



**The Abdus Salam  
International Centre for Theoretical Physics**



**2139-14**

**School on Synchrotron and Free-Electron-Laser Sources and their  
Multidisciplinary Applications**

*26 April - 7 May, 2010*

**Powder Diffraction - overview and applications**

Paolo Scardi  
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ICTP School on Synchrotron and Free-Electron-Laser Sources and their Multidisciplinary Applications  
Trieste, April 26 - May 7, 2010

# Powder Diffraction

## overview and applications

Prof. Paolo Scardi

Department of Materials Engineering and Industrial Technologies,  
University of Trento





# PRESENTATION OUTLINE

## PART 1

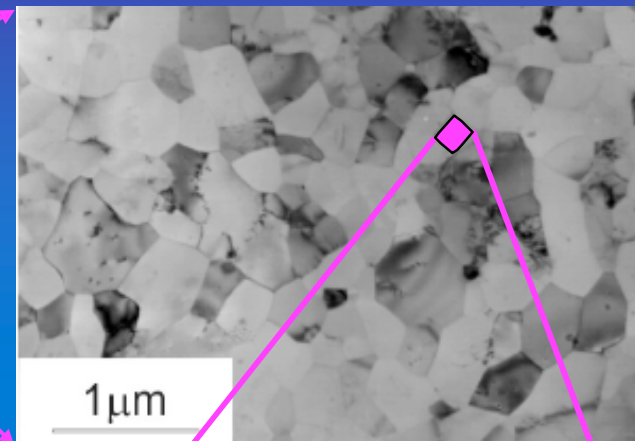
- Basic elements of crystallography and X-ray diffraction (XRD) theory
  - Some advantages and peculiarities of synchrotron radiation XRD (SRXRD)
- 

## PART 2

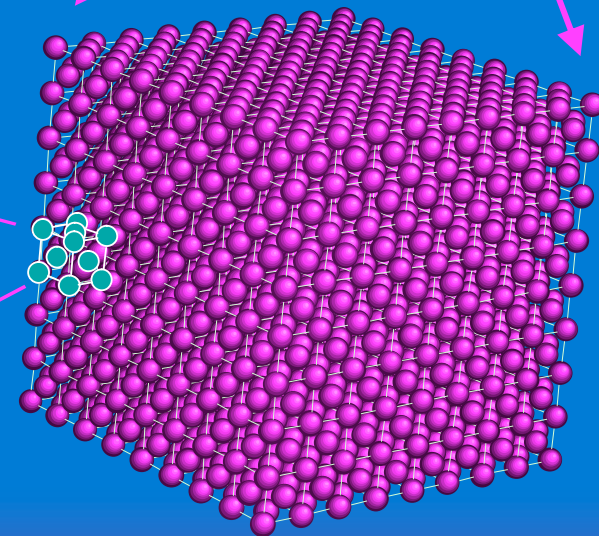
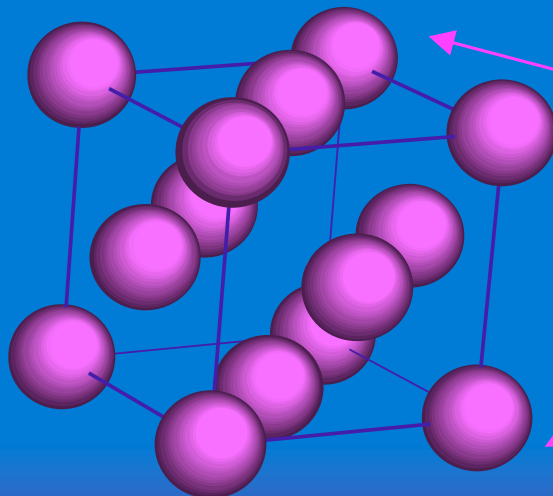
- SRXRD from nanocrystalline and highly deformed materials



# STRUCTURE & MICROSTRUCTURE

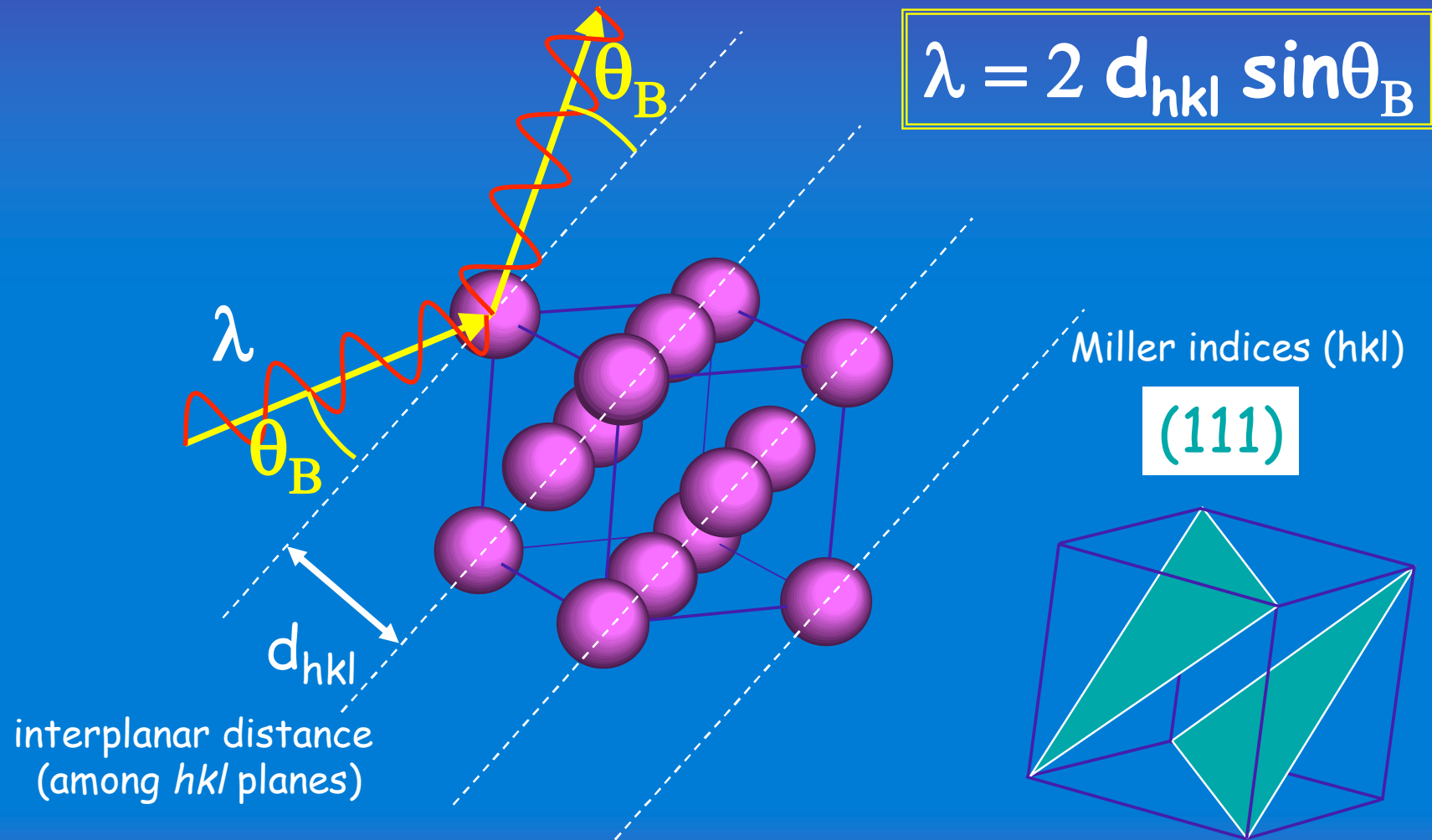


Al





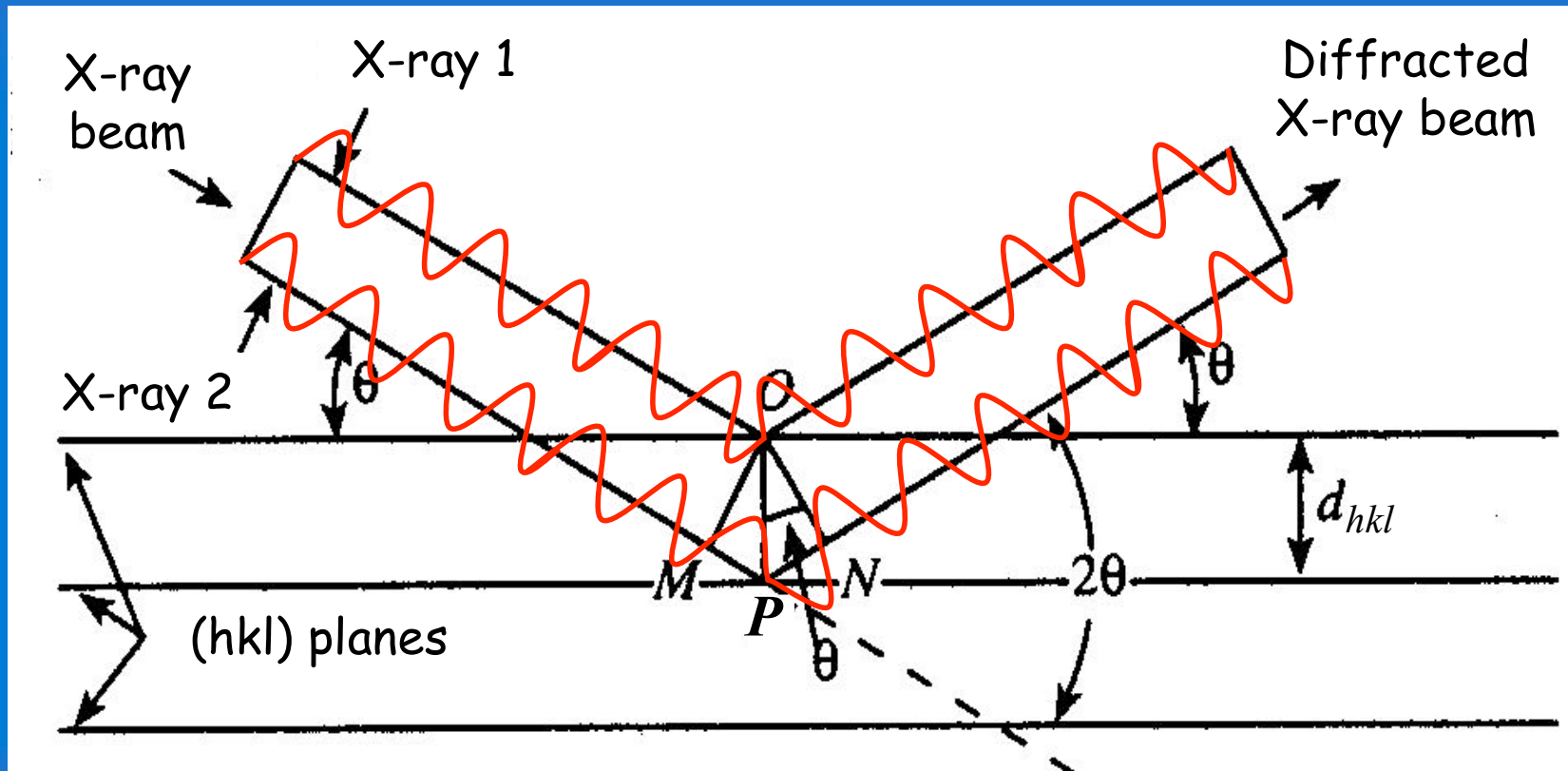
# ATOMIC PLANES AND DIFFRACTION CONDITION





## ATOMIC PLANES AND DIFFRACTION CONDITION

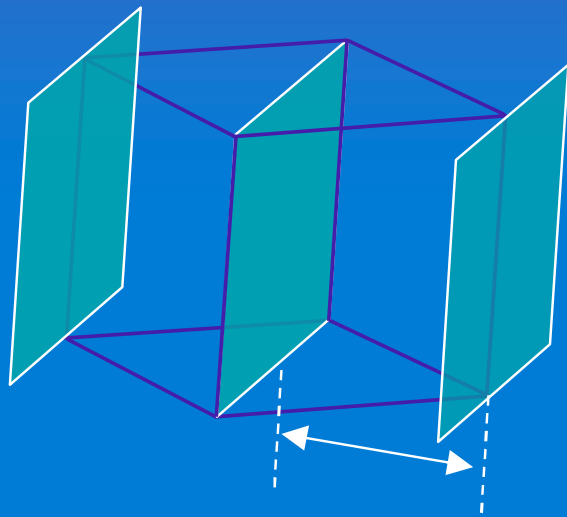
$$MP + PN = 2d_{hkl} \sin \theta = n\lambda \quad \text{Bragg Law}$$



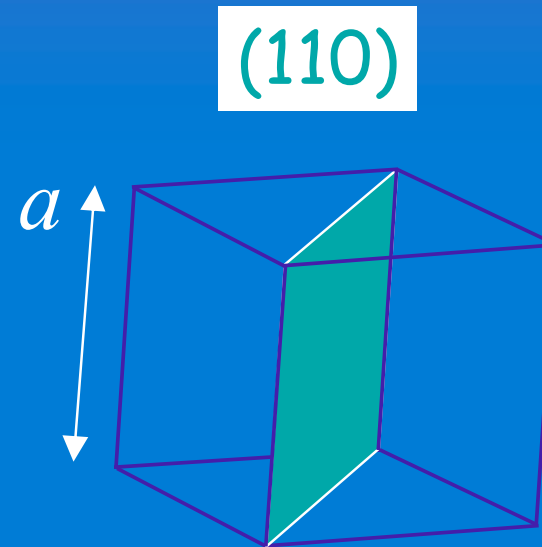


# ATOMIC PLANES AND DIFFRACTION CONDITION

Interplanar distance,  $d_{hkl}$



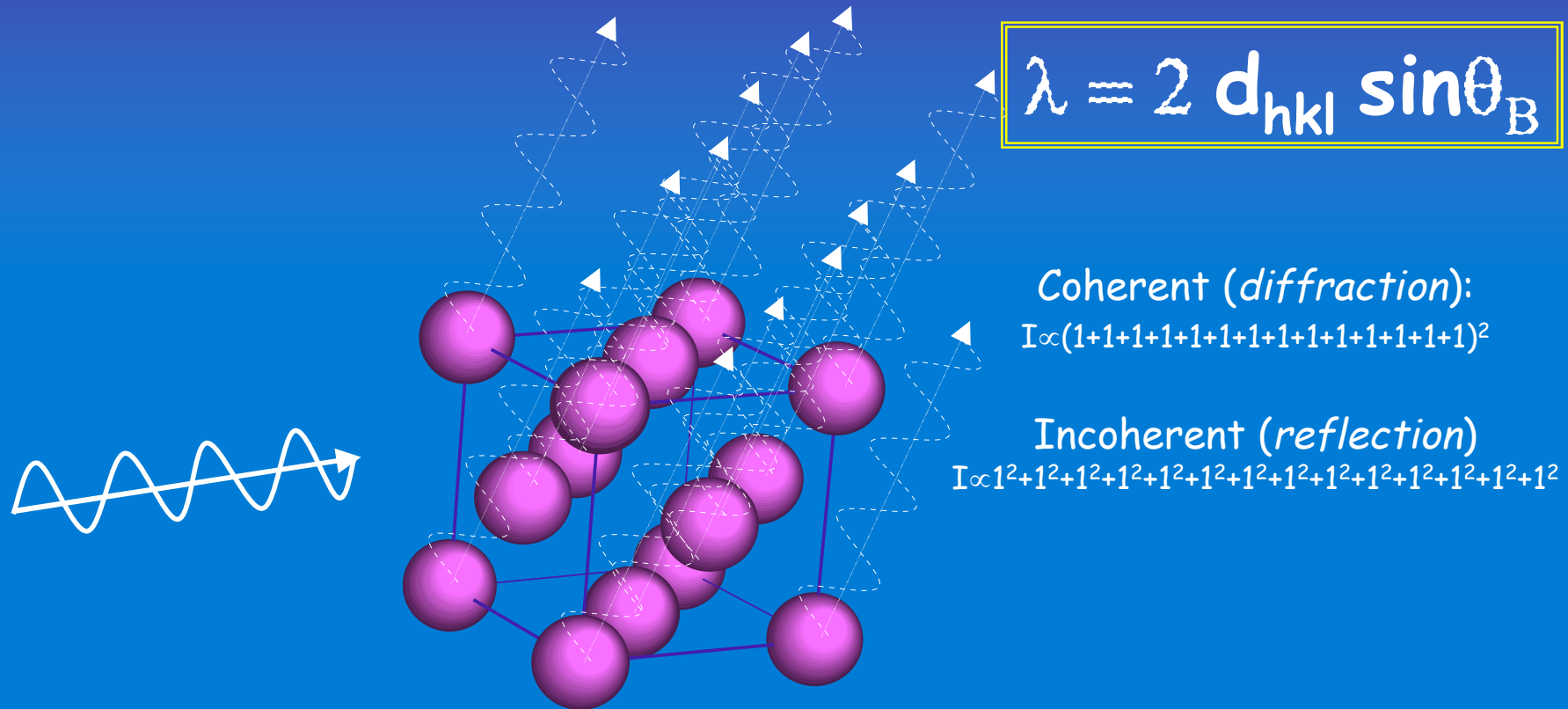
$$d_{110} = \frac{a}{\sqrt{1^2 + 1^2}} = a/\sqrt{2}$$



For cubic materials: 
$$d_{hkl} = \frac{a}{\sqrt{h^2 + k^2 + l^2}}$$



# COHERENT vs INCOHERENT SCATTERING



In diffraction conditions the scattered intensity is proportional to the square of the sum of the amplitudes

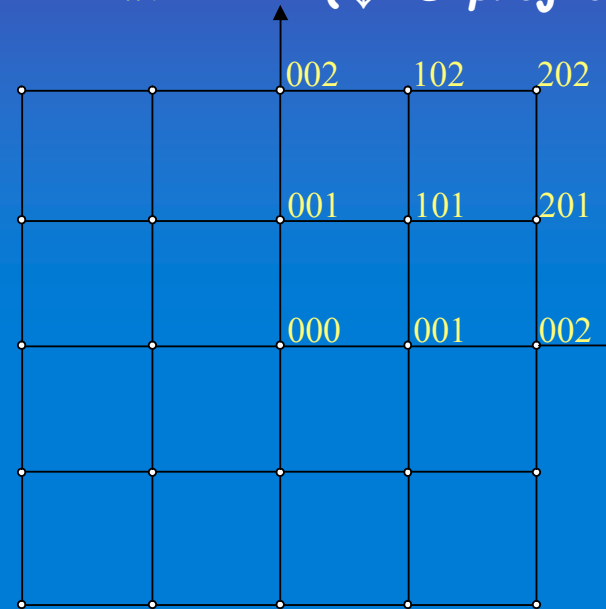
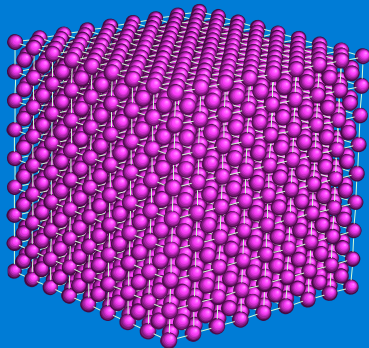
(all atoms are 'in phase')





# DIRECT AND RECIPROCAL SPACE

For a perfect (infinite) crystal the **reciprocal lattice** is made of *infinitely small* points representing sets of planes of Miller indices ***hkl*** (↓ 2D projection)

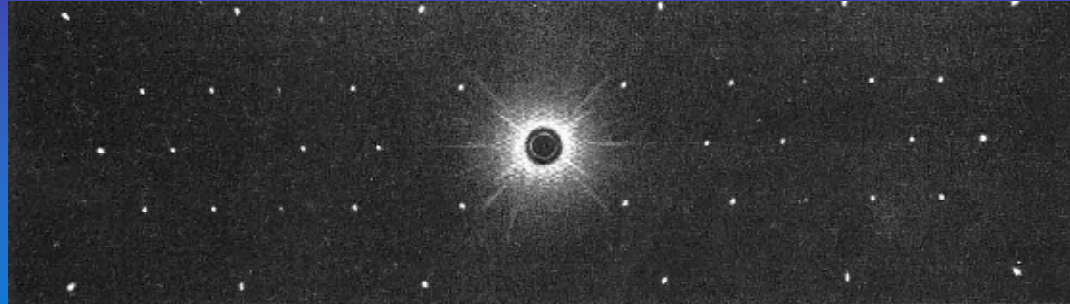
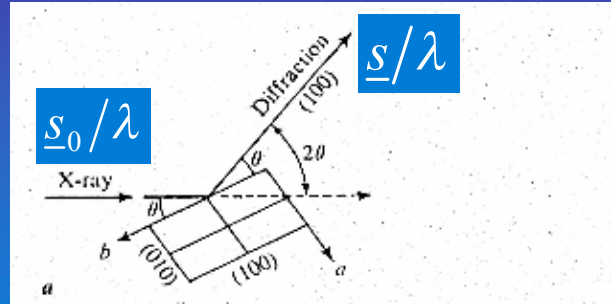


The distance  $d_{hkl}^*$  from the 000 origin to a ***hkl*** point is the **inverse of the interplanar distance**

$$d_{hkl}^* = \left| \underline{d_{hkl}^*} \right| = \frac{1}{d_{hkl}}$$



# DIFFRACTION FROM A SINGLE CRYSTAL



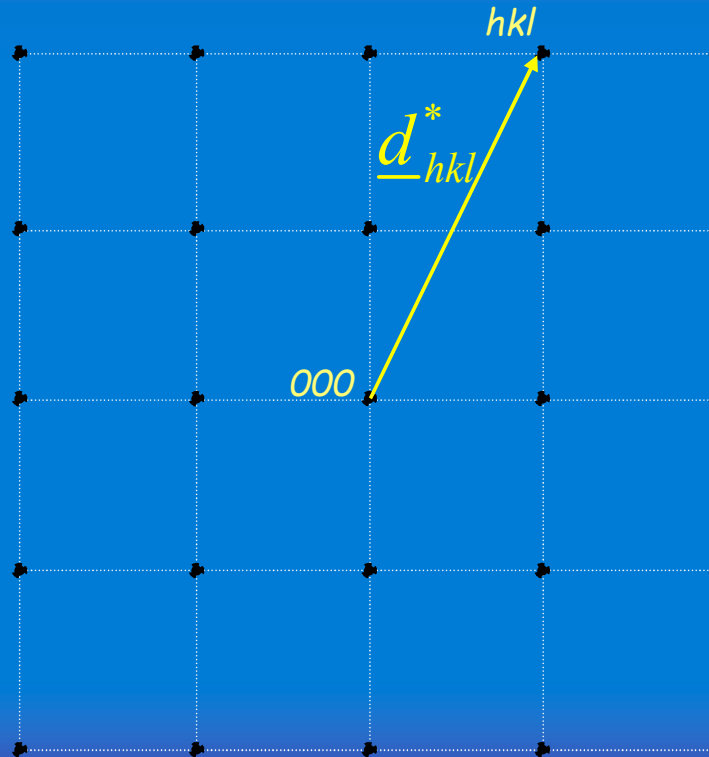
Diffraction conditions correspond to the scattering vector  $(\underline{s} - \underline{s}_0)/\lambda$  being equal to:

$$\frac{\underline{s}}{\lambda} - \frac{\underline{s}_0}{\lambda} = \underline{d}_{hkl}^*$$



$$\lambda = 2 d_{hkl} \sin \theta$$

Bragg law





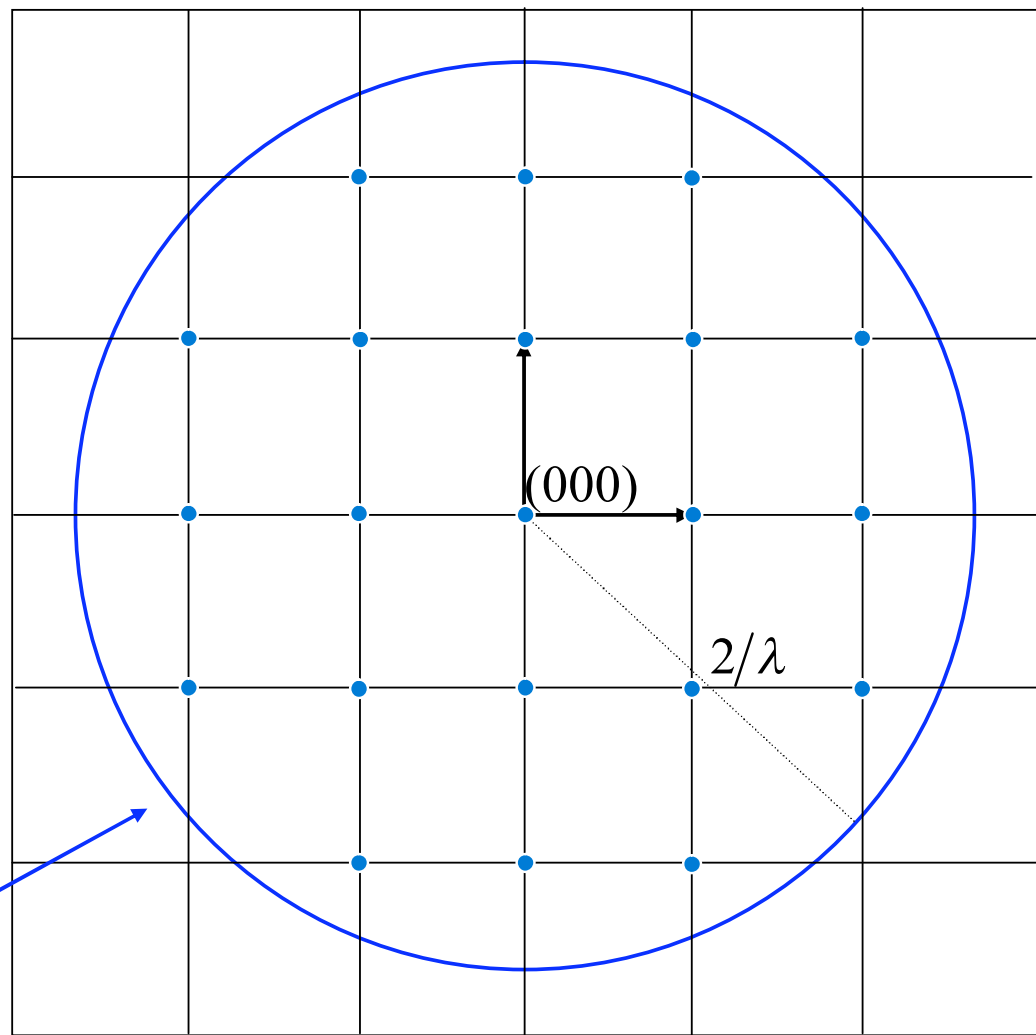
# RECIPROCAL LATTICE: DIFFRACTION CONDITIONS

For a given wavelength, the Bragg law sets a limit to the interplanar distances for which diffraction is observed:

$$\sin \theta = \lambda/2d = \lambda d^*/2 \leq 1$$

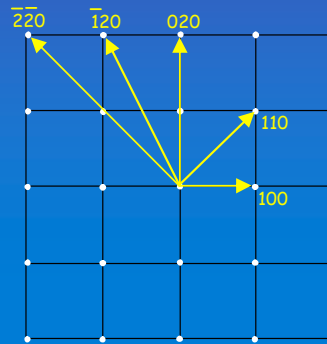
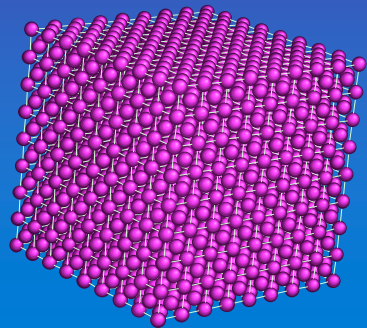
$$d^* \leq \frac{2}{\lambda}$$

All points representing planes that can diffract are inside a sphere of finite radius,  $2/\lambda$  (*limiting sphere*)

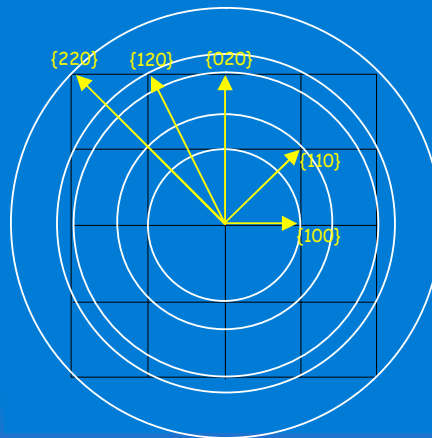
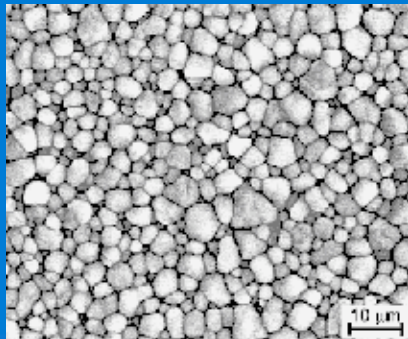




# DIFFRACTION: SINGLE CRYSTAL AND POWDER



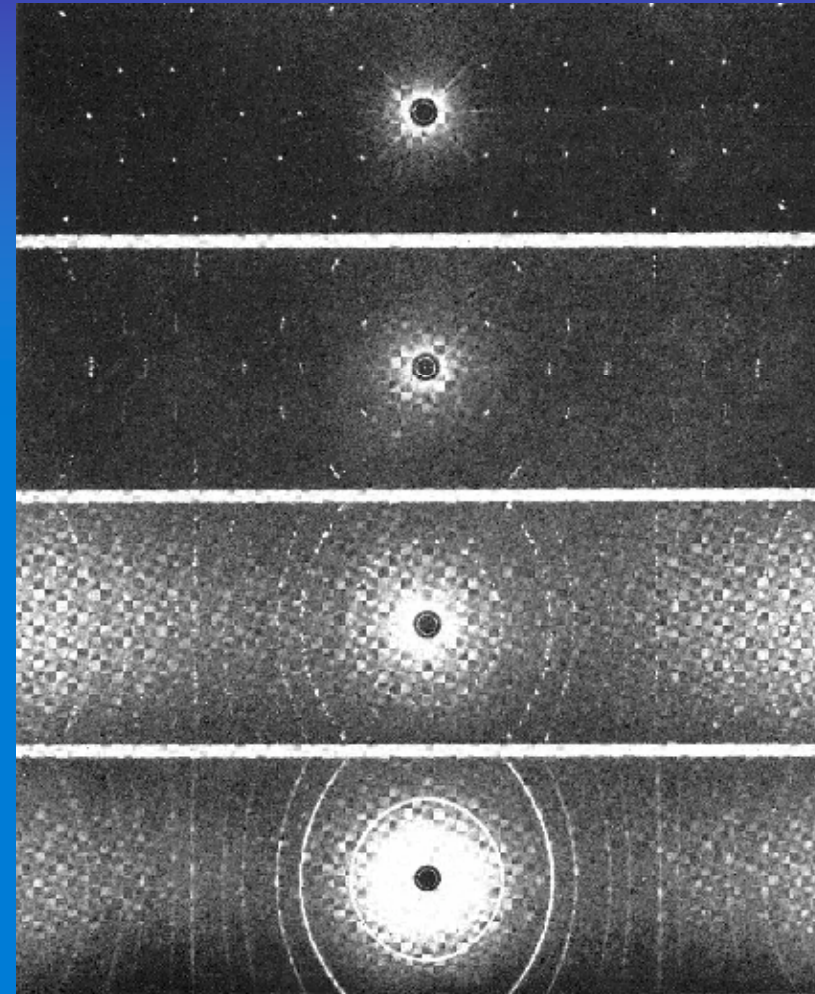
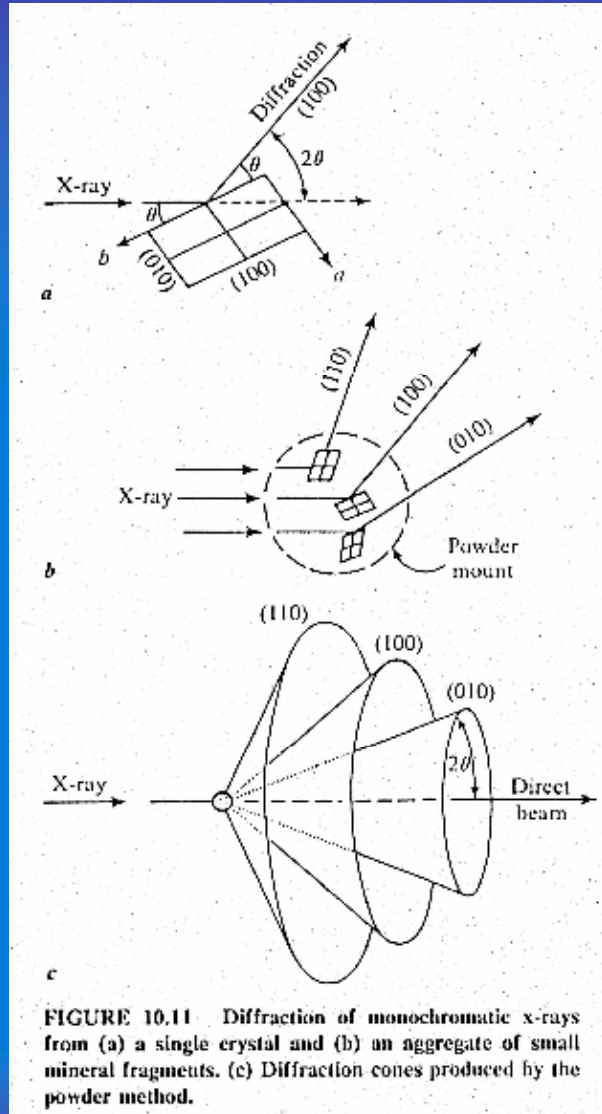
single crystal



powder  
(bulk polycrystalline)



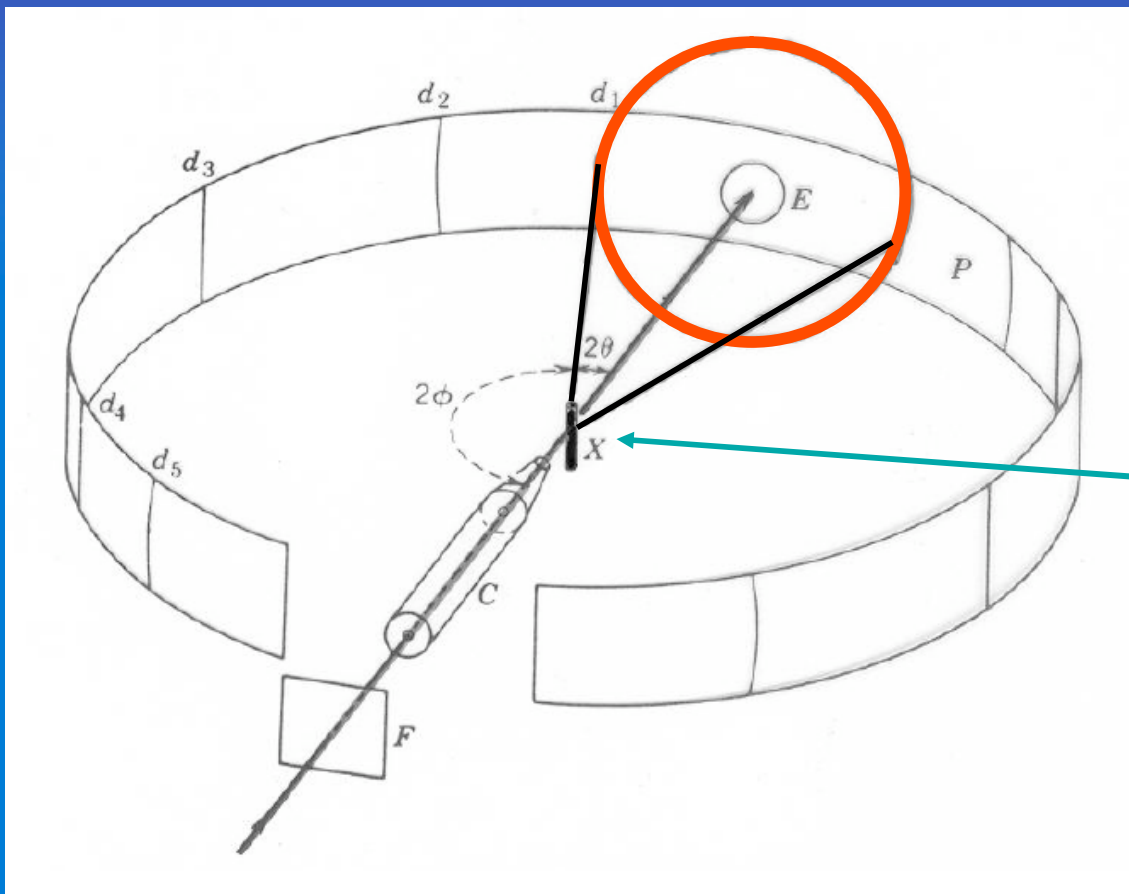
# DIFFRACTION: SINGLE CRYSTAL AND POWDER



(From top to bottom). Fig. 197: Single-crystal rotation photograph of fluorite [100] vertical; Fig. 198: Single crystal rotation photograph of fluorite [200] 2° to vertical; Fig. 199: X-ray photograph of five randomly oriented crystals of fluorite; Fig. 200: Powder photograph of fluorite.



