



The Abdus Salam
International Centre for Theoretical Physics



2167-27

Advanced School on Direct and Inverse Problems of Seismology

27 September - 8 October, 2010

**The study of fluid induced and triggered seismicity
Theory - 2**

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The study of fluid-induced and triggered seismicity: case studies

ICTP Course 2010

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Lecture B: case studies

I. Fluid injection and pore pressure diffusion

II. Hydro-fracturing & magma intrusions

- Gas field stimulation
- Long lasting intrusions

III. Gas field depletion and induced earthquakes

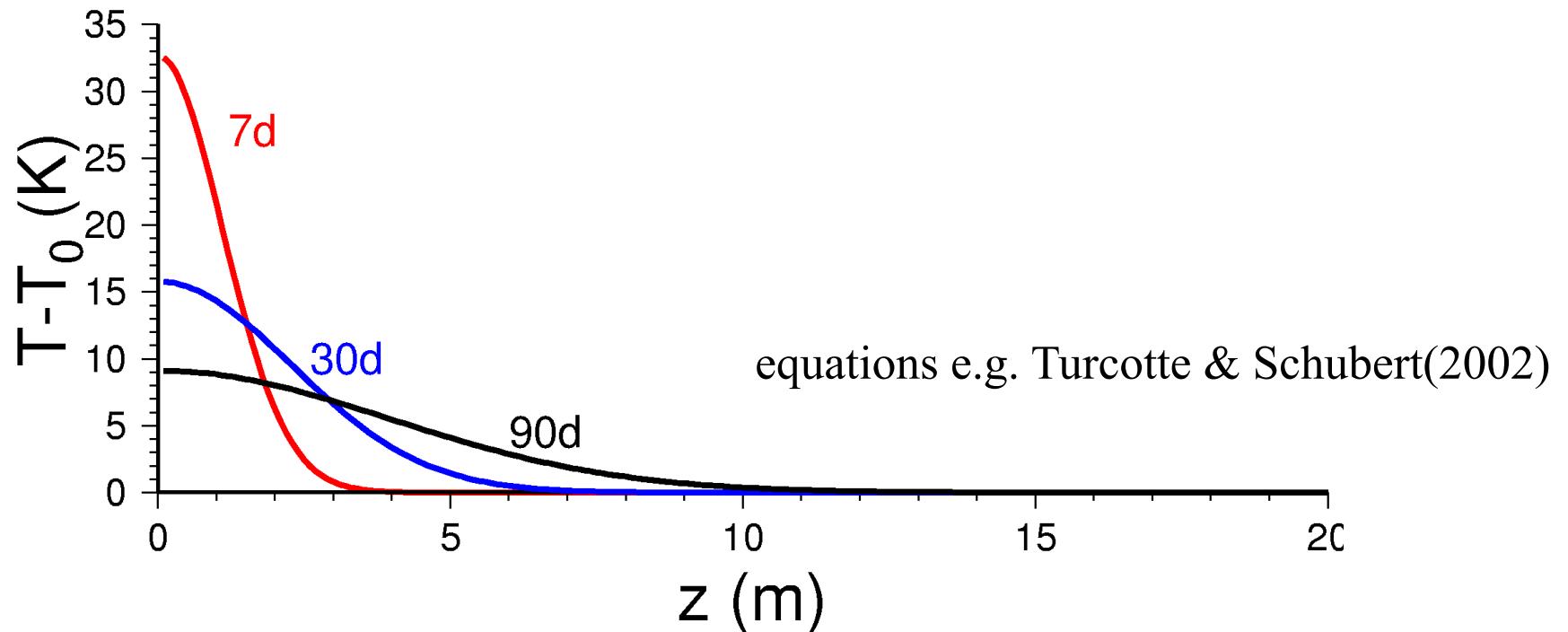


I) fluid & pore pressure diffusion

Examples:

- Denver 1962-1968: three $M>5$ events, 21 month after end of injection
- Chalia chemical waste disposal 1972-1985, $M5$ event 12 km south of well 14 years after injection
- Ashtabula, Ohio, sequence 1987-2003, $M<4.3$, 9 years after end of injection

Example: Temperature-diffusion in salt mine

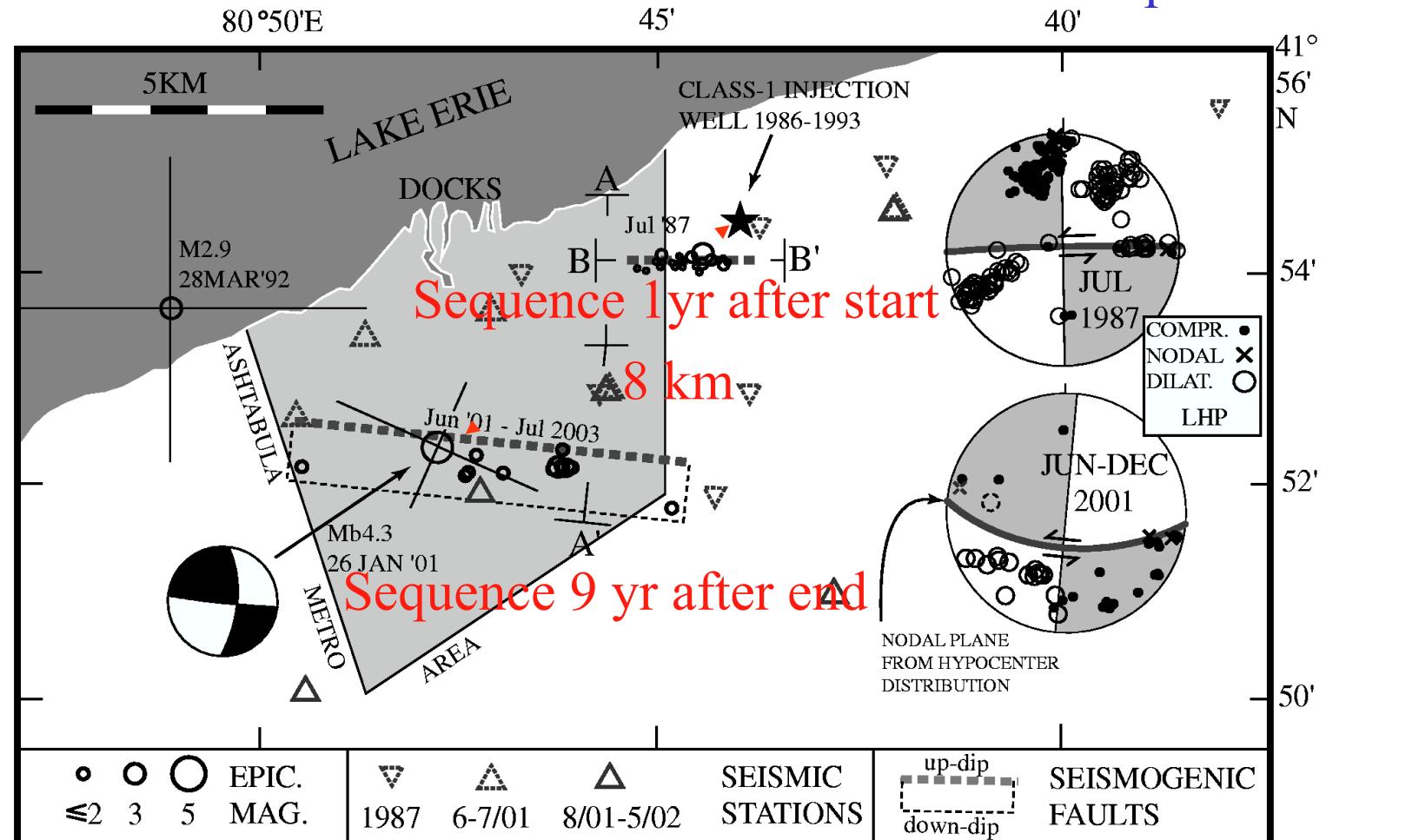


1-D Temperature diffusion after “heat injection” at plane $z=0$.

Temperature (and stress) slowly spreads out and “relaxes” at “injection point”

The same laws apply for fluid diffusion or for dissolution problems

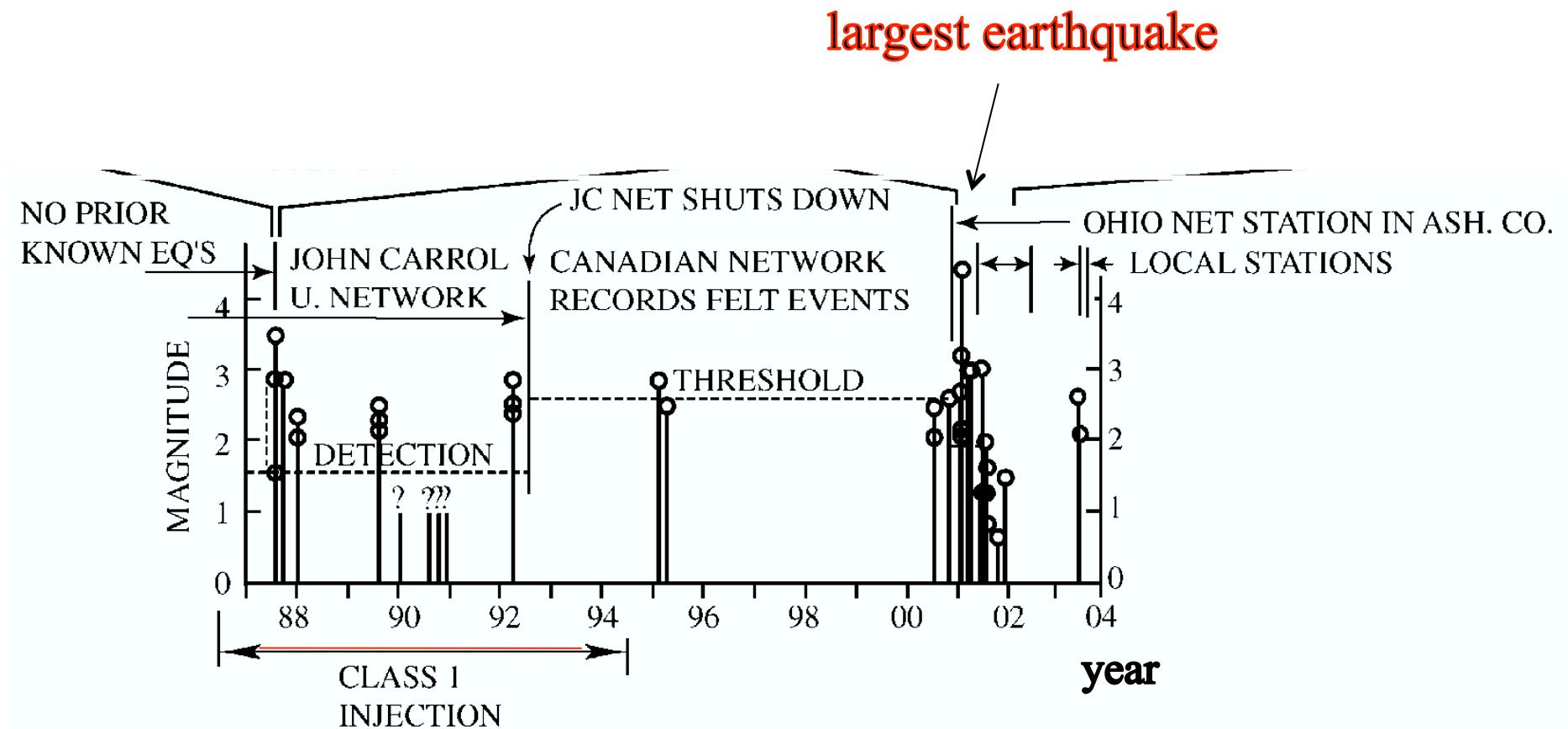
The Ashtabula, Ohio, sequence related
to waste fluid injection
into 1.8 km deep sandstone



Hypo depth in basement 2 km below
the injection layer

Seeber et al., 2004, BSSA 94, 76-87

Temporal evolution

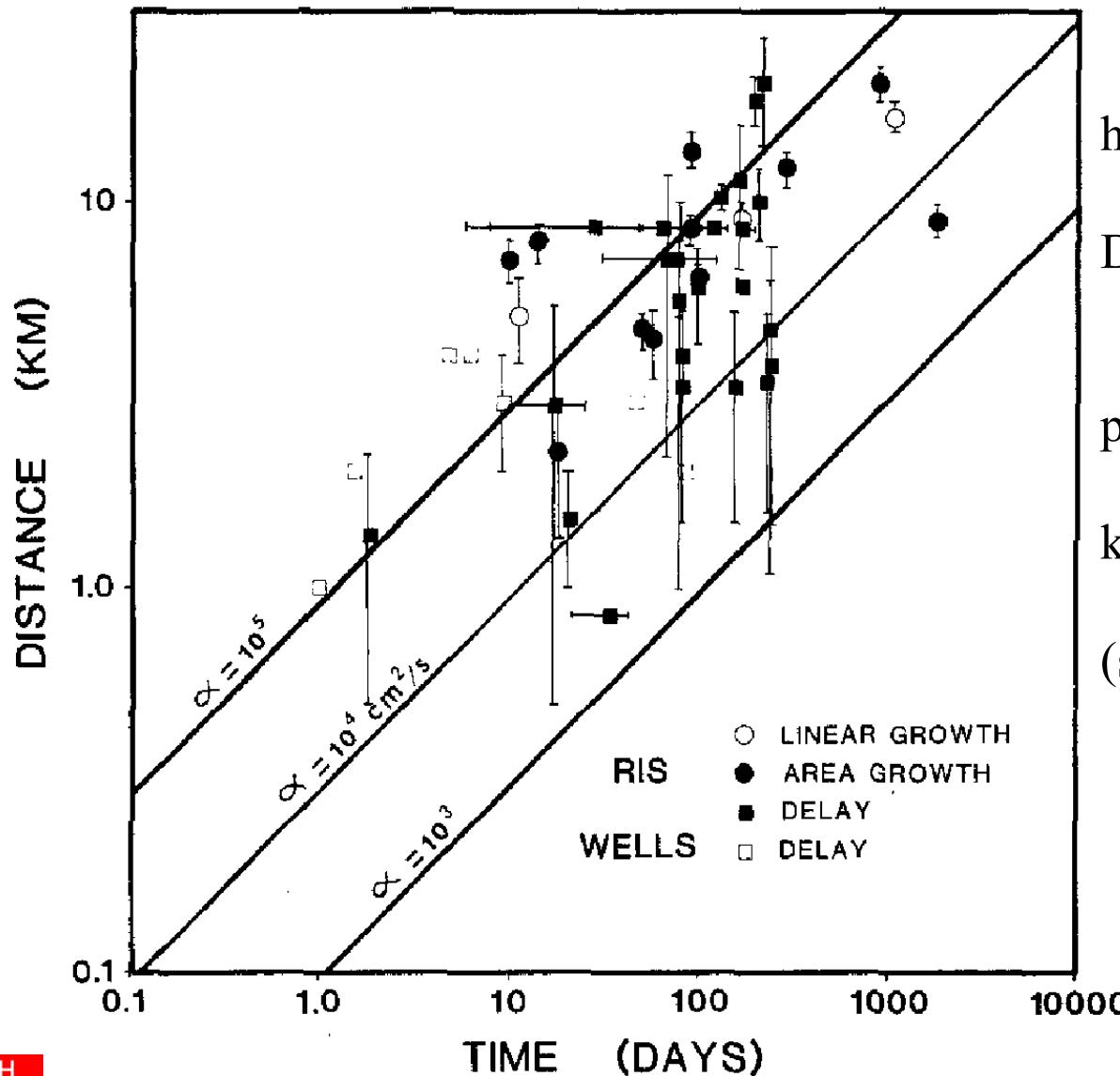


164 m³/day at 10 MPa (59.860 t/yr)

Seeber et al., 2004, BSSA 94, 76-87

Diffusivity: comparison of RIS and injection

Talwani & Acree (1985): PAGEOPH 122, 947-965



hydraulic diffusivity:

$$D \approx 1 - 10 \text{ m}^2 / \text{s}$$

permeability range:

$$k \approx 10^{-16} - 10^{-14} \text{ m}^2$$

(see Kümpel 1991 for formula)

Fluid-injection triggered events

1. Injection related pore pressure rise may trigger earthquakes (Coulomb failure)
2. Pore pressure decreases at the well after injection stops, but pressure front continuous to spread away from injection well for tens of years up to 8 - 14 km distance or more
3. Pore pressure transients can be simulated as diffusion process

Case II

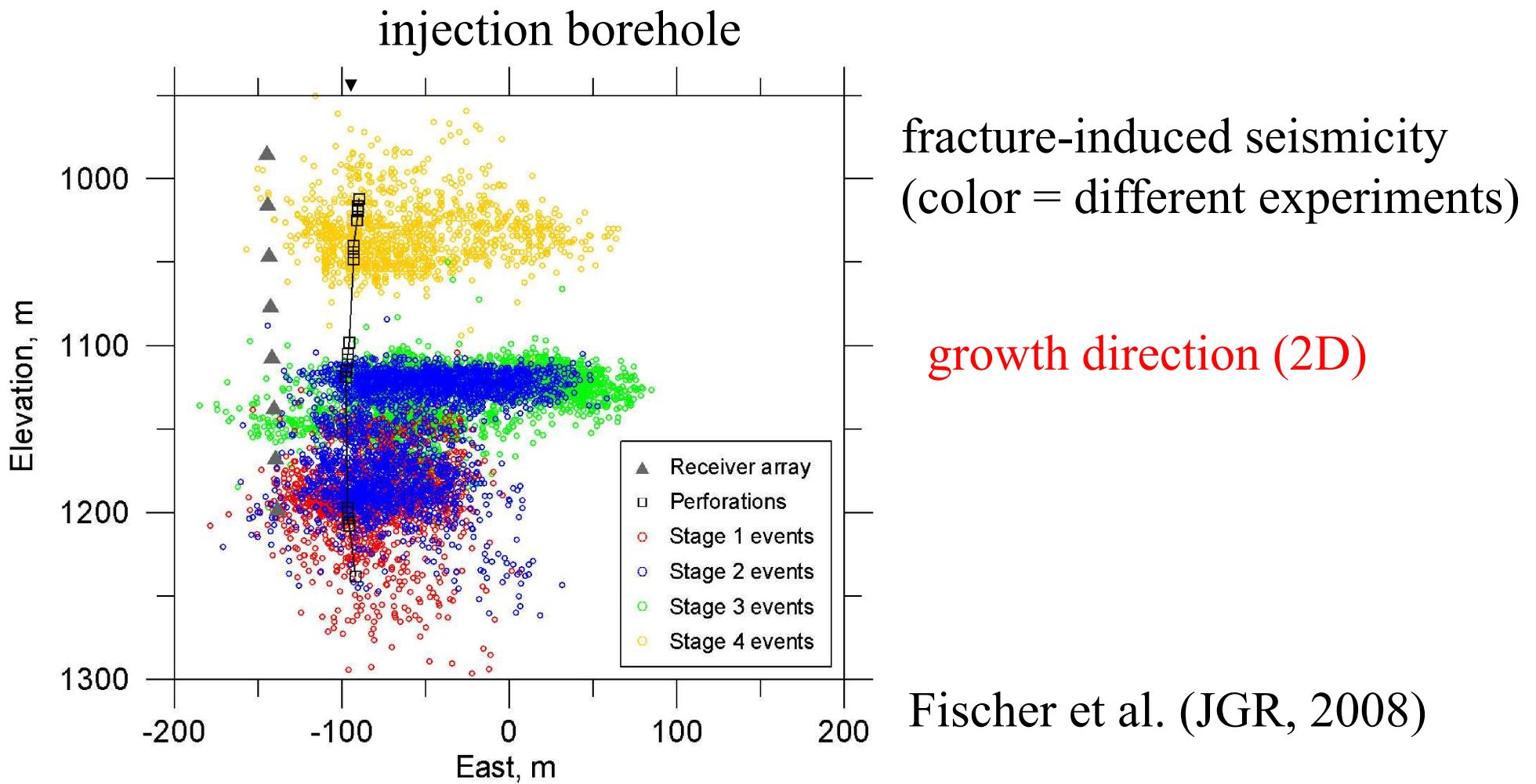
Hydrofracture induced seismicity



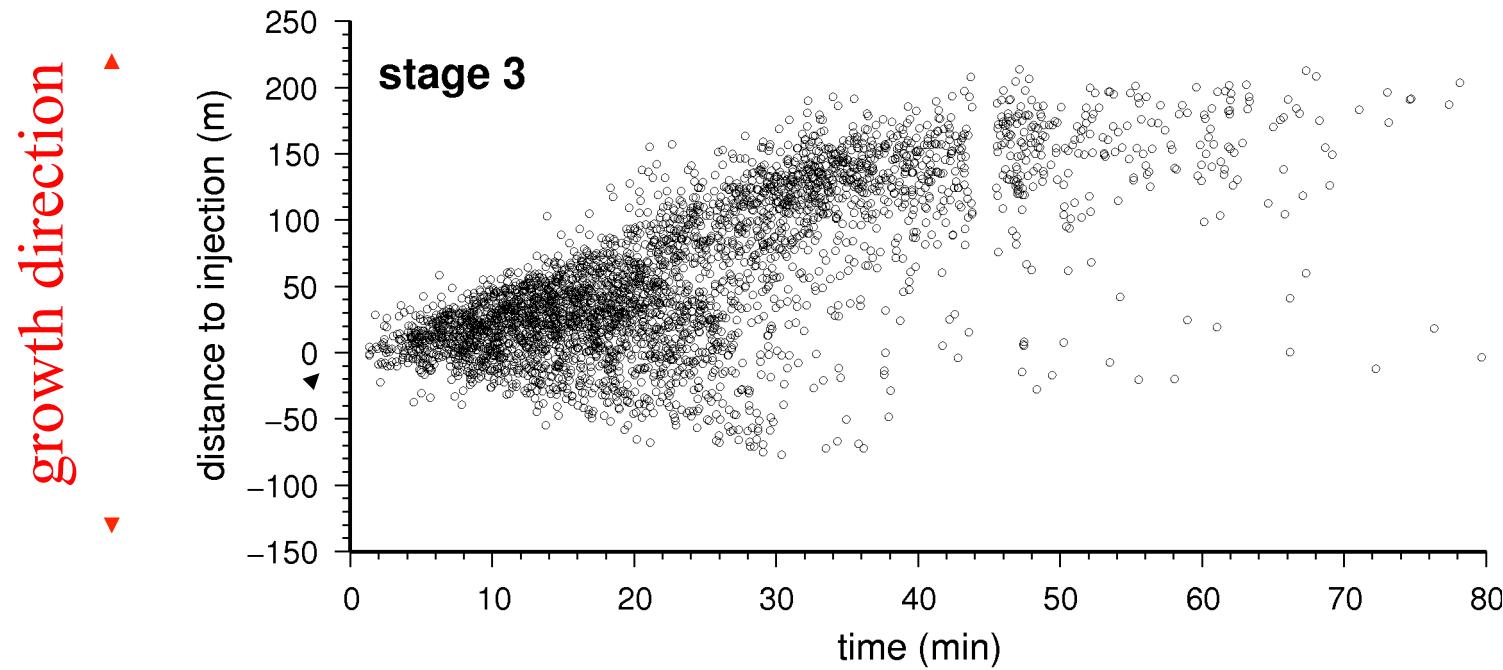
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Hydrofrac stimulations in Canyonsand gas field, W. Texas



