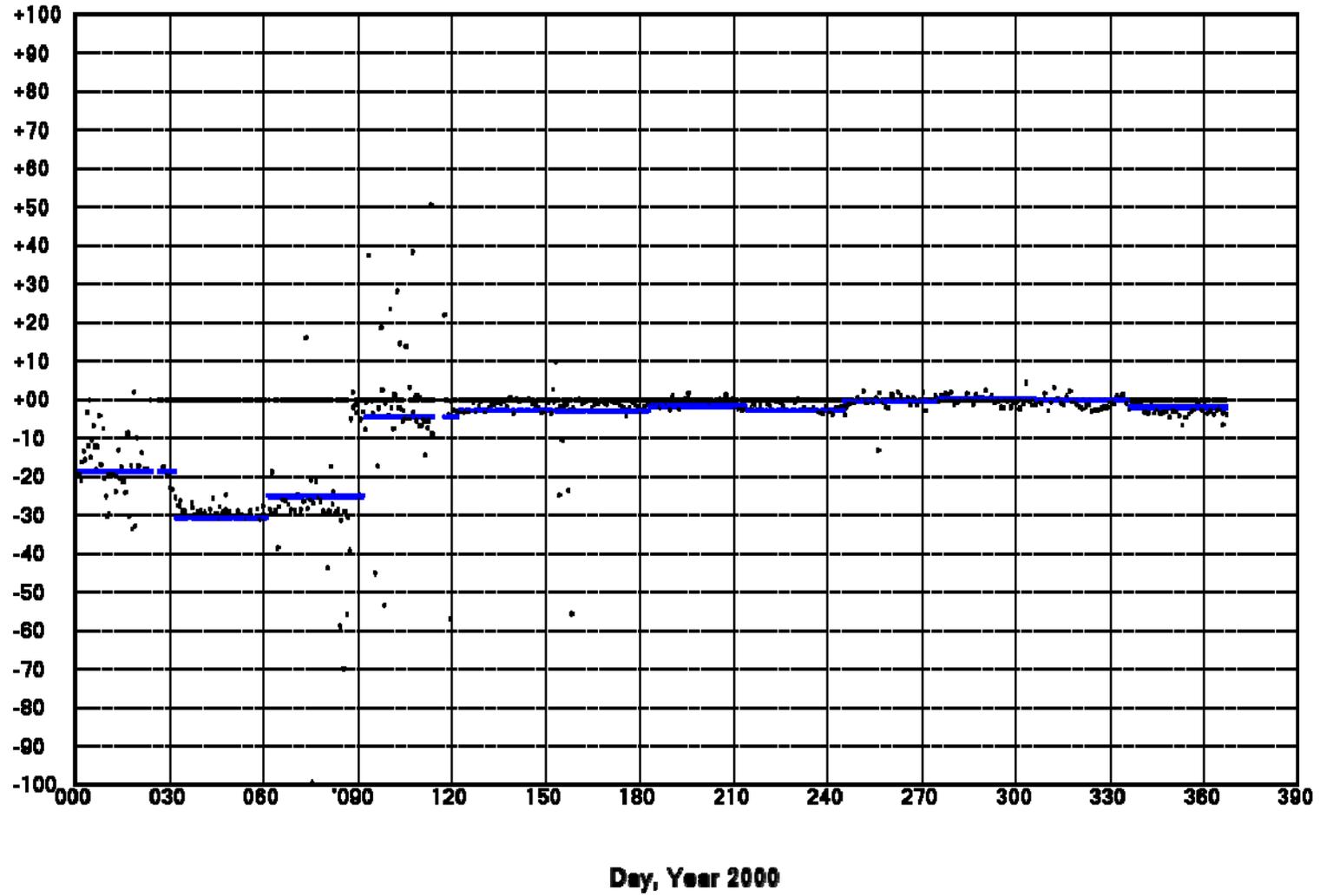
In the following slides it can be seen that the two solutions agree in the average, but the difference in bias can amount to 10 *TECu*

The pattern of the jumps, similar for different satellites, simply indicates that something has changed in the receiver