# DEBYE-SCHERRER GEOMETRY



POWDER



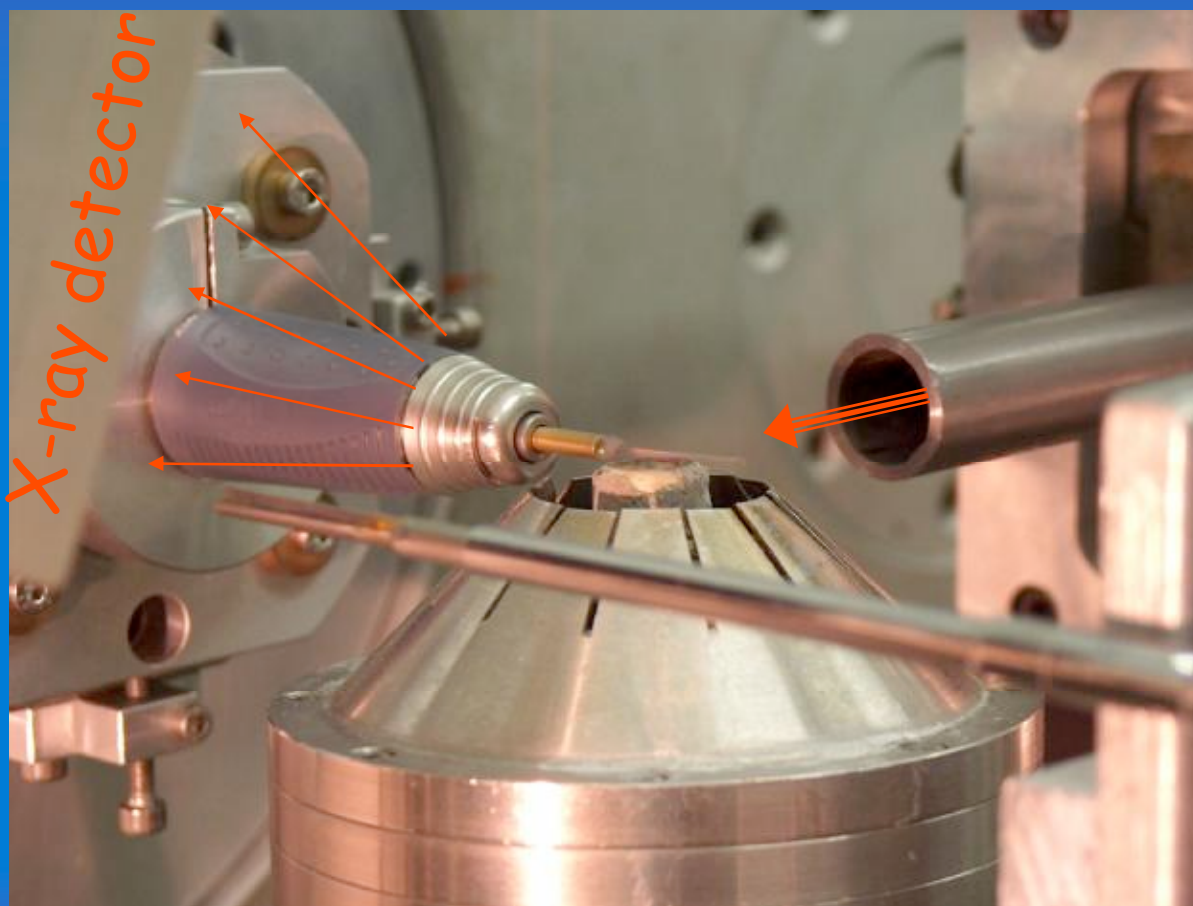
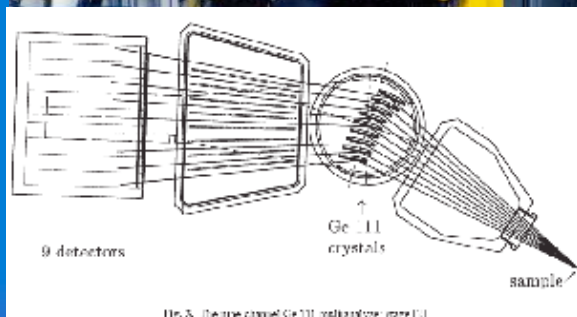
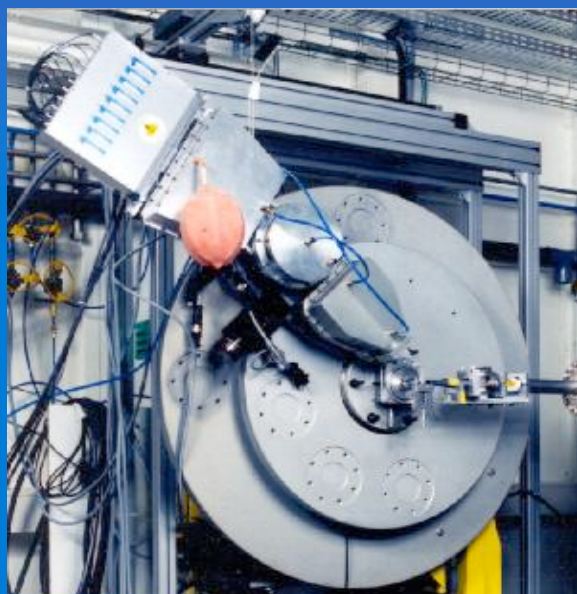


# SRXRD POWDER GEOMETRY: A TYPICAL EXAMPLE

## Parallel beam geometry at ID31 (ESRF)

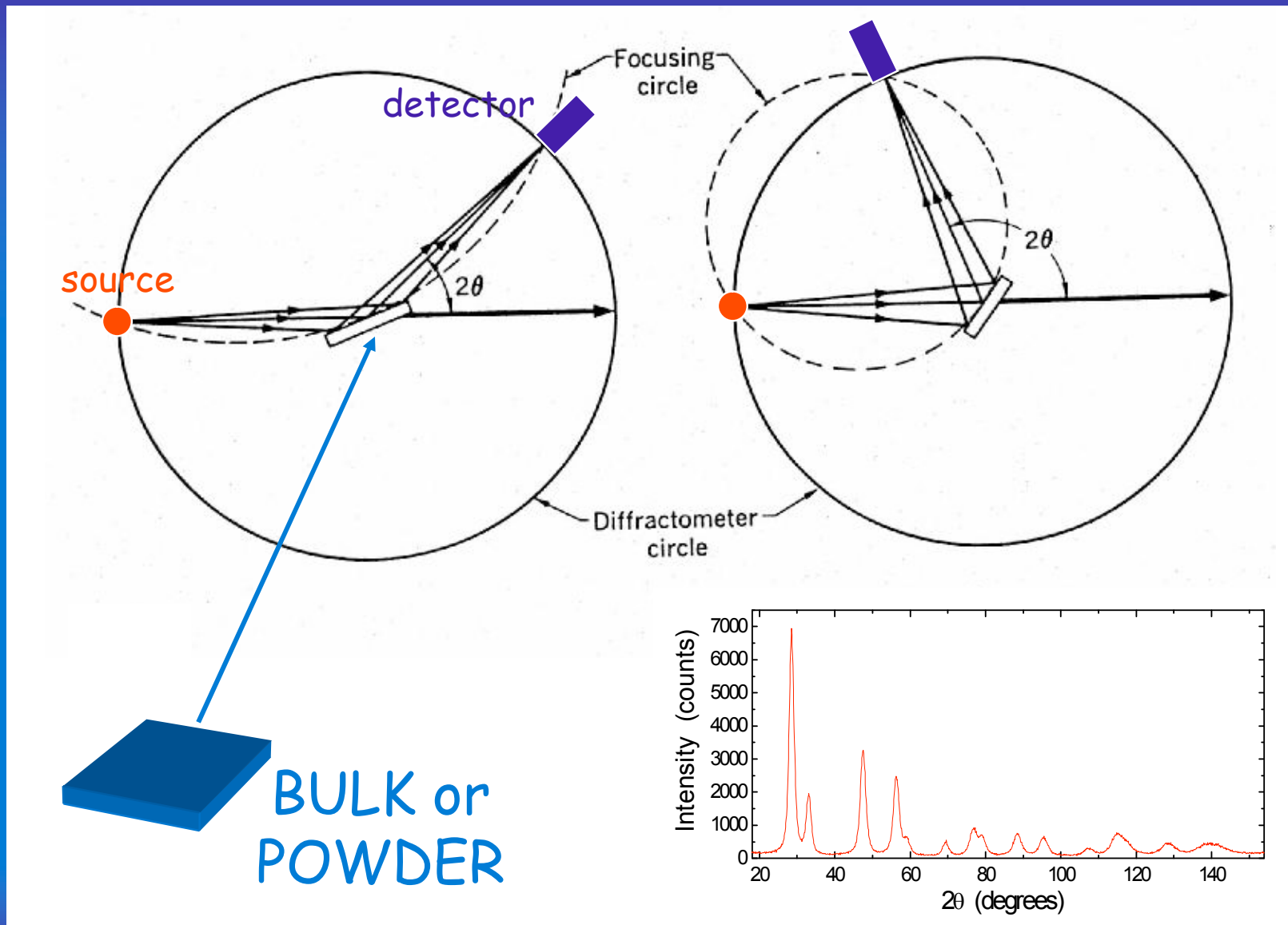
ID31 Goniometer and  
nine-crystal analyzer

capillary holder / high temperature blower





# TYPICAL LAB GEOMETRY: BRAGG-BRENTANO (POWDER)



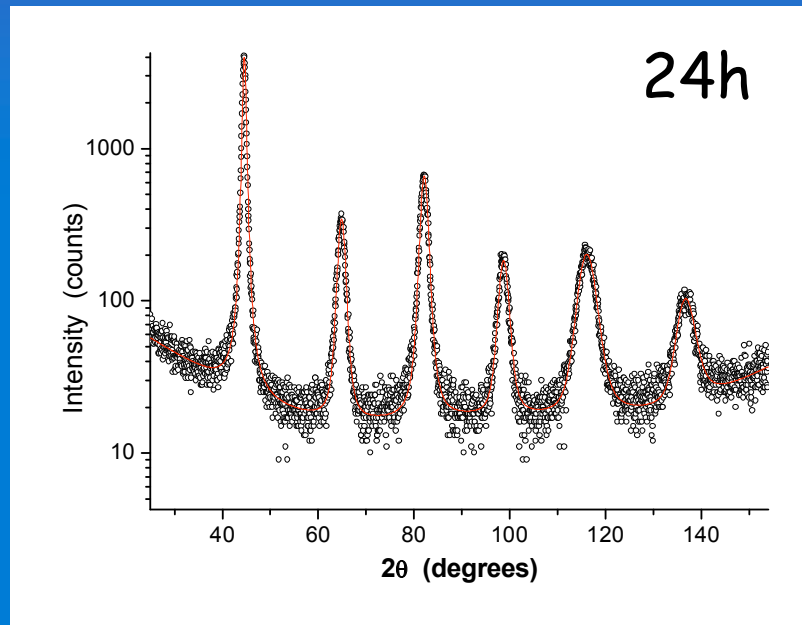




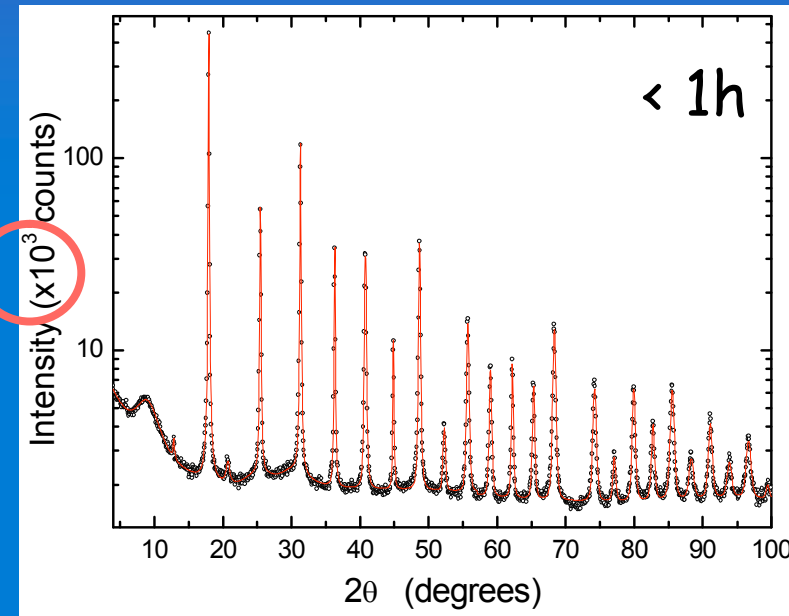
# SOME ADVANTAGES OF SRXRD

- 1) High brilliance, much better counting statistics / shorter data collection time (→ fast kinetics, in situ studies)

Ball milled FeMo



CuK $\alpha$   $\lambda=0.15406$  nm

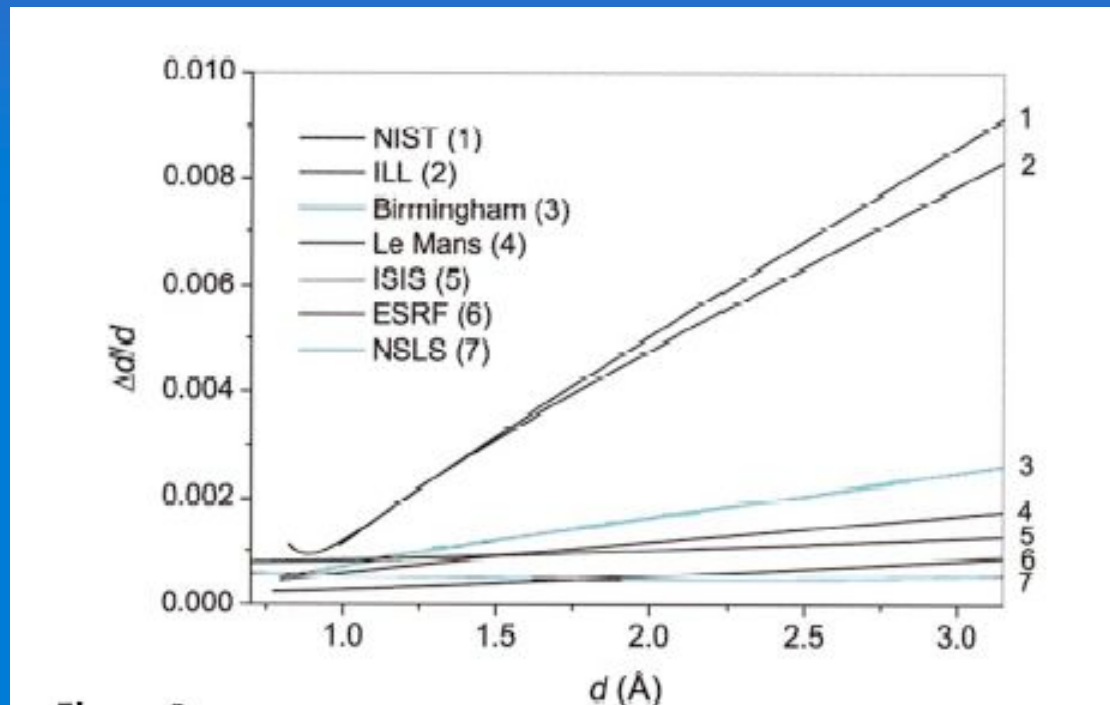


ESRF ID31  $\lambda=0.0632$  nm



## SOME ADVANTAGES OF SRXRD

2) With proper selection of optics, very narrow instrumental profile: increased resolution and accuracy in the measurement of peak position, intensity and profile width/shape.



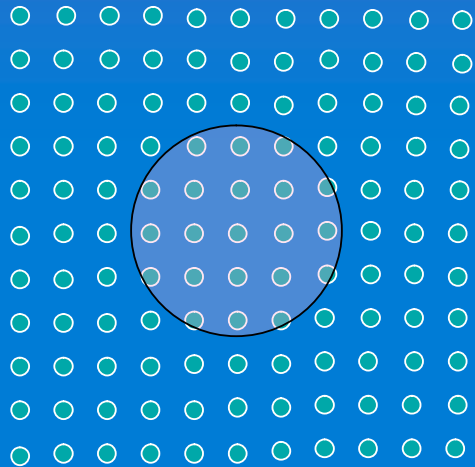
Lab instrument:  
FWHM  $\approx 0.05-0.1^\circ$

ID31 @ESRF:  
FWHM  $\approx 0.003-0.004^\circ$

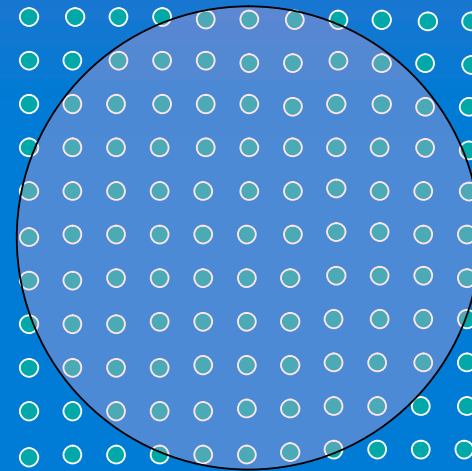


## SOME ADVANTAGES OF SRXRD

3) Extending the accessible region of reciprocal space well beyond what traditional lab instruments can make



$$\lambda_1$$



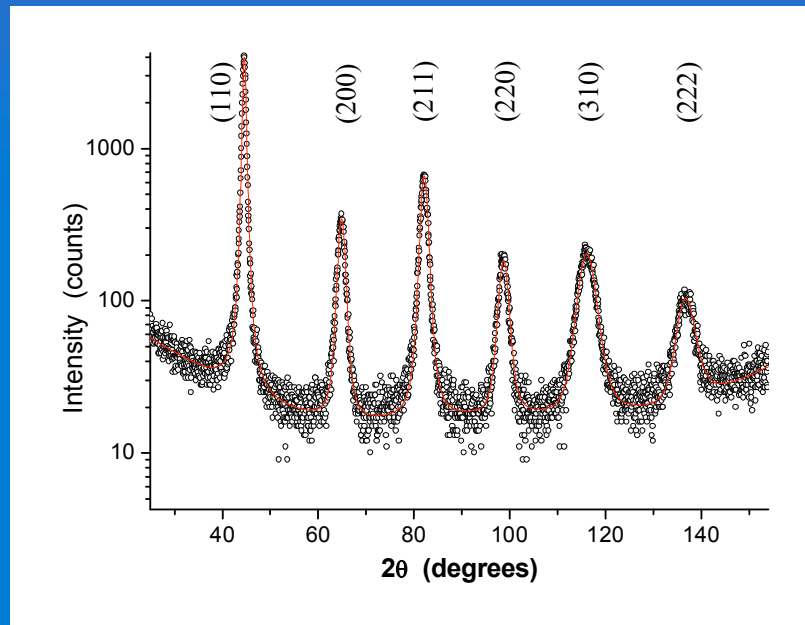
$$\lambda_2 < \lambda_1$$



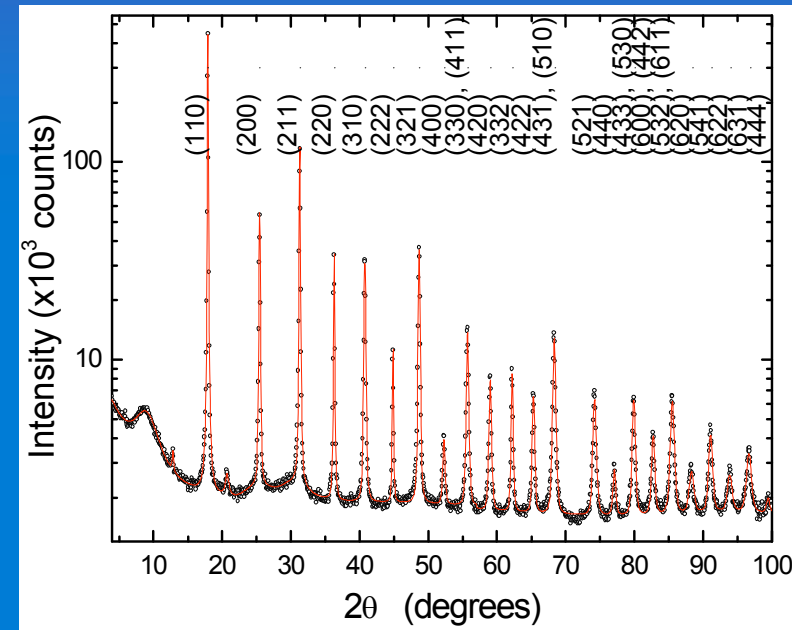
# SOME ADVANTAGES OF SRXRD

3) Extending the accessible region of reciprocal space well beyond what traditional lab instruments can make

Ball mill FeMo



CuK $\alpha$   $\lambda=0.15406$  nm



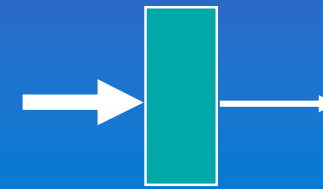
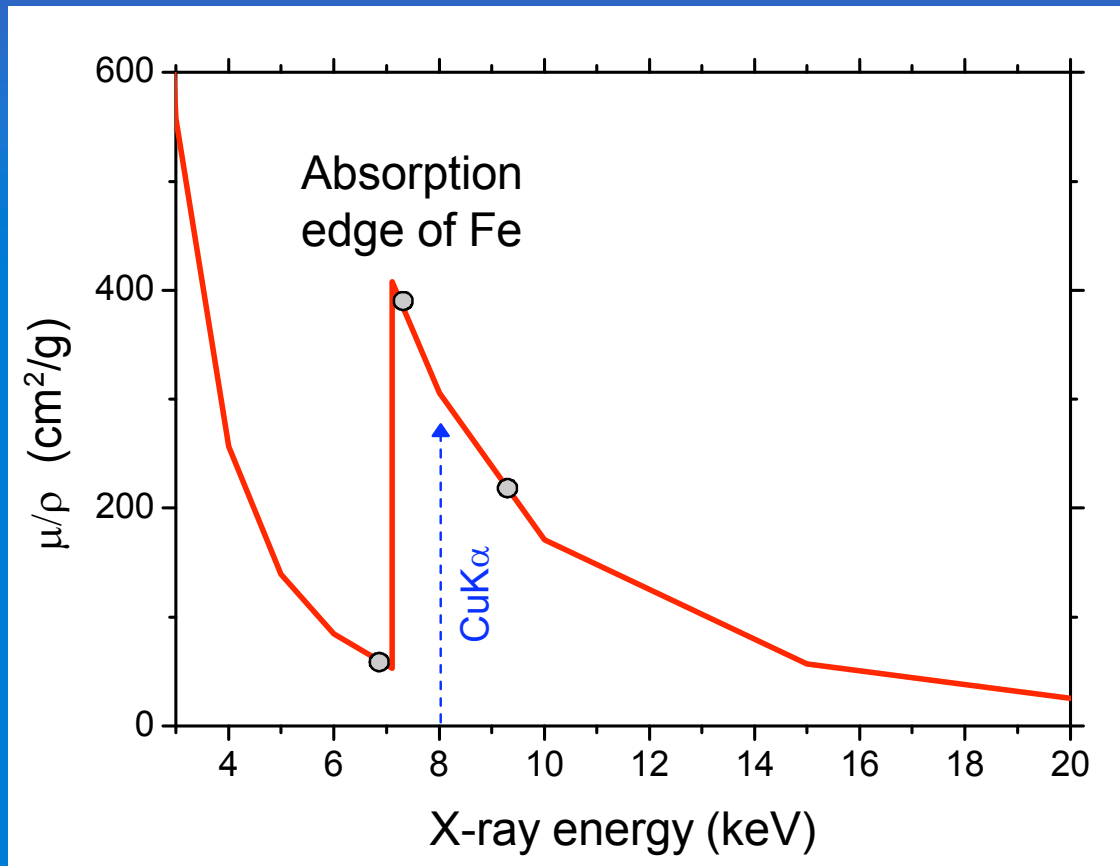
ESRF ID31  $\lambda=0.0632$  nm

M. d'Incau, Leoni & P. Scardi, *J. Materials Research* 22 (2007) 1744-1753.



## SOME ADVANTAGES OF SRXRD

4) Tuning the energy according to adsorption edges. Resonant scattering, control of fluorescence emission and depth of analysis.



$$I = I_0 e^{-\left(\frac{\mu}{\rho}\right)\rho t}$$



# X-RAY POWDER DIFFRACTION

## Most frequent applications of powder diffraction

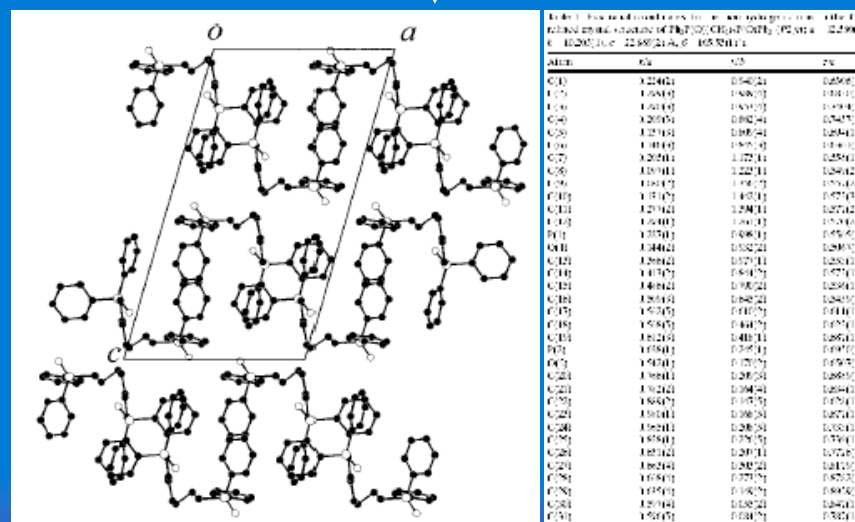
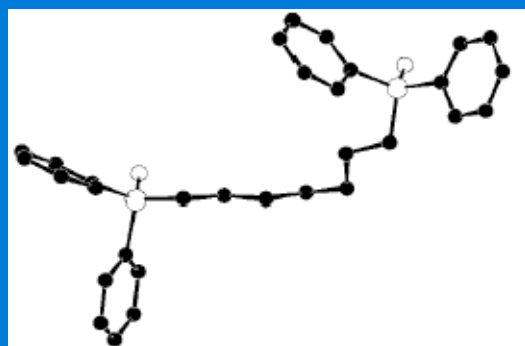
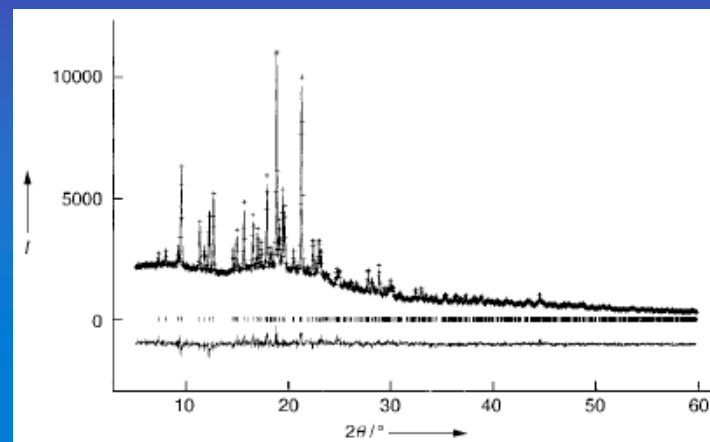
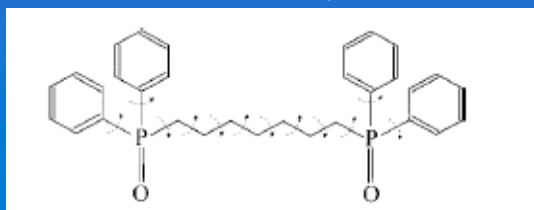
- Crystal structure determination  
(Powder diffraction structure solution and refinement)
- Phase Identification - pure crystalline phases or mixtures  
(Search-Match procedures)
- Quantitative Phase Analysis (QPA)
- Amorphous phase analysis (radial distribution function)
- Crystalline domain size/shape and lattice defect analysis  
(Line Profile Analysis - LPA)
- Determination of preferred orientations (Texture Analysis)
- Determination of residual stress field (Residual Stress Analysis)



# STRUCTURE SOLUTION: WHY POWDER?

Structure solution of heptamethylene-1,7-bis(diphenylphosphane oxide)

Structural formula  
 $\text{Ph}_2\text{P}(\text{O})(\text{CH}_2)_7\text{P}(\text{O})\text{Ph}_2$



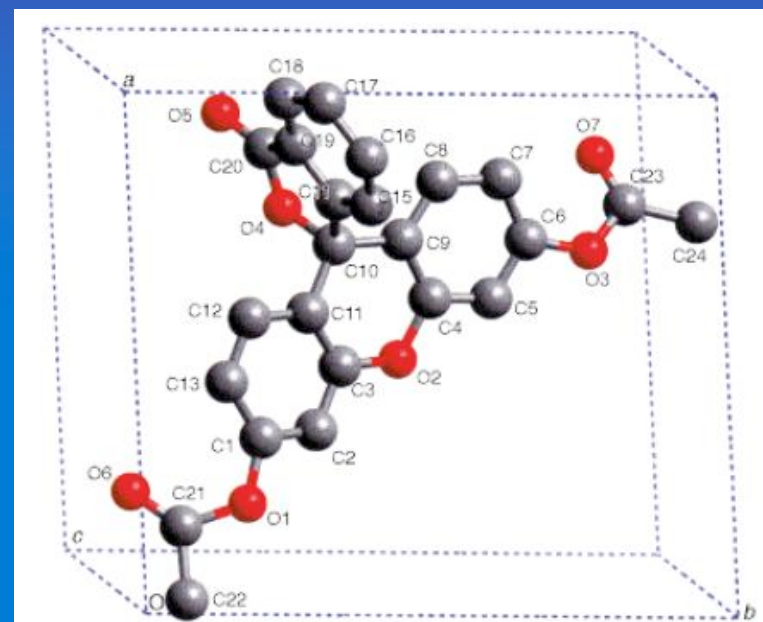
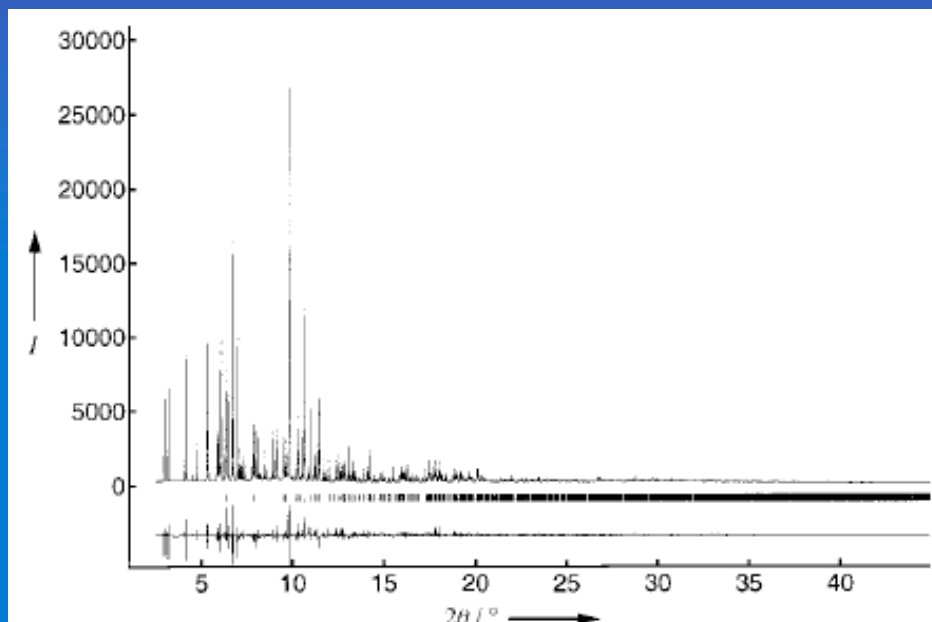
B.M. Kariuki, P. Calcagno, K. D. M. Harris, D. Philp and R.L. Johnston, *Angew. Chem. Int. Ed.* 1999, 38, No. 6, 831-835.