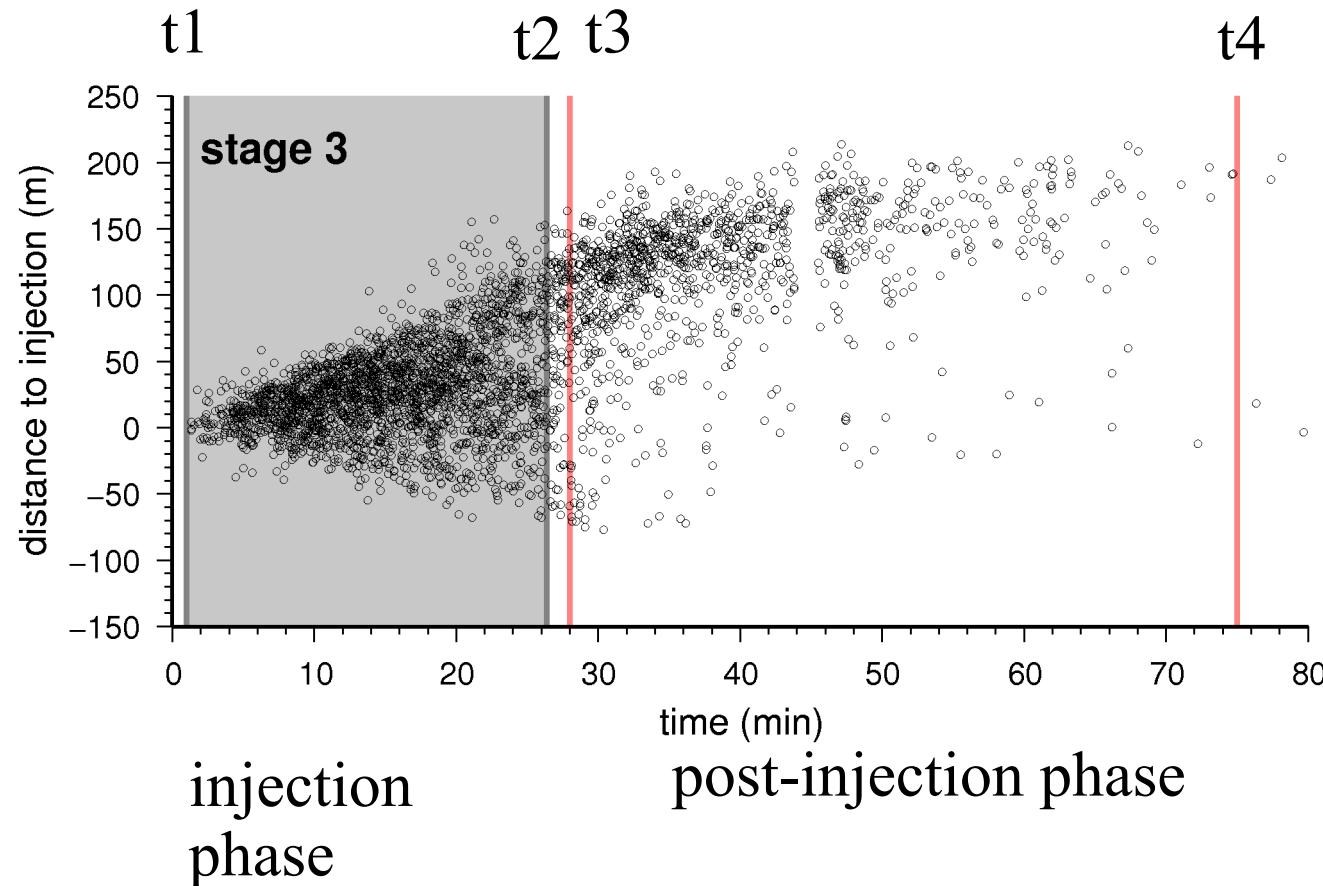
distance time plot, stage 3



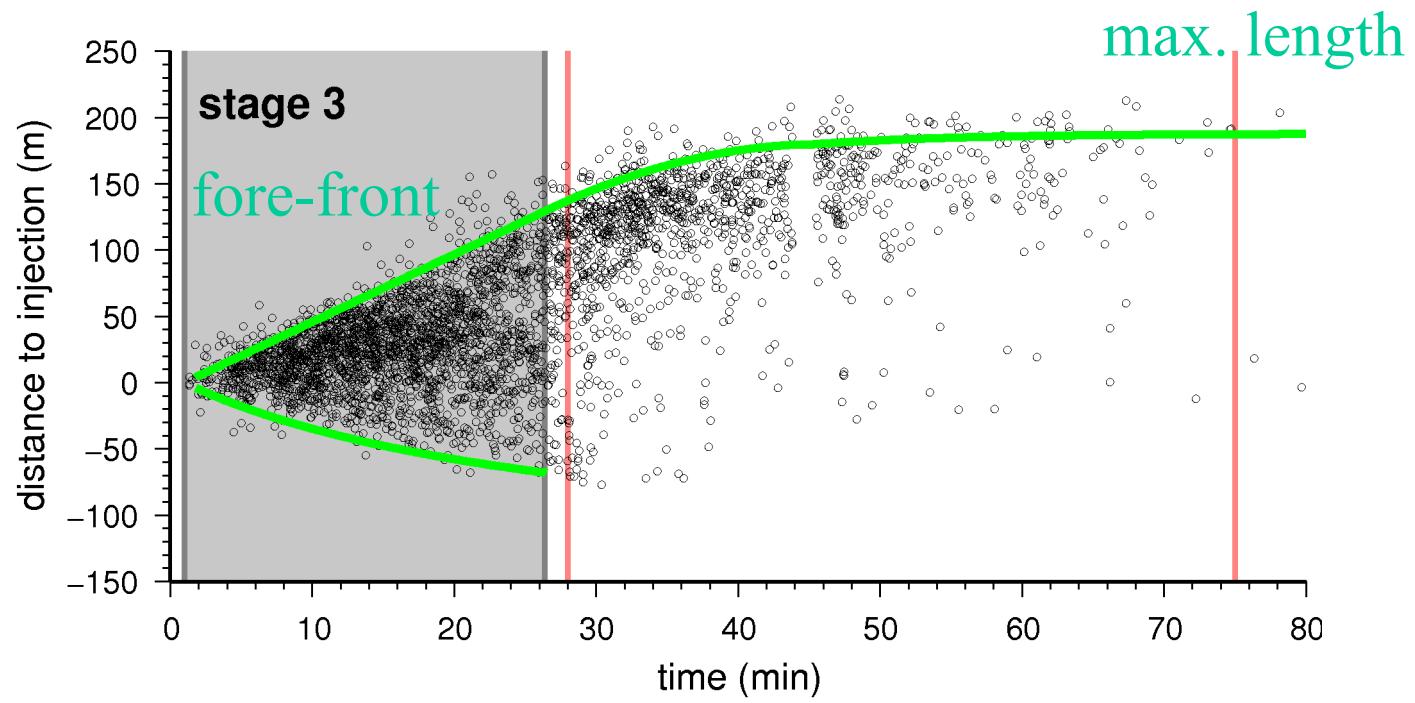
injection point



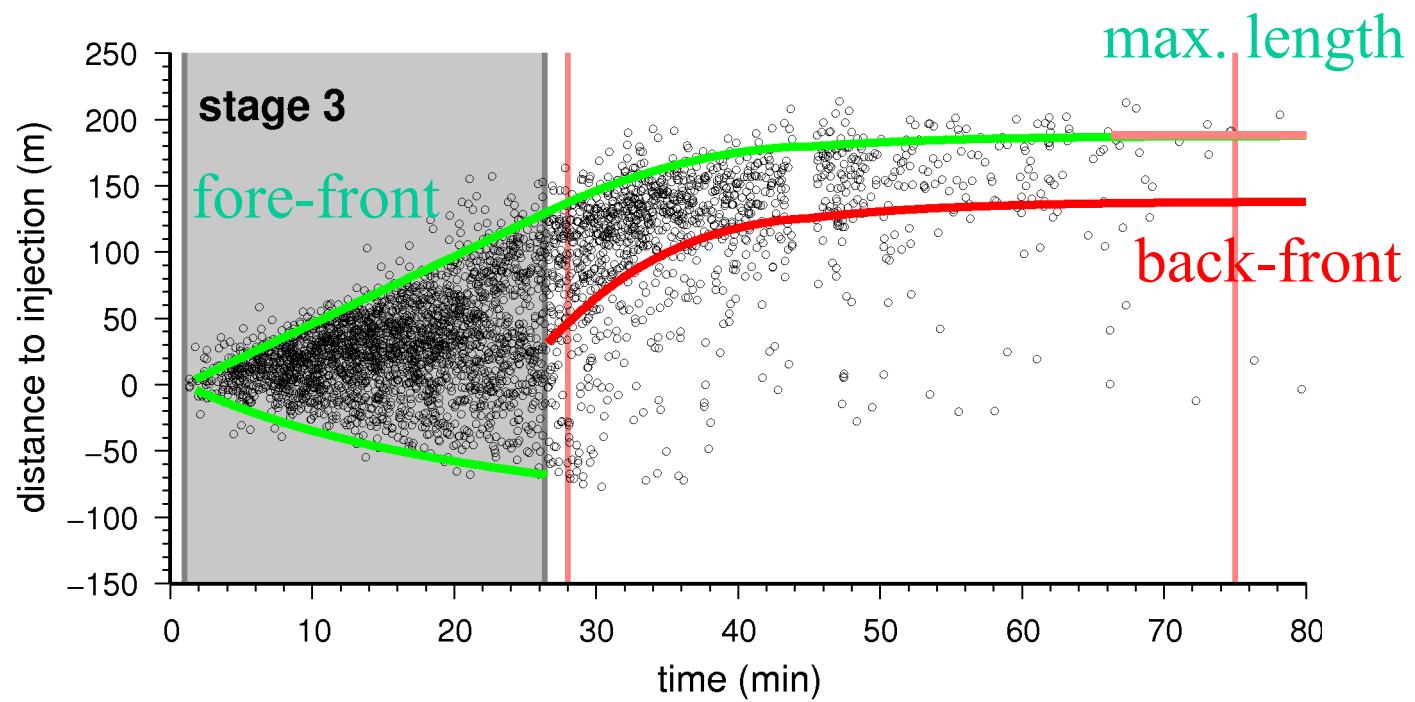
distance time plot, stage 3

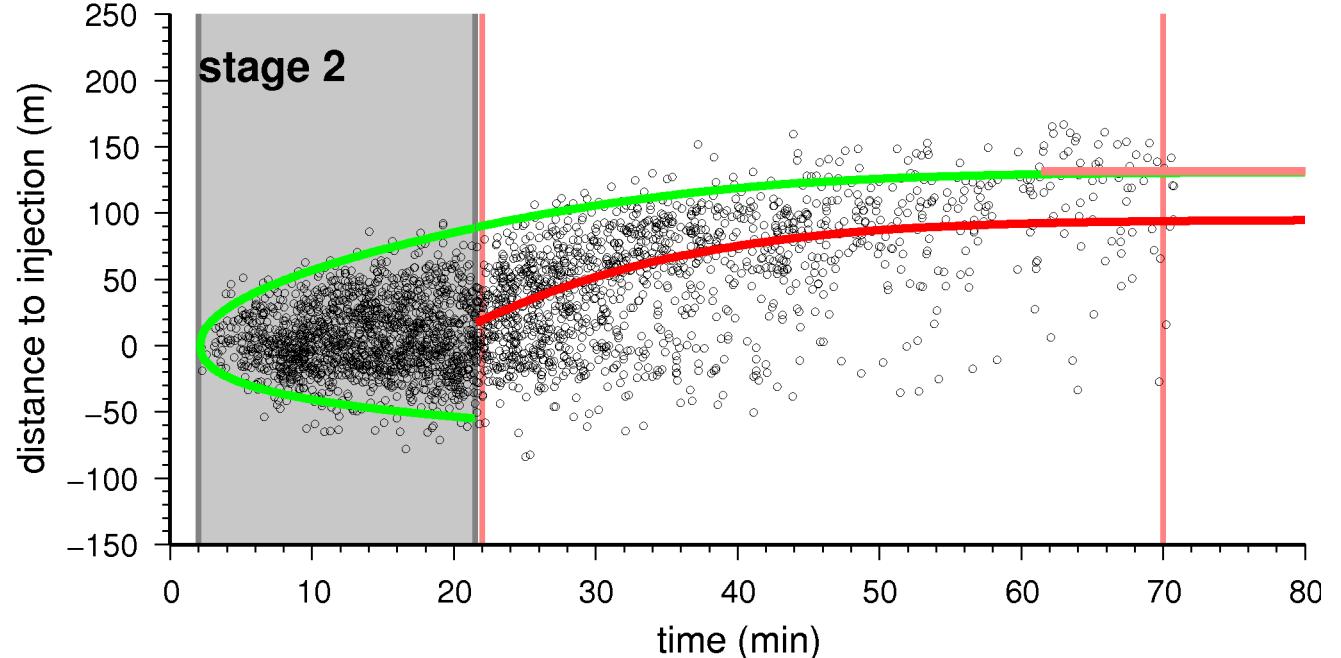


distance time plot, stage 3



distance time plot, stage 3





Hypotheses:

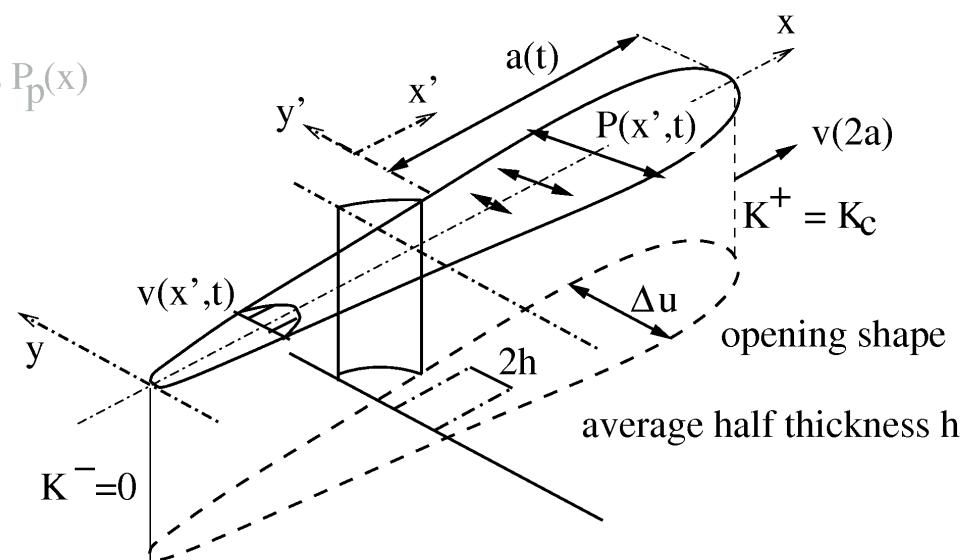
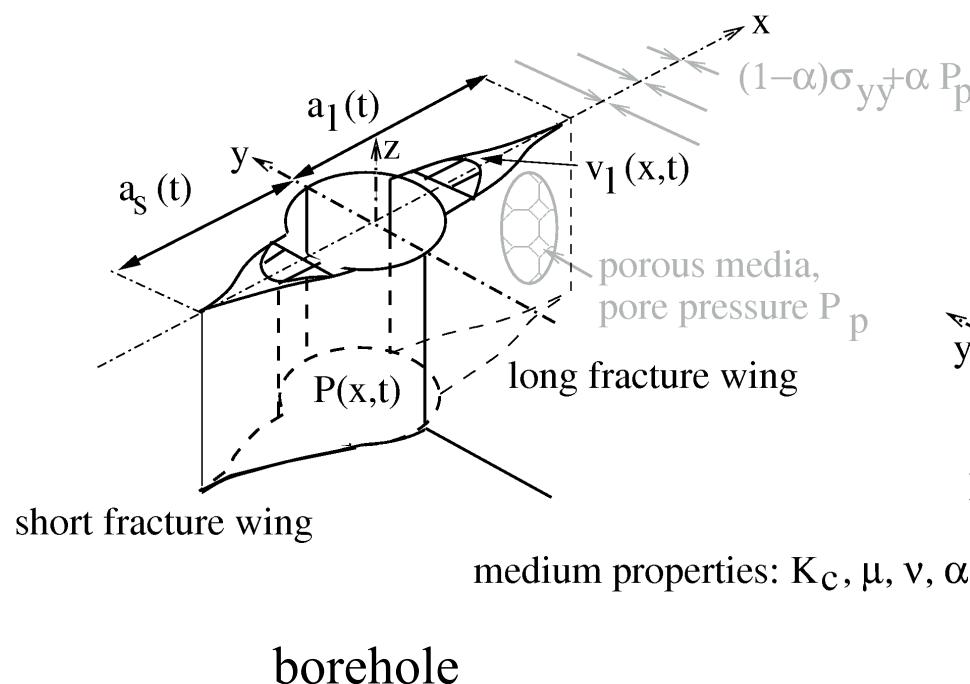
- a) Front and backfront are controlled by pressure diffusion (see RIS and waste fluid injection)
- b) Front- and backfront, asymmetric growth and intensity of seismicity are controlled by the shape of the fluid-filled fracture (e.g. Fischer, Hainzl and Dahm, 2009, Dahm et al., 2010)

I) Fracture model for asymmetric & unilateral growth

Injection, bilateral growth

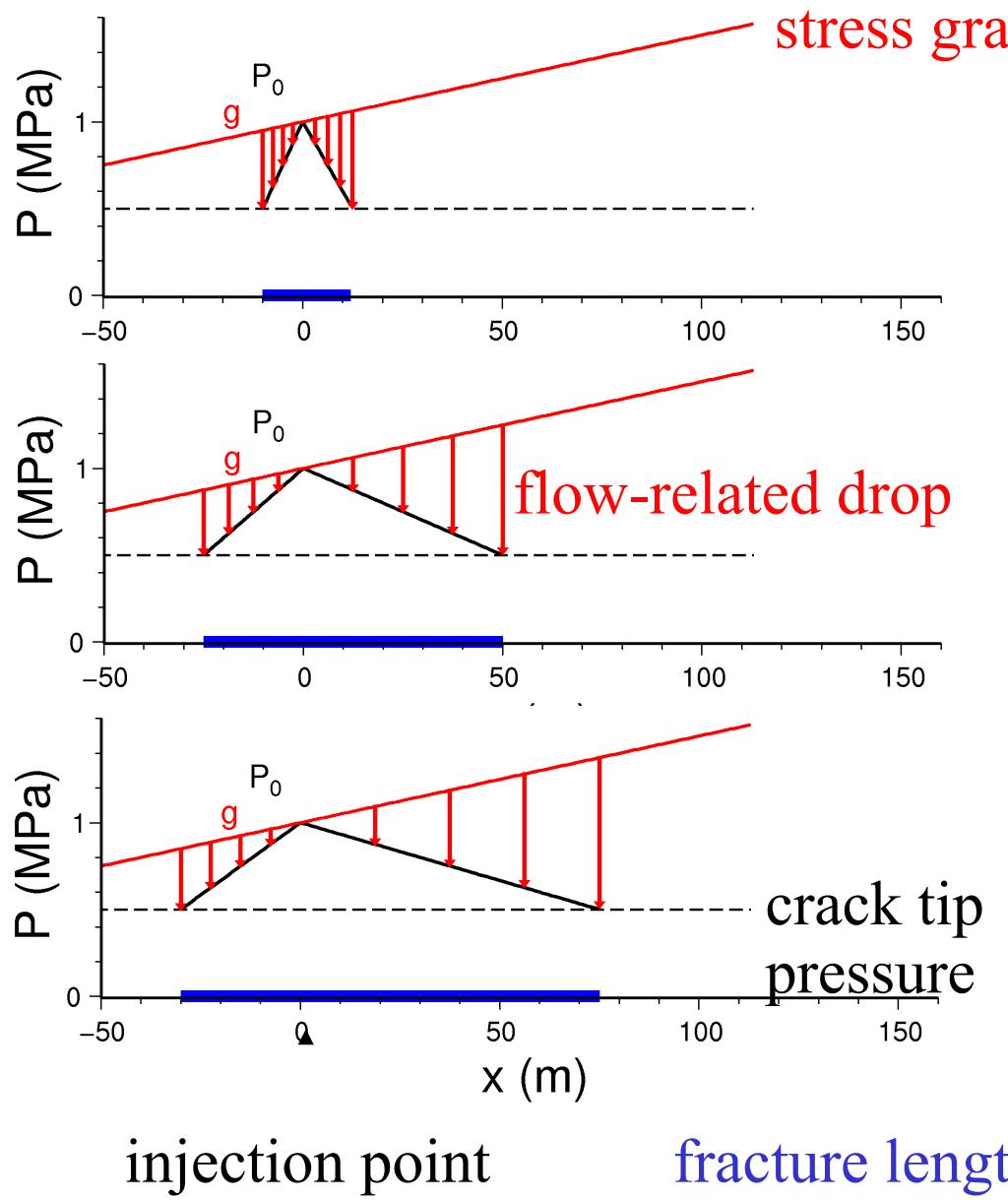
Post-injection, unilateral growth

growing style is controlled by stress gradient g !



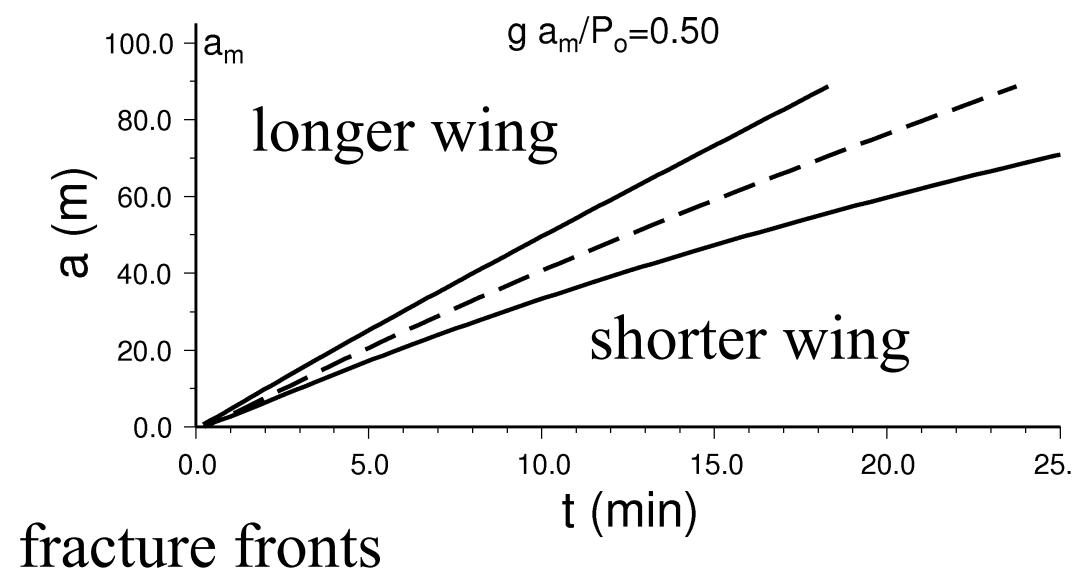
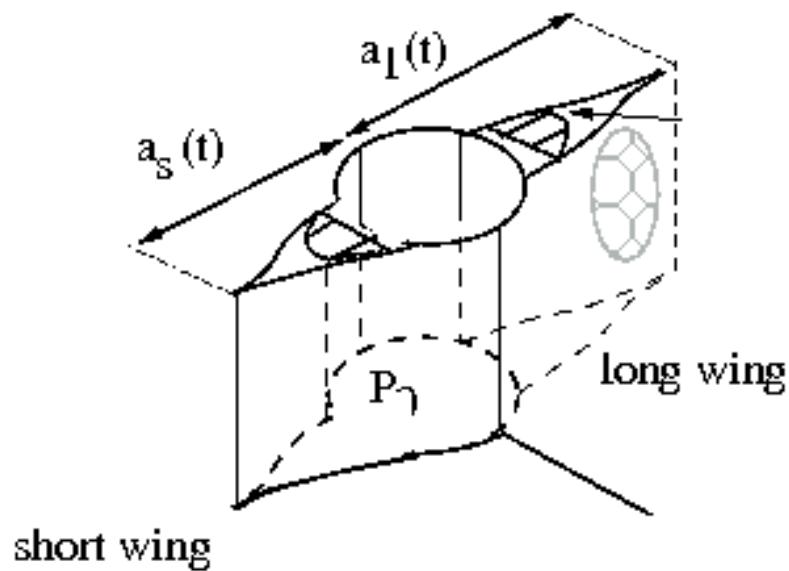
(Dahm, Hainzl and Fischer, JGR 2010)

Injection phase: driving pressure and flow



- asymmetric bilateral growth
- tip grow velocity decreasing with length

Asymmetric growth during injection



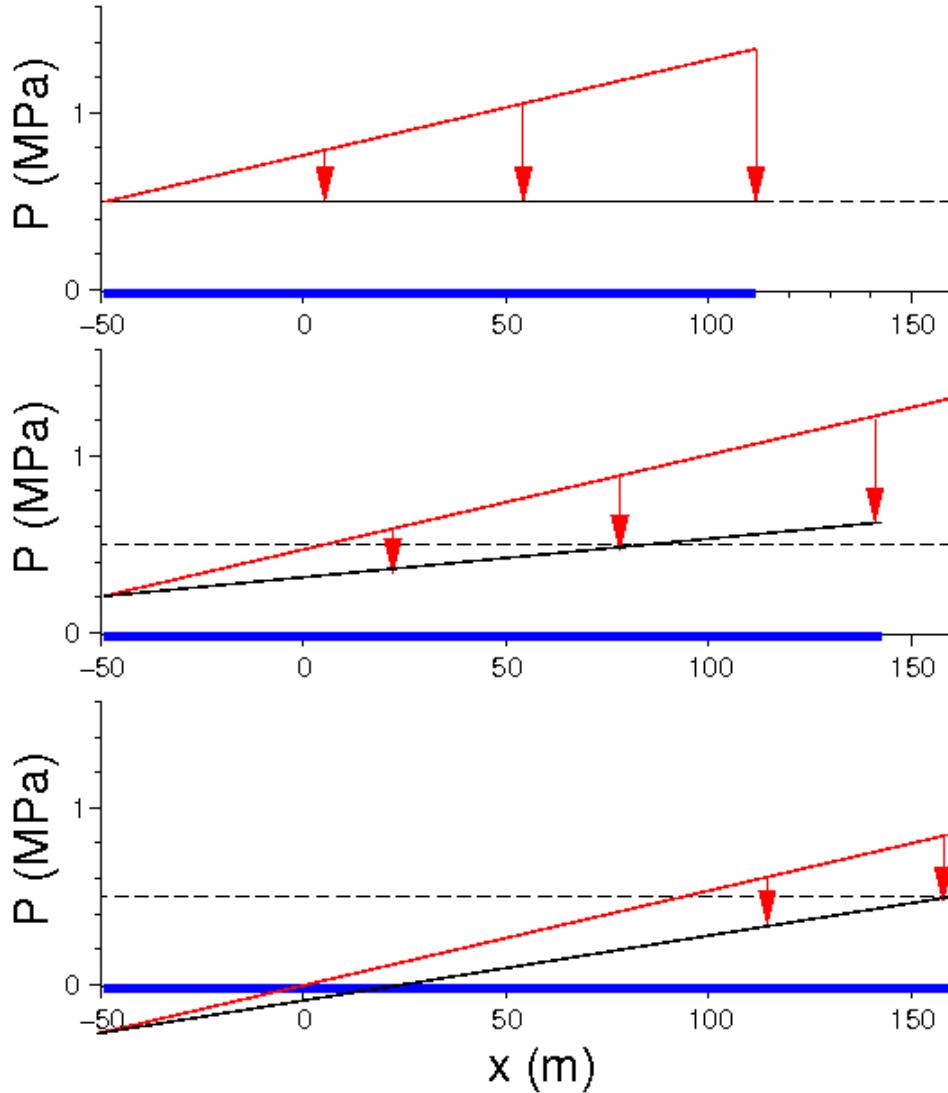
$$\pi \left(\frac{a_l(t) - a_s(t)}{a_s^2(t) + a_l^2(t)} \right) \approx \frac{g}{P_0}$$

see Fischer, Hainzl and Dahm (2009)

$a(t)$ is the time dependent
wing length of the fracture

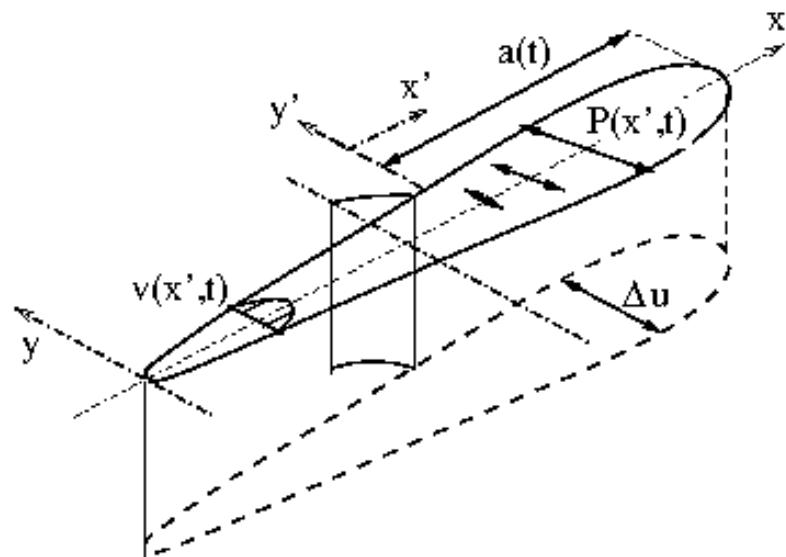
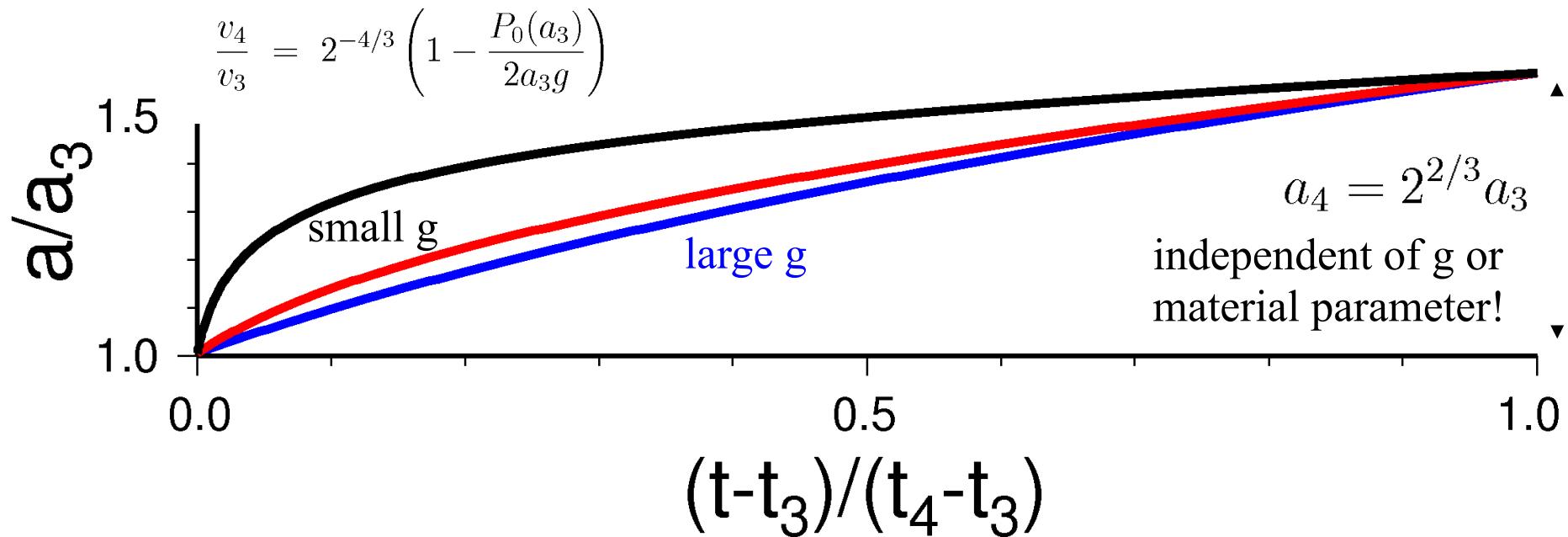
gradient / overpressure

self-expanding unilateral growth

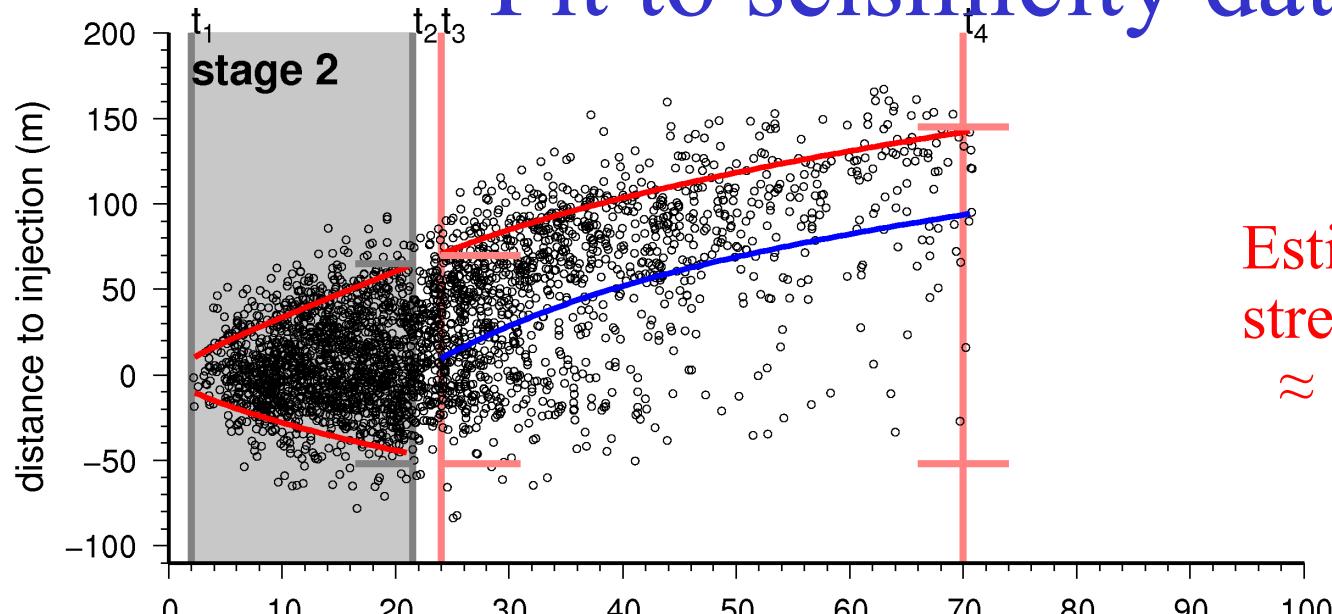


- unilateral growth
- ambient overpressure is further decreasing
- overpressure at taller tip is decreasing below critical value
- at final stage the overpressure at taller tip is below zero (Weertman crack)