# CODE Station + Satellite Biases

Arc offset solution, individual values

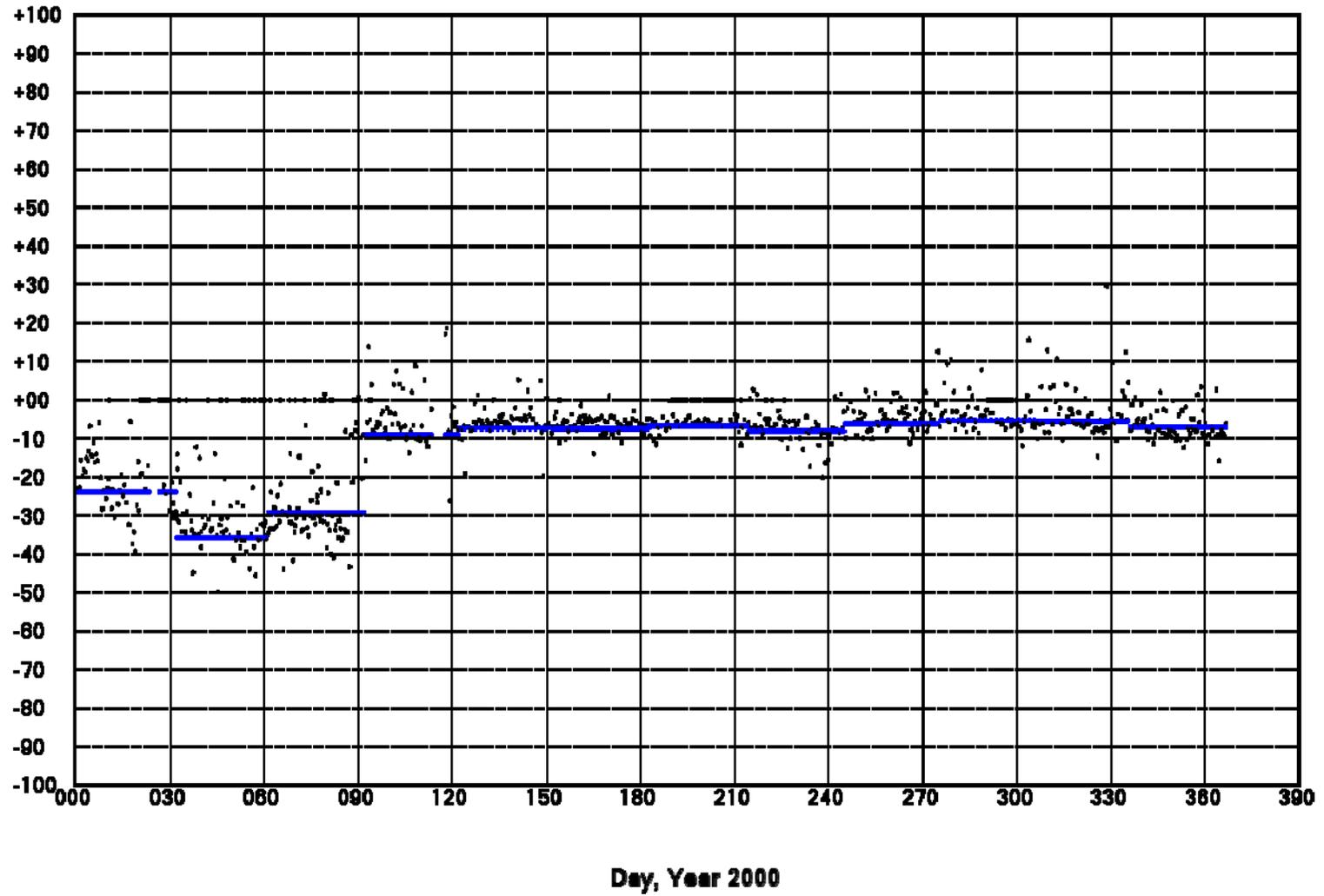
Station brus PRN #1



# CODE Station + Satellite Biases

Station brue PRN #4

Arc offset solution, individual values



Thank you