# STRUCTURE SOLUTION & REFINEMENT: SRXRD

Structure solution/refinement of a complex triclinic organic compound ( $C_{24}H_{16}O_7$ )

K. D. Knudsen *et al.*, *Angew. Chem. Int. Ed.*, 37 (1998) 2340



- Narrow peak profiles
- Large number of measurable peaks
- Accurate peak position/intensity
- X-ray energy tuning to adsorption edges

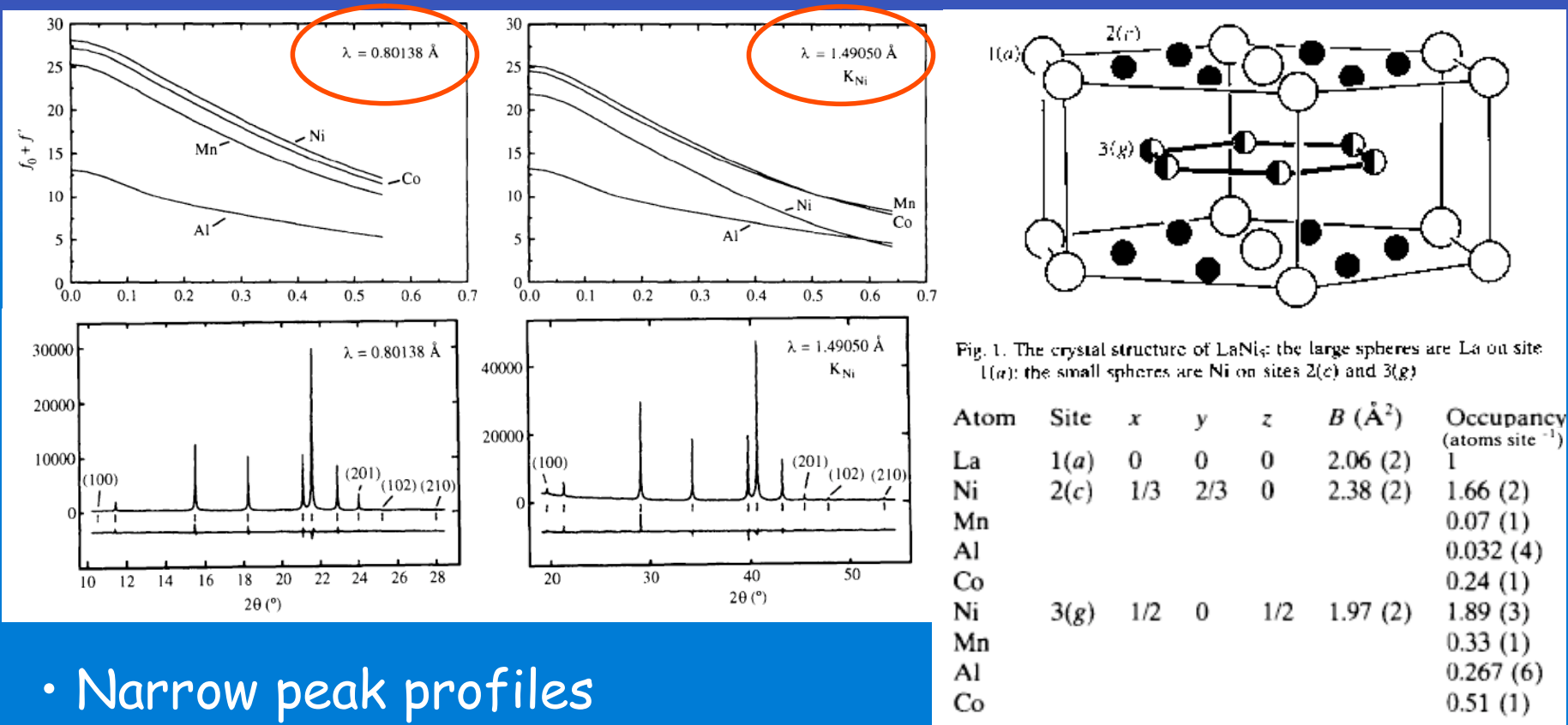




# STRUCTURE SOLUTION & REFINEMENT: SRXRD

Site occupancy in battery electrode material  $\text{LaNi}_{3.55}\text{Mn}_{0.4}\text{Al}_{0.3}\text{Co}_{0.75}$

J.-M. Joubert *et al.*, *J. Appl. Cryst.* 31 (1998) 327

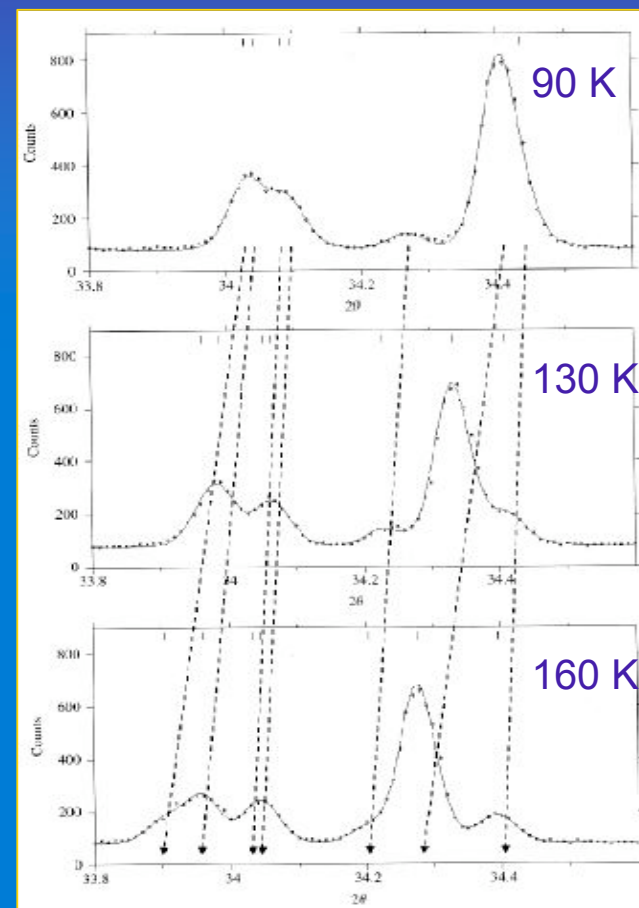
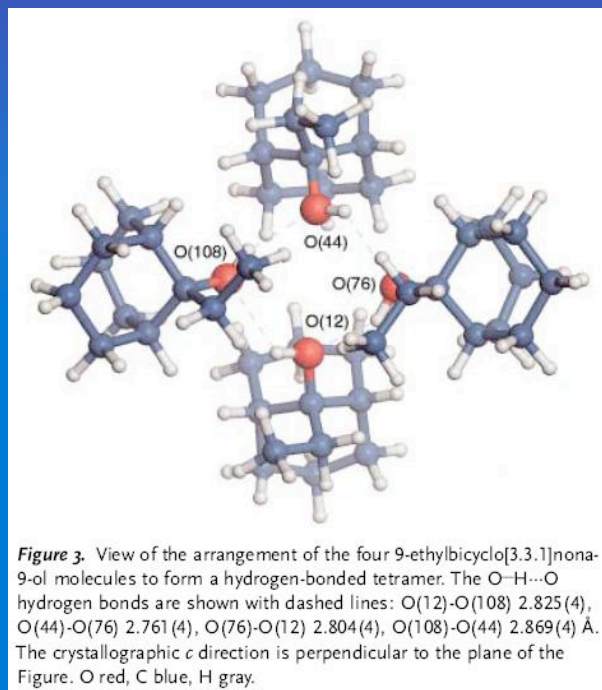


- Narrow peak profiles
- Large number of measurable peaks
- Accurate peak position/intensity
- X-ray energy tuning to adsorption edges



# STRUCTURE SOLUTION & REFINEMENT: SRXRD

Solving Larger Molecular Crystal Structures from Powder Diffraction Data by Exploiting Anisotropic Thermal Expansion, M. Brunelli et al., *Angew. Chem. Int. Ed.* 42, 2029, (2003)



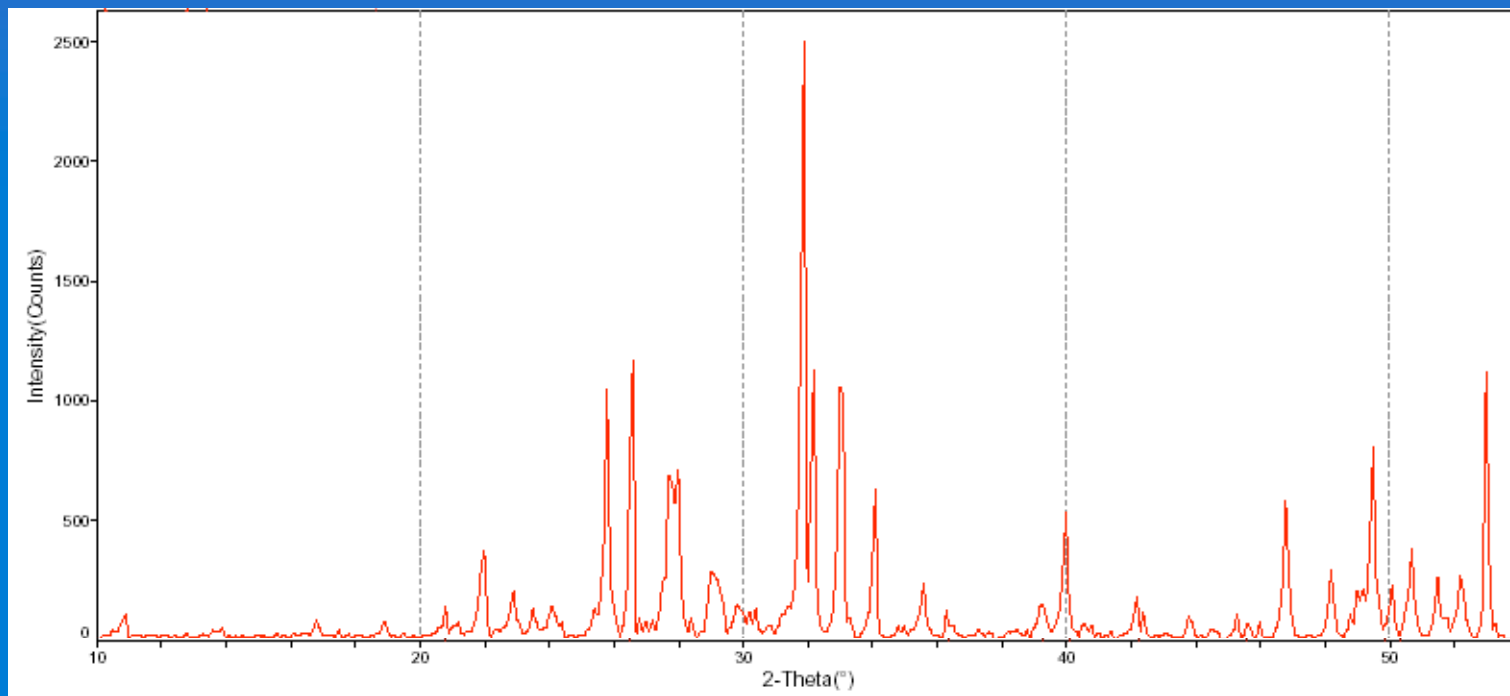
- Narrow peak profiles
- Large number of measurable peaks
- Accurate peak position/intensity
- X-ray energy tuning to adsorption edges
- Anisotropic thermal expansion



# PHASE IDENTIFICATION

Phase identification is one of the first and most diffuse applications of powder diffraction, especially in industry for production, quality control and diagnostics, but also in research.

Each crystalline phase has its own pattern that can be used as a 'fingerprint'



'Fingerprints' of unknown substances can be compared with those of known crystalline phases of a database → *Search-Match procedures*



# PHASE IDENTIFICATION

The most powerful database is the PDF (Powder Diffraction File) by the ICDD (International Centre for Diffraction Data - [www.icdd.com](http://www.icdd.com))



PDF-2  
Peak pos/int



PDF-4  
full structural information

ICDD DDView+ - PDF-4+ 2006 RDB

File Edit Tools Window Help

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PDF Card - 04-001-2097

File Edit d-Spacings Tools Help

2D 3D

d-Spacings

Wavelength: Cu Kα1 1.54056Å

Intensity

Fixed Slit

Variable Slit

Integrated

2θ	d(Å)	I	h	k	l
28.5491	<b>3.124</b>	999	1	1	1
33.0829	2.7055	270	2	0	0
47.4886	<b>1.913</b>	450	2	2	0
56.3453	<b>1.6315</b>	327	3	1	1
59.094	1.562	59	2	2	2
69.4222	1.3527	52	4	0	0
76.7043	1.2414	103	3	3	1
79.0846	1.2099	64	4	2	0
88.4378	1.1045	85	4	2	2
95.4167	1.0413	68	5	1	1
107.2806	0.9565	25	4	4	0
114.7472	0.9146	69	5	3	1
117.3338	0.9018	31	6	0	0

Intensity

2θ

— 04-001-2097 (Fixed Slit Intensity)

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PDF | Experimental | Physical | Crystal | Optical | Structure | Miscellaneous | Comments

Atomic Coordinates (2)

TF Type: B

Atom	Num	Wyckoff	Symmetry	x	y	z	SOF	ITF	AET
Ce	1	4a	m-3m	0.0	0.0	0.0	1.0	0.7	8-a
O	2	8c	-43m	0.25	0.25	0.25	1.0	1	10-a

Origin:

SG Symmetry Operators (48)

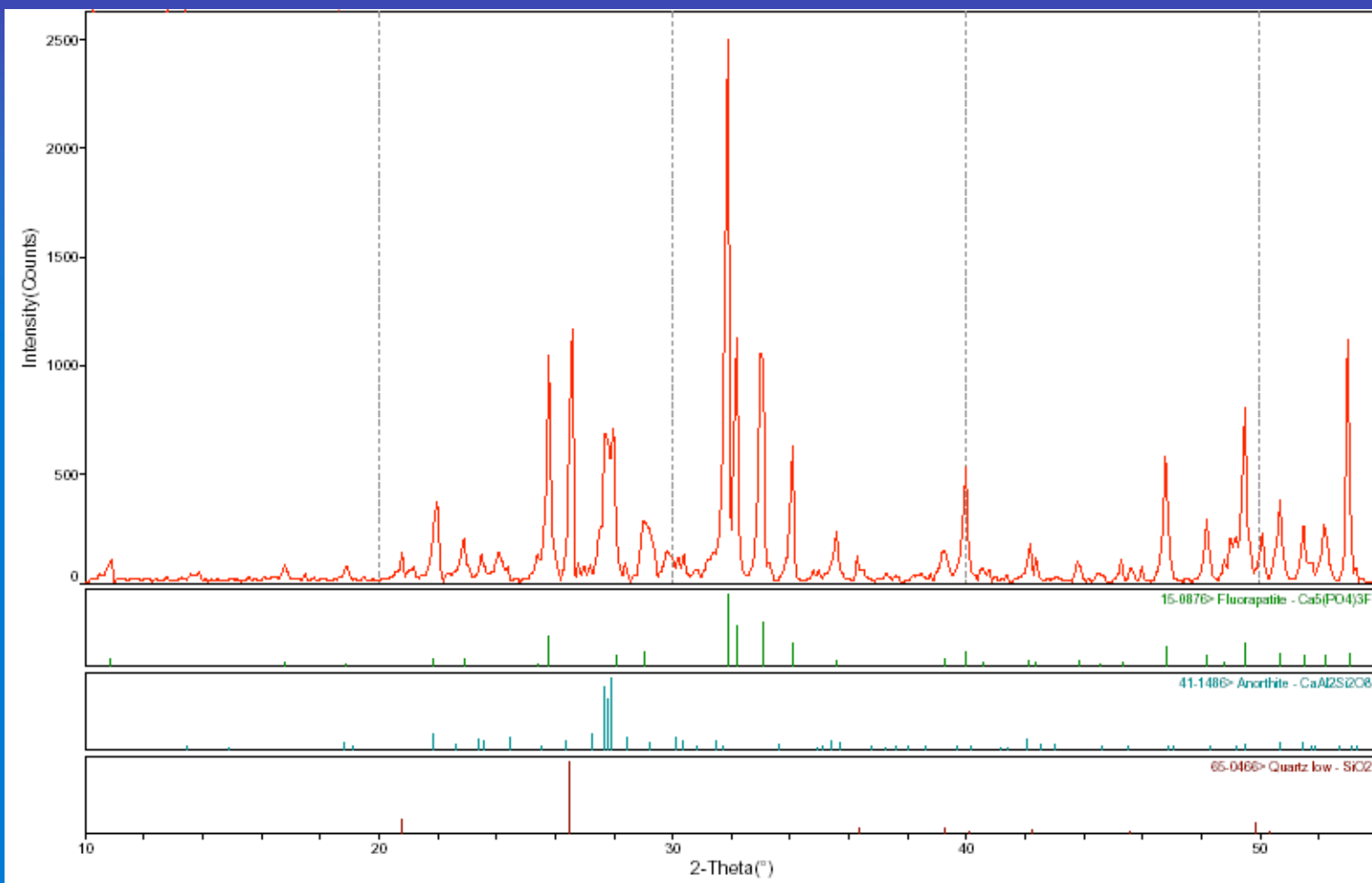
Seq	Operator
1	x,y,z
2	-x,-y,-z
3	z,x,y

Anisotropic Temperature Factors (0)

Search Results - Database (LPF ...) PDF Card - 04-001-2097



# PHASE IDENTIFICATION

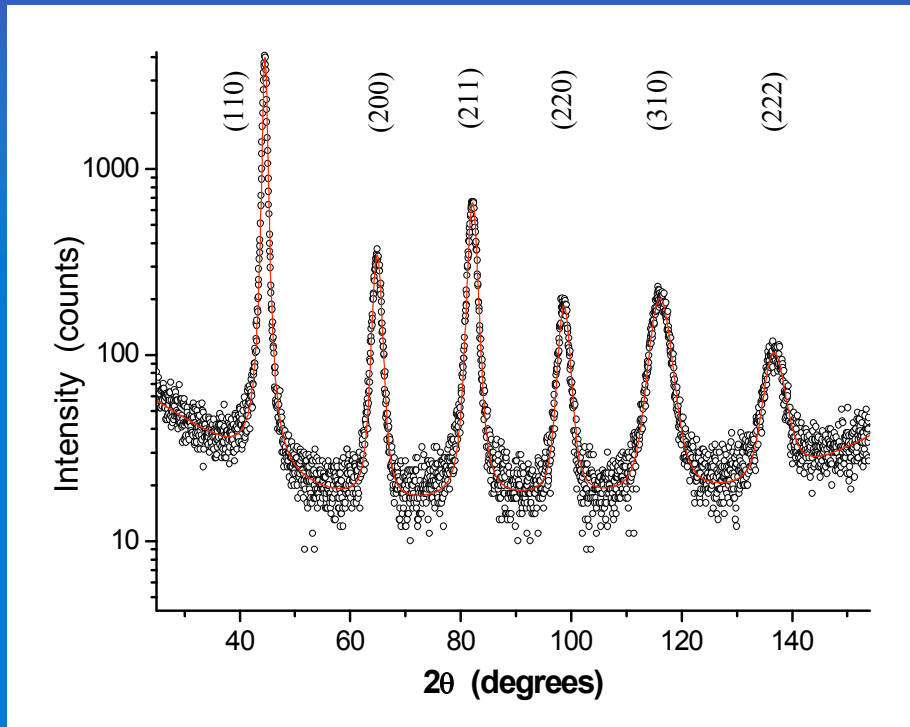


Automatic search-match procedures are based on peak position / intensity

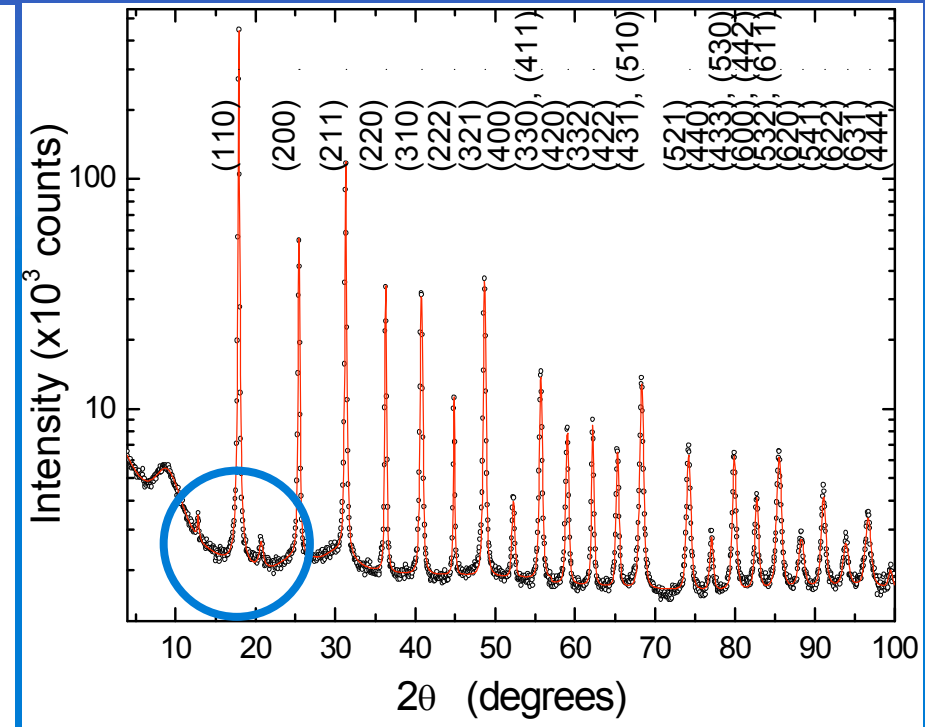


# MINOR PHASE IDENTIFICATION BY SRXRD

## Iron oxide traces in ball milled $\alpha$ -Fe powder



CuK $\alpha$   $\lambda=0.15406$  nm



ESRF ID31  $\lambda=0.0632$  nm

M. d'Incau, Leoni & P. Scardi, *J. Materials Research* 22 (2007) 1744-1753.



## QUANTITATIVE PHASE ANALYSIS (QPA)

The pattern of a phase mixture is the **WEIGHTED** sum of the patterns corresponding to the constituent phases. The weight depends of the specific scattering power and absorption of each phase in the mixture.

Several techniques exists for a quantitative determination of the phase content:

- **QPA with internal standard**
- **QPA with "virtual standard" (RIR method)**
- **QPA via the Rietveld method (virtual standard)**



# THE RIETVELD METHOD

Intensity of the i-th point in the pattern

$$y_{ci} = \sum_j S_j \sum_k I_{k,j} \cdot \phi_{k,j}(2\theta) \cdot P_{k,j} + y_{bi}$$

Scale factor  
of j-th phase

Integrated Intensity  
k-th peak of j-th phase

Profile function

Preferred  
Orientation

Background term

Using the normalization condition:  $\sum_k x_k = 1$  (not obvious !!)

it is possible to calculate the weight fraction  $x_j$  of the phase j in a polyphasic mixture as:

$$x_j = \frac{S_j \rho_j v_j}{\sum_l S_l \rho_l v_l}$$

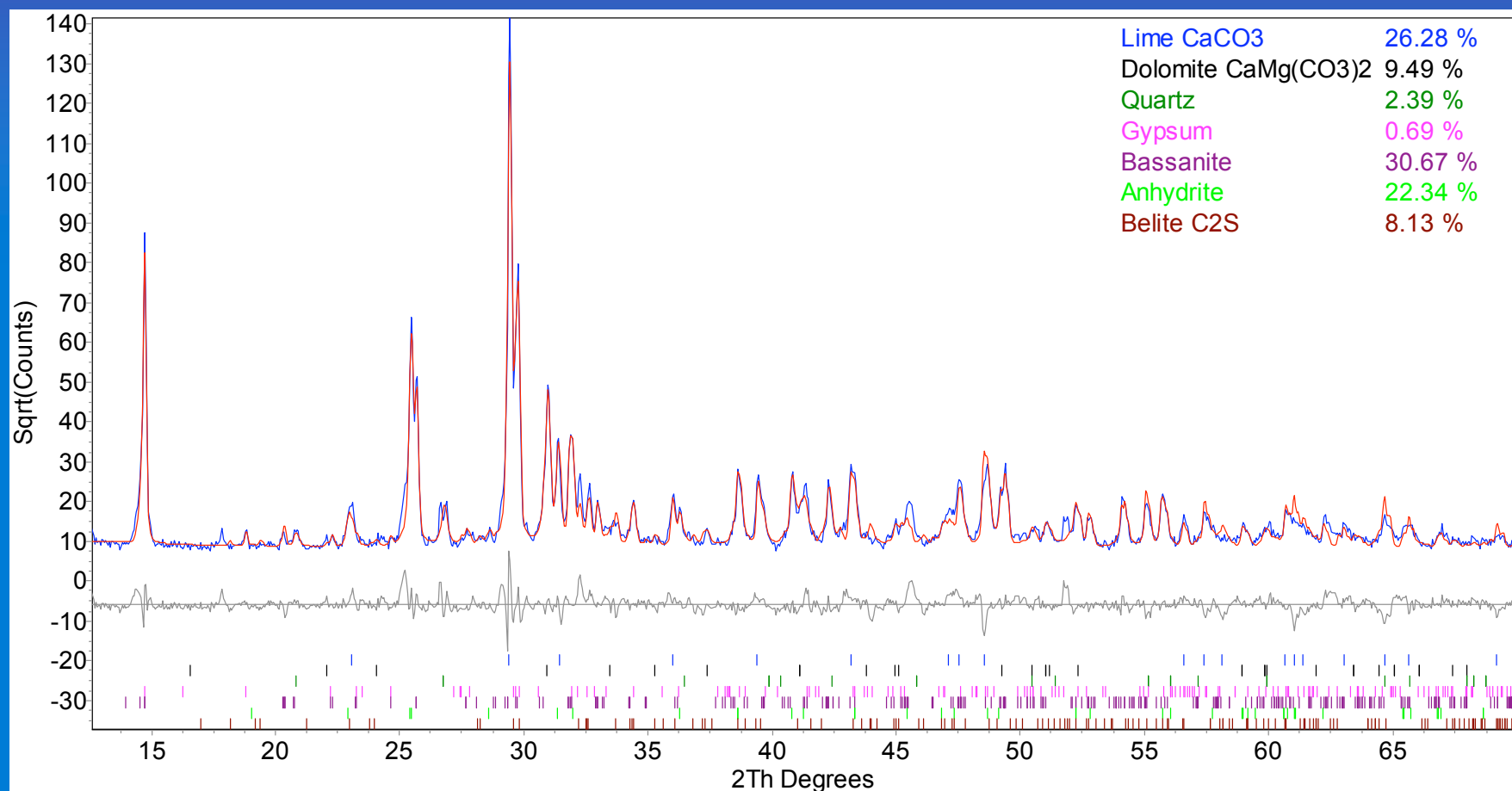
→ J. Plasier





# RIETVELD-BASED QPA

Example: mixture of mineral phases in a ligand





# STRUCTURE SOLUTION IN MULTIPHASE SAMPLES

Structural and electronic properties of noncubic fullerenes  $A'_{40}C_{60}$  ( $A'=Ba,Sr$ )

*C.M. Brown et al., Phys. Rev. Let. 83 (1999) 2258*

ESRF BM161  $\lambda=0.084884$  nm

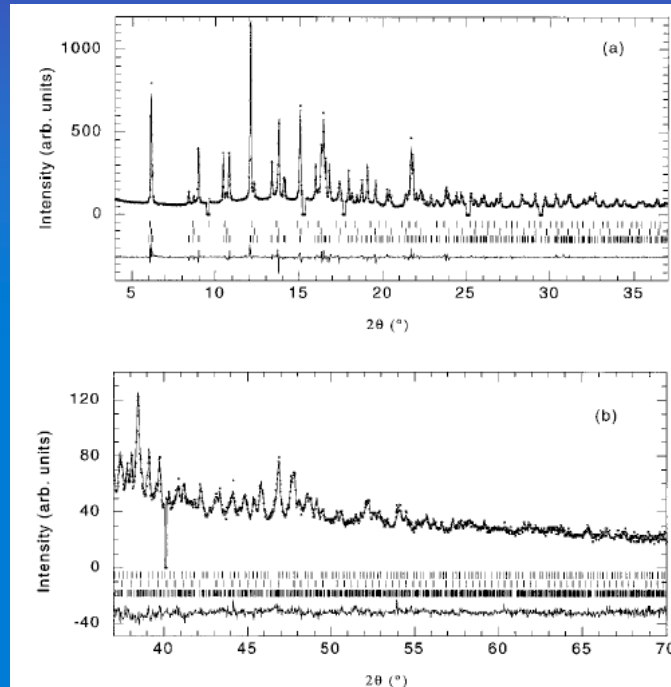


FIG. 2. Final observed (points) and calculated (solid line) synchrotron x-ray powder diffraction profiles for  $Ba_4C_{60}$  at 295 K in the range  $4^\circ$  to  $70^\circ$  ( $\lambda = 0.84884 \text{ \AA}$ ). The lower panels show the difference profiles and the ticks mark the positions of the Bragg reflections of  $Ba_4C_{60}$  [majority phase: 86.1(2)%, lower most],  $Ba_5C_{60}$  [minority phase: 11.8(1)%, middle], and  $Ba_3C_{60}$  [minority phase: 2.1(1)% upper most]. Some sharp peaks originating from a nonfulleride phase were excluded from the refinement.

- Narrow peak profiles
- Large number of measurable peaks
- Accurate peak position/intensity
- X-ray energy tuning to adsorption edges



# STRUCTURE SOLUTION IN MULTIPHASE SAMPLES

Structural and electronic properties of noncubic fullerides  $A'_{40}C_{60}$  ( $A'=\text{Ba},\text{Sr}$ )

*C.M. Brown et al., Phys. Rev. Let. 83 (1999) 2258*

TABLE I. Refined parameters for orthorhombic  $\text{Ba}_4\text{C}_{60}$  obtained from Rietveld refinement of the synchrotron x-ray powder diffraction data at 295 K (space group  $Immm$ ,  $R_{wp} = 5.3\%$ ,  $R_{exp} = 2.6\%$ ). The cell constants are  $a = 11.6101(2)$ ,  $b = 11.2349(2)$ , and  $c = 10.8830(2)$  Å, and the weight fraction of the  $\text{Ba}_4\text{C}_{60}$  phase is 86.1(2)%. The weight fractions of the minority phases,  $\text{Ba}_6\text{C}_{60}$  and  $\text{Ba}_3\text{C}_{60}$  are 11.8(1)% and 2.1(1)%, respectively. The cell constants of cubic  $\text{Ba}_6\text{C}_{60}$  (space group  $Im\bar{3}$ ) and  $\text{Ba}_3\text{C}_{60}$  (space group  $Pm\bar{3}n$ ) are 11.1959(2) and 11.338(1) Å, respectively.

Atom	$x/a$	$y/b$	$z/c$	$B_{iso}/\text{Å}^2$ ( $\beta_{11}, \beta_{22}, \beta_{33}$ )
Ba(1)	0.5	0.2034(2)	0.0	1.9(1), 2.9(2), 0.9(1)
Ba(2)	0.2488(1)	0.5	0.0	2.7(1), 3.7(2), 0.6(1)
C(11)	0.3005(2)	0.0	0.0652(1)	0.16(8)
C(12)	0.0	-0.063 88(4)	0.3206(2)	0.16(8)
C(13)	0.10014(6)	-0.127 86(7)	0.2798(2)	0.16(8)
C(21)	0.2003(1)	-0.63 88(4)	0.2389(1)	0.16(8)
C(22)	0.12373(7)	-0.271 0(2)	0.106 82(6)	0.16(8)
C(23)	0.06187(4)	-0.310 5(2)	0.0	0.16(8)
C(31)	0.2240(2)	-0.207 0(1)	0.066 00(3)	0.16(8)
C(32)	0.06187(4)	-0.231 4(1)	0.213 7(1)	0.16(8)
C(33)	0.2622(2)	-0.103 45(6)	0.131 99(8)	0.16(8)

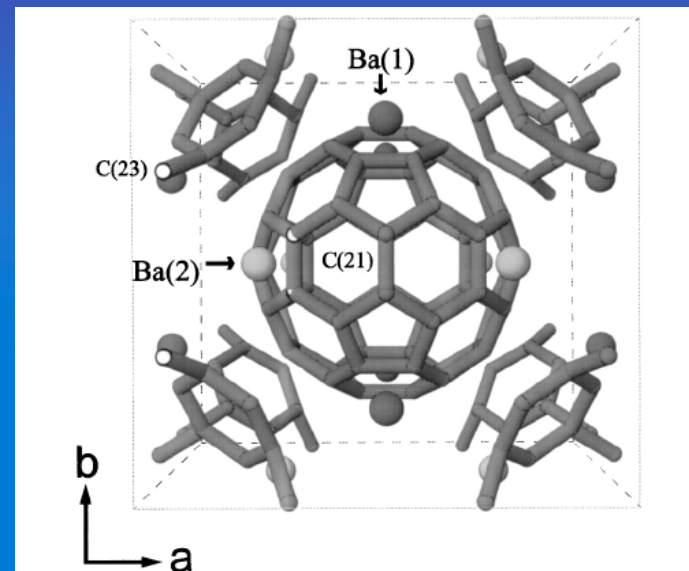


FIG. 3. Projection of the body centered orthorhombic structure of  $\text{Ba}_4\text{C}_{60}$  on the  $[110]$  basal plane. The two sets of crystallographically distinct barium ions, Ba(1) ( $m2m$  site) and Ba(2) ( $2mm$  site) are depicted as dark and light grey spheres, respectively. The hexagon C(21) and pentagon C(23) atoms which are in close contact to Ba(2) are depicted as white spheres.

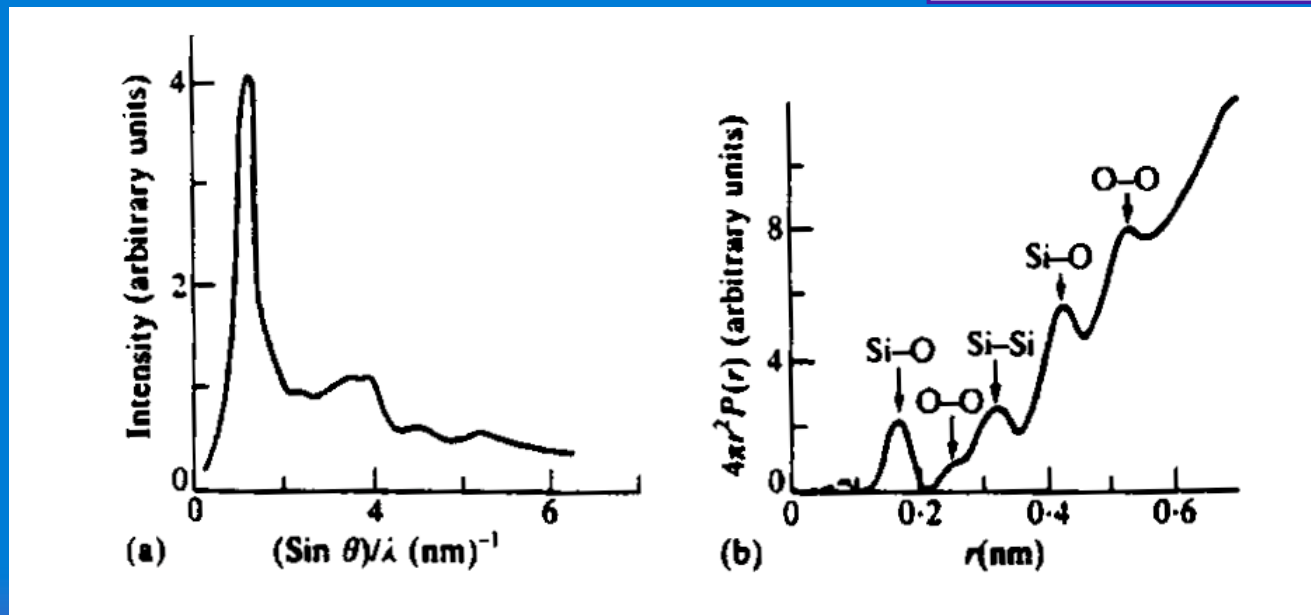
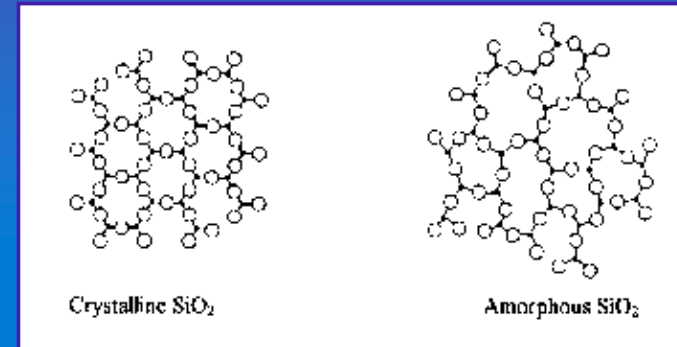
- Narrow peak profiles
- Large number of measurable peaks
- Accurate peak position/intensity
- X-ray energy tuning to adsorption edges



# AMORPHOUS PHASE ANALYSIS

The long-range order typical of crystalline structures is absent in amorphous materials. However, a certain degree of short-range order is always present.

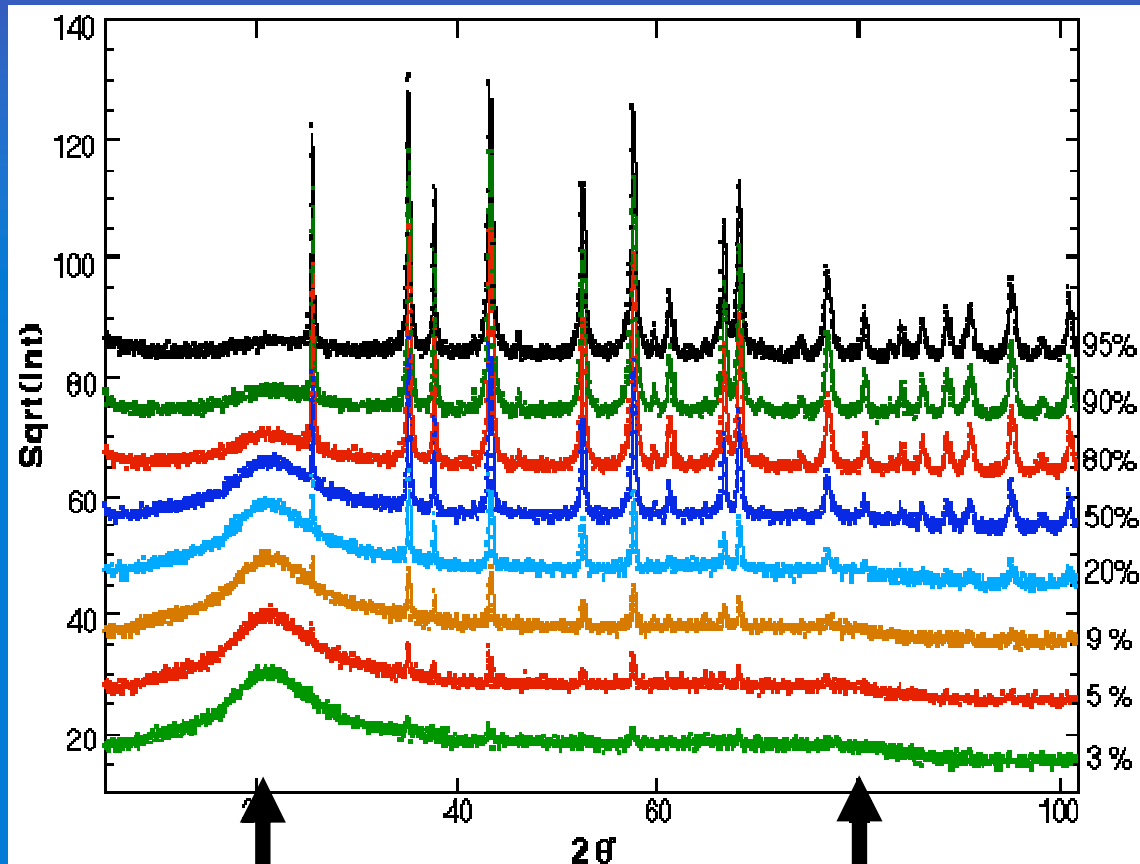
Diffraction can be used to measure the *radial distribution function*, i.e., the probability distribution to find an atom at a distance between  $r$  and  $r+\delta r$  taken from a reference atom.