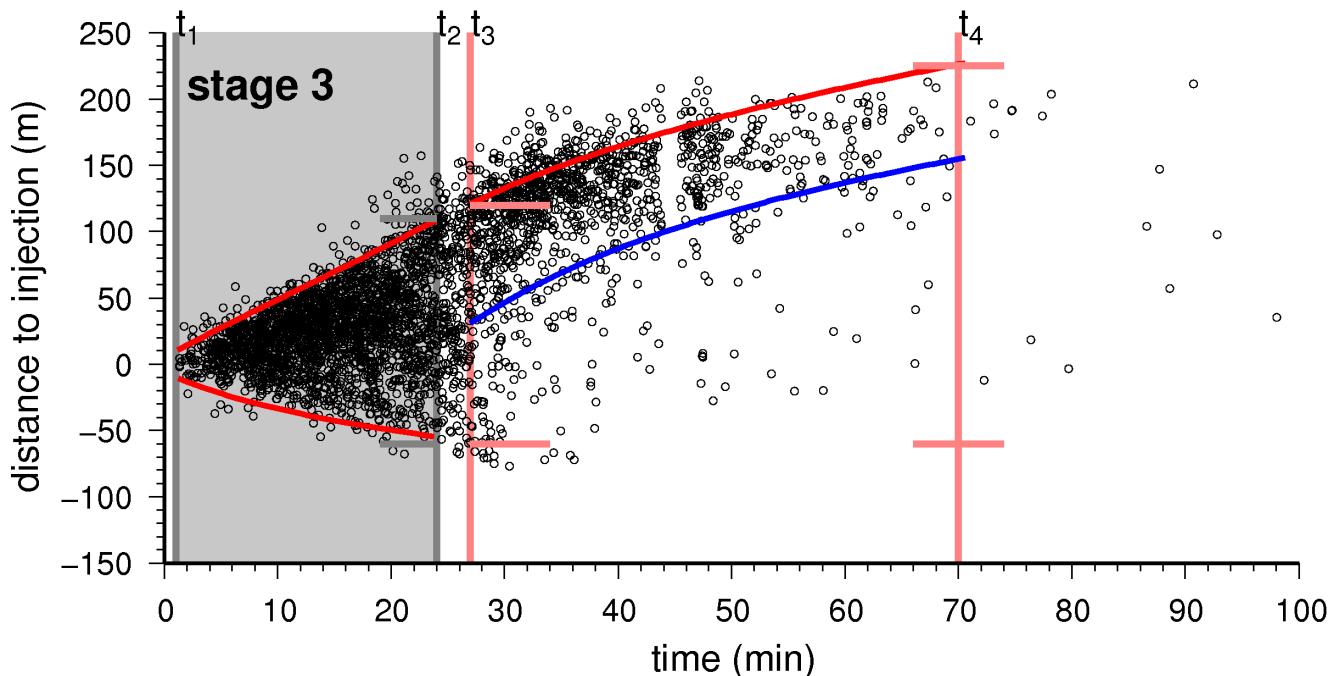
Unilateral growth during post-injection



Fit to seismicity data

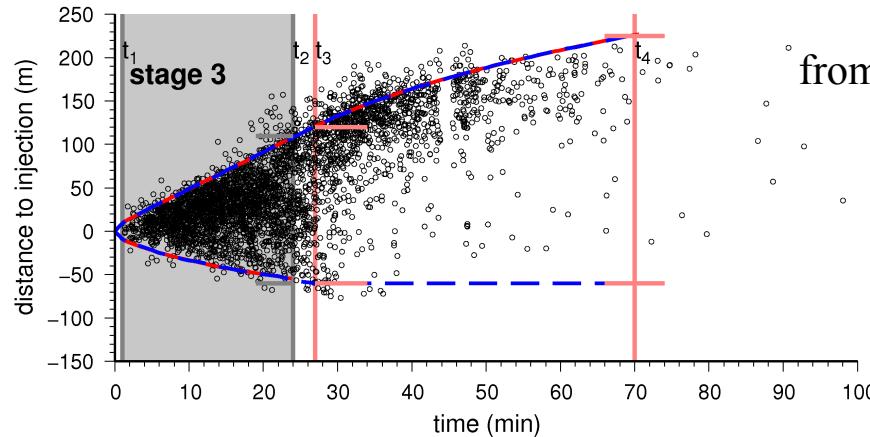


Estimated driving
stress gradient:
 $\approx 10 \text{ MPa/km}$



Dahm et al., 2010

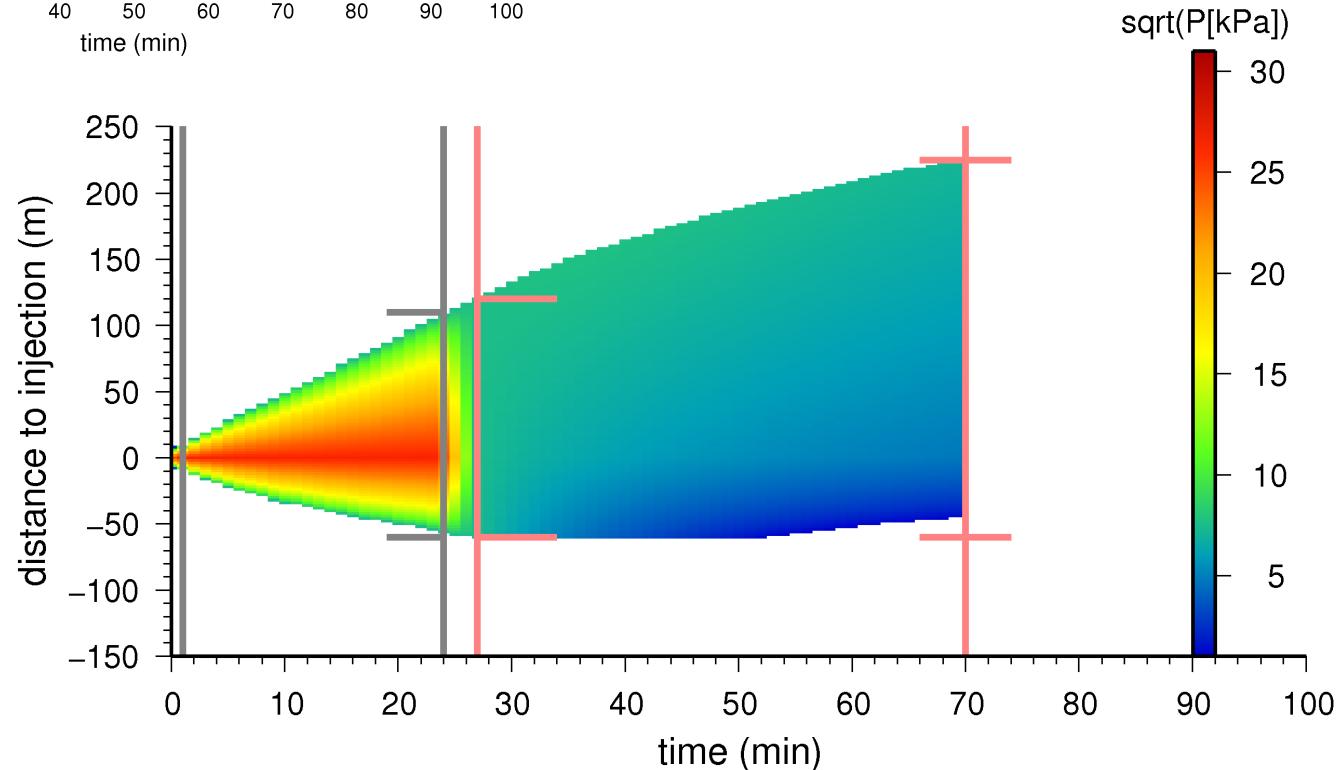
II) Modeling stress changes: Input to BE Method



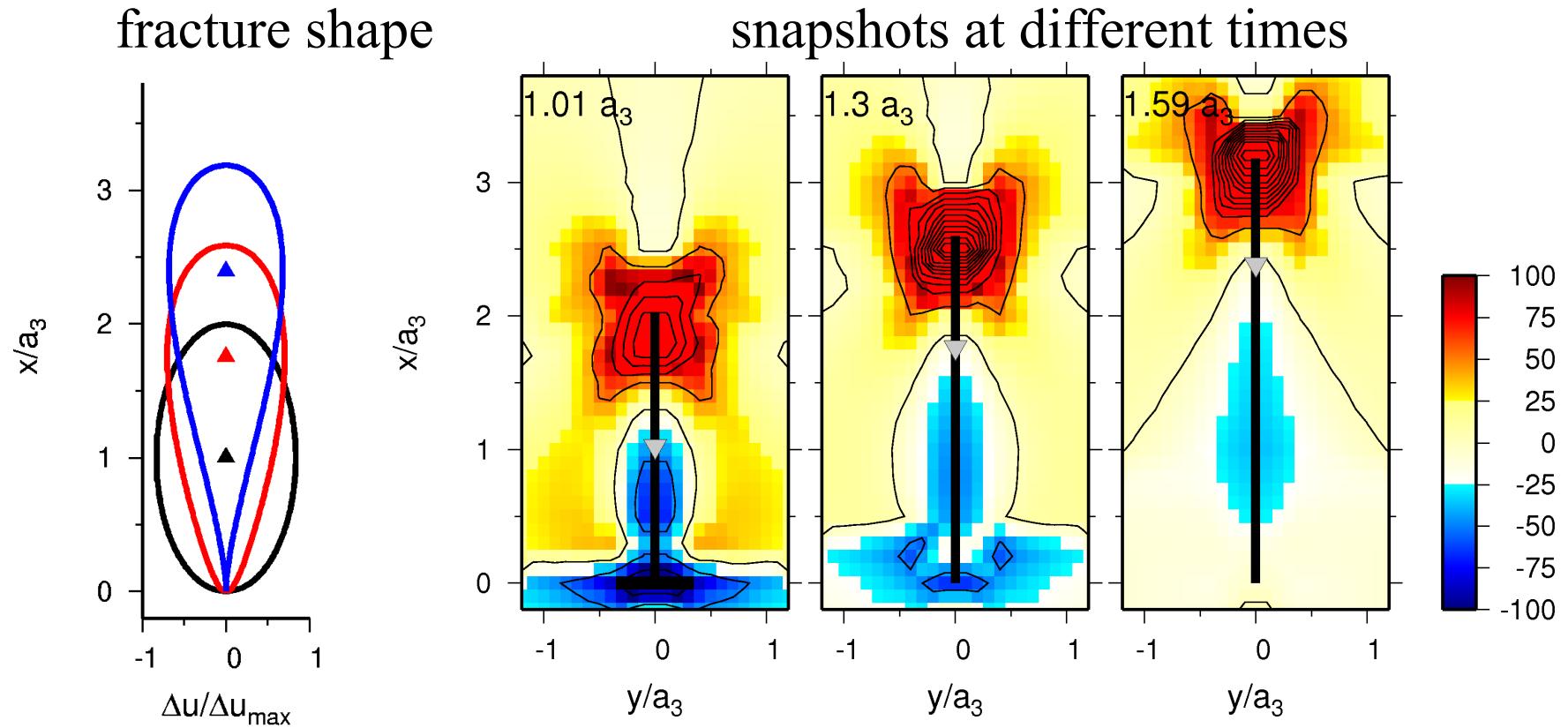
from Dahm, Hainzl and Fischer (JGR, 2010)

hydrofrac length

internal
effective
pressure

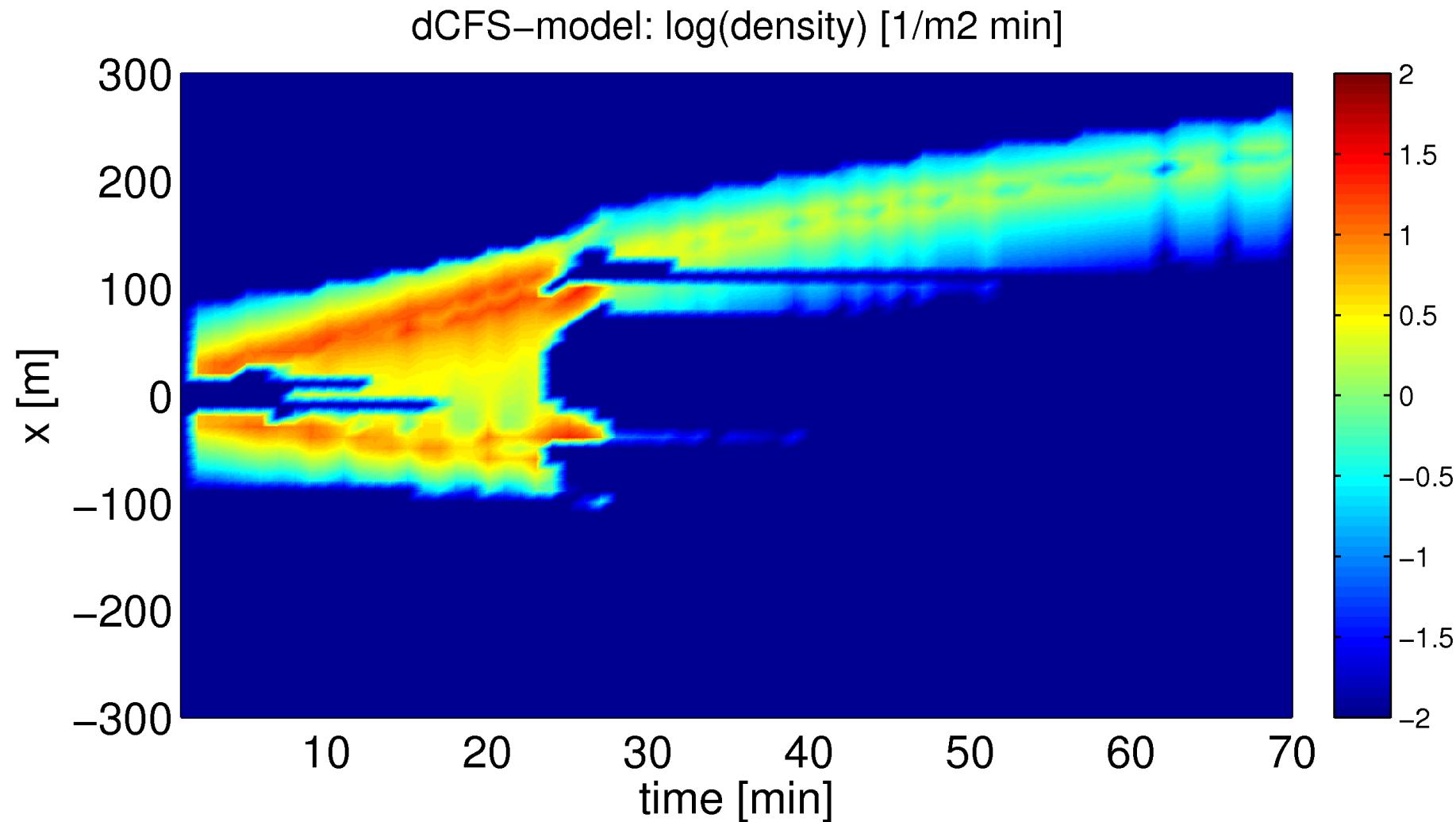


Associated opening and Coulomb stress change (CFF)

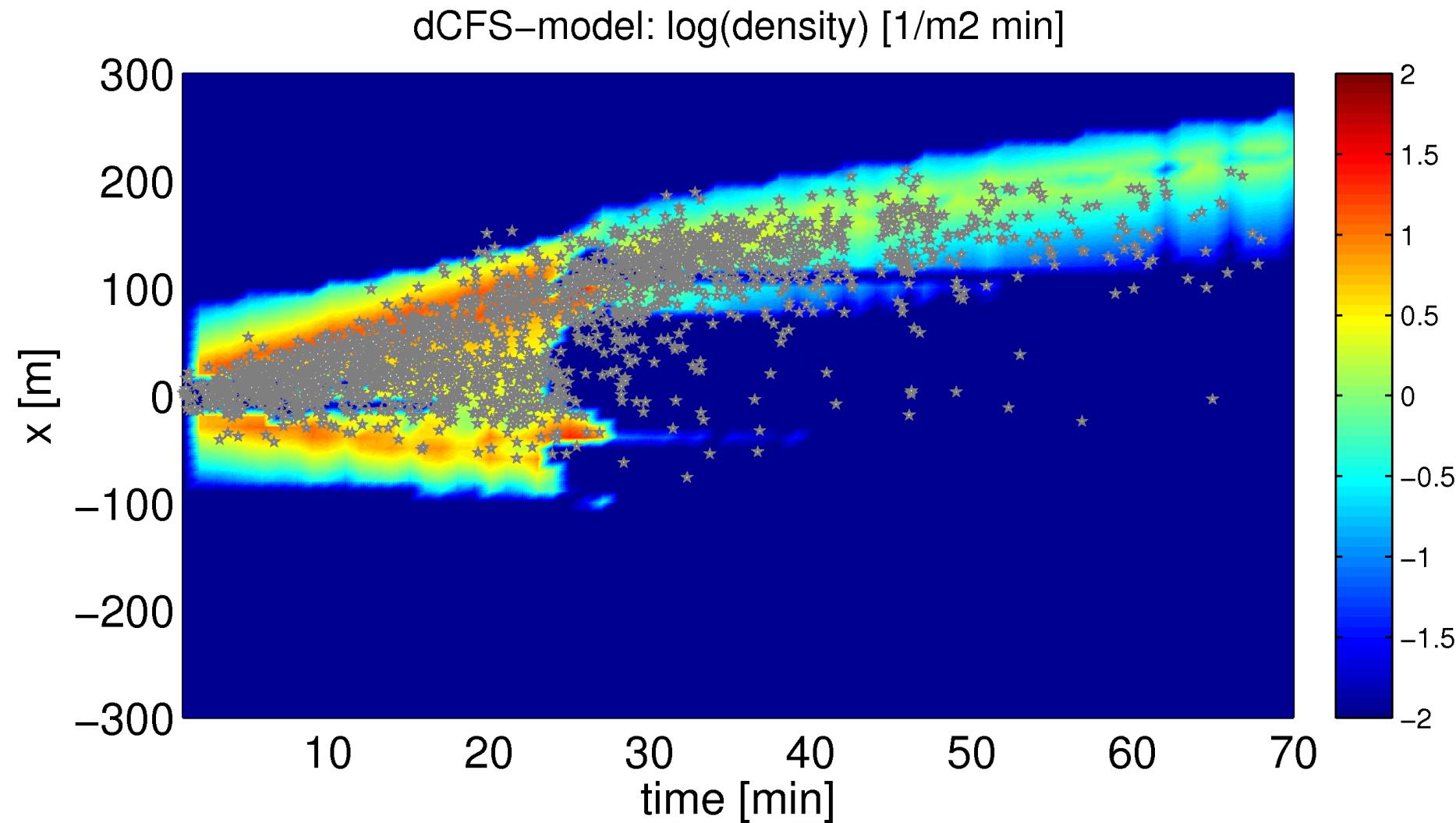


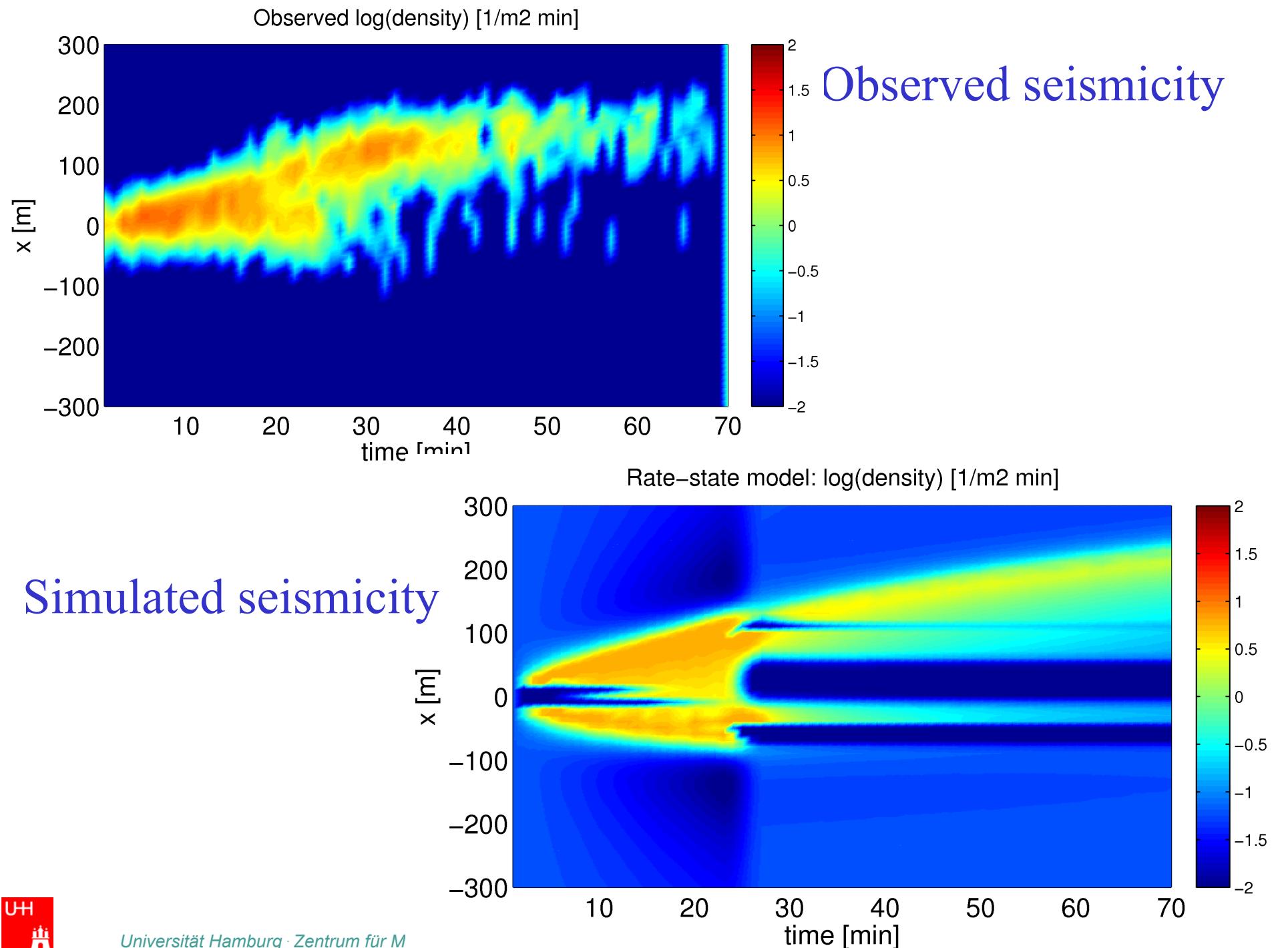
- unilateral migration of front and backfront

Positive CFF projected on fracture axis



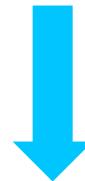
Positive CFF projected on fracture axis





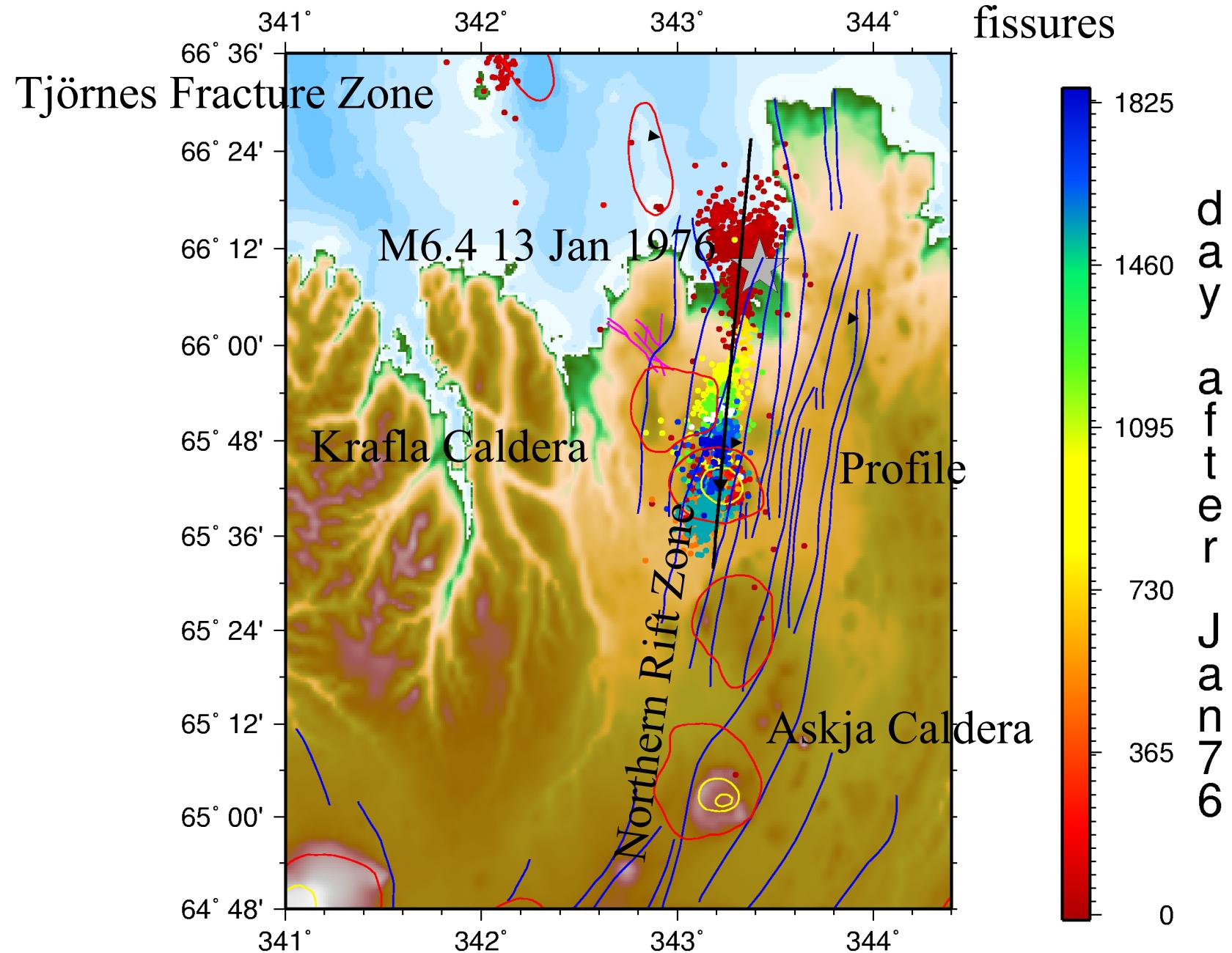
Conclusion

1. Hydrofracture-flow model predicts time-dependent length, opening shape and effective internal pressure
2. Asymmetric and uni-directional growth can be explained by fracture model with stress or pore pressure gradients
3. Rate and state dependent seismicity model explains main features of observed seismicity