# AMORPHOUS PHASE ANALYSIS

Mixture of (crystalline) corundum and amorphous silica



amorphous bands typical of the glass

Diffraction can provide:

- **fraction of amorphous phase** in mixtures
- **degree of crystallinity** (e.g. in glass-ceramics or in polymers)



# PAIR DISTRIBUTION FUNCTION: USE OF SRXRD

Structure of nanocrystalline materials using atomic Pair Distribution Function (PDF) analysis: study of  $\text{LiMoS}_2$ .

V. Petkov *et al.*, Phys. Rev. B 65 (2002) 092105

$$PDF : G(r) = 4\pi r [\rho(r) - \rho_0]$$

TABLE I. Structural parameters for  $\text{MoS}_2$ . Space group is  $P6_3/mmc$ . Mo is at  $(\frac{1}{3}, \frac{2}{3}, \frac{1}{4})$  and S at  $(\frac{1}{3}, \frac{2}{3}, z)$ .

	PDF	Rietveld	Single crystal <sup>a</sup>
$a$ (Å)	3.169(1)	3.168(1)	3.1604(2)
$c$ (Å)	12.324(1)	12.322(1)	12.295(2)
$z$	0.623(1)	0.625(1)	0.629(1)

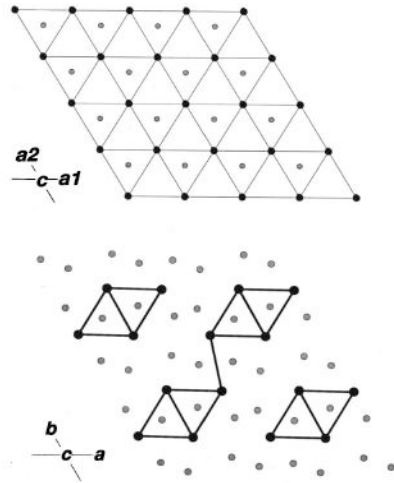


FIG. 4. Projection down the  $c$  axis of the crystal structures of hexagonal  $\text{MoS}_2$  (up) and triclinic  $\text{LiMoS}_2$  (down). The large black circles are Mo atoms and the small gray circles are the S atoms. Li atoms are not shown for the sake of clarity.

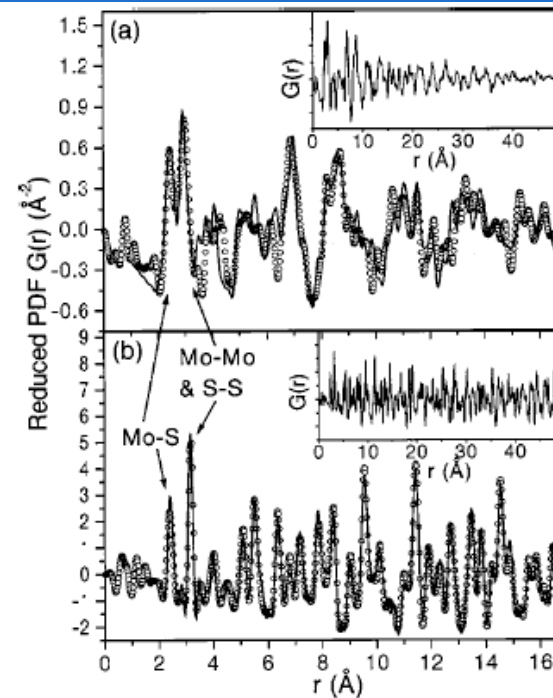
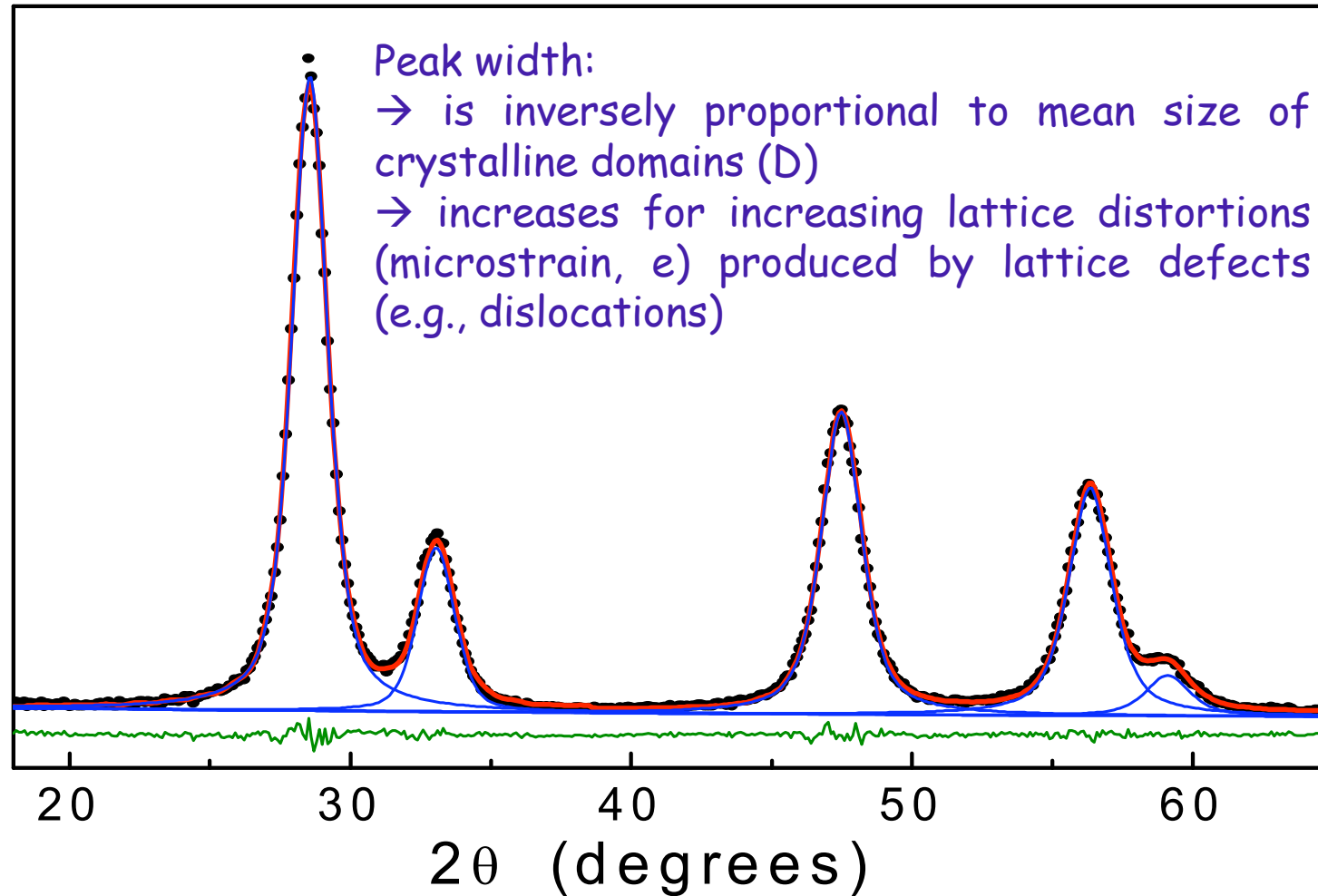


FIG. 2. Experimental (dots) and fitted (solid line) PDF's for  $\text{LiMoS}_2$  (a) and  $\text{MoS}_2$  (b). Note the different scale between (a) and (b). The first two peaks in the PDF's are labeled with the corresponding atomic pairs. The experimental data are shown in an expanded scale in the insets.



# LINE PROFILE ANALYSIS

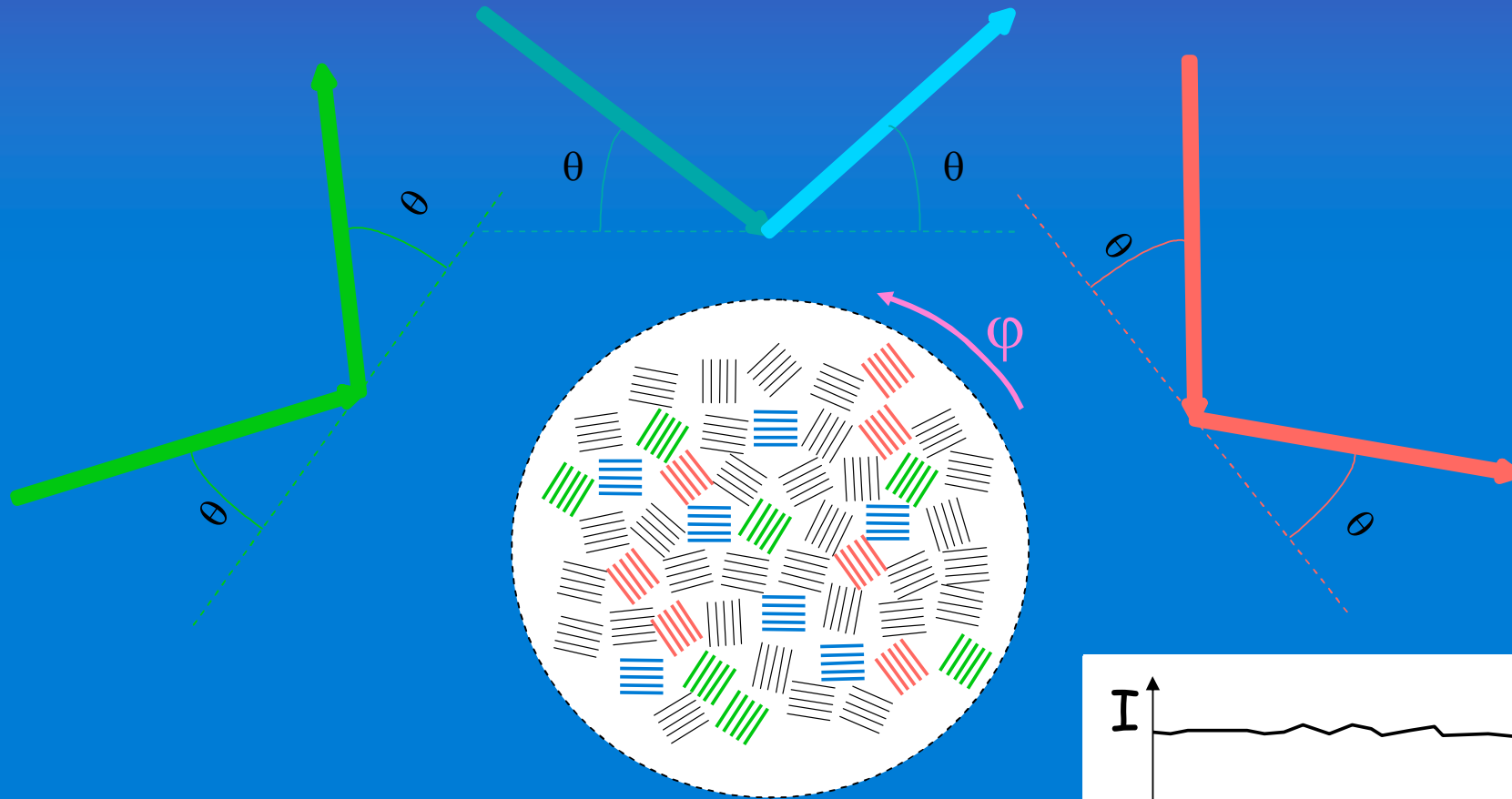


→ LPA: second part of this lecture



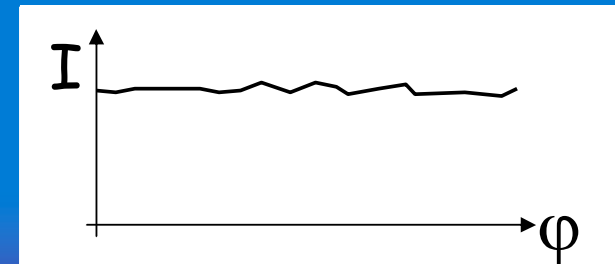
# TEXTURE ANALYSIS

A 'true' powder has randomly oriented crystalline domains.  
The diffracted intensity does not depend on the probing direction.



for any  $hkl$

random orientation

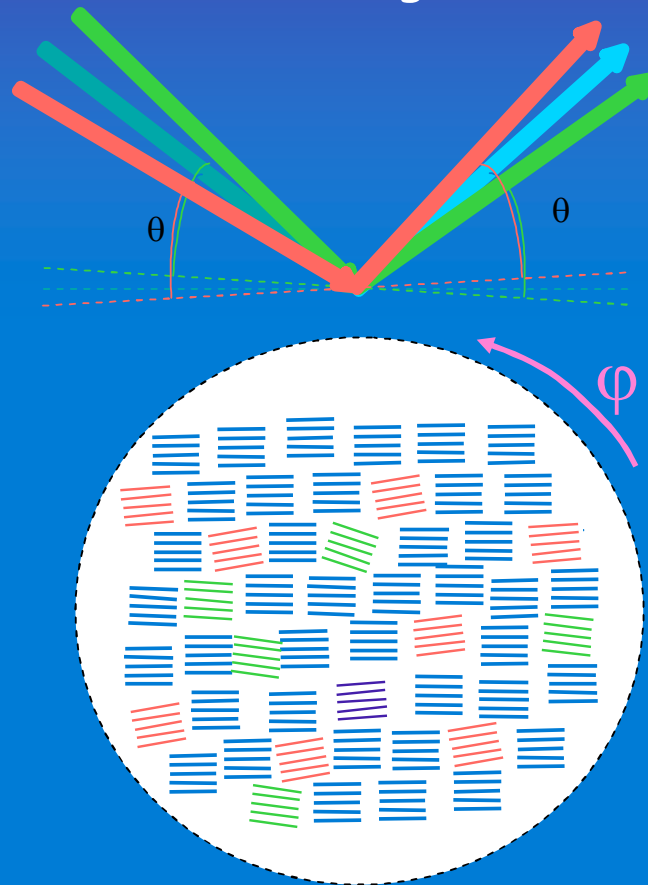




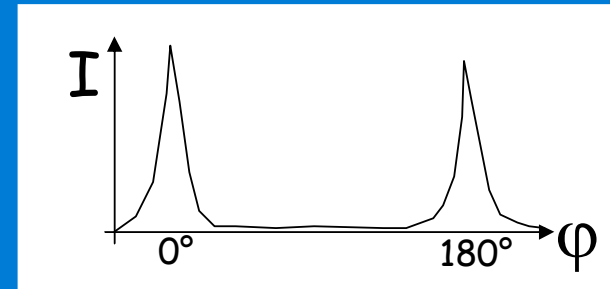


# TEXTURE ANALYSIS

If the grain (crystal) orientation is not random, the diffracted signal depends on the incident angle.



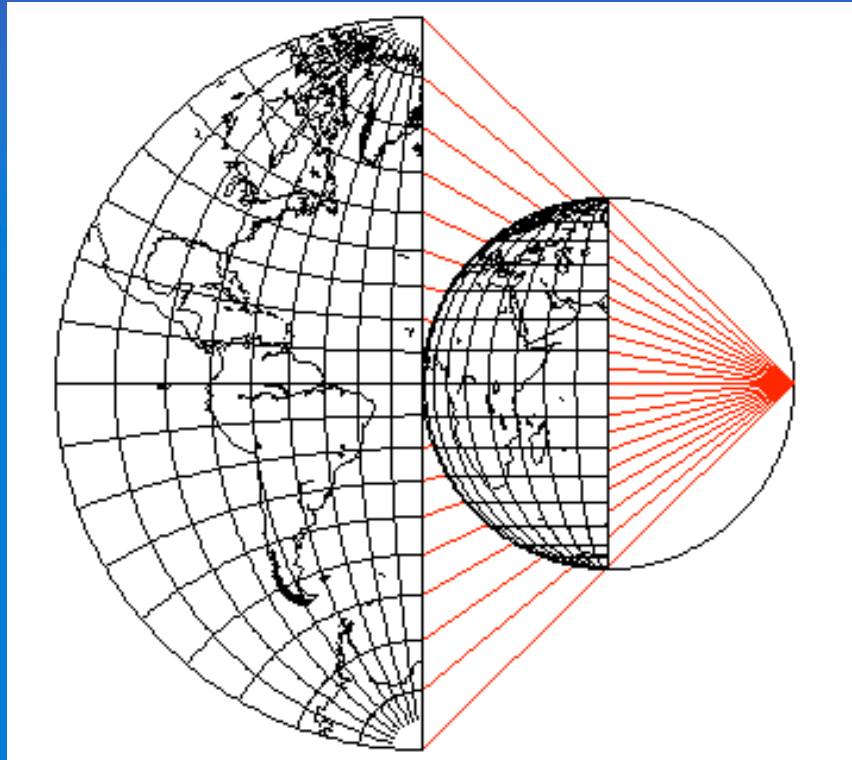
preferred orientation



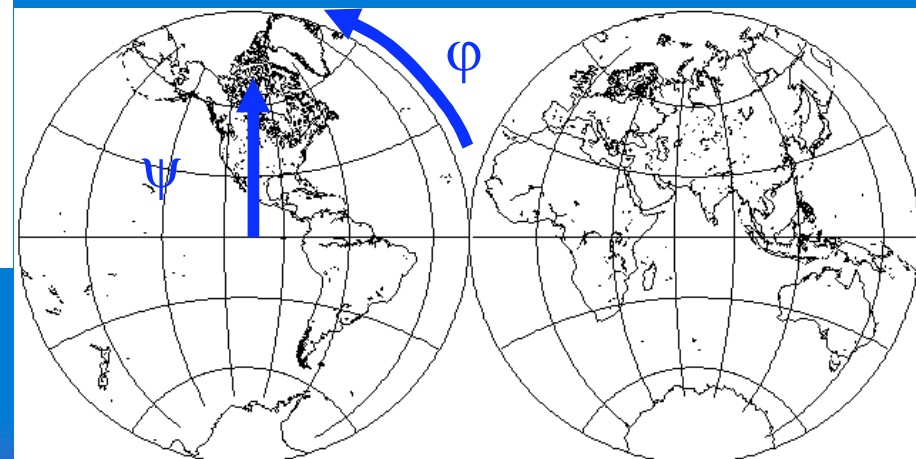


# TEXTURE ANALYSIS

The information can be reported on suitable maps: pole figures.  
The stereographic projection is adopted



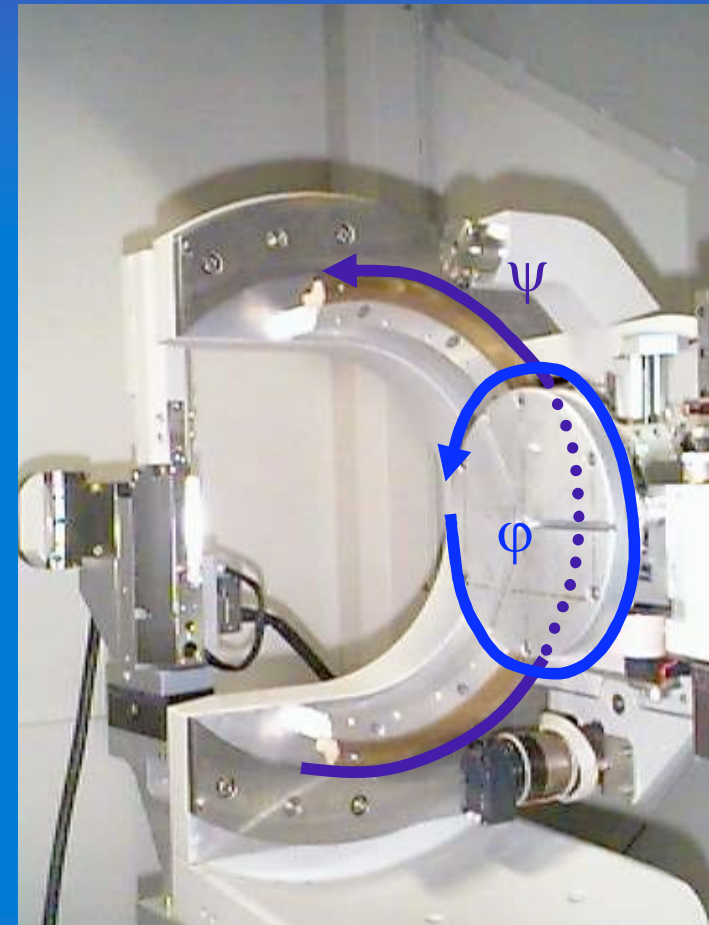
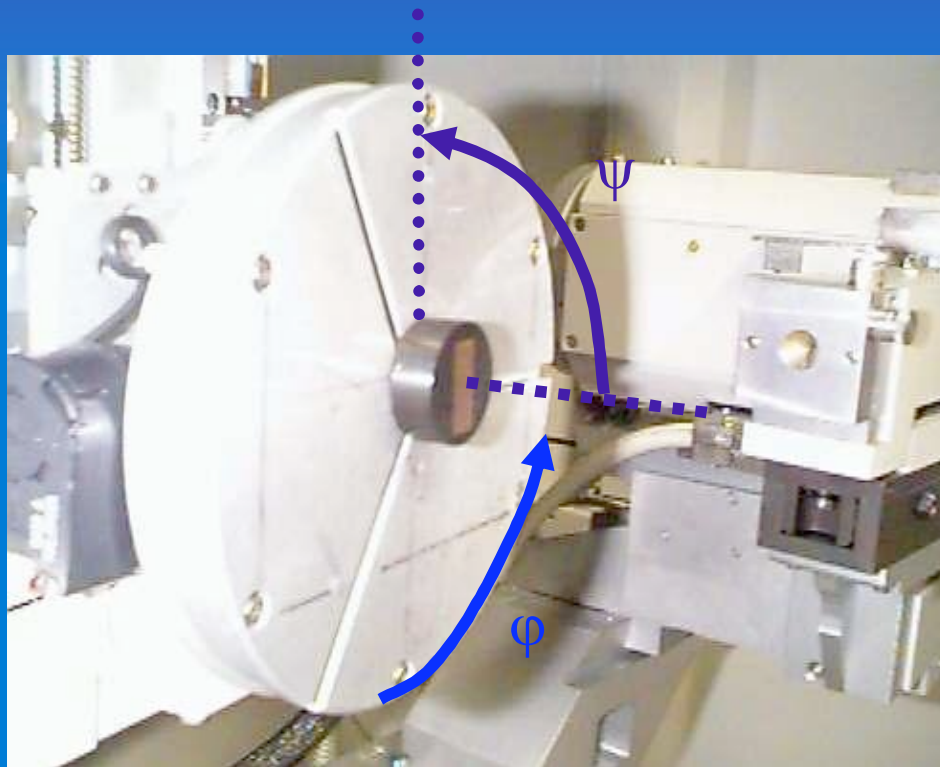
Two angles are used in the projection





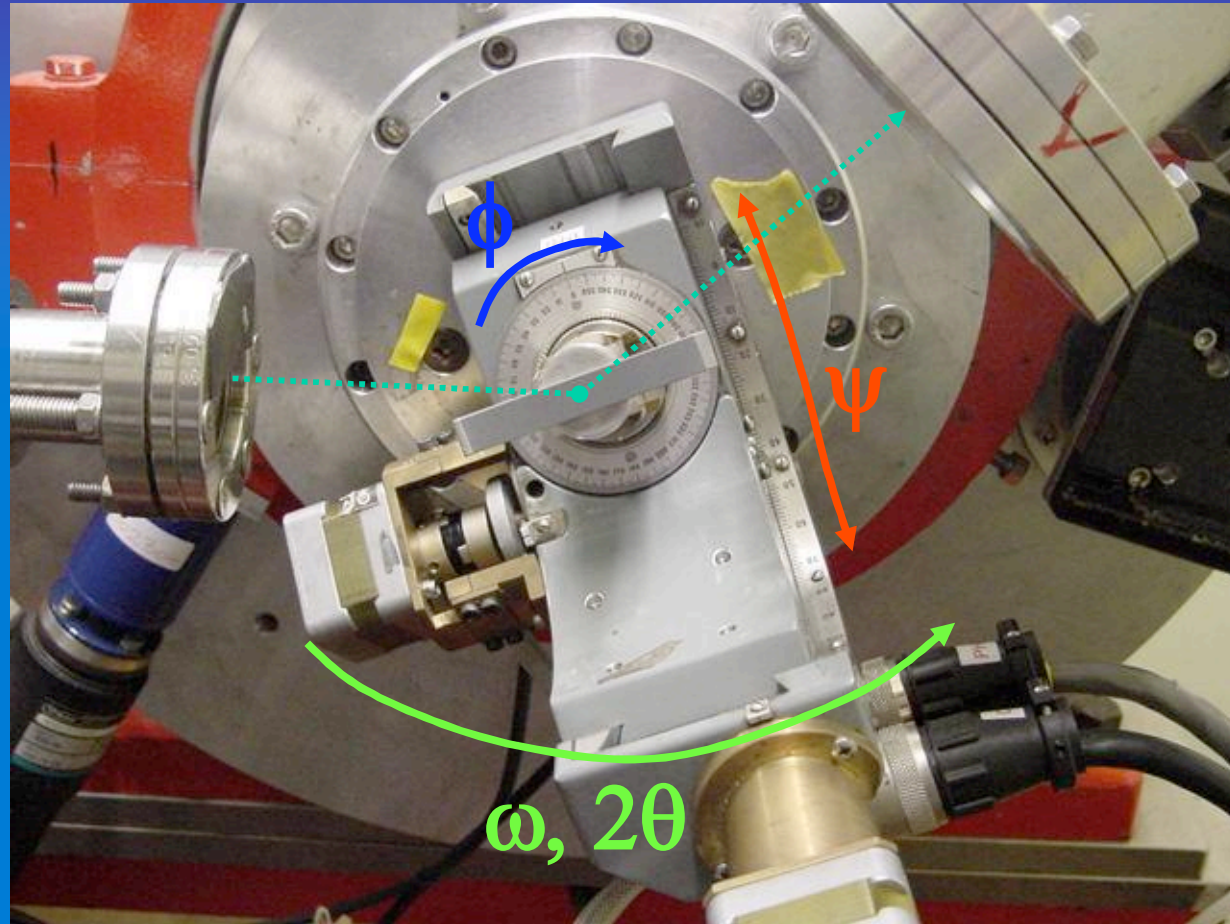
# TEXTURE ANALYSIS

Eulerian cradle for stress/texture measurement: laboratory instrum.





# TEXTURE & STRESS ANALYSIS BY SRXRD

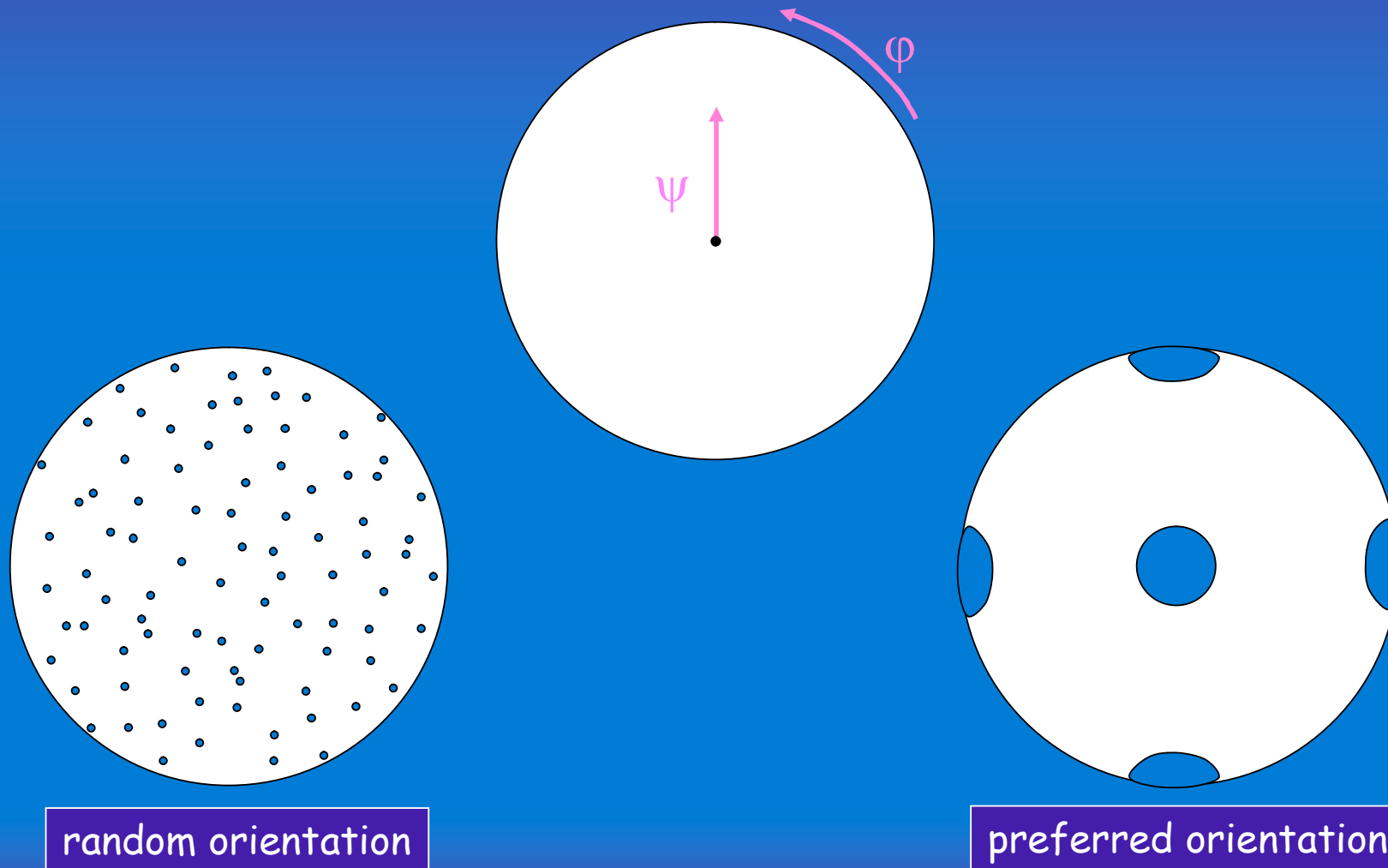


Eulerian cradle for stress/texture measurement: Daresbury beamline 2.3



# TEXTURE ANALYSIS

## Crystallographic texture: pole figures



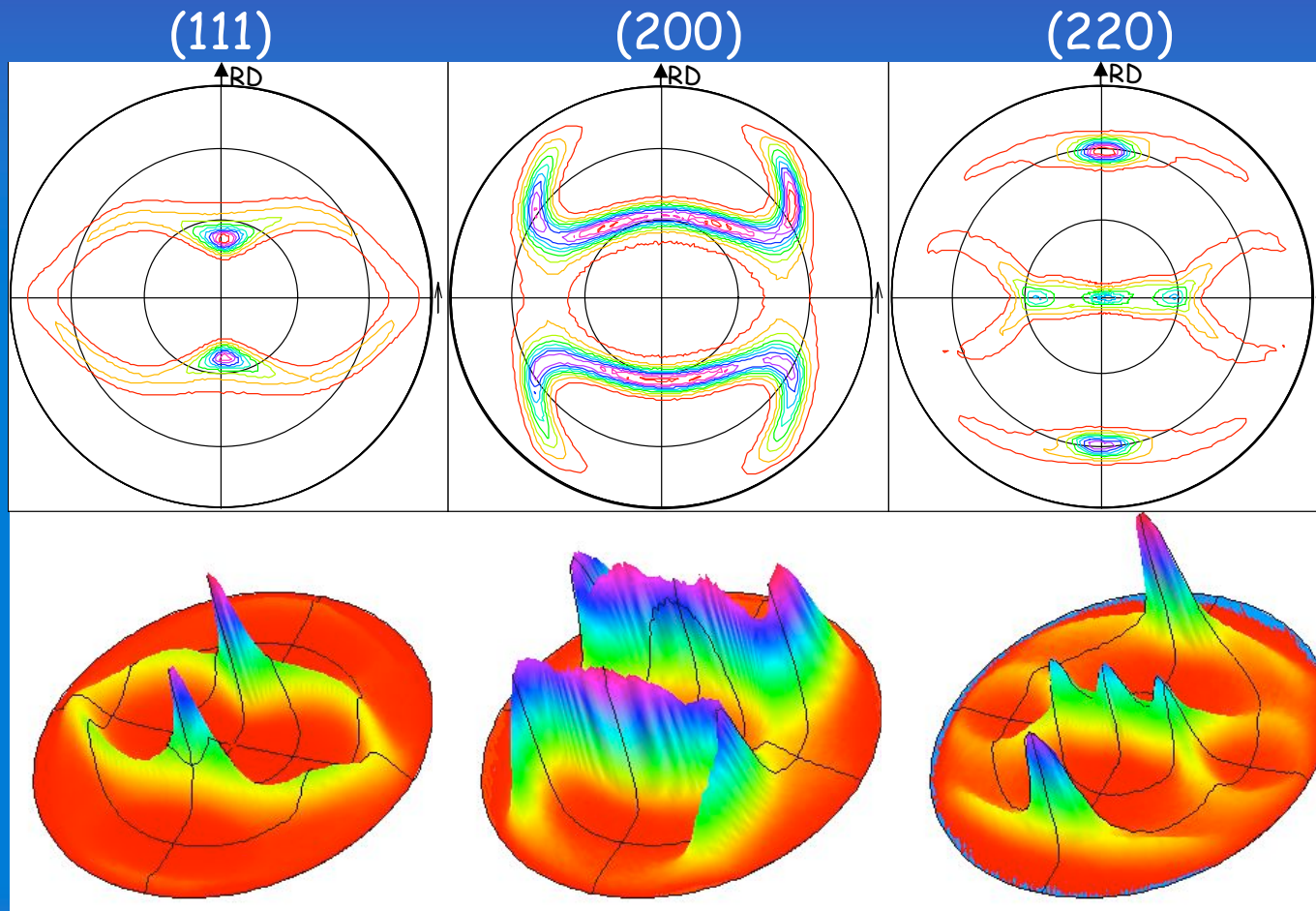
random orientation

preferred orientation



# TEXTURE ANALYSIS

In general, texture can be quite complex. Several pole figures, for different (hkl), may be required to understand the orientation



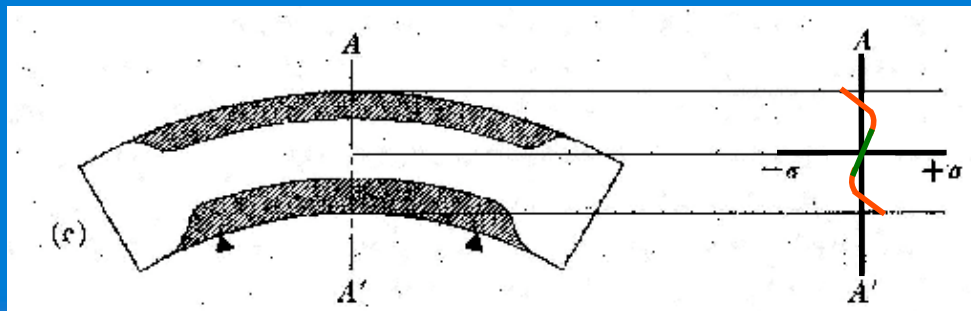
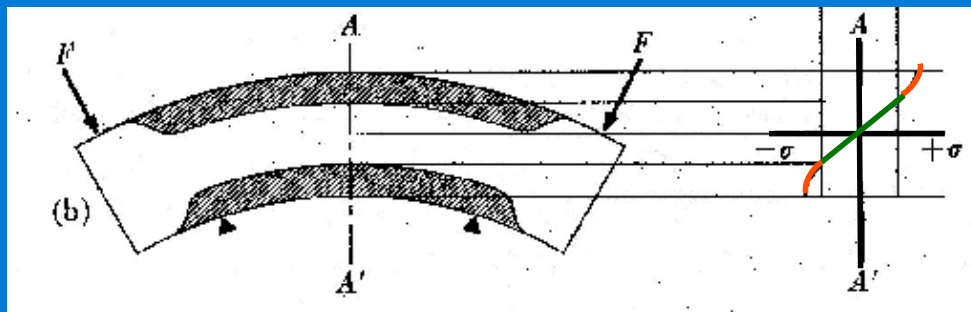
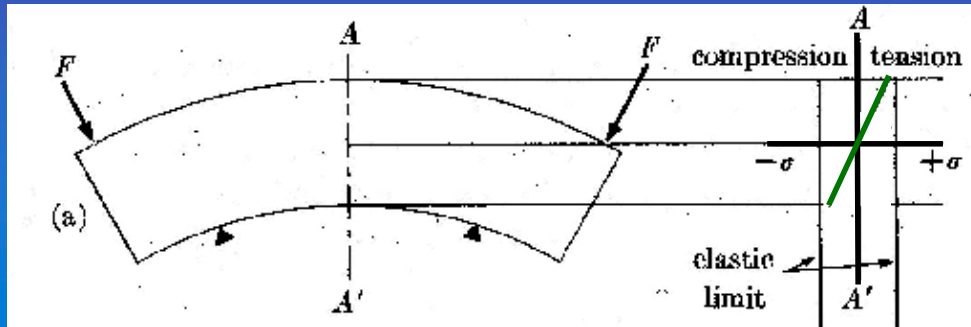
Cold-rolled Ni for high- $T_c$  superconducting wires



# RESIDUAL STRESS ANALYSIS

## Why residual stresses?

Example: residual stress by plastic flow in bending:



(a) loaded **below** elastic limit

(b) loaded **above** elastic limit

(c) unloaded

Shaded regions have been plastically deformed

Source: B.D. Cullity "Elements of X-ray diffraction" II Edition. Addison-Wesley. Reading (1978)

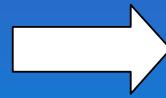


# RESIDUAL STRESS ANALYSIS

Crystalline domains can be used as strain gauges

grain deformation

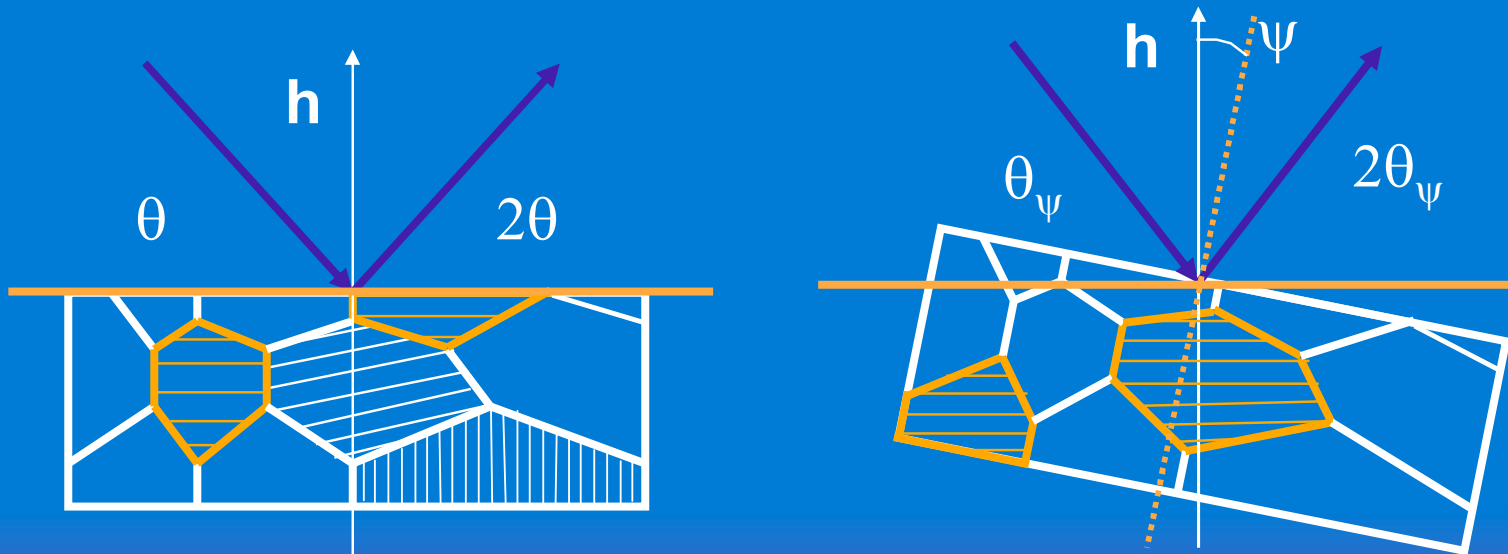
$$\varepsilon = \frac{\Delta l}{l}$$



lattice deformation

$$\varepsilon = \frac{\Delta d}{d}$$

The deformation is measured along different directions, by tilting the sample. The in-plane strain is obtained by measuring  $d$  along off-plane directions.



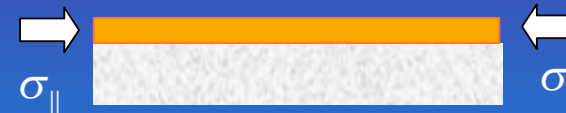




# RESIDUAL STRESS ANALYSIS

If the stress field is plane and rotationally symmetric:

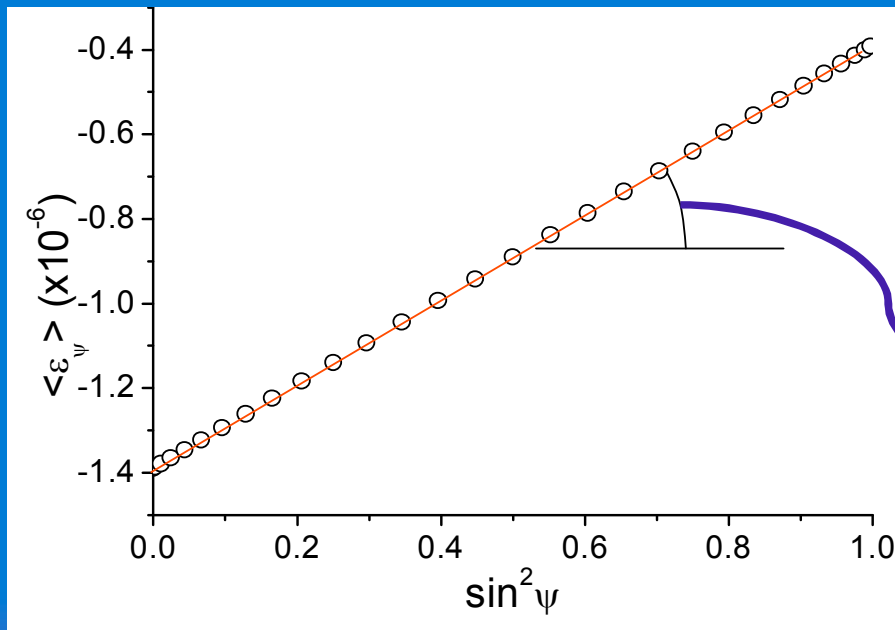
$$\sigma_{11} = \sigma_{22} = \sigma_{\parallel}, \quad \sigma_{12} = \sigma_{13} = \sigma_{23} = \sigma_{33} = 0$$



and if no gradient and no texture are present, then:

$$\langle \varepsilon_{\psi}^{hkl} \rangle = \left( 2S_1^{hkl} + \frac{1}{2}S_2^{hkl} \sin^2 \psi \right) \sigma_{\psi}^S$$

"sin<sup>2</sup>ψ formula"



$$S_1^{hkl}, \frac{1}{2}S_2^{hkl}$$

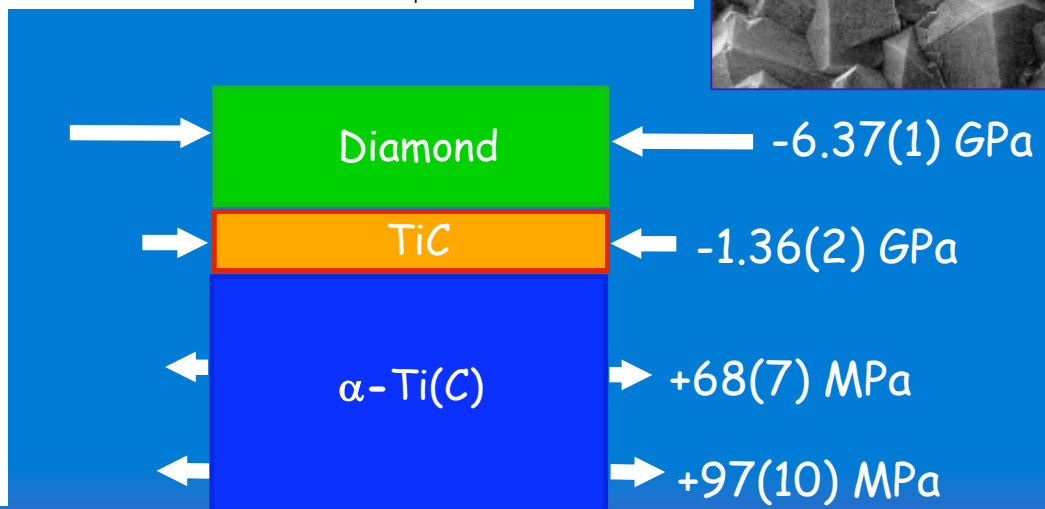
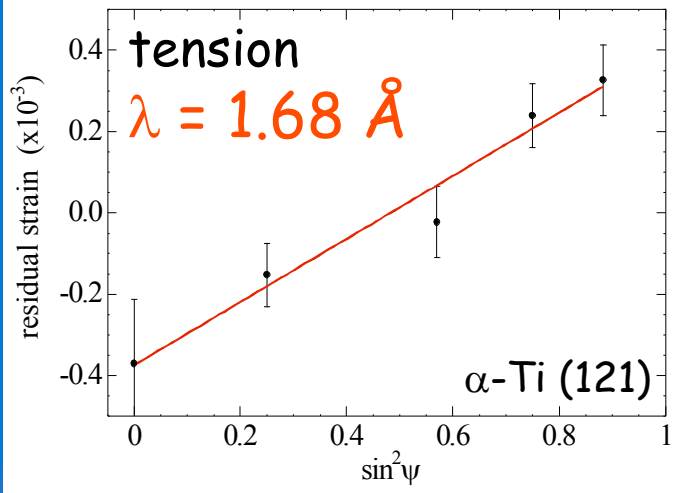
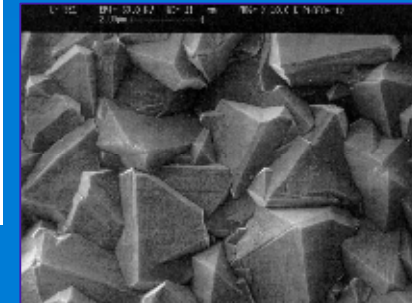
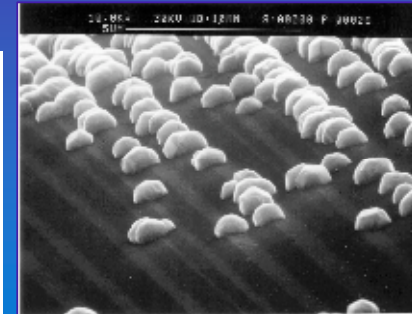
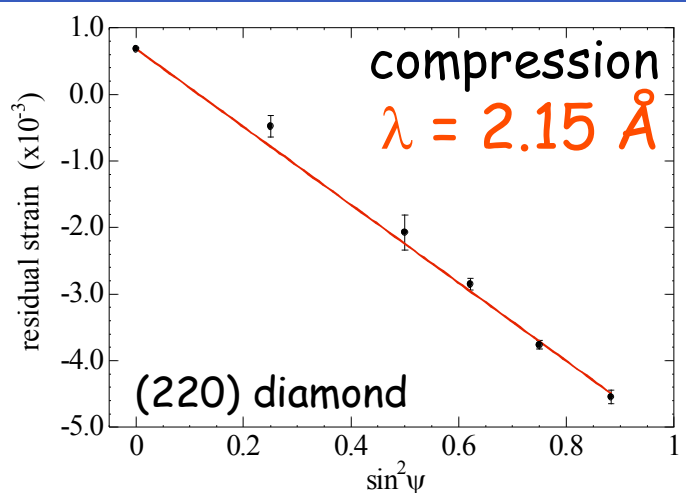
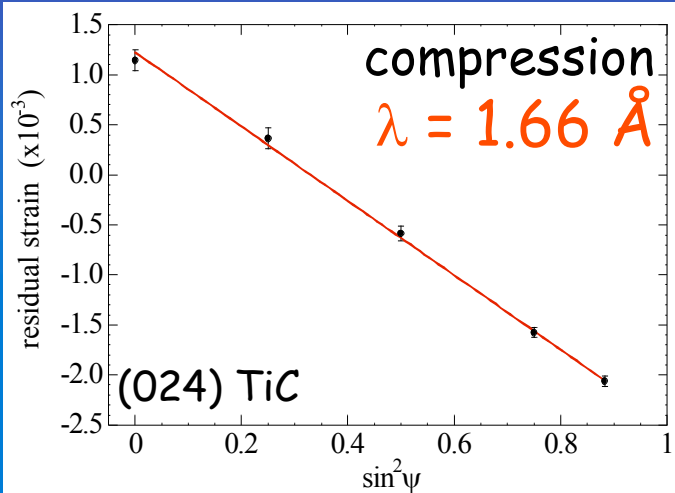
X-ray elastic constants (XECs)

slope related to the average *in-plane* stress



# RESIDUAL STRESS GRADIENT BY SRXRD

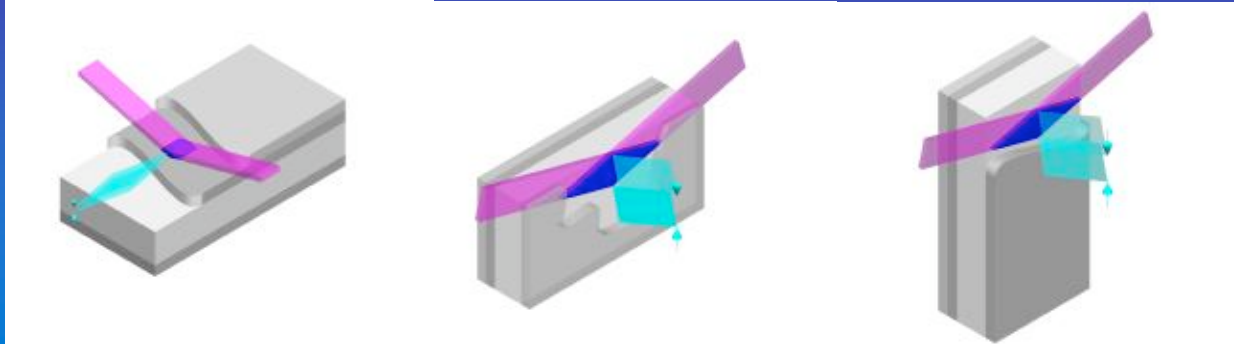
Residual stress in diamond coated components: multiple wavelength XRD



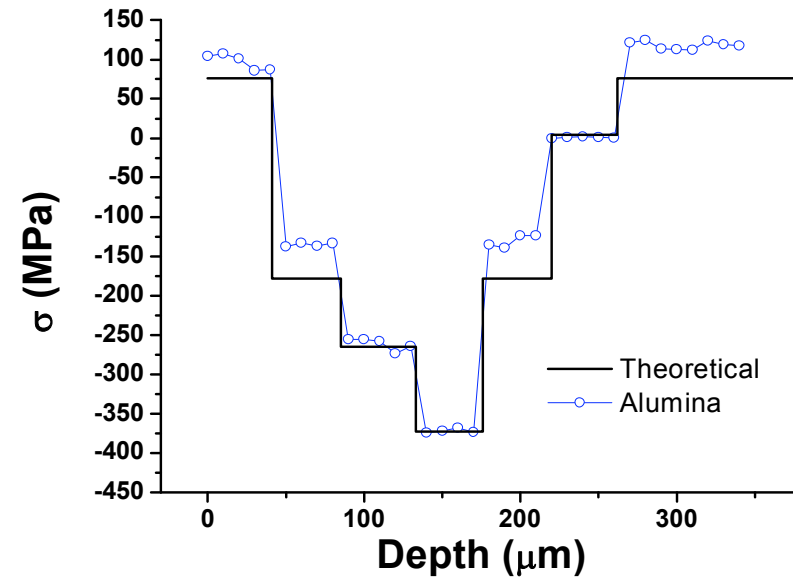
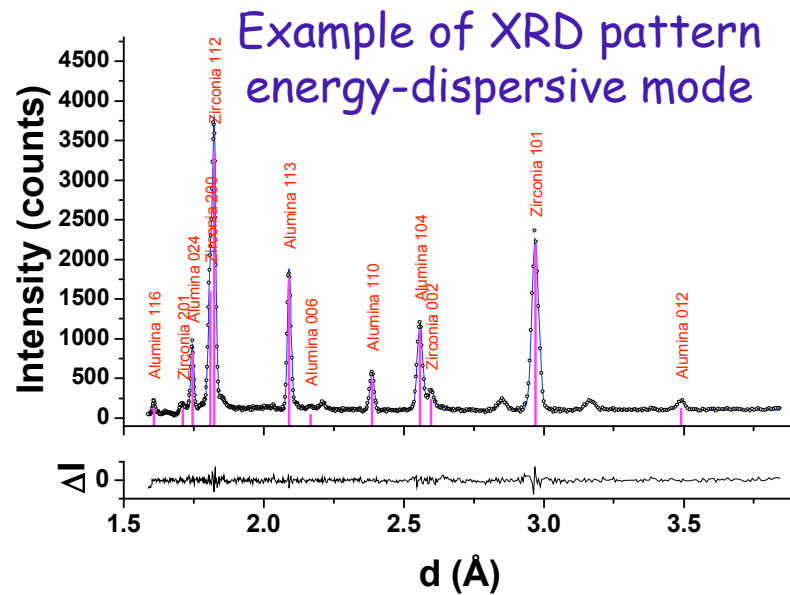


# RESIDUAL STRESS GRADIENT BY SRXRD

Possible geometries for through-thickness stress mapping



Residual stress profile in a Alumina-Zirconia-Mullite ceramic laminates





# PART 1: REFERENCES

- [1] B.D. Cullity, *Elements of X-ray Diffraction*, Addison-Wesley, Reading MA, 1978.
- [2] R. Jenkins & R. L. Snyder, *Introduction to X-ray Powder Diffractometry*, Wiley, New York, 1996
- [3] H.P. Klug & L.E. Alexander, *X-ray Diffraction procedures*, Wiley, New York, 1974.
- [4] B.E. Warren, *X-ray Diffraction*, Addison-Wesley, Reading, MA, 1969.
- [5] R.A. Young (Ed.), *The Rietveld method*, Oxford University Press, Oxford, 1993.
- [6] R.E. Dinnebier and S.J.L. Billinge (Eds.), *Powder Diffraction: Theory and Practice*, The Royal Society of Chemistry, Cambridge, 2008.
- [7] International Tables for X-ray Crystallography, 3<sup>rd</sup> series. [Kluwer Academic Publishers](http://www.kluweronline.com), Dordrecht, Boston, London. Vol.A (1983), Vol.B (1993), Vol.C (1992), "Brief Teaching Edition of Volume A" (1985).
- [8] P.P. Ewald, *Fifty years of X-ray Diffraction*, Reprinted in pdf format for the IUCr XVIII Congress, Glasgow, Scotland. Copyright © 1962, 1999 International Union of Crystallography, Chester, UK.
- [9] International Union of Crystallography: <http://www.iucr.org>
- [10] International Centre for Diffraction Data, Newtown Square, PA, USA. <http://www.icdd.com>



# PRESENTATION OUTLINE

## PART 1

- Basic elements of crystallography and X-ray diffraction (XRD) theory
  - Some advantages and peculiarities of synchrotron radiation XRD (SRXRD)
- 

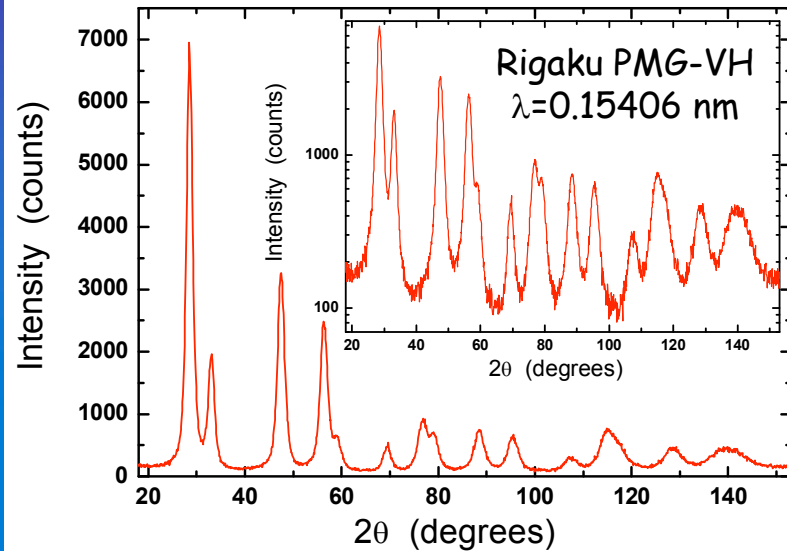
## PART 2

- SRXRD from nanocrystalline and highly deformed materials

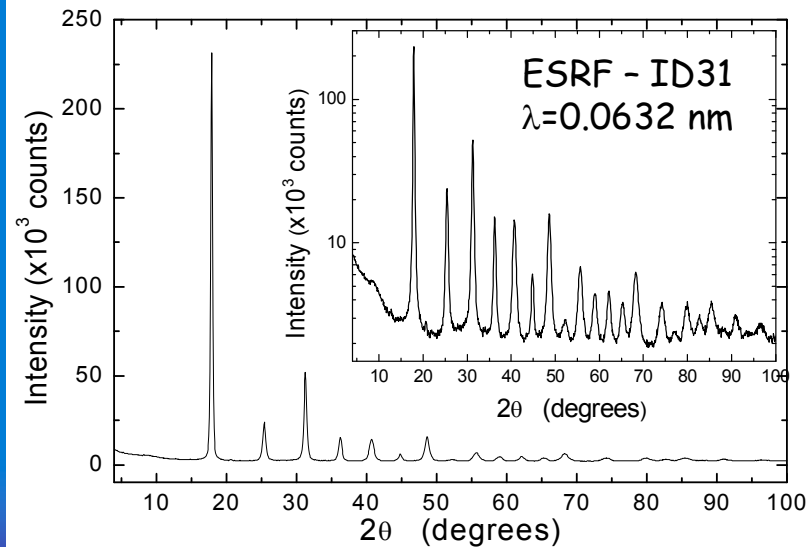
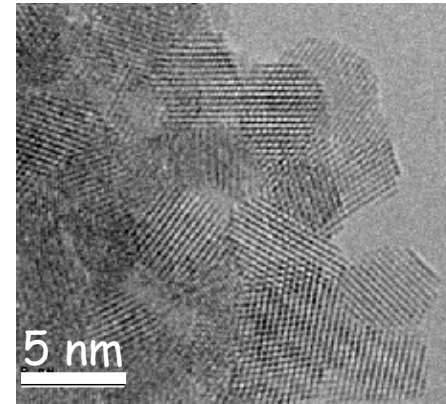


# NANOCRYSTALLINE & HEAVILY DEFORMED MATERIALS

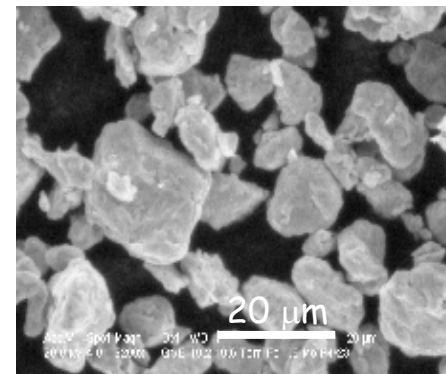
## Two typical cases of study



*Cerium oxide powder from xerogel*



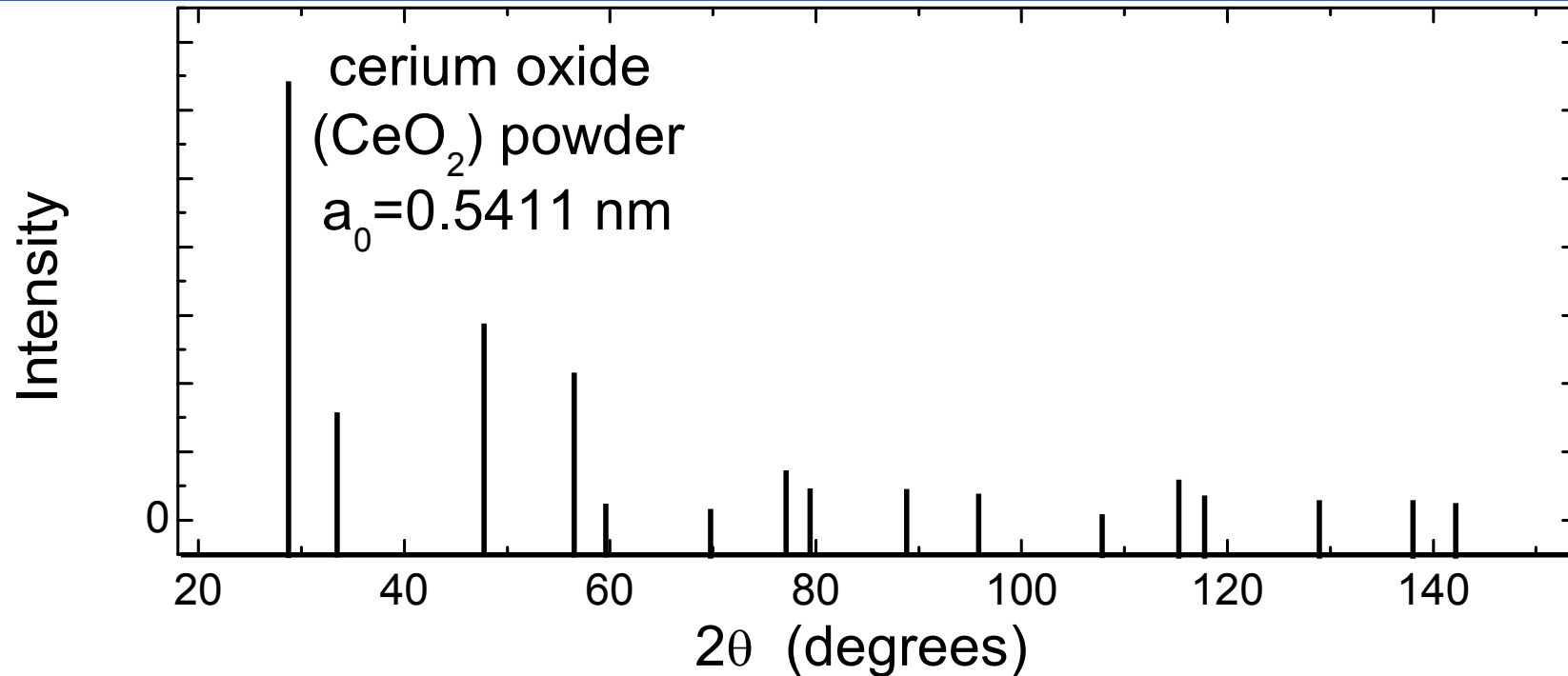
*Ball milled Fe-1.5%Mo*





# DIFFRACTION PATTERN FROM A POLYCRYSTALLINE

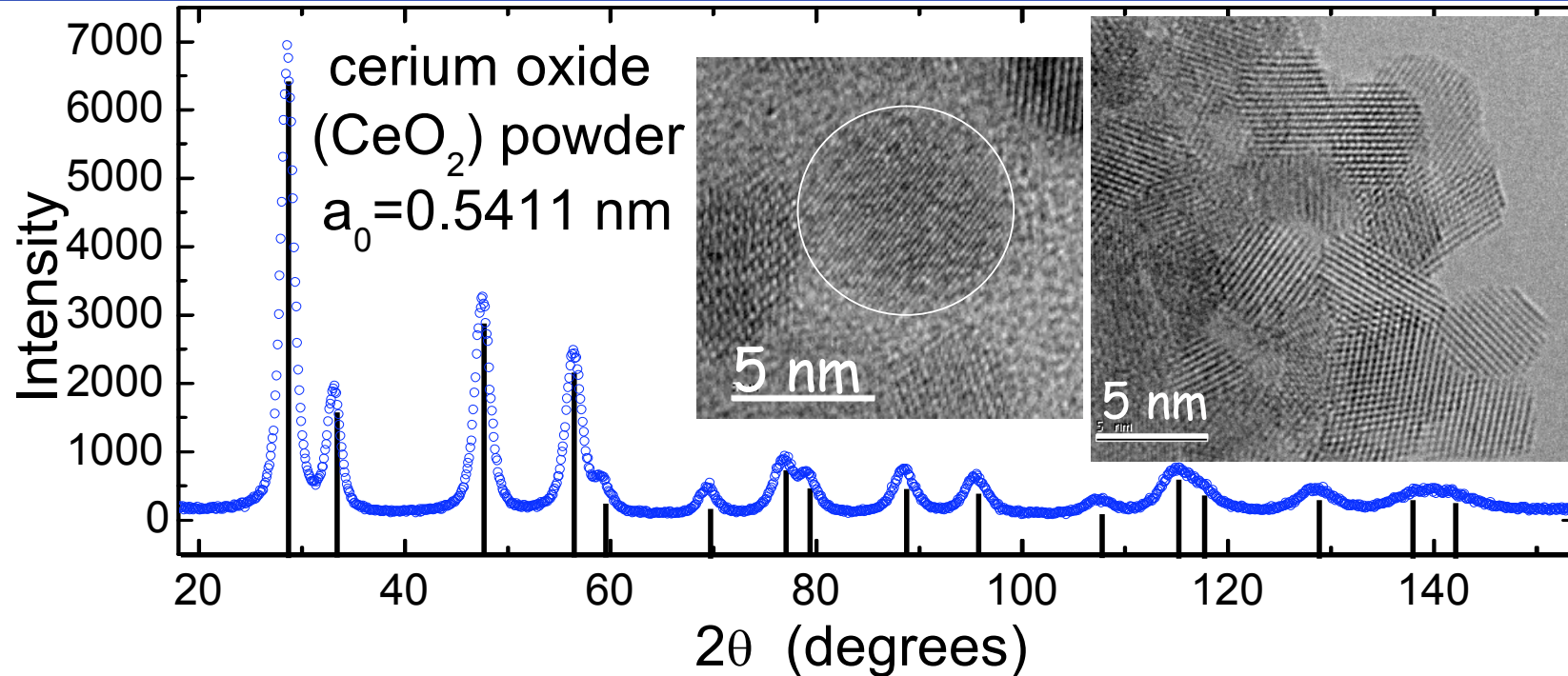
According to Bragg's law, peaks are  $\delta$ -functions (infinitely narrow)





# DIFFRACTION PATTERN FROM A POLYCRYSTALLINE

Actually, Bragg peaks from real (nanocrystalline) materials are broadened

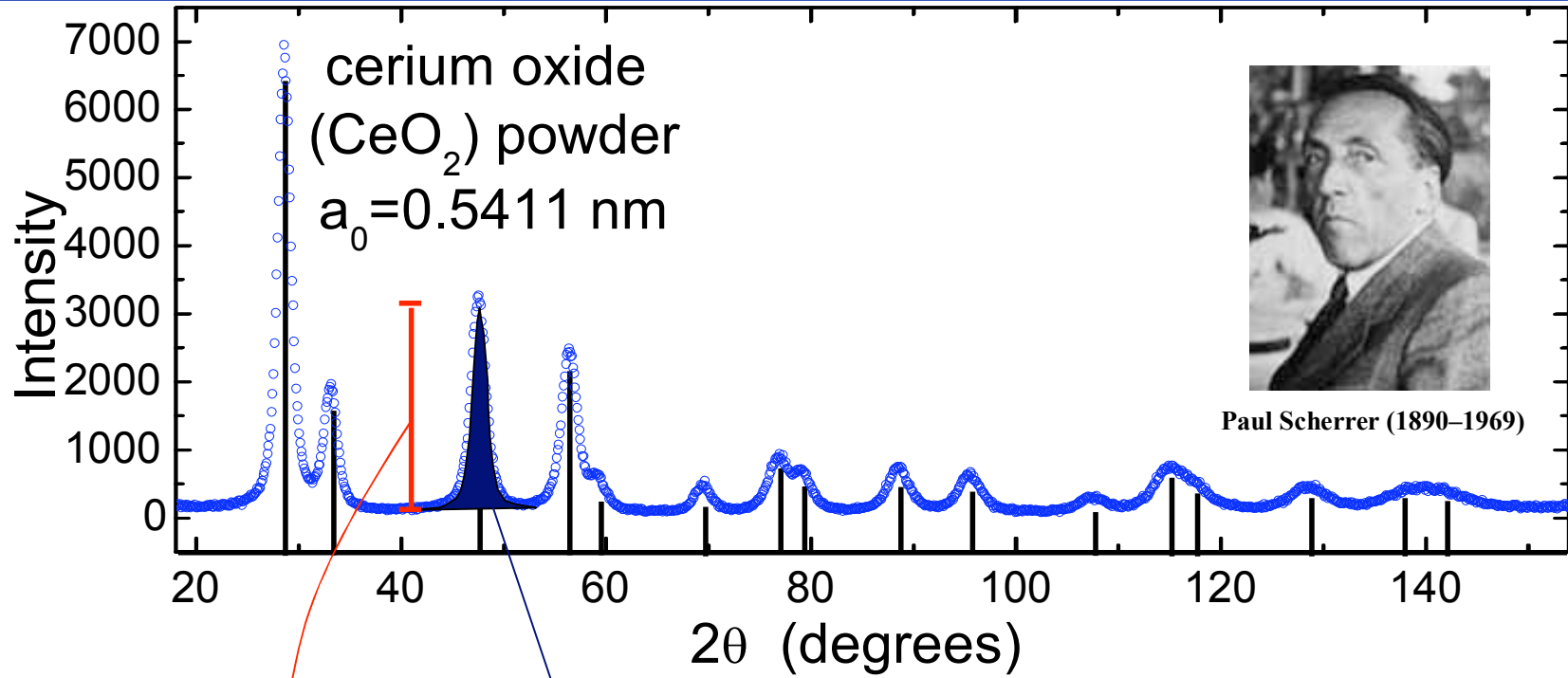






# DIFFRACTION PATTERN FROM A POLYCRYSTALLINE

Integral Breadth (area/intensity) as a measurement of peak broadening



Integral Breadth

$$\beta = \frac{\int I(2\theta) d2\theta}{I(2\theta_B)} = \frac{\lambda}{L \cos \theta}$$

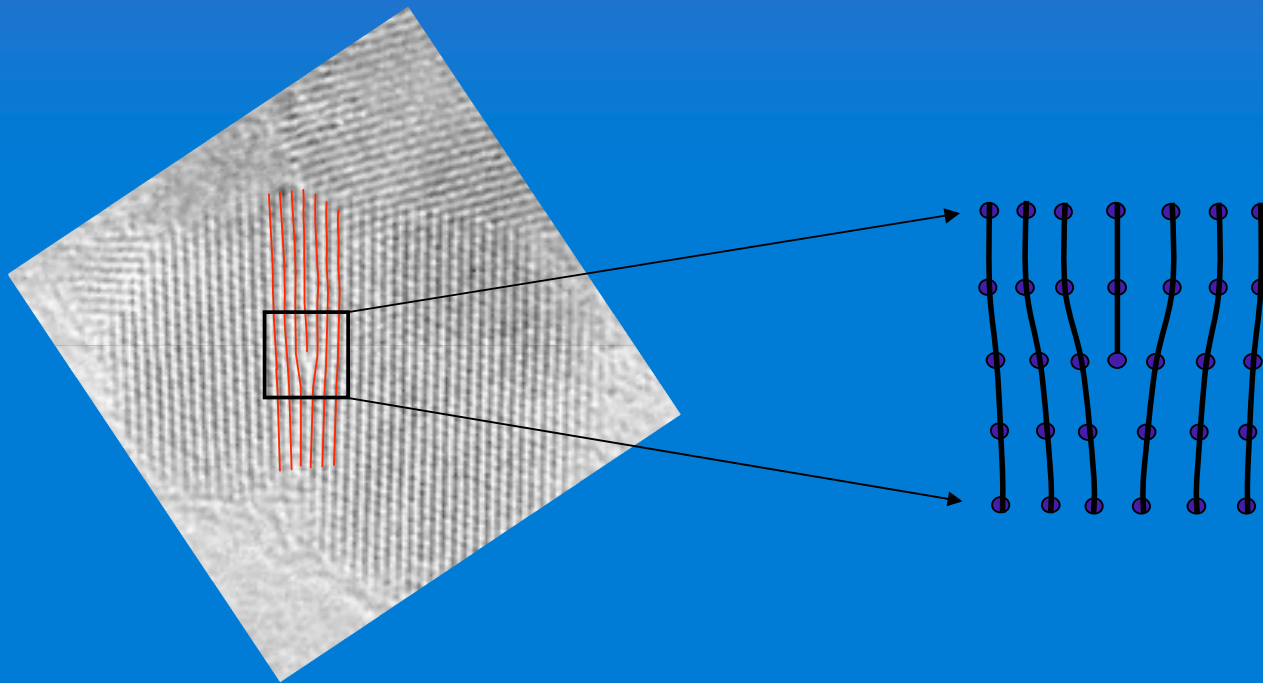
Scherrer formula  
(1918)