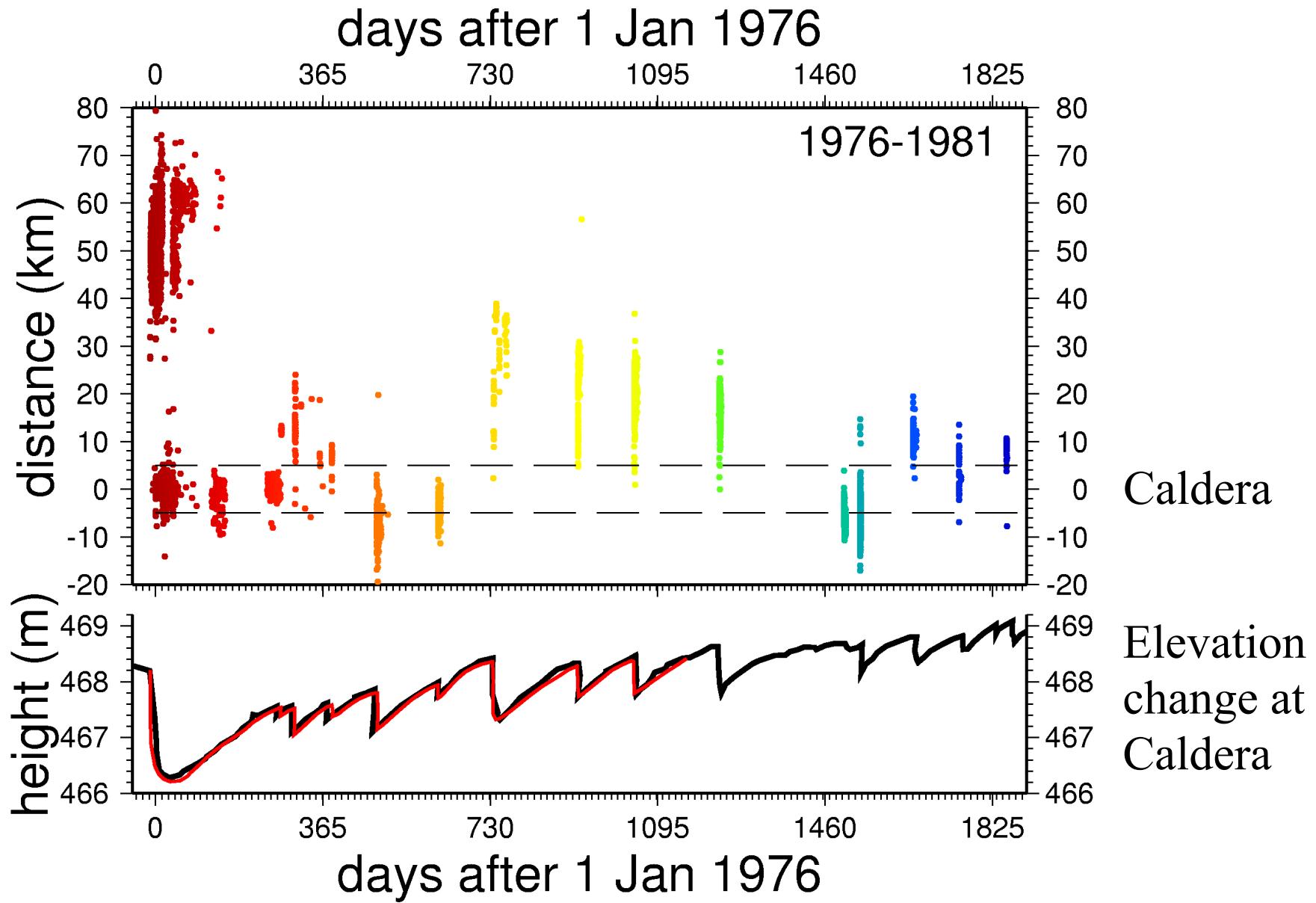


Induced seismicity can be linked to deterministic hydrofrac model

Seismicity during the Krafla rifting events Dec75 - Jan81

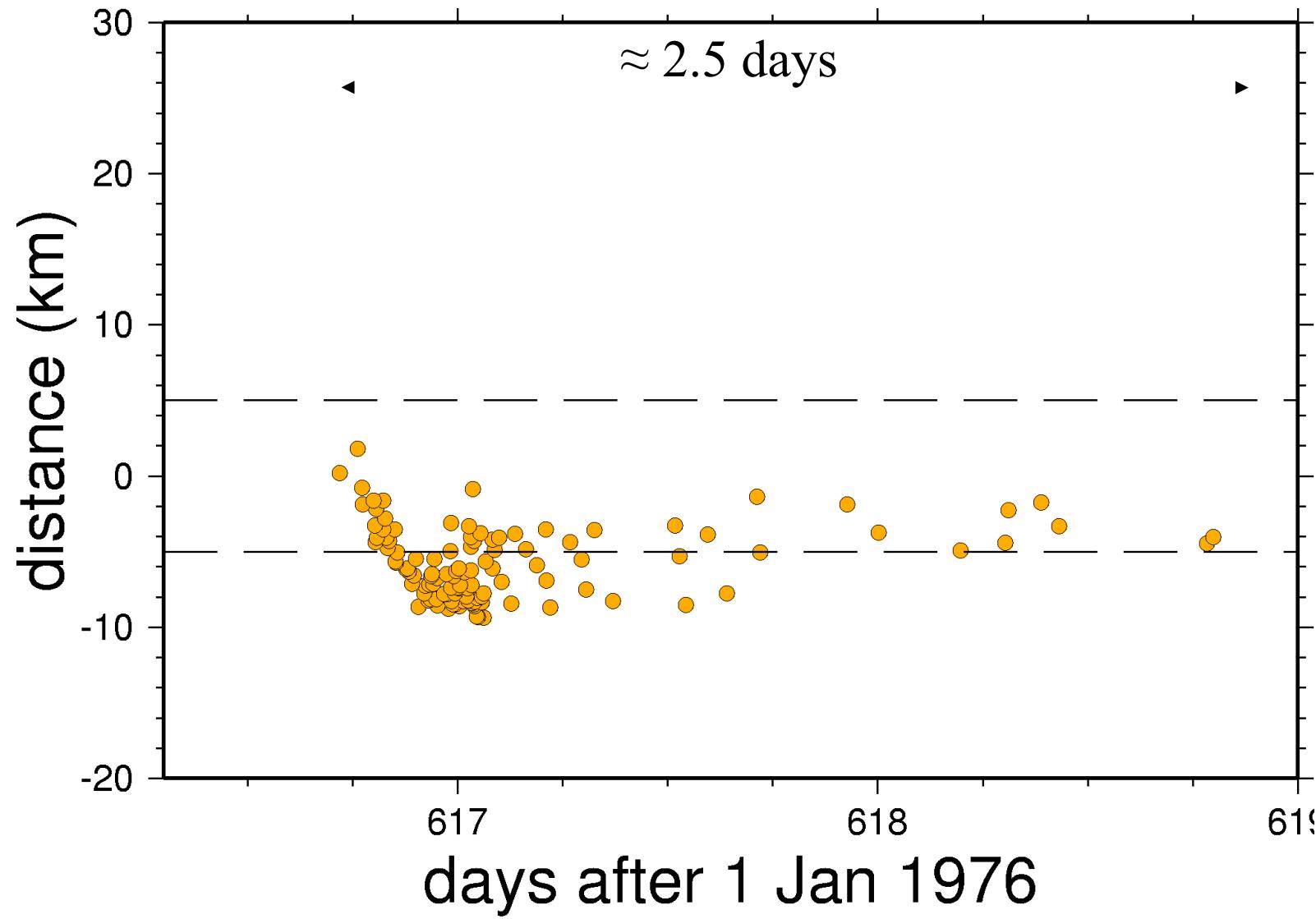


Along strike seismicity and caldera deflation

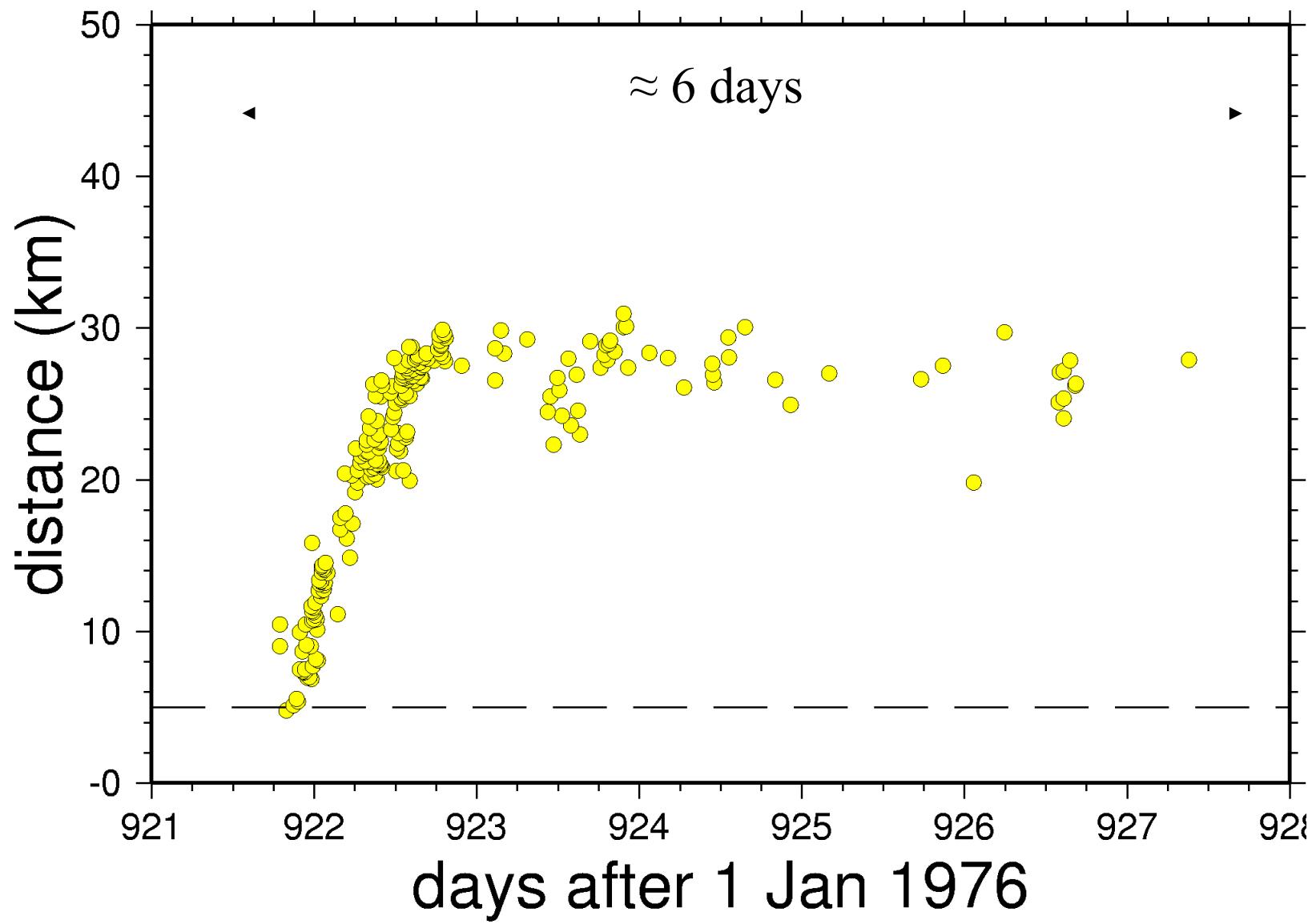


see Einarsson, 1991, Buck et al., 2006 and references therein

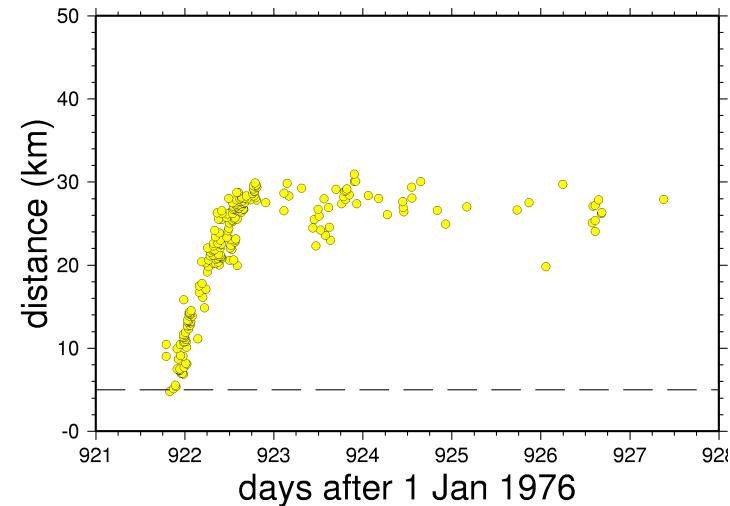
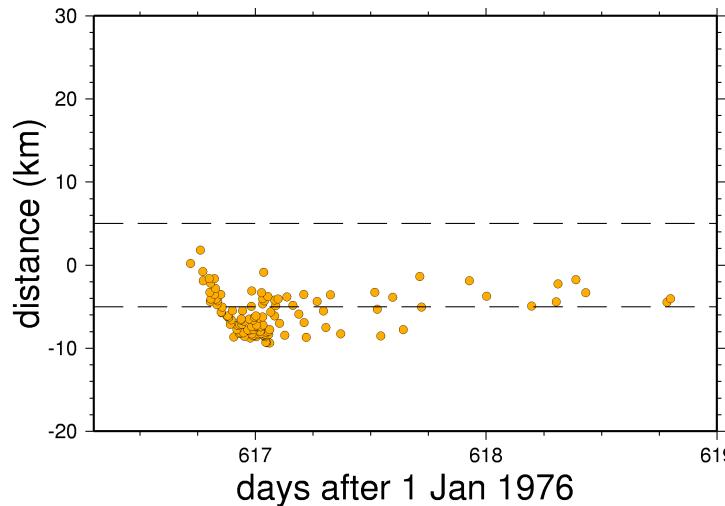
induced seismicity: Sep 77 intrusion



induced seismicity: Jul 78 intrusion

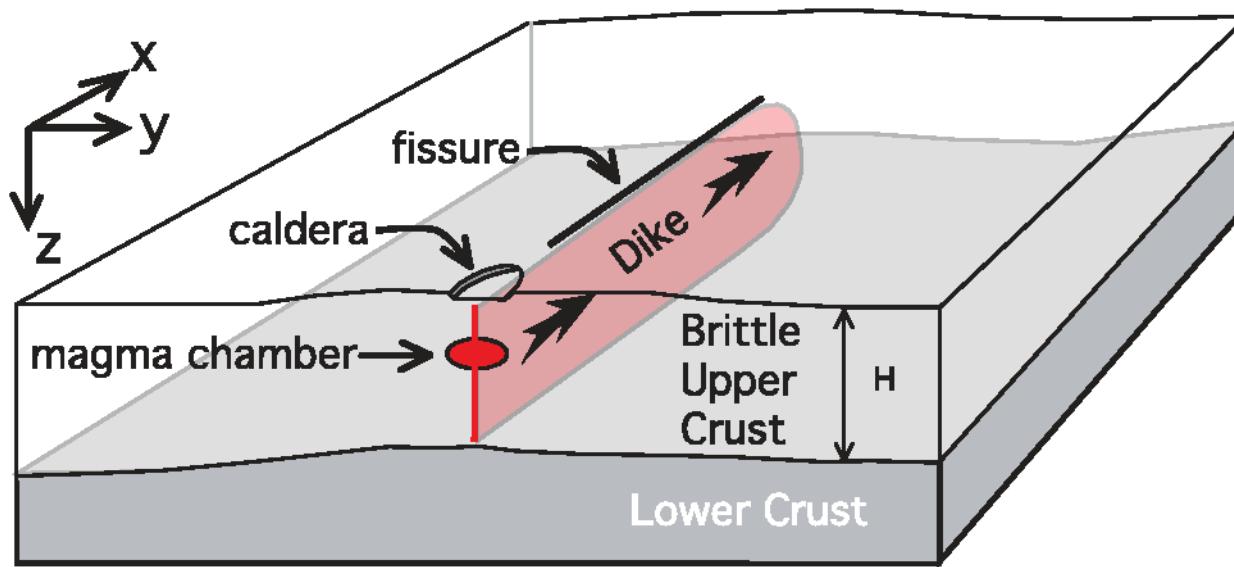


Questions

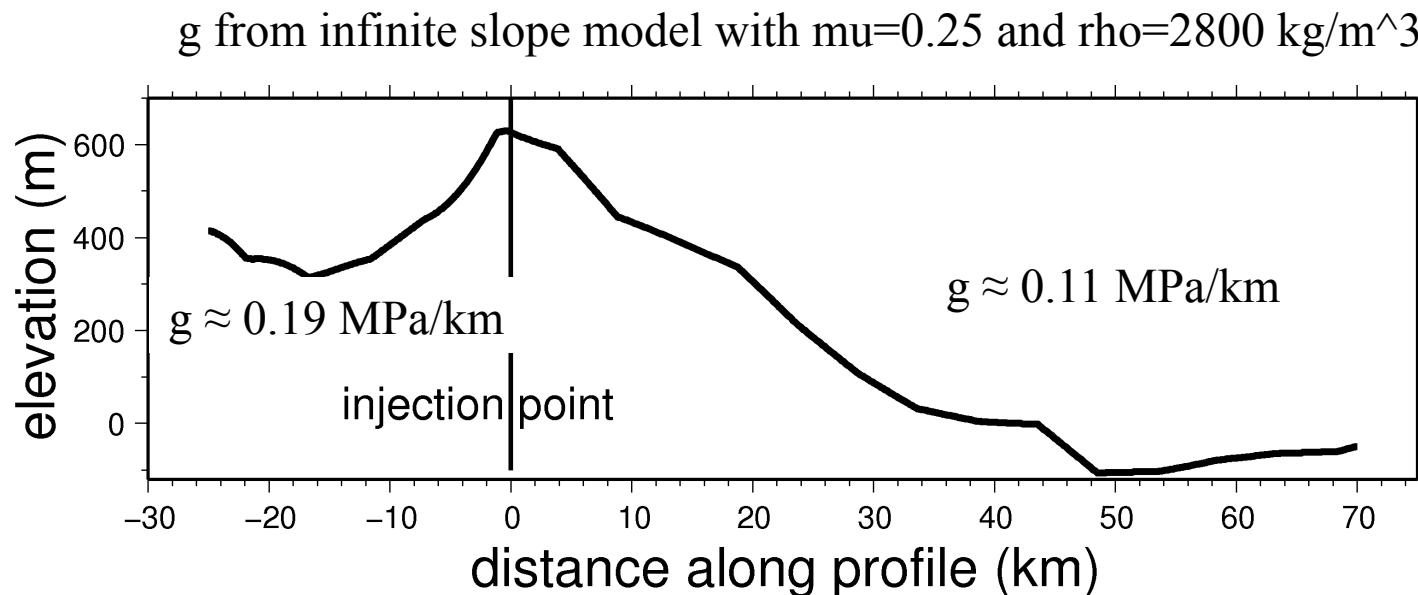


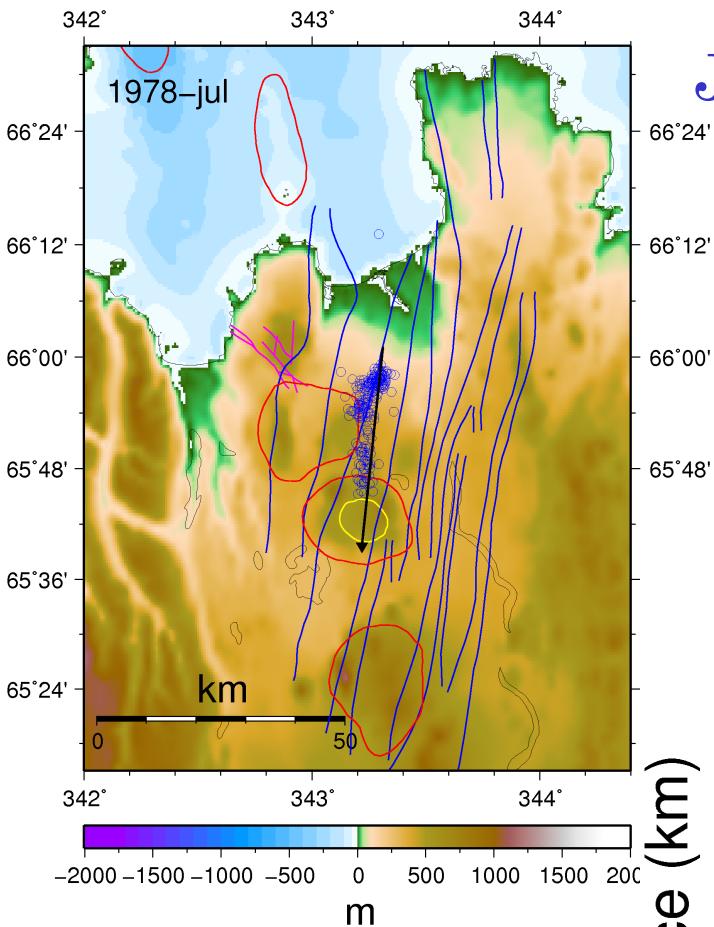
- Why do we observe a one-directional migration of seismicity?
- Why is there a backfront of the seismicity cloud ?
- Can we model the time-dependency of front and backfront?

Rifting at Krafla: topography may control stress gradients

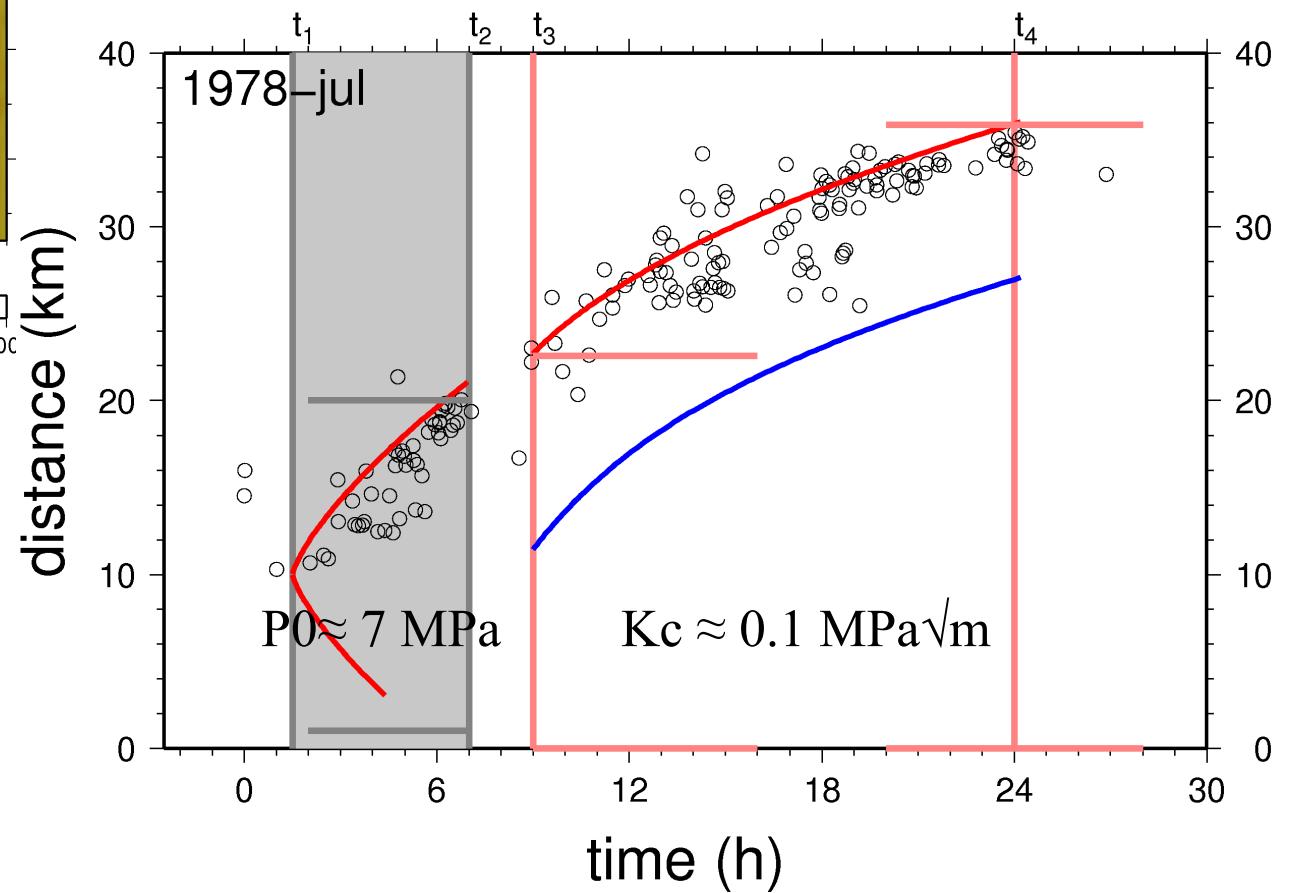


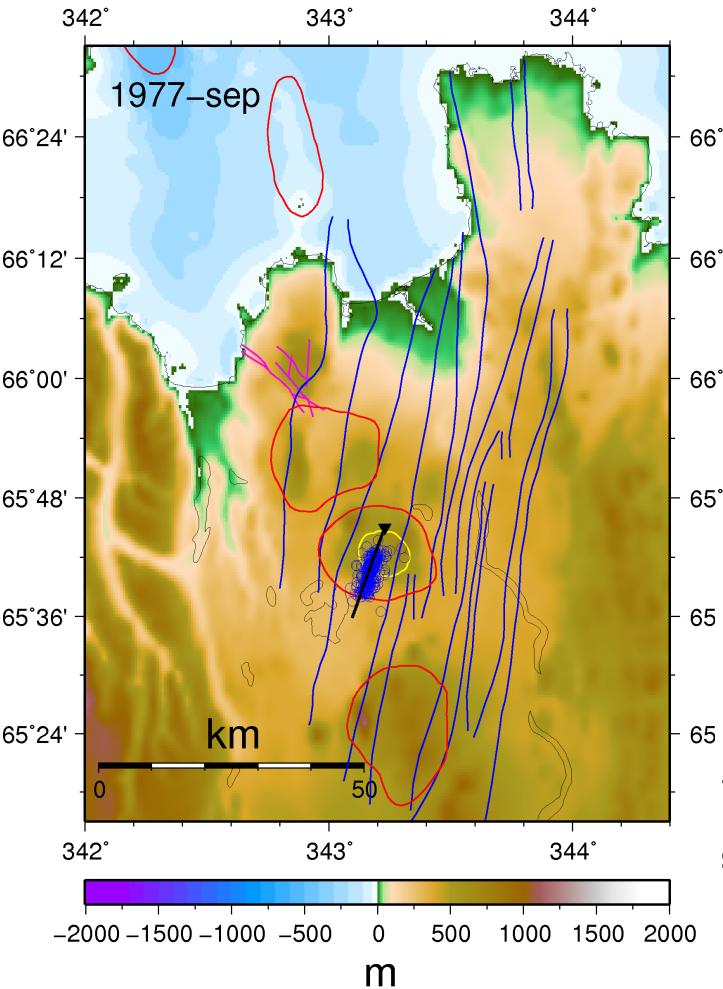
Buck et.al. (2006)





- self-expansion starts after 9 h
- injection controlled length is 19-22 km
- final length is 34 km
- gap after 7 h: re-organisation of flow