*L* : effective crystalline domain size ( $L \approx 1 - 200$  nm)



# STRAIN BROADENING: DISLOCATIONS

Lattice defects may also cause line broadening: e.g., dislocations

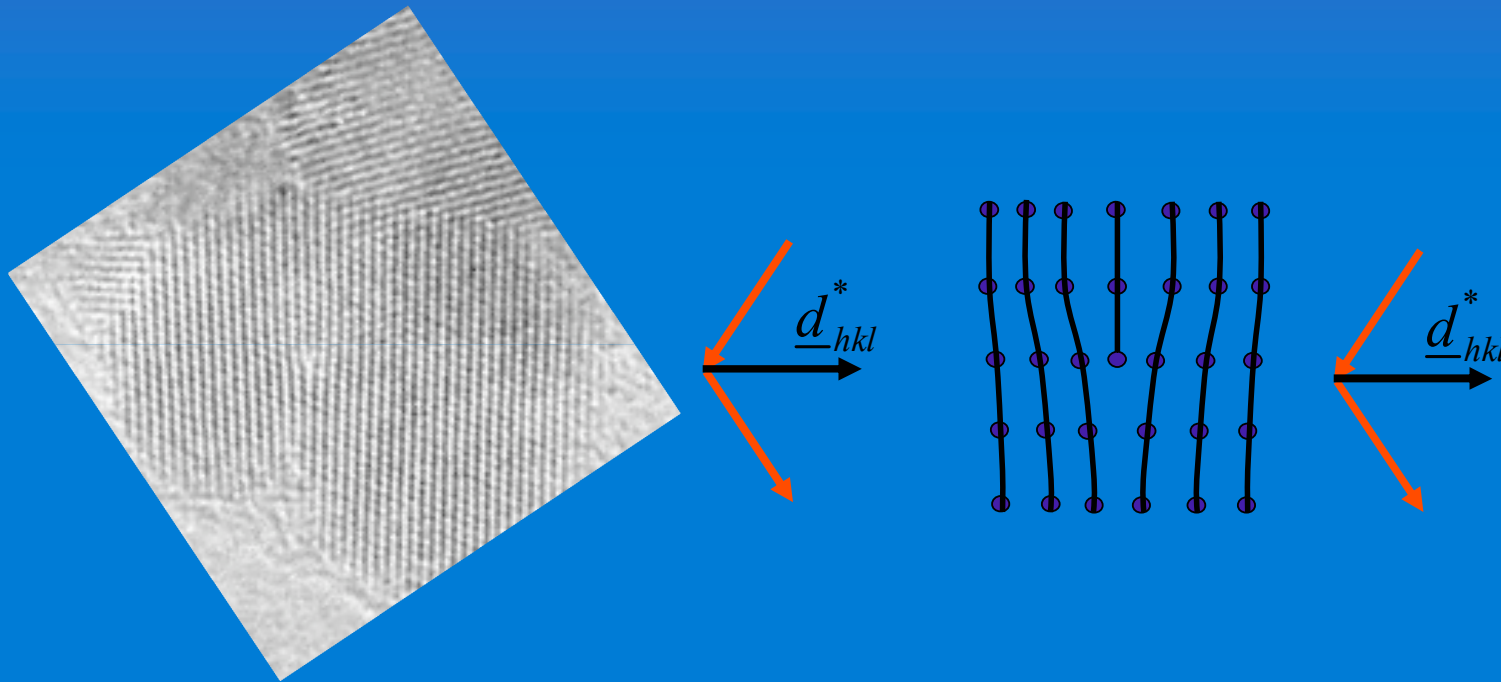


Edge dislocation in a crystalline nanograin



# STRAIN BROADENING: DISLOCATIONS

Lattice defects may also cause line broadening: e.g., dislocations

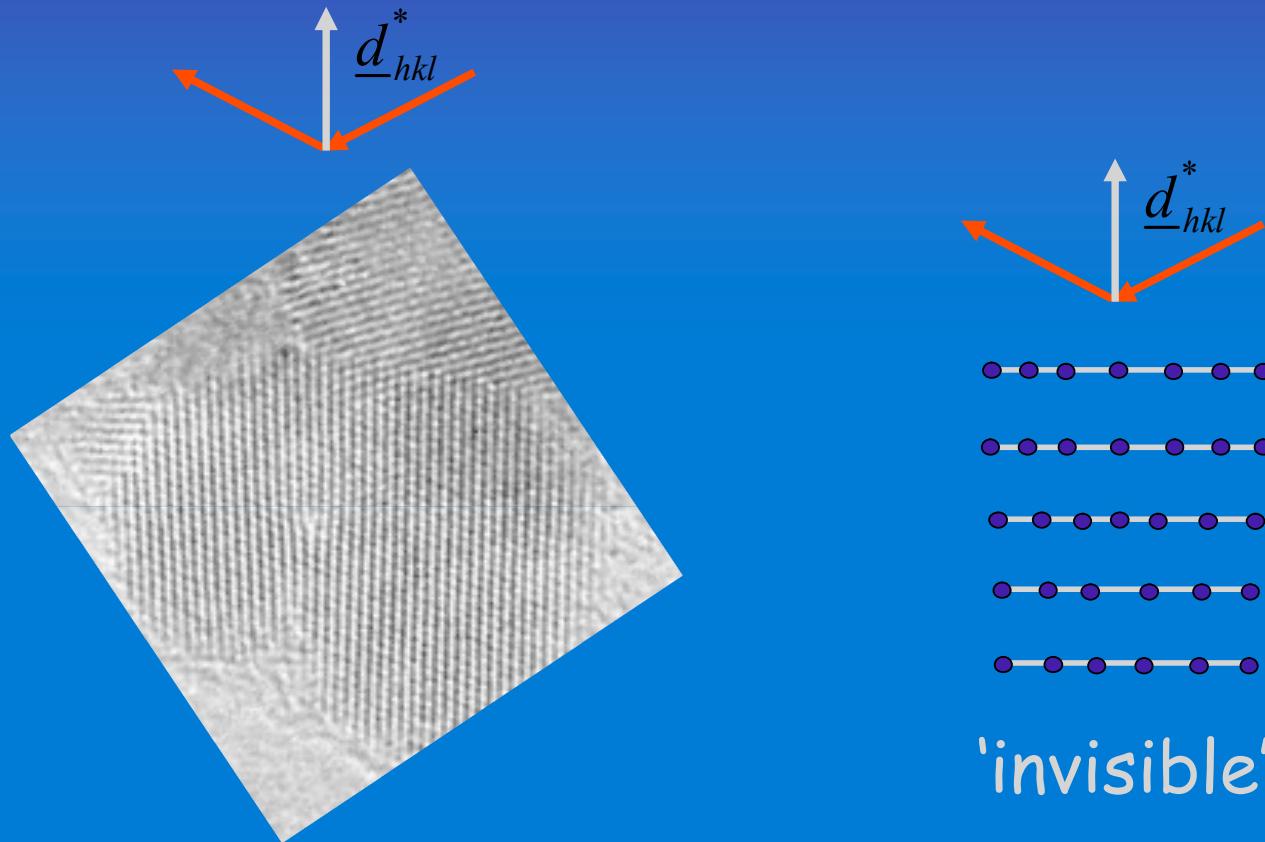


Dislocation "visibility" depends on the viewing direction ( $d_{hkl}^*$ )  
→ line broadening anisotropy



# STRAIN BROADENING: DISLOCATIONS

Lattice defects may also cause line broadening: e.g., dislocations



Dislocation "visibility" depends on the viewing direction ( $d_{hkl}^*$ )  
→ line broadening anisotropy



# MICROSTRAIN EFFECT IN POWDER DIFFRACTION

Heuristic approach: differentiate Bragg's law (with  $\lambda = \text{constant}$ ):

$$0 = 2\Delta d \sin(\theta) + 2d \cos(\theta) \Delta(\theta)$$

Introducing the strain:  $\varepsilon = \Delta d / d$

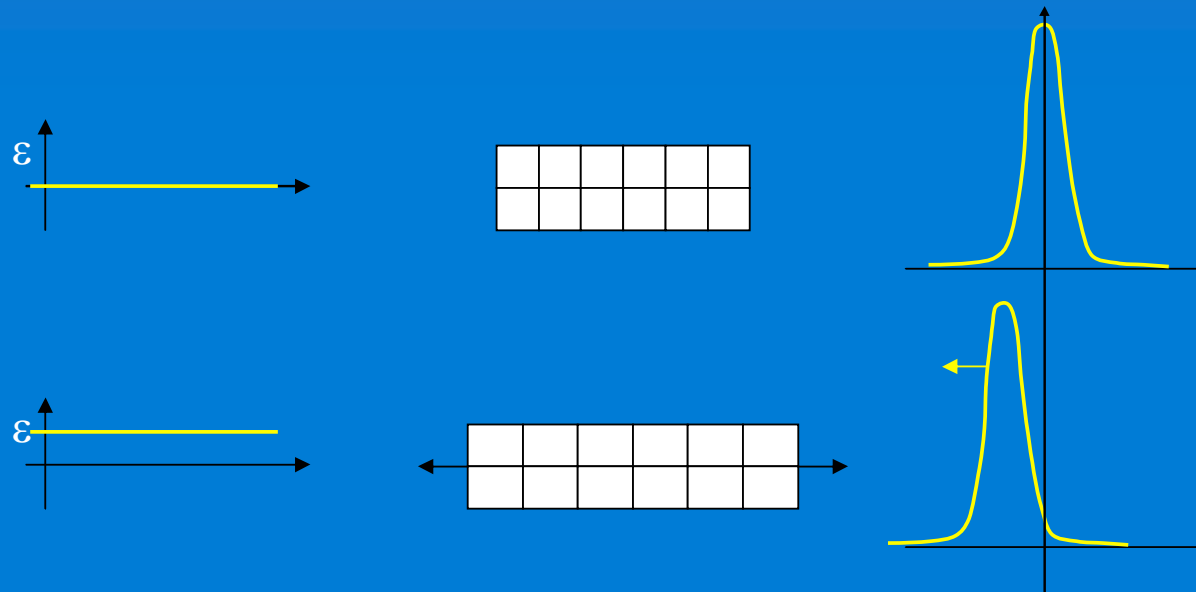
$$\Delta(2\theta) = -2 \tan(\theta) \frac{\Delta d}{d} = -2\varepsilon \tan(\theta)$$



# MICROSTRAIN EFFECT IN POWDER DIFFRACTION

A uniform strain, gives a *shift* in diffraction peak position:

$$\Delta(2\theta) = -2\varepsilon \tan(\theta)$$



⇒ *Residual strain/stress analysis*

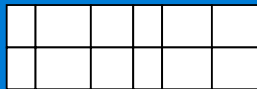
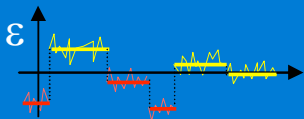
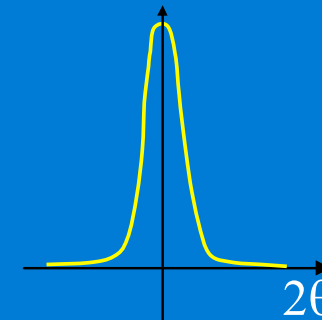
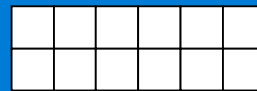
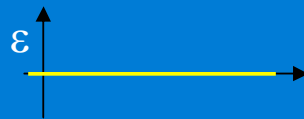


# MICROSTRAIN EFFECT IN POWDER DIFFRACTION

Non-uniform strain gives a distribution  $p_L(\varepsilon)$ . Mean strain can be zero (e.g. in a powder), even if a microstrain (r.m.s. strain) is present:

$$\langle \varepsilon^2 \rangle^{1/2} = \langle (\Delta d/d)^2 \rangle^{1/2}$$

$$\Delta(2\theta) = -2\varepsilon \tan(\theta) \implies \beta(2\theta) \approx 2 \langle \varepsilon^2 \rangle^{1/2} \tan \theta$$

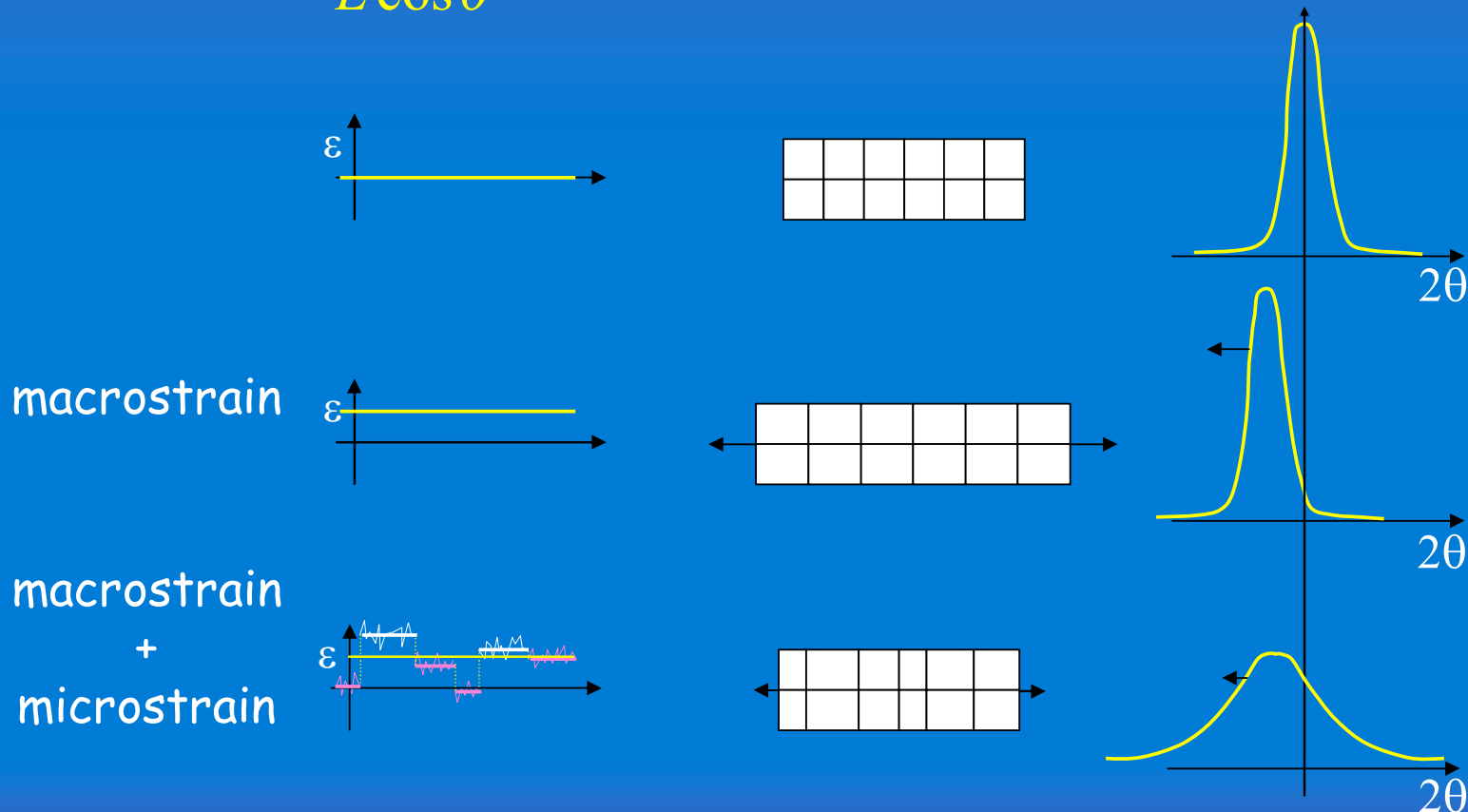




# SIZE - STRAIN EFFECT IN POWDER DIFFRACTION

Combined effects - domain size and lattice distortions

$$\beta(2\theta) \approx \frac{\lambda}{L \cos \theta} + 2 \langle \varepsilon^2 \rangle^{1/2} \tan \theta$$

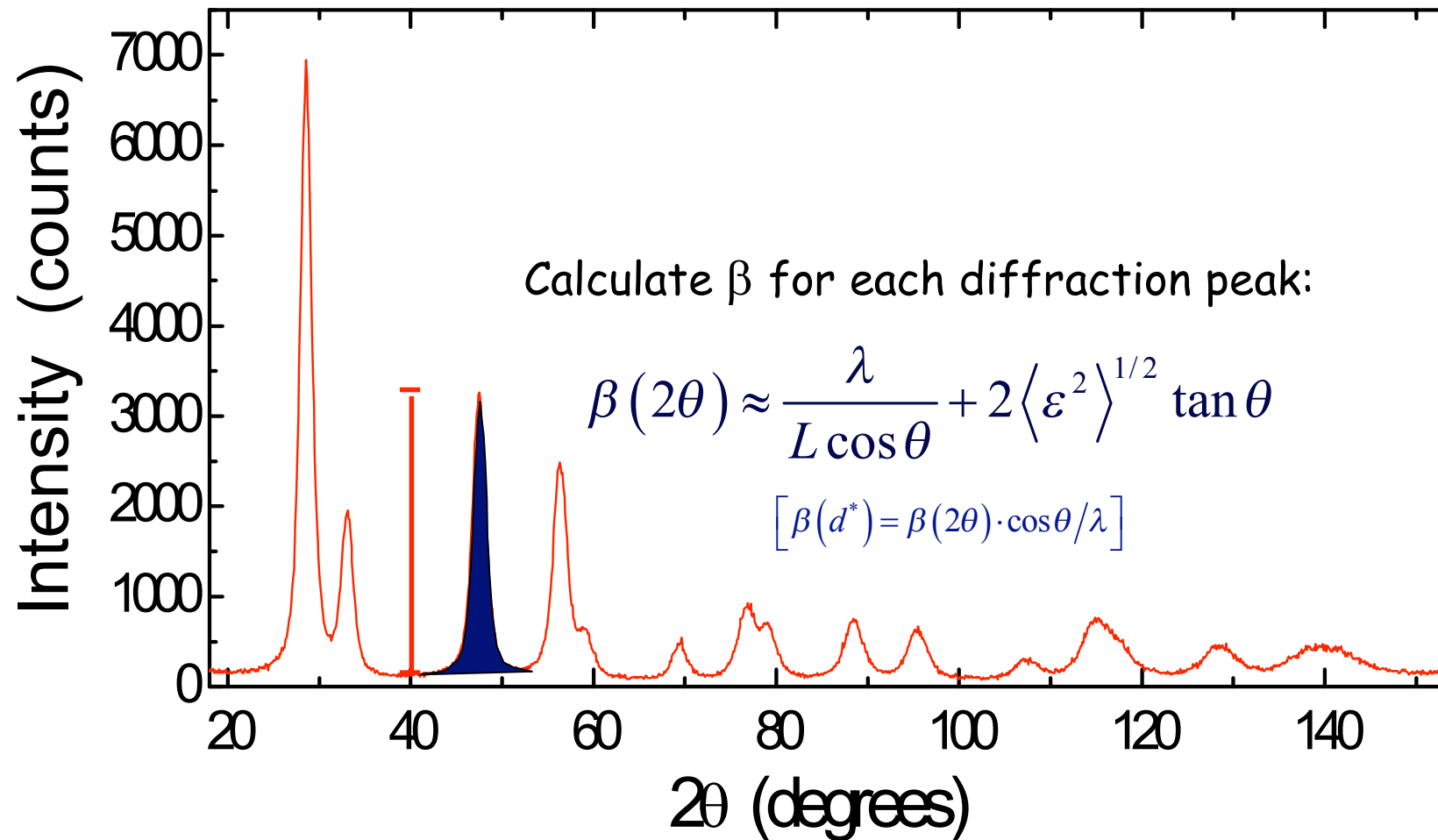






# INTEGRAL BREADTH METHODS

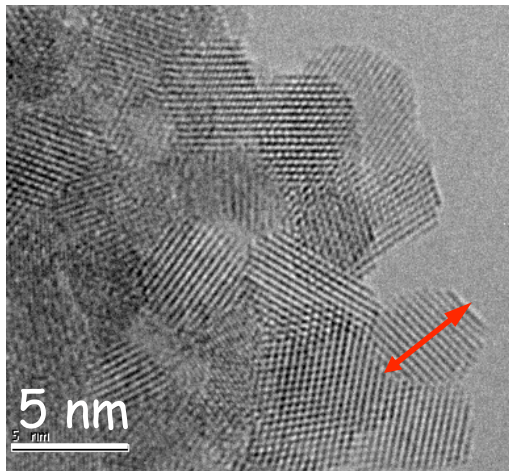
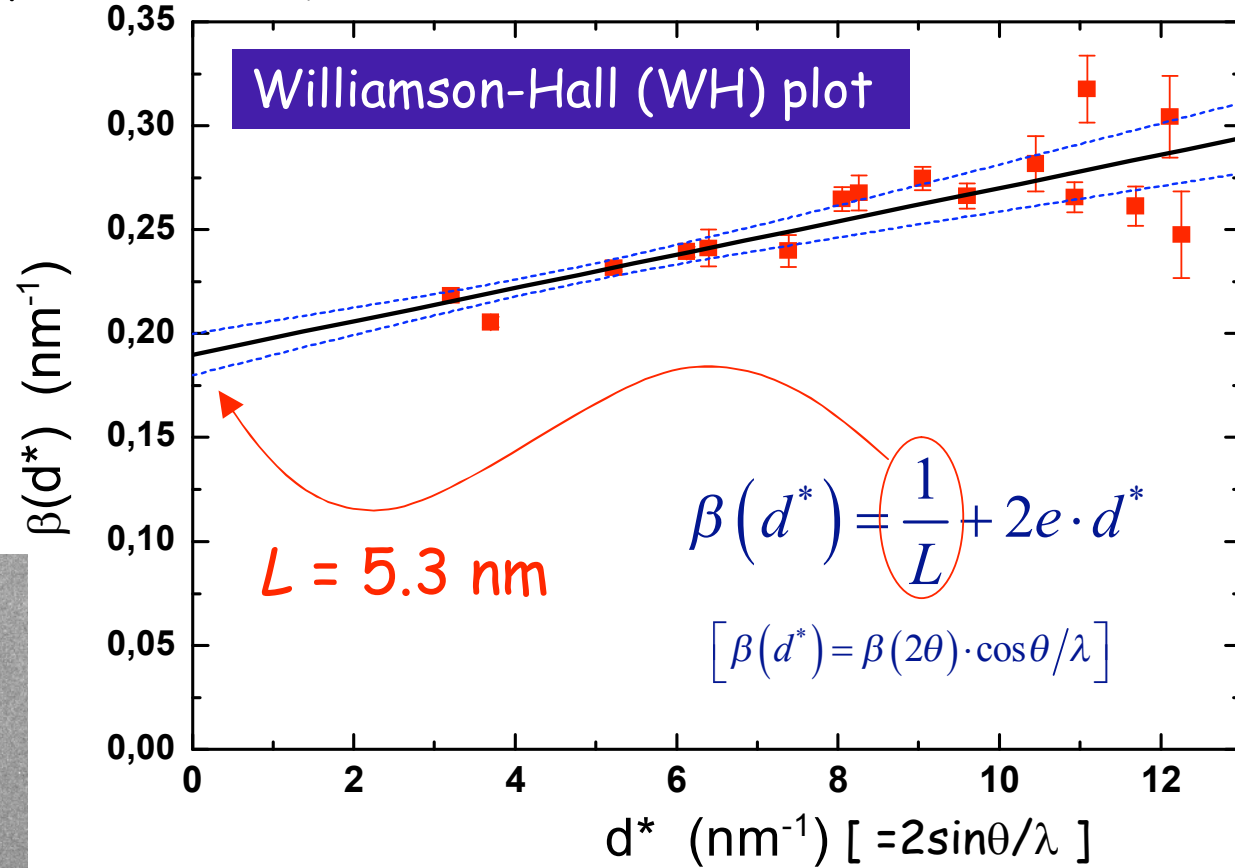
Combined effects - domain size and lattice distortions





# INTEGRAL BREADTH METHODS

Combined effects - domain size and lattice distortions





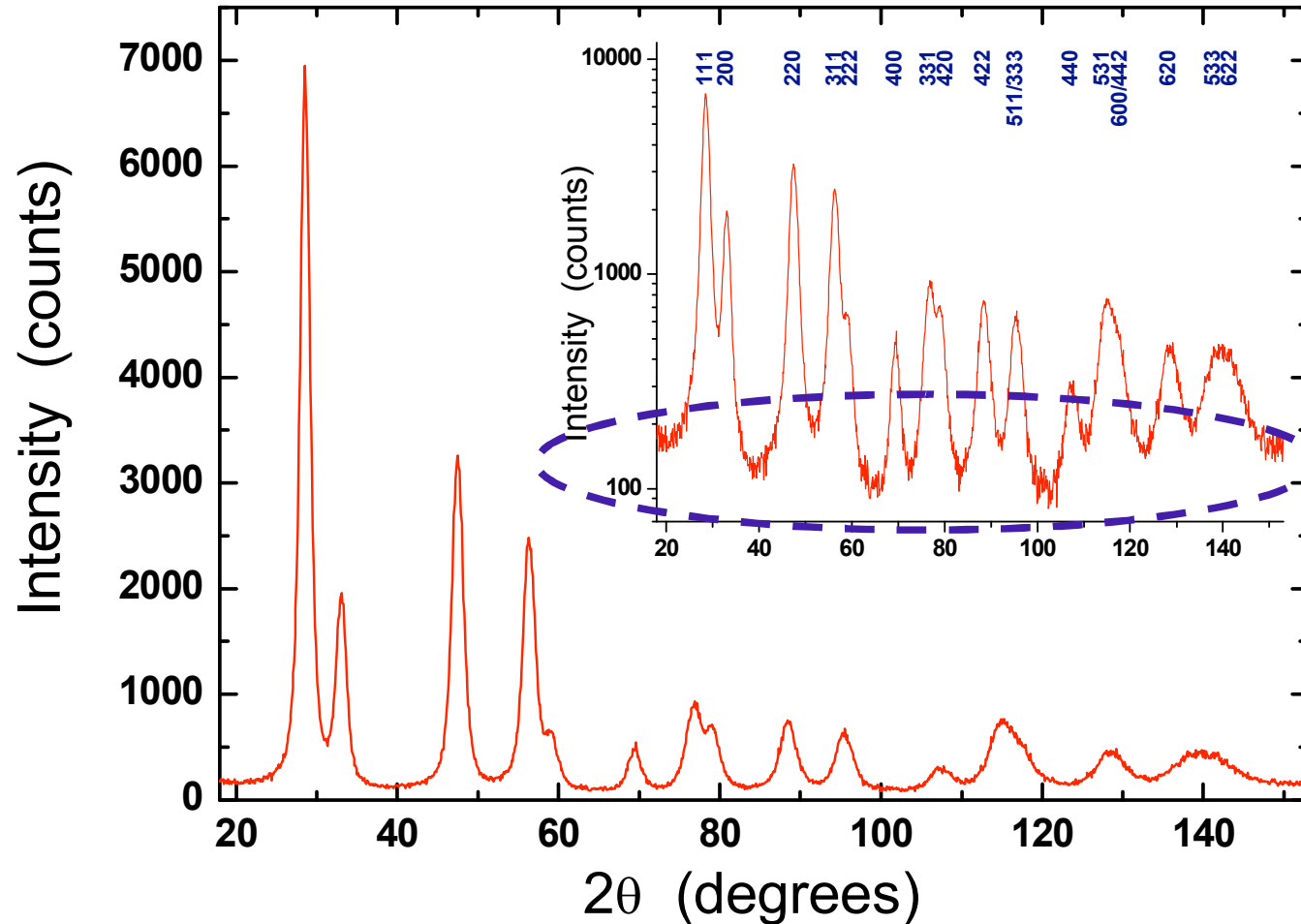
# LINE PROFILE ANALYSIS

## LIMITATIONS OF TRADITIONAL METHODS OF LINE PROFILE ANALYSIS

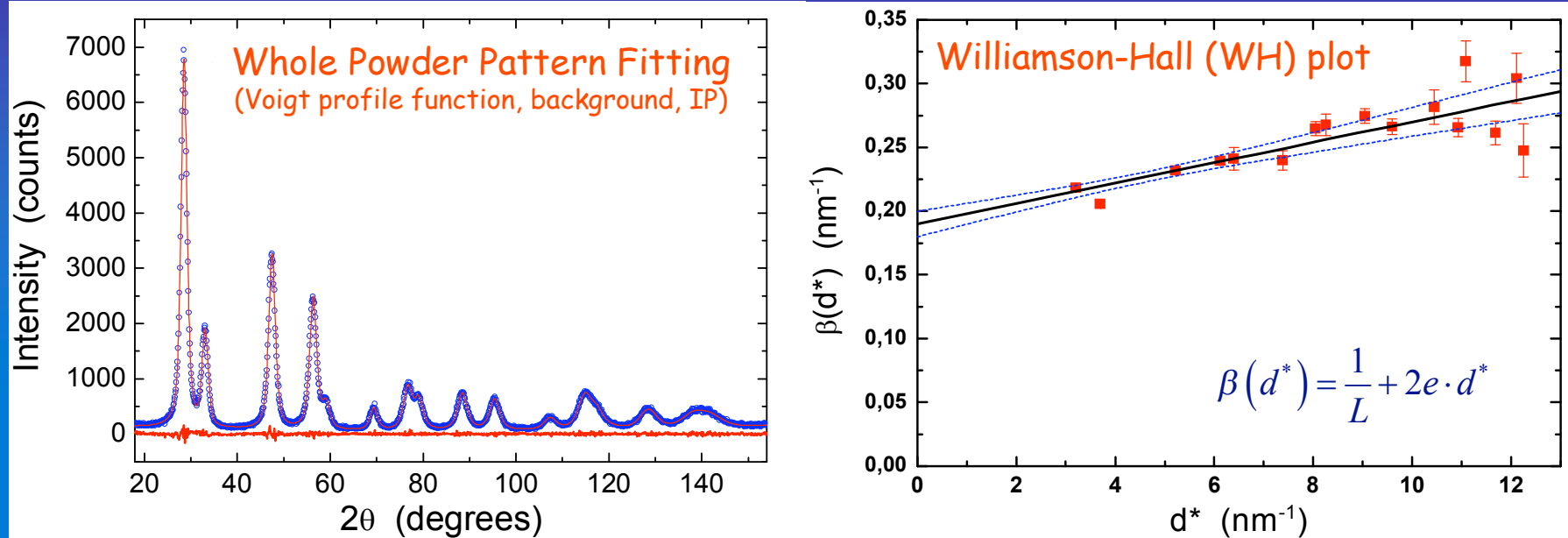


# INTEGRAL BREADTH METHODS: LIMITATIONS

Peak profiles tend to overlap: difficult to obtain integral breadths



# PROFILE FITTING AND LINE PROFILE ANALYSIS



MARQX software: Y.H. Dong & P. Scardi J. Appl. Cryst. 33 (2000) 184

Modern approach to LPA relies on peak profile fitting for

- Pattern decomposition
- Background separation
- Deconvolution / convolution with instrumental profile component

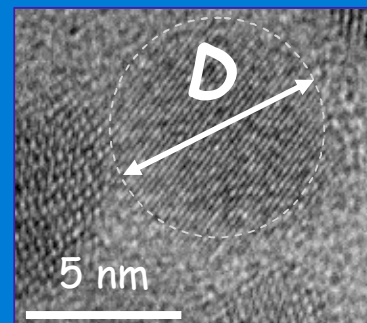
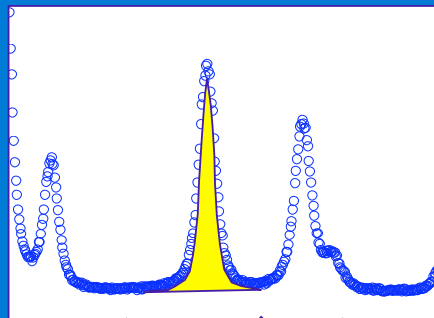
**Although simple and flexible profile fitting is substantially arbitrary and controversial: no reason for adopting a given analytical shape !!!**



# INTEGRAL BREADTH METHODS: LIMITATIONS

What is the meaning of  $L$ ,  
the 'size' value given by the Scherrer formula ??

$$\beta(2\theta) = \frac{\lambda}{L \cos \theta}$$

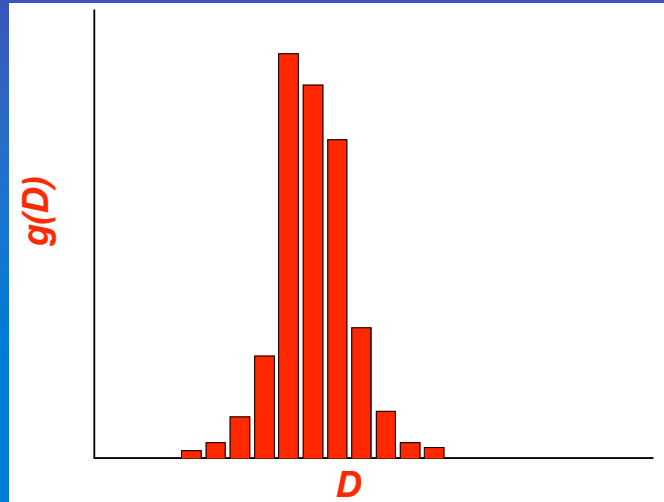


$L \neq D$



# INTEGRAL BREADTH METHODS: LIMITATIONS

In most cases nano powders have a distribution of sizes (and shapes)



Distribution 'moments'

$$M_i = \int D^i g(D) dD$$

$M_1 \rightarrow$  mean

$M_2 - M_1^2 \rightarrow$  variance

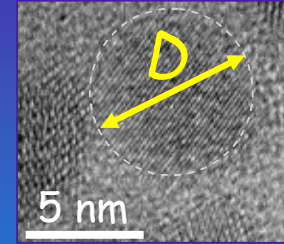
$$L \rightarrow \langle L \rangle_V = \frac{1}{K_\beta} \frac{M_4}{M_3}$$

$K_\beta$ , a shape factor, generally function of  $hkl$  (4/3 for spheres)

# INTEGRAL BREADTH METHODS: LIMITATIONS

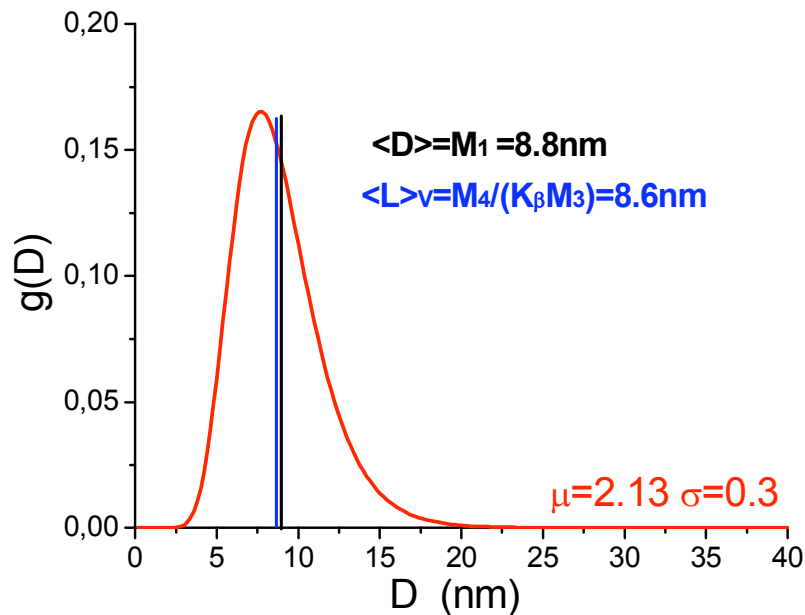


$$L \rightarrow \langle L \rangle_V = \frac{1}{K_\beta} \frac{M_4}{M_3} \neq D$$

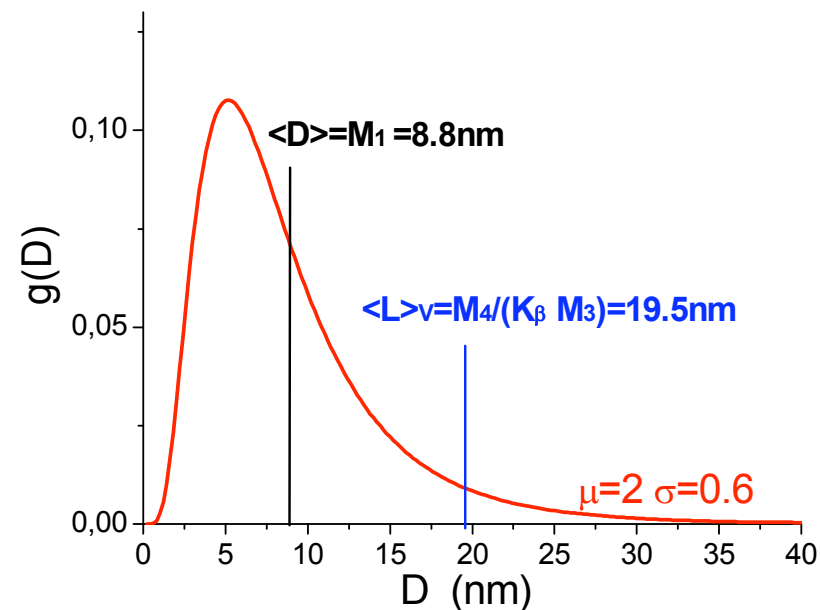


Example: lognormal distributions of spheres,  $g(D)$  (mean  $\mu$ , variance  $\sigma$ )