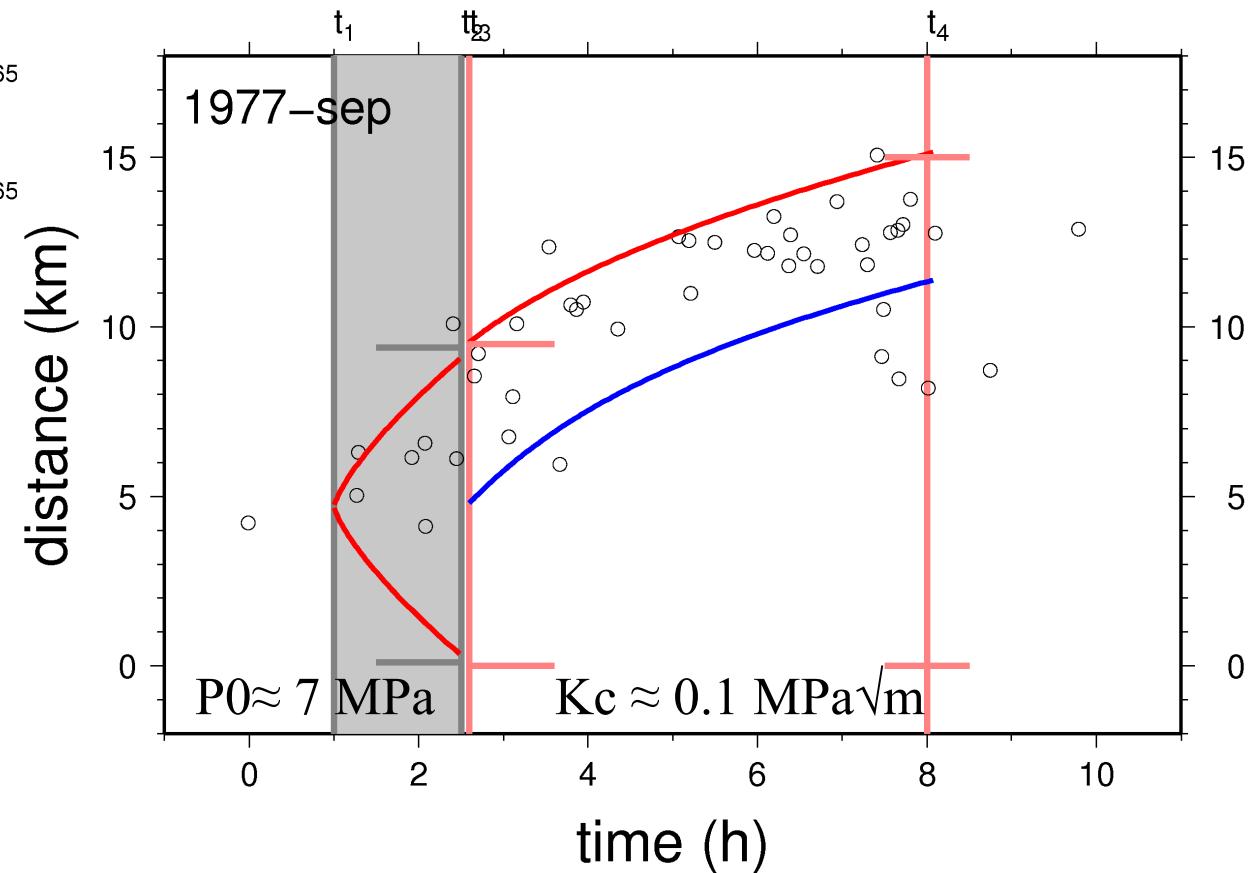




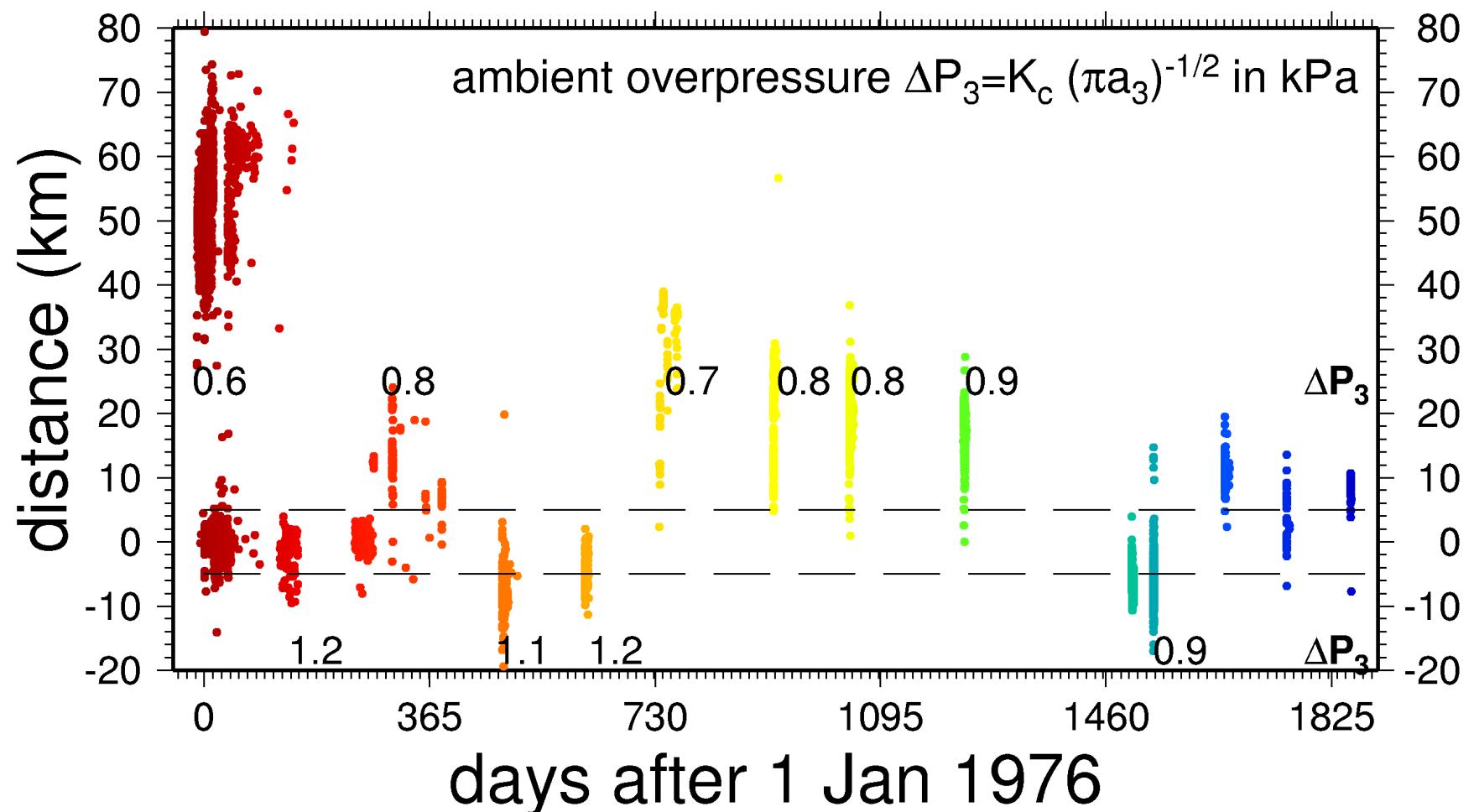
assuming $g \approx 0.19 \text{ MPa/km}$
 $\eta \approx 20 \text{ Pa s}$

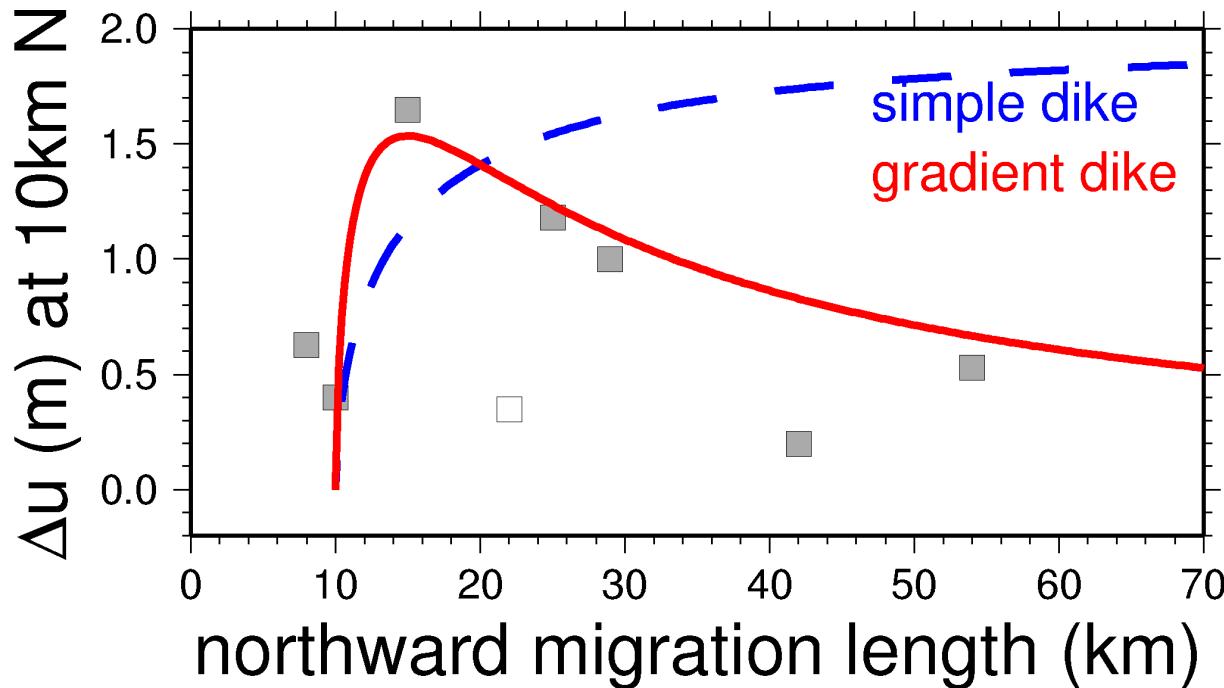
Sep 1977 intrusion southward

- self-expansion starts after 2.5 h
- injection controlled length $\approx 10 \text{ km}$
- final length is $\approx 15 \text{ km}$



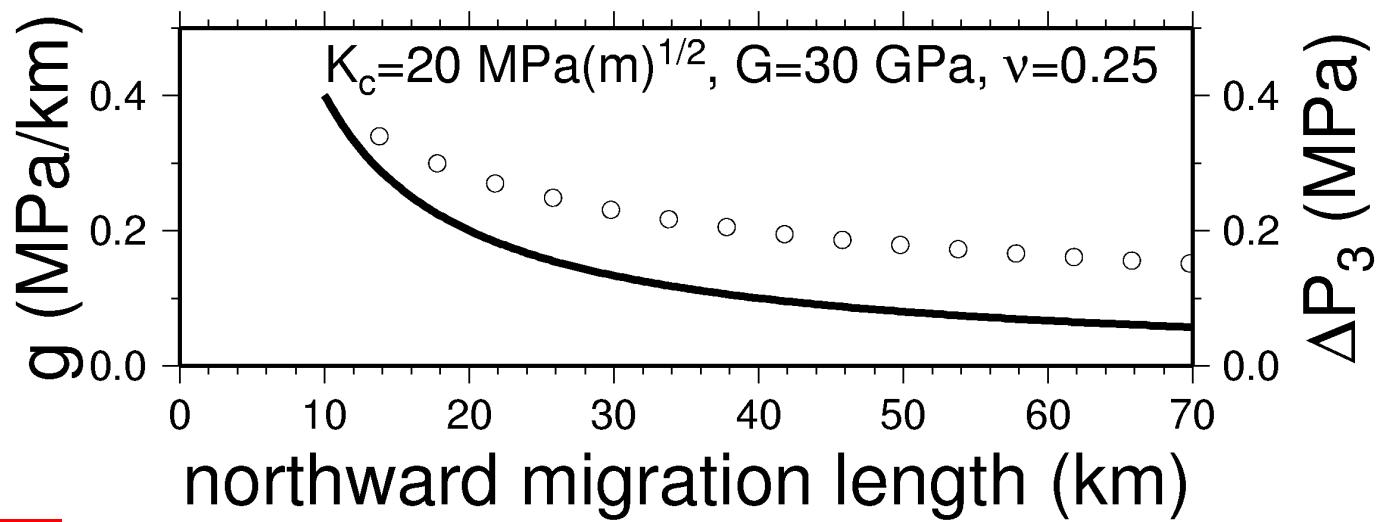
Estimated post-injection driving pressure P3 is only a few kPa





opening north of
caldera:
(static model)

data from Tryggvason (1984)



Results

- Stress-gradient crack-model explains unilateral dike intrusion and seismicity patterns (injection, post-injection phase).
- Overpressure during injection is ≈ 7 MPa
- Final ambient overpressure is only ≈ 0.2 MPa
- Largest opening is far from Caldera
- K_c to stop dikes is ≈ 50 MPa \sqrt{m}
- K_c during re-injection is ≈ 0.1 MPa \sqrt{m}
- g possibly decreased with distance to Caldera

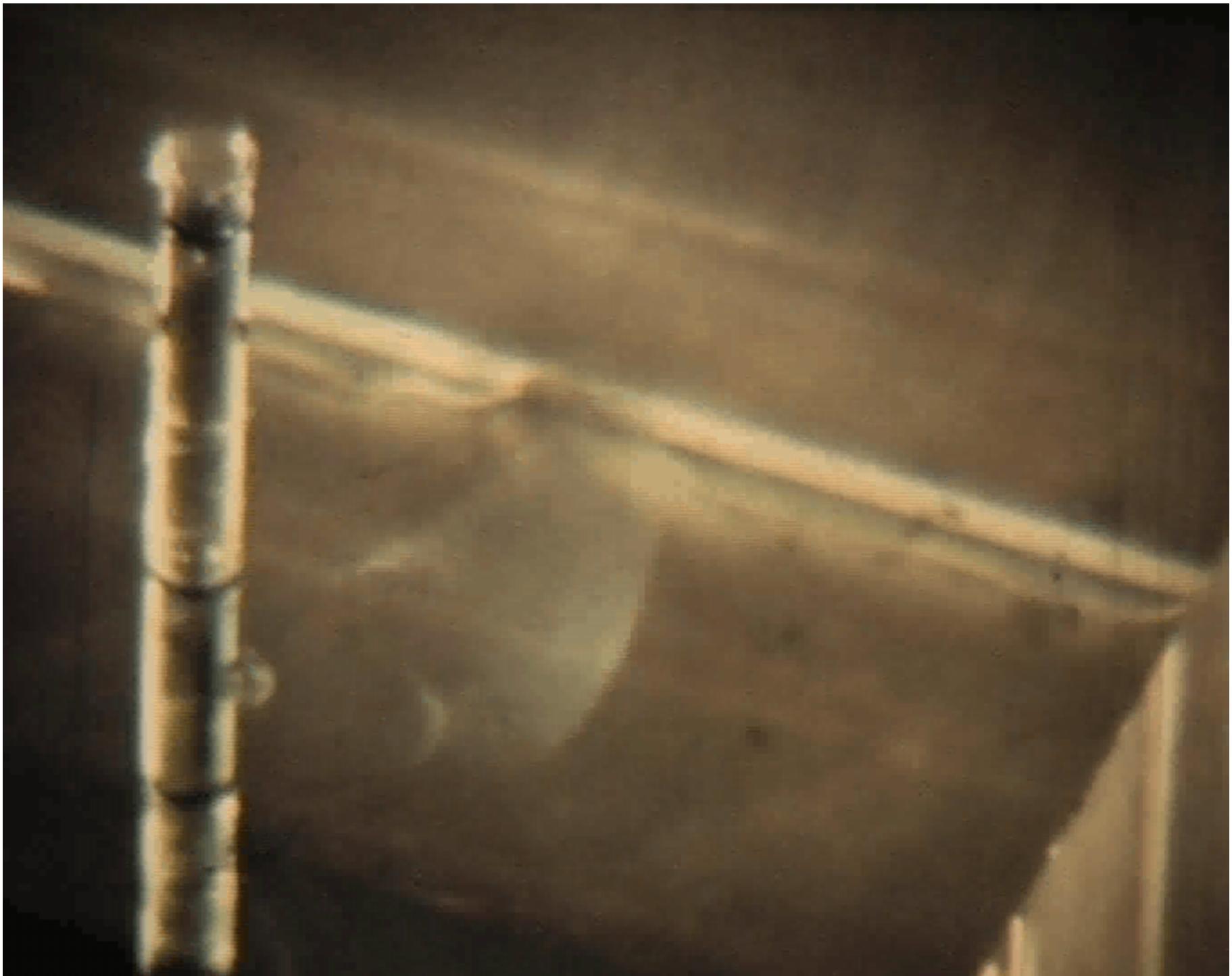
Case III

Slow natural intrusions

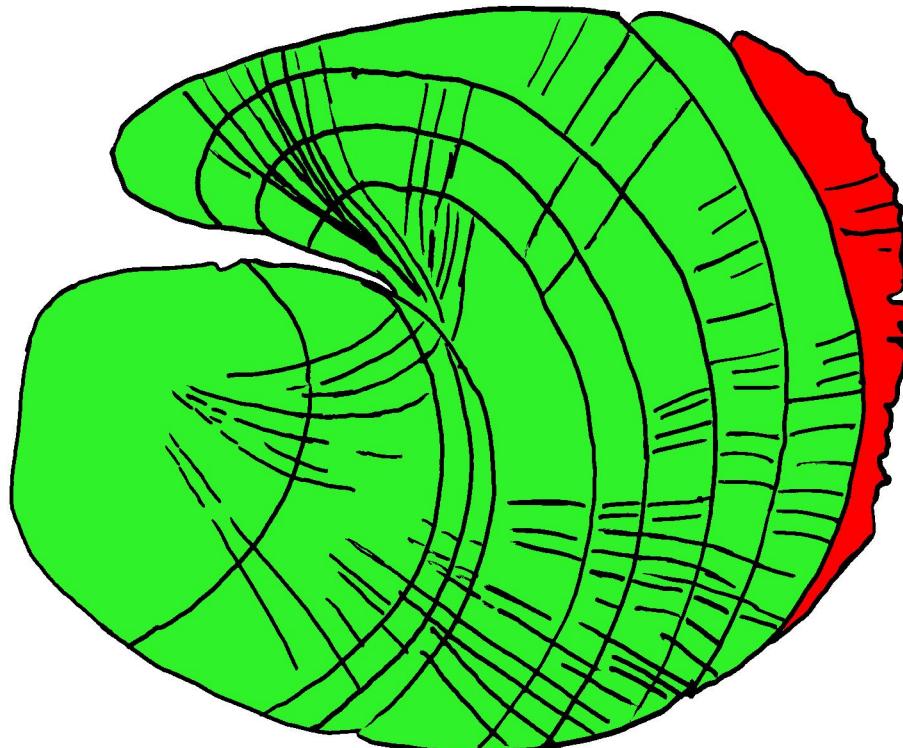


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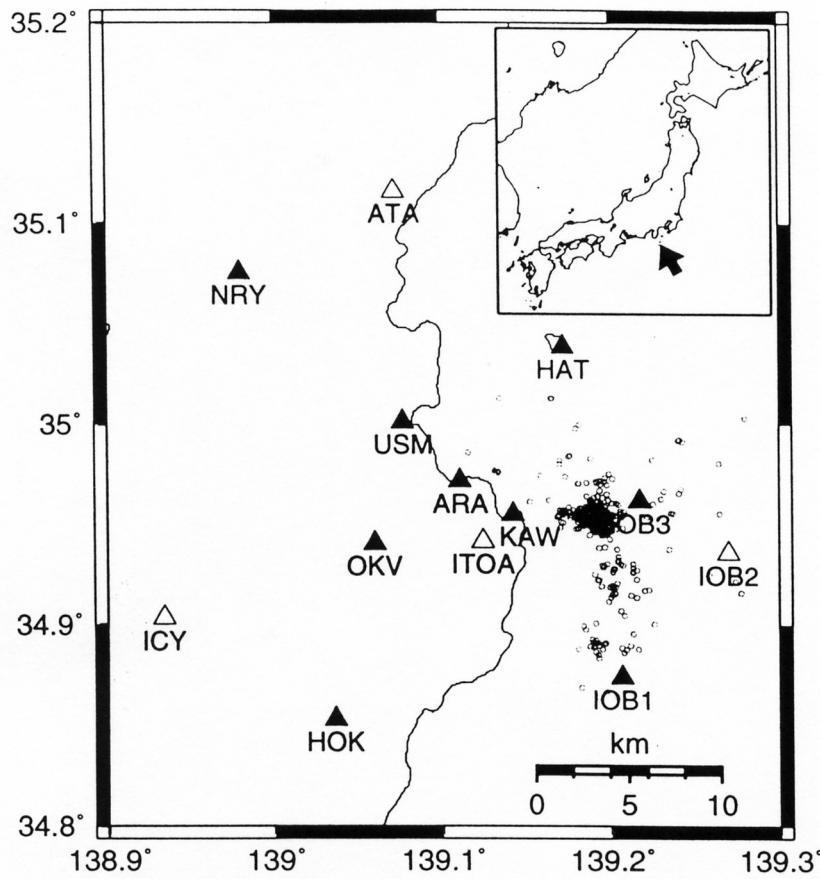




Hydrofrac in plexiglass

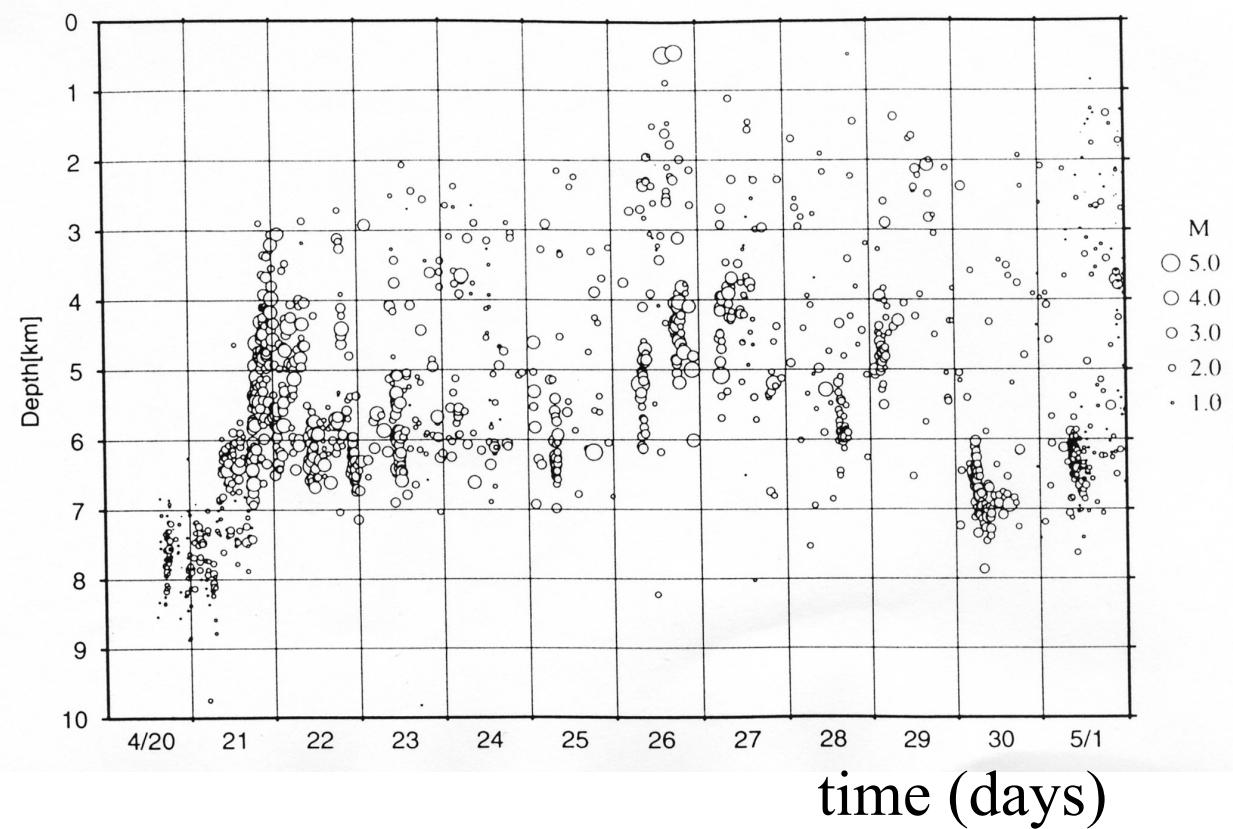


- episodic path-like growth of the fracture
- final shape is circular or elliptical

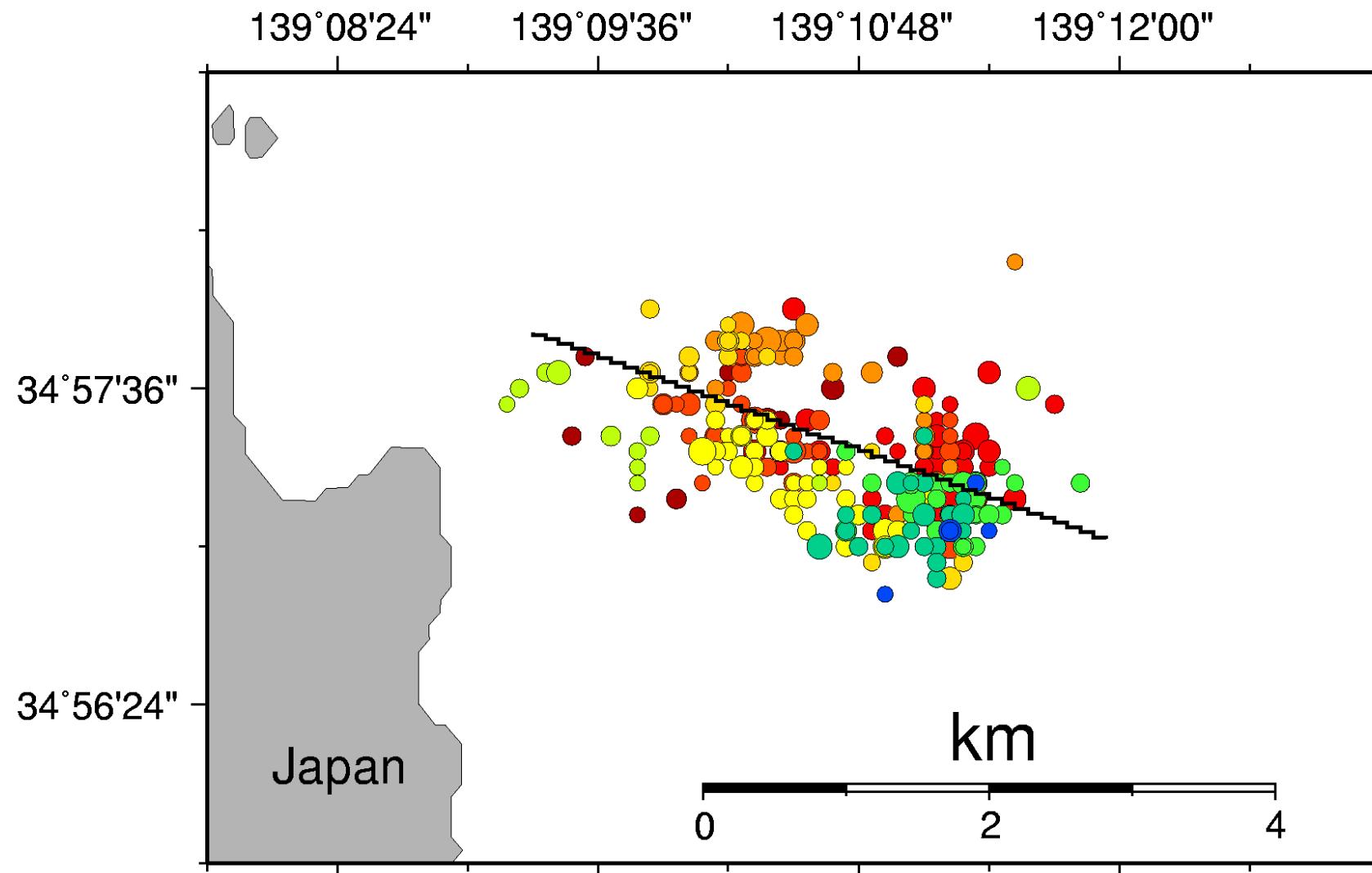


Hayashi & Morita (2002):
A magma intrusion process
inferred from hypocenter
migration of earthquake
swarms, GJI

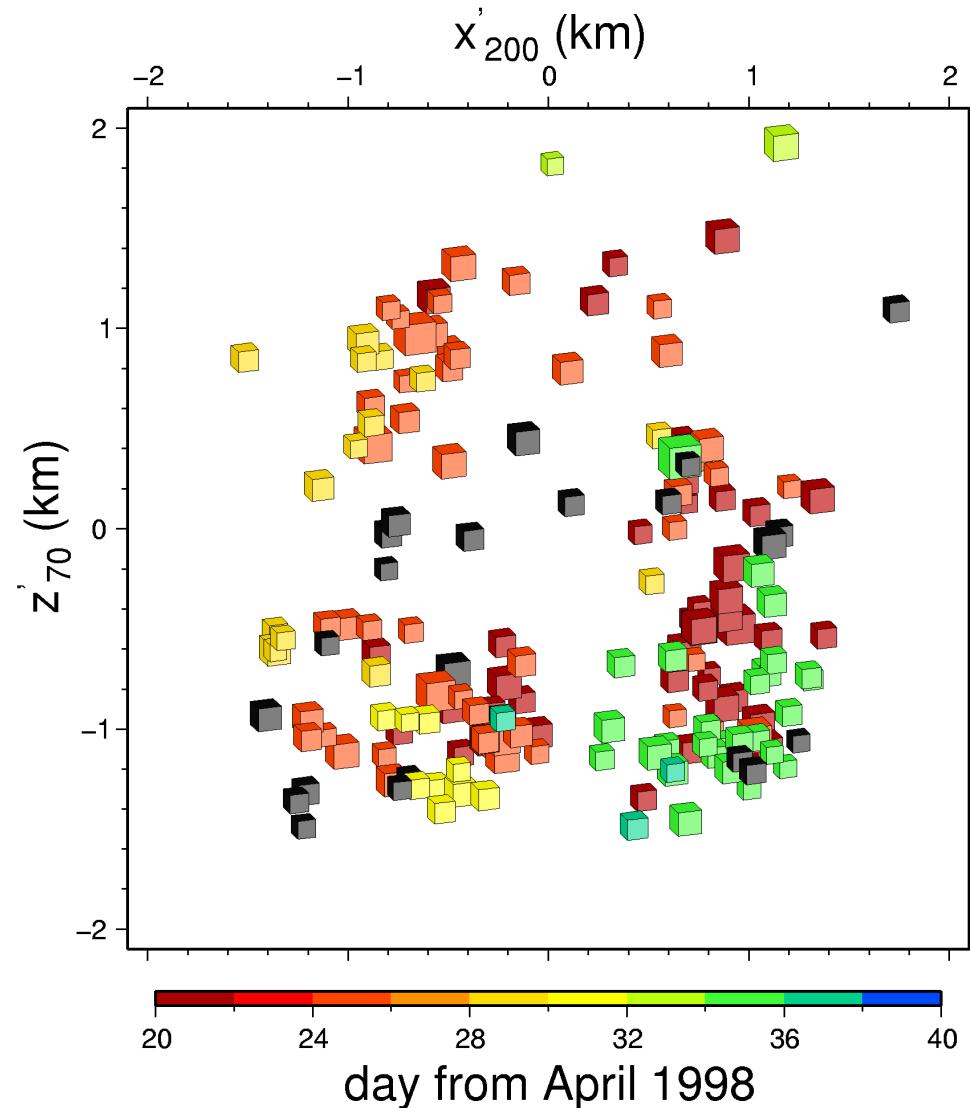
Example A: Izu Bonin Magma Intrusion Apr 2000



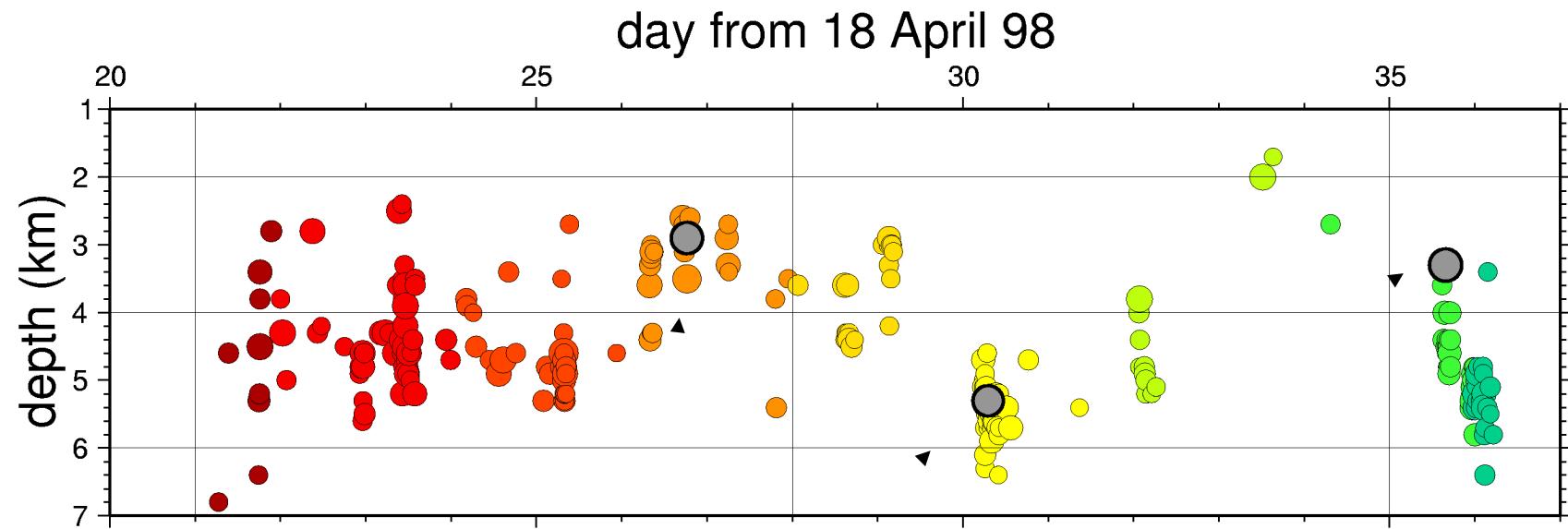
Penny-shaped hypocenter pattern



Penny-shaped hypocenter pattern

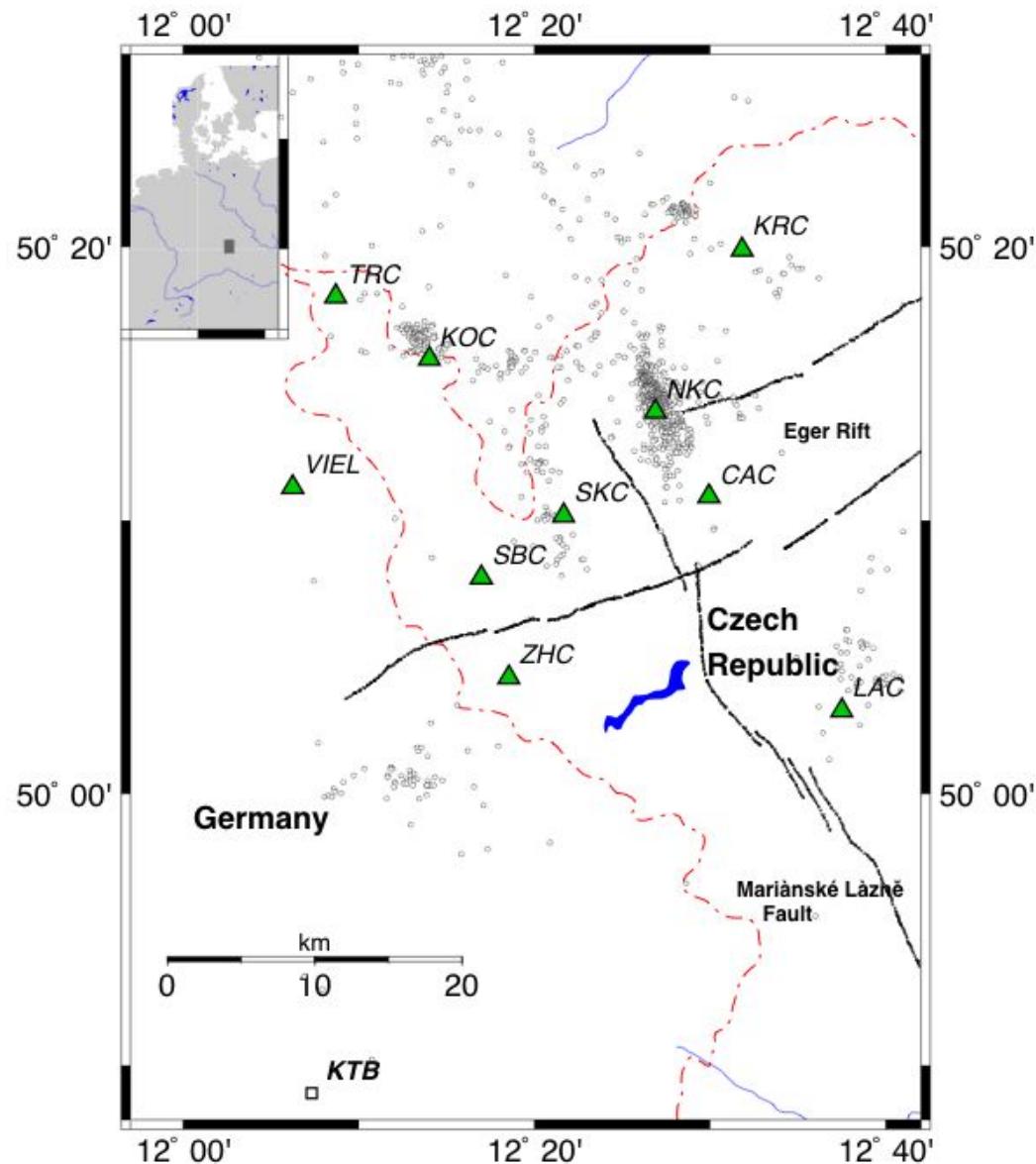


Penny-shaped hypocenter pattern



strongest events occur at the end of the sequence

maximal magnitudes \approx M 4.5



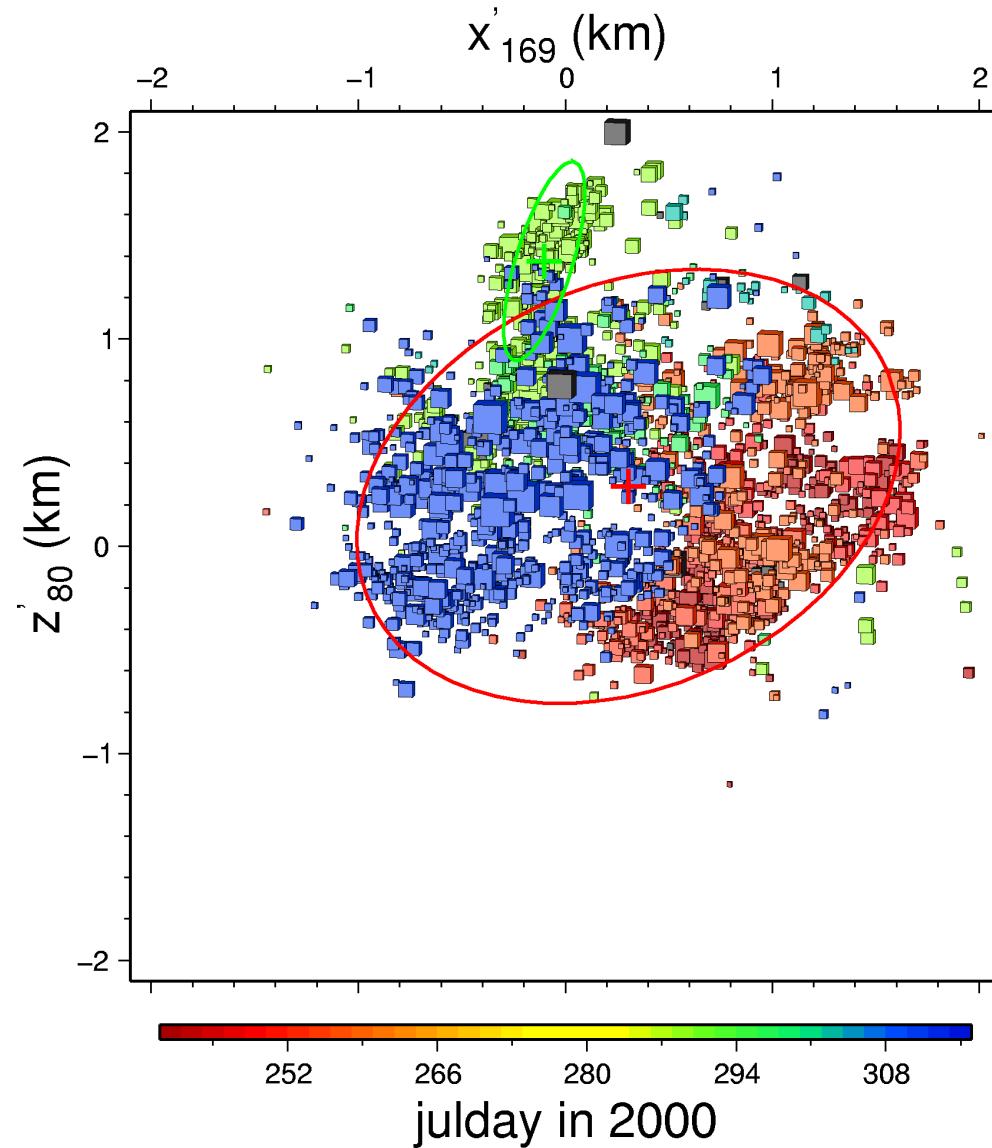
Example B: Earthquake swarm NW-Bohemia 2000

several 100 events in 2 month

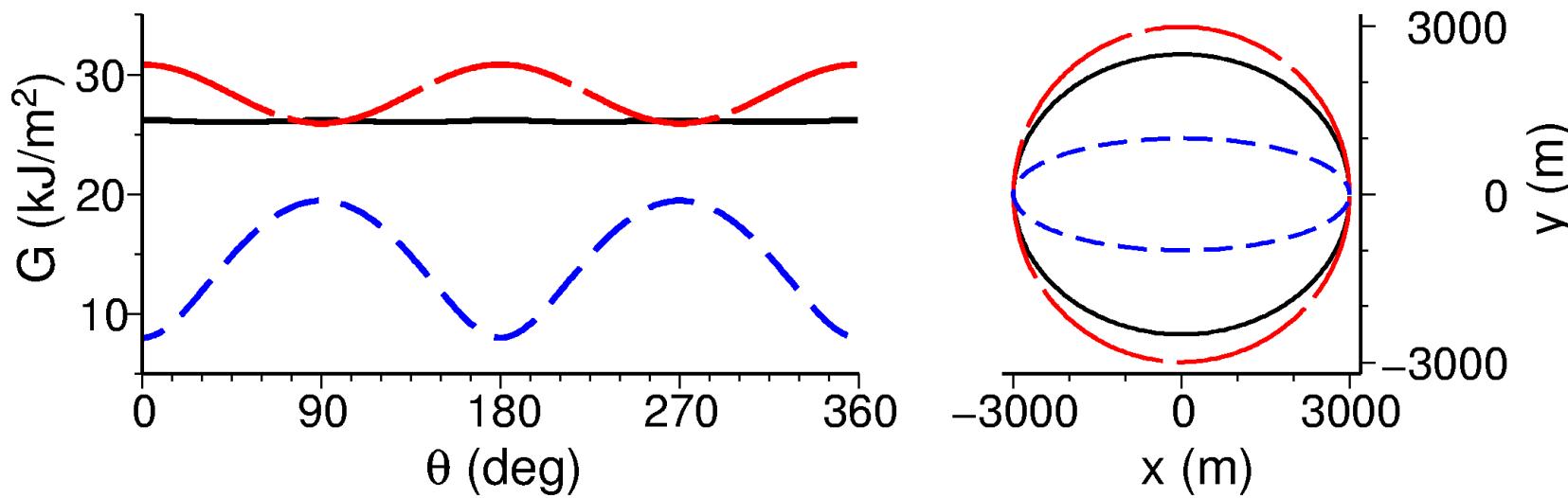
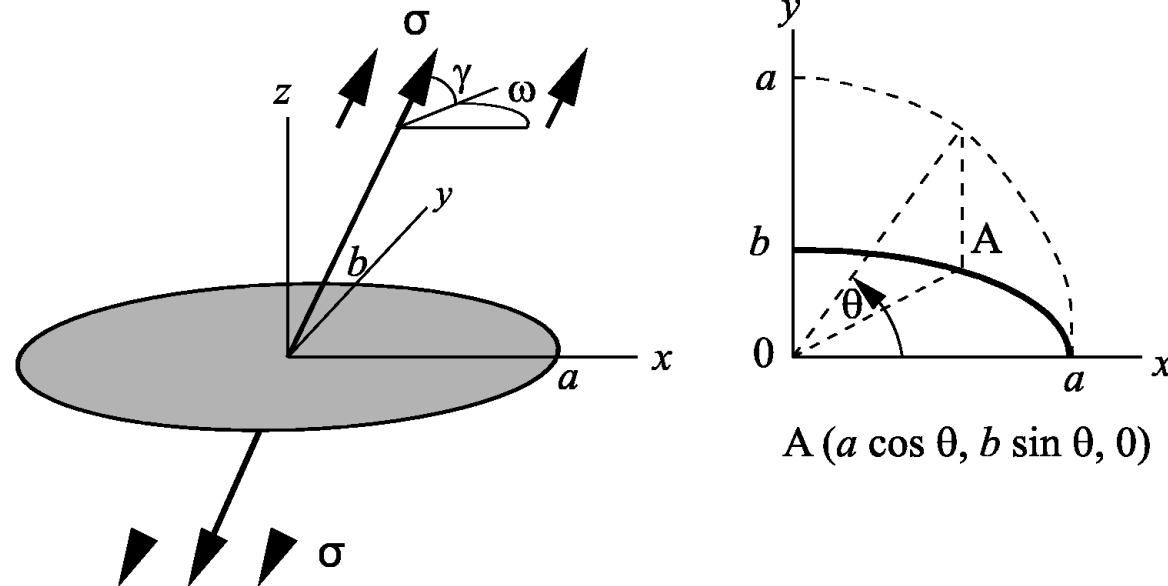
Max Ml \approx 3

Hypo depth \approx 8 km

“Weekly” migration of hypocenters

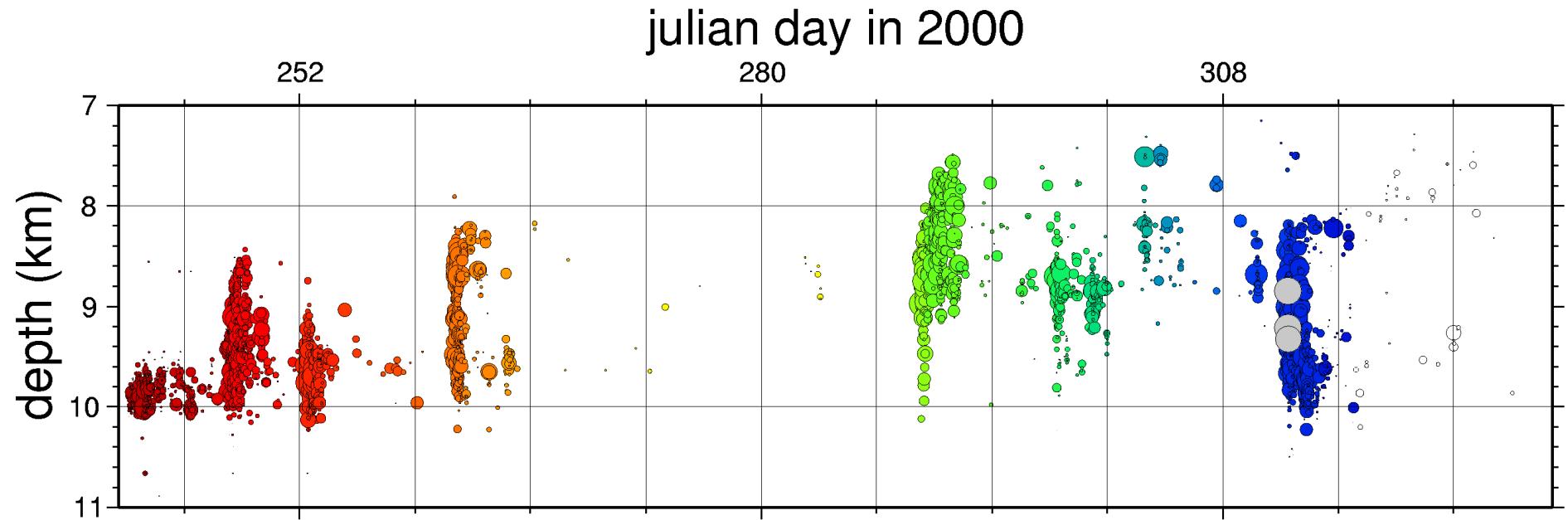


Elliptical crack develops under mixed loading

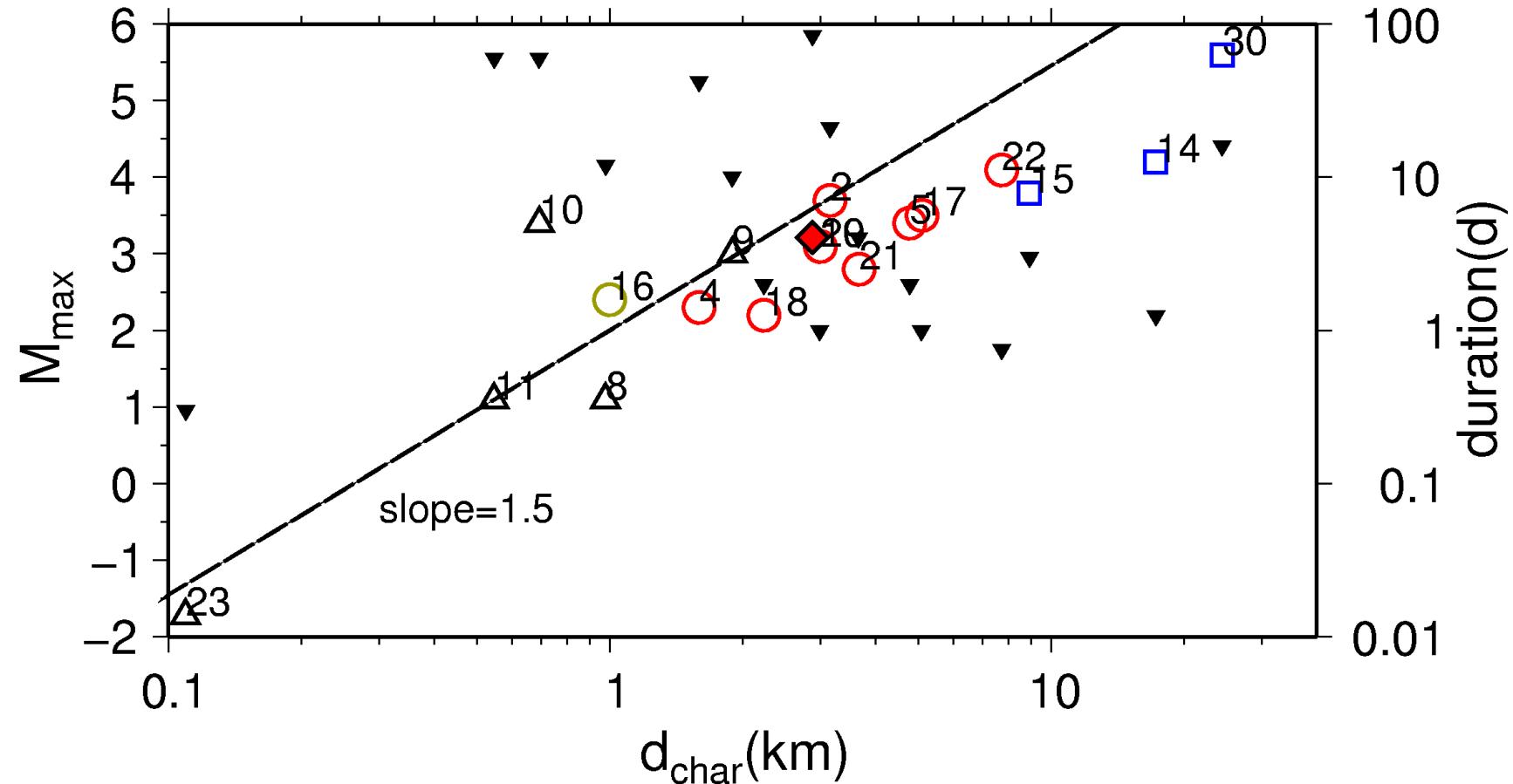


Dahm, Fischer and Hainzl (2008), Studia Geofisica

strongest events at the end of the sequence



“scaling relations” of intrusion-induced seismicity ?



Dahm, Fischer and Hainzl (2008), Studia Geofisica

Summary of fluid-fracture growth

1. Fluid-filled fractures (non-buoyant) grow towards circular or elliptical final shape
2. The growth is episodic and discontinuous when the overpressure is small
3. Tendency that strongest induced earthquakes occur at the end of fracture growth

Case IV

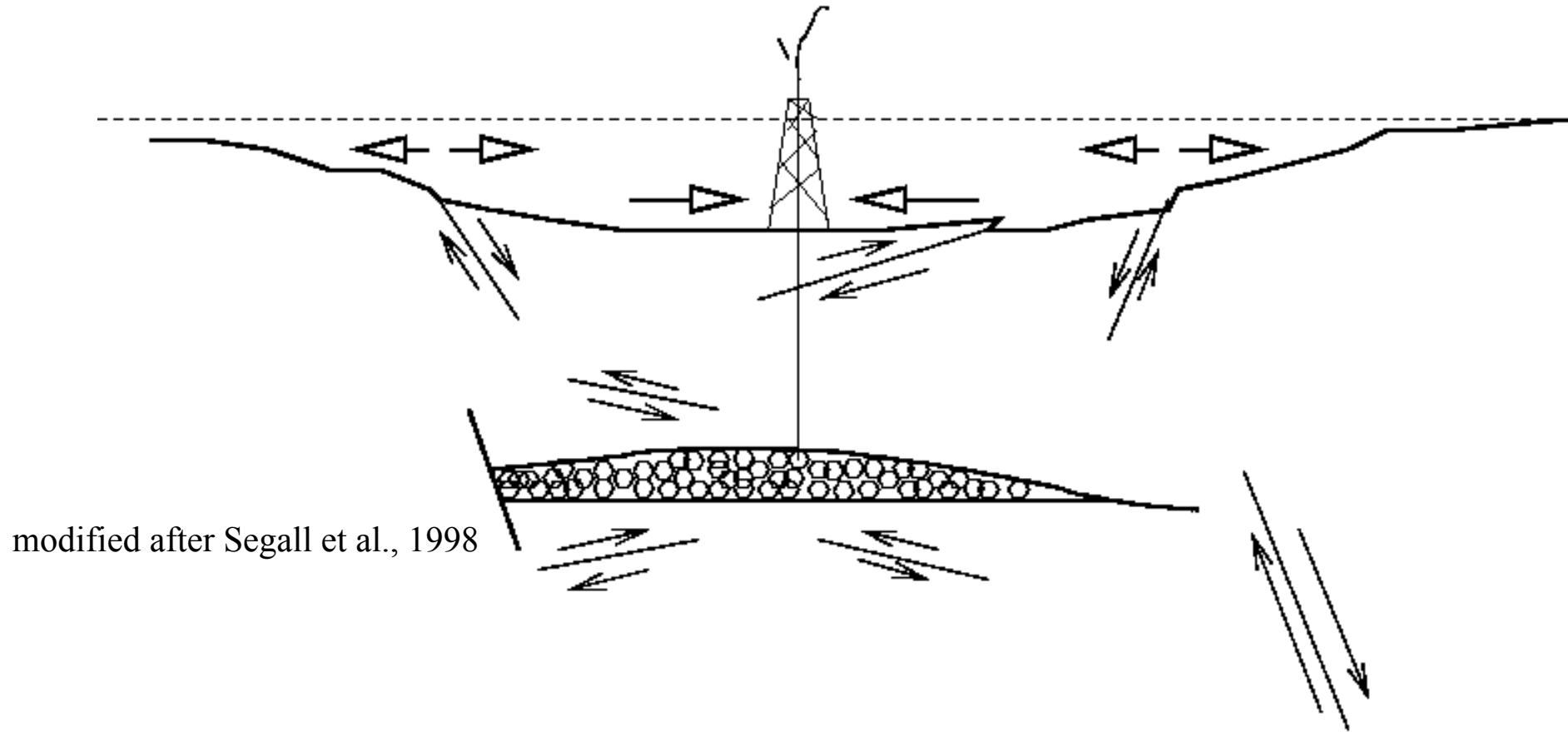
Gas field depletion



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Trigger potential outside the reservoir



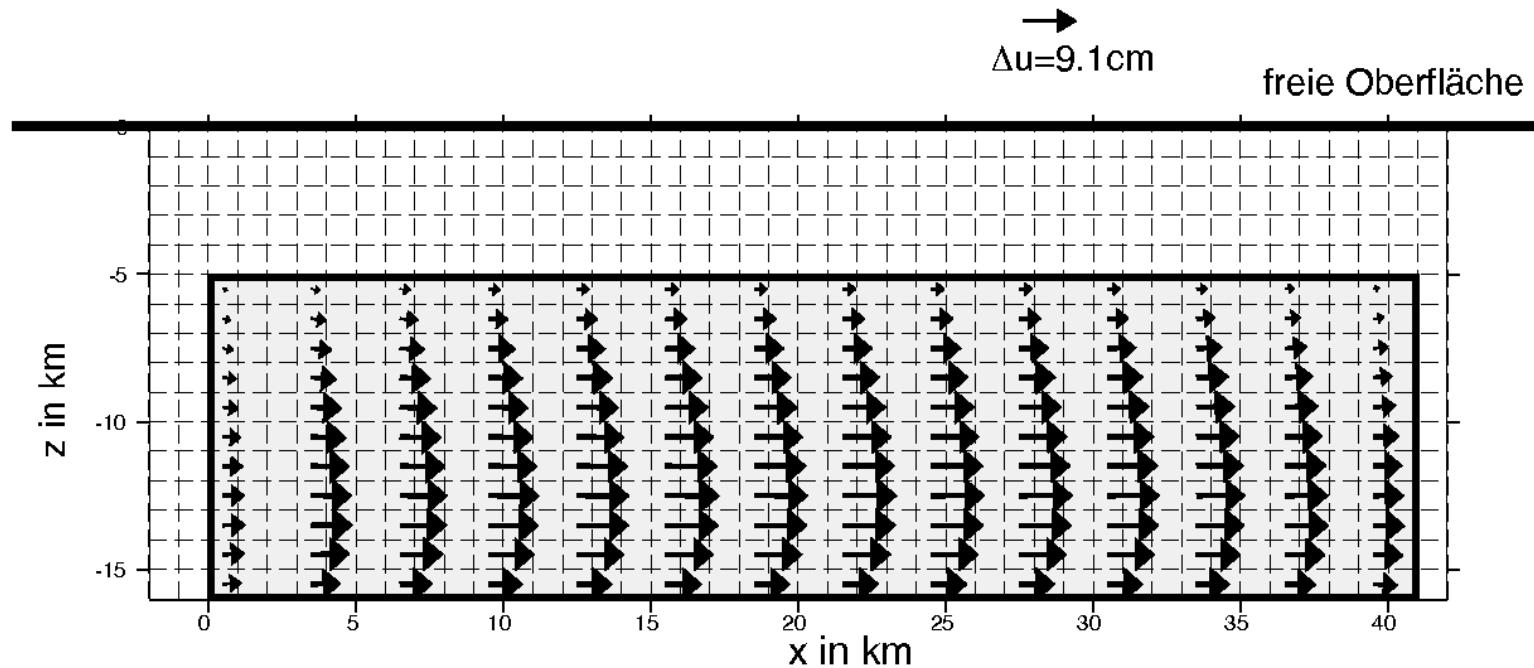
- Can distant earthquakes be triggered and what is mechanical evidence?
- Can seismic trigger potential be estimated ?