For little asymmetrical or narrow distributions



For broad, asymmetrical distributions

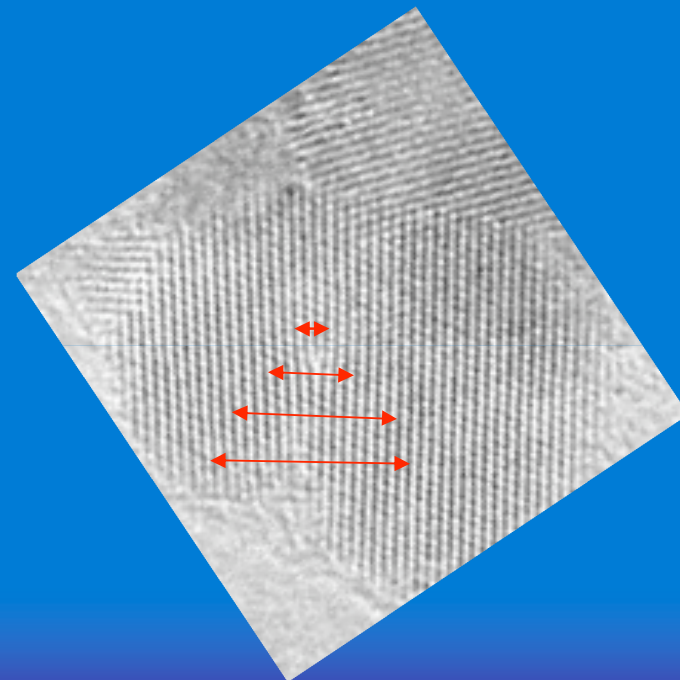






## INTEGRAL BREADTH METHODS: MAIN LIMITATIONS

- Peak overlapping  $\rightarrow$  requires profile fitting with *arbitrary* profile functions
- Effective domain size,  $L \rightarrow$  real information is the *size distribution*
- Microstrain  $\epsilon$  is not a constant  $\rightarrow$  *microstrain distribution*





## INTEGRAL BREADTH METHODS: MAIN LIMITATIONS

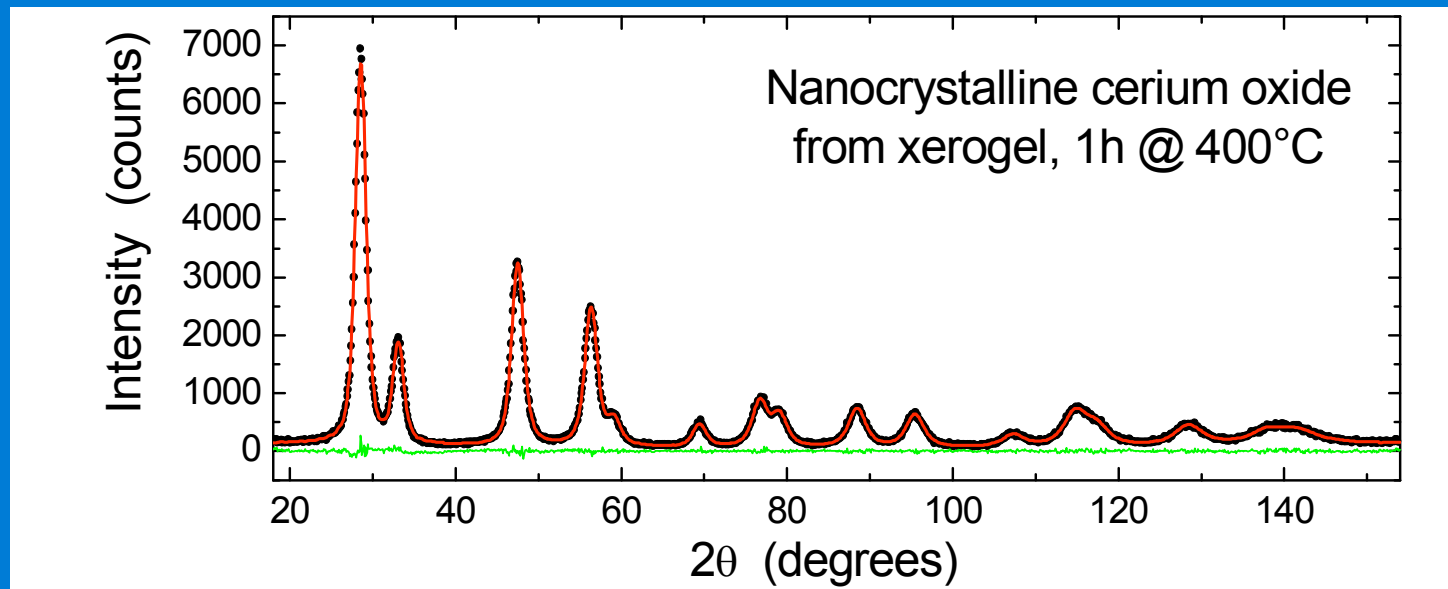
- Peak overlapping → profile fitting with *arbitrary* profile functions
- Effective domain size,  $L$  → real information is the *size distribution*
- Microstrain  $e$  is not a constant → *microstrain distribution*
- Line broadening effects *do not* simply “add” as in the Williamson-Hall formula

$$\beta(d^*) = \underbrace{\frac{1}{L}}_{\text{'size'}} + \underbrace{2e \cdot d^*}_{\text{'strain'}}$$



# WHOLE POWDER PATTERN MODELLING - WPPM

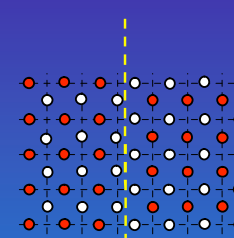
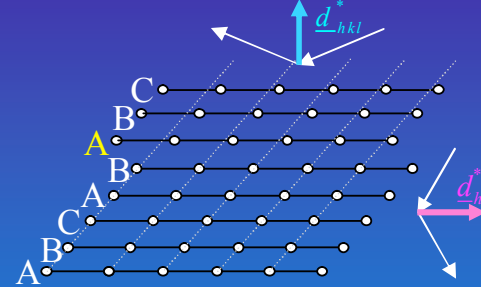
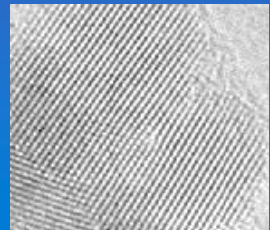
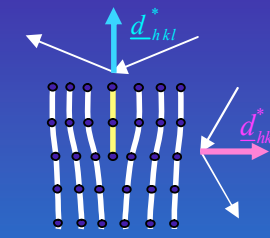
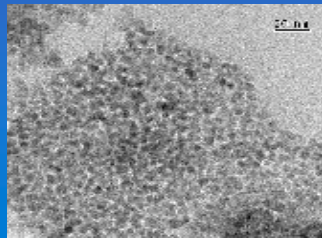
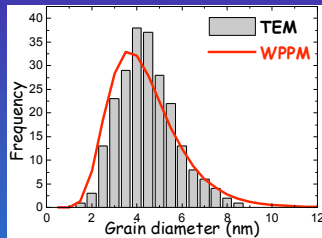
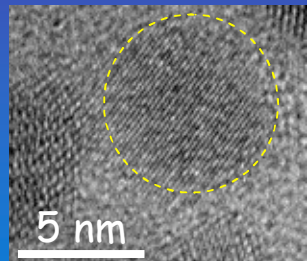
Modelling of the experimental pattern based on physical models of the microstructure and lattice defects:



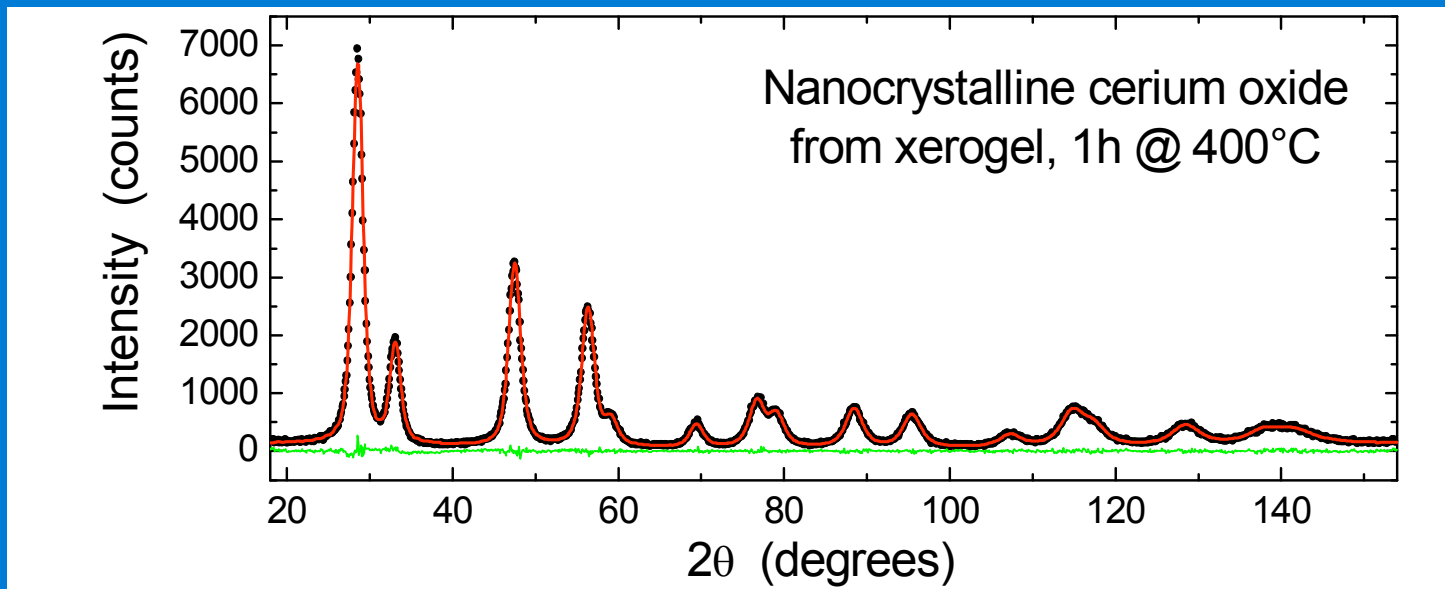
M. Leoni, R. Di Maggio, S. Polizzi & P. Scardi, *J. Am. Ceram. Soc.* 87 (2004) 1133.

P. Scardi & M. Leoni, *Acta Cryst. A* 57 (2001) 604. P. Scardi & M. Leoni, *Acta Cryst. A* 58 (2002) 190

# WHOLE POWDER PATTERN MODELLING



(...)



M. Leoni, R. Di Maggio, S. Polizzi & P. Scardi, *J. Am. Ceram. Soc.* 87 (2004) 1133.

P.Scardi & M. Leoni, *Acta Cryst. A* 57 (2001) 604. P.Scardi & M. Leoni, *Acta Cryst. A* 58 (2002) 190



# WHOLE POWDER PATTERN MODELLING

Modelling of the experimental pattern based on physical models of the microstructure and lattice defects:



How does it work ??



# DIFFRACTION LINE PROFILE: CONVOLUTION OF EFFECTS

The diffraction peak is a **convolution** ( $\otimes$ ) of *profile components* :

instrumental profile (IP), domain size (S), microstrain (D), faulting (F), anti-phase domain boundaries (APB), stoichiometry fluctuations (C), grain surface relaxation (GSR), etc.

$$I(s) = I^{IP}(s) \otimes I^S(s) \otimes I^D(s) \otimes I^F(s) \otimes I^{APB}(s) \otimes I^C(s) \otimes I^{GRS}(s) \dots$$

$$h = g$$

Instrument

$$\otimes$$

$$f$$

Specimen-related

What is the difference between *convolution* and *sum of effects* ??



# DIFFRACTION LINE PROFILE: CONVOLUTION OF EFFECTS

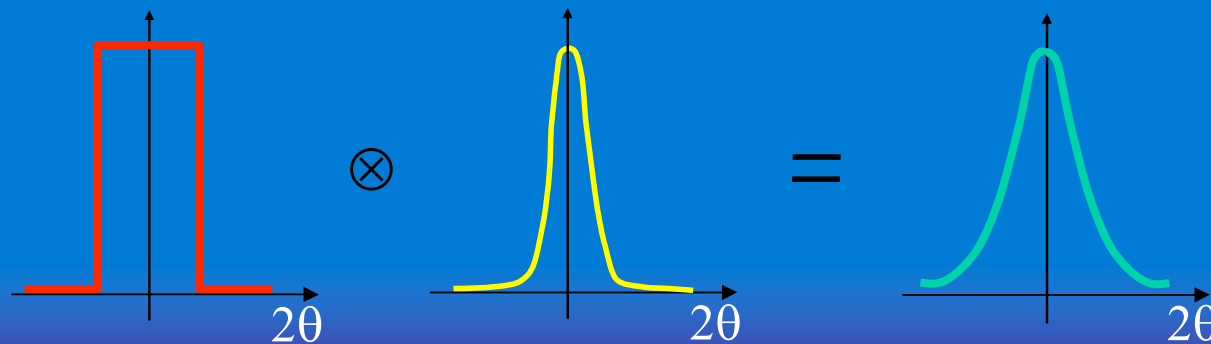
Example: consider instrument (IP) and domain size (S):

$$I(s) = I^{IP}(s) \otimes I^S(s)$$



$$I(s) = \int I^{IP}(t) I^S(s-t) dt$$

g profile, slit (box) function; f profile, bell-shape function (e.g. gaussian)





## WPPM : HOW DOES IT WORK ??

The diffraction profile results from a convolution of effects:

$$I(s) = I^{IP}(s) \otimes I^S(s) \otimes I^D(s) \otimes I^F(s) \otimes I^{APB}(s) \otimes I^C(s) \otimes I^{GRS}(s) \dots$$

the Fourier Transform of  $I(s)$  is the product of the FTs of the single profile components

$$I(s) \propto \int_{-\infty}^{\infty} C(L) e^{2\pi i L \cdot s_{hkl}} dL$$

$$C = \prod_i A_i = \underbrace{T_{pV}^{IP}}_{\text{instr. profile}} \cdot \underbrace{A_{\{hkl\}}^S}_{\text{domain size/shape}} \cdot \underbrace{A_{\{hkl\}}^D \cdot (A_{hkl}^F + iB_{hkl}^F)}_{\text{lattice defects / strain}} \cdot A_{\{hkl\}}^{APB} \cdot \dots$$





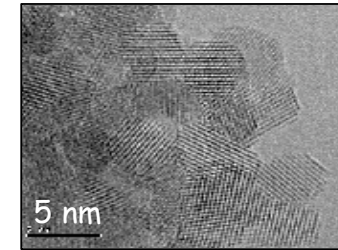
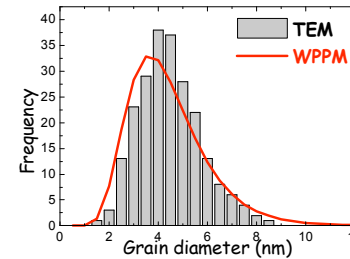
# $A_i(L)$ EXPRESSIONS (ANALYTICAL OR NUMERICAL FORM)

$$T_{pV}^{IP}(L) = (1-k) \cdot \exp(-\pi^2 \cdot \sigma_s^2 L^2 / \ln 2) + k \exp(-2\pi \cdot \sigma_s L)$$

Instrumental profile

Domain size effect:  $\mu, \sigma$

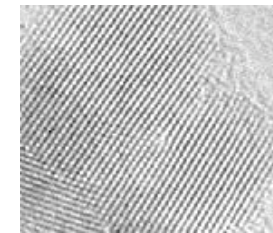
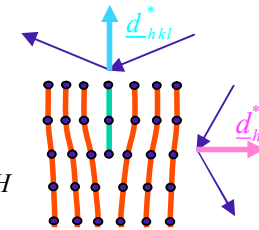
$$A^S(L) = \sum_{n=0}^3 H_n^c \cdot \text{Erfc} \left[ \frac{\ln(L \cdot K^c) - \mu - (3-n)\sigma^2}{\sigma\sqrt{2}} \right] \frac{M_{l,3-n}}{2M_{l,3}} \cdot L^n$$



Dislocation (strain) effect:  $\rho, Re, (\bar{C}_{hkl})$

$$A_{\{hkl\}}^D(L) = \exp \left[ -\frac{1}{2} \pi |b|^2 \bar{C}_{hkl} \rho d_{\{hkl\}}^{*2} \cdot L^2 f^*(L/R_e) \right]$$

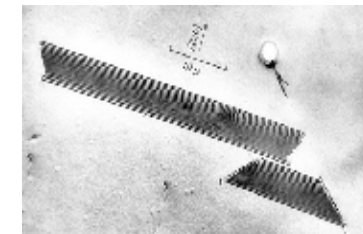
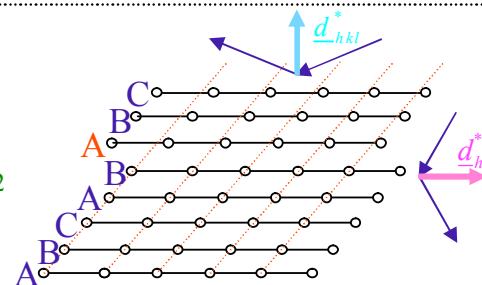
$$\bar{C}_{hkl} = A + B \cdot \frac{h^2 k^2 + k^2 l^2 + l^2 h^2}{(h^2 + k^2 + l^2)^2} = A + B \cdot H$$



Faulting:  $\alpha$  (def.),  $\beta$  (twin)

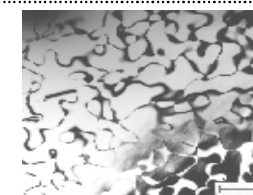
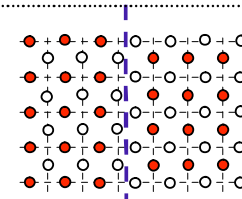
$$A_{hkl}^F(L) = (1 - 3\alpha - 2\beta + 3\alpha^2) \left| \frac{1}{2} L d_{\{hkl\}}^* \frac{L_o}{h_o^2} \sigma_{L_o} \right|$$

$$B_{hkl}^F(L) = -\sigma_{L_o} \cdot \frac{L}{|L|} \cdot \frac{L_o}{|L_o|} \cdot \beta / (3 - 6\beta - 12\alpha - \beta^2 + 12\alpha^2)^{1/2}$$



Anti-Phase Domains:  $\gamma$

$$A_{\{hkl\}}^{APB}(L) = \exp \left[ -\frac{-2\gamma (|h| + |k|) \cdot L}{d_{hkl} (h^2 + k^2 + l^2)} \right]$$





# WHOLE POWDER PATTERN MODELLING

- Diffraction profiles are modelled directly in terms of relatively few microstructural parameters:  $\mu, \sigma - \rho, Re - \alpha, \beta - \gamma \dots$
- No arbitrary profile functions (Voigt, pseudo-Voigt, Pearson VII, etc.)

*WPPM* : based on physical models of microstructure and lattice defects



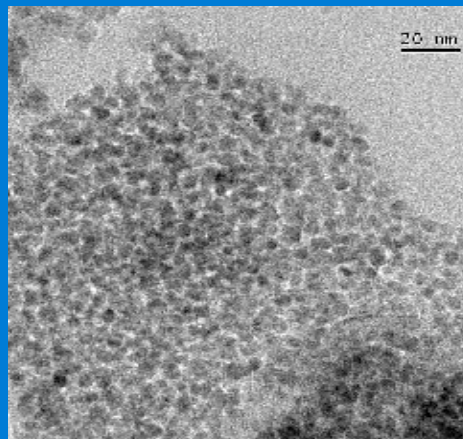
More Theory: see REFERENCES



# WPPM APPLICATIONS



## Nanocrystalline cerium oxide: growth kinetics of a xerogel

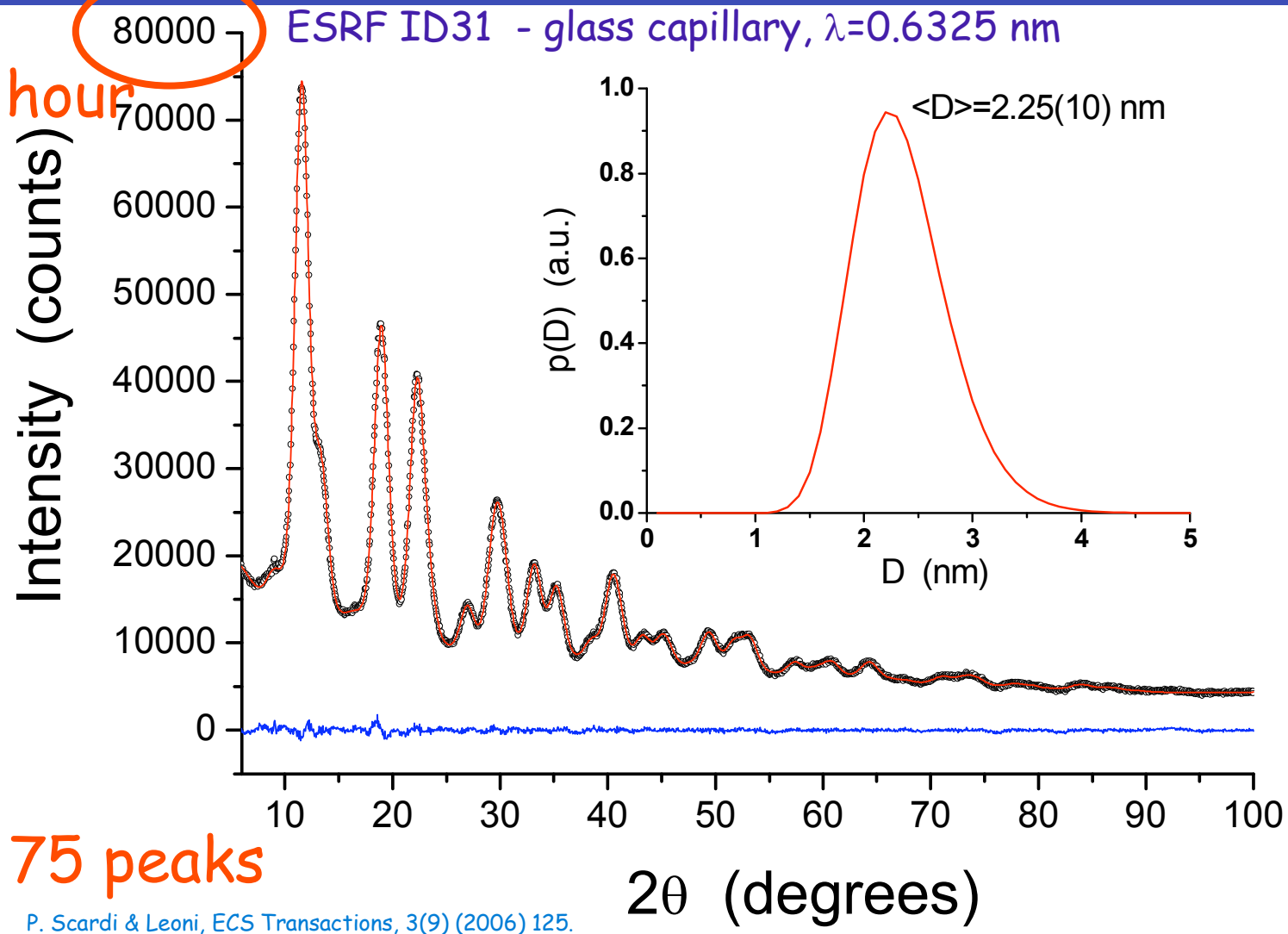




# WPPM APPLICATIONS: NANOCRYSTALLINE CERIA

Xerogel obtained by vacuum-drying: broad diffraction lines of nanocrystalline fcc phase

0.8 hour

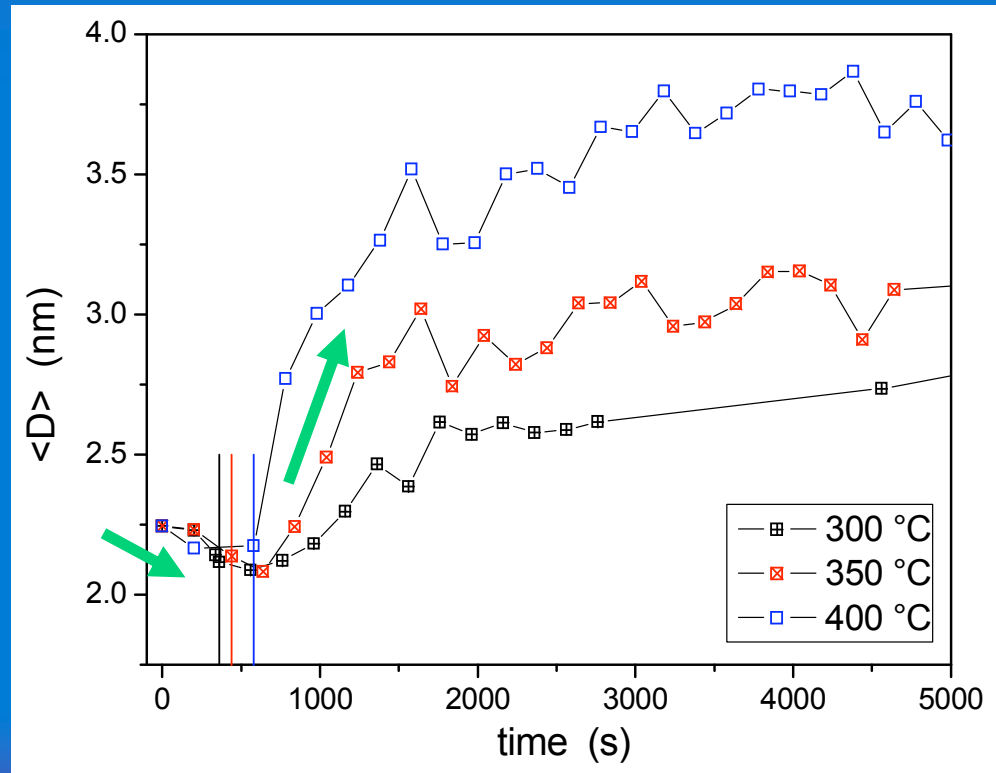




# WPPM APPLICATIONS: NANOCRYSTALLINE CERIA

Evolution of line profiles during isothermal treatment: 300°C, 350°C, 400°C

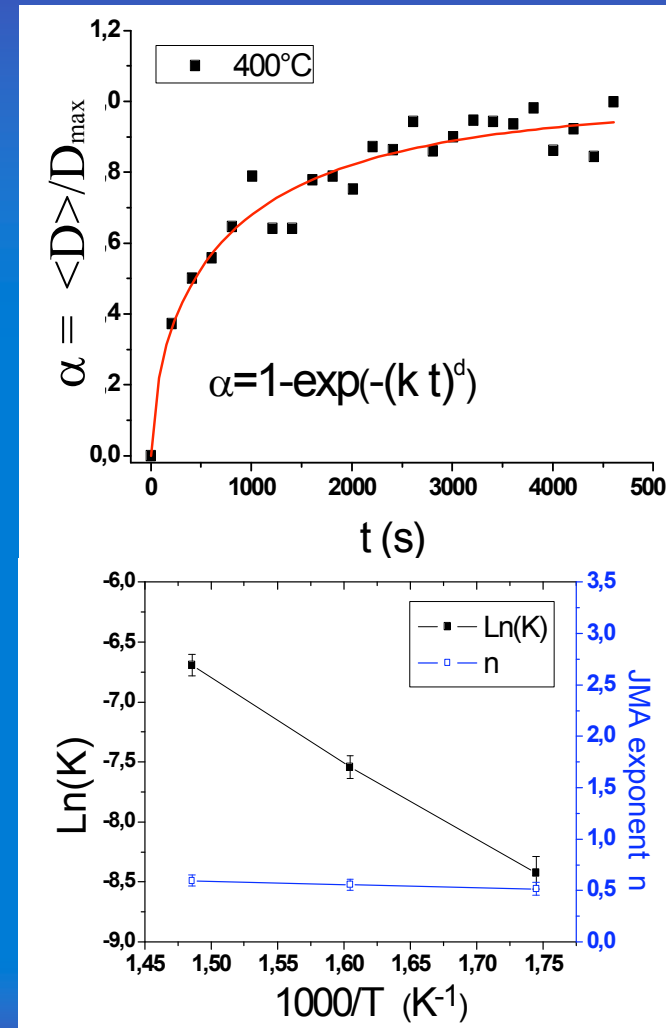
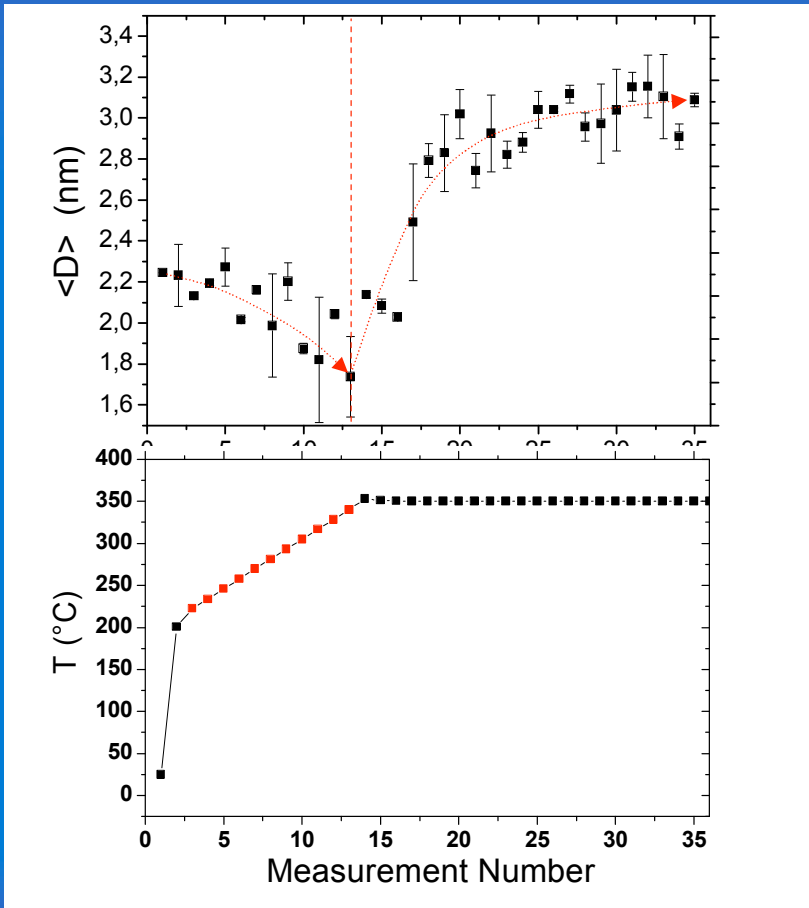
High temperature blower on ID31 at ESRF





# WPPM APPLICATIONS: NANOCRYSTALLINE CERIA

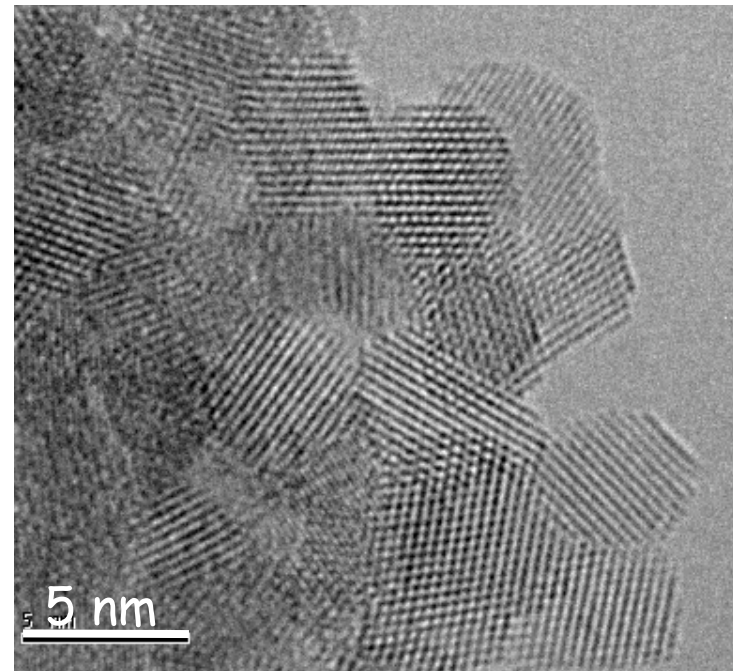
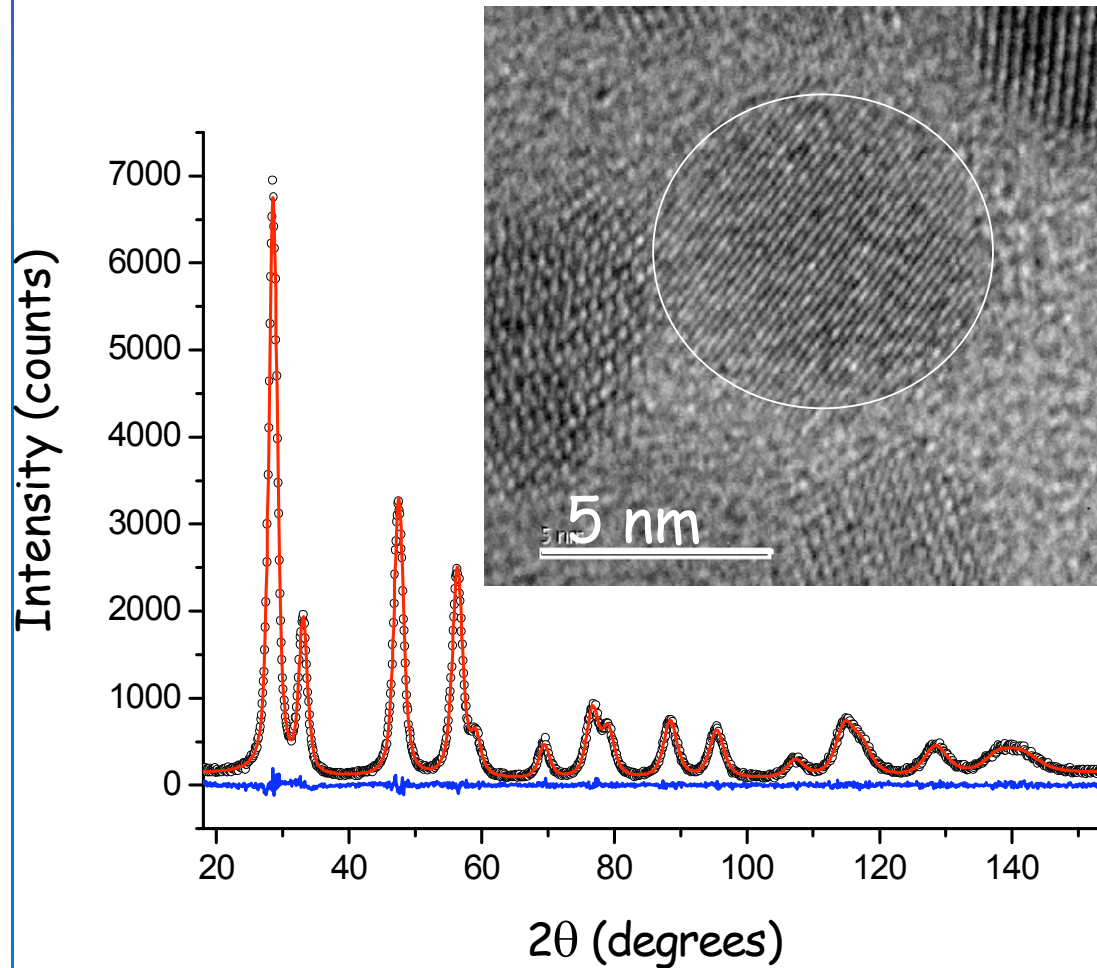
Nucleation during the heating stage: mean domain size initially decreases, before the grain growth starts