Outline

1. numerical method to calculate subsidence and stress
2. kinematic rupture of induced earthquakes
3. comparison of rupture and stress field

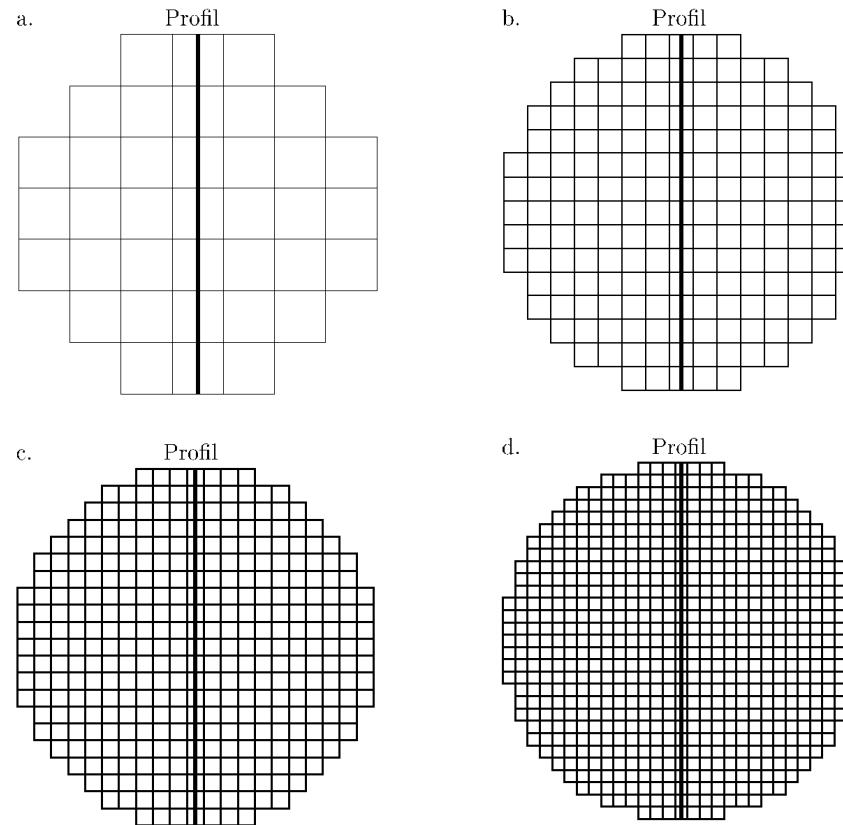


3D boundary element method (in-house)

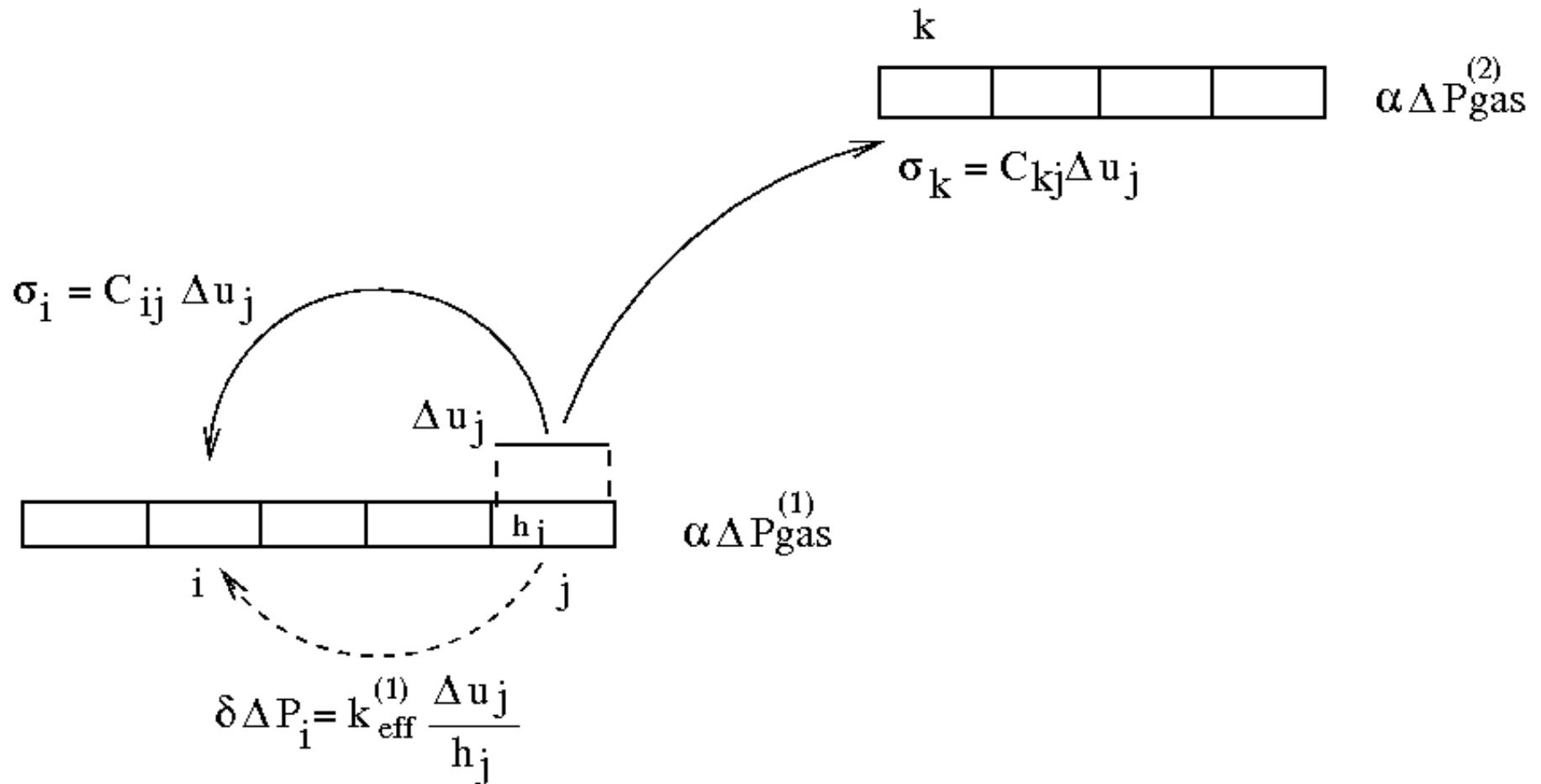


shear stress linearly
growing with depth

Simulation of deflating penny shaped cracks

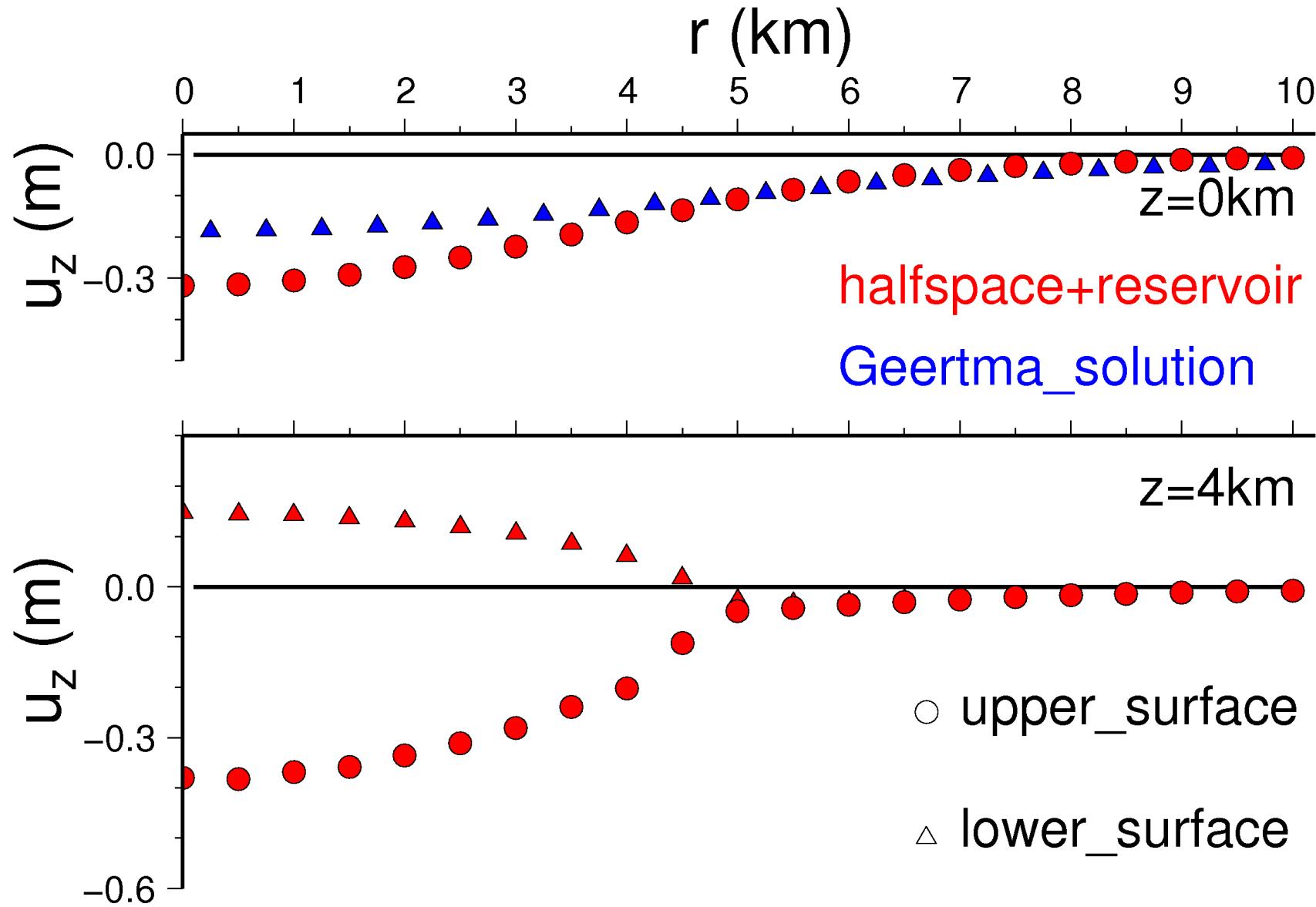


Accounting for internal porous field effect

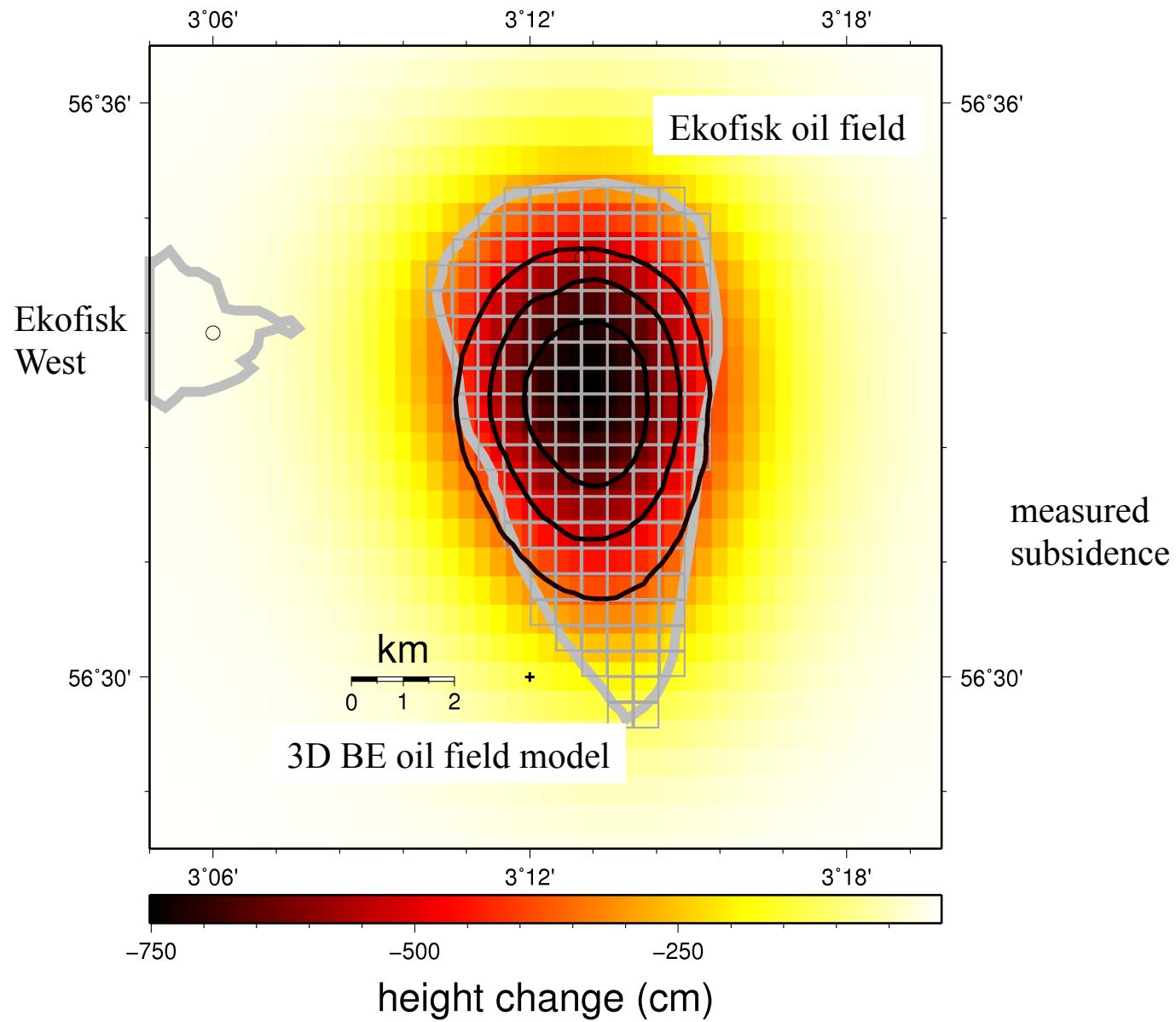


Comparison to Geertma's disk reservoir

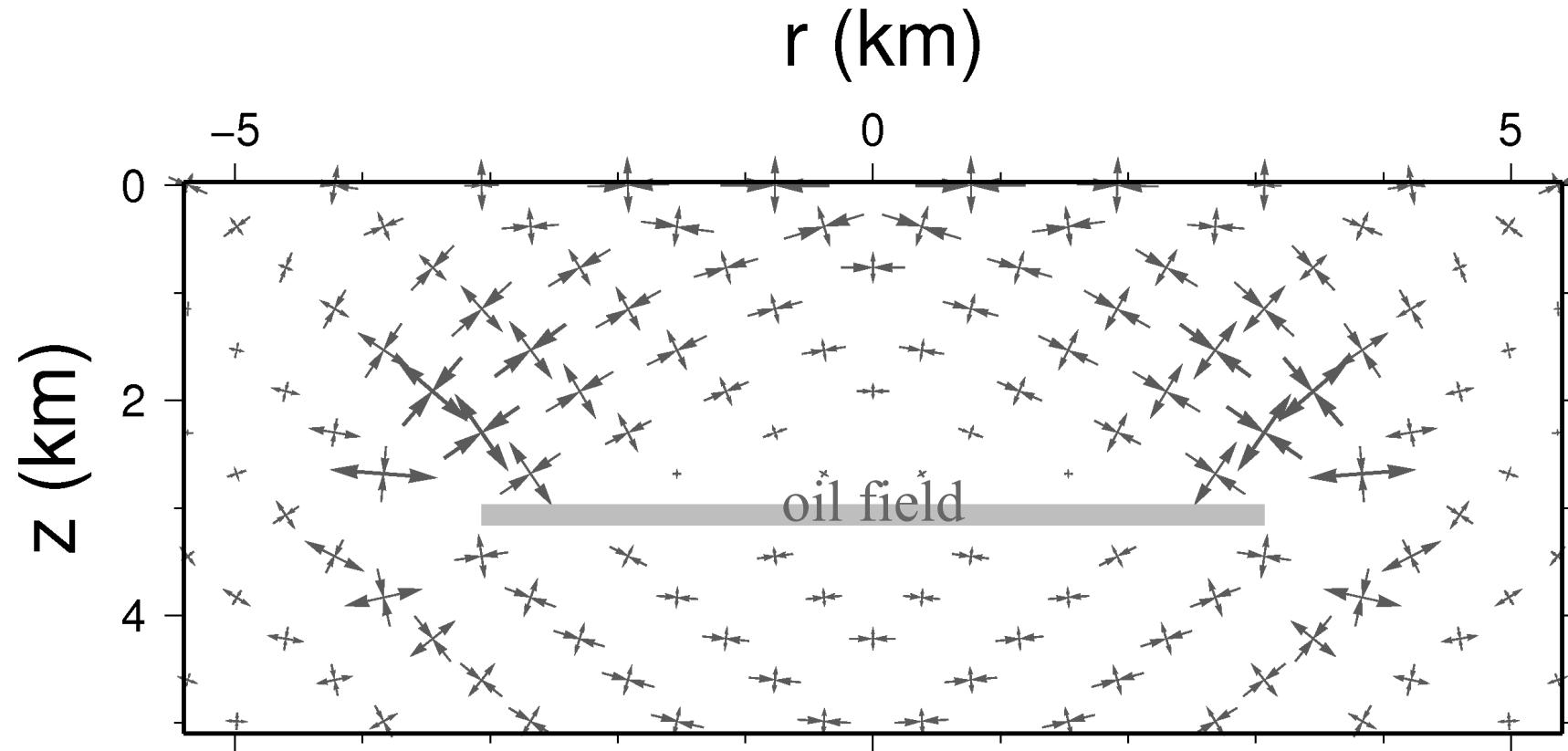
$z=4\text{km}$, $h=200\text{m}$, $\Delta P=30\text{MPa}$, $k=16\text{GPa}$, $\alpha=1$



The Ekofisk oil field subsidence bowl

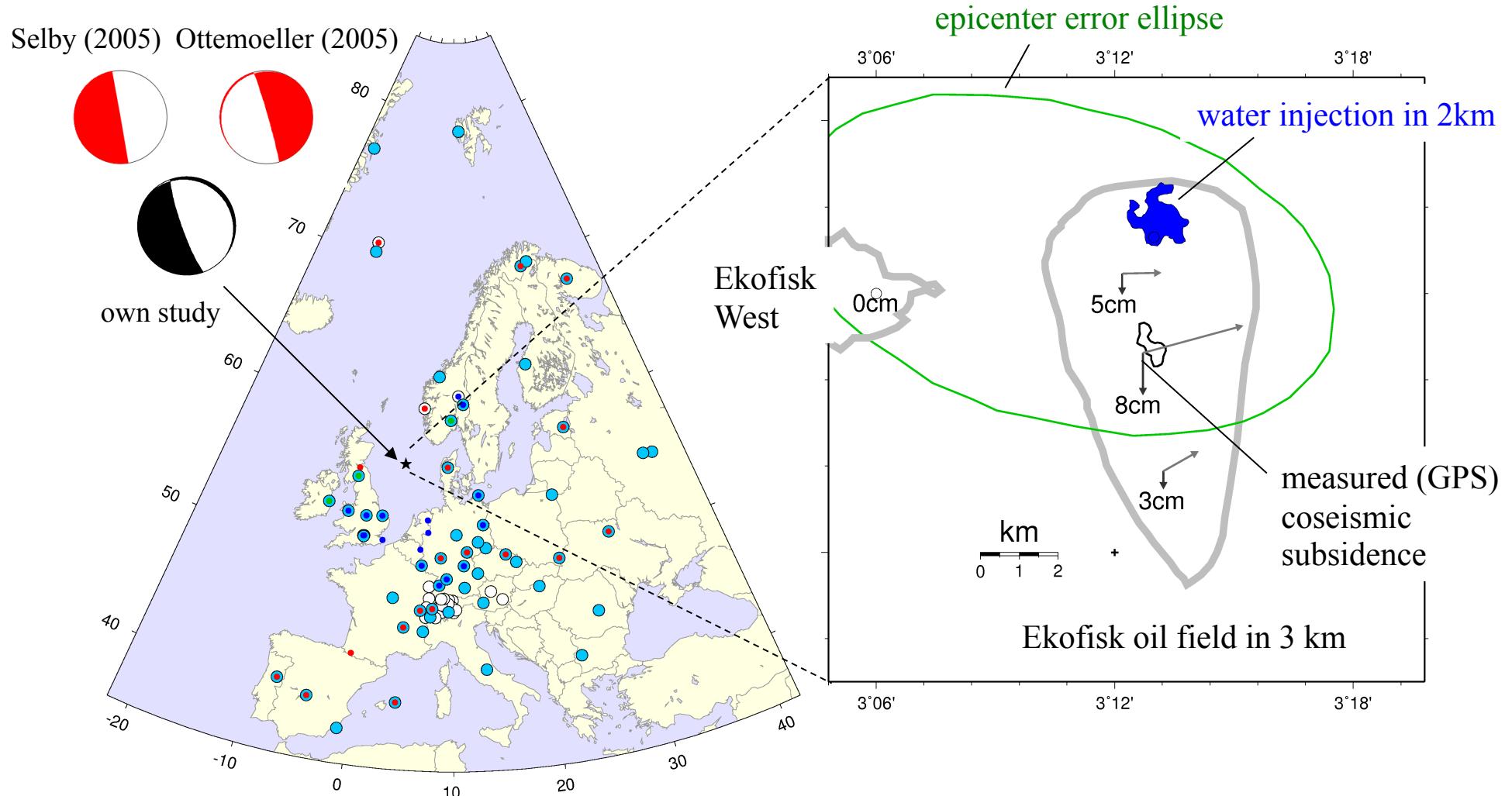


Ekofisk: Depletion induced stress



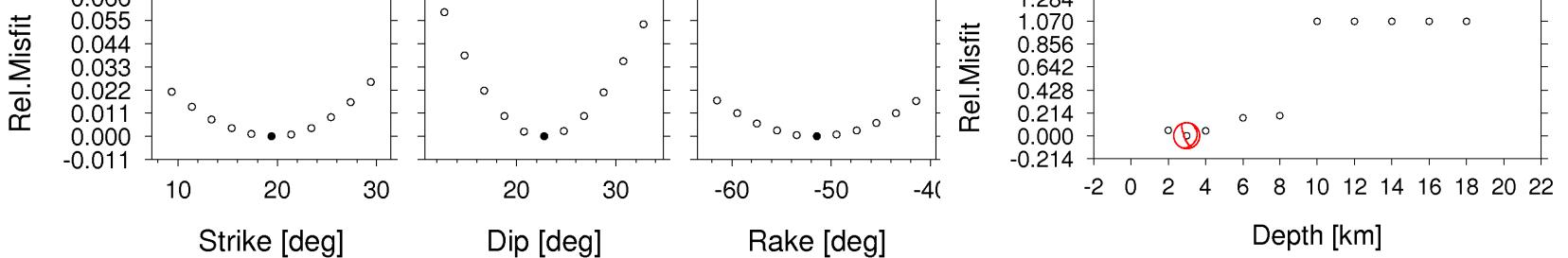
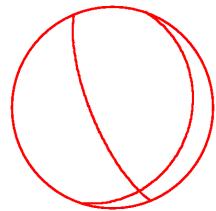
depletion-induced stress

The Ekofisk 2001 M 4.2 induced earthquake

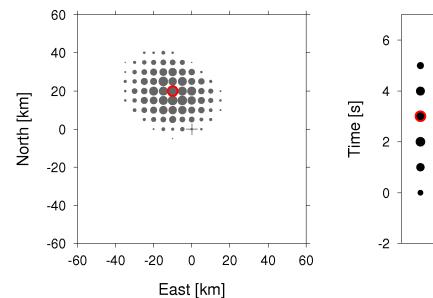
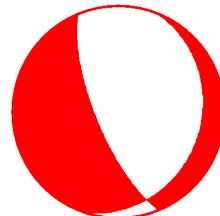


Multi-step amplitude spectra / full waveform inversion

Step 1 Focal mechanism, Depth, M_0 (from amplitude spectra)



Step 2 sense of slip, centroid location, apparent duration (from waveforms)



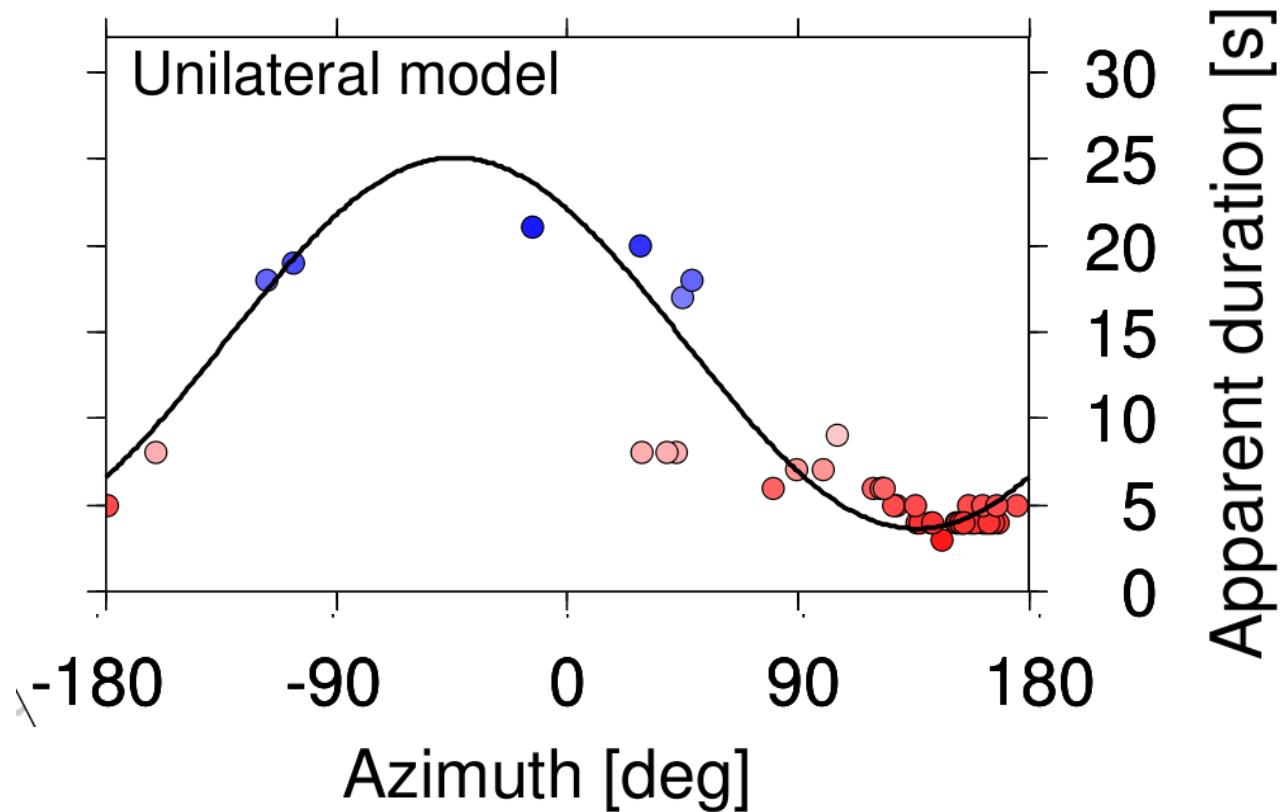
CMT inversion, KINHERD-KIWI project (Uni Hamburg, Uni Potsdam, GFZ, BGR)
Directivity, method



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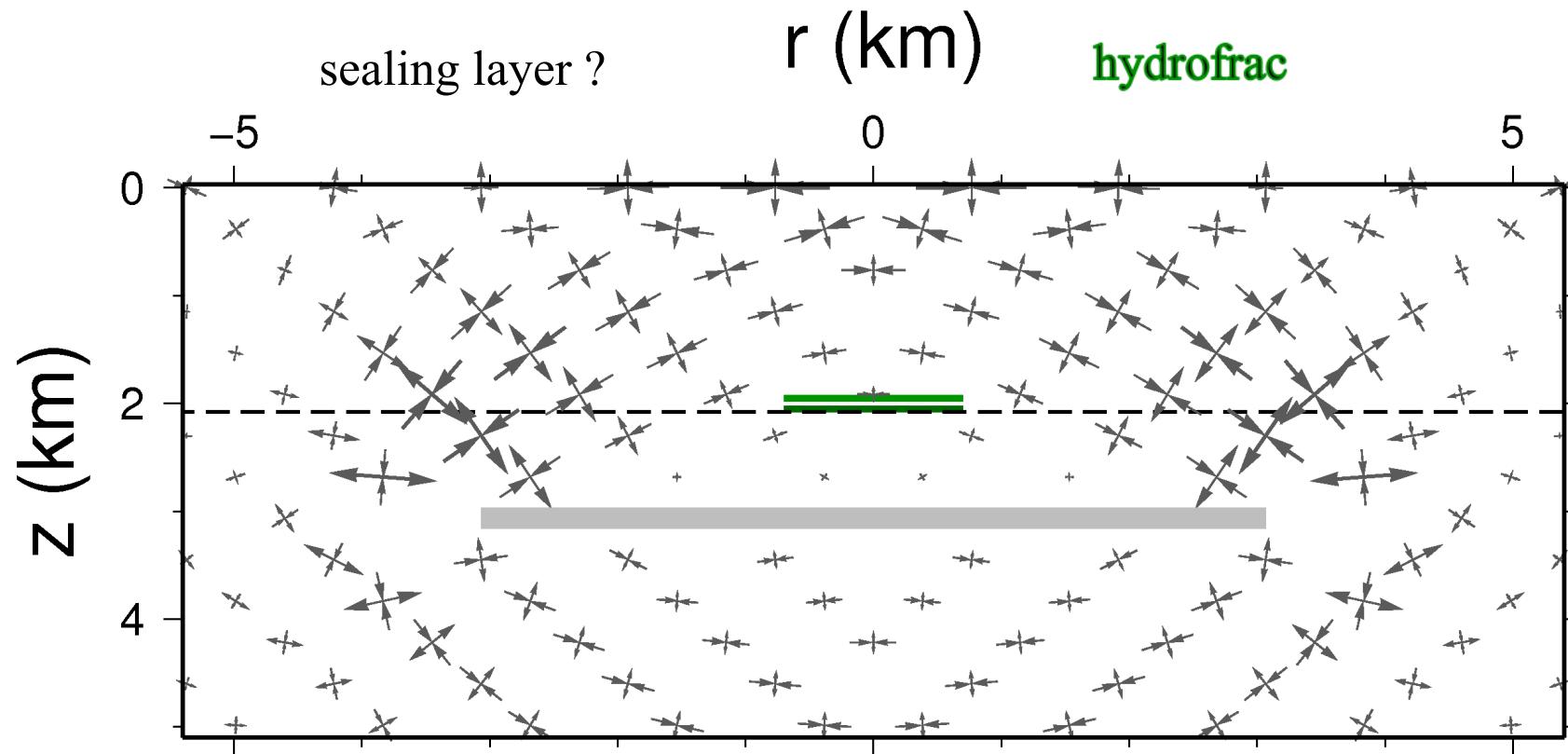


Unidirectional rupture in 140°



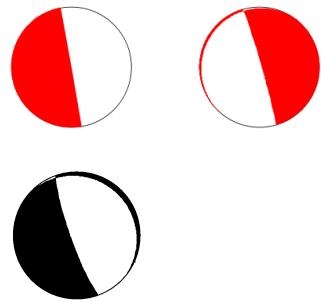
Cesca et al., in preparation

Was the earthquake triggered by the pre-seismic hydrofrac in 2 km depth

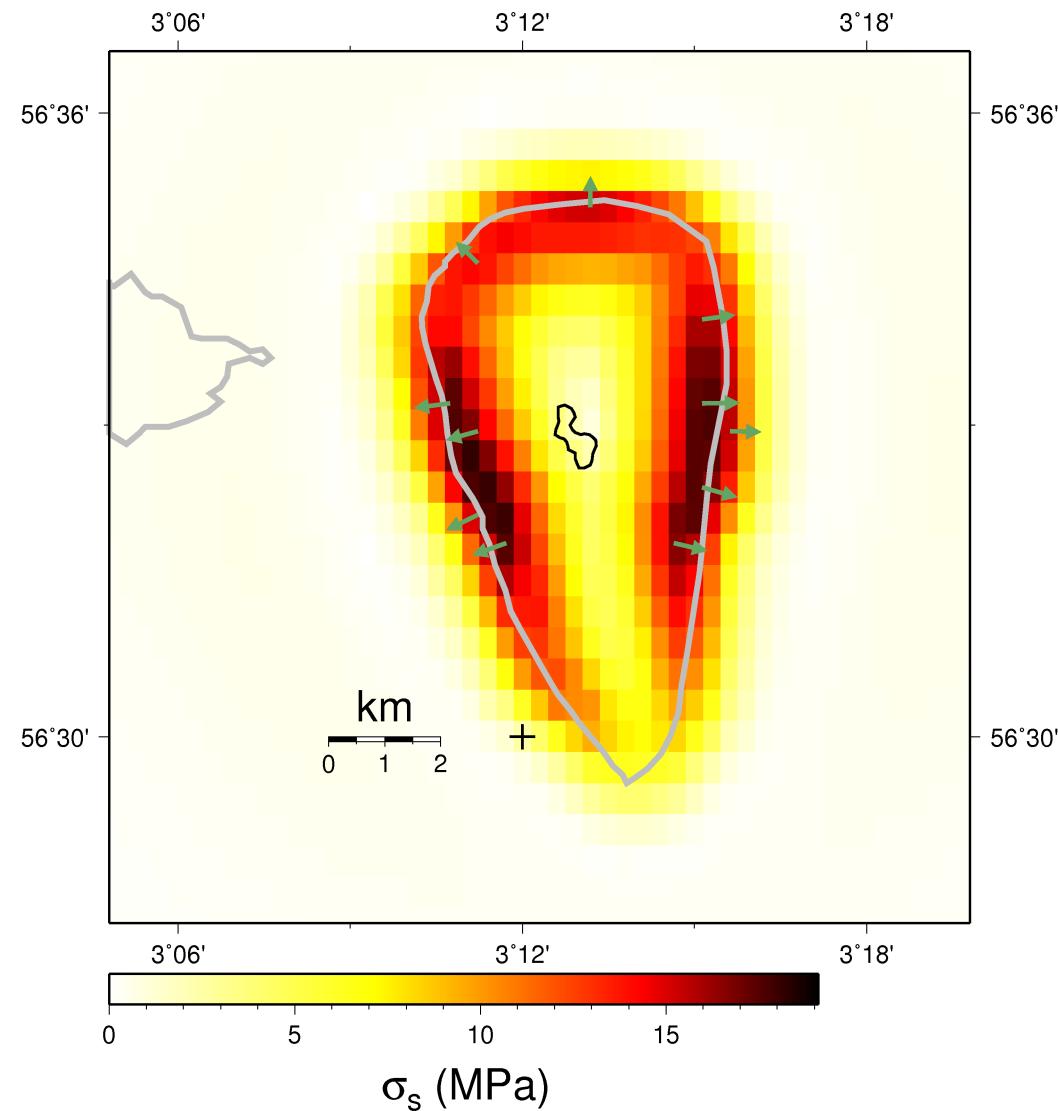


Ekofisk: Depletion induced shear stress in 2 km depth

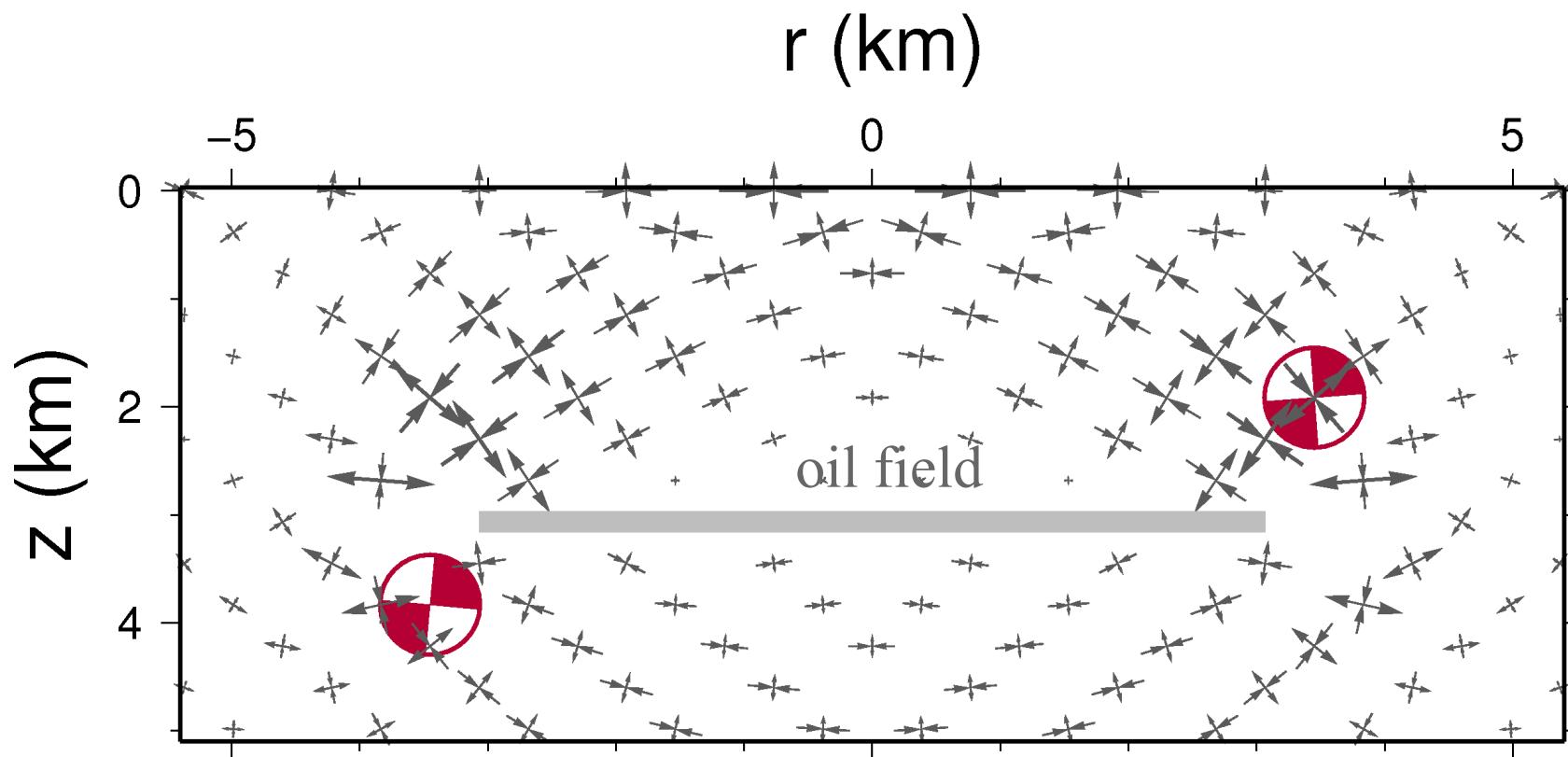
Selby (2005) Ottemoeller (2005)



own study

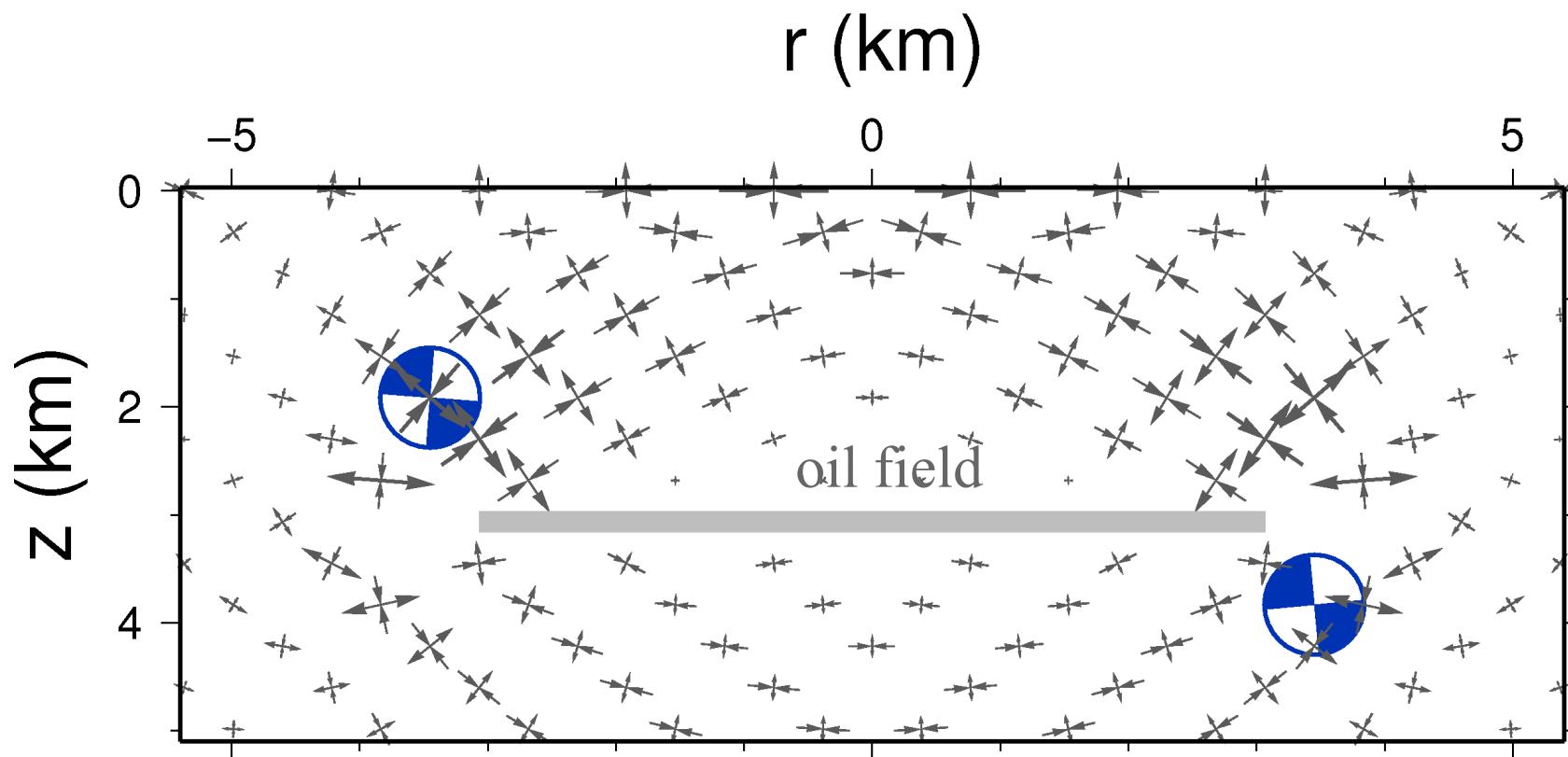


Possible location of the earthquake



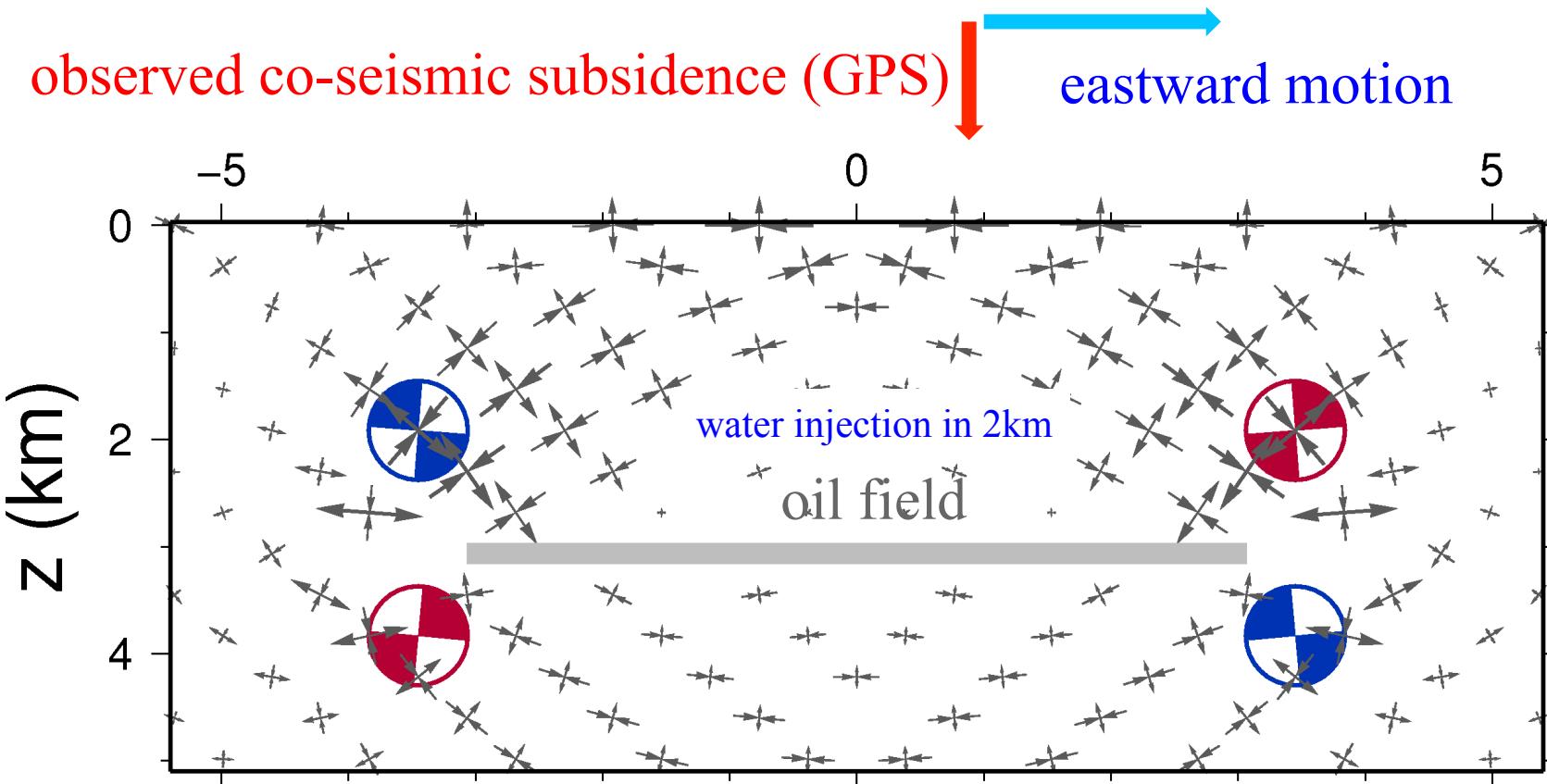
own study and Selby et al. (2004)

Possible location of the earthquake

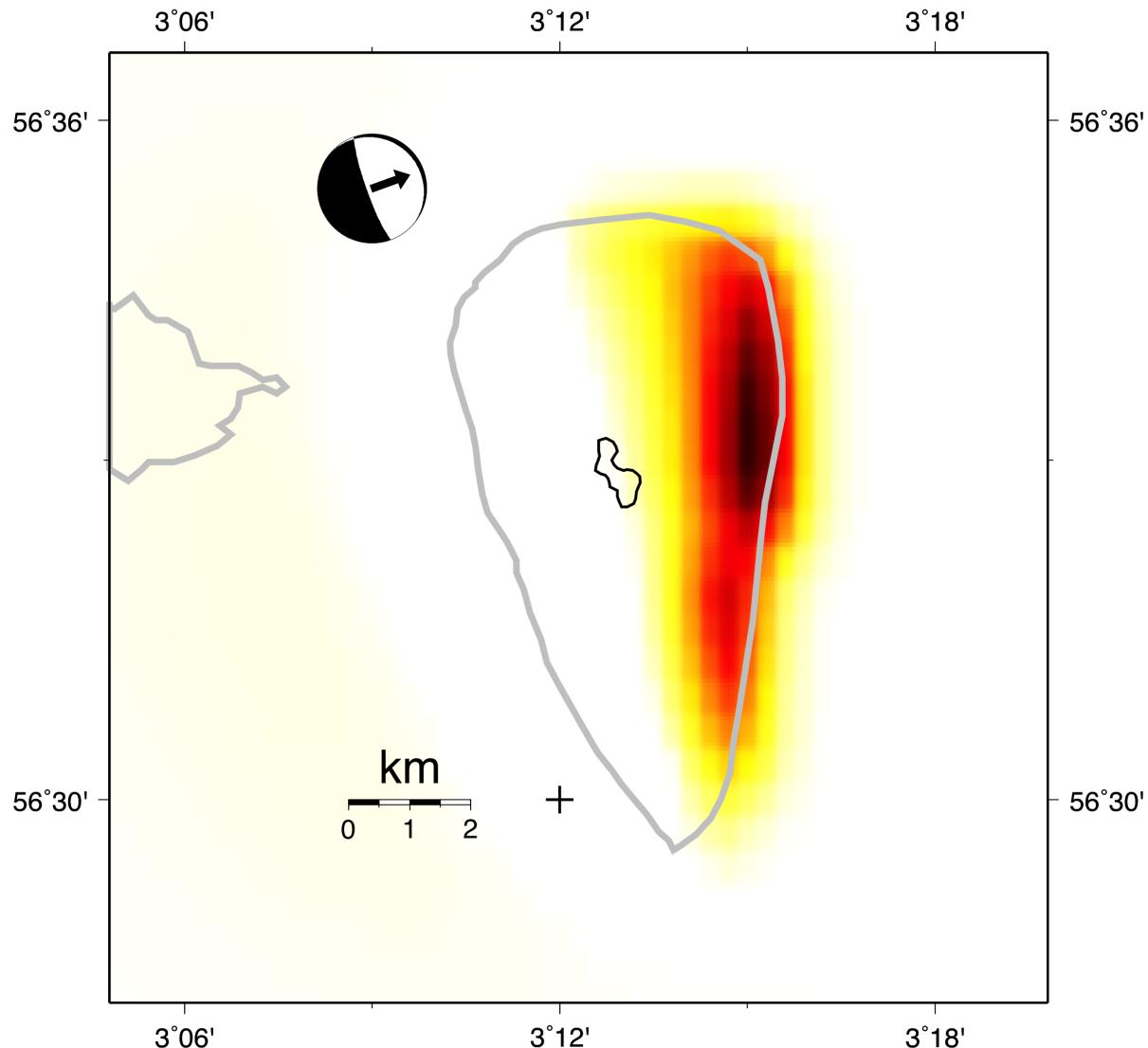


Ottemöller et al. (2004)

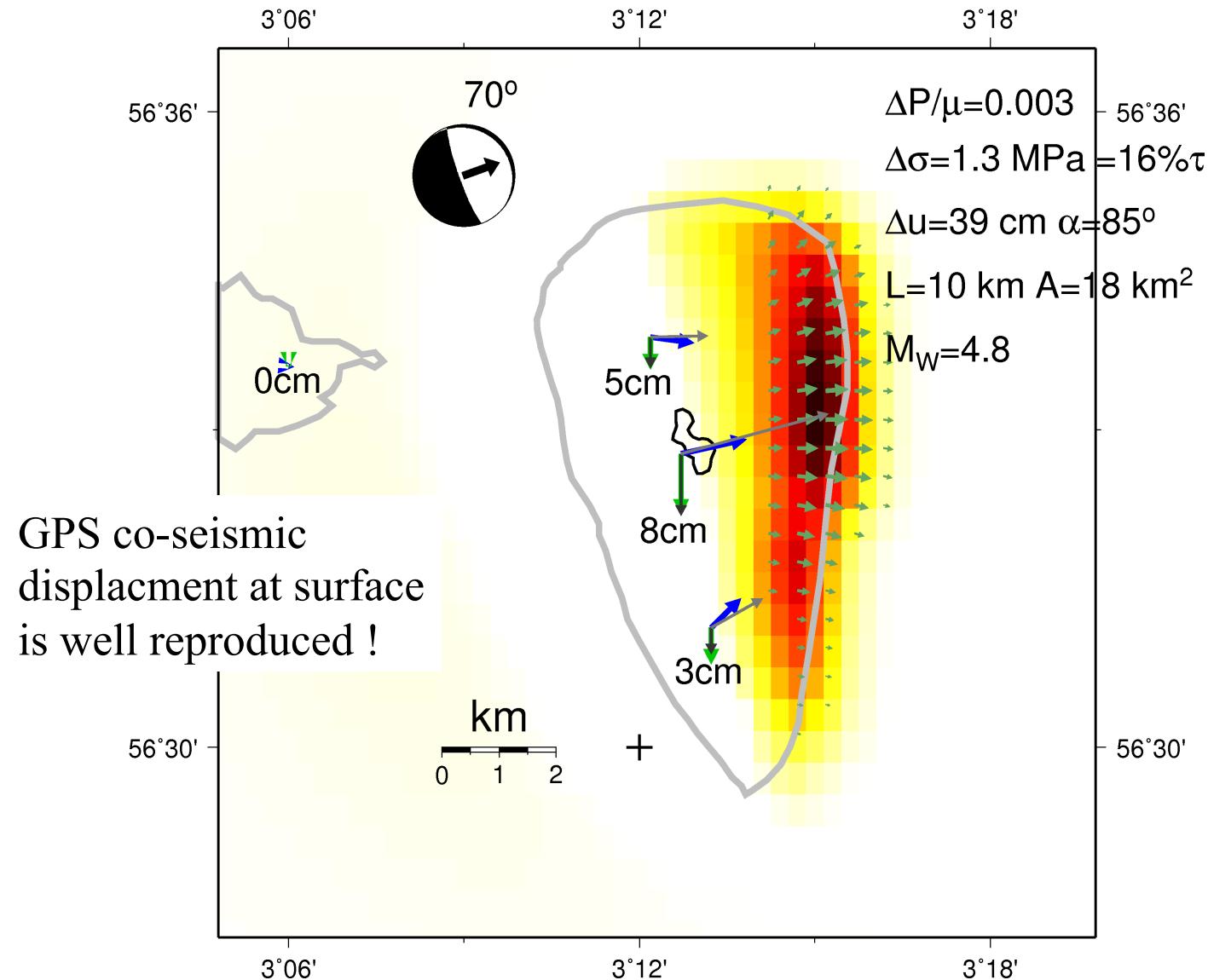
Co-seismic displacement (GPS) verifies eastern border solution in 2 km depth



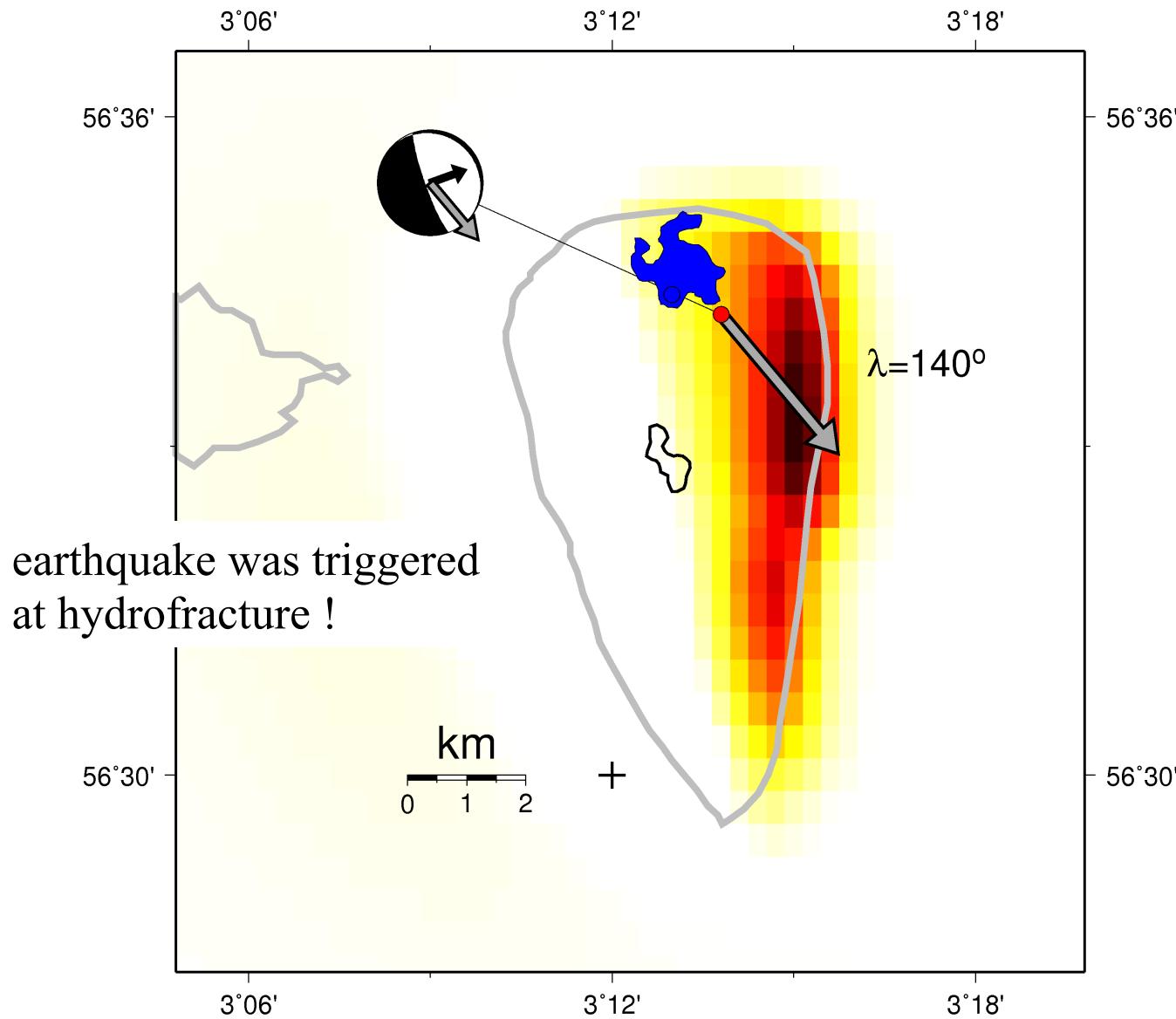
Shear stress resolved in slip direction



BE modeling of fault slip on patch of high shear stress



Rupture propagated “downhill” towards patch of high stress



Conclusion Ekofisk study

- Source mechanism, rupture plane, epicenter, centroid and rupture direction is resolved
- The Ekofisk earthquake was possibly fluid-triggered
- The rupture in 2 km was driven by field-induced shear stress
- Rupture propagation towards high stress regions
- The modeling of “resolved Coulomb stress” is a valid approach to discriminate induced, triggered and natural earthquakes

Overall summary

- Induced and triggered seismicity has many causes and is often difficult to distinguish from natural seismicity
- It is not sufficient to correlate a loading cycle with earthquake statistical parameter. A time dependent stress model is needed to strengthen the trigger hypothesis
- Natural fluid-induced seismicity can be used to study the intrusion parameter
- Many tools are needed to study triggered and induced seismicity (relative location and depth studies, source mechanism, modeling of fluid diffusion, intrusion, depletion related stress changes)

supplement material

- lecture III: techniques (relative location and relative moment tensor inversion)
- plotting moment tensors: New Package MOPAD by Krieger & Heimann (2010)

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