# WPPM APPLICATIONS: NANOCRYSTALLINE CERIA

## Heat treated 1h @ 400°C



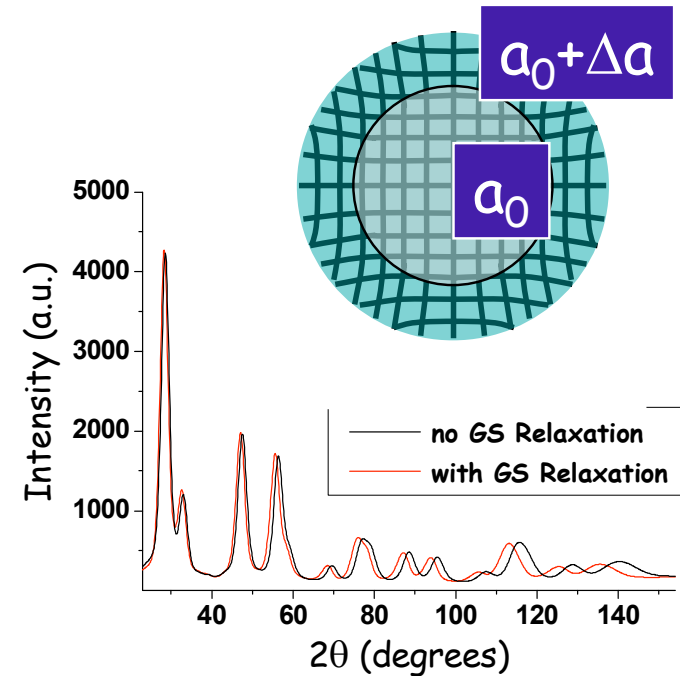
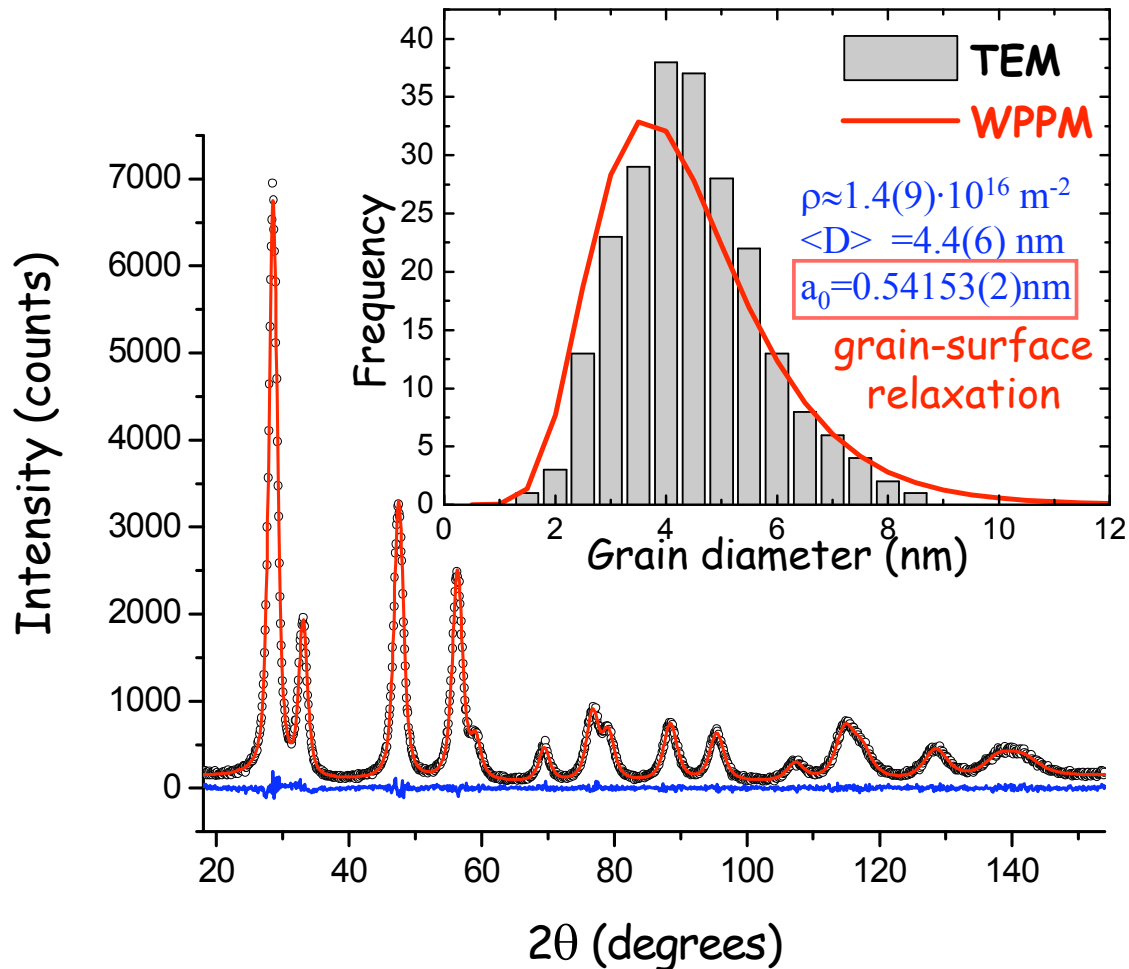
M. Leoni & P. Scardi, in *Diffraction Analysis of Materials Microstructure*. E.J. Mittemeijer & P. Scardi, editors. Berlin: Springer-Verlag, 2004





# WPPM APPLICATIONS: NANOCRYSTALLINE CERIA

## Heat treated 1h @ 400°C

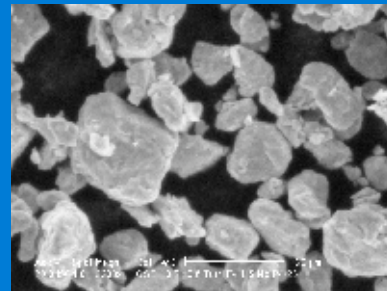


M. Leoni & P. Scardi, in *Diffraction Analysis of Materials Microstructure*. E.J. Mittemeijer & P. Scardi, editors. Berlin: Springer-Verlag. 2004



# WPPM APPLICATIONS: NANOCRYSTALLINE CERIA

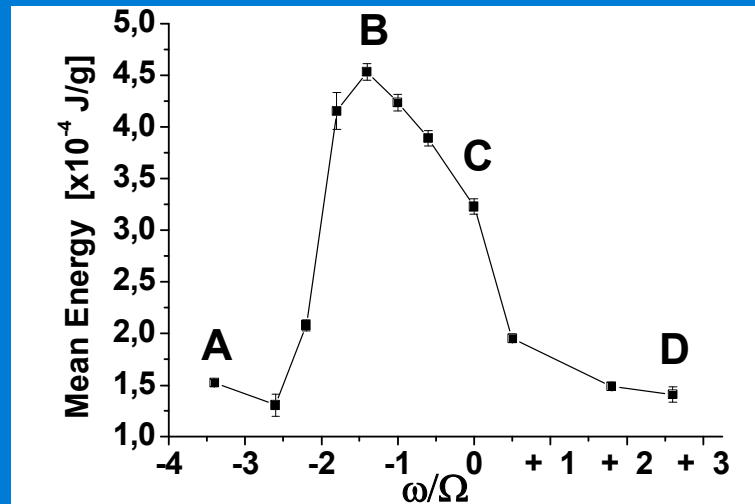
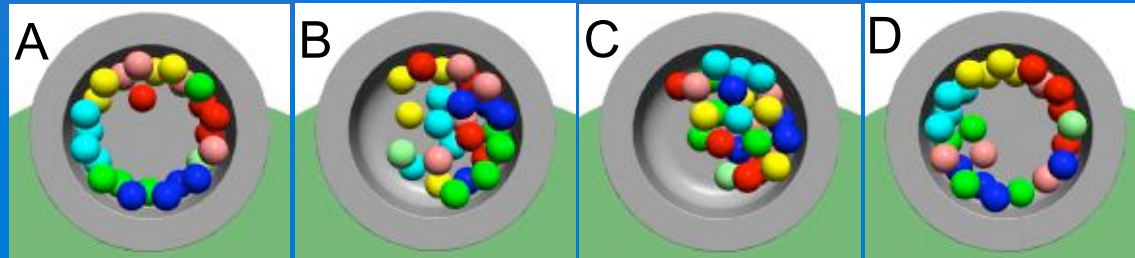
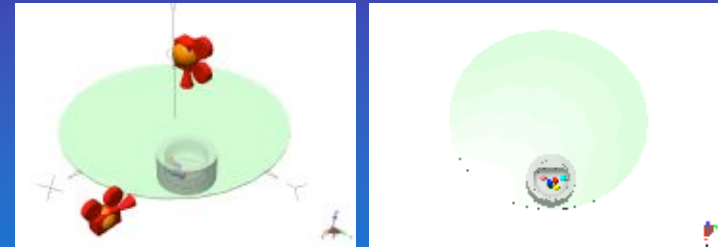
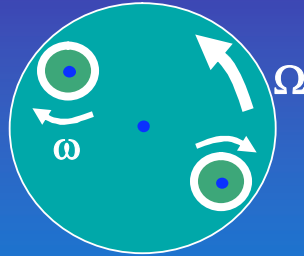
## Highly-energy mechanical grinding ball-milled Fe-1.5%Mo





# NANOCRYSTALLINE Fe-1.5%Mo POWDER

## Planetary ball mill - process modelling & production

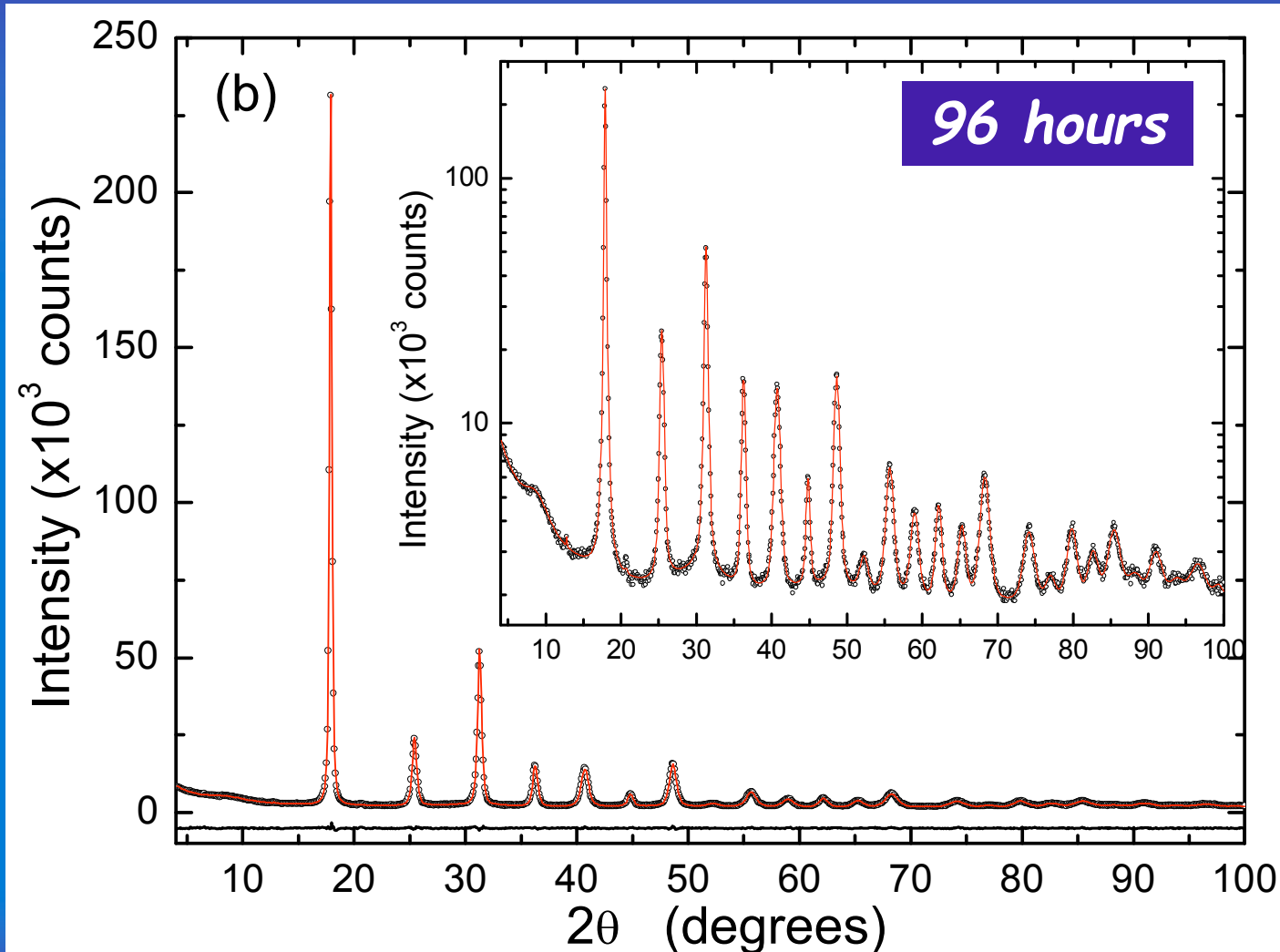


M. d'Incau, Leoni & P. Scardi, *J. Materials Research* 22 (2007) 1744-1753.



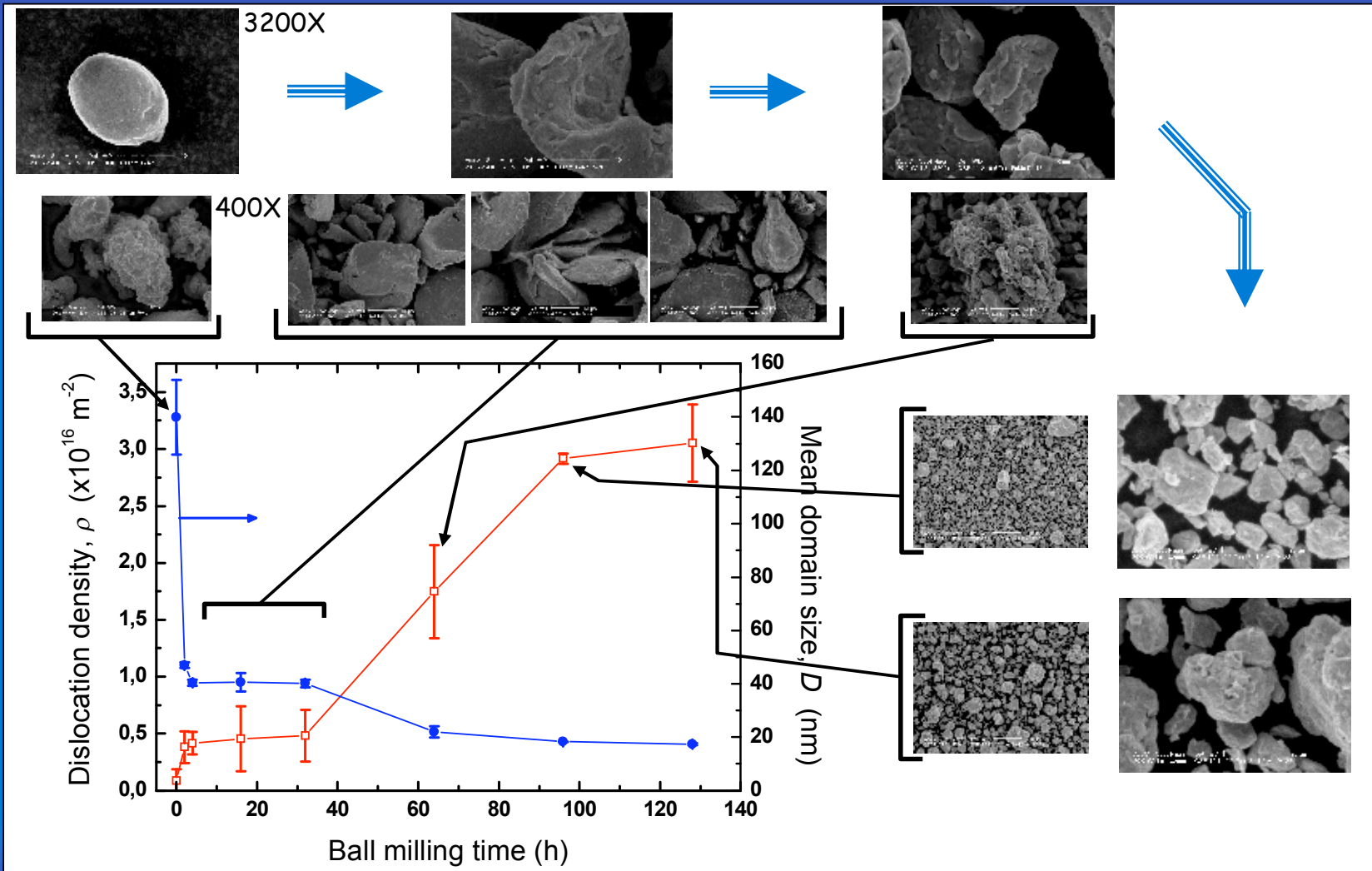
# NANOCRYSTALLINE Fe-1.5%Mo POWDER

Ball milled Fe1.5Mo (Fritsch P4) - data collected at ESRF - ID31  $\lambda=0.0632$  nm



# NANOCRYSTALLINE Fe-1.5%Mo POWDER

Ball milled Fe1.5Mo (Fritsch P4) - data collected at ESRF - ID31  $\lambda=0.0632$  nm  
 dislocation density/domain size vs. morphology





# NANOCRYSTALLINE Fe-1.5%Mo POWDER

Ball milled Fe1.5Mo (Fritsch P4) - data collected at **ESRF - ID31**  $\lambda=0.0632$  nm  
 dislocation density/domain size vs. morphology

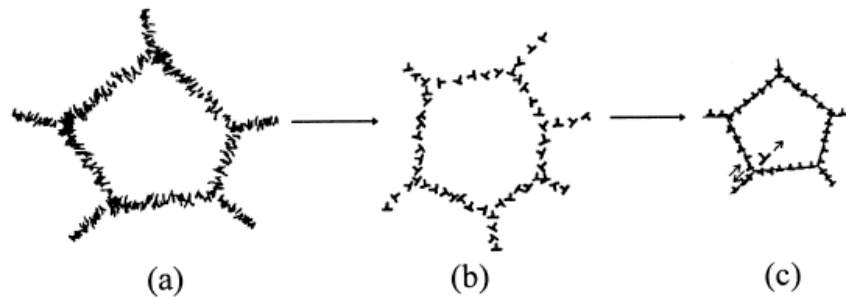


Fig. 15. Schematic model of dislocation structure evolution at different stages during severe plastic deformation.

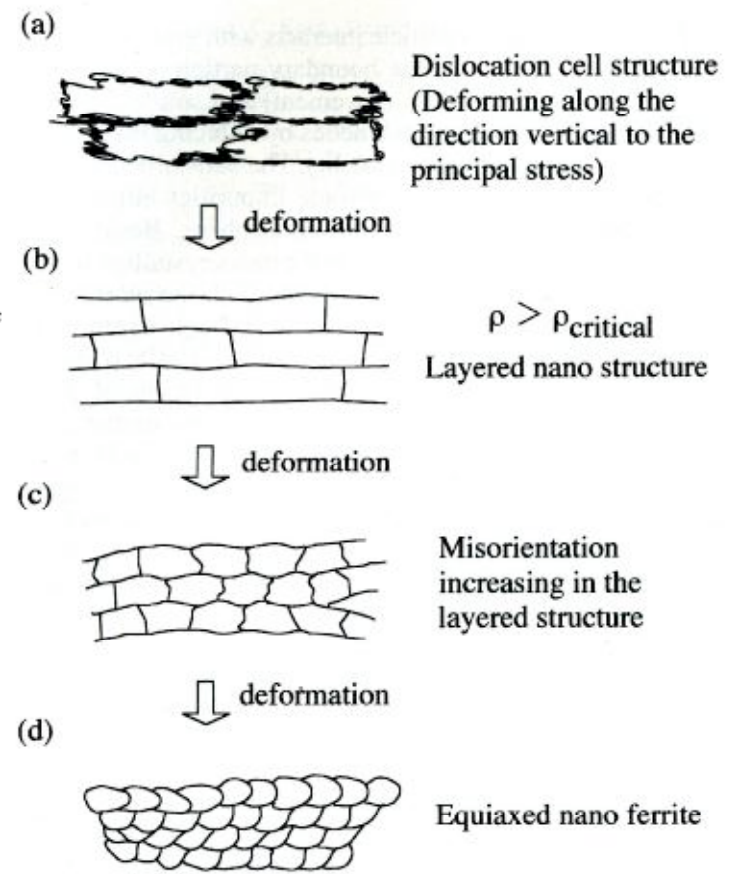
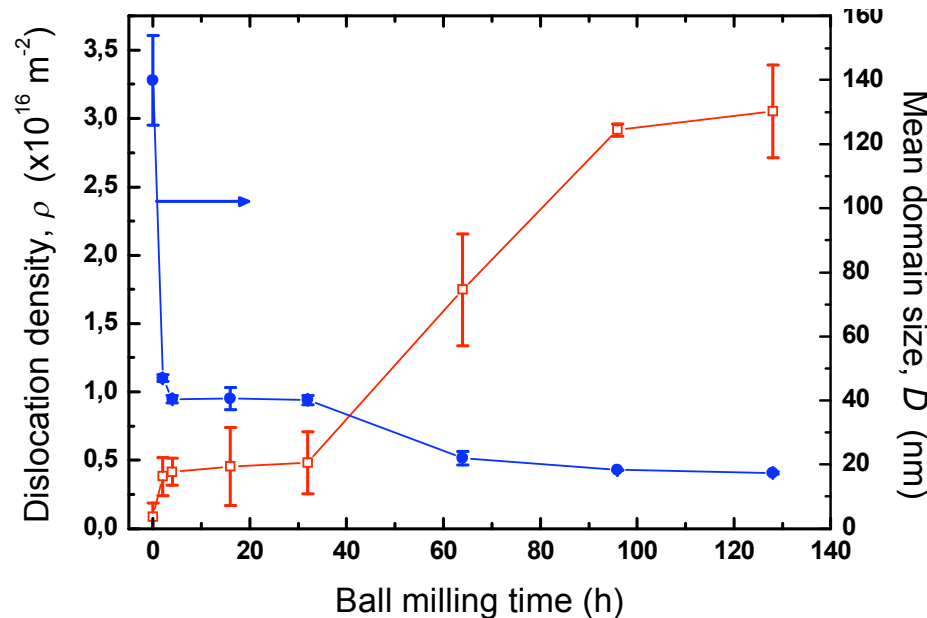


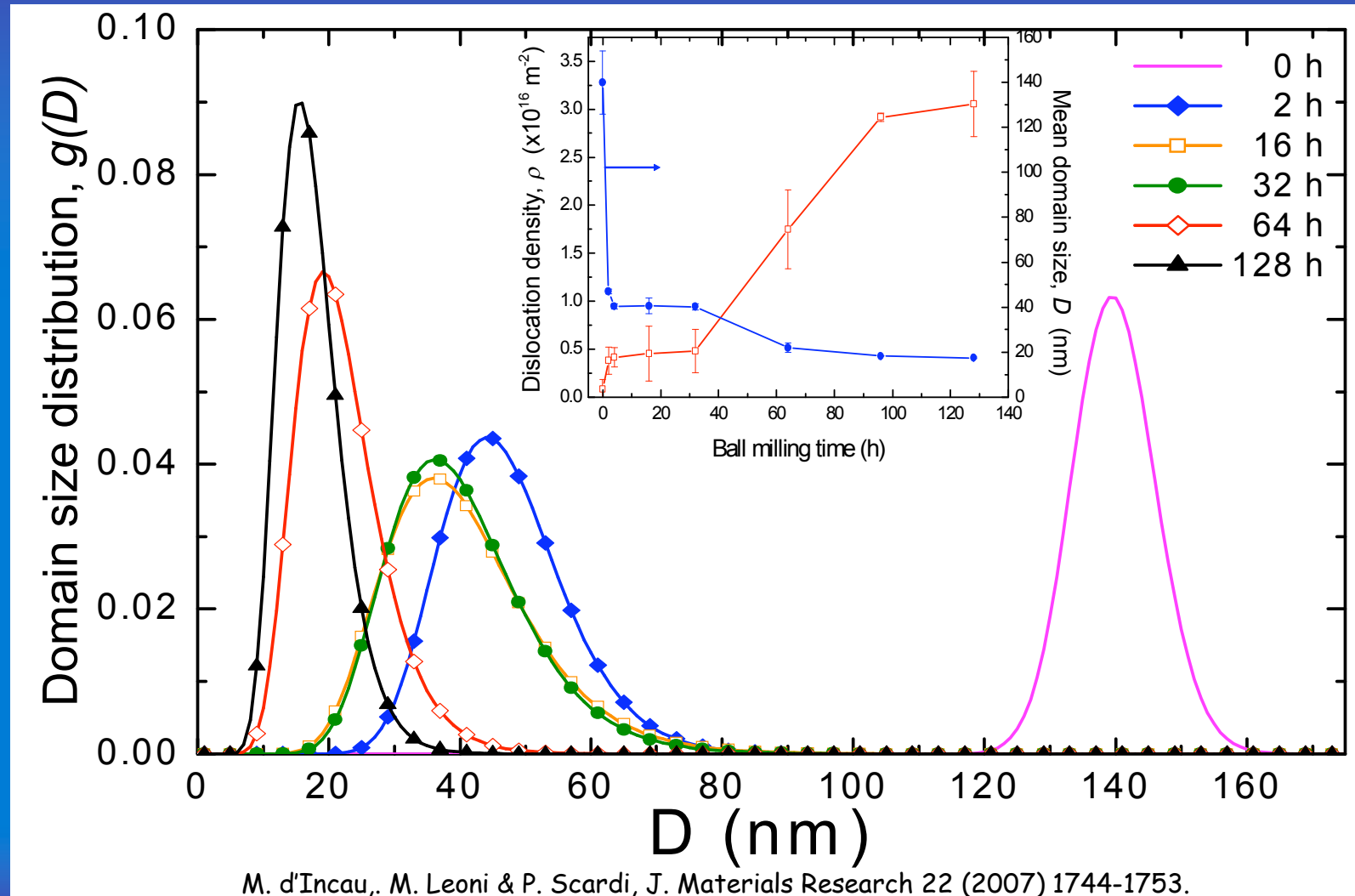
Fig. 11—(a) through (d) A schematic drawing of nanocrystalline ferrite formation by ball milling.



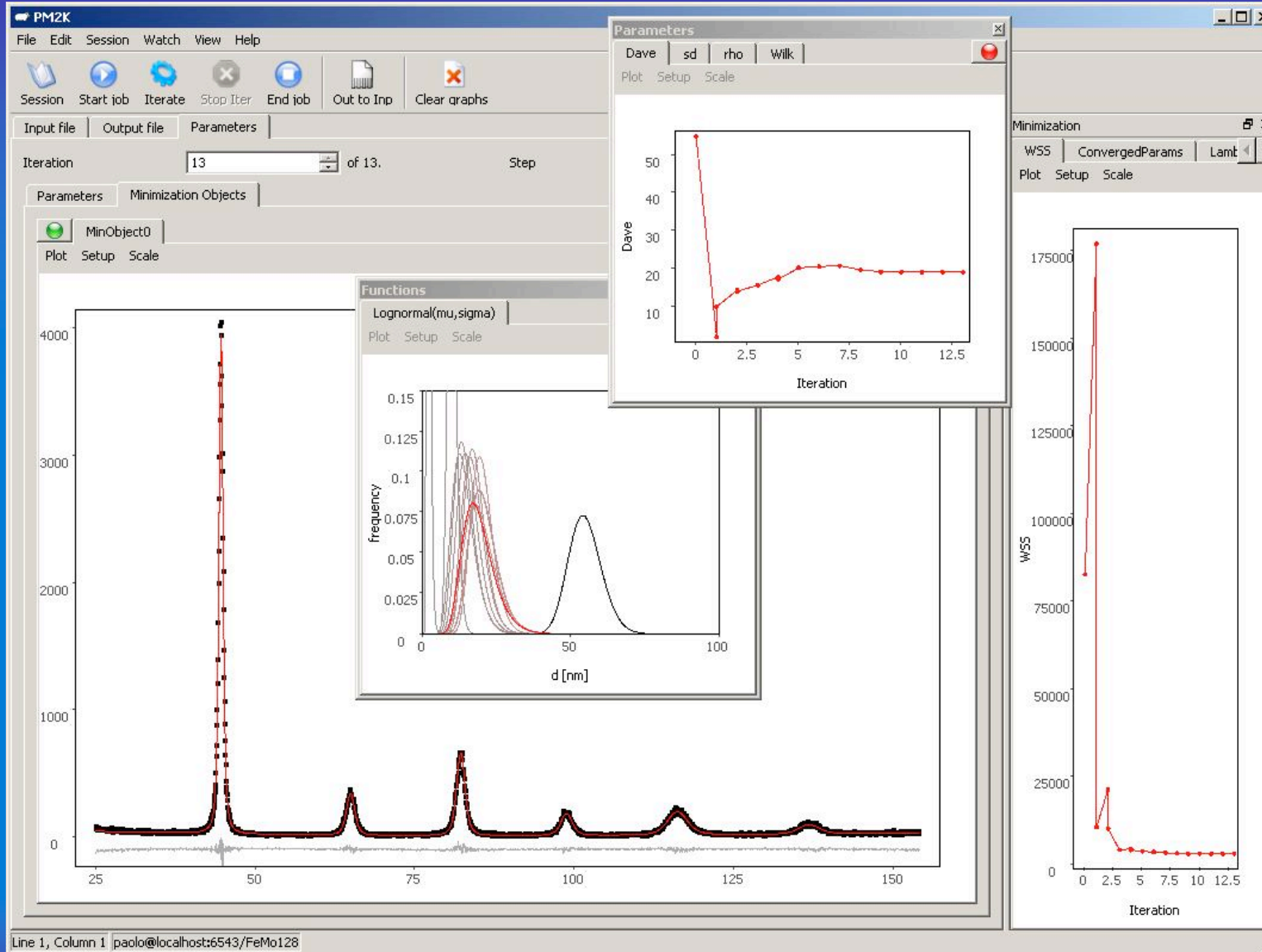
# NANOCRYSTALLINE Fe-1.5%Mo POWDER

Ball milled Fe1.5Mo (Fritsch P4) - data collected at ESRF - ID31  $\lambda=0.0632$  nm

In addition to mean values, WPPM provides the size distribution



M. d'Incau, M. Leoni & P. Scardi, J. Materials Research 22 (2007) 1744-1753.







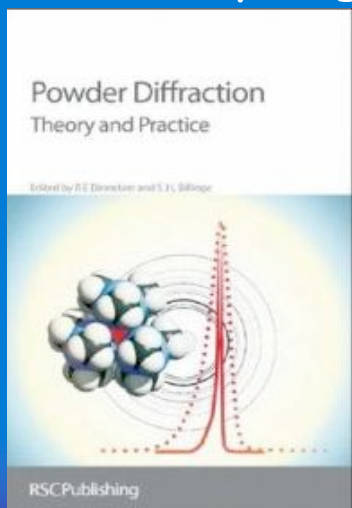
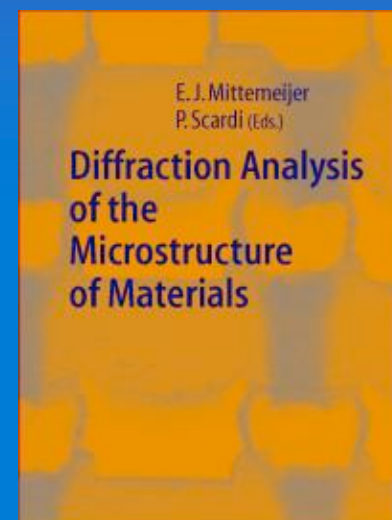
## PART 2: REFERENCES - Paolo.Scardi@unitn.it

- P.Scardi & M. Leoni, *Acta Cryst. A* 57 (2001) 604
- P.Scardi & M. Leoni, *Acta Cryst. A* 58 (2002) 190
- P.Scardi, M. Leoni, R. Delhez *J. Appl. Cryst.* 37 (2004) 381
- M. Leoni, P. Scardi *J. Appl. Cryst.* 37 (2004) 629
- P. Scardi & M. Leoni, *Acta Mater.* 53 (2005) 5229.
- P. Scardi & M. Leoni *J. Appl. Cryst.* 39 (2006) 24.

### *Diffraction Analysis of Materials Microstructure*

E.J. Mittemeijer & P. Scardi, editors.

Berlin: Springer-Verlag, 2004.



### *Powder Diffraction: Theory and Practice*

R.E. Dinnebier & S.J.L. Billinge, editors.

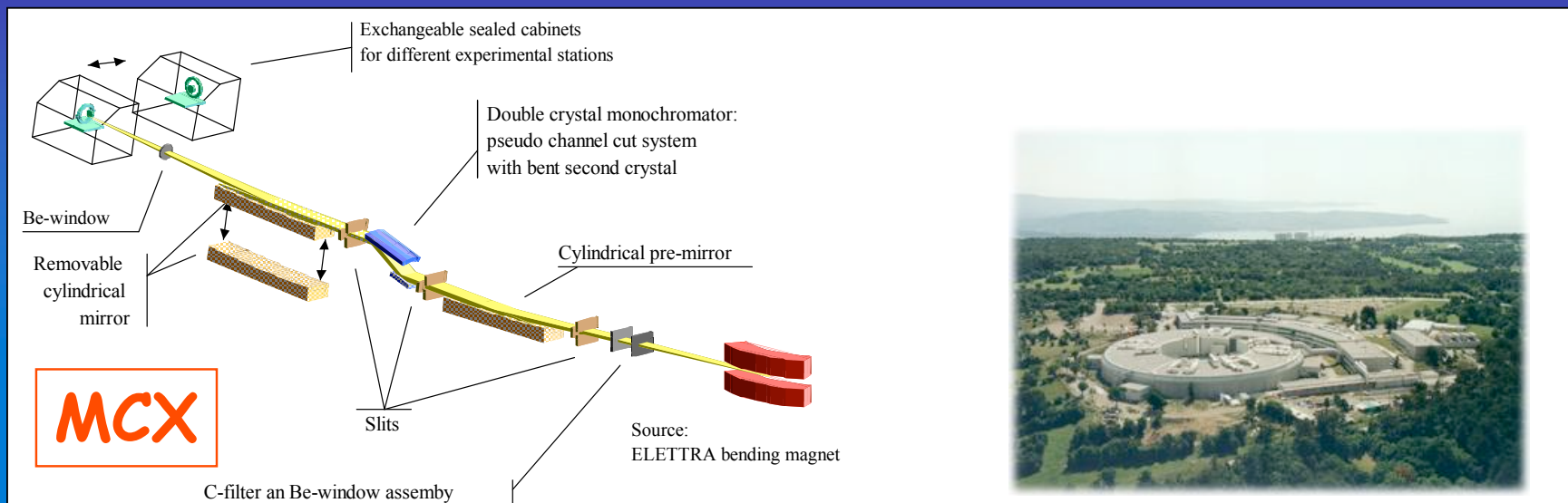
Cambridge: Royal Society of Chemistry, 2008.





## MCX - A new beamline for Materials Characterization by XRD at ELETTRA (Trieste, Italy)

G. Paolucci, E. Busetto, A. Lausi, J. Plasier (Sincrotrone Trieste), P. Scardi (Univ. Trento & INSTM)



## Examples of typical applications

- Residual stress and texture analysis in thin films by multiple wavelength XRD
- Surface analysis by grazing incidence XRD and reflectivity
- Medium-low energy (3.5÷20 keV) anomalous scattering XRD
- Line Profile Analysis (e.g., nanocrystalline, highly defected materials)
- Non-ambient studies (controlled atmosphere, high temperature kinetics)
- Surface mapping by microdiffraction (diffraction on small area)

University of Trento

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*Information and applications:*